

G~178

PASTS

FIELD BOOK

No. 385

Page 28 - TIES FANDOSA

45 TIE IF 7 LINE IN
MONTALVO

89¢ 51-30

| | |
|------|-------|
| 3664 | 21000 |
| 1830 | 1830 |
| 2700 | 2700 |
| 2562 | 2562 |

3664

1600
1264

1360
1098

2620
2562

580

| | |
|------|------|
| 1280 | 1280 |
| 1098 | 1098 |
| 23 | 23 |
| 1182 | 1182 |

Indexed
c.s.k.

72 LX 27 } B.C.
49 RT }

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

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THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

MICROFILMED

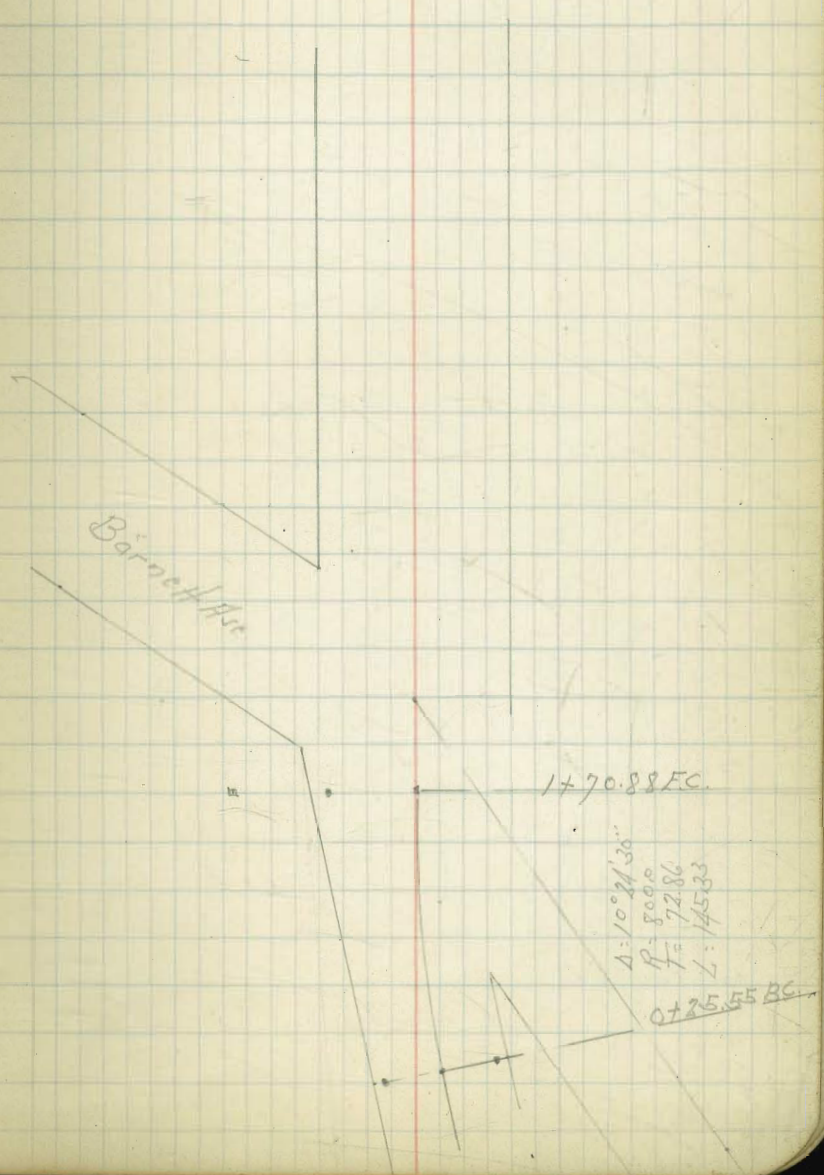
APR 12 1965

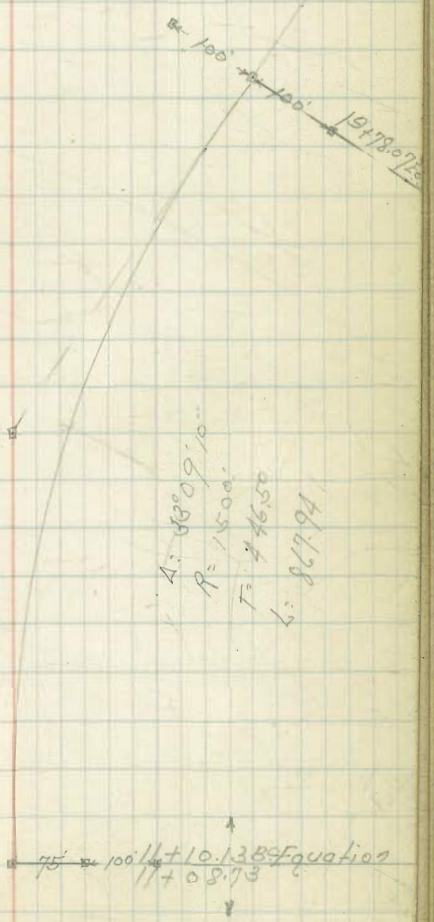
B.M. page 35

Location
Montalvo

Page
~~30~~ 40

3-3-33
Mason
S10507
Northampton





8-23

4

100 100 29+04.65 EC.

75320
1500
77946
8081

100 100 26+15.57 BC.

3970353 POT 90 100

~~U.S. Gov. Dyke 100' 100' 100' 100' 100'~~
 60765-10 P.O.T.
 30679

2 ATTACHED

18+6846 EC 100' 100'

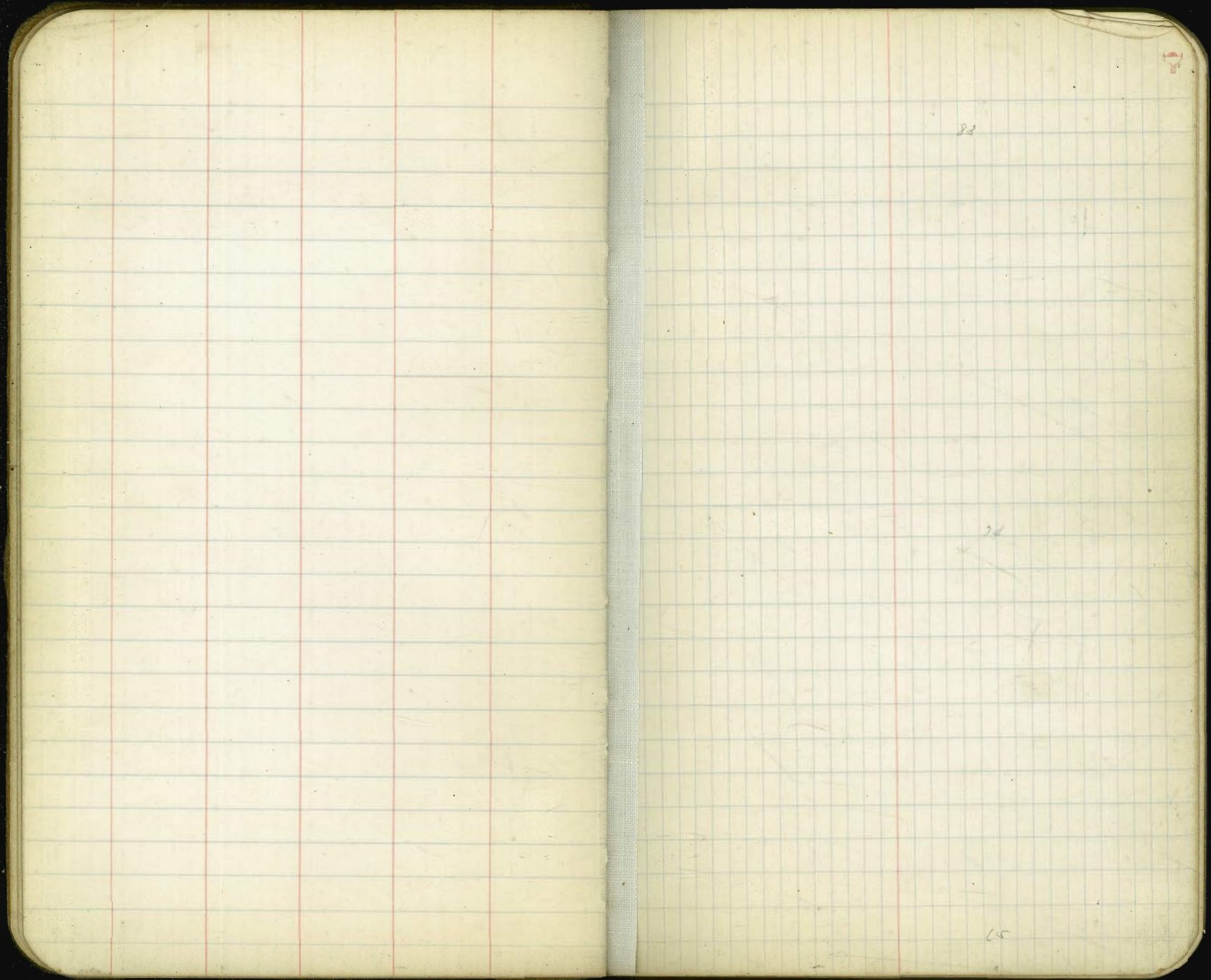
A = 7° 33' 20"

P = 1500'

T = 99.05

L = 197.80

11+7066 BC 100' 100'



7

22

22

25

100

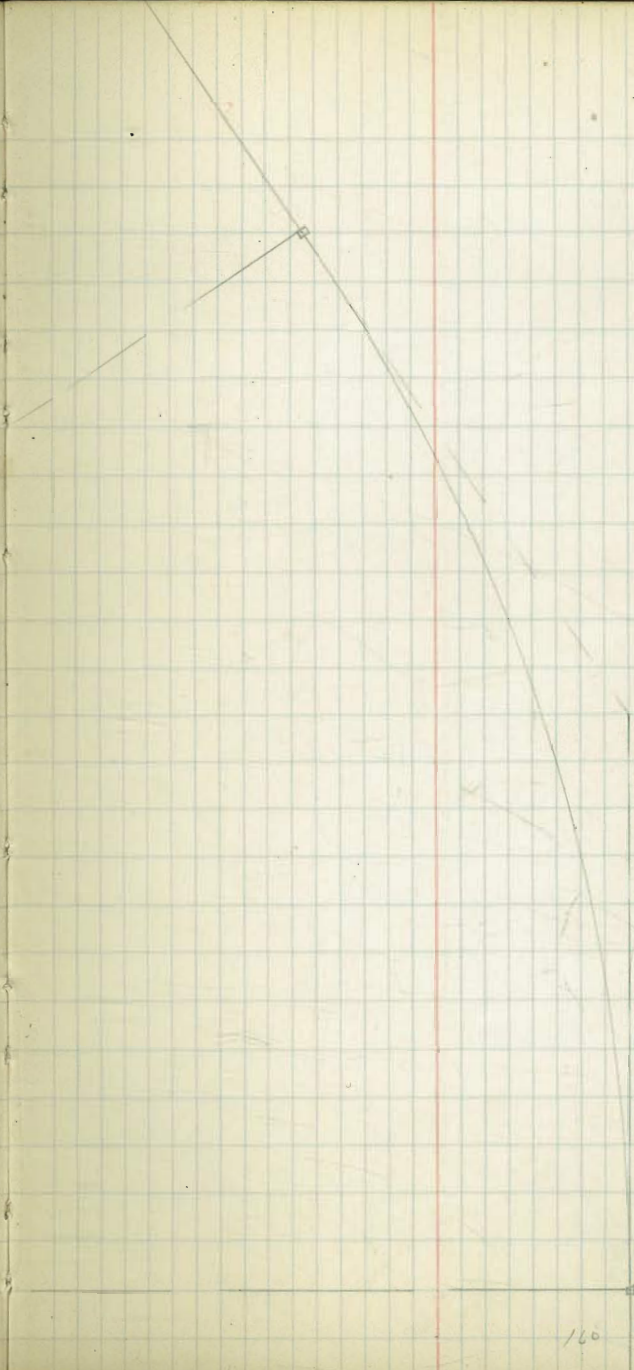
81

11

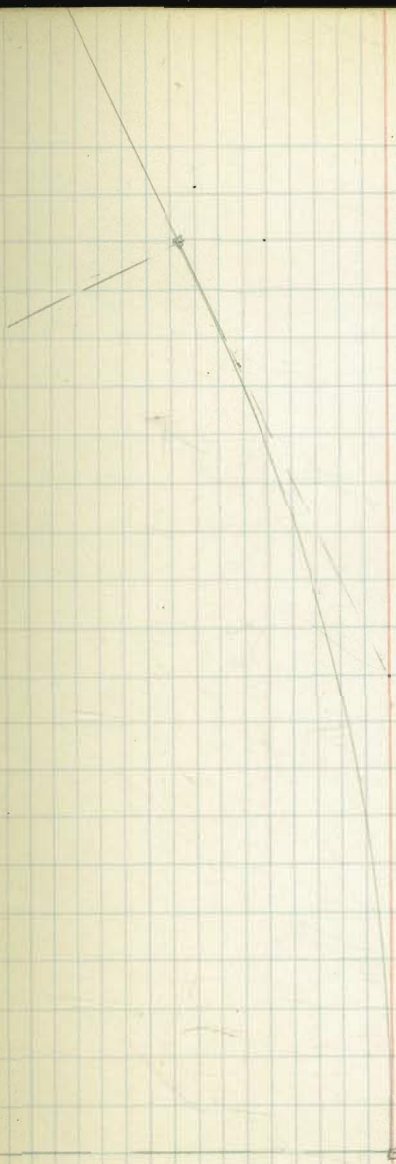
108

109

110



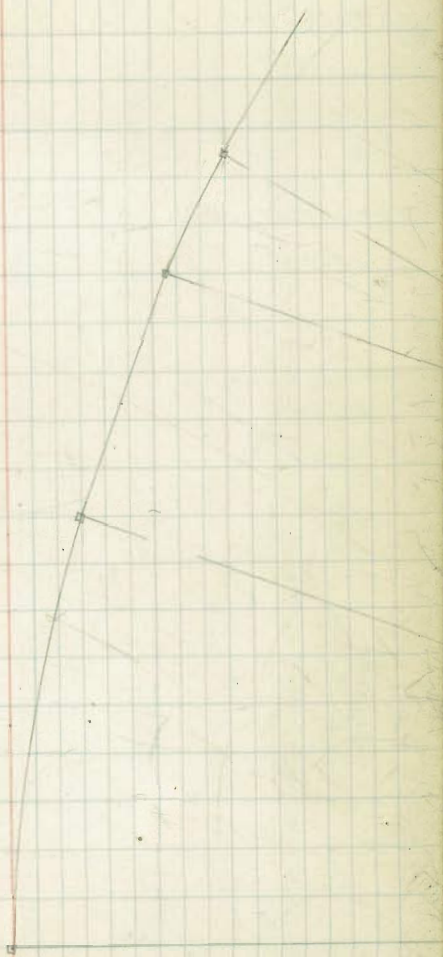
160



225

219

210



Indexed
a. s. k.

| | Lt | L | Rt |
|---------------------|----|------|------|
| 2+60 = F.V.C. | | 2.38 | 1.78 |
| 2+30 | | 2.44 | 1.84 |
| 2+0 = R.P.C. casing | | 2.46 | 1.86 |

16

| Lt | Rt |
|---------|--------------------|
| | $\frac{5.5}{2.0}$ |
| | 13.5 |
| | 34.0 |
| 4.0 | |
| outrock | $\frac{5.40}{2.0}$ |
| | 1.05 |
| | 24.0 |
| 5.4 | |

BM 7 - 0.46
 $\frac{7.40}{7.24}$

3.7.33
Morrison
Northey **17**

| | | Lt. | S | Rt. | | Lt. | S | Rt. |
|------|------|-------|------|------|--|-----------------------------|---|-----------------------------|
| 9+10 | EVC- | 1.60 | 2.50 | 1.90 | | 3.8 5.3 -1.5 36.0 | | 3.5 6.1 -2.6 30.4 |
| +60 | | 1.70 | 2.60 | 2.00 | | 3.7 5.1 -1.4 35.6 | | 3.6 6.0 -2.4 31.6 |
| 8+10 | | 1.73 | 2.63 | 2.03 | | 3.7 5.1 -1.4 34.9 | | 3.4 6.0 -2.6 31.6 |
| +60 | | 1.70 | 2.60 | 2.00 | | 3.70 5.1 -1.4 35.4 | | 3.4 6.0 -2.6 31.6 |
| 7+10 | PVC | 1.61 | 2.51 | 1.91 | | 3.8 5.3 -1.5 35.2 | | 3.5 6.1 -2.6 31.2 |
| +55 | | 1.13 | 2.39 | 1.79 | | 6.1 4.9 +1.2 32.2 | | 5.5 6.5 -1.0 30.0 |
| 6+0 | | 0.99 | 2.25 | 1.65 | | 6.2 4.8 +1.4 33.7 | | 5.6 6.5 -0.9 30.0 |
| +50 | EVC | 0.86 | 2.12 | 1.52 | | 6.4 4.8 +1.6 34.0 | | 5.7 6.1 -0.4 33.4 |
| 5+0 | | 0.77 | 2.03 | 1.43 | | 6.5 4.7 +1.8 33.8 | | 5.6 6.5 -0.9 30.8 |
| +50 | | | 2.00 | 1.40 | | | | 5.8 6.2 -0.4 33.8 |
| 4+0 | | | 2.04 | 1.44 | | | | 5.8 6.1 -0.3 33.4 |
| +50 | PVC | | 2.14 | 1.54 | | | | 5.20 6.1 -0.9 30.8 |
| 3+0 | | -0.27 | 2.27 | 1.67 | | | | 5.6 6.5 -0.9 30.8 |

