



5/11/36

Scriber

C" Line

Sta 4+50 - 4+00	50 x 0.7 x 3
4+00 - 3+88	12 x 0.7 x 3
3+88 - 3+78	10 x 2.8 x 3
3+78 - 3+68	10 x 1.8 x 3
3+56 - 3+50	6 x 1 x 3
3+48 - 3+43	5 x 1.5 x 3
3+07 - 3+37	30 x 1.5 x 3
3+05 - 2+85	20 x 2.7 x 3
2+85 - 2+78	7 x 5.4 x 3
2+73 - 2+64	12 x 5.5 x 3
2+61 - 2+54	7 x 2 x 3
	15 x 5.4 x 3

B.F. "A" Line RH to MH36

13 x 3 x 6
13 x 2 x 6
13 x 3.2 x 6
9 x 1.5 x 6

= 5.065  
5.15  
5.80

5.30  
4.785  
1.515

R.H. B.F.  
10 x 1 x 4.5 =

1.03  
5.17

"A" π 5.16

"B" π = 5.175  
A 4.795  
0.386

5.70  
5.16  
0.54

"B" 5.70  
5.4

A π 5.145  
5.690  
5.45

B π 5.30  
5.30  
5.45  
4.755  
4.9  
5.30  
5.2  
4.78

999

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
ENGINEERING and DRAFTING SUPPLIES  
IRVING PARK STATION  
CHICAGO, ILL.

MICROFILMED

APR 12 1965

$$\begin{array}{r} 8.05 \\ 6.30 \\ \hline 14.35 \\ 12.65 \\ \hline 1.70 \\ 1.70 \end{array}$$

$$\begin{array}{r} 8.05 \\ 6.30 \\ \hline 14.35 \\ 12.65 \\ \hline 1.70 \\ 1.70 \\ \hline 0.85 \end{array}$$

$$\begin{array}{r} 1.70 \\ 1.70 \\ \hline 0.85 \end{array}$$

$$\begin{array}{r} 6.30 \\ 8.05 \\ \hline 14.35 \\ 1.70 \\ \hline 1.70 \end{array}$$

INDEX

PAGE

"A" Line Grades. Sewer N. Adams Ave & Mt View Dr.	1-24
" " " " " "	26-39
	64-76
Estimates work done on project	
"A" Line "C" Line, "F" Line pump house	
Sewer N. Adams Ave & Mt. View Dr.	40-63
Elevs at Pump House " "	5
Revised levels and grades "A" Line	
Sta 0+98 - Sta 4+50	33 & 13
Relocation MH #39 "A" Line	14 & 66
"F" Line Grades. Sewer N of Adams & Mt View	25, 36
	72
"C" Line " " " " " "	30, 38, 39
	65-69, 70-76

WPA #2353  
SEWER, N. ADAMS AVE.

Clear  
Mch 6-36  
McC  
Walker  
Elev F.L. Gr.

STA	+	H. 1	-	Elev	F.L. Gr.
14+50	3.62	44.66		41.04	30.69
14+22			6.98	37.68	30.90
14+00		44.65	0.78	43.88	30.95
14+22	} 0.44		6.98	37.67	
MH 38		44.63	3.84	40.79	31.31
13+80					31.09
13+37					31.28

Mch 6-36

11+50	1.04	42.43		41.39	32.27
12+00			1.06	41.37	32.01
T.P.	8.45	50.27	0.61	41.82	
			9.17	41.10	31.31
		41.06			
M.H. 38					31.31
14+50	0.55	41.94	0.02	41.04	32.27
			8.86	33.08	
8+50	0.39	41.06		40.67	33.80
MH 39				41.04	32.96
	0.55				

Indexed

1

Gr. Rod	Cut or F. H.
	10.35
	1
	End pipe
	12.92
	9.48
for 1" High	12.54
	C 1.00
for 1" High	12.35
	C 1.00
	9.12
	9.05
	C 9.36
	C 9.48
	C 9.79
	C 9.12
	0.86 Above F. L.
	C 6.81
	08

A Line

STA + H<sub>11</sub> - Elev F.L.

12+00 0.22 41.28 41.06 32.01 ✓ C. 9.05

11+50 0.55 40.73 32.27 ✓

MH#38 7.66 46.45 ✓ <sup>H<sub>16</sub></sup> 40.79 33.31 MH#38 - C. 9.48

T.P. 3.40 41.36 10.49 37.96 ✓

12+00 0.28 41.08 32.01 ✓ C. 9.07 Moore C. 9.05 check 0.02

12+04 8.51 <sup>Str. Line</sup> 32.85 <sup>F.L.</sup> 31.99 ✓

11+50 8.22 33.14 32.27 ✓ 0.86 Above F.L.

11+50 0.61 40.75 32.27 C. 8.48 H<sub>16</sub> 0.86

T.P. 2.76 39.37 5.85 36.51

9+70.35 2.83 36.54 33.18 C. 2.23

9+70.35 5.98 41.39 35.41 33.18 C. 2.23

T.P. 3.46 37.93

32.85 32.85

11+50 0.67 40.72 32.27

0.35 41.04 New cut C. 8.45 Old cut C. 9.12

12+00 1.21 42.29 41.08 32.01 C. 9.07

12+04 9.61 32.68 31.99 ✓ Top pipe (F.L. <sup>set</sup> 31.93) should be 31.99

11+80 9.55 32.74 32.12 ✓ Top pipe (F.L. <sup>set</sup> 31.99) " " 32.12

11+50 9.31 32.98 32.27 ✓ " (F.L. <sup>set</sup> 32.23) " " 32.27

"A" Line

3-10-35

W. McCarty  
C. Walker

STA.	+ H.I.	-	Elev.
B.M.	8.14	354.97	346.83
		11.41	343.56
6+00.		11.74	43.23
5+50		12.90	42.07
4+50		7.13	47.84
4+00		8.88	46.09
B.M.	0.87	344.43	343.56
6+37			35.77
6+37		1.19	43.24
6+10		8.52	35.91
6+00		8.47	
5+87		8.40	
5+50		8.21	36.22
	7.74	351.30	343.56
7+00		3.01	348.29
B.M. T.P.	1.99	342.37	10.92 340.38
M.H. Hub		0.41	341.96
String Br.		7.17	35.20

Grade 5.12%

B.M. established 3/10/36 1' NE. of Century plant STA 6+38

Offset Hub 6' in path Mark C 8.16 C 8.13

" C 6.86 C 6.71

" C 12.12 C 11.98

" C 12.12 C 11.98

C 10.10 C 9.97

Portal Tunnel

Hub on line at top tunnel

Mark C 13.75 C 13.71

20' E of M.H. 41

Mark C 7.72

28623

"A" Line N. Adams Ave

4

STA	+	H.I.	-	Elev.	F.L.	
MH #38	0.44	41.23		40.79	31.31	Mark 9.48.
			9.09	32.14		End of pipe Top Bell
			9.04	32.19	31.33	4' s. MH.
			8.97	32.26	31.40	17' s MH.

17+84  
MH #36 4.94 44.08 4 39.14 28.96 C. 10.18

T.P. 1.24 40.94 4.38 39.70

18+44 11.91 3 28.65 Too close to read

18+48 11.91 29.03 28.63

18+56 11.93 28.59 0.12

40.94 = H.I.  
11.93 6" C.I.  
29.01 = Top pipe  
54  
28.47 = Bottom "

B.M. 6.95 360.38 353.43 Near P.H.

6.35 354.03 28.62 C 25.42

18+54 8.46 51.92 28.60

(Copy from scratch Book)

Feb 10-36  
Partly CloudyJ. McCarty  
H. Walker

Exist MH Foot of 29th St	12.40	<del>340.77</del>		<del>38.67</del>		
P.L.			12.10	38.67	38.10	Flow Line
MH #45	6.10	351.64		45.54		
0+00			13.90	38.64	38.07	
MH #45	5.42	350.96		45.54	37.67	
End of Exist Sewer			12.63	38.33	37.76	
			4.95	346.01	37.40	
MH #45	5.20	50.74		45.54	37.78	
Top pipe 1450			12.40	38.34		
			4.73	46.01		

Diff. in elev MH #42  
= Line = 0.16 Low,  
0.20 to be gained.

45.59 Elev of 6" Offs.

MH #45  
Makes elev exist sew = 37.83  
37.92 - 37.83 = 0.09 Low

Top of 6" Sewer.

6' Offset. Hub.

Top 6" Sewer P. Line

C. 7.87.

37.92 - 37.76 = 0.16 Low

37.93 = Grade given

C. 8.61 Check to 0.01 Stake Marked C. 8.62

Check to 0.01

37.92 - 37.78 = 0.14 Low

Adjustment  $\nabla$ 

3-11-36

Clear  
McCarty  $\nabla$   
Walker Rod

5

"A" 4.805

25 ft from  $\nabla$ 

"B" 3.41

325 ft  $\nabla$ 

"A" Line N. of Adams Ave.

12+00	0.11	341.18		341.07	32.01	C. 3.06	
T.P.	4.31	340.53	4.96	336.22	32.01		
11+50			0.39	40.14	32.27	C. 7.87	Offset. 4.8
New Line 11+25			5.15	35.38	32.40		
T.P. 11+00	5.13	40.85	4.81	35.72	32.53	C. 3.19	
10+75			4.94	35.91	32.65	C. 3.20	
10+50			5.25	35.60	32.78	C. 2.82	
10+00			4.94		32.91 <sup>8</sup>	C. 3.00	
9+83			4.85		33.00		
9+80			4.81	36.04	33.02		
9+70.35			5.43	3	33.18	C. 2.23	35.41 = Elev Hook

4-21-36.

B.M.	3.76	351.19		353.43		
SE. cor			5.75	351.44		Pump House Top
SW "			5.75	351.44		" " "
NW "			5.74	351.45		" " "
NE "			5.80	351.39		
			5.29	351.90		Pump House Hatch
			15.80	341.39		Top of slab Top floor. Check Again 41.25



Project 2353. 3-12-36  
Sewer Copley & Mt. View W. McCarty  
Drive. C.L. Walker T

"A" Line

STA	+ 11.1	-	Elev	F.L.
B.M.	0.94	44.50		343.56
6+28	0.94		Sta. Gr. 8.58	35.84 34.96

B.M. 2.01 348.84 346.83 On stump opp. Sta 5+39

5+50 Hub. 6.82 342.02 35.36

5+44 10.04 46.29 12.59 336.25 35.39 Tap Bell

336.25 Tap Bell  
86  
335.39 O.K !!!

6+00 10.34 35.95 35.10 35.95  
86  
35.09

5+75 10.22 36.07 35.23 36.07  
86  
35.21

B.M. 4.53 351.36 346.83 on stump.

A+50 3.53 347.83 35.86 Mark C 12.12 C 11.97 0.15 Diff.

A+00 5.28 46.08 36.12 C 10.10 C 9.96 0.14 Diff

B.M. 8.73 355.56 346.83

3+50 8.60 346.96 36.37 C 10.71 C 10.59 0.12 Diff

T.P. 11.76 354.97 12.35 343.21

1+50 9.03 45.94 37.40 C 8.62 C 8.54 0.08 "

MH #45 9.48 45.49 37.67 C 7.87 C 7.82 0.05 "

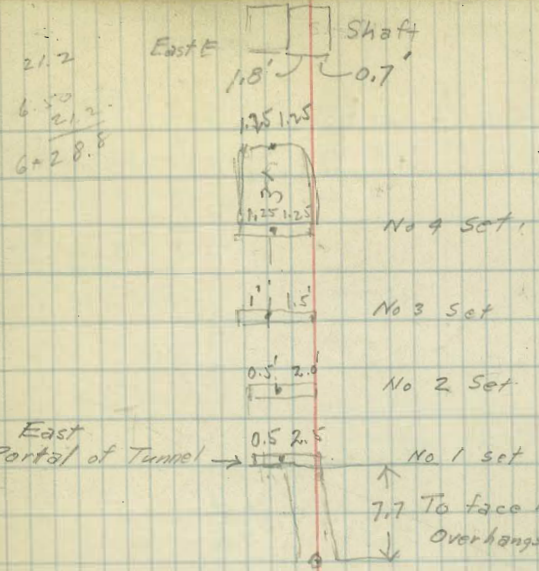
T.P. 8.51 360.33 3.15 351.82

3.52 356.81 B.M. 356.95 0.14 Diff.

"A" Line      3-12-36  
 STA.      "A" Line      Elev.

6+15.8					
6+00					
5+78.8	23'	10°48'			
6+78.8					Check on Conc Pipe
9+70	4.87	340.28	335.41		
10+13		6.475	33.805	32.955	
10+25		6.52.0			
10+34		6.55.0			
10+04		6.62	333.66	32.93	

E. Edge Shaft



0 2.23 Herb  
 Top Bell  
 " "  
 " "

"A" Line:

3-13-36,  
McCarty  
Wallace

STA	" +	H.I.		
1	1.81	342.19		340.38
7+60			0.25	341.94
7+47			7.97	34.27 34.34
T.P.	2.12	37.61	6.70	35.49
7+34				34.21 34.40
	0.31	41.10		<sup>40.79</sup> 31.31
4' S of MH			8.95	32.15 31.27
± 38		Top Bell	8.88	32.09 31.21
22.5 "			8.79	
22.5 "			9.84	
4' S of MH			9.93	

B.17 20' E MH 41

C.7.72

9.13

32.15  
86  
31.29

0.02 High 9' W. of MH

C 9.48

C 9.03 Top Bell

Top Bell

Bottom Bell

Bottom Bell

Deq Adjustment.

"A"	5.09		
"B"		3.13	= 1.96
"B"	5.08	7.05	= 1.98

MH 38	3.98	44.17		40.79 31.31
13+50			2.03	42.14 31.21
			12.04	32.13 31.29
			12.07	32.10 31.32
			12.00	32.17 31.42

C.9.48

.93

2' from C of MH on low side

Top Bell

2 " " " " High "

Top pipe

Top Pipe 21' Back from MH

353.43  
3501  
358.44

"A" Line

3-16-36

STA	+	H.I.	-	Elev.	F.L.
	5.01	358.44		353.43	
			7.01	351.43	
					328.25
18+50			4.40	354.04	28.62
			10.79	347.65	
	0.26	42.25		41.99	34.27
			1.82	40.43	
T.P.	0.90	36.46	6.69	35.56	34.4
7+33				2.06	34.40
7+3					
B.M. 6+37	0.90	344.46		343.56	
T.P.	1.07	337.82	7.71	336.75	
6+36			1.70	36.12	334.91
6+30					334.94
6+51					334.83
	0.02	43.85		43.83	
5+11			7.57	36.28	35.54
4+78			7.39	36.46	35.72
5+16			7.63	36.22	

B.M. 12' E of Pump House

B.M. NE. Cor Pump House

C. 25.42

35.10

C. 7.72

Hub 4' E of Portal W.

Nail in brace on N. side 2' from Portal of tunnel.

On 1st set Rt Hand past Set string Ga. 35.77

35.80 = Str. Grade Set

Blue keel mark on post S. side tunnel G. = 35.69

9-21-36

Top pipe

Top pipe

Top pipe

36.56

35.71

32  
56

"A" Line

3-17-36

36.49  
33.02  
3.47

33  
0.  
16

33.18  
2.23  
35.41  
5.22  
40.63  
4.44  
36.19  
5.29  
41.48

10

STA	+	H.I.	-	Elev	F.L.Gr	
9+70.35	5.22	340.63		35.41	33.18	C. 2.23

11+50  
146'  
10+04 Inters  
34.5'

9+70.35

10+33			1.73	38.90	32.86	
-------	--	--	------	-------	-------	--

12+04			7.98	32.65	31.99	Top Bell. 3/4" Low
-------	--	--	------	-------	-------	--------------------

T.P.	5.29	41.48	4.44	36.19		
------	------	-------	------	-------	--	--

12+00			0.44	41.04	32.01	C. 9.05
-------	--	--	------	-------	-------	---------

			8.84	32.64		
--	--	--	------	-------	--	--

11+50	0.50	40.64		40.14	32.27	C. 7.87
-------	------	-------	--	-------	-------	---------

T.P.			4.42	36.22		
------	--	--	------	-------	--	--

11+56			7.67	32.97	32.24	Top pipe 32.97 7.74 32.23 Check
-------	--	--	------	-------	-------	---------------------------------------

12+00	.08	341.14		341.06	32.01	C. 9.05
-------	-----	--------	--	--------	-------	---------

12+23			8.41	332.73	31.89	Set 31.87 + 86 = 32.72 Str. Grade Stake at side of wall.
-------	--	--	------	--------	-------	--

12+04			8.47	332.67	31.93	.06 Low
-------	--	--	------	--------	-------	---------

9+70.35	6.15	41.56		35.41	33.18	C. 2.23
---------	------	-------	--	-------	-------	---------

			5.07	36.49	33.02	
--	--	--	------	-------	-------	--

"A" Line

Partially Clear Sultry  
3-17-36

Sta + H.I. - K. McCarty FL  
Ref - Walker  
Arc - Challard

P.I. 19°34' Lt Semi Tan 8, Ext = 08

P.I. 33°20" C = 7.3 R = 167 L = 97.1

C = 24.25

d = 4°10'

B.M. 4.64 358.07 353.93 E of P.H.