Hotel: Grade Change 0.25

50

| | | Lt | L | Rt | Lt | | Rt | |
|---------------------------|-----------|------|------|------|-------------------------|--|--|---|
| 750 | 8°24'012" | 4.17 | 2.97 | 2.17 | | $\frac{1.8}{4.2}$ $\frac{2.4}{7.0}$ | $\frac{3.8}{4.0}$ $\frac{1.0}{2.0}$ | $\frac{1.5}{5.7}$ $\frac{1.0}{6.7}$ $\frac{0.3}{7.5}$ |
| 15+0 | 7°26'435" | 4.05 | 2.85 | 2.05 | | $\frac{1.9}{4.2}$ $\frac{2.2}{7.2}$ | $\frac{3.9}{4.0}$ $\frac{1.0}{2.0}$ | $\frac{1.5}{5.9}$ $\frac{1.0}{6.9}$ $\frac{0.3}{7.9}$ |
| 750 | 6°29'258" | 3.92 | 2.72 | 1.92 | | $\frac{2.1}{4.2}$ $\frac{2.1}{7.2}$ | $\frac{1.0}{4.0}$ $\frac{1.0}{2.0}$ | |
| 14+0 | 5°32'081" | 3.80 | 2.60 | 1.80 | | $\frac{2.3}{4.2}$ $\frac{1.7}{7.2}$ | $\frac{1.2}{4.0}$ $\frac{1.3}{2.0}$ | |
| 750 | 4°34'504" | 2.67 | 2.47 | 1.67 | | $\frac{1.2}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.3}{4.0}$ $\frac{1.0}{2.0}$ | $\frac{1.5}{5.7}$ $\frac{1.0}{6.7}$ $\frac{0.3}{7.5}$ |
| 13+0 | 3°37'327" | 3.55 | 2.35 | 1.55 | | $\frac{2.2}{4.2}$ $\frac{2.0}{7.2}$ | $\frac{1.2}{4.0}$ $\frac{1.0}{2.0}$ | |
| 750 | 2°40'15" | 3.42 | 2.22 | 1.42 | | $\frac{1.0}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.1}{4.0}$ $\frac{1.0}{2.0}$ | |
| 12+10.13 | 1°54'354" | 3.32 | 2.12 | 1.32 | | $\frac{2.6}{4.2}$ $\frac{2.2}{7.2}$ | $\frac{1.1}{4.0}$ $\frac{1.0}{2.0}$ | |
| 11+6°13 | 57'177" | 3.06 | 2.03 | 1.24 | | $\frac{2.6}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.1}{4.0}$ $\frac{1.0}{2.0}$ | 1.42 |
| 11+10.13 11+08.73 B.C. | | 2.49 | 1.99 | 1.26 | See page 35 11+11.58 | $\frac{2.0}{4.2}$ $\frac{2.0}{7.2}$ | $\frac{1.1}{4.0}$ $\frac{1.0}{2.0}$ | |
| 10+58.73 | | 1.81 | 2.01 | 1.35 | | $\frac{2.6}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.1}{4.0}$ $\frac{1.0}{2.0}$ | |
| 10+08.73 | | 1.37 | 2.10 | 1.48 | | $\frac{1.1}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.0}{4.0}$ $\frac{1.0}{2.0}$ | |
| 9+58.73 | | 1.35 | 2.25 | 1.65 | | $\frac{1.1}{4.2}$ $\frac{1.0}{7.2}$ | $\frac{1.0}{4.0}$ $\frac{1.0}{2.0}$ | |

| | U. | Z | P. |
|------------------------------|------|------|------|
| 21+50 | | 2.73 | |
| 21+28.07 End Transition 1.88 | | 2.78 | 2.18 |
| 20+78.07 | 2.29 | 2.91 | 2.29 |
| 20+28.07 | 2.83 | 3.03 | 2.37 |
| +78.07 EC 16°34'35" | 2.66 | 3.16 | 2.43 |
| 19+28.07 15°37'17" | 4.31 | 3.28 | 2.50 |
| 19+50 E.V.C. | | | |
| +78.07 14°39'58" | 4.59 | 3.39 | 2.59 |
| +50 14°07'48" | 4.64 | 3.44 | 2.64 |
| 18+0 13°10'30" | 4.68 | 3.48 | 2.68 |
| +50 12°13'12" | 4.64 | 3.44 | 2.64 |
| 17+0 P.V.S 11°15'54" | 4.55 | 3.35 | 2.55 |
| +50 10°18'36" | 4.42 | 3.22 | 2.42 |
| 16+0 9°21'18" | 4.30 | 3.10 | 2.30 |

5907
432
7.20
16.40

47
46
45
44

3.7
3.6
3.5
3.4

| | Lt | L | Rt |
|------------------------|------|------|------|
| 27+5738 | 2.53 | 2.50 | 1.71 |
| 27+1011 | 2.58 | 2.38 | 1.58 |
| 26+6284 | 2.29 | 2.26 | 1.47 |
| 26+1557-BC | 2.64 | 2.14 | 1.41 |
| 26+0 PVC | | | |
| 25+6230 | 1.85 | 2.05 | 1.39 |
| 25+2102 | 1.27 | 2.00 | 1.38 |
| 24+7376. Pind/Torridos | 1.09 | 1.99 | 1.39 |
| 24+50 | | 2.00 | |
| 24+0 PVC | | 2.10 | |
| +50 | | 2.23 | |
| 23+0 | | 2.35 | |
| +50 | | 2.48 | |
| 22+0 | | 2.60 | |

| | ht | h | PL |
|-----------------|------|------|------|
| 34+0 | | 4.11 | |
| +50 | | 3.99 | |
| 33+0 | | 3.86 | |
| +50 | | 3.74 | |
| 32+0 | | 3.61 | |
| +50 | | 3.49 | |
| 31+0 | | 3.36 | |
| +50 | | 3.24 | |
| 30+0 | 2.21 | 3.11 | 2.51 |
| 29+46.46 FT. on | 2.09 | 2.99 | 2.39 |
| 28+99.19 | 2.13 | 2.86 | 2.24 |
| 28+51.92 | 2.54 | 2.74 | 2.08 |
| 28+04.65-FC | 2.12 | 2.62 | 1.89 |

| | lt | z | Pl |
|--------------|----|------|----|
| 40+50 | | 4.21 | |
| 40+0 | | 4.34 | |
| +50 | | 4.47 | |
| 39+0 | | 4.60 | |
| +50 F.V.C. | | 4.73 | |
| 38+0 | | 4.83 | |
| +50 | | 4.86 | |
| 37+0 | | 4.83 | |
| +50 - P.V.C. | | 4.74 | |
| 36+0 | | 4.61 | |
| +50 | | 4.49 | |
| 35+0 | | 4.36 | |
| 34+50 | | 4.24 | |

| | Lt | L | Rt |
|---------------|----|------|----|
| 46+70.6680 | | 2.86 | |
| 46+21.21 | | 2.83 | |
| +71.76 | | 2.87 | |
| +50 P.V.C. | | 2.91 | |
| +22.31 P.Tray | | 2.98 | |
| 45+0 | | 3.04 | |
| +50 | | 3.17 | |
| 44+0 | | 3.20 | |
| +50 | | 3.43 | |
| 43+0 | | 3.56 | |
| +50 | | 3.69 | |
| 42+0 | | 3.82 | |
| +50 | | 3.95 | |
| 41+0 | | 4.08 | |

H L PA

50+16.81 ETCAN.

49+75 - P.V.C.

49+67.36

4.07

49+17.91

3.85

48+68.46 EC

3.63

48+19.01

3.41

47+69.56

3.19

47+50 ETC

2.10

47+20.11

2.96

Indexed
C.S.K.

Water Grades
35th & Pigel. Newton to Man
6" Line

with 4' flat
S.E. Hyd.

51 Newton 100

30.80 ✓

4119

609

44.28

10.79

33.49

37.64

11.50

26.34

7.4

8.0

8.6

9.2

9.8

10.4

10.9

11.5

1.3

2.1

3.8

4.5

4.8

5.5

6.3

5.7

+6.1

+6.0

+4.8

+4.7

+5.0

+4.9

+4.6

+5.8

+50

30.20 ✓

1

29.62 ✓

37.64

11.50

26.34

11.8

12.7

13.1

13.3

13.6

14.7

9.7

6.2

7.3

7.4

8.5

8.5

9.6

10.7

+5.4

+4.6

+5.7

+4.9

+4.8

+4.5

+5.1

+50

29.04 ✓

T.P. Stub
6+50

2

28.45 ✓

14.6

15.2

16.6

17.3

18.7

19.7

20.3

21.8

+50

27.87 ✓

3

27.28 ✓

10.1

10.1

11.3

12.3

13.8

14.8

15.8

16.8

+4.5

+5.1

+4.3

+4.3

+4.3

+4.3

+4.3

+4.3

+50 = 6" x 6" Cross - Boston

26.70 ✓

N.E. Cor.
Curb Gr.

4

26.14 ✓

2980⁵³⁸
802
+2.34

+50

24.95 ✓

26.34 TP on 5' flat

887. 6.150

351.87

+76.5 = Gate Valve

24.50 ✓

5

24.30 ✓

+41 = 6" x 6" Cross - Acacia

24.00 ✓

S.E. Cor.
Curb Gr.

5

23.50 ✓

2670⁸⁴⁸
802
+0.45

+50.3 = 6" Bend

23.00 ✓

26.34 TP

0.85

27.19

+50

22.43 ✓

6

21.00 ✓

7.6

9.0

10.5

11.9

13.3

14.8

16.3

17.8

2.7

4.1

5.3

6.6

8.0

9.3

10.7

12.1

+4.9

+4.6

+4.2

+3.6

+4.0

+4.2

+4.2

+3.8

+50

19.57 ✓

7

18.14 ✓

+50

16.71 ✓

8

15.28 ✓

+20.3 = 6" x 6" Cross - Birch

13.00 ✓

S.E. Cor.
Curb Gr.

9

13.64 ✓

17.00^{10.19}
9.02
+0.27

Moore
Sisson
Northard
Walker
8/1/23
24
Oct. 30, 33

Nov. 5-33

10 +00 14.27
 +40.3 = P.K. 15.0
 +80.2 15.3
 11 +20.2 15.3
 +60.2 14.9
 12 +00.2 = EXC. 14.0
 +50 14.43
 14 +61.1 Gate Valve 17.08
 13 +11.1 = 6" x 6" Cross 11.00
 +41.1 = Gate Valve 9.88
 +46.1 = F.H. Tee 9.63
 14 7.68
 +50 5.82
 15 2.35
 +50 2.09
 16 0.32
 +51.1 = 6" Tee to West Bk -1.70
 17 +11.1 = 6" Tee to East -4.00
 +46.1 = F.H. Tee -3.21
 18 Bk 0 -2.00
 +50
 19
 +50
 20
 +36.1 = F.H. Tee -2.00

27.13T
 16.45
 TP 16.74
 8.86
 17.10T
 12.26
 12.4
 12.85
 5.09T

12.9 12.2 11.9 11.9 12.3 13.2 14.8 15.1
 9.1 8.3 7.3 6.8 7.0 7.5 8.8 8.9
 +3.8 +4.0 +4.7 +5.1 +5.3 +5.7 +6.3 +6.3

17.10T
 2.53
 8/14/57 10 1/4 Pipe
 SH. Co. Ho. med

6.1
 1.2
 +4.9

S = 0.04%

Bk 0

20 + 41.1 = Gate Valve - 2.0

+ 63.1 = N. edge paving

21 + 01.1 = Ex. Water Main

2' S of S edge paving

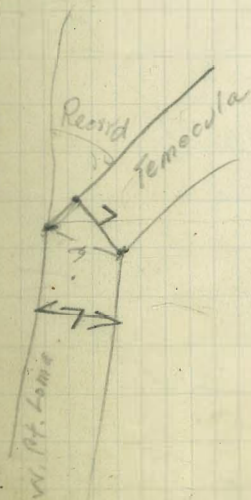
on Main St.

West Point Loma Blvd.
 Stovida Place to

| Sta | h.c. | z | S.L. |
|---------|-------|---|-------|
| 2+78.70 | 15.80 | | 16.00 |
| 2+38.70 | 15.80 | | 16.00 |
| 2+02.50 | 16.35 | | 16.50 |
| 1+62.50 | 17.25 | | 17.55 |
| 1+22.50 | 18.70 | | 19.35 |
| 0+82.50 | 20.80 | | 21.10 |
| 0+41.85 | 23.20 | | 23.45 |
| 0+0 | 25.60 | | 25.80 |

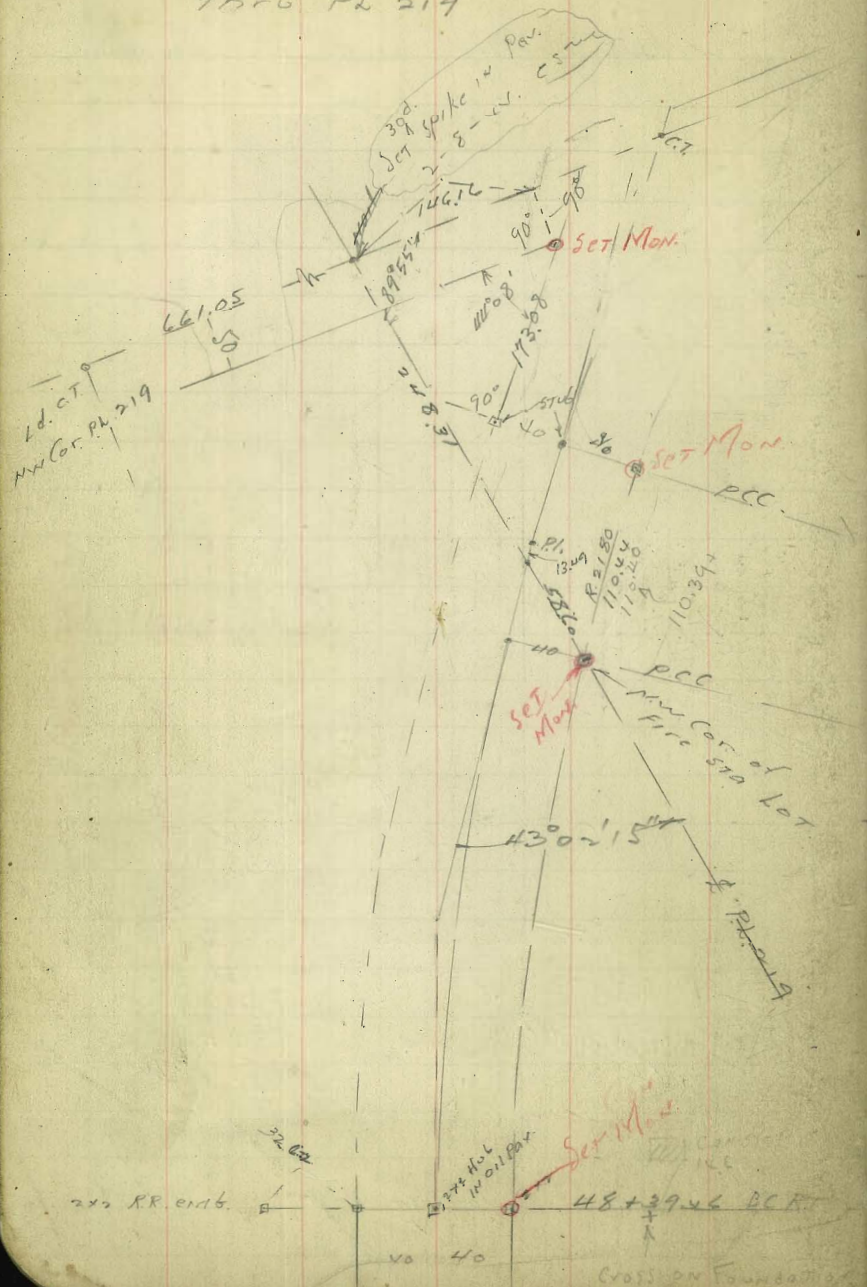
Tras West Point Loma Blvd.