4.03 354.04 2862

18+68 3.88 354.19 2851

3-18-36

12+00 0.56 41.62 41.06 32.01 C. 9.05

12+04 8.86 32.76 31.99 Top Bell

12+22 9.00 32.62 31.90 Top Pipe

12+05 8.97 32.65 31.98 Top Pipe

13+50 12.61 ~~54.75~~ 42.14 31.21 M C10.93 0.08 Low

13+00 ~~1.27~~ ~~50.48~~ 31.49 M C19.07 C. 18.39

12+50 6.11 ~~48.64~~ 31.75 M C17.16 C. 16.89 0.27 Low Settled

13+50 12.80 54.94 42.14

13+00 4.36 50.58 Hub

13+50 6.11 48.83 31.75

12+79 9.98 44.96 31.60 C. 13.36

T.P. 0.21 42.66 12.49 42.45

1.61 4

"A" Line Sewer N Adams Ave

Sta	+	H. I	-	Elev.	F.L	
13+50	6.55					07
MH 38			7.89			
B.M.	7.55	351.11		343.56		343.56 7.55 351.11 9.74 341.37
6+70			9.74	341.37	347.4	C. 6.63 Blue keel mark in 2nd Set E. End Shaft
T.P.	0.95	36.51		35.56		Na'
7+25			2.06		34.45	F.L.
		W Portal				
0+00						
						Point 26.7 to 1st set.
						3-19-36.
12+00	1.35	42.41		41.06	32.01	C. 9.05
			9.80	32.61		End of pipe Top pipe
12+35			9.73	32.68	31.83	(32.69 Top Bell)
12+37			9.74	32.67	31.82	
12+39			9.74	32.67	31.81	Str. Gr. Top Bell ✓
T.P. on rock			6.22	36.19		
11+42			9.16	33.25	32.31	32.39 .08 High
11+50	0.93	41.07		40.14	32.27	C. 7.87
11+54			7.99	33.08	32.25	31.96
			7.81	33.26	32.31	33.17

32.01  
9.05  
41.06  
1.35  
42.41

STA	L	H.I.	-	Elev	F.L.G.	
12+00	0.05	41.11		41.06	32.01	C. 9.05
T.P. Rock			4.91	36.20		45.73
11+54			8.03	33.08		37.44
11+42			7.85	33.26		7.79
4-21-36						
5+35		355.55		343.94		Nail in Bottom Stamp B.M. = 343.94 New Elev Old Elev 343.83
B.M.	11.61	355.44		343.83		
4+50			7.61	47.94	35.95	6' offset. 355.55 C 11.99
4+50			7.86	47.89	35.95	3' " C 11.94
4+25			7.83	47.72	36.06	3' " C 11.66
4+00			11.01	44.54	36.18	3' " C 8.36
4+00			9.36	46.19	36.18	6' " C 10.01
M.H. #43	3+83.42		11.62	43.93	36.26	6' " C 7.67
3+50			10.01	45.54	36.41	3' " C. 9.13
3+50			8.48	47.07	36.41	6' " C 10.66
3+37 T.P.	2.44	352.63 352.52	5.36	350.19 350.08		On Stone Wall 13' L.
3+25					36.52	3' offs.
3+00			8.11	44.52	36.64	3' offset C 7.88
3+00			6.23	46.40	36.64	6' " C 9.76
2+75			6.61	46.02	36.75	3' " C 9.27
2+43 M.H. #44			5.28	47.35	36.90	6' " C. 10.45
2+20			8.42	44.21	37.01	3' " (Close Shot) C 7.20
2+00			6.63	46.00	37.10	4' " C. 8.90
2+00			6.01	46.62	37.10	6' " C 9.52
T.P.	3.97	348.30 348.19	8.30	344.33 344.22		
1+75			5.94	342.36	37.21	Piece Conc.
1+49			2.78	345.52	37.33	3' offset
1+49			2.28	346.02	37.33	3' " Start + 2.73
1+25			3.07	345.23		3' " C 8.01

Grade 00.450 of

$345.57 = 6' \text{ offset}$   
 $37.56 = \text{F.L.G}$   
 $C 8.01$   
 M.H. 45



RELOCATION  
"A" Line MH #39.

Sta. Angle Cont P15

11+38.04=B.C.

11+07.52=E.C.

12°11'30"lt.

10+95.02

9°45'lt

10+85.02

7°48'lt

10+75.02

5°51'lt

10+65.02

3°54'lt

10+55.02

1°57'lt

10+45.02=B.C.

49°36'rt

MH #39

10+06.95

N. Pier.

9+89.45

S. Pier.

9+73.45

MH #40

9+42.35

MH 41

Clear

3-19-36

McCarty X

Walker D.

Challand Ave.

Cont P15

Curve Data ✓

T = 31.73 ✓

e = 3.39 ✓

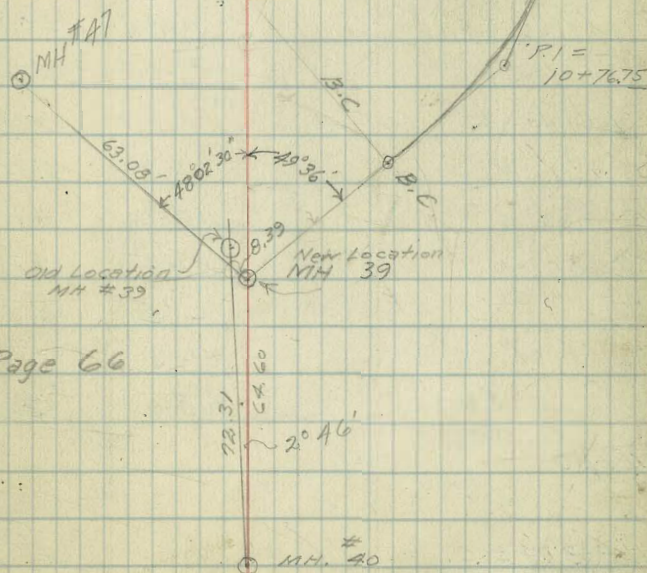
Δ = 24.23

R = 146.86

L = 62.50

End of pipe.

See Page 66



## "A" Line

Sta	#	H.I.	-	Elev.	F.L.	
11+50	1.07	341.21		340.14	32.27	C. 7.87
T.P. on rock			5.01	336.20		
11+39			5.48	35.73	32.33	C. 3.40
11+25			2.45	38.76	32.40	C. 6.36
11+00			3.10	38.11	32.53	C. 5.58
T.P. 10+76.7 P.I. 4.90		341.73	4.38	36.83	32.67	C. 4.16
10+50			4.52	36.69	32.79	C. 3.90
10+25					32.92	
10+06.95	M14 #39		3.75	37.98	33.01	6' W on line fro
9+93.45	N. Pier		7.91	33.82	33.08	offset 10' to W C. 0.74
9+93.45	N. Pier		5.60	36.13	33.08	" 20' to W C. 3.05
9+81.45	S. Pier		11.61	30.12	33.14	" 6' to W F. 3.02
9+69.45			6.31	335.42	33.20	" 7.2' to W = 9+70.35 C. 2.23
9+69.45	⊕ ground		8.8	32.9	33.20	on ground F = 0.3
S. Pier	⊕ ground		12.8	28.9	33.14	" " F = 4.2
N. Pier	⊕ ground		10.2	31.5	33.08	" " F = 1.6
9+85			14.5	27.2		Bottom of draw
			9.5			" " " 22' to W at it is on nat. gr.
			14.6			" " " 10' E " " " Filled
			18.0	23.7		" " " 23' E " " " not on ground
11+50	Angle.					

11+53.04 E.C.

7°48'30" Rt.

11+38.04 B.C.

Cont from P14

## Curve Data.

Δ = 15°37'

R = 55'

L = 15'

T = 7.53'

"A" Line

Partly Cloudy  
3-23-36

16

Sta.	+	H.I.	-	Elev	Flood Line
T.P.	1.02	36.58		35.56	
			2.08	34.50	34.5

Sill

3-24-36

Cloudy Springling

7+00	2.46	50.79		348.33	334.58
6+68					
6+50			5.09	45.70	34.84
			7.19	43.60	
			10.36	40.43	
	7.19	50.77		43.58	

Hub - C 13.75 6' Offset Left.

Hub C. 10.93

B.M.

B.M. <sup>Re</sup> Marked 43.58.

Hub 4' E of W. Portal Mark 340.45.

B.M. Remarked 43.58.

6+68			9.43	41.34	34.49
			9.39	41.36	34.48

C. 6.85

C. 6.88

B.M.	8.01	51.59		43.58	
6+68			10.24	41.35	34.49
7+00			3.28	48.29	

C 13.75

7+00	1.93	50.46		48.53	34.78
			10.04	40.42	

C 13.75

B.M	1.40	44.98		43.58	
6+29			9.31	35.67	34.95

Check on end of pipe



"A" Line

3-25-38

STA	+	H.I.	-	Elev	F.L.	
13+00	1.61	52.19		350.56	31.49	C 19.07
13+50			10.07	342.10	31.21	C 10.93 04
12+97					31.50	
12+73			11.52	40.67	31.63	Gr Rod = 20.56 C. 9.04 to F.L.
12+68			7.21	44.98	31.65	Gr Rod = 20.54 C 13.33 to F.L.
12+58	10.46	55.44		44.98		
			11.20	44.24	31.70	C 12.54 to F.L.
				3-25-36		

~H

\*  
 MH #39. 10+06.95  
           17.5  
 N. Pier 10+89.45  
           16  
 S. Pier 10+73.45  
 MH 9+42.35

12+55	1.51	45.75		44.24	31.72	C 12.54
12+65				44.24	31.67	
12+57			13.34	32.41	31.71	
12+50			13.36	32.39	31.75	0.11 Low

"A" Line

STA. M.H. #40	+	H.I	-	Elev.	F. L.	Cut or Fill
9+42.35					333.33	
9+69.45	6.31	341.72		Hub. Offs. 335.41		C. 2.23 = 9+70.35 old Line
9+73.45					33.17	End of 8" C.I. Pipe
9+89.45					33.09	
10+06.95			3.75	37.97	333.20	
10+25			5.10	36.62	32.91	C. 3.71 for Grading only 6' offset.
10+45.02	B.C.		5.57	36.15	32.81	C. 3.34 " " 5' "
10+55.02			4.94	36.78	32.76	C. 4.02 " " 5' "
10+65.02			4.75	36.97	32.71	C. 4.26 " 4' offset
10+75.02			4.67	37.05	32.66	C. 4.39 " 4' "
10+85.02			3.66	38.06	32.61	C. 5.45 " 5' "
10+95.02			4.58	37.14	32.55	C. 4.59 " 4' "
11+00					32.53	on timber
11+07.52	E.C.		3.52	38.20	32.46	C. 5.74 4' offset
10+50			5.05	36.67	32.79	C. 3.88
S. End						Offset 6' E + W
Middle Rec						9' offset 18' offset 90°
9+69.45	5.62	341.03		Hub. Offs. 35.41		
9+73.45			7.96	33.07	33.17	W. off F 0.10
9+73.45			10.27	30.76	33.17	E - F 2.41
9+89.45			9.16	31.87	33.09	9' off West F 1.22
9+89.45			7.38	33.65	33.09	18" " West C 0.56

32.18  
2.23  
35.41

K McCarty  
I Walker  
Challand.

Partly Cloudy  
3-25-36

"A" Line	T.	H.I.	-	Elev	FL	
12+55	1.01	345.25		44.24		
12+58			12.83	32.42	31.71	End of pipe Top pipe
12+50			12.83	32.42	31.75	31.69 = F.L. "

3-26-36 Clear

	8.62	362.05		353.43		B.M.
18+95			8.62	353.43		
18+75			8.62	353.43		
18+50			8.01	54.04		Check 0.0

3-26-36 Clear

13+00	1.80	352.36		350.56	331.49	MARE C 1927
13+50		352.39	10.25	42.11	31.21	C = 10.90 from Auto 13+00
12+55			8.14	44.25	31.73	Nail in X timber check = C 13.52 + C 13.49
12+77		20.12	+12.86 +7.26	32.27	31.62	on top pipe 32.27-73 = 31.54
12+58						End Pipe

Tunnels MH 91 to MH 42

	7.58	351.14		343.56		
			9.82	41.32	34.75	C 6.57 To Flow Line.

0.15 Fall in 19'

"A" Line Sta.	+	H.I. ✓	-	Elev.	F.L. Grade	
	1.10	344.68		343.58		
T.P.	1.74	38.51	7.91	336.77		
6+31			1.94	34.69	34.94	End. of pipe Top
6+43			3.48	35.03	34.88	2nd set timbers on S side
6+51					34.84	
11+50	0.92	41.06		40.14	32.27	0.7.87
T.P.			4.88	36.18	32.52	on rocks
11+01			7.69	33.37	32.52	String Grade on rent bar
11+21			7.78	33.28	32.41	End Pipe
	1.33	38.10		36.77		
6+51			3.19	34.91	34.84	.97 F 0.78 to Str. Grade. 4th Set Nailin Post S. Side.
6+55			3.29	34.81	34.82	F 0.86 to String Grade.



"A" Line

STA	+	H.I.	-	Elev.	Grade	
7+00	3.47	351.80		48.33	34.58	C 13.75
	8.19	51.77	8.19	43.58		
			11.36	40.41		
	7.07	50.65		43.58		B.M. E. Portal
			10.24	40.41		
			2.34	48.31		
7+00	2.34	50.67		48.33	34.58	C 13.75
6+68			7.39	43.28	34.75	C 8.53 to F.L. C 7.68 (to String Grade Top Bell) on cross timber.
	1.27	38.04		36.77		
6+43			3.01	35.03	34.88	34.73 String Grade set red mark on iron stake.
6+31	Top pipe		2.34	35.70	34.94	Top of pipe checked to 0.2'
6+55			3.23	34.81	34.82	35.65 String Grade set red mark on iron stake

43.58  
8.19  
51.77  
11.36  
40.41

"A" Line

STA	+	17.1.	-	Elev.	Grade
7+00	2.94	51.27		48.33	34.58

C 13.75

7+15

Lateral. 10' - South <sup>to</sup> N. Edge of Shaft  
 ↳ point

7+19.4

7+05

99°

7+15

7+15 10' Lt. 99° Lt 0.18 51.1

7' Lt. 0.25 51.0

FOR 6' Lt. 2.85 48.5

Ft of Rock Wall

Lateral to 2 Lt 3.00 48.3

Lot 28 1 Lt 4.90 46.4

Bonnie Brae

4 4.90 46.4

T.P. Spilke 1.25 36.74 35.49

35.49 4' W Portal on N. side

7+15 2.55 34.2

Floor Tunnel

Check on Cit. Pipe  
P.H. to MH 36

4.53 57.96 353.13

B.M. E of P.H.

19+05 5.96 52.00 28.34

23.66 23.12 Top

Sta	+	H.I.	-	Elev.	Grade	
	9.06	62.49		353.43	<del>28.34</del>	B.M.
19+05			10.51	51.98	28.34	
18+93			9.06	53.43	28.40	
			9.06	53.43		
11+50	1.29	341.43 ✓		340.14	32.27	C. 7.87
10+81			7.95	32.63	33.48 ✓	
11+02			8.06	32.54	8.09 = 0.03 L.W.	
10+50				32.79		
				Grade 0.515		
9+70.35	7.04	4245 ✓		335.41	33.18	C. 2.23
9+69.45			8.42	33.18	34.03	Red Mark on iron stake
9+33			3.03	3942	33.38	F.L. Gr. Rod = 9.07 C 6.04
8+92			3.50	38.95	33.59	C 5.36
7+00	3.38	51.71		48.33	34.58	C 13.75
6+87			11.84	39.87	34.65	C. 5.22 to F.L.
6+93			11.84		34.62	C. 5.25

"F" Line

Clear.  
4-1-36  
McCarty  
Walker

Sta	H.I	"F" Line	Elev	F.L.
0+00 = MH #40			333.33	C 11.30
0+22 Hub 6' offset	2.76		47.89	C 12.73
0+22 Ground	4.07		46.6	C 11.4
0+50 Brk 8.75	50.65		41.90	C 4.40
0+50 Ground	10.15		40.5	C 3.0
1+00			45.04	C 7.90
1+14 Hub	5.68		59.38	47.15
1+50	4.95	65.06	60.11	52.58
2+00			60.12	C 4.78
2+15.82 D.E.			362.50	C 3.81

8.34%  
15.07%

"F" Line

4-7-36

0+50	8.45	50.35	41.90	37.50	C 4.40
0+40		12.93		36.67	37.42 Too high
0+68		9.29		40.21	41.06
0+50		12.00		37.50	38.35
0+97		4.92		44.58	45.43
2+00	3.15	368.05	364.90	360.12	C 9.78
1+75		6.43	61.62	56.35	3' offs C 5.37

"F" Line

A' Line		Clear		4-2-36		Grade	
Sta	+	H.I.		F.L.			
MH #40	9+42.35	0.05	44.63	33.33			C 11.30 Hub
9+70. (old)			9.29	35.39	33.18		Check 0.92
9+70.			10.67	34.01			Iron stake Red Mark String Grade
10+01.					33.03		Sta. G. 33.88
9+96			11.69		33.05		Bottom pipe
MH #40			33.2	33.33			Ground
~K~							
MH 40	0.73	45.36	44.63	33.33			C 11.30
9+00			0.63	44.73	33.54		11.19 (Mark C 11.18)
9+13			11.04	34.32	33.47		String Grade.
9+31			11.13	34.23	33.38		
9+55.			11.23	34.13	33.26		0.87 Iron Pipes
8+92			10.93	✓ 34.43	33.58		
8+80			10.87	✓ 34.49	33.64		
9+70.35	6.08	41.49	35.41	33.18			C. 2.23
10+45			5.9	35.6	32.81		
10+61			7.91		32.73		33.58
10+84			8.02		33.62		33.47 8.54
10+06.95		F.L.	8.49		33.00		
N.E. Pipe			7.62	33.87	33.00		
N. Pier			7.54	✓ 33.95	33.08		
S Pier			7.46	✓ 34.03	33.16		
S. End Pipe			7.38	34.11	33.24		

Allowed 0.87 from F.L.  
to top Bell  
on 8" iron pipe

"A" Line

4-2-36

0.85 to top of Bell from F.L. 27  
0.74 to top Bell from F.L.

7+00	2.09	50.42	48.33	34.58	13.75
6+87		11.52	38.90	34.65	4.25

4-3-36

9+00	0.27	45.09	44.72	33.54	C 11.18
8+50		4.29	40.80 40.67	33.80	C 6.87
8+03		10.54	34.55	33.62	Bell 34.47
8+80		10.53	34.56	33.64	34.49
8+00		3.48	41.61	34.06	C 7.40

8+00	3.48	44.94	41.46		
8+50		4.29	40.65		
9+13		10.78	34.16	33.47	Top pipe 34.21 0.05 Low Check
8+83		10.67	34.27	33.62	34.46 0.29 High
8+83		10.54	34.40	33.62	Bell grade 34.47 0.07 " Check

9+00	0.27	45.09	44.72	F.L. ✓	
8+61		10.44	34.65	33.74	Set Bell 33.79 34.65 Set, 06 High 34.59
9+24		10.84		33.42	34.27 ✓ 10.84 Set 0.02 Low

"A" Line

4-3-36

Sta	+	H.I	-	Elev.	F.L. Grade		
7+00	2.60	50.93		48.33	34.58	C13.75	
6+75			11.18	39.75	34.71	Nail in bottom of ladder.	39.75 35.56
6+95			11.06	39.87	34.61	X timber & Blue keel Notches on each side	C4.19 to Str. Grade 39.87 35.46 C441
7+00	2.57	50.90		48.33			
6+95			11.03	39.87			
6+75			11.15	39.75			
6+68			9.62	41.28	34.75		
6+68			7.60	43.30			
	9.67	45.08		35.41	33.18	C.223	
M.H # 40			10.90		33.33		45.08 34.18 10.90
9+00			0.34	44.74	33.54	C.11.19	33.33 85 34.18
			Clear.				33.54 11.19 44.75
			4-6-36				
7+00	1.85	350.18		348.33	34.58	C13.75	
B.M.			9.74	340.44		Sto 7+40	2' N. of &
4-24-36			Check on pipe	Laid at MH #1			
B.M.	1.13	341.58		340.45			
7+55			6.63	334.95		Top pipe	} 0.09 Fall in 12ft.
7+67			6.72	334.86		Top pipe	

"A" Line

Sta	+	H.I	-	Elev	Grade	
	0.38	45.01		44.63		C 11.30
			10.825		33.33	34.18 Check .005
9+00	1.00	45.72		44.72	33.54	C 11.18
MH #40			1.09	44.63		
8+50			5.01	40.61	33.80	C 6.81 (Marked C 6.87)
8+00			4.22	41.50	34.06	C 7.44 " C 7.40
T.P.	7.28	43.47	9.53	36.19		
			2.94	40.53		40.44
8+62			8.96	34.51	33.74	34.59 End of pipe on bell <u>0.08</u> Low
8+30			5.51	37.96	33.91	3' offset Hula.
MH #41						
7+61					34.31	



3-6-36

30

Sta	+	H.I	-	Elev.	Grade
13. M. on Stump.					
10' L	5+39	7.04	353.87	346.83	
"A" Line					
5+35			11.49	42.38	35.42 C 6.96
M.H. 42					
5+14			11.77	42.10	35.51 Hub on S. Side M.H. C 6.59
5+50			11.86	42.01	35.36 C. 6.65

"C" Line	Sewer.		3-6-36			
Sta 1+00						
Sewer in Copy	6.93	367.20	↑	360.27	353.74	C 6.53 Sewer 6"
0+75			8.16	59.04	52.30	C. 6.74 3' offset
1+00			6.31	60.89	53.74	C 7.15 3' "
1+25			8.21	58.99	55.18	C 3.81 3' "
1+50			6.38	60.82	56.67	C 4.21 3' "
1+74 M.H.					58.00	

"A" Line						
7+00	2.74	51.07		48.33	34.58	
6+95			11.20	39.87	34.62	Str. 6. 35.49 C 4.40 Middle of X timber
6+89			11.21	39.86	34.52	
	6.54	41.95		35.41	33.18	C. 2.23 Gr. Rod.
10+63			8.36		32.71	End Pipe Bell 32.56 8.39
10+44			8.27		32.81	33.66 8.29 Set 0.02 High.
10+34			8.23		32.86	33.71 8.24 Set 0.01 High.

4-7-36

"A" Line  
Sta

Tunnel

Sta	+	H.I	-	Elev.	F.L
B.M.	0.55	340.99		340.44	
T.P. Sta 7+48			5.45	335.54	
7+61 M.H.			4.90		34.30
7+45					
7+37					
7+29					
7+21					
7+13					
7+05					
6+95					34.62
8+30			3.11	37.88	
T.P.			4.90	36.09	
7+46.			5.76	35.23	34.38
5+14 M.H. 42					35.51
B.M.	0.08	46.91		46.83	
5+29			10.60	35.44	36.29
5+45			10.66	35.35	36.20
5+50			4.90	42.01	
	6.16	52.99		46.83	
M.H. 5+14 4+50			5.15	47.84	35.51
5+00			11.41	41.58	35.58
4+81					35.67
B.M.			9.16	43.83	

Tunnel

E W  
4' from portal on Surface.  
Spike in wall on N side 3' W of W Portal.  
Raised Grade 003 old grade = 34.27  
Portal of tunnel

35.23 Nail in <sup>South Side</sup> plank to String Grade.

Stamp G.R. set .02  
10.62 10.60  
10.71  
C 6.65

B.M Top Stamp 5+35  
H 6 3' offset  
H 6 6' offset  
Spike N. side Stamp 5+35

"A" Line

Clear.

4-8-36

32

Sta	+	H.I.	-	Elev.	F.L.	
B.M. on 5+35 Stamp	4.86			46.83		
" Nail in Station	7.85	51.68		43.83		
4+81			7.61	44.07	35.67	C 8.40
4+50			3.86	47.82	35.82	C 12.00 6' offset to Right <sup>old</sup> Mark C 12.12
4+50			4.11	47.57	35.82	C 11.75 3' " "

4-8-36

9+00	0.46	45.19		44.73	33.54	C 11.19 Hub.
8+62			10.70	<sup>Str. Grade</sup> 34.49	33.74	<sup>Str. Gr.</sup> 34.59 Check Top Ben 0.10 Low Checks
8+30			7.23	<sup>Hub</sup> 37.96	33.85	C 4.11
8+46			10.60	<sup>Str. Grade</sup> 34.59	33.82	34.67 0.98 Low Checks
8+00			5.92	39.27	34.05	C 5.22

4-8-36

B.M.	3.53	43.97		340.44		4' E of W Portal Tunnel
8+00			4.79	39.18	34.05	C 5.13
8+30			6.10	37.87		C 4.02
8+46			9.45	34.52	33.74	
T.P.			8.43	35.54		4' W of <sup>W</sup> Portal on N side Splice in wall
4+50	4.40	52.22		47.82		6' offset
4+25			4.63	47.59	35.94	C 11.65 5' offset.
4+00			6.14	46.08	36.06	C 10.02 6' " ( <sup>old</sup> Marked C 10.10)
4+00			7.79	44.43	36.06	3' "
MH 43			8.41	43.81		6' "

"A" Line

Clear

4-9-36

McCarty  
Walker

33

Sta.	+	H.I.	-	Elev.	F.L.	
B.M. on stump	0.37	44.20		343.83		Nail in bottom of stump.
5+27			Gr Rod	Elev Ball	35.45	36.30
End of pipe on ball			7.86	36.34	35.45	36.30
5+16			Gr Rod	7.81	36.39	35.50
						36.35
M.H. #43						
3+83.42	11.73	55.54		43.81		6' offset. Left 43.88 by Moore
3+50.			8.61	46.93		6' " L 47.08
3+50			10.14	45.40		3' " Left
3+50			5.54	350.00		Top Stone Wall 12' Left Blue Keel
3+25			11.27	44.27		3' offset Left
T.P.						
3+00	8.27	52.67	11.14	44.40		3' " Left
2+75			6.80	45.87		3' " "
3+00			6.42	46.25		6' " "
T.P.						
2+99	5.95	52.50	6.12	46.55		Top SW Cor. Wall 1.60 Left
2+49.78 M.H. 45			5.31	47.19		6' offset L. Hub
2+00			6.05	46.45		6' " L Moore 46.60 Hub
2+00			6.67	45.83		4' " L "
1+75			10.29	42.21		3' " L "
T.P.	7.25	351.42	8.33	44.17		In Wall on concrete (piece) Sta 1+55
1+49			5.56	45.86		6' offset L
1+49			6.06	45.36		3' " L
1+25			5.83	45.59		6' " L
1+25			6.35	45.07		3' " L
M.H. 45			6.01	45.41		6' " R. Moore 45.54
0+50			1.85	49.57		6' " L
0+50			1.69	49.73		3' " L

43.83  
37  
44.20

Checked .05 High

Set .005 High

43.88 by Moore

Blue Keel

Top SW Cor. Wall 1.60 Left

Hub

Moore  
46.60 Hub

Moore  
45.54

"A" Line

4-9-36

STA	+	H.I.	-	Elev	F.L.
	0.72	45.45		44.73	33.54
8+48			10.87	34.58	33.81
8+35			10.77	34.67	
8+30			7.50	37.95	
8+00			6.19	39.26	

C 11.19  
 34.66 Check on ball 0.08 Low back  
 0.15 Low Ahead

4.19  
 33.54  
 44.73  
 45.45

0.699  
 8+48  
 7+61

4-10-36

B.M. piece of Conc Sta 1+55	4.20	48.37		344.17	
2+20			4.30	44.07	
2+43.78			1.19	47.1.8	

8+30	3.96	41.91		37.95	
			7.34	34.57	
		41.97	7.25	34.66	
7+66			7.74	34.23	

Tunnel

"A" Line	Tunnel	Grades	
7+45	1.40		34.29
7+25		1.34	
7+03		51.25 Bell 1.36	
7+46	3.28		
7+167		3.39	
7+90		3.49	

Top Pipe

"A" Line	1.41	45.24	43.83		
#5+17			8.92	36.32	35.53
Stak 5+15			8.88	36.36	
MH #5+14			8.86	36.38	
4+94			8.76	36.48	
MH #41			34.22	34.22	
9+00	0.64	45.36	44.72	33.54	C 11.18
8+35			10.74	34.62	
8+22			10.67	34.69	
7+67			10.21		
8+00 T.P.			6.10	39.26	3' offset.
	8.42	43.83	35.41	33.18	C 2.23
10+34			10.10	33.73	32.88
10+14			10.00	33.83	32.98
8+00	6.15	45.41	39.26		
8+35			10.80	34.61	
8+23			10.73	34.68	
					} Check on top Bell
B.M.	1.68	45.51	43.83		
5+17			9.20	36.31	35.46
5+14			9.11	36.40	
5+00			9.03		

4-13-36

"F" Line

0+50	8.38	50.28	41.90	37.56	6.4.40
0+70			12.94	37.34	36.67
0+25			8.87	41.46	36.09 35.42
	9.77	45.18		35.41	6.5.32 X timber

MH 40			11.18	33.33	34.00
-------	--	--	-------	-------	-------

"A" Line

1+55	9.66	53.83		44.17	
on Eb. S. Cor Dr. Way on West Side 39th St			5.53	48.30	
Fire Hyd.			6.09	47.74	Foot of 39th on E. Side
on Ch. S. Cor Dr.	10.02	58.32		48.30	
B.M.			1.59	56.73	Elev = 56.95 <sup>check</sup> 0.22

Piece of Concrete in Wall.

8+00	6.05	45.31		39.26	
8+23			10.62	34.69	Check on Bell
8+12			10.54	34.77	

	1.55	45.38		43.83	
--	------	-------	--	-------	--

5+14			8.98	36.40	
End Pipe 5+17			9.06	36.32	
4+92			8.86	36.52	

8+30	2.86			37.95	
	1.56	40.82		19.26	

8+11			6.05	34.77	Check
87 89			5.90	34.92	
7+66			5.79	35.03	
T.P.			2.32	38.50	

Brass Plug SE. Cor 39th & Circle Dr.

"A" Line

4-14-36

Sta	+	H.I	-	Elev.	Grade
T.P	6.89	45.39		38.50	
B.M.	4.88	45.33	4.88	40.51 35.05	40.45
7+66			10.34	34.99 34.98	
7+88			10.49	34.84	
T.P.			6.89		
B.M	0.09	40.54		40.45	
7+48			5.33	35.21	(35.14 Reset 07 lower.
7+66			5.56	34.98	
9+70	9.15	44.56		35.41	33.19 C. 2.23
9+42.35			10.56	34.00	33.33 For 6" pipe "F"
			10.50	34.06	Top pipe
0+50	5.96	47.86		41.90	37.50 C. 4.40
0+24			11.86	36.00	35.33
	1.59	45.47		43.88	
<sup>514</sup> 4+94			8.91	36.56	
5+13			9.14	36.33	Top pipe 36.44
5+17			9.15	36.32	
5+14			9.04	36.43	on Stake at M.I
4+77			8.83	36.64	
4+77			9.48	35.99	Stake by iron Stake Mess up 065
B.M	0.28	40.73		40.45	
7+48			5.56		
7+67			5.75		
8+11			6.03		Ball



Cloudy in morning

A.M. 4-15-36.

T. McCarthy  
J. Walker

Check Levels.		A.M.		Correct Elev.	
"A" Line Sta.	+ H.I.				
B.M.	3.01	359.96		356.95	
T.P.	5.95	356.15	9.76	350.20	
B.M. 5+35			9.21	346.94	
B.M. Nail Bottom Stump 5+35			12.21	343.94	
T.P.	2.75	352.95	5.95	350.20	
MH #45			7.36	345.59	
T.P.	8.03	359.96	1.02	351.93	
B.M.			3.03	356.93	

Brass Plug SE Cor Circle Drive & 39th St.

on conc. wall

(46.83 Moore.) Top Stump

Nail in bottom of stump.

on conc. wall

6' offset 335.54 (By Moore.)

on Ch.

B.M. Brass Plug SE Cor Circle Dr. & 39th St = 356.95

"C" Line Relocated MH #50 Drop.