Nov. 24-33
 West
 Point
 Loma
 28



1490.53
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W. Pt. Loma Blvd. Opening Survey
Thru PL 219



E. of Ingraham St.
Midway

Moore
Hazard
Hoopes
4-9-44 **30**

Plotted TR 5648 Mcg

✓ See G.B. 179 - 76
for Proposed Fire Sta.

$\Delta = 44.08$
 $R.R. = 718.34$ for 70' ST
 $R.L. = 291.20$ " " " "

$\Delta = 20.54$
 $R.R. = 2220$ for 80' ST
 $R.L. = 51.19$ " " " "

$\Delta = 13.01$ for 30' ST
 $R.R. = 1366.72$ " " " "
 $R.L. = 156.02$ " " " "
 $R.L. = 310.69$ " " " "

Note - Replaced Auto

with Cox. Mens.

City Engineer # 498

⊙ = Mon.

C. Moore
C. Sommer Meyer
W. Moore
E. Boeggs

2-14-44

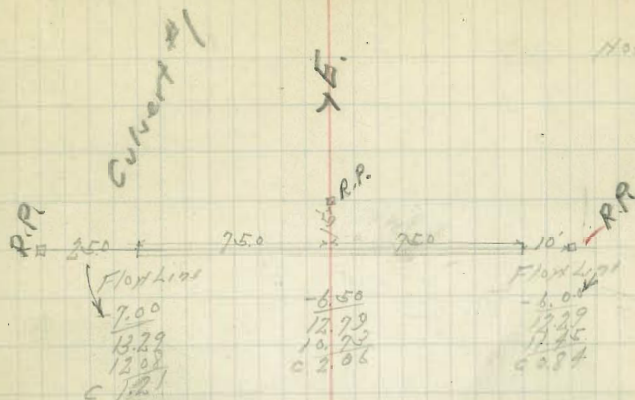
West Point Lomo Blvd.
Culverts

Culvert #1

6.29 T

31

Nov 25-33



Fast Point Loma

Grade 80 Side

| St. No. | St. Grade | St. No. | St. Grade |
|----------------|-----------|---------|---|
| 2+72.29 | 15.80 | 16.00 | 2+76.09 |
| 2+60 - Culvert | | | |
| 2+34.19 | 15.80 | 16.00 | 2+34.19 |
| 1+38 | 16.35 | 16.50 | 1+38 |
| 1+58 | 17.25 | 17.55 | 1+58 |
| 1+18 | 18.70 | 19.25 | 1+18 |
| 0+780 A/C | 20.80 | 21.10 | Pic. 0+82.50 |
| TP 129 | 6.29 | 12.78 | 5.00 |
| TP 129 | 0.92 | 17.78 | 12.41 |
| 0+390 | 23.20 | 23.45 | 0+41.25 |
| 0+0 | 25.60 | 25.80 | 0+0 |
| 3+1 | 1.85 | 27.62 | NW Spd X Fast Point Loma Soo Side |

Notes - For TTR
Page 27 to 30

32

| St. No. | St. Grade | St. No. | St. Grade |
|----------------|-----------|---------|---|
| 2+72.29 | 15.80 | 16.00 | 2+76.09 |
| 2+60 - Culvert | | | |
| 2+34.19 | 15.80 | 16.00 | 2+34.19 |
| 1+38 | 16.35 | 16.50 | 1+38 |
| 1+58 | 17.25 | 17.55 | 1+58 |
| 1+18 | 18.70 | 19.25 | 1+18 |
| 0+780 A/C | 20.80 | 21.10 | Pic. 0+82.50 |
| TP 129 | 6.29 | 12.78 | 5.00 |
| TP 129 | 0.92 | 17.78 | 12.41 |
| 0+390 | 23.20 | 23.45 | 0+41.25 |
| 0+0 | 25.60 | 25.80 | 0+0 |
| 3+1 | 1.85 | 27.62 | NW Spd X Fast Point Loma Soo Side |

S.L. Nov. 25. 03
Moore
S. 1507
Hartman

-9.5 F 21.5
12.0 32.2

-9.7 F 21.4
11.7 32.1 ⊕

-9.5 F 20.9
11.2 31.4

-9.7 F 21.6
11.5 31.8

-10.1 F 20.9
10.8 31.4

-10.2 F 21.8
11.6 32.7

-11.0 F 21.8
10.8 32.7

-11.3 F 22.2
11.0 32.5

-12.4 F 23.8
10.2 34.8 ⊕

-13.0 F 24.2
11.2 36.2

-14.5 F 25.0
10.5 37.5

-14.8 F 25.7
10.9 38.6

-5.4 F 23.6
18.2 35.4

→ 17.78

6.0 F 21
13.1 10.7

3.7 C 0.2
3.7 5.0

3.7 C 1.2
2.7 5.0

29.47

$$\begin{array}{r} 487.57 \\ 564.51 \\ \hline 952.08 \\ 222.5 \\ \hline 729.58 \\ \hline 11.6 \end{array}$$

$$\begin{array}{r} 514.32 \\ 497.50 \\ \hline 16.82 \end{array}$$

$$\begin{array}{r} 409.32 \\ 401.79 \\ \hline 7.53 \end{array}$$

33

| H. Sta | Alt. Grad | Sl. Grad | SL Sta | | | |
|-----------------|-----------|----------|--------|-----------|--------------|-----------------------------|
| 6+04.82 FIC | 25.00 | | 25.20 | 6+22.50 | Ed. Washburn | |
| 5+10 5+78.73 | | | | | | |
| 5+58.82 H. 9 | 24.90 | | 24.90 | 5+26.05 | | 12.0 02.5 9.5 0.0 |
| H. 6.00 | | | | | | 12.8 03.7 3.1 0.0 |
| 5+12.52 | 24.10 | | 24.60 | 5+59.08 | | 12.3 03.2 3.1 0.0 |
| 21.31 | | | | 35.76 | | |
| 1+81.51 | 23.10 | | 23.65 | 5+74.32 R | 11° 45.10 ✓ | 12.5 05.0 8.6 0.0 |
| 1+76.19 | 23.10 | | 23.20 | 4+97.50 | 10° 44.85' | 13.6 05.0 8.6 0.0 |
| | | | | | 10° 19.96 | 13.7 05.0 ⊕ |
| TP H. 92 | 6.60 | 36.89 | 0.19 | 30.28 | 7° 36.0 | 36.89 |
| 1+34.52 | 22.00 | | 21.80 | 4+59.02 | 8° 28.13 | 8.7 05.4 3.3 0.0 ⊕ |
| TP | 12.35 | 30.47 | 1.08 | 18.12 | | 19.20 30.47 |
| TP | 12.91 | 19.20 | 0.00 | 8.29 | | |
| 3+86.89 | 19.80 | | 19.45 | 4+01.75 | 4° 30.58 | -13.3 F 21.0 10.7 36.0 ⊕ |
| | | | | | 5° 02.13 | -13.7 F 15.8 3.8 36.2 ⊕ |
| 3+18.43 | 17.95 | | 17.70 | 2+59.89 | 2° 01.36 | -11.7 F 22.4 10.7 33.6 ⊕ |
| | | | | | 2° 32.05 | -11.4 F 21.7 10.3 32.8 ⊕ |
| 3+17.12 | 16.77 | | | | | -10.5 F 21.1 10.3 31.7 |
| 2+10.39 | 16.50 | | 16.65 | 3+12.45 | 3.906 | -10.2 F 20.9 10.7 31.4 ⊕ |
| | 6.29 | | | | | -10.3 F 21.5 11.3 32.3 ⊕ |

West Point Lemo Blvd.

North L. adjustment
52 of 1

Nov. 27-33
Warr
Sawyer
North 31

Sta H L 2 S

H L S L

9+0 ✓ 10° 21.08' 22.83 22.63 23.03

58
104 F 55
8.0 139
25 C 6.4
5.0

11+50 ✓ 8° 41.43' 23.18 22.99 23.33

49
82 F 50
5.0 139
21 C 6.2
5.0

8+0 ✓ 7° 11.18' 23.52 23.33 23.72

46
74 F 28
7.2 139
81 C 7.1
5.0

11 2.57 28.12 11.32 25.55

North Point

28.12 X 36.88 X 5

1+50 ✓ 5° 33.33' 23.57 23.17 24.07

130
147 F 17
2.8 138
6.4 C 6.4
5.0

7+0 ✓ 3° 56.35' 24.21 24.01 24.41

130
130 F 13
2.0 135
3.2 C 6.3
5.0

4+50 ✓ 2° 18.22' 24.56 24.26 24.76

133
130 0.0
5.0 131
5.1 C 7.0
5.0

2+0 ✓ 0° 41.38' 24.90 24.70 25.10

130
130 C 1.5
0.0 118
3.9 C 7.9
5.0

5+78.77 (PRG) BCR 25.00 24.85 25.20

36.1549

36.88 X 36.88

119
100 C 1.9
5.0 117
3.7 C 8.0
5.0

36.88

850 1126 1 21.61

11 21

750 20.43 20.33 20.63

11/31 F 20/120 11.8 C 2.8/5.0

750 20.72 20.57 20.97

10.8 F 9.2/13.8 11.5 C 6.0/5.0

750 21.17 20.91 21.31

10.4 F 2.2/14.0 11.3 C 1.5/5.0

TP 1.83 21.55 23.85 19.72

07 25 S RP

21.55 21.2 22.0 21.5

BM 1.10 22.57 0.15 27.97

11+1138 E.C.

11+1138 EC 17° 15.00 21.38 21.19 21.58

10.7 F 9.0/17.0 11.2 C 3.0/5.0

11+1138 16° 55.00 21.51 21.26 21.66

10.9 F 9.0/16.0 11.2 C 3.5/5.0

150 15° 15.00 21.80 21.66 22.00

10.1 F 9.0/16.0 11.2 C 3.4/5.0

1000 12° 40.00 22.14 21.94 22.34

10.2 F 9.0/16.0 11.2 C 5.0/5.0

900 12° 00.00 22.48 22.28 22.68

10.6 F 9.0/16.0 11.2 C 4.0/5.0

28.12

28.12 36.88

Sta 12.60 12.60 12.60

TP 10.26 12.12 12.63 8.92

16.70 14.11 14.67

4.50 15.55 16.39

15.10 17.59 18.10

14-88.25 Brk ✓ 18.00 18.50

14-42.97 18.72 19.07

13-97.29 Brk ✓ 19.45 19.25 19.65

4.50 19.75 19.55 19.95

13.40 20.10 19.90 20.20

21.55 TL

11.6 SL

7.4 F 10.3
19.8 15.6 + 17.9 C 7.0
19.9 5.0

5.7 F 1.9
10.6 7.7 16.2 C 9.1
1.9 5.0

10.8 F 1.2
8.2 8.3 12.5 C 10.3
10.1 5.0

3.6 F 1.1
7.7 8.0 12.1 C 11.1
2.8 5.0

2.8 F 1.3
6.4 5.7 13.5 C 10.3
13.1 5.0

2.1 F 1.1
8.2 8.2 12.3 C 11.1
1.8 5.0

1.8 F 1.0
6.8 7.5 12.6 C 11.1
1.5 5.0

1.5 F 1.7
8.0 10.1 12.9 C 8.8
2.5 5.0

21.55 TL

22.57 SL

19 + 80.89 - Oct
 11.65 52.50
 3.60 4.10

19 + 35.51
 2.80 4.10

4.00. 8.16 ✓
 1.00 4.20

2.50 5.11 6.10

1.40 2.15 3.21

7.50 8.19 9.53

TP 1.64 10.17 10.65 8.53

17.40 10.62 11.24

16.450 12.27 12.01
 19.12

11.1 5.4
 6.5 1.51 C 6.50
 3.2 4.2

6.4 1.56 C 6.1
 3.3 4.1

6.2 1.55 C 6.5
 3.1 3.0

4.8 1.31 C 6.2
 3.3 6.8

3.0 1.11 C 6.1
 3.8 3.7

1.3 1.07 C 6.0
 6.7 3.1

8.5 1.8 C 6.6
 13.9 11.0 + 2.3 5.0

6.8 1.62 C 6.2
 13.3 13.7 + 6.0 5.0

10.17 TL

13.18

199099
 3762
 2347.19
 592

24+1629.27

EQUATION

247191

2018

BM

750

2210

750

2140

750

2040

11.66
 2.00

2.00

2.21

2.43

2.64

2.86

3.08

3.30

3.52

1019T

51.65
 2.00

2.00

2.37

2.58

2.87

3.17

3.48

3.78

4.09

North Trench Pit
 West End S.O. 17th
 Grade 2.502

0.17
 2.58
 0.59

11

W.L. Famosa

77 F12
 95 27

75 F16
 91 27

73 F21
 91 32

71 F24
 95 32

69 F28
 93 36

67 F25
 92 38

20+50
 21.71
 25+50
 24+1629
 34.71

51

155 C20
 187 50

150 C25
 187 50

145 C27
 187 50

157 C31
 187 50

157 C43
 177 50

157 C45
 166 50

1077M 1918SL

H.L.

S.L.

H.L.

S.L.

24-17-19

2.00

2.00

Montalvo. W. Side

| Sta | + 20' on curbs H. 1 | - | ELY |
|------|------------------------|---|------------------------|
| D.M. | 1.32 | J | 43.66 42.34 |
| D.M. | 2.49 | H | 44.83 44.83 |
| 1 | | | 0.66 44.17 |
| 2 | | | 0.89 43.94 |
| 3 | | | 1.26 43.57 |
| 4 | | | 1.66 43.17 |
| 5 | | | 2.38 42.45 |
| 6 | | | 3.07 41.76 |
| 7 | | | 3.84 40.99 |
| 8 | | | 4.74 40.09 |
| 9 | | | 5.68 39.15 |
| | | | 10.77 34.06 |

Dec 5/33.

Lewis
Baker
Shyred
Palmer

40

Remarks

N. Cor. Brown Fence, Nail.

On Existing Curb

"

"

"

"

"

"

"

"

E.V. C"

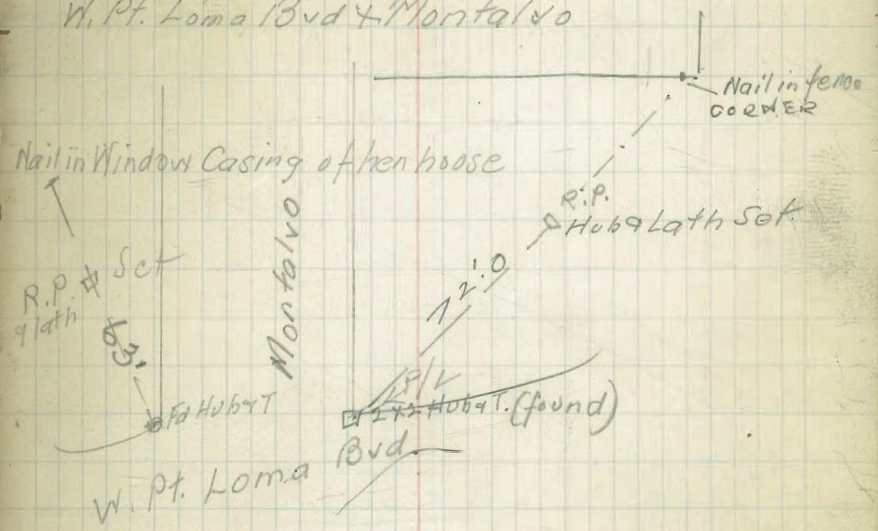
N. End Existing Curb on W. Side

W. Pt. Loma Blvd + Montalvo

99
54
45

41

Ref. Pt. for Hub + T. ft. 12" down at S.W. Cor.
W. Pt. Loma Blvd + Montalvo



| | | |
|-----------------|--------|-------|
| E. Side, 5' off | 120' | |
| W. " " " | 145.48 | 55.48 |

Montalvo

E. Side of H.

Levels on 1st lath, 5' Offsets Grade

| Sta | + H.I | - Ely |
|------|--------------|--------------|
| B.M. | 0.29 / 42.63 | 42.34 |
| 0+00 | | 4.72 / 38.41 |
| 0+20 | | 5.4 / 37.4 |
| 0+40 | | 6.4 / 36.7 |
| 0+90 | | 8.9 / 33.7 |

~~11.3~~

W. Side of S.

| | | | | |
|------|-------|------------|-------|------|
| B.M. | 1.71 | H.I. 44.05 | 42.34 | |
| | | | 44.35 | 44.1 |
| | x 0.7 | | 43.8 | 43.9 |
| | x 0.3 | | 43.7 | |
| | x 0.7 | | 43.3 | |
| | x 0.7 | | 43.3 | |
| | x 1.7 | | 41.3 | |
| | x 7.6 | | 41.4 | |
| | x 3.3 | | 40.7 | |
| | x 4.6 | | 39.4 | |
| | x 7.7 | | 36.3 | |

Dec 4/33

42

26.5
75.0
62.0
31.0

21.5
1.5

Page 40

29.7

Sy Hub. 5' Off.

Above C. & F
- 5' pt. 1 F.O. 11

Mentone St.

Dec 11/35

Levin
Carr
Shreve
Lunn

39.0
29.5

6 5

43

Remarks

Moore's, on S. Side W. Pt. Loma Blvd, E. of Mentone

N. Line

| Sta | + H. I | - | Elev | Co. F |
|----------|---------|-------|-------|--------------|
| B.M. | 11.09 | 39.06 | 27.97 | Grade |
| T.P. | 11.06 | 49.29 | 0.83 | 38.23 |
| | | | | |
| | S. Line | | | |
| 0+00 | | 1.9 | 47.4 | 47.8 Co. 4.1 |
| +25 | | 3.3 | 46.0 | 45.3 Co. 7.1 |
| +50 | | 4.5 | 44.8 | 44.0 Co. 8.1 |
| 1+00 | | 7.5 | 41.8 | 39.5 Co. 2.5 |
| 1+50 | | 11.1 | 38.2 | 35.0 Co. 3.2 |
| B.M. 7.0 | 0.97 | 39.15 | 38.23 | |
| 2+00 | | 4.3 | 34.8 | 30.5 Co. 4.3 |
| 2+50 | | 7.3 | 31.8 | 26.0 Co. 5.8 |
| 2+70 | | 8.4 | 30.7 | 24.4 Co. 6.3 |
| 2+88.85 | | 9.6 | 29.5 | 23.5 Co. 6.0 |

| Sta | + H. I | - | Elev | Grade | Co. F |
|------|--------|------|------|-------|---------|
| | | | 49.3 | | |
| 0+50 | | 6.6 | 42.7 | 43.0 | Co. 3.1 |
| 1+00 | | 10.7 | 38.6 | 38.5 | Co. 1.1 |
| 1+50 | | 4.4 | 34.7 | 34.0 | Co. 7.1 |
| 2+00 | | 8.7 | 30.4 | 29.5 | Co. 9.1 |

Temecula St.

27.71
1.13

| Sta | T | H.I. | Elev | Grade |
|-------------|------|-------|--------|-------|
| B.M. | 6.42 | 34.13 | 27.705 | 2 |
| B.M. & T.P. | 1.45 | | 32.68 | |
| | 9.68 | 42.36 | | |
| T.P. | 1.41 | | 40.95 | |
| | 4.39 | 45.34 | | |

SOUTH

| | | | ELEV. | GRADE |
|--------------|-------|------|-------|-------|
| 0 = W Clovis | 45.34 | 1.6 | 43.7 | 41.4 |
| 1 (0+10) | | 1.5 | 43.8 | 41.0 |
| 2 (0+40) | | 1.6 | 43.7 | 40.11 |
| 3 (0+70) | | 1.2 | 44.1 | 39.22 |
| 4 (1+00) | | 3.1 | 44.2 | 38.33 |
| 5 (1+23.70) | | 1.6 | 43.7 | 37.63 |
| 6 (1+43.7) | | 4.2 | 43.1 | 36.80 |
| 7 (1+63.7) | | 4.6 | 44.7 | 35.80 |
| 8 (1+83.7) | | 3.7 | 44.1 | 34.50 |
| 9 (2+03.7) | | 4.5 | 40.8 | 32.90 |
| 10 (2+23.7) | | 4.9 | 40.4 | 31.00 |
| 11 (2+43.7) | | 5.9 | 39.4 | 28.80 |
| 12 (2+63.7) | | 7.1 | 38.2 | 26.40 |
| 13 (2+83.7) | | 8.9 | 36.4 | 23.5 |
| 14 (2+93.7) | | 9.5 | 35.8 | 22.15 |
| 15 (3+03.7) | | 10.5 | 34.8 | 21.20 |
| 16 (3+13.7) | | 11.4 | 33.9 | 20.55 |
| 17 (3+23.7) | | 12.3 | 33.0 | 20.30 |

1/33
All Elevs are 0.27 low

0.3 added to cuts
0.3 deducted from fills

G. Lewis (Inst.)

NORTH

| + - | STA | H.I. | Elev | Grade |
|------|------|-------|-------|-------------------|
| | 0 | 45.34 | 7.2 | 38.1 40.70 F 26' |
| C23 | 1 | | 7.7 | 37.6 40.50 F 29.1 |
| C28 | 2 | | 7.9 | 37.4 39.6 F 22.2 |
| C36 | 3 | | 8.4 | 36.9 38.7 F 19' |
| C49 | 4 | | 9.4 | 36.1 37.8 F 18.8 |
| C38 | 5 | | 9.5 | 35.8 37.23 F 14.4 |
| C67 | 6 | | 10.1 | 35.7 36.4 F 12 |
| C63 | 7 | | 11.0 | 34.3 35.5 F 12 |
| C69 | 8 | | 11.85 | 33.49 34.1 F 0.6 |
| C76 | 6.65 | 40.14 | | |
| C79 | 9 | | 7.6 | 32.5 32.4 Co.1 |
| C94 | 10 | | 8.7 | 31.4 30.4 C10 |
| C106 | 11 | | 9.6 | 30.5 28.1 C2A |
| C118 | 12 | | 10.9 | 29.2 25.6 C36 |

All Grades superseded
See Page 12

Gate
Hydro
Lewis
PAGE 35
STA 11+11.38
E.C. Hub (Ref) S. Side W.P.
On 25' Tie Pt. W
Side of Temecula St

Montalvo

Hub, inside yard, under tree
 □ 45' Tie

Cut in Curb }
 98' Tie

Set Hub
 Inside fence

157-53
 98
 Exist'g Curb W. Side Montalvo

Montalvo, Vert. Curve on N. End of Street

W. Side or S.

| Sta | + H.I. | Elev | Grade |
|------|--------|-------|------------|
| B.M. | 0.95 | 43.29 | 42.34 |
| 0 | | | 2.58 40.71 |
| 1 | | | 3.82 39.47 |
| 4 | | | 5.21 38.08 |
| 3 | | | 6.45 36.84 |

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E. End of V.C.

Cor F

E. Side or N.

| | | | |
|--------------|-----------------|------|-------|
| 0 | 4.87 | | |
| 1 | 6.05 | | |
| 0 | 43.29 | 7.10 | 36.19 |
| 1 | | 7.34 | 35.75 |
| 2 | | 9.09 | 34.76 |
| 3 | | 9.55 | 33.74 |

E. End of V.C.

W. Pt. Loma Blvd. + Seaside

Dec. 12/33

48

| Sta | + | H.I. | - | Elv |
|------|------|--------|---------|---------|
| B.M. | 1.36 | ✓ 8.98 | | 27.62 |
| | | | 3.17 | ✓ 5.81 |
| T.P. | { | 0.17 | ✓ 11.74 | ✓ 17.74 |
| B.M. | | | | |
| T.P. | { | 0.45 | ✓ 7.57 | ✓ 7.54 |
| | | | | |
| B.M. | | | 10.06 | - 0.07 |

Nail in Pole N.W. Cor. W. Pt. Loma + Seaside, page 32
 Hub at 0+00-5 N. of H. - { Blvd. DARK C 0.2 }
 GUINEA { ELEV GRADE 25.60 }

RUBBLE
 Top of post, S side Concrete Wall,

10.56
 9.99
 0.57

Hub, Foot of bank, W. Side of Channel, close to bush
 2 FEET S. OF WEST PT. LOMA BLVD.

Dec 14/33

| | | | | |
|------|---|-------|---------|---------|
| B.M. | { | 11.77 | 13.20 | 1.48 |
| | | | | 0.67 |
| | | 11.37 | ✓ 13.90 | |
| T.P. | { | 10.85 | 33.69 | 1.06 |
| | | | | ✓ 44.84 |
| T.P. | { | 8.56 | 41.99 | 0.26 |
| | | | | 33.43 |
| T.P. | { | 7.16 | ✓ 47.42 | 1.73 |
| | | | | 40.46 |
| B.M. | | | 5.05 | ✓ 41.37 |

Hub, E. Side Channel

Nail in Fence, W. Side Montalvo 42.34

Clovis.

27.71

11.18

49

Sta + H.I. - EIV. 7'

B.M. 10.86 38.83^x 27.97

T.P. { 10.76 49.19 } 2.42 38.43

T.P. { 10.46 59.14 } 0.51 48.68

T.P. { 4.88 63.63 } 0.39 58.75

St. Side W.P. La Brd.

E. or S. Side on 5' Off.

± E. of St

Grade

| T.P. | H.I. | EIV. | Grade | H.I. | EIV. | | | |
|--------|-------|-------|-------|-------|-------|------|------|---------------------------|
| T.P. { | 63.63 | 10.22 | 53.41 | 54.45 | 10.9 | | | |
| | 6.53 | 59.94 | 53.41 | | | | | |
| | 1.04 | 54.45 | 53.41 | | | | | |
| 0+00 | | 11.78 | 43.2 | 47.5 | 54.45 | 10.9 | 43.6 | 0+00 = TEMECULA |
| 0+10 | | 9.9 | 44.5 | 43.5 | 54.45 | 10.1 | 44.4 | |
| 0+50 | | 5.4 | 49.0 | 47.7 | 54.45 | 7.1 | 47.4 | |
| 1+00 | | 1.04 | 53.41 | 51.7 | 54.45 | 3.2 | 51.3 | |
| | 10.17 | 63.58 | | | 54.45 | | | |
| 1+30 | | 8.4 | 55.4 | 54.8 | 54.45 | 9.0 | 52.6 | Alley |
| B.M. | | 5.71 | 57.87 | | 54.45 | | | Nail in Tel. pole S. Side |
| 1+70 | | 4.3 | 59.3 | 57.1 | 54.45 | 6.3 | 57.3 | |
| 2+10 | | 7.1 | 61.5 | 58.5 | 54.45 | 4.4 | 59.7 | |
| T.P. { | | 0.31 | 63.27 | | 54.45 | | | |
| | 8.94 | 77.71 | | | 54.45 | | | |
| 2+55 | | 8.9 | 69.4 | 59.6 | 54.45 | 11.5 | 60.7 | |

Dec 12/33

50

Clovis (Cont'd)

| Sta | E. or S. Side on 5 th off | | | | ± of St. | | | | | |
|--------|--------------------------------------|--------|------|-------|----------|--------|--------|------|------|---------------------------|
| | T | H. 1/2 | — | Elv | Grade | Cal F. | H. 1/2 | — | Elv | |
| 2+65 | | 72.21 | 8.6 | 63.6 | 59.9 | 13.7 | 72.21 | 11.3 | 60.9 | N. Line Montone |
| 0+00 | | | 6.8 | 65.4 | 60.85 | 4.5 | | 9.8 | 64.4 | S. " " |
| 0+10 | | | 6.6 | 65.6 | 61.0 | 4.6 | | 9.6 | 64.6 | |
| 0+50 | | | 5.3 | 66.9 | 61.4 | 5.5 | | 9.1 | 63.1 | |
| 1+00 | | | 4.1 | 68.1 | 61.9 | 6.2 | | 9.0 | 63.2 | |
| 1+50 | | | 3.5 | 68.7 | 62.4 | 6.3 | | 9.1 | 63.1 | |
| 2+00 | | | 2.4 | 69.8 | 61.9 | 6.9 | | 9.0 | 63.2 | |
| 2+55 | | | 2.3 | 69.9 | 63.5 | 6.4 | | 9.4 | 64.8 | |
| 2+65 | | | 5.8 | 66.4 | 63.65 | 2.7 | | 9.4 | 64.8 | N. Line Montalvo |
| T.P. { | | | 2.34 | 69.87 | ✓ | | | | | |
| | 4.00 | 73.87 | | | | | 73.87 | | | |
| 0+00 | | | 7.50 | 66.4 | 63.7 | 2.7 | | 11.3 | 64.6 | S. Line Montalvo |
| 0+10 | | | 4.00 | 69.9 | 63.5 | 6.4 | | 11.1 | 64.8 | |
| 0+50 | | | H. H | 69.5 | 62.9 | 6.6 | | 10.8 | 63.1 | |
| 1+00 | | | 5.4 | 68.5 | 62.2 | 6.3 | | 10.8 | 63.1 | N. COLLIER PARK |
| 1+20.7 | | | 5.7 | 68.2 | 62.0 | 6.2 | | 10.9 | 63.0 | |
| B.M. | | | 5.49 | 68.38 | ✓ | | | | | 100' R.P. for Pueblo Cor. |

Rialto

Sta + H.I. - Elev Grade

B.M. 0.35 58.22 57.87

T.P. { 0.69 46.99 11.89 46.33

T.P. { 11.17 35.20

B.M. 8.75 38.24

T.P. { 0.40 35.92 11.47 35.52

T.P. { 11.87 24.05

T.P. { 11.04 26.09

0-60 } 14.51 11.58 4.9 6.5

0-40 } 13.21 12.88 5.4 7.5

0-20 } 17.04 14.05 6.1 8.0

South 5' Line (from Clovis)

0+00 } 26.09 11.70 14.89 7.4 6.5 26.09 14.8 11.3

0+40 } 9.04 17.05 10.4 6.7 18.3 12.8

0+80 } 8.04 18.05 12.8 6.9 11.8 14.3

1+20 } 7.20 18.89 14.6 4.3 10.5 15.6

T.P. { 8.85 17.24

1+60 } 11.47 20.44 15.85 4.6 5.3 16.6

2+00 } 1.70 20.71 16.70 3.5 4.6 17.3

2+40 } 1.10 20.81 17.0 3.7 4.7 17.7

2+80 } 1.95 19.96 17.0 3.0 4.5 17.4

3+20 } 2.60 19.31 16.5 2.8 5.3 16.6

2.97
1.50
1.179

~~7.35~~
~~3.6~~
11.51

~~4.22~~
~~1.92~~
13.21

~~7.8~~
~~3.~~
4.16

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{ N.W. Cor. Con. Step Stone of
4380-Temeoula (E. of Clovis)
+ Cut in step

{ 60' W. of E. Line of Clovis, approx. 1st 90⁰⁰
Going East. (Moore)

Street (Rialto)

H.I. - Elev Grade

21.91

Hand level reference

Rialto (Cont'd) 5' off.

| Sta | H.I. | — | EL. | Grade | Corr. | H.I. |
|----------------------|-------|-------|-------|-------|-------|-------|
| 3+60 | 21.91 | 3.7 | 18.2 | 15.25 | C2.9 | 41.91 |
| 4+80 | | 4.6 | 17.3 | 13.0 | C4.3 | |
| 4+26 ⁹⁶ | | 5.4 | 16.5 | | | |
| 4+40 | | 5.9 | 16.0 | 9.6 | C6.4 | |
| 4+60 | | 6.8 | 15.4 | 7.9 | C7.2 | |
| 4+80 | | 7.9 | 14.0 | 7.15 | C6.8 | |
| North Side of Street | | | | | | |
| 4+47 ¹³ | 21.91 | 15.46 | 6.45 | | | |
| 4+40 | | 12.78 | 9.13 | 8.6 | C0.5 | |
| 4+26 ⁹⁶ | | 9.67 | 12.29 | | | |
| 4+80 | | 8.7 | 13.7 | 14.2 | C1.5 | |
| 3+60 | | 7.1 | 14.8 | 14.6 | C0.2 | |
| 3+90 | | 6.4 | 15.5 | 16.00 | F0.5 | |
| 4+80 | | 5.7 | 16.2 | 16.50 | F0.3 | |
| 4+40 | | 5.6 | 16.3 | 16.60 | F0.3 | |
| 4+00 | | 5.7 | 16.2 | 16.25 | C0.0 | |
| 1+60 | | 6.7 | 15.2 | 15.35 | F0.1 | |
| 1+40 | | 8.7 | 13.7 | 14.05 | F0.3 | |
| 0+80 | | 9.7 | 12.2 | 14.7 | C0.0 | |
| 0+40 | | 11.5 | 10.4 | 9.8 | C0.6 | |
| 0+00 | | | | | | |

10178
 @ Street (Rialto) 11.12
 21.34
 10246 5'

| — | EL. | |
|------|------|--|
| 6.1 | 15.8 | Previous Page |
| 7.2 | 14.7 | |
| 7.8 | 14.1 | |
| 8.2 | 13.7 | |
| 8.8 | 13.1 | |
| 13.1 | 8.8 | |
| 9.9 | 12.0 | N. Edge of Travelled Grade Opp. 4+480 |

R.O.T.