Sta	+ H.I.				
Sta 2+21					
Old 2+09	6.18	87.32		81.14	75.00
2+21			5.73	81.59	75.28

6.14

C6.31 C16.31

"A" Line

MH #40	+ H.I.				
MH 9+42.35	0.27	44.90		344.63	33.33
Top 6" pipe			11.87	33.03	32.46
Top 8" " Gang F			11.87	33.03	32.29
"8" " " N onbell			11.79	33.11	32.26
9+70 Hub			9.52	35.32	
0+50 "F"	8.60	50.50		41.90	37.50
			12.37	38.13	37.56
	0.60	44.43		43.83	
4+78			7.85	36.58	35.73 <sup>2</sup>
5+			8.15	36.28	
5+26	9.12		8.12	36.31	35.46

C11.30

-0.57

-0.74

-0.85

35.41 Check.

0.4.40

-0.57 Top pipe

B.M. on Stump

35.73 (piperbell?)

Pop 35.52

Top Bell

By old levels.

Elev FL 5414 = 35.62

By new levels

35.73

Elev MH #45 0+98.40 = 37.58

4-1-36

	+	H.I.	-	Elev	F.L.	
M.H. #45	10.75	56.34		45.59		Hub 6' offset
		56.29		45.54 (by Mark)		
T.P.	7.93	59.87	4.40	51.94		on Ch.
		59.82		51.89		
B.M.			2.93	56.94	check to 0.02	SE cor Circle 56.95
				56.89		Check: 0.06 Low.

37.67  
78.7  
45.54  
107.5  
56.29  
44.40  
51.89  
79.3  
59.82  
2.93  
55.919

4-10-36

"A"	5.04	34.045		35.41	33.18	33.18 C, 2.23
10+05			6.81	33.64	32.93	Top Bell
M.H. 10+6.95					33.00	
10+13						
10+36			6.71	33.74	32.89	Top Bell
	4.99	40.40		35.41		
S. Pier			6.37	34.03	33.16	Top Bell Iron Pipe
			6.76	33.64	32.93	N. End. of pipe 0.07 Low Est. Grade = 33.00
N. Pier			6.47	33.93	33.06	Set 33.08 Settled 0.02
10+36			6.67	33.73	32.88	33.86 = Est. Grade Set 0.02 High.
10+13			6.59	33.81	32.96	Set mark on iron stake String Grade Top Bell
Copley Arc C Line						
+50 Sewer	5.68	65.79		60.07	56.62	C 3.45
+25			9.96	55.83	55.18	String grade Top Bell 6" pipe mark on iron stake
+00			11.40	54.39	53.72	" " " " " " " "
+15			12.84	52.95	52.28	" " " " " " " "
B.M. #35	0.205	44.035		43.83		Nail in bottom of Stamp
Line 5+26			7.725	36.310	35.57	
5+15			7.68	36.345	35.61	Top pipe
5+11			7.64	36.395	35.65	Top pipe

35.62 = Elev. M.H. 35.73 = Grade by new levels.  
35.53 = Est. Grade.  
.09 High

Estimate #2353, 3/6/36

Pump House

Excav.  $14 \times 4.5 \times 4.5 = 11 \text{ yds}$

MH 37 to 38

MH 38 Grade

Hole #6 21' to Cut 4.1

	5.6	41.3	40.8	31.31	09.48
Hole #5		7.2	34.1		02.6
A		6.1	35.2		3.7
3		5.0	36.3		5.2
T.P	0.4	39.5	2.4	38.9	7.4
Hole #2		3.1	36.2		4.7
Hole 1		10.2	37.1		00
" 1		11.7	27.6		06
		12.8	26.5		00
11+50	-0.1	41.2	41.39		9.12
		9.0	32.2		

$\sum = 315$

3/6/36

40

Geo. Ex 2 yds. bet MH 37 + 38

E 18 yds. " MH 38 + 39

B.F 22 yd " MH 37 + 38

5th Hole from MH 38 to 2nd  
 Count in 39 yds

$1.5 \times 5 \times 2.5$

$7' \times 4 \times$

$11 \times 4$

$9 \times 4 \times 5.0$

Add 20 yds  
 for Mch 6-'36

$6 \times 11 \times 2.5$

(Add Bench  $11 \times 2.2 \times 0.5$ )

$12 \times 3 \times 6.0$

$40 \times 2.5 \times 5.5$

$15 \times 2.5 \times 4$

Around Dump

$4.5 \times 1.8 \times 30 = 243$

$20 \times 1.5 \times 12 = 360$

$18 \times 1.5 \times 3 = 81$

$30 \times 2.0 \times 3 = 180$

$4 \times 2.0 \times 4 = 32$

$\frac{896}{896} = 33 \text{ yds}$

3/6/36

41

MH 41

$$8 \times 6 \times 3.5 = 108$$

$$6' \text{ dia} \times 6.8 \text{ High} = 192$$

$$7 \times 5 \times 3.5 = 122.5$$

$$\frac{422.5}{26} = 16 \text{ yds}$$

MH 41 to MH 42

$$8 \times 7 \times 3 = 41$$

$$5 \times 0.8 \times 8 = 32$$

$$\frac{73}{23} = 3 \text{ yds}$$

56 yds Exc } Total,  
21 yds B.F. } Estimate 3/10/36

# MH 42  
E. Tunnel 9' dug,  
 $8.5 \times 3 \times 5 = 5 \text{ yds.}$

# MH 41 to  
W. Tunnel 16' Edge MH.  
 $6 \times 7 \times 4 = 148 = 6 \text{ yds}$

} 11 yds.

MH 37 to 38

To date → B.F. complete to 10' from MH 38  
 $= 10 \text{ yds B.F. } 3/10$   
3/10/36

10 yds B.F. }  
12 yds Exc } B.F. =  $2 \times 48 \times 3 = 288 = 10 \text{ yds.}$

18 yds Exc,  $2 \times 8 \times 3.5 = 2 \text{ yds.}$   
4 yds B.F.

$131 \times 4 \times 3 = 1072$  } 53 yds  
360 }  
120 }  
 $\frac{120}{1552} = 58 \text{ yds}$   
10 yds 3/10/3

MH #36 to Pump House 11 yds. Exc  
7 yds B.F.

Estimate 3/10/36

42

Exc 11 Dick.

" 18 Steve

" 20 Geo.

" 7 Borron

56 yds total. "A" Line Ditch 3/10/36

B.F. 4 Steve.

" 7 Borron

" 10 George ✓

21 yds B.F. "A" Line Ditch 3/10/36

3/11/36

MH 41 to MH 42

30 63 ft of 8" Conc. Pipe,

75  $6.0 \times 0.5 \times 2.5 = 3$  yds.

2 1/2

Tunnel E Portal 11.5' progress

$2.5 \times 11.0 \times 3 = 82.5 = 3$  yds,

13' Edge of MH to Portal Tunnel.

W Tunnel 7' from portal.

$2 \times 9 \times 4 = 64 = 72 = 3$  yds.

MH 38 to 39

Sta 12+01 to Sta 11+59

B.F.  $13 \times 6.5 \times 3 =$

"  $2 \times 7.0 \times 3 =$

"  $23 \times 4.4 \times 27 =$

In. Fill

$30 \times 5 \times 1 = 150$  } Pulled down

$18 \times 18 \times 1 = 324$  } on path

$20 \times 30 \times 1.5 = 900$  }  $\downarrow$

$27 \overline{) 1371}$

135

21

MH 38 to 39 Cont

$13' \times 1 \times 3 = 39$  ✓

$10 \times 2 \times 3 = 60$  ✓

$10 \times 2 \times 0.5 = 10$  ✓

$9 \times 2 \times 4 = 72$  ✓

$5 \times 2 \times 4 = 40$  ✓

$7 \times 2.5 \times 4 = 70$  ✓

$21 \times 0.5 \times 3 = 32$

$27 \overline{) 323} \quad 12 \text{ yds.}$   
27  
53

STARTING MH 38

3/11/36

#1 Hole 21' finished

2 "  $6.5 \times 6.0 \times 4$  W

3 "  $11.0 \times 9.0 \times 4$

4 "  $9.0 \times 7.3 \times 4$

5 "  $10.0 \times 1.5 \times 3$  3' Elev to W.P. "

6 "  $8.0 \times 1.0 \times 3$  "Top W "

7 "  $23.0 \times 0.5 \times 3$  STA 12+25

8 "  $15.0 \times 1.8 \times 3$  Top West Wall Plate

Exc. complete 12+10 to 11+50

Depth from <sup>Elev</sup> Top Wall plate

"Top W "

Total for  
73 yds  
Fill

25  
50  
5  
100  
50  
50  
100

3-12-30

44

Pump House to MH 36

12 yds total in hole next to P.H.

14 x 5.5 x 4 = 12 yds. Beron

MH 38 to MH 39

Tunnel 5' 10 x 3 x 5 = 150 + = 6 yds.

Hole #2	Depth 8'	6.0 = 2.0	6.5 x 4	} 21.6
3	4.2'	4. = 0.2	11 x 4	
4	7.6	7.3 = 0.3	9 x 4	
5	3.5	1.5 = 2.0	10 x 3	} 252.9
6	2.2	1.0 = 1.2	8 x 3	
7	3.5	1.4 = 1.7	23 x 3	} 324.5
8	3.0	1.8 = 1.2	13 x 3	

12 yds  
- 6

18 yds for Geo.

35 yds remov fill

35  
- 18  
---  
17 yds.

W. Tunnel 11' from portal  
 11 x 4 x 3.5 = 6 yds.  
 11 x 3.8 x 3.5 = 5 yds. } 11 yds.  
 E Tunnel 16' from portal.

P.H. to M.H. #36

2 yds. for Geer

8 yds B.F.

$$5 \times 4 \times 3 = 60$$

$$11 \times 5 \times 1.5 = 82$$

} 6 yds Ex  
2  
8 yds Total

MH 38 to MH 39

2.5' finished

Hole #2  $1.5 \times 3 \times 6.5 =$

" 3  $0.6 \times 3.5 \times 11.0 =$

" 4 Same. No yds.  $7.5$

" 5  $1.3 \times 3.0 \times 10 =$

" 6  $1.3 \times 3.0 \times 8 =$

" 7  $0.2 \times 3.0 \times 23 =$

" 8  $1.2 \times 3.5 \times 15 =$

AV  
Depth

9.5'

4.7'

7.5

4.8

3.5

3.7

4.2

} 7 yds

$2 \times 12 \times 3 = 72 = 3 \text{ yds}$

Steve.

37 yds

MH 41 to MH 42.

{ 4 1/2 yds. Portal of W Tunnel 13' to face - 3' pro.

{ 4 1/2 yds. " " E " 19' " " 3' pro.

Shaft = 1 yds 3' prog.

B.F.  $16' \times 4.7 \times 2.5 = 7 \text{ yds}$

10 yds.

$-4$   
 $3 \text{ yds.}$

Totals for 3-13-36

65 yds Exc. "A" Ditch

11 yds B.F. "A" "

30' 8" conc. pipe

11' x 3 1/2"

" 8" x 3

" 9' 5" x 3 1/2"

" 6' x 3 1/2"

" 5' x 3

" 5' 6" x 3 1/2"

" 5' x 3 1/2"

" 6' 5" x 3 1/2"

" 10' 11" 6' 6" x 3 1/2"

HOLE SO. PUMP HOUSE LONG

13' 5' 12'

Mon. 3-16 -

Exc = 55

B.F. = 4

Tues -17th.

Exc 71 yds

B.F. 6 yds

Wed. Exc 46 yds

B.F. 37

18'

Thurs. Exc 38 Exc

33 B.F.

33' - 8" pipe

} 21' 8" pipe

12' - 6" C.I. pipe

21 pipe



3-17-36

Pump House

P.H. to MH #36

L = 12 D = 13' from timber W = 5' 3/17

L = 12 D = 10.5 " " W = 5 3/16

$12 \times 2.5 \times 5 = 150 = 5 \frac{1}{2}$  yds. F. Geer Est = 10 yds

$12 \times 3 \times 5.5 =$

$1 \times 6 \times 5.5 =$

$$\begin{array}{r} 35 \\ 15 \\ \hline 180 \\ 180 \\ \hline 198.0 \\ 3 \\ \hline 22) 23 \frac{1}{2} \\ \underline{22} \\ 1 \end{array}$$

Mch 18-36 Estimate

MH 41 to MH 42

W Portal 25' to face 3' progress

Shaft 9' Length Depth = 8.2 from top set.

W = 3.2 = 3 yds.

E Portal 20' to face No progress

→ previous meas 9' Length 6' depth 3.2 = W

W Tunnel 13' x 3.5 x 3 = 136 = 5 yds. 8 yds total

MH #38 to MH #39

- 18' x 3 x 2
- 3 x 0.5 x 2
- 6 x 3.0 x 2.5
- 11 x 1.0 x 2.5
- 12 x 4.2 x 2.5

13 yds Stone 4.2  
3.5  
11'

- 2 Hole # 11'
- #3 Hole { 10.5' 2/3'  
8.3 5'
- #4 10.8
- #5 6.5
- #6 6.5
- #7 { 6.5  
8.0  
8.3
- #8 Uncomplete.

12 yds Geo.

MH 36 to P.H.  
 $13 \times 5.5 \times 16 = 9$  yds 3/18  
 $5 \times 5 \times 4.2 = 4$  yds

Estimate 2-19-36

P.H. to MH #36

$$13 \times 5.5 \times \frac{18}{16} =$$

$$\text{Geo} \left\{ 13 \times 3.5 \times 2 = 5 \text{ yds. Exc } 5 \text{ yds. B.F.} \right.$$

$$\left. \begin{array}{l} 9 \times 5 \times 6 = 270 \\ 105 \\ \hline 165 \end{array} \right\} \text{Borran } [6 \text{ yds. B.F.}]$$

MH 38 & 39.

No Exc in #1, 2.

Hole No	Depth	Hole	W
3	12'	5' x 2 1/2'	
4	11.8	Same length	3 1/2'
5	7.7	" "	3'
6	6.9	" "	3'
7	8.1	" "	3'
8	No Excav		

} Geo

$$20' \times 3.5 \times 2.5$$

$$13 \times 1.5 \times 2.5$$

$$20 \times 3.0 \times 2.5$$

$$13 \times 1.5 \times 2.5$$

$$+ 5 \text{ yds Overburden} = 12 \text{ yds. Total.}$$

Progress 4' in W portal.

$$4 \times 12 \times 3.5 = 168 = 6 \text{ yds}$$

$$\text{Shatt } 9' = L \quad 10.7 = D \quad W = 3.2 = 72 \text{ cu. ft.}$$

$$= 3 \text{ yds}$$

$$9 \text{ yds. Exc}$$

$$3 \text{ " B.F.}$$

$$\rightarrow 3.5 \times 12 \times 3.0 = 126$$

$$1.0 \times 9 \times 3.5 = 31.5$$

$$0.7 \times 10 \times 3 = 21.0$$

$$0.4 \times 8 \times 3$$

$$0.5 \times 23 \times 3 = 54.1$$

$$232.6 = 9 \text{ yds. Geo}$$

$$12 \text{ yd Store.}$$

$$9 \text{ " Dick}$$

$$6 \text{ " Borran}$$

$$5 \text{ " Geo}$$

$$41 \text{ " Exc}$$

#2353.

Mon. Estimate 3-23-36

48

MH 41 to MH 42.

Depth of Shaft 11.4 x 9.

Tunnel 4' going E. from shaft.  $11.5 \times 3.5 \times 4$ Shaft  $0.7 \times 9 \times 3.2 =$ 

W Tunnel

 $33.9 - 29.5 = 4.4$  progress $12 \times 4.4 \times 3.5$ 

$$\begin{array}{r} 27 \overline{) 366} \text{ cu ft} \\ \underline{14} = \text{yds.} \end{array}$$

Hole #3	11.8	-	2.5' W	$\times 12.5 = L$	
Tunnel $1\frac{1}{2}'$	$13 \times 1\frac{1}{2}$	$\times 3.5 = 68$			
Hole #4	13.4	- 9	2.5	Same L	$1.7 \times 9 \times 2.5$
" 5	8.0	- 10	2.5	" "	$0.8 \times 10 \times 2.5$
" 6	8.8	- 8.0	2.5	" "	$1.9 \times 8 \times 3.0$
" 7	8.5	- 15.0	2.5	" 15'	$0.5 \times 15 \times 3.0$

27) 183	7 yds Exc
189	8 yds B.F.
	10 yds B.F.

Total = 42 yds  
Exc = 42 yds B.F.  
B.F. = 49 yds B.F.

beer Depth	19.5	$1.5 \times 13 \times 10 = 195$
	18	136
	$1.5 \times 13 \times 7 = 136\frac{1}{2}$	27) 331 $\frac{1}{2}$ yds
		221

Est. Tues 3-24-35

49

MH 41 to MH 42 (DICK)

W. Tunnel  $37.6 - 33.9 = 3.7$  ft. = 155<sup>00</sup>'

E Shaft w. Portal 4'-4' = 0 ft.