Note.

E. Side
 7' Line abt Rialto + Clavis, Ref'd S. E. y
 100' hub & hub close to S. W. Con. Green Fence
 do on W. Side, hub at 100' & 200'⁶⁴
 = N.L. of Rialto & S.L. of W. Pt. Loma Blvd.

Elev's on posts in Channel
W. Pt. Loma Blvd

| Sta | + H.I | - Elev |
|----------------|-------|-----------------|
| B.M. | 1.91 | +1.84 ✓ |
| Post #1 | | 7.025 - 5.185 ✓ |
| 10' N. of Post | | 7.40 - 5.56 |
| | | 7.49 - 5.65 |
| | | 8.7 - 6.86 |
| | | 7.65 - 5.78 |
| | | 8.9 - 7.06 |
| Lev. B.M. | | 0.36 + 1.48 |

~~1.91~~
~~- 0.07~~
+ 1.84

Dec 12/33

5

Page 48.

10' S. of Culvert Intake

End of Culvert

On line with S. Slope Stake

GROUND → 12.8 North of Post #1

Ground on E

25' N. of End of Culvert

N. End of Culvert, Grd.

GROUND → in channel

DISTANCE MISSING → Hub, foot of E. bank

FROM FIRST

— — — → 100' R.P. OF P.C. 3417.42

Rosecrans St., E. Side 5' Off

Dec 15/33

indexed
c.s.k.

54

| Sta | + H.1 | - | Elv. |
|------|-------|---|-------|
| B.M. | | | 20.64 |
| | | | 1.145 |

Brass Plug

S.W. Cor. Canyon Rd. Rosecrans

" " Garrison "

| | | | |
|------|------|-------|-------|
| B.M. | 3.19 | 13.83 | 20.64 |
|------|------|-------|-------|

S.W. Cor. Canyon (above)

| | | | |
|--------|------|-------|-------|
| T.P. { | | 6.99 | 16.84 |
| | 5.04 | 16.86 | |

| | | | |
|------|--|------|-------|
| 2+00 | | 3.92 | 12.92 |
|------|--|------|-------|

N. Line Carlton

| | | | |
|------|--|------|-------|
| 1+50 | | 4.75 | 12.11 |
|------|--|------|-------|

| | | | |
|------|--|------|-------|
| 1+00 | | 5.59 | 11.27 |
|------|--|------|-------|

| | | | |
|------|--|------|-------|
| 0+50 | | 6.38 | 10.48 |
|------|--|------|-------|

| | | | |
|------|--|------|------|
| 0+00 | | 7.26 | 9.60 |
|------|--|------|------|

S. Line Dickens

| | | | |
|------|--|------|------|
| 2+00 | | 8.54 | 8.32 |
|------|--|------|------|

N. " "

| | | | |
|------|--|------|------|
| 1+50 | | 9.48 | 7.38 |
|------|--|------|------|

| | | | |
|--------|------|------|------|
| T.P. { | 1.57 | 8.95 | 9.48 |
| | | | 7.38 |

| | | | |
|------|--|------|------|
| 1+00 | | 2.25 | 6.70 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+50 | | 3.17 | 5.82 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 4.02 | 4.93 |
|------|--|------|------|

S. Line Emerson

| | | | |
|------|--|------|------|
| 2+00 | | 4.65 | 4.30 |
|------|--|------|------|

N. Line Emerson

| | | | |
|------|--|------|------|
| 1+50 | | 4.96 | 3.99 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+00 | | 5.29 | 3.66 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+50 | | 5.91 | 3.04 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 6.02 | 2.93 |
|------|--|------|------|

S. Line Fenelon

| | | | |
|------|--|------|------|
| 2+00 | | 6.88 | 2.07 |
|------|--|------|------|

N. Line Fenelon

| | | | |
|------|--|------|------|
| 1+50 | | 7.57 | 1.42 |
|------|--|------|------|

Cont'd

| Sta | + | 8.95 HI | - | Elev | Grade | Cut | Fill |
|--------------------|------|------------|------|------|-------|------|------|
| T.P. | 3.39 | 4.78 | 7.56 | 1.39 | | | |
| 1+00 | | | 3.76 | 1.02 | | | |
| 0+50 | | | 3.74 | 1.04 | | | |
| 0+00 | | | 4.23 | 0.55 | | | |
| ^{ch} B.M. | | | 3.63 | 1.15 | | | |
| 2+00 | | | 4.12 | 0.66 | | | |
| 1+50 | | | 4.14 | 0.64 | | | |
| 1+00 | | | 3.90 | 0.88 | | | |
| 0+50 | | | 3.82 | 0.96 | | | |
| 0+00 | | | 3.85 | 0.93 | | | |
| 2+00 | | | 3.87 | 0.91 | | | |
| T.P. | 6.05 | 6.96 | 3.87 | 0.91 | | | |
| 1+50 | | | 5.80 | 1.16 | | | |
| 1+00 | | | 5.52 | 1.44 | | | |
| 0+50 | | | 5.14 | 1.82 | | | |
| 0+00 | | | 4.88 | 2.08 | | | |
| 2+00 | | | 4.51 | 2.45 | | | |
| 1+50 | | | 3.77 | 3.19 | | | |
| 1+00 | | | 3.26 | 3.70 | | | |
| 0+50 | | | 2.68 | 4.28 | | | |
| 0+00 | | | 2.22 | 4.74 | | | |
| 2+00 | | | 2.21 | 4.75 | 4.00 | 0.75 | |
| T.P. | 5.52 | 10.27 | 2.21 | 4.75 | | | |
| 1+50 | | | 4.44 | 5.83 | 4.25 | 1.58 | |
| 1+00 | | | 4.44 | 5.83 | 4.50 | 1.33 | |

S. Line Garrison
 1.145 Brass Plug on S.W. Curb Ref. Garrison

N. Line Garrison

S. Line Hugo

N. Line Hugo

S. Line Ingelow

N. Line Ingelow

S. Line Jarvis

N. Line Jarvis

Rosecrans (Cont'd)

| Sta | + | HI | - | Elev | Grade | Cut | Fill |
|------|------|-------|------|------|-------|------|----------------|
| 0+50 | | 10.27 | 4.71 | 5.56 | 4.75 | 0.81 | |
| 0+00 | | | 4.49 | 5.78 | 5.00 | 0.78 | S. line Keats |
| 2+00 | | | 3.81 | 6.46 | 6.00 | 0.46 | N. line Keats |
| 1+50 | | | 3.58 | 6.69 | 6.25 | 0.44 | |
| 1+00 | | | 3.30 | 6.97 | 6.50 | 0.47 | |
| 0+50 | | | 2.72 | 7.55 | 6.75 | 0.80 | |
| 0+00 | | | 2.37 | 7.90 | 7.00 | 0.90 | S. line Lowell |
| T.P. | 3.13 | 11.03 | 2.37 | 7.90 | | | |
| B.M. | | | 4.00 | 7.03 | | | |

40' East of 0+75 of 5' offset line

| | | | | | | | |
|-----------------|--|--|-----------------|-----------------|-----------------|-----------------|--|
| 2+80 | | | 4.81 | 8.77 | 7.50 | 0.77 | |
| 1+50 | | | 4.71 | 8.37 | 7.63 | 0.69 | |
| 1+00 | | | 4.97 | 8.11 | 7.75 | 0.36 | |
| 0+50 | | | 4.46 | 8.57 | 7.88 | 0.69 | |
| 0+00 | | | 4.15 | 8.88 | 8.00 | 0.88 | |

~~Error in
Chainage~~

~~N. Line Lowell~~

~~See page
62
for correct
elevs~~

~~S. Line Macaulay~~

To Check

| | | | | | | | |
|------|------|-------|------|--------------|--|--|--|
| B.M. | 5.80 | 17.88 | | 7.03 | | | |
| | | | 4.77 | 8.11 = 8.063 | | | |

Above

Curb S.W. Cor Lowell

Rosecrans (Cont'd)

| Sta | + | H. 1 | - | E.L.V |
|-------------|------|-------|------|-------|
| 0+00 | | 12.88 | 5.15 | 7.73 |
| 2+00 | | | 4.44 | 8.46 |
| 1+50 | | | 4.00 | 8.88 |
| 1+00 | | | 3.55 | 9.33 |
| 0+50 | | | 3.14 | 9.74 |
| 0+00 | | | 4.74 | 10.14 |
| 2+00 (T.P.) | | | 7.52 | 10.36 |
| | 1.74 | 17.10 | | |
| 1+50 | | | 4.51 | 9.59 |
| 1+00 | | | 4.93 | 9.17 |
| 0+50 | | | 3.39 | 8.71 |
| 0+00 | | | 3.87 | 8.28 |
| 2+00 | | | 4.75 | 7.35 |
| 1+50 | | | 5.13 | 6.97 |
| 1+00 | | | 5.49 | 6.61 |
| 0+50 | | | 5.81 | 6.29 |
| 0+00 | | | 6.19 | 5.91 |
| 2+00 (T.P.) | | | 6.57 | 5.53 |
| | 3.60 | 9.13 | | |
| 1+50 | | | 3.76 | 5.37 |
| 1+00 | | | 3.97 | 5.16 |
| 0+50 | | | 4.14 | 4.99 |
| 0+00 | | | 4.31 | 4.82 |
| 2+00 | | | 4.79 | 4.34 |

Temp. 8.1
New page

On E. Edge of Paving,
Running North

57

X.I. → Previous Page S. Line Lowell (7')

N. " "

\$ S. (?) Macaulay
N.L. of Macaulay

\$ Newell
N.L. of Newell

S. Line of Oliphant
N. " " "

S. Line of Poe
N. " "

Contd

| Sta | + | H. 1 | - | ELV |
|------|---|-------|------|------|
| 1+50 | | 9.13 | 4.65 | 4.48 |
| 1+00 | | | 4.46 | 4.67 |
| 0+50 | | | 4.28 | 4.85 |
| 0+00 | | 4.062 | 4.06 | 5.07 |

~~2+00 5.1~~

Dec. 1933

| | | | | |
|------------|------|------|------|------|
| Temp. B.M. | 3.83 | 9.36 | | 5.53 |
| T.P. { | 4.25 | 9.12 | 4.49 | 4.87 |
| 2+00 | | | 4.85 | 4.77 |
| 1+50 | | | 5.35 | 3.77 |
| 1+00 | | | 5.85 | 3.27 |
| 0+50 | | | 5.95 | 3.17 |
| 0+00 | | | 6.15 | 2.97 |
| 2+00 { | | | 6.59 | 7.53 |
| T.P. { | 7.03 | 9.56 | | |
| 1+50 | | | 7.04 | 2.52 |
| 1+00 | | | 6.82 | 2.74 |
| 0+50 | | | 6.45 | 3.11 |
| 0+00 | | | 5.86 | 3.70 |
| 2+00 | | | 5.21 | 4.35 |
| 1+50 | | | 4.37 | 5.24 |
| 1+00 | | | 2.70 | 6.86 |

47
427.45

5'

S. Line of QUIMBY

~~H. " " "~~

Previous Page.

N. Line Quimby

S. Line Russell St.

N. " " "

S. Line? Sterne St

N. " " "

Cont'd

| Sta | + | H.I | - | EIV |
|--------|------|-------|------|------|
| 0+50 | | 9.56 | 1.06 | 8.50 |
| I.P. } | | | 0.39 | 9.17 |
| | 7.99 | 17.16 | | |

| | | | |
|------|--|------|-------|
| 0+00 | | 6.93 | 10.23 |
|------|--|------|-------|

| | | | |
|------------|--|------|-------|
| B.M. LHECK | | 3.21 | 13.95 |
|------------|--|------|-------|

Running South From Lowell, Edge Expaving

| | | | |
|------|------|-------|------|
| B.M. | 3.91 | 10.94 | 7.03 |
|------|------|-------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 3.34 | 7.62 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+50 | | 3.54 | 7.50 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+00 | | 3.87 | 7.07 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+50 | | 4.14 | 6.80 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 2+00 | | 4.37 | 6.57 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 5.00 | 5.94 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+50 | | 5.36 | 5.58 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+00 | | 5.66 | 5.28 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+50 | | 6.08 | 4.86 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 2+00 | | 6.39 | 4.55 |
|------|--|------|------|

| | | | | |
|--------|------|------|------|------|
| I.P. } | 1.97 | 6.52 | 6.39 | 4.55 |
|--------|------|------|------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 2.59 | 3.93 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+50 | | 3.07 | 3.47 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+00 | | 3.58 | 2.94 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 1+50 | | 3.96 | 2.56 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 2+00 | | 4.43 | 2.09 |
|------|--|------|------|

| | | | |
|------|--|------|------|
| 0+00 | | 4.93 | 1.59 |
|------|--|------|------|

Tennyson St
S. Line
B. Plug in Curb, N.W. Cor. Curb

Page 56
S. L. of Lowell
7' pt.

N. Line Keats
S. " "

N. Line Jarvis

S. Line Jarvis

N. Line Ingelow
S. Line Ingelow

Cont'd

60

| Sta | + | HI | - | Elev |
|------|------|------|------|------|
| 0+50 | | 6.52 | 5.11 | 1.41 |
| 1+00 | | | 5.25 | 1.37 |
| 1+50 | | | 5.41 | 1.11 |
| 2+00 | | | 5.46 | 1.06 |
| T.P. | 4.22 | 5.28 | 5.46 | 1.06 |
| 0+00 | | | 4.28 | 1.00 |
| 0+50 | | | 4.41 | 0.87 |
| 1+00 | | | 4.49 | 0.79 |
| 1+50 | | | 4.63 | 0.65 |
| 2+00 | | | 4.78 | 0.50 |
| 0+00 | | | 4.75 | 0.53 |
| B.M. | | | 4.16 | 1.12 |
| 0+50 | | | 4.67 | 0.61 |
| 1+00 | | | 4.33 | 0.95 |
| 1+50 | | | 4.10 | 1.18 |
| 2+00 | | | 3.84 | 1.44 |
| T.P. | 7.45 | 8.98 | 3.75 | 1.53 |
| 0+00 | | | 7.45 | 1.53 |
| 0+50 | | | 6.94 | 2.04 |
| 1+00 | | | 6.44 | 2.54 |
| 1+50 | | | 5.96 | 3.02 |
| 2+00 | | | 5.48 | 3.50 |
| 0+00 | | | 4.00 | 4.00 |
| 0+50 | | | 3.20 | 5.78 |
| 1+00 | | | 2.49 | 6.49 |

N. line Hugo

S. line Hugo

N. line Garrison

S. line Garrison

B.M. Elev 1.145 S.W. Curb Garrison Brass Plug

N. line Fenelon

S. line Fenelon

N. line Emerson

S " "

Cont'd

61

| Sta | + | HI | - | Elev |
|---------------------------------|-------|-------|------|-------|
| 1+50 | | 8.98 | 1.74 | 7.24 |
| 2+00 | | | 0.96 | 8.02 |
| T.P. | 10.55 | 18.57 | 0.96 | 8.02 |
| 0+00 | | | 9.04 | 9.53 |
| 0+50 | | | 8.13 | 10.44 |
| 1+00 | | | 7.29 | 11.28 |
| 1+50 | | | 6.42 | 12.15 |
| 2+00 | | | 5.55 | 13.02 |
| ^{ch} 2+00 5' offset | | | 5.64 | 12.93 |

N. line Carleton

S. line Carleton

N. line Dickens

Ch on 5' offset stake N. " " Elev 12.94

Rosecrans. 5' Off.
Running North

Dec. 18th 1933.

62

| Sta | + H. 1 | - E. 1. |
|-----------------|--------|-----------|
| B.M. | 6.15 | 13.18 |
| 2+00 | | 4.85 8.33 |
| 1+50 | | 4.87 8.36 |
| 1+00 | | 4.34 8.84 |
| 0+50 | | 4.42 8.66 |
| 0+00 | | 3.76 9.32 |
| 2+50 | | 3.90 9.28 |
| T.P. | 2.12 | 11.76 |
| 1+50 | | 3.54 9.64 |
| 1+00 | | 2.80 8.96 |
| 1+00 | | 3.07 8.74 |
| 0+50 | | 3.59 8.17 |
| 0+00 | | 4.21 7.55 |
| 5+00 | | |
| 2+00 | | 4.89 6.87 |
| 1+50 | | 5.41 6.35 |
| 1+00 | | 5.63 6.13 |
| 0+50 | | 5.59 6.17 |
| 0+00 | | 6.20 5.56 |
| 2+00 | | 6.77 4.99 |
| T.P. | 3.88 | 8.87 |
| 1+50 | | 3.98 4.89 |
| 1+00 | | 4.41 4.46 |
| 0+50 | | 4.34 4.53 |
| 0+00 | | 4.69 4.18 |
| 2+00 | | 4.72 4.15 |

Page 56

N. Line Lowell

S. Line Macaulay

N. Line Macaulay

S. Line Newell

N. Line Newell

S. Line Oliphant

N. " "

S. Line Poe

N. " "

Cont'd

| Sta | T | H.I. | - | EIV |
|------|---|------|------|------|
| 1+50 | | 8.87 | 4.93 | 3.94 |
| 1+00 | | | 4.66 | 4.21 |
| 0+50 | | | 4.39 | 4.50 |
| 0+00 | | | 5.10 | 3.77 |
| 2+00 | | | 5.07 | 3.85 |
| T.P. | { | 3.69 | 7.54 | |
| 1+50 | | | 3.70 | 4.34 |
| 1+00 | | | 3.46 | 4.08 |
| 0+50 | | | 3.14 | 4.40 |
| 0+00 | | | 3.83 | 3.71 |
| 1+00 | | | 4.19 | 3.35 |
| 1+50 | | | 4.08 | 3.46 |
| 1+00 | | | 4.67 | 3.12 |
| 0+50 | | | 4.99 | 2.55 |
| 0+00 | | | 6.17 | 1.42 |
| 1+00 | | | 6.45 | 1.09 |
| T.P. | { | 4.95 | 6.04 | |
| 1+50 | | | 5.11 | 0.93 |
| 1+00 | | | 4.80 | 1.24 |
| 0+50 | | | 4.43 | 1.61 |
| 0+00 | | | 4.93 | 1.11 |
| | | | 3.07 | 2.97 |
| 2+00 | | | 4.18 | 1.86 |

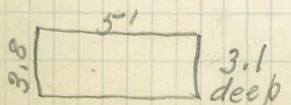
63

S. Line Quimby
H. " "

S. Line R — St.
H. " " "

S. Line S — St.
H. " " "

S. Line Tennyson



Top S.D. Con. G. & E. Manhole
+ 25' S. of 2+00 + 10' W. of 1st St.

N. Line Tennyson

Cont'd.

| Sta | + | H. I. | - | EL |
|------|------|-------|------|----------------------|
| 1+50 | | 6.04 | 4.54 | 3.52 |
| 1+00 | | | 0.62 | 5.42 |
| T.P. | 9.78 | 15.20 | | |
| 0+50 | | | 8.34 | 7.28 6.88 |
| 0+00 | | | 6.97 | 8.23 |
| B.M. | | | 1.28 | 13.92 |

S. Line U- St.
Page 59, Check

61

W. Pt. Loma Blvd
Pile Cut Off

| Sta | + H.I | El. | Grade | Red |
|-----|-------|-----|-------|-----|
| | | | -5.6 | |

| | | | | |
|------|------|------|-------|--|
| B.M. | 3.79 | 3.72 | -0.07 | |
|------|------|------|-------|--|

CULVERT # 1

9.32 Set 0.5 above
 Rod 8.82

± Cut Off
Page 48

Set 8.32 0.5 above
 8.82 { 5.1 Intake Cut Off - 5.1
 0.72
 8.82 Disch " - 6.1

6.1
 3.72
 9.82
 5
 9.32 = Disch, 0.5 above

W. Pt. Loma Bud. 5' Off
S. Side

N. Side 5' Off

Width 80' ± 40' $\frac{5.2}{2.82}$
 $\frac{5.14}{2.7}$
 $\frac{8.1}{8.1}$

66

| Sta | M.I. | Elev | Grade | Cd F |
|--------------------------|------|-------|--------|-------------|
| B.M. | 3.27 | 8.41 | 5.14 | |
| 23+00 | | 11.85 | -3.44' | |
| T.P. | 5.39 | +1.95 | | |
| 23+45 ²² | | 5.82 | -3.87 | 2.00 F 5.87 |
| 24+50 | | 6.24 | -4.29 | 3.70 F 5.39 |
| 25+00 | | 4.82 | -2.87 | 7.75 F 5.12 |
| 25+50 | | 4.91 | -2.96 | 7.40 F 5.36 |
| 26+00 | | 4.63 | -1.68 | 9.65 F 3.33 |
| 26+50 | | 4.54 | -2.59 | 7.70 F 5.20 |
| 27+00 | | 4.55 | -1.60 | 2.85 F 5.45 |
| 27+50 | | 4.43 | -2.48 | 3.00 F 5.30 |
| T.P. | 5.19 | +2.71 | 4.43 | -2.48 |
| 28+00 | | 5.25 | -1.54 | 3.15 F 5.60 |
| 28+50 | | 5.08 | -1.37 | 3.30 F 5.6 |
| 29+00 | | 4.78 | -1.07 | 3.45 F 5.55 |
| 29+50 | | 4.78 | -2.07 | 3.60 F 5.65 |
| 30+00 | | 5.03 | -1.32 | 3.75 F 6.07 |
| 30+50 | | 5.02 | -1.31 | 3.90 F 6.21 |
| 30+80 ⁷⁶ P.C. | | 4.72 | -1.01 | 3.99 F 6.20 |
| T.P. | 7.30 | +5.29 | 4.72 | -2.01 |
| B.M. | | 2.01 | +3.28 | |

| Sta | M.I. | Elev | Grade | Cd F |
|--------------------------|------|------|-------|-------------|
| 17.16.55 | | | | |
| 24+50 | | 4.72 | -2.77 | 2.00 F 5.87 |
| 25+00 | | 4.75 | -2.80 | 7.75 F 5.05 |
| 25+50 | | 4.68 | -2.73 | 7.40 F 5.13 |
| 26+00 | | 4.69 | -2.74 | 7.65 F 5.39 |
| 26+50 | | 4.60 | -2.65 | 2.70 F 5.35 |
| 27+00 | | 4.53 | -1.58 | 2.85 F 5.43 |
| 27+50 | | 4.38 | -2.43 | 3.00 F 5.43 |
| 28+00 | | 5.19 | -2.48 | 3.15 F 5.63 |
| 28+50 | | 4.92 | -1.21 | 3.30 F 5.51 |
| 29+00 | | 4.72 | -2.01 | 3.45 F 5.46 |
| 29+50 | | 4.81 | -2.10 | 3.60 F 5.70 |
| 30+00 | | 4.29 | -1.58 | 3.75 F 5.33 |
| 30+50 | | 4.31 | -1.60 | 3.90 F 5.50 |
| 30+80 ⁷⁶ P.C. | | 4.48 | -1.77 | 3.99 F 5.76 |

See foot of page 24 + 16²⁹

Page 58

Block Corner

Top P.P.P.C. 42' From N. Prop. Line

B.M. 1.41 6.55 5.14
10.16 -3.66

24+16²⁹ -3.61

W. Pt. Loma Blvd 5' Off.
Curve To Left, S. Side

Def'n. Chord Dist. Sta. (±)

| Def'n. | Chord Dist. | Sta. (±) |
|----------------------|-------------|-------------------------------|
| 9°24' ⁰²⁵ | | 37+09.2 = 37+08 ⁵⁴ |
| 9°17.3' | 51.18 | 37+00 |
| 8°52.3' | 51.18 | 36+50 |
| 7°47.27' | 51.18 | 36+00 |
| 7°02.3' | 51.18 | 35+50 |
| 6°17.3' | 51.18 | 35+00 |
| 5°32.28' | 51.18 | 34+50 |
| 4°47.28' | 51.18 | 34+00 |
| 4°02.3' | 51.18 | 33+50 |
| 3°17.3' | 51.18 | 33+00 |
| 2°32.30' | 51.18 | 32+50 |
| 1°47.31' | 51.18 | 32+00 |
| 1°02.31' | 51.18 | 31+50 |
| 0°17.31' | 19.62 | 31+00 |
| 30+80 ⁷⁶ | | B.C. |

T.P.

67

N. Side

Def'n. Chord

Sta. (±)

30+80.76
19.62

| | | |
|-------|-------|---------------|
| 0°00' | 08.7 | 37+08.7 E.C. |
| 0°08' | 48.87 | 37+00 |
| 0°53' | 48.87 | 36+50 |
| 1°38' | 48.87 | 36+00 |
| 2°23' | 48.87 | 35+50 |
| 3°08' | 48.87 | 35+00 |
| 3°53' | 48.82 | 34+50 (Check) |

Backed up

Inst. at E.C. Def'n's to Right

| | | |
|------------|-------|----------------|
| √ 6°17.3' | 48.87 | 34+50 |
| √ 5°37.28' | 48.87 | 34+50 T.P. (+) |
| √ 4°47.28' | 48.87 | 34+00 |
| √ 4°02.3' | 48.87 | 33+50 |
| √ 3°17.3' | 48.87 | 33+00 |
| √ 2°34.3' | 48.87 | 32+50 |
| √ 1°47.3' | 48.82 | 32+00 T.P. |
| √ 1°02.3' | 48.82 | 31+50 |
| √ 0°17.31' | 19.72 | 31+00 |

W. Pt. Loma Blvd. 5' Off.
S. Side Curve.

Sta + H.I. - Elev Grade

Cor. F

R.P.P.C. 42' From N. Prop. Line Page 66

B.M. 6.76 10.04 +3.28

31+00 12.14 -2.10 4.05
+50 12.10 -2.06 4.20

32+00 12.65 -2.61 4.33
+50 9.94 +0.10 4.44

33+00 2.15 +7.89 4.51
T.P. 9.88 17.77 2.15 7.89

+50 3.22 +14.55 4.56
34+00 4.04 +13.73 4.57

+50 9.50 +8.27 4.56
T.P. 1.45 7.56 11.66 6.11

35+00 10.57 -3.01 4.51
+50 9.42 -1.86 4.44

36+00 9.24 -1.68 4.33
+50 9.18 -1.62 4.20

37+00 9.18 -1.62 4.02
37+08⁵⁸ (E.C.) 9.26 -1.70 4.00

N. Side Curve

37+08⁵⁸ E.C. 11.33 -3.77 4.00
37+00 11.56 -4.00 4.02

36+50 10.66 -3.10 4.20
36+00 10.75 -3.19 4.33

35+50 10.86 -3.30 4.44
35+00 6.60 +0.96 4.57
T.P. 10.60 17.73 0.43 7.13

F 6.15
F 6.76
F 6.94
F 4.34
C 3.38
C 9.99
C 9.16
C 3.71

6.1 6.3
9.0 9.5
6.26
6.94
18.4
4.3 4.9 5.3
6.5 7.4 7.9
5.3
2.6
7.9

7.5
11.3
6.3
9.5
6.5
9.0 5.8
5.6 8.7
8.4 5.7
5.6

7.8 7.4
11.7 11.1
8.0 7.7 7.5 7.4
12.0 10.8 10.3 11.1
7.5 7.7 8.1 9.3
11.0 11.6 12.0 12.5
7.5 8.4 8.4
11.3 12.6 12.3
7.7 7.8
11.6 11.7
3.6
5.4

See page 79

W. Pt. Loma Blvd 5' Off.
N. Side Curve

| Sta | Hij | Elev | Grade | Cor. F. |
|---|-------|--------|--------------|----------|
| | 17.73 | | | |
| 34+50 | 4.79 | +12.94 | 4.56 | C √ 8.38 |
| Stas from 32+50 to 34+50 where omitted but tom of cut | | | | |
| 32+00 | 11.84 | +5.89 | 4.33 | C √ 1.56 |
| T.P. | -0.01 | 5.88 | 11.84 + 5.89 | |
| 31+50 | 8.23 | -7.35 | 4.72 | F 6.55 |
| 31+00 | 7.74 | -7.86 | 4.05 | F 5.91 |

30+80 B.C.

W. Pt. Loma Blvd 5' Off.
N. Side Curve

| B.M. | 5.91 | 9.19 | 3.28 | R.P.P.C | 22' From N Prop | Page 66 |
|-------|------|------|------|---------|-----------------|---------|
| 32+50 | 3.58 | 5.69 | 4.44 | C | 1.45 | |
| 33+00 | 4.37 | 4.80 | 4.51 | C | 0.29 | |
| 33+50 | 3.59 | 5.60 | 4.56 | C | 1.04 | |
| 34+00 | 3.03 | 6.16 | 4.57 | C | 1.59 | |

W. Pt. Loma Blvd Stas 23+00 to 24+16²⁹

| B.M. | 3.13 | 8.27 | 5.14 | Nail in Power Pole | W End Bridge |
|---------------------|-------|-------|------|--------------------|--------------|
| 23+00 | 11.21 | -2.94 | 2.21 | F 5.15 | |
| 23+45 ²² | 11.79 | -3.52 | 2.00 | F 5.52 | |
| 24+16 ²⁹ | 11.86 | -3.59 | 2.00 | F 5.59 | |

5.2
7.8
5.5
8.3
5.6
8.4

5.9
7.0
7.9
12.0
5.3
8.0

5.3
2.7
8.

5.6
1.8

Mentone, N. Side, 5' Off

S. Side 5' Off

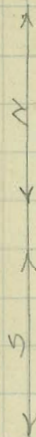
| Sta | + | H.I. | - | Ely. | Grade | Cor. F | + | H.I. | - | Ely. | Grade | Cor. F | |
|----------------|------|-------|-------|-------|-------|--------|---|-------|-------|-------|-------|--------|---|
| B.M. (base 49) | 8.00 | 65.87 | | 57.87 | | | | | | | | | |
| 0+00 | | | 4.27 | 61.60 | 60.2 | C1.4 | ✓ | 65.87 | 0.64 | 65.23 | 60.80 | C4.4 | ✓ |
| 0+10 | | | 1.94 | 63.93 | 60.5 | C3.4 | ✓ | 72.03 | 6.27 | 65.76 | 61.00 | C4.8 | ✓ |
| T.P. | 6.80 | 72.03 | 0.64 | 65.23 | | | | | | | | | |
| 0+35 | | | 7.54 | 64.49 | 61.4 | C3.1 | ✓ | 5.22 | 66.81 | 61.90 | C4.9 | ✓ | |
| 0+75 | | | 6.98 | 65.05 | 62.2 | C2.8 | ✓ | 4.32 | 67.71 | 62.70 | C5.0 | ✓ | |
| 1+15 | | | 7.74 | 64.29 | 62.2 | C2.1 | ✓ | 4.65 | 67.38 | 62.70 | C4.7 | ✓ | |
| 1+55 | | | 9.26 | 62.77 | 61.3 | C1.5 | ✓ | 5.87 | 66.16 | 61.80 | C4.4 | ✓ | |
| 1+95 | | | 11.20 | 60.83 | 59.5 | C1.3 | ✓ | 7.74 | 64.29 | 60.00 | C4.3 | ✓ | |
| 2+50 | | | 14.34 | 57.69 | 56.44 | C1.2 | ✓ | 10.95 | 61.08 | 56.94 | C4.1 | ✓ | |
| T.P. | 0.68 | 61.00 | 11.71 | 60.32 | | | 61.00 | | | | | | |
| 3+00 | | | 7.09 | 53.91 | 53.6 | C0.2 | ✓ | 3.55 | 57.45 | 54.16 | C3.3 | ✓ | |
| 3+50 | | | 11.37 | 49.63 | 50.88 | F1.3 | ✓ | 6.95 | 54.05 | 51.38 | C2.7 | ✓ | |
| 4+00 | | | 15.20 | 45.80 | 48.10 | F2.3 | ✓ | 9.86 | 51.14 | 48.60 | C2.5 | ✓ | |
| T.P. | 1.09 | 51.01 | 11.08 | 49.92 | | | 51.01 | | | | | | |
| 4+50 | | | 8.65 | 42.36 | 45.32 | F3.0 | ✓ | 1.88 | 49.13 | 45.82 | C3.3 | ✓ | |
| 5+00 | | | 10.28 | 40.73 | 42.54 | F1.8 | ✓ | 3.37 | 47.64 | 43.04 | C4.6 | ✓ | |
| 5+50 | | | 12.66 | 38.35 | 39.76 | F1.4 | ✓ | 5.30 | 45.71 | 40.26 | C5.4 | ✓ | |
| 5+90 | | | 14.85 | 36.16 | 37.53 | F1.4 | ✓ | 7.13 | 43.58 | 38.00 | C5.6 | ✓ | |
| 6+0.0 | | | 15.38 | 35.63 | 36.8 | F1.2 | ✓ | 8.16 | 42.85 | 37.70 | C5.1 | ✓ | |
| Set B.M. | | | 1.33 | 49.68 | | | Top R.P. 75' to 7 Tie Pt S.W. Cor Mentone & Carr. | | | | | | |

W. Line Camulos 5' Offset

| Sta | + | HI | - | Elev |
|---------------------|-------|-------|------|-------|
| B.M. | 11.41 | 61.09 | | 49.68 |
| 1+50 | | | 8.81 | 52.28 |
| 1+00 | | | 5.66 | 55.43 |
| 0+10 | | | 0.81 | 60.28 |
| T.P. | 9.51 | 69.79 | 0.81 | 60.28 |
| 0+00 | | | 9.30 | 60.49 |
| 0+00 | | | 6.20 | 63.59 |
| 0+10 | | | 5.55 | 64.24 |
| 0+50 | | | 3.67 | 66.12 |
| 1+00 | | | 1.46 | 68.33 |
| 1+27 ¹⁴ | | | 0.23 | 69.56 |
| B.M. ^{set} | | | 3.87 | 65.92 |

71

Top R.P. 75' S.W. Cor Mentone + Camulos Page 70



10' N. of N. Line Mentalvo

N. line Mentalvo

S. line "

N. line Alley.

50' R.P. S.W. Cor. Mentalvo + Camulos

Temecula

| Sta | + | H.I | - | ELY | Grade |
|----------|------|-------|------|---------------------|-------|
| Sta 1+00 | 3.24 | 45.74 | | 41.74 ⁴¹ | 4 |
| | | | 3.10 | 44.61 | |
| | | | 9.40 | 36.51 | |
| | | | 9.26 | 36.78 ⁴⁵ | |

S. Side, 5' Off

0+00
0+10
+40
+70
1+03Z
1+23Z
1+42Z
1+60Z
1+80Z
2+03Z
2+23Z
2+43Z
2+63Z
2+83Z
2+93Z
3+03Z
3+13Z
3+23Z

BYC.