W " 3.3 x 5 x 9.5 }

Prev. - 3.3 x 3 x 9.5 } = 3.3 x 2 x 9.5 = 63

218

218 cu ft = 8 yds.

Total "A" Line Exc. = 28 yds.

B.F. = 30 yds

12' of 6" Conc.

Est. Wed. 3-25-36.

7.3  
4.2  
3.1

W. Portal  $42.0 - 37.6 = 4.4 = 185^{\text{cu}}$

E. Shaft. W Tunnel  $8' - 4' = 4'$  progress 154

W "  $3.3 \times 5 \times 2.6 = 43 \text{ cu ft}$   
 $= 382^{\text{cu}} = 14 \text{ yds.}$

Total Exc. = 28 yds.

B.F. = 55 "

51' of 8" Conc. Pipe

Estimate Thurs. 3-26-36

MH 36 to PIH

18+67 to Grade

Tunnel start 18+81 Length of Tunnel 5'

MH 38 to MH 39

	L	W	D	
MH 38 <sup>n</sup> (Back Filled except	11	3	4	= 132
to	"	10	3.5	14 = 490
11+30	"	11	3.5	12 = 462
"	"	16	3.5	9.7 = 544
				1628

Exc. 4.5 Top Timber upper side } 23' Long  
5.0 " " " " "  
6.0 " " " " "

4.2' " " " " " 18' "

MH 40 to MH 41 150 Clear G. Grub

W. Portal  $46 - 42 = 4'$  progress  $4 \times 11 \times 3.5$  } 10 yds  
 $3 \times 11 \times 3.5$  }

Shaft E. Tun 11 - 8 = 3' "

W. Shaft -  $4.2 \times 10 \times 3.2$  } = 194<sup>cu</sup> out  
 $+ 3.1 \times 6 \times 3.2$  } 194<sup>cu</sup> prog

Exc 40 yds total No prog

B.F. 42 yds 18' Conc. Pipe

Fri. Est. 3/27/36

51

Grand Total Pipe 6" C.I. = 80 ft.  
 includ 3/26/36 8" Conc. = 732 "  
 Rent. Steel. 6262 ft. lineal feet  
 3 Manholes completed.  
 "A" Line Excav. = 1477 yds  
 "A" Line B.F. = 602 yds.  
 P.H. Concrete 45 yds.

Total of Week Ending 3/27/36  
 up to 3/26/36

W. Portal 2' progress  $11 \times 3.5 \times 2 = 77 \text{ cu ft.}$   
 $3.2 \times 10 \times 7.5 = 46 \text{ cu ft.}$

E (F. Portal  $12 \times 1 \times 3.5 = 42$   
 Staff } W  $11 \times 2 \times 3.5 = 77$   
 $77$   
 $46$

$242 = 9 \text{ yds.}$

MH 40 to MH 41

$35 \times 0.5 \times 2.5$

$7 \times 2.0 \times 3.5$

$8 \times 1.5 \times 3.5$

$15 \times 3.4 \times 3.5$

$5 \times 3.7 \times 3.5$

$11 \times 2.0 \times 3.5$

$7 \times 3.0 \times 3.5$

$7 \times 3.0 \times 3.5$

$616 \text{ cu ft.} = 23 \text{ yds}$

MH 40 4.7' x 6' dia

$\frac{28.3}{4.7} = 5.99$   
 $\frac{27}{27} = 1.33$  (5 yds.)

$8 \times 3 \times 3 = 72$

$16 \times 3.3 \times 3 = 158$

$230 = 8 \text{ yds.}$

Piers = 1 yd

MH  $23 \times 1.3 \times 3 = 89 = 3 \text{ yds. Stone } 39 \text{ to } 38$

7 yds Baker 39 to 38

12 yds. Total

Fri Est 3/27/36

$$24' \times 5 \times 3.5$$

$$10 \times 11 \times 3.5$$

$$11 \times 4.0 \times 4.0$$

$$1628 - 1261^{\square} = 367^{\square}$$

$$= 314 \text{ yds}$$

30 yds B.F. total.

To be back filled

720  
385  
176

Estimate Mon. 3/30/36

W. shaft

$$(11.6 \times 10 \times 3.2) - (7.5 \times 10 \times 3.2) = 5 \text{ yds.}$$

Shaft to Schneider lateral

$$33 \times 5 \times 5 = 82 = 3 \text{ yds}$$

$$35 \times 0.5 \times 2.5 = 44^{\square}$$

$$13 \times 3.0 \times 3.5 = 369$$

$$7 \times 3.0 \times 3.5 =$$

$$13 \times 3.5 \times 3.5 =$$

$$13 \times 3.0 \times 4.0 =$$

$$12 \times 2.0 \times 4.0 = 392$$

$$7 \times 5.0 \times 4.0 =$$

$$805 = 30 \text{ yds.}$$

MH #40

$$6' \times 5.8 = 164^{\square} = 6 \text{ yds.}$$

$$\text{Exc. } 24 \times 5.0 \times 3.0 = 360 = 13 \text{ yds.}$$

$$\text{Conc. Pieces } \left. \begin{array}{l} 0.8 \times 1.8 \times 3.0 \\ 0.8 \times 2.2 \times 6.5 \end{array} \right\} = 15.8^{\square} = \frac{1}{2} \text{ yd. Concrete}$$

MH 39 to MH 38

$$7 \times 3 \times 2.5 = 52.5$$

$$30 \times 2 \times 3.0 = 180$$

$$232 = 8 \text{ yds.} + 5 \text{ yds. } 0.13 = 13 \text{ yds.}$$

PH to MH 36 54' of 6" O.I. Pipe.

Estimate Tues 3/31/36

P.H. to MH 36 To hole B.F.  $(16.5 \times 16 \times 6 =$   
 $8.2 \times 24 \times 6 =$   
 Steve. 3 yds.  $25 \times 13.5 \times 6 =$

2 yds. Exc. =

18' - 8" conc. pipe

MH 39 to MH 40

$$13 \text{ yds. } (24 \times 5.6 \times 3) - (24 \times 5.0 \times 3) = 43^{\circ} = 2 \text{ yds}$$

MH 40 Same = 6 yds

MH 40 to MH 41

$9 \times 5 \times 4.0 = 180^{\circ}$

$23 \times 5 \times 4 = 460$

$13 \times 7 \times 3.5 =$

$7 \times 4.5 \times 3.5 =$

$13 \times 3.0 \times 3.5 = 692$

$35 \times 0.5 \times 3.5$

$11 \times 1.7 \times 3.5 \Rightarrow 1332^{\circ} = 49 \text{ yds.}$

1.2 yds

Geo.

at 1:30 PM

1.3 yds

Schneider Lat. Shaft

$$\begin{matrix} 131 & 82^{\circ} \\ (5 \times 3.5 \times 7.5) - (5.5 \times 5 \times 3.3) = 49^{\circ} = 2 \text{ yds} \end{matrix}$$

$$\left\{ \begin{matrix} \text{W. Shaft. } (12 \times 3.3 \times 10) - (11.6 \times 3.2 \times 10) = 25^{\circ} = 1 \text{ yd.} \\ \text{E. Portal } 12 \times 2 \times 3.3 = 79 = 3 \text{ yds} \end{matrix} \right. = 6 \text{ yds Total (Duke)}$$

No B.F.

Summary 3/31/36.

Exc. = 21 yds

B.F. =

Pipe 8" Conc = 54 ft.

36' Pipe 8" Concrete

# Estimate 4-1-36.

MH 41 to MH 42

B.F. 8' of tunnel  $11 \times 8 \times 3.5 = 308 = 11 \text{ yds} + 5 = 16 \text{ yds}$

$$\begin{matrix} \text{E Portal} = 4.6 - 2 = 2.6 \times 12 \times 3.3 = 103^{\circ} \\ \text{W. Shaft} \text{ W. } = 2 \times 12 \times 3.3 = 79^{\circ} \end{matrix}$$

Schneider Shaft.  $(9.5' - 7.5') 2 \times 5 \times 3 = 33^{\circ}$

Tunnel  $3.5 \times 9 \times 2 = 63^{\circ} = 10 \text{ yds}$

MH 40 to 41

$35 \times 0.5 \times 3.5 = 61.3$

$13 \times 3.4 \times 4.0 = 176.8$

$8 \times 5.4 \times 4.0 = 172.8$

Tunnel. 5'  $7.5 \times 5 \times 3 = 112.5$

$13 \times 7.5 \times 3 = 292.5$

$14 \times 8.0 \times 3 = 336.0$

$18 \times 5.0 \times 3.5 = 315.0$

$1466.9 = 54 \text{ yds}$

MH 40  $8.5 \times 6 \text{ dia} = 280^{\circ} = 10 \text{ yds}$

add 1 yd. = 9 yds for Geo.

Duke "F" Line MH 40 West.

$13 \times 2.9 \times 2.5$

$18 \times 2.8 \times 2.5$

$7 \times 4.5 \times 2.5$

$11 \times 5.0 \times 2.5$

16 yds.

Sleeve 6 yds Ext.

5 yds B.F.

B.F. MH 36 to P.H.

Except

$15 \times 16 \times 6 = 1440$

$20 \times 10 \times 6 = 1200$

5 yds B.F.

2640



Est. 4-2-36

Duke "F" line W

$$11 \times 5 \times 2.5 =$$

$$8 \times 5.5 \times 2.5 =$$

$$22 \times 4.5 \times 2.5 =$$

$$4 \times 4.0 \times 2.5 =$$

$$15 \times 3.8 \times 4.0 =$$

228

763 <sup>00</sup> = 25 yds  
14 prelim

11 yds <sup>3</sup>/<sub>2</sub>

# MH 40 Same. No excav.

MH #40 to MH #41

7' not excav next MH #40

30' conc pipe 8"

Pitch Finish Exc. 8+60 to 9+35

$$7 \times 2.9 \times 3.5 =$$

$$35 \times 0.5 \times 2.5 =$$

Steve MH #38 to MH #39 Grade Comp to 10+61

10+61 to 10+44 17 x 3 x 3.4

B.F. Starts 10+90

Copley 70 x 1.0 x 2.5 = 175 = 6 yds.

Est. 4-3-36

32  
33  
99  
99  
1089

# MH 41 to MH #42

Schneider Shaft. 11 x 3.3 x 3 = 4 yds.

B.F. 8 x 3.5 x 4 = 4 yds

MH 41 to MH 40

$$5 \times 3.5 \times 3$$

$$3 \times 1.0 \times 3$$

$$6 \times 2.2 \times 3.5$$

$$35 \times 0.5 \times 2.5$$

Ditch Finished 8+55 to MH 40

"F" Line Duke

$$17 \times 3.3 \times 3.5 = 162$$

$$8 \times 3.5 \times 2.5 = \frac{70}{232} = 8 \frac{1}{2} \text{ yds.}$$

0+50 to 1+00 Finished

$$12 \times 3.0 \times 3.5 =$$

$$10 \times 4.2 \times 3.5 = 273 = 10 \text{ yds } \frac{1}{3}$$

Est. 4-6-36

MH 41 to MH 40

$$18' \times 3.5 \times 3.5 = 220$$

$$35 \times 0.5 \times 2.5 = 112$$

$$7 \times 2.0 \times 2.5 = 35$$

$$9 \times 1.5 \times 2.5 = 33.75$$

$$\frac{220 + 112 + 35 + 33.75}{333} = 12 \text{ yds.}$$

3.5' Ditch finished 8+55 to MH 40 9+42.35

$$= (45 \times (5.6 + 7.8)) \times 3.5 =$$

B.F. 8+62 to 9+42 = Except 2' x 12 x 3.5 = 84

$$10 \times 7.8 \times 3.5 =$$

8+62 to 9+42 } 65 yds. 46 yds total B.F.

$$2' \times 8 \times 4 = 64$$

$$20 \times (7.8 + 4.9) \times 3.5 =$$

$$3 \times 30 \times 4 = 360$$

$$9 \times 7.6 + 4.9 \times 3.5 =$$

$$\text{Except } 19 \text{ yds.} = 508$$

$$1893 = 70 \text{ yds}$$

70  
12  
19  
101 yds

Conc. Pipe laid to 8+62

34 yds Exc.

$$\text{MH 39 } 8 \times 5.5 \times 4' = 176 = 6\frac{1}{2} \text{ yds}$$

76 B.F.

$$\text{MH 39 } 13 \times 0.5 \times 2.5 = 16 = \frac{1}{2} \text{ yds}$$

30' Conc Pipe

to Exc to grade 10+40 to 10+60

MH 38 " " 1' from " 10+40 to 10+30

B.F. Comp to 9+65

$$\text{"F" line } 0+22 \text{ to } 0+37 = 15 \times 3.5 \times 4 = 84 \text{ yds}$$

Finished 0+37 to 1+00

$$45' \times 3' \times 3.5 = 470 = 17 \text{ yds}$$

MH 41 to MH 42 End of pipe 5+45

$$\text{Duke } \left\{ \begin{array}{l} 18 \times 4.5 \times 2 = \\ 5 \times 3.5 \times 2 = \end{array} \right\} 197.0$$

$$\text{MH 42 } 6' \text{ dia } \times 4 = 4 \text{ yds}$$

MH #42

Excav. 6.5 x 6' dia = 184 = 7 yds

MH #41 to MH #42

18' - 8" Concrete Sewer Pipe Laid.

$21 \times 5.5 \times 2 = 231$

$6 \times 5.0 \times 2 = 60$

$291 \ominus 197 = 94 \ominus = 3\frac{1}{2} \text{ yds}$

Tunnel B, Filled 35' W from E. Portal. Sta 6+37 + 6+68

B, Sta 6+76 to 6+85 =  $9 \times 11.4 \times 3.3 =$

= 42 yds

$339 \ominus = 12\frac{1}{2} \text{ yds}$

$54\frac{1}{2} \text{ yds}$

36 yds Exc.

25 " B, F

24' Conc Pipe

$1\frac{3}{4} \text{ yds concrete on piers}$

MH 41 to MH 40

$9 \times 4 \times 2.5 = 90$

$8 \times 2 \times 2.5 = 40$

$18 \times 3.5 \times 3.5 = 220$

$35 \times 0.5 \times 2.5 = 44$

$7 \times 3.7 \times 3.5 = 41$

$435 \ominus = 16 \text{ yds}$

86 yds Total.

8+55 to 9+42 Ditch Finish = 70 yds

B, B 8+62 to 9+42 Same as  $4/6/36 = 46 \text{ yds}$

"F" Line 28 x 5.5 x 3.5 = 539 = 20 yds

0+50 on same

10+60 to 10+34 Gr. Comp.

10+34 to 10+21 2' from Gr.

MH 39 Same

Copley Line "Beer"

$26 \times 1.6 \times 3 =$

$9 \times 3.5 \times 3 =$

$219 \ominus = 8 \text{ yds} \leftarrow \text{Add to previous}$

Estimate 4-8-36

MH 41 to MH 42

6+65+675 Add to prev  $10 \times 17 \times 3.5 = 420 = 15\frac{1}{2}$

Tunnel 2 yds

B.F. 18 yds

Duke MH 42 to grade

MH 42 Add  $\rightarrow 1.5 \times 28.3 = 42 \text{ cu.ft.} = 2 \text{ yds}$

$6 \times 1.5 \times 2.5 = 22.5 = 1 \frac{1}{4}$

3 yds

MH 41 to MH 40

Geo  
7 B.F.  
21 Exc

$18 \times 4 \times 3 = 216$   
 $27 \times 3 \times 3 = 243$   
 $25 \times 0.5 \times 2.5 = 31.25$   
 $11 \times 2.0 \times 2.5 = 55$   
 $\frac{86}{545} = 20 \text{ yds.}$

Exc. completed 8+45 to 9+42

B.F. = 2 yds. 2 yds Exc.

$\frac{4 \text{ yd}}{6 \text{ yds for Geo}}$

15' of 8" Conc. pipe

F<sup>W</sup> Line Tunnel  $8' \times 10' \times 3.3 = 264 = 10 \text{ yds}$

$0+22 \text{ to } 0+50 = 28 \times 6.0 \times 4.0 = 672 = 25$

" 5 yds B.F. from tunnel 20  
5 yds

Baker 2 yds Concrete.

6 yds Exc 6 yds B.F.

2 yds " Stord

Total 8 yds 6 yds B.F.

Water line

$16 \times 1.6 \times 1 = 25.6 = 1 \text{ yd.} \rightarrow 2 \text{ yds}$

~~$77 \times 1 \times 2 = 144 = 5 \text{ yds}$~~

28 yds Beer.