APEX

E.V.C.

Grade Change

(160 8 3.4
5.1
39.69
1.23
39.92
1.7 79)

Page 44, So. Side
B.V.C. So. Line
B.V.C. N. Line
N. Side 0+70, Page 44

S. Side ← N. Side 5' Off

| Cor F. | ELY | Grade | Cor F. |
|--------|---------|-------|--------------------------------|
| | | | W.L. Clouis |
| | 44.07 | 41.00 | C 3.07 ✓ |
| | 43.97 | 40.65 | C 3.32 ✓ |
| | 44.37 | 40.31 | C 4.06 ✓ |
| | ⊕ 42.61 | 39.92 | C 2.69 ✓ ³⁶ |
| | 43.97 ⊗ | 39.69 | C 4.28 ✓ |
| | 43.37 | 39.22 | C 4.15 ✓ |
| | 42.97 | 38.27 | C 4.70 ✓ |
| | 41.37 | 36.81 | C 5.56 ✓ |
| | 41.07 | 34.89 | C 6.18 ✓ |
| | 40.67 | 34.46 | C 8.26 ✓ |
| | 39.67 ⊗ | 29.55 | C 10.12 ✓ |
| | 38.47 | 26.40 | C 12.07 ✓ |
| | 36.67 | 23.50 | C 13.17 ✓ |
| | 36.07 | 22.15 | C 13.92 ✓ |
| | 35.07 | 21.20 | C 13.87 ✓ |
| | 34.17 | 20.55 | C 13.62 ✓ |
| | 33.27 | 20.30 | C 12.97 ✓ |
| | | | See page 75 for these elevs |
| | | | Opp Temecula W. Pt. Loma B. |

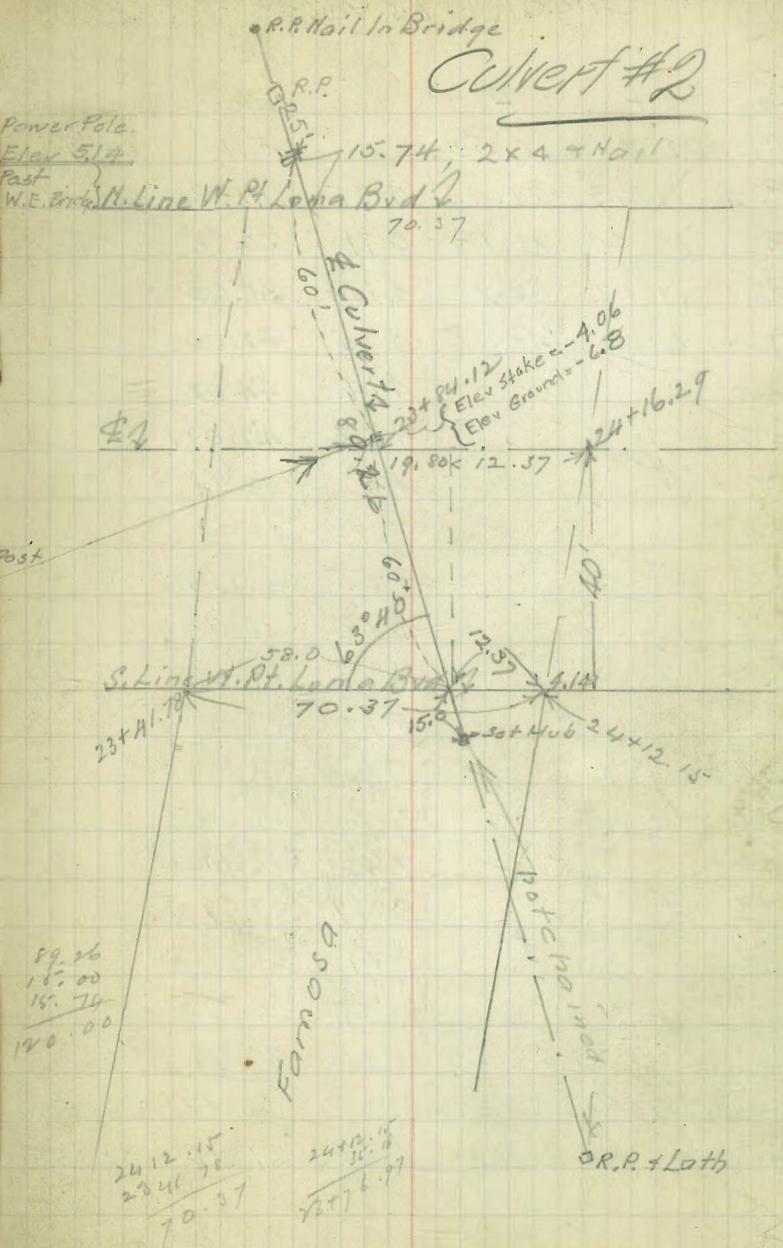
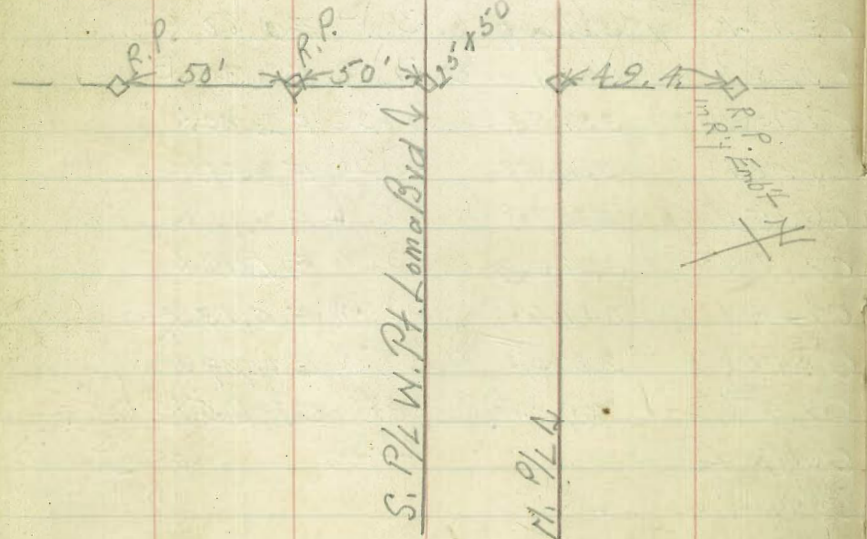
See page 75 for these elevs

Opp Temecula
W. Pt. Loma B.

Cut Off Culvert Grades Intersection
W. Pt. Loma Blvd + Famosa.

| Sta | + | HI | - | Elev | |
|-------------------------|------|-------|-------|-------|---|
| B.M. | 1.97 | 7.11 | | 5.14 | BM Nail in Power Pole W. End Bridge Elev 5.14 |
| Set B.M. | | | 5.67 | 1.44 | Nail in 3x8 Post Marked B.M. W.E. End N. Line W. Pt. Loma Blvd |
| T.P. | 3.92 | +0.73 | 10.30 | -3.19 | |
| & Intake | | | 6.33 | -5.60 | Top of Post & Culvert |
| T.P. | 4.74 | +3.11 | 2.36 | -1.63 | |
| & Outlet on B.M. | | | 8.86 | -5.75 | ch=01 BM=144 |
| B.M. | 2.86 | 4.30 | | 1.44 | Nail in 3x8 Post W. End Bridge |
| & Culvert + 1/2 Way Pt. | | | 8.36 | -4.06 | On Stake. |

| | | | | | |
|-------------------------|------|------|------|-------|-----------------------------------|
| B.M. | 2.86 | 4.30 | | 1.44 | Nail in 3x8 Post W. End Bridge |
| & Culvert + 1/2 Way Pt. | | | 8.36 | -4.06 | On Stake. |



89.26
15.00
15.74
140.00

24+12.15
2046.78
70.37

24+12.15
12.15
2376.97

173

16127 Check Levels - Temecula
S. Side

70

| Sta | + | HI | - | Elev | |
|--------------|--------|-------|-------|---------------------------|---|
| B.M. | 5.39 | 10.53 | | 5.14 | On Power Pole W. End of Bridge App - Opp Sta 22+80 W. Ft. Loma Blvd |
| T.P. | 11.23 | 21.45 | 0.31 | 10.22 | |
| T.P. | 10.44 | 31.18 | 0.71 | 20.74 | |
| T.P. | 11.12 | 42.15 | 0.15 | 31.03 | |
| T.P. | 6.16 | 48.16 | 0.15 | 42.00 | |
| 0+00 | | | 4.14 | 44.02 | |
| 0+10 | | | 4.07 | 44.091 | |
| 0+40 | | | 4.22 | 43.94 ✓ | |
| 0+70 | | | 3.73 | 44.43 ^{ob} ✓ | |
| 1+031 | B.V.C. | | 5.55 | 42.61 ✓ | |
| 1+231 | | | 4.18 | 43.98 ✓ | |
| 1+431 | | | 4.79 | 43.37 ✓ | |
| 1+631 | | | 5.17 | 42.99 ✓ | |
| 1+831 | | | 5.76 | 42.40 ✓ | |
| 2+031 | | | 7.12 | 41.04 ✓ | |
| 2+231 | | | 7.42 | 40.74 ^(0.07) ✓ | |
| 2+431 | E.V.C. | | 8.49 | 39.67 ✓ | |
| 2+631 | | | 9.74 | 38.42 ^(0.05) ✓ | |
| 2+831 | | | 11.37 | 36.79 ^(0.12) ✓ | |
| T.P. | 6.42 | 43.20 | 11.38 | 36.78 | |
| T.P. on B.M. | 1.76 | 34.69 | 10.27 | 32.93 | B.M. Elev = 32.68 (.25 Error) B.M. = 25' Tie Point Sta 13+97 ²⁹ W. Ft. Loma Blvd |
| B.M. | | 6.73 | 27.96 | 27.97 | B.M. Elev = 27.97 B.M. = 25' Tie E.C. Sta 11+11 ³⁸ W. Ft. Loma Blvd Refer to Page 35 |

Check Levels, Temecula
N. Side

| Sta | + | H.I | - | Flv |
|---------------|------|-------|-------|-------|
| T.P. | 2.96 | 44.96 | | 42.00 |
| 0+10 | | | 7.07 | 37.89 |
| 0+40 | | | 7.75 | 37.71 |
| 0+70 | | | 7.76 | 37.70 |
| 1+08 I | | | 8.47 | 36.49 |
| 1+23 I | | | 8.85 | 36.11 |
| 1+43 I | | | 9.43 | 35.53 |
| 1+63 I (T.P.) | | | 10.29 | 34.67 |
| | 5.29 | 39.96 | | |
| 1+83 I | | | 6.18 | 33.78 |
| 2+03 I | | | 7.43 | 34.53 |
| 2+23 I | | | 8.50 | 31.46 |
| 2+43 I | | | 9.45 | 30.51 |
| 2+63 I | | | 10.70 | 29.76 |

Page 7A

Notes:

0+00 = W. P/L of Clovis

75
07

Clovis to Camulos

Montalvo. S. Side, 5' Off

| Sta | + | H.I. | - | Elv | Grade |
|---------------------|-------|-------|------|-------|---------------|
| B.M. | 6.39 | 48.73 | | 42.34 | |
| T.P. | 10.80 | 56.34 | 3.19 | 45.54 | |
| T.P. | 11.50 | 67.53 | 0.31 | 56.03 | |
| 3rd B.M. | 12.07 | 77.56 | 2.04 | 65.49 | Nail in |
| 0+00, E. 1/4 Clovis | | | 8.98 | 68.58 | |
| 0+10 | | | 7.20 | 70.36 | |
| 0+57 | | | 2.46 | 75.10 | |
| 0+97 | | | 1.20 | 76.36 | |
| 1+37 | | | 1.06 | 76.50 | |
| 1+77 | | | 3.50 | 74.06 | |
| 2+17 | | | 4.03 | 73.53 | |
| 2+50 | | | 5.80 | 71.76 | |
| 3+00 | | | 8.30 | 69.46 | |
| T.P. | 1.13 | 68.95 | 9.74 | 67.82 | |
| 3+50 | | | 1.94 | 67.01 | |
| 4+00 | | | 2.70 | 66.75 | |
| 4+50 | | | 2.51 | 66.44 | |
| 5+00 | | | 2.75 | 66.20 | |
| 5+50 | | | 3.48 | 65.47 | |
| 5+90 | | | 4.76 | 64.19 | |
| 6+00 | | | 5.71 | 63.24 | |
| B.M. | | | 3.04 | 65.91 | 50' R.P. Hub. |

N. Side, 5' Off.

76

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| H.I. | Elv | Grade | Cor F |
|-------|------|--------|--|
| 77.56 | 9.68 | 167.89 | |
| | 7.18 | 170.38 | |
| | 2.53 | 175.03 | |
| | 1.28 | 176.78 | |
| | 1.57 | 175.99 | |
| | 3.45 | 174.11 | |
| | 5.66 | 171.90 | |
| | 6.50 | 71.06 | |
| | 9.73 | 67.89 | |
| 68.95 | 3.41 | 165.54 | |
| | 4.76 | 164.19 | |
| | 5.31 | 163.64 | |
| | 5.87 | 163.09 | |
| | 6.66 | 162.29 | |
| | 8.09 | 160.86 | |
| | 9.16 | 159.79 | |
| | | | 50' W. Cor Montalvo + Camulos Elev=65.92 |

H.I. Montalvo + Clovis, page 71.

Check Fill, W. Pt. Loma Brd.

9.44
4.20

77

| Sta | + | HI | - | Elev | |
|------|-------------------|-------|-------|-------|--|
| B.M. | 1.23 | 28.85 | | 27.62 | Nail in Pole N.W. Cor W. Pt. Loma + Seaside Page 32. |
| 0+00 | Top. of Pavement. | 3.19 | 25.66 | 25.70 | |
| 0+39 | | 4.96 | 23.89 | 23.32 | C. 0.57 |
| 0+78 | | 5.62 | 23.23 | 20.95 | C. 2.28 |
| 1+15 | | 7.59 | 21.26 | 18.97 | C. 2.29 |
| 1+58 | | 11.06 | 17.79 | 17.40 | C. 0.39 |
| 1+98 | | 13.44 | 15.41 | 16.42 | F. 1.01 |

W. Pt. Loma Blvd.

Sta + H.I - Elev Grade

South Side, 5' Off

B.M. 5.55 8.83 3.28

T.P. 5.95 5.23 9.55 -0.72

set B.M. 1.99 ~~3.27~~ B.M. Nail

37+50 6.4 -1.2 3.26

38+00 5.9 -0.7 3.13

38+50 5.5 -0.3 2.99

39+00 4.8 +0.4 2.83

39+50 5.2 0.00 2.66

40+00 4.5 +0.7 2.47

40+10^s 4.51 +0.7

T.P. 4.20 4.92 4.51 0.72

set B.M. 8.15 8.53 4.54 0.38

set B.M. 5.26 11.53 2.26 6.27

B.M. 5.28 6.25 U.S.G.S - B.M. Marked F. 61 - Date 1927

#3 Culvert, 100' long.