8 yds prev.

20 yds Balance 17 yds Turned in.

Estimate

4-9-36

" Dick

MH 42 to MH 42

W. Shaft B.F.  $5 \times 5 \times 3.5 = 3$  yds.

Tunnels between shafts.  $6$  "  $9$  yds.

" Duke

36" Clear & Grub

MH 42 to MH 43 { Exc  $21 \times 3 \times 2.5$  }  $203 = 7\frac{1}{2}$  yds }  $7$  yds Exc

MH 41 to MH 42 B.F.  $15 \times 5.5 \times 2.5$  }  $211 = 8$  yds }  $8$  yds B.F.

MH 41 to MH 40

$16 \times 6 \times 3 = 288$

15'-8" Conc. Pipe  $16 \times 3 \times 3.5 = 238$

$10 \times 2 \times 3.5 = 70$

" Geo = 17 yds exc  $25 \times 0.5 \times 2.5 = 73$

10 yds B.F.  $15 \times 3.7 \times 2.5 = 599$  4p to sta 8+46

B.F.  $20' \times 4 \times 3.5 = 280 = 10$  yds.

Tunnel in 12' 11' cut  $\times 3.5 \times 4 = 5$  yds

45' of 6" Concrete pipe.

$28 \times 9 \times 4 = 1008 =$

$672 = 12$  yds out

Turn in 9 yds.

BAKER

10+34 to 10+11

$21 \times 5 \times 3.5 = 368 = 13\frac{1}{2}$  yds. Total

24" Conc 8" pipe + Conc piers

Geor

$7 \times 5 \times 6.0 = 210$

$8 \times 7 \times 4.5 = 252$

$14 \times 5 \times 2.7 = 189$

1" Line.

$10 \times 3 \times 2.7 = 81$

$13 \times 2.7 \times 3.0 = 105$

$10 \times 0.5 \times 3.0 = 15$

$14 \times 2.5 \times 3.0 = 105$

$70 \times 0.5 \times 3 = 105$

$651$   
 $411$   
 $1061 = 39$  yds

9 yds for Geor

4-10-36

58

L

$7.5 \times 6.5 \times 2.5 = 396 = 14$  yds.

$18.0 \times 5.5 \times 2.5 = 247.5 = 7$  yds. - Exc

$7$  yds. - Exc

$3$  yds B.F.

Dick

Tunnel between shafts 4 yds.

W. shaft. 3 yds.

Long W. Tunnel  $2.5 \times 12 \times 3.5 = 4$  yds

11 yds. B.F.

Geo

$23 \times 5.5 \times 2.5 = 312$

$20 \times 3.5 \times 3.5 = 245$

$13 \times 3.5 \times 2.5 = 113$

$25 \times 0.5 \times 2.5 = 31$

B.F. 8+35 to 9+42

$11 \times 4 \times 3 = 5$  yds

$13$  yds

$18$  yds

$43$

$458 = 580$

Except.  $18 \times 2.5 \times 4$

$11 \times 2.5 \times 4$

$25 \times 2.0 \times 4$

" F Line Tunnel. Eportal.

17' in

$5 \times 12 \times 3.5 = 210$

$2\frac{1}{2} \times 12 \times 3.5 = 176$

$28 \times 9.5 \times 4 = 1064$

1400

$21 \times 5.5 \times 3.5 = (21 \times 5.5 \times 3.5) = 11\frac{1}{2}$  yds.

+ Piers  $2\frac{1}{2}$  yds

25 yds B.F. 2" yds Exc. for Baker. + 4 yds.

Geor

Copley Ave

$7 \times 6 \times 4 = 168$

$10 \times 7 \times 3.7 = 259$  + 6 yds over.

$13 \times 6.5 \times 2.5 = 211$

$10 \times 3 \times 3 = 90$

128

$26 \times 3 \times 3 = 234$

$6 \times 10 \times 3 = 18$

$24 \times 28 \times 3 = 201$

$9 \times 2 \times 3 = 54$

$61 \times 0.5 \times 3 = 91$

598

1326

= 50 yds

56 yds

10 yds.

1" Line on Copley Ave

$50 \times 1 \times 1 = 50 = 2$  yds bottom

7 yds on top

9 yds - 5 yds = 4 yds.

40 yds for ditch Total. 6 yds " Overlap.

WATER LINE  $7\frac{1}{2} \times 1 \times 1 \times 2 = 14\frac{1}{2} = 5$  yds  
Pier = 2 yds. Total  $7\frac{1}{2} = 3$  yds

27222  
Duke Mon 4-13-36 24 60 1440

MH 42 { 40' Linear ft. Clearing 6 Grub.  
to }  $22 \times 0.5 \times 3 = 33$   
MH 43 {  $15 \times 2.7 \times 3 = 121$  } 154 =  $5\frac{1}{2}$  yds.  
 $30 \times 5.9 \times 2.7 = 47.8 = 18$  yds. - 14 = 4 yds  
3 yds. overb. = 12 yds. Duke No B.F.

Dick Tunnel  $6 \times 12 \times 3.5 = 252 = 6$  yds B.F.  
W. Shaft W. Portal,  $9 \times 5 \times 3.5 = 157.5 = 6$  yds.  
Exc. 12 yds B.F.

6 yds. Exc reported.  
3 yds B.F. {  $7-66 - 8+00$  }  $134 \times 5.7 \times 3.5 = 2583$   
863 }  $10 \times 3.5 \times 2.5 = 87.5$  } 32 yds  
8+25 }  $13 \times 3.0 \times 2.5 = 97.5$

Total 20 yds Exc 24 of 8" Concr. Pipe.  
19 yds B.F. }  $6' \times 12 \times 3.5 = 252 = 10$  yds. Tunnel } " " } F Line  
MH 40 to MH 42 } 4 yds Exc } F Line

Exc to Grade 10+13 to 10+34 } 3 yds  
10 yds B.F. }  
Main Ditch 1 yd. at Sta 0+30 } 141 0+92 }  
1" Line  $18 \times 2.5 \times 2 = 90$  } 1446+95 }  
 $16 \times 1.8 \times 2 = 57.6$   
 $147.6 = 5$  yds.  
3 yds  
8 yds Exc.

Baker { 3 yds Exc }  
18 yds B.F. }  
MH 38  
MH 39  
MH 39  
MH 40

Tues Estimate 4-14-36 WPA # 2353 59

"Duke" " 4+25  $15 \times 2.4 \times 4 = 144$   
MH 42 to MH 49  $10 \times 1.0 \times 4 = 40$   
 $17 \times 4.0 \times 3 = 204$   
 $34 \times 5.8 \times 2.5 = 493$   
881 = 32 = 9 yds  
overb 3 yds  
12 yds  
MH 41 to MH 42  
"Dick" W. Portal  $12 \times 5 \times 3.5 = 210 = 8$  yds  
E "  $3 \times 5 \times 3.5 = 52.5 = 2$  yds  
10 yds B.F.

" " MH 41 to MH 42  
Geo.  $34 \times 5.8 \times 3.5 = 670$   
 $10 \times 3.7 \times 2.5 = 92.5$   
 $13 \times 3.2 \times 2.5 = 104$   
866 = 32 yds No yds  
Exc 8 yds "F" Line  
5 yds B.F. on "F"

0+90 }  $10 \times 6.0 \times 5.5 = 330 = 12$  yds } " "  
1+00 } + Tunnel -> } Geo

" " Geor Copley Ave.  
Ditch Finish 0+32. Sewer Stationing.  
 $0+32 - 0+50$  }  $12 \times 3 \times 3 = 108$   
 $0+60 - 0+89$  }  $29 \times 2.6 \times 3 = 228$   
 $1+00 - 1+15$  }  $15 \times 3.0 \times 3 = 135$   
 $1+15 - 1+35$  }  $20 \times 2.0 \times 3 = 120$   
 $1+35 - 2+00$  }  $65 \times 0.6 \times 3 = 117$   
706 = 26 yds.  
37 yds  
Total to 63 "  
Date.

1" Line Copley Ave.  
 $1+50 - 2+00$  }  $50 \times 2 \times 1.2 = 120$   
 $1+37 - 1+50$  }  $13 \times 0.5 \times 1.2 = 7.8$   
 $1+00 - 1+37$  }  $37 \times 2.5 \times 1.2 = 111.75$   
16 yds.  
0+50 - 1+00 }  $50 \times 2.7 \times 1.5 = 202.5$   
Geo reported.  
6 yds B.F.  
12 yds Exc.

"Steve" MH 38 to MH 39. 2 yds Exc.  
Baker (between MH 39+40) + MH 39

Est Wed. 4-15-36

"Duke" 10 yds, Excav. No B.F.  
Report 30 ft Brush & Clearing

"Dick" Tunnel 5' progress  $12 \times 5 \times 3.5 = 210 = 8 \text{ yds}$   
Report Raise 2' ..  $12 \times 2 \times 3.5 = 84 = 3 \text{ yds}$   
11 yds.

"Baker" 54'-6" pipe } 6" Line "F"  
Report 9 yds B.F. }

"Steve" 1/2 yds Exc. for piers.  
Report.

"Geo" MH 40 to MH 41 23 yds B.F. "A" Line  
Report Tunnel 6 yds Exc. 6" Line ("F" Line)

Geor →

Est 4-15-36

MH #42 to #MH 43, "Duke"

Sta 4+00 - 4+17 =  $17 \times 2 \times 3 = 112$   
30' clearing & 4+25 - 4+41 =  $16 \times 3.5 \times 4.5 = 252$   
Brushing. 4+41 - 4+51 =  $10 \times 2 \times 3.5 = 70$   
4+51 - 4+66 =  $15 \times 5 \times 3.5 = 262$   
26-14 = 12 yds. for 4-15-36  $696 = 26 \text{ yds}$

"Geo" "F" Line 1+00 - 1+03 3' progress in tunnel = 6 yds

Geor Copley Line 0+50 - 1+15 =  $65 \times 3.8 \times 3 =$   
 $20 \times 2 \times 3 =$   
 $6.5 \times 0.6 \times 3 =$  } 978 = 36

36 + 37 = 73 yds total.

63  
10 yds in sewer line.

Est. 4-16-36 Thurs.

60

BAKER #  
MH #42 to MH #43 B.F.  $15 \times 5.7 \times 2.7 = 8 \text{ yds B.F.}$   
(Excav 5 yds Between 41 & 42) XX  
{ Dick 7 yds B.F. Tunnel } MH 41 to MH 42  
3 yds }  
10 yds. 15' of 8" pipe Laid.

{ Geo.  $10 \times 3.3 \times 2 = 132 = 5 \text{ yds}$  1+18 + 1+28  
Tunnel No 6' progress in tunnel. } 11 yds Exc.  
 $8 \times 6 \times 3.5 = 168 = 6 \text{ yds.}$  }  
E Tunnel No 1.  $12 \times 3.5 \times 8 = 12 \text{ yds B.F.}$

{ Steve 1 yds for piers. 2 yds MH 39 }

{ Geor }  
 $65 \times 5 \times 3 = 1975 = 40 \text{ yds} - 36 = 4 \text{ yds}$   
 $50 \times 1.5 \times 1 = 75 = 3 \text{ yds} = 7 \text{ yds total.}$   
8 yds B.F. around P.H. 8 yds  
45 of 6" pipe. 15 yds

Friday → 4-17-36

Tunnel W-Portal. G' progress  $12 \times 6 \times 35 = 252 = 8 \text{ yds}$   
 "Geo" 10 yds Exc 15 yds B.F. "F" Line  
 "Steve" 4 yds " MH 39 4 " B.F. MH 39 to 40  
 Geer. 0+50 to 1+15  $65 \times 6.8 \times 3 =$  to 1+15  
 $65 \times 1.8 \times 3 = 7$   $50 \times 11 \times 15 =$  to 1+00  
 $50 \times 1.0 \times 1.5 = 461$   $10 \times 5.0 \times 3 =$  to 1+25  
 $10 \times 1.5 \times 3 =$   
 = 19 yds Exc Sta 1+25 to 1+60 2 yds  
 = B.F.

Tues. 4-21-36

Tunnel "F" Line 1+00 West 9' from portal.  
 $10 \times 8 \times 50 =$   
 $34 \times 3 \times 35 =$   
 Stingley 12 yds B.F. (8' in tunnel) (4' shaft)  
 " " Steve 6 yds B.F. 4 yds Exc  
 F → Geo. 17 " B.F. 8 " 3' progress tunnel  
 Baker. 27' - 8" conc Baker  
 " " Geer 26 yds Exc.

Est # 2353  
 Wed. 4-22-36

1+11 "F" Line  $10 \times 9.2 \times 5.0$  Tunnel  $12-9 = 3 \text{ ft}$  progress  
 West. Same →  $34 \times 3 \times 3.5$  2 yds. = 5 yds  
 Geo. Eastlick } 7 yds exc.  
 } 4 yds B.F.  $2 \times 3.5 \times 18 = 4 \text{ yds. B.F.}$   
 "A" Line MH 41 to 42 7' B.F. in tunnel = 11 yds  $7 \times 12 \times 3.5 =$   
 Stingley Outside = 3 yds.  
 "A" Line  $18' \times 5.5 \times 3.4 = 337$   $14 \times 2.5 \times 3.5 = 122$   
 Starting  $5 \times 2.5 \times 3.0 = 37$   $2 \times 6 \times 2.5 = 30$  4+73  
 4+73  $19 \times 4.5 \times 4.4 = 376$  1146  
 S. side shed  $18' \times 5.5 \times 4.0 = 396$   
 Stevens  $18' \times 5.5 \times 4.0 = 396$   
 MH #43 started 6' dia x 2' = 2 yds. Total.  $\frac{152}{1146} = 18 \text{ yds}$   
 Baker. 21' of 8" conc. pipe 10+13 - 10+34. also cemented.  
 " 21 " 8" " " Torn out  
 Geer 8" Line DMH 5.80

ESTIMATE Thurs. 4-23-36

MH #43  $3.5' \text{ deep} \times 6' \text{ dia} = 99 \text{ cu} = 3 \frac{1}{2} \text{ yds}$   
 MH 42 to MH #43.  
 $31 \times 5 \times 3.5 = 543.$   
 $10 \times 4 \times 4.0 = 160$   
 $10 \times 5.3 \times 4.0 = 212$   
 $3 \times 2.2 \times 3.0 = 19$   
 To N side  $18 \times 6.5 \times 3.5 = 409$   
 $7 \times 7 \times 2.5 = 123$   
 $1466 = 54 \text{ yds.}$   
 Stevens.

MH 41 to MH 42 Tunnel  $8 \times 3.5 \times 9 = 252 = 9 \text{ yds}$   
 outside = 2  
 11 yds  
 "F" Line G. Eastlick Tunnel  $2 \times 12 \times 35 = 84 = 34 \text{ yds}$   
 cuts above tunnel  $10 \times 10 \times 5 = 50 = 2 \text{ yds.}$   
 $34 \times 3.7 \times 3 = 153 = 5 \frac{1}{2} \text{ yds}$   
 Report 11 yds Exc  
 2 yds B.F.  
 MH 39 to MH 40 19 yds B.F.  
 C. Line D.M.H. =  $8.3 \times 6 \text{ dia} =$  3 yds prog.  
 Portal Tunnel = 4 yds  
 Tunnel  $18 \times 4 \times 3.5 = 252 = 9 \text{ yds.}$  19 yds Exc. 100 ft  
 Foot Bank  $4.5 \times 6 \text{ dia} = 2 \frac{1}{2} \text{ yds prog.}$  12 yds B.F.



Estimate  
Friday 4-27-36

MH #42 to MH #43

$31 \times 5.3 \times 3.5 = 575$   
 $10 \times 5.5 \times 4.0 = 240$   
 $3 \times 8 \times 3.5 = 84$   
 $1.9 \times 8 \times 3.5 = 53.2$   
To N. Side House  
 $10 \times 8.2 \times 2.5 = 205$

$1808 = 67 \text{ yds} = 13 \text{ yds} + 1 \text{ yd.}$   
 $-54$   
 $13$

MH 41 to 42 } 2' Tunnel  $7 \times 3.5 \times 2 = 49 \text{ yds.}$  } B.F.  
 $10 \times 3.5 \times 4 = 140 = 5 \text{ yds.}$

MH 41 to 40  $5 \text{ yds B.F.} = 12 \text{ yds Total.}$

"F" Line Tunnel  $13' \text{ in} - 12 = 1 \times 3.5 \times 12 = 1 \frac{1}{2} \text{ yds}$   
Same  $10 \times 10 \times 5 = 50$   
 $25 \times 5.5 \times 3 = 393.75$   
Sky 5 yds.  $9 \times 3.7 \times 35 = 1147.5$   
 $5 \text{ yds.}$   
 $7 \text{ yds.}$

Geer. D.M.H. =  $6 \text{ dia} \times 19.2 = 8.3 = 2 \text{ yds.}$   
Tunnel  $6 \frac{1}{2} - 4 = 2 \frac{1}{2} \times 18 \times 3.5 = 157 = 5 \frac{1}{2} \text{ yds}$   
MH  $5.7 \times 6' \text{ dia} = 1.2 \times 28.3 = 34 = 1 \frac{1}{2}$   
 $9 \text{ yds. Excav.}$   $10 \text{ yds reported}$   
 $8 \text{ yds B.F.}$

Baker 5 yds B.F. MH 38 to MH 39

WPA PROJECT #2353  
Mon. Estimate 4-27-36

62

MH #42 to MH #43. (Stevens Foreman)

$31 \times 6 \times 3.5 = 651$  MH #43  
To shed  $29 \times 6.5 \times 4 = 754$   
 $5 \times 4 \times 6 = 120$   $12 \times 8.5 \times 3.5 = 357$   $5' \text{ deep} \times 28.3 = 141.5$   
 $1762 = 65 \text{ yds.}$   $= 5 \text{ yds.}$

MH #43 to MH #44 Stingley Foreman.

$80 \times 3.3 \times 1.0 = 264$   
 $80 \times 3 \times 0.2 = 48$   
 $= 12 \text{ yds. Clearing \& Grubbing} =$

"F" Line Geo. Eastlick, Foreman.

14' Tunnel - 13' =  $1 \times 12 \times 3.5 = 42$

$10 \times 11 \times 5 = 550 - 500 = 50$   
 $34 \times 5.5 \times 3.5 = 654 - 514 = 140$   
 $35 \times 1 \times 3 = 105$   
 $295$   $337 = 12 \frac{1}{2}$

"C" Line, F. Geer Foreman

D.M.H. #50 Depth =  $13.6 - 10.2 = 3.4 \times 28.3 = 96$   
Tunnel  $10 - 8 = 2 \times 4 \times 18 = 144 = 5 \frac{1}{2} \text{ yds.} = 3 \text{ yds.}$   
outside =  $1 + 6 + 3 = 10 \text{ yds Total}$

Estimate 4-28-36

MH #43 to MH #44  
 $76 \times 3.5 \times 3 = 801$   $12 \text{ yds} = 18 \text{ yds}$

MH 43 to MH 42  
Stevens  $30 \times 7.3 \times 3.5 = 767$   
F.  $10 \times 7.7 \times 3.5 = 269$   
 $18 \times 10 \times 4 = 720$   
 $13 \times 9 \times 3.5 = 409$   
 $2075 - 1762 = 313 = 11 \frac{1}{2} \text{ yds Exc}$   
 $10 \text{ yds B.F.}$

Baker 18 yds B.F.

"F" Line G. Eastlick

Tunnel  $19 - 14 = 5' \times 12 \times 3.5 = 210$   
 $34 \times 6 \times 3.5 = 714 - 654 = 108$   
 $318 = 12 \text{ yds.}$

"C" Line, F. Geer

$16.5 - 13. = 3.5 \times 28.3 = 99 \text{ yds}$

Estimate 4-29-35

# MH 44 to MH 43

Beyond Stone W.  $\left. \begin{array}{l} 8 \times 2.5 \times 3 = 192 \\ 20 \times 2.2 \times 3 = \end{array} \right\} = 7 \text{ yds}$

4.2 Sta  $3+00$  to  $3+25 = 25 \times 2.9 \times 3.3 = 239$  To 1st Bk  
 $(4+2+6) \rightarrow 3+25$  to  $3+50 = 25 \times 5.1 \times 3.5 = 947$   
 $3+50$  to  $3+68 = 18 \times 4.7 \times 3.5 = 294$   
 $3+68$  to  $51 = 13 \times 4.5 \times 3.5 = 1186$  1378 total = 51 yds

MH 43 = 5' deep

53-30 = 23 yds. 50 yds

MH 43 to MH

$(30 \times 8.6 \times 3.5) = 803$

23 Tunnel  $4 \times 12 \times 3.5 = 168 = 6 \text{ yds}$

14  $10 \times 27.7 \times 3.5 = 269$

37  $18 \times 11.4 \times 4 = 807$

3  $13 \times 9 \times 3.5 = 409$

34 yds Report  $\frac{1485}{803}$

$2288 - 2075 = 8 \text{ yds}$

14 yds

Geo. Eastlick "F" Line 10 yds

178 cu. ft. in ditch =  $6\frac{1}{2}$  yds  
 100 cu. ft. covered in =  $3\frac{1}{2}$  yds } 10 yds.

"O" Line F. Geer.

Tunnel E Portal  $14.5 - 12.5 = 2$  progress.

Tunnel W Portal 3 progress  $\times 16.3 \times 4 = 196$

W Tunnel Started.

Estimate 4-30-36

MH 44 MH 45  $22 \times 0.5 \times 3.3 = 36$  MH 44  $6 \times 0.5 \text{ depth} = 14$

MH 44 to 43 To Stone W

$16 \times 2.4 \times 3.3 = 21$

$8 \times 2.5 \times 3 = 60$

$20 \times 5.5 \times 3.5 = 1872$

3+00 3+25

$4 \times 2.5 \times 3.5 = 1872$

3+25 3+50

$21 \times 3.0 \times 3.5 = 1953$

3+50 3+80

$25 \times 5.5 \times 3.5 = 1378$

$30 \times 6.7 \times 3.5 = 575$

MH 43 Stone

MH 43 to 42

$30 \times 8.6 \times 3.5 = 10 \text{ yds B.F.}$

Tunnel  $4 \times 12 \times 3.5 = 172$

Tunnel  $2 \times 12 \times 4 = 96$

12.3  $10 \times 12 \times 4 = 172$

$18 \times 6 \times 3 = 168 = 10 \text{ yds}$

2.3  $18 \times 6 \times 3 = 168$

$13 \times 6 \times 3 = 168$

4-30-36 Cont

63

"F" Line

Geo Eastlick "F" Line

BAKER PIPE

"F" Line  $10 \times 10.5 \times 5.0 = 525$

$34 \times 7.5 \times 3.3 = 333$

$35 \times 7 \times 3 = 735$

"C" Line

E. Portal  $2.5 \times 18 \times 4 = 180$

6 yds Exc.

3 yds. B.F.

2 1/4 ft of 6" pipe

16' from 1st set

8 yds out Exc

8 yds B.F.

Ditch MH 36 to P.H.

$13 \times 14.5 \times 6 = 1352$

$12 \times 4.5 \times 6 = 324$

$16 \times 1.6 \times 5.2 = 1331$

$20 \times 8 \times 5.5 = 880$

1352

3563

1331

880

MH 44 to MH 45

$23 \times 1.0 \times 3.5 = 34 \text{ yds} - 1 = 2 \text{ yds}$

5-1-36

MH 44

$6' \times 0.5'$

None = 1/2 yd.

MH 44 to 43

$17 \times 2.0 \times 3 = 72$

$25 \times 3.3 \times 3.5 = 292$

$8 \times 3 \times 3.5 = 84$

$30 \times 6.6 \times 3.5 = 2092$

$21 \times 5 \times 3.5 = 367.5$

211 = 8 yds

$25 \times 5 \times 3.5 = 437.5$

2764 = 80

MH 43 to 42

1 yd. Tunnel =  $2 \times 12 \times 4 = 96$

B.F. = 20 yds.

"F" Line

$10 \times 11 \times 5 = 550$

25

$7 \times 3 \times 3 = 63$

At 1 P.M.

$34 \times 8.4 \times 3.3 = 947$

101

$2.2 \times 1.2 \times 2.5 = 65$

$5\frac{1}{2} + 2\frac{1}{2} = 8 \text{ yds}$

126

$\frac{65}{128} - 105 = 1 \text{ yd}$

$40'$  of 6" pipe laid

"C" Line

F. Geer

19 yds Exc

19 yds B.F.

Stone Bank Exc

20 yds B.F.

Ditch 11 yds Exc

$13 \times 9 \times 6 = 729$

$13 \times 3.5 \times 6 = 273$

$19 \times 10.5 \times 5.2 = 1011$

$25 \times 7.1 \times 5.5 = 962$

729

2618

681

3563

2618

2618

3563

35 yds

5-1-36

(F.L. 085 Below)

64

## A" Line

Sta	+	H.I.	-	Elev	Top Bell String Grade	
4+50	2.085	379.975		347.89		3' offset c 11-94
4+37			12.88		37.09	Top of Bell
4+09			11.71 Top Iron Stake	338.265	37.21	12.765 Gr Red Top Bell Red Mark Iron Stake Raise .01
3+83.42			11.57 Top Iron Stake	338.405	37.335	12.64 " " " " " "
3+50	2.72	349.79		47.07		6' offset 37.09
3+83.42	} 0.15 Diff.		Top stake 11.59			Top main stake.
3+51			Top stake 11.63			12.51.5 12.50
4+50	9.29	48.33		43.94 B.M. 47.94		6' offset Hub.
4+37			11.44	36.89		Top Bell Check
4+10			11.325	37.005		Top " Check
3+83 MH #43			11 10.12	38.21	37.13	
			K. McCarthy & Walker			5-4-36 Monday Clear
3+50	2.48	349.55		347.07		6' Offset
Str. Grade Top Bell MH #43			<del>12.41</del>	<del>337.14</del>	37.14	
3+51			11.39	38.16	38.31	Top Iron Stake
MH 43 Top Stake			11.35	38.20		
4+50	0.83	348.77		47.94		6' Offset
4+10			11.77	37.00	37.00	Top Bell
3+83 T.P.	11.24	49.44	10.57	38.20	37.115	Top Stake
3+51			11.29	38.15	37.360	" "
3+25			11.075 Top stake	38.365	37.477	Top Stake
3+00			9.84		37.59	Gr Red 11.85 (For Grading only)
3+50			2.37	347.07		6' Offset

"C" Line.

5-4-36

Sta	+	H.1	-	Elev	F.L.	
M.H. 1+74	3.95	367.37		363.42	358.00	C.S. 4" Hub 6' offset.
F.L. M.H. 4 1+74.			9.40	357.97	358.00	
1+79			8.21	59.16	58.48	Top Bell
1+88	4.2 3.2	63.4	7.16	60.21		on ground. 3.2 Hand ls.
1 94.5			H.L. 2.5	60.9		on ground.
2+02.5			H.L. 1.2			on ground.
2+23.0					65.28	

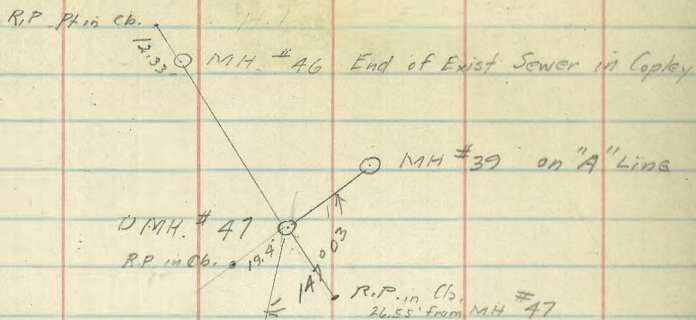
5-6-36

2+09	5.41	386.55		381.14		Hub. 6' offset
2+21			4.96	381.59	65.28	D.M.H. Hub 6' offset. C 16.31
2+21			4.67	381.88	65.28	C. 16.60 to F.L. C 15.92 to Str. Gr. Blue Keel on timber

"A" Line

5-6-36

3+00	3.93	350.33		46.40		6' offset.
			3.62	46.71		Stone Wall 1' Right 2+99
3+25			12.87	37.46	36.61	Top Bell.
2+99			11.63	38.70	36.73	Top Iron Stake C 1.12 Gr. Rod = 12.75 37.52 = 54
2+84			8.76	41.57		
3+52			13.06	37.27		Top Bell
3+50	2.39	49.46	5-6-36 P.M.	47.07		6' offset. 12.305 12.75 13.0
3+25			12.00	37.460		
2+99			11.875	37.585	36.735	
3+50			12.175			Top Bell - Rod
3+80			12.42	37.04	36.30	Top pipe 3+78 12.305 Top Bell
3+80			12.50			Top pipe



Sta.	+	H.I.	-	Elev	F.L
39 <sup>th</sup> & Circle Dr.					
B.M. Br. Plug	1.81	358.76		356.95	
T.P. on Cb.	7.69	356.19	10.26	348.50	
F. Hyd. Foot of 39 <sup>th</sup> St.			8.25	347.94	
6' Off. MH #45	1.76	347.36	10.59	345.60	
2+99 End of pipe.			9.76	3760	36.75
K. McCarty J. Walker. Clear & Warm 5-7-36					
3+00	0.79	347.19		46.40	
2+99			9.615		
			8.27		
2+79	Top Bell	String grade	9.535		
5-8-36					
3+00 6' offset	0.98	347.38		346.40	
2+99			9.805	337.575	36.725
2+79			9.725	337.655	36.805

Top F.H.  
 17 345.54 By Moore  
 Top Bell  
 6' Offset  
 End pipe Top Bell  
 C 1.265  
 C 9.16  
 Top Bell ✓  
 String Grade Top Bell ✓

COPLEY AVE

5-11-36

Clear, Warm.

"C" Line High Pressure

McCarty  
Walker

Sta.	+	H.H.	Elev.	F.L.
5+00	5.21	392.83	387.62	382.91
5+00			5.09	387.74
5+50	4.09	392.83	388.74	384.11
5+50			4.04	388.79

"A" Line

2+43.78 MH #44	2.34	49.69	47.35	36.90
-------------------	------	-------	-------	-------

"A" Line

2+82 <sup>00</sup>		12.05	37.64	36.79
2+43.78	3.22 @ 00.4%	10.82	38.87	36.94
2+06.78		11.20	38.49	37.09
2+75		3.68	46.01	
3+00		3.31	46.38	

"A" Line Check on pipe 5-12-36

2+75	3.57	349.59	46.02	
2+82		11.95	37.64	36.79
2+43.78 = MH #44		10.71	38.88	36.94
2+07		11.10	38.49	
2+07.78		No H.I.	6.39	
2+			6.47	
2+38.78			6.49	
2+43.78	2.175	349.525	347.35	
2+82	} a.35		11.875	337.65
2+46.18			11.770	337.755

36

6.09

35  
20

6.39

.10

6.39

6.47

6.49

5.24

67

11 36  
6' offset Left Set by Moore  
6' " Right Set 5/11  
6' offset Left Set by Moore  
6' " Right Set 5/11  
6' offset Lt.  
Top Bell Str. Grade  
Str. Gr. Rod = 11.90 C.1.08 Top Stake  
11.75 C.0.55 " " 2+4  
C.9.27  
C.9.76 6' offset  
46.90  
C.9.27  
Top Bell  
Top Stake C.1.09 String Grade = 37.79  
Top Stake 11.87  
on bell  
on bell  
Hub  
Top Bell  
on "

"C" Line

4-21-36

Sta.	+	H.I.	-	Elev.	F.L.
1+00				360.27	353.74
+25		65.45	8.6	58.99	55.18
+50	536	65.48		360.07	56.62
1+74 = MH #49				363.42	358.00
1+75			9.60	55.85	
1+50			8.16	57.29	
1+69			7.07	58.38	
1+74			2.01	63.44	58.00
1+91					60.63
1+74	5.19	368.61		363.42	58.00
1+90.8				68.61	60.60
	4.97	340.38		35.41	
			6.73	33.65	32.92
			7.46		
			7.51		
Hub Offset					
9+70.35	5.06	340.47		35.41	
1st joint					
10+10			6.82	33.65	
2nd "			6.74	33.73	32.88
3 "			6.76	33.71	32.86
4 "			6.77	33.70	32.85
5 "			6.77	33.70	32.85
6 "			6.77	33.70	32.85
7 "			6.76	33.71	32.86
8 "			6.75	33.72	32.87
			6.74	33.73	32.88

CG.53  
 3.81 3' offset  
 C3.45  
 C5.42  
 Str. Gr. Top Bell  
 Str. Grade Top Bell  
 " "  
 Hub 6' offset C5.44

C2.24  
 0.73 to F.L.  
 F.L. 7 9" 0.05 Fall  
 F.L.

Old Hub offset 9+70.35 old Stationing  
 1100  
 Read. N. End Pipe 0.73 F.L.