37+95^{SE} #3 Culvert 13.14

" Inlet Flow Line (Profile) -0.5

" Outlet " -1.0

H.I - Elev Grade Corf

N. Side 5' Off

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Middle bent on top 12x14 S side of Bridge No BA-80

5.23 8.1 -2.9 3.26 F6.16 $\frac{7.3}{10.9}$

6.7 7.0 -1.8 3.13 F4.93 $\frac{7.8}{11.7}$

5.9 8.5 -3.3 2.99 F6.29 $\frac{7.3}{11.0}$

5.0 8.8 -3.6 2.83 F6.43 $\frac{7.0}{10.5}$

4.9 8.4 -3.2 2.66 F5.86 $\frac{6.5}{9.8}$

4.3 8.3 -3.1 2.47 F5.57 $\frac{6.2}{9.3}$

2.7 8.2 -3.0

Sta 48+13^s R.P. 100' from old S Pk of old alignment of W. Pt. Loma Blvd.

Trolley Pole Between tracks app-opp Sta 51+00

B.M. Marked F. 61 - Date 1927

See page 68

37+08^{SE}
87
37+95^{SE} = # Culvert #3

10.55
4.74
5.81

10.55
4.83
5.72

10.55
5.1
5.15
3
5.7

5.87
2.99

8.86

Going West

| Sta | + | # | 1 | - | Elev |
|------|-------|-------|---|---|-------|
| 0+00 | H. 99 | 19.88 | | | 14.89 |
| 0+20 | | | | | 5.85 |
| 0+20 | (now) | | | | 6.12 |
| 0+40 | | | | | 7.03 |
| | | | | | 8.34 |

100) 1.000
960
400
360

.00833

288
2.000
1.99
007

W. End Elev 1.44
11+11 38 EC. " 27.97
End Fence Mont. No. 4240

24+88
23+46.92
23+45.92
84.12
1772.4
1x14.6

Distance // slope stake from side stake for any width roadway, slope stake is located by the double end of the left column and top row. The number in body of the table is the number of the stake in the row and column.

Hub
IMPROVED TABLES
AND
INFORMATION

TABLE No. 2
To find Tangent and External of curve of any other degree, divide by degree and add correction found in column of correction. Degree of curve with a given I may be found by dividing tangent (or external) opposite I by given tangent (or external).
The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

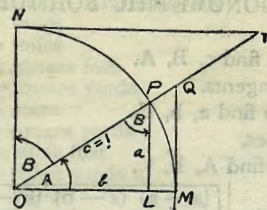


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol} = \frac{h}{6} (B + b + 4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|
| $\frac{1}{16}$ | .0052 | .0885 | .1719 | .2552 | .3385 | .4219 | .5052 | .5885 | .6719 | .7552 | .8385 | .9219 |
| $\frac{1}{8}$ | .0104 | .0938 | .1771 | .2604 | .3438 | .4271 | .5104 | .5938 | .6771 | .7604 | .8438 | .9271 |
| $\frac{3}{16}$ | .0156 | .0990 | .1823 | .2656 | .3490 | .4323 | .5156 | .5990 | .6823 | .7656 | .8490 | .9323 |
| $\frac{1}{4}$ | .0208 | .1042 | .1875 | .2708 | .3542 | .4375 | .5208 | .6042 | .6875 | .7708 | .8542 | .9375 |
| $\frac{5}{16}$ | .0260 | .1094 | .1927 | .2760 | .3594 | .4427 | .5260 | .6094 | .6927 | .7760 | .8594 | .9427 |
| $\frac{3}{8}$ | .0313 | .1146 | .1979 | .2813 | .3646 | .4479 | .5313 | .6146 | .6979 | .7813 | .8646 | .9479 |
| $\frac{7}{16}$ | .0365 | .1198 | .2031 | .2865 | .3698 | .4531 | .5365 | .6198 | .7031 | .7865 | .8698 | .9531 |
| $\frac{1}{2}$ | .0417 | .1250 | .2083 | .2917 | .3750 | .4583 | .5417 | .6250 | .7083 | .7917 | .8750 | .9583 |
| $\frac{9}{16}$ | .0469 | .1302 | .2135 | .2969 | .3803 | .4635 | .5469 | .6302 | .7135 | .7969 | .8802 | .9635 |
| $\frac{5}{8}$ | .0521 | .1354 | .2188 | .3021 | .3854 | .4688 | .5521 | .6354 | .7188 | .8021 | .8854 | .9688 |
| $\frac{11}{16}$ | .0573 | .1406 | .2240 | .3073 | .3906 | .4740 | .5573 | .6406 | .7240 | .8073 | .8906 | .9740 |
| $\frac{3}{4}$ | .0625 | .1458 | .2292 | .3125 | .3958 | .4792 | .5625 | .6458 | .7292 | .8125 | .8958 | .9792 |
| $\frac{13}{16}$ | .0677 | .1510 | .2344 | .3177 | .4010 | .4844 | .5677 | .6510 | .7344 | .8177 | .9010 | .9844 |
| $\frac{7}{8}$ | .0729 | .1563 | .2396 | .3229 | .4063 | .4896 | .5729 | .6563 | .7396 | .8229 | .9063 | .9896 |
| $\frac{15}{16}$ | .0781 | .1615 | .2448 | .3281 | .4115 | .4948 | .5781 | .6615 | .7448 | .8281 | .9115 | .9948 |
| 1 | .0833 | .1667 | .2500 | .3333 | .4167 | .5000 | .5833 | .6667 | .7500 | .8333 | .9167 | 1.0000 |
| | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |

TABLE IV
USEFUL RELATIONS

| | | |
|---------------|-----------|----------------|
| Lineal feet | ×.00019 | = miles |
| Lineal yards | ×.0006 | = miles |
| Square inches | ×.007 | = square feet |
| Square feet | ×.111 | = square yards |
| Square yards | ×.0002067 | = acres |
| Acres | ×4840 | = square yards |
| Cubic inches | ×.00058 | = cubic feet |
| Cubic feet | ×.03704 | = cubic yards |
| Links | ×.22 | = yards |
| Links | ×.66 | = feet |
| Feet | ×1.5 | = links |

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790''$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

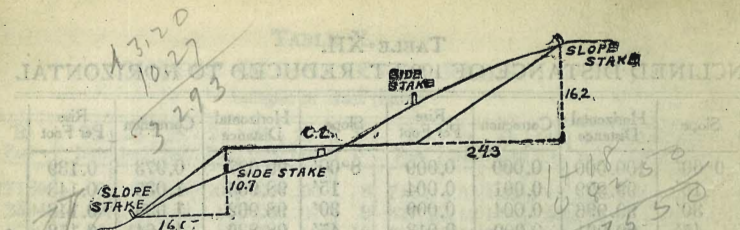
a = angle of elevation for mid Reading

3.11
1.64
1.45
8.86
3.11
5.75

5.23

4.54

7.2



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0 00 | 0 15 | 0 30 | 0 45 | 0 60 | 0 75 | 0 90 | 1 05 | 1 20 | 1 35 |
| 1 | 1 50 | 1 65 | 1 80 | 1 95 | 2 10 | 2 25 | 2 40 | 2 55 | 2 70 | 2 85 |
| 2 | 3 00 | 3 15 | 3 30 | 3 45 | 3 60 | 3 75 | 3 90 | 4 05 | 4 20 | 4 35 |
| 3 | 4 50 | 4 65 | 4 80 | 4 95 | 5 10 | 5 25 | 5 40 | 5 55 | 5 70 | 5 85 |
| 4 | 6 00 | 6 15 | 6 30 | 6 45 | 6 60 | 6 75 | 6 90 | 7 05 | 7 20 | 7 35 |
| 5 | 7 50 | 7 65 | 7 80 | 7 95 | 8 10 | 8 25 | 8 40 | 8 55 | 8 70 | 8 85 |
| 6 | 9 00 | 9 15 | 9 30 | 9 45 | 9 60 | 9 75 | 9 90 | 10 05 | 10 20 | 10 35 |
| 7 | 10 50 | 10 65 | 10 80 | 10 95 | 11 10 | 11 25 | 11 40 | 11 55 | 11 70 | 11 85 |
| 8 | 12 00 | 12 15 | 12 30 | 12 45 | 12 60 | 12 75 | 12 90 | 13 05 | 13 20 | 13 35 |
| 9 | 13 50 | 13 65 | 13 80 | 13 95 | 14 10 | 14 25 | 14 40 | 14 55 | 14 70 | 14 85 |
| 10 | 15 00 | 15 15 | 15 30 | 15 45 | 15 60 | 15 75 | 15 90 | 16 05 | 16 20 | 16 35 |
| 11 | 16 50 | 16 65 | 16 80 | 16 95 | 17 10 | 17 25 | 17 40 | 17 55 | 17 70 | 17 85 |
| 12 | 18 00 | 18 15 | 18 30 | 18 45 | 18 60 | 18 75 | 18 90 | 19 05 | 19 20 | 19 35 |
| 13 | 19 50 | 19 65 | 19 80 | 19 95 | 20 10 | 20 25 | 20 40 | 20 55 | 20 70 | 20 85 |
| 14 | 21 00 | 21 15 | 21 30 | 21 45 | 21 60 | 21 75 | 21 90 | 22 05 | 22 20 | 22 35 |
| 15 | 22 50 | 22 65 | 22 80 | 22 95 | 23 10 | 23 25 | 23 40 | 23 55 | 23 70 | 23 85 |
| 16 | 24 00 | 24 15 | 24 30 | 24 45 | 24 60 | 24 75 | 24 90 | 25 05 | 25 20 | 25 35 |
| 17 | 25 50 | 25 65 | 25 80 | 25 95 | 26 10 | 26 25 | 26 40 | 26 55 | 26 70 | 26 85 |
| 18 | 27 00 | 27 15 | 27 30 | 27 45 | 27 60 | 27 75 | 27 90 | 28 05 | 28 20 | 28 35 |
| 19 | 28 50 | 28 65 | 28 80 | 28 95 | 29 10 | 29 25 | 29 40 | 29 55 | 29 70 | 29 85 |
| 20 | 30 00 | 30 15 | 30 30 | 30 45 | 30 60 | 30 75 | 30 90 | 31 05 | 31 20 | 31 35 |
| 21 | 31 50 | 31 65 | 31 80 | 31 95 | 32 10 | 32 25 | 32 40 | 32 55 | 32 70 | 32 85 |
| 22 | 33 00 | 33 15 | 33 30 | 33 45 | 33 60 | 33 75 | 33 90 | 34 05 | 34 20 | 34 35 |
| 23 | 34 50 | 34 65 | 34 80 | 34 95 | 35 10 | 35 25 | 35 40 | 35 55 | 35 70 | 35 85 |
| 24 | 36 00 | 36 15 | 36 30 | 36 45 | 36 60 | 36 75 | 36 90 | 37 05 | 37 20 | 37 35 |
| 25 | 37 50 | 37 65 | 37 80 | 37 95 | 38 10 | 38 25 | 38 40 | 38 55 | 38 70 | 38 85 |
| 26 | 39 00 | 39 15 | 39 30 | 39 45 | 39 60 | 39 75 | 39 90 | 40 05 | 40 20 | 40 35 |
| 27 | 40 50 | 40 65 | 40 80 | 40 95 | 41 10 | 41 25 | 41 40 | 41 55 | 41 70 | 41 85 |
| 28 | 42 00 | 42 15 | 42 30 | 42 45 | 42 60 | 42 75 | 42 90 | 43 05 | 43 20 | 43 35 |
| 29 | 43 50 | 43 65 | 43 80 | 43 95 | 44 10 | 44 25 | 44 40 | 44 55 | 44 70 | 44 85 |
| 30 | 45 00 | 45 15 | 45 30 | 45 45 | 45 60 | 45 75 | 45 90 | 46 05 | 46 20 | 46 35 |
| 31 | 46 50 | 46 65 | 46 80 | 46 95 | 47 10 | 47 25 | 47 40 | 47 55 | 47 70 | 47 85 |
| 32 | 48 00 | 48 15 | 48 30 | 48 45 | 48 60 | 48 75 | 48 90 | 49 05 | 49 20 | 49 35 |
| 33 | 49 50 | 49 65 | 49 80 | 49 95 | 50 10 | 50 25 | 50 40 | 50 55 | 50 70 | 50 85 |
| 34 | 51 00 | 51 15 | 51 30 | 51 45 | 51 60 | 51 75 | 51 90 | 52 05 | 52 20 | 52 35 |
| 35 | 52 50 | 52 65 | 52 80 | 52 95 | 53 10 | 53 25 | 53 40 | 53 55 | 53 70 | 53 85 |
| 36 | 54 00 | 54 15 | 54 30 | 54 45 | 54 60 | 54 75 | 54 90 | 55 05 | 55 20 | 55 35 |
| 37 | 55 50 | 55 65 | 55 80 | 55 95 | 56 10 | 56 25 | 56 40 | 56 55 | 56 70 | 56 85 |
| 38 | 57 00 | 57 15 | 57 30 | 57 45 | 57 60 | 57 75 | 57 90 | 58 05 | 58 20 | 58 35 |
| 39 | 58 50 | 58 65 | 58 80 | 58 95 | 59 10 | 59 25 | 59 40 | 59 55 | 59 70 | 59 85 |
| 40 | 60 00 | 60 15 | 60 30 | 60 45 | 60 60 | 60 75 | 60 90 | 61 05 | 61 20 | 61 35 |
| 41 | 61 50 | 61 65 | 61 80 | 61 95 | 62 10 | 62 25 | 62 40 | 62 55 | 62 70 | 62 85 |
| 42 | 63 00 | 63 15 | 63 30 | 63 45 | 63 60 | 63 75 | 63 90 | 64 05 | 64 20 | 64 35 |
| 43 | 64 50 | 64 65 | 64 80 | 64 95 | 65 10 | 65 25 | 65 40 | 65 55 | 65 70 | 65 85 |
| 44 | 66 00 | 66 15 | 66 30 | 66 45 | 66 60 | 66 75 | 66 90 | 67 05 | 67 20 | 67 35 |
| 45 | 67 50 | 67 65 | 67 80 | 67 95 | 68 10 | 68 25 | 68 40 | 68 55 | 68 70 | 68 85 |
| 46 | 69 00 | 69 15 | 69 30 | 69 45 | 69 60 | 69 75 | 69 90 | 70 05 | 70 20 | 70 35 |
| 47 | 70 50 | 70 65 | 70 80 | 70 95 | 71 10 | 71 25 | 71 40 | 71 55 | 71 70 | 71 85 |
| 48 | 72 00 | 72 15 | 72 30 | 72 45 | 72 60 | 72 75 | 72 90 | 73 05 | 73 20 | 73 35 |
| 49 | 73 50 | 73 65 | 73 80 | 73 95 | 74 10 | 74 25 | 74 40 | 74 55 | 74 70 | 74 85 |
| 50 | 75 00 | 75 15 | 75 30 | 75 45 | 75 60 | 75 75 | 75 90 | 76 05 | 76 20 | 76 35 |

Computed by L. Leland Locke.

4594
5168
7.9
40.26
39.4
8

5.3
2.8
7.9

5.4
2.6
8.0

5.4
2.7

40.97
39.4
1.57

5.4
2.7
8.1

5.5
2.7
8.2

4.74
1.63
3.11

45.94
4.97
40.97
2.6
7.1

45.94
3.31
42.63

40.47
2.6
2.1

SE top 419

$107 \frac{118}{25275}$ SW of pile of
 1000 E Bridge S side
 51.8
 2.9
 8.7

27.96
 27.705
 74
 $1023 + 8413$
 19.8
 8.27

100
 25
 197
 32
 8
 37
 $23 + 71$
 $37 + 08$

$374 + 0392$
 94
 25750
 $86 + 46$
 08
 3.52
 11.86
 8.27

89.76
 15
 104
 15
 20.00
 20.00
 130130
 63045
 89.44
 88.45
 10.30
 711
 3.19
 3.59

130130
 63045
 89.44
 88.45
 10.30
 711
 3.19
 3.59
 $25 + 50$
 $23 + 18$
 $2 + 3$
 188
 900
 20

2.48
 2.55
 25.23
 5.19
 2.48
 2.71
 596
 72
 324
 443
 195
 2.48
 5.23
 7.30
 1.99
 2.01
 3.24
 5.29
 2.01
 36
 328
 117.8
 10.4

2.4
 2.7
 21.9
 $.0564$
 87.6
 25
 1314
 61.3
 4.01
 476.7
 10
 486.7
 125
 361.7
 161
 98
 8
 2.7
 6.33
 73
 2.36
 73
 392
 319
 0.06
 9.90
 73
 8.36
 4.30
 106
 10.94
 0.827
 0.148
 28
 5.85
 45.94
 3.31

$25 + 50$
 1.63
 1.78
 2.01
 8.36
 4.30
 106
 10.94
 0.827
 0.148
 28
 5.85
 45.94
 3.31

$25 + 50$
 1.78
 2.01
 $25 + 50$
 1.78
 2.01
 $25 + 50$
 1.78
 2.01
 $25 + 50$
 1.78
 2.01