This line corrected to give 0.08 Fall

"C" Line

4-22-36

STA.	+	H.I.	-	Elev.	Grade		
1+50	6.97	367.04		60.07	56.62	0.3, 45	Hub 6' offset
			6.21	360.83		0.9, 21	"
1+50			9.69	357.35	56.68	Checks	"
1+50			9.75	357.29	56.62		"
1+74							
1+23			11.32	<sup>Bell</sup> 55.72	55.05	Check 0.01	
0+99			12.71	<sup>Bell</sup> 54.33	53.66	Check 0.02	

"A" Line

	0.51	44.34		343.83			B.M. on Nail bottom stump Sta 5+35 - Lt.
5+11			8.07	36.27	35.51	Top Pipe	"
5+16			8.11	36.23		" "	"

"C" Line

Check on 6" pipe concrete

1+50	5.13	65.20		60.07			
1+68			6.84	58.36	57.69	on bell	
1+50			8.01	57.19	56.62	on pipe	
1+25			9.45	55.75	55.18	" "	

4-29-36

B.M. E. of P.H.	3.65	357.08		353.43			
			5.62	351.46		Top P.H. above outlet	
				348.61		F.L. of P.H.	
SW			5.64	351.44			



Iron Pipe	Partly Cloudy	4-24-36	McCarty II Walker		
STA.	H.1	Elev.	F.L.	Bell Grade	
B.M.	9.46	362.89	353.43		
0+00			348.61	50.75	
0+3.08	3.08		348.61		
0+19.04	15.96	12.44	349.77	50.45	✓ 1
0+35	✓	11.26	350.94	51.62	✓ 2
0+50.95		10.11	352.10	52.78	✓ 3
0+66.91		8.94	353.27	53.95	✓ #4
0+82.87		7.78	354.43	55.11	✓ #5
0+98.83		6.61	355.60	56.28	#6
1+14.78		5.45	356.76	57.44	#7
1+30.74		4.28	357.93	58.61	#8
1+46.70		3.12	359.09	59.77	#9
1+62.66		1.95	360.26	60.94	
1+78.61			361.42	62.10	

1507  
52.8  
12056  
301.4  
7535  
7956.96

13  
145  
1+11 1507  
14.52  
7535  
6028  
7507  
21851.5

7.96  
47.15  
55.11

47.15  
21.19  
29.34

54.92  
47.82  
6.22  
6.68  
54

MH 44  
MH 45  
140.14

Sever. 4-28-36

"C" Line	2.44	365.86	363.42	358.0	65.42
MH #99	1+74		7.99	357.87	F.L.
MH 76			7.25	358.61	58.05
			2.83		Top pipe
1+95			00	65.86	60.93
"F" 1+14	5.19	6457		59.38	47.15
1+18.3			10.55	54.02	47.80
1+28.5			9.82	54.75	49.34
1+52.8			8.98	55.59	55.11

Sta. 6  
C 4.25  
Nail 2' 5' Partial

C 5.54 to Str. Line  
C 5.41  
C 4.73 to Str. Gr.  
C 4.48  
F 0.20 to Str. Grade

5  
1.3

Partly Cloudy

4-29-36

T. McCarty  
D. Walker

"A" Line  
Sta

+	4.1	-	Elev.	F.L. Grade
---	-----	---	-------	---------------

4+25	2.01	349.73	47.72	36.06
------	------	--------	-------	-------

Hub 3' offset - C 11.66

4+55			12.925 085	36.805	35.955
------	--	--	---------------	--------	--------

4+36			12.840	36.880	36.03
------	--	--	--------	--------	-------

4+26			8.76	40.97	36.08
------	--	--	------	-------	-------

Marked C. 5.0 to F.L. on spreader.

T.P. 3.86

Hub 3' offset

4+18			12.04	39.59	36.12
------	--	--	-------	-------	-------

Marked C. 3.5 on Wall plate

4+50	3.64	51.62	3.64	47.94	35.93
------	------	-------	------	-------	-------

6' offset C 12.0'

4-27-36

MH #43	1.23	45.16		43.93	36.26
--------	------	-------	--	-------	-------

C. 7.67 6' offset Hub.

MH #43			8.06	37.10	36.25
--------	--	--	------	-------	-------

Set string grade top bell on iron stake & of MH

4+00			0.60	44.56	
------	--	--	------	-------	--

Hub 3' offset.

B.M.	5.51	349.45		343.94	
------	------	--------	--	--------	--

4+55			12.65	36.80	35.95
------	--	--	-------	-------	-------

4+79			12.75	36.69	35.84
------	--	--	-------	-------	-------

B.M. Stone Wall	5.13	355.32		350.19	
-----------------	------	--------	--	--------	--

3+25			10.92	344.40	36.52
------	--	--	-------	--------	-------

C. 7.86 3' offset

2+99 B.M.			8.62	346.70	
-----------	--	--	------	--------	--

B.M. on Conc. Wall corner 2.4' L. of &

3+00			10.79	344.53	36.64
------	--	--	-------	--------	-------

C. 7.89

1.87

C 11.94

12.76

12.68

F Line

4-29-36  
McCart  
Walker  
Partly Cloudy

Sta

1+14	5.35	64.73	59.38	47.15	C 12.23	
1+18.3		10.70	54.03	47.15	Str. G.	C 5.54 Top Bell 6" pipe spreader (Blue Keel)
1+30.5		9.08	55.65	50.64	Str. G.	C 4.33 Top Bell 6" pipe spreader
1+60.5		7.19	57.54	55.16	Str. G.	C 1.70 " " " spreader
1+14	5.38	64.76	59.38	47.89		
1+18.9		11.89	52.87	47.89		C 4.30 to string grade
1+14	5.72	65.10	59.38	47.15	C 12.23	
1+30.6		9.47	55.63	49.65	Str. G.	To Str. G. C 5.30
2+00	2.92	367.82	364.90	360.12		C 4.78
2+00.5 stake		7.03	360.79	360.20		Str. Gr.
1+60		12.30	355.52	59.09		Top Bell Str. Grade
1+14		8.48	359.34	47.11		C 12.23

"C" Line

5-13-36

3+00	4.58	387.68	383.10	377.12	Top Bell Str. G.	77.79	C 5.98
2+28		11.57		75.44	61.80	76.11	11.57
2+50		11.06		75.95		76.62	11.06
2+75		10.47		76.54		77.21	10.47
3+00		8.89		77.12		77.79	9.89 C 1.0
3+25		7.31		77.70		78.37	9.31 C 2.0

5-13-36

	3.41	38.82	35.41				
MH #39		5.49	33.33	33.30			

5-14-36

Clear & Warm,  
McCarty  
& Walker

"C" Line, Grav. Sewer

Sta	+ 2.82	H.I. 385.92	- 8.78	I/c 383.10	F.L. 377.12	Str. Grade 76.09	Gr. Rod 9.83	C 1.05	From Top Iron Stake
3+00									
2+27			8.78	377.14	75.42	76.09	9.83	C 1.05	From Top Iron Stake
2+50			8.05	377.87	75.96	76.63	9.29	C 1.24	" "
2+75			8.21	377.71	76.57	77.21	8.71	C 0.50	" "
3+00	2.62	85.72		83.10	77.12	77.79		C	
3+00			6.46			77.79	7.93	C 1.47	
3+25			6.33			78.37	7.35	C 1.22	
3+50			5.78			78.95	6.77	C 0.99	
3+50	3.60	87.82		84.22	78.28	78.95	8.87		
3+50			Top Iron S. 7.89				8.87	C 0.98	
3+00			9.52			77.79	10.03	C 0.51	
2+27			10.96			76.09	11.73	C 0.77	
3+00			4.74	83.08				85.72	
								77	
4+00	4.77	90.09		385.32	79.45	80.12	9.97	C 5.87	
3+50			5.86	84.23				5.94	84.22
4+00			9.97	80.12					Red Mark on Iron Stake
			11.20	78.87					Check on end of pipe
			2						

"A" Line

F.L. Top MH

Copy of Moore's Notes  
Book G 180

9+70.35 = 9+69.45	33.18		C 2.23
9+42.35	333.33	✓ 342.0	C 11.30 ✓
9	333.54	✓	C 11.18 ✓
8+50	333.80	✓	C 6.87 ✓
8	334.06		C 7.40 ✓
7+60 M.H. #41 33°10' Lt.	334.27	339.0	C 7.72 ✓
7	34.58		C 13.75 ✓
6+50	34.84		C 10.93 ✓
6	35.10		C 8.16 ✓
5+50	35.36		C 6.86 ✓
5+14.2 MH #42 104°20' Rt.	35.53	345.0	C 12.27 ✓
5		out.	
4+50	35.86		C 12.12 ✓
4	336.12		C 10.10 ✓
3+83.42 M.H. #43 29°17' Lt.	336.20	341.0	C 7.68 ✓
3+50	336.37		C 10.71 ✓
3	336.63		C 9.79 ✓
2+43.78 = M.H. #44 13°57' Rt.	336.92	343.5	C 11.50 ✓
2	337.14		C 9.46 ✓
1+50	337.40		C 8.62 ✓
Eg $\frac{0+98.40}{+51.36}$ = M.H. #45 89°26' Lt.	337.67	345.8	C 7.87 ✓
0+00 Make Con. to exist sewer	337.92		

Clear, Warm 5-18-36  
 C Line Sta + H.I. - Elev. F.L.  
 K McCarty  
 J Walker

3+00	3.84	386.94		383.10		Hub 6' Offset Right.
2+89			7.57	379.37	378.83	Top iron 6" pipe
2+50			8.94	378.00	377.46	" " 6" "
2+27			10.25	376.69	376.15	" " 6" "
2+28			10.92	376.02	375.46	Top 6" Conc. Sewer Pipe
2+20			5.44	381.50		Rim of DMH #50 E. Side
2+21			5.56	381.38		Top Cb. on N. Side
3+50			2.71	384.23		Hub 6' Offset Right (384.22 By Moore.)

ALLOW 0.54 to F.L.  
 ALLOW 0.56 to F.L.

Peg Adjustment Transit.

30° "A" K	4.625	"B" K	5.175	5.175
"B"	4.125	"A"	5.710	5.710
Diff	- .500	Diff	.535	0.018 out

4+00	5.39	390.71		385.32	379.95	6' Offset Hub.
4+50			4.04	386.67	381.99	End of pipe on bell
3+98			10.66	380.05		Str. Gr. Top Bell
4+33			8.44	382.27	380.22	380.89 9.82 C 1.38 = 1'-4 9/16"
4+66			7.84	382.87	380.99	Str. Gr. Top Bell 381.66 9.05 C 1.21 = 1'-2 1/2"
3+50	6.53	395.32		388.79	384.11	C 4.68 - 6' Offset Rt
F.L. Ex. MH.			12.32	383.00		
			8.54	386.78		Ensl Top 6" pipe in Mt View Drive
			9.71	386.21		Exist. Bottom 6" " in Mt View Drive
MH Rim			5.68	389.64		
B.M			5.96	389.36	384.11	389.37 NE. Cor. Copley Ave & Mt. View Drive B.P. in Cb.
4+50			8.66	386.66		6' Offset, Rt.
6+05.5			9.83	385.49		F.L. entering Conc. Exist MH. Copley & Mt. View Drive

Clear Warm  
6" L.I.C.

5-19-36

Mc Carty  
Walker

Sta	+	H.I.	-	Elev.	Flow Grade
High Pressure					
3+50	5.31	389.53		384.22	
3+58			9.29	380.24	
4+06			8.22	381.31	380.57
2+92			10.05	379.48	378.74
4+03 T.P.	7.21	392.52	4.22	385.31	
4+53			5.85	386.67	381.79
4+53			9.61	382.91	
5+01			8.17	84.35	381.86
5+49			7.85		
6+05.2			7.23	385.29	

B.M.	3		3.17	389.35	
3	3.17	392.54		389.37	
3+56			12.30	380.24	79.45
3+58			12.28	80.26	

"A" Line  
0+51 = 0+98 Ahead, 5-19-36  
MH #45 3.08 348.65

2+09			10.71	337.94	37.09
1+25			3.41	345.24	

5-21-36 Clear mild.

MH # 0+98	2.49	348.06		345.57	37.55
1+25			2.83	45.23	37.44
1+49			2.03	46.03	37.34
1+49			2.53	45.53	37.34
1+59			3.91	344.15	37.38
1+75			5.69	342.37	37.23
2+09			10.12	337.94	37.09

Note - Sewer pipe at P.L. near foot of 39th St. <sup>stub</sup> 76  
is 2" Lower than elev. given on profile.

6' offset Hub. Allow C.484  
Str. Grade 0.74  
Top Bell  
Str. Grade

77.94 Top Bell as laid

H.P. Line  
Hub C.4.88 Str. G. 6 Rod.  
Str. Grade 382.53 9.99 C.0.38  
" " " " 8.92 C.0.75  
Nail N. side Str. G. 7.85

Bottom of hole cut in exist. M.H.

380.19 12.35 12.30 Set.  
Nail in N. Side Wall

6' offset C.8.01  
Top Bell End of pipe 1:30 P.M. 5/19  
3' Offset Left.

C.8.02 6' offset Right  
3' Offset Hub. Left.  
" " " " C.8.69  
" " " " C.8.19/  
on top 2" pipe & C=6.77  
C.5.14 3' offset Hub Left.  
End of pipe Top Bell

K McCarty  
Walker

5-21-36

Clear & Mild

	+	H.I	-	Elev	Grade	
3+25	2.63	347.03		344.40	36.52	c. 7.88 3' offset L
Y 3+32			6.10	340.93		Top upright.
Y 3+70			6.36	340.67		Top "
M.H.						
3+81.5 Back						
3+83 Ahead						
3+00			2.50	344.53		3' offset
B.M.	1.10	344.66		343.56		Sta 6+38
Y Top 5+92			7.96	336.70	335.14	(Y only) No upright.
MH #40	1.04	45.67		44.63		c. 11.30 - 10' offset
			9.26		36.41	36.41 07

5-22-36

	0.29	45.01		44.72		
N. Pier			11.14	33.87	33.00	
S Pier			11.03	33.98	.03	
			11.36	33.65	32.91	Top Concrete pipe 8' up from M.H.
	5.55					
	5.55	40.96		35.41		
S. Pier			6.94	34.02	33.15	
N. Pier 9+99			7.05	33.91	33.04	Top Bell Allow 0.87 Top Bell to F.L. 8" C.I. pipe
10+15			7.28	33.68	32.94	Top 8" Concrete Pipe
End C.I. Pipe Sta 10+05			7.34	33.62	32.91	} Raised 0.09 Allow 0.21 Top Pipe to F.L. for 8" C.I. pipe
Sta 10+05			7.25	33.71	33.00	
End C.I. Pipe as raised S			7.25	33.71	33.00	} 0.06 Fall in 10 ft. Allow 0.24 Top pipe to F.L. 8" conc pipe
Top Conc Pipe 10+15			7.28	33.68	32.94	
MH #39 Sta 10+06.95					32.98	



LINE BETWEEN MH #39 & MH #47

5-22-36 Clear & Mild  
T. McCarty  
J. Walker.

STA.	+	14.1	-	Elev	Grade
6" pipe		40.96			
MH #39	0400		7.31	33.65	32.98
0+17			2.25	37.28	36.61
9+00	0.81	21.948 45.53		44.72	
0+17			8.42	37.11	
0+25.2			6.38	39.15	38.48

7.31 C. 0.79  
Gr. Rod = 3.68 C 1.43  
6' offset  
on Bell as laid,  
As set.  
38.51 using Hub Offset 9+69 ET 335.41

T. McCarty  
J. Walker

5-26-36 Cloudy  
Mild.

2+20	1.83	346.040		44.21	
2+09			8.125	337.915	{ 37.07
1+87			8.037	338.003	
1+87			6.94	339.100	
1+75			3.69	342.35	
			5-27-36		
1+86	5.73	347.09		42.36	
			10.10	36.99	36.14
1+64.5			9.99	37.10	36.25
			5-27-36		
1+4+49	4.31	349.88		345.57	37.56
1+25			CO2		37.36
			Grade		37.47

C. 7.20 3' offset  
Top bell as laid  
String Grade Top Bell  
Top Iron Stake C 1.10  
EI 342.36 -3' offset  
End of pipe as laid Top Bell  
9.99 37.10 Red mark on Iron Stake Checked  
Pipe  
Bottom Ditch  
" "

T McCarty  
J Walker

5-22-36

Clear, mild.

79

Sta	+	H.I.	-	Elev.	Top upr.	
4+50	0.44	348.38		347.94		012.00
4+35 Y			1.94	346.44	345.4	Top ground as B. Filled
B.M.	0.35	344.29		343.94		Nail in bottom stump
5+06 Y			3.3	341.0	340.4	Top Ground as B. Filled. 3 1/2' below Top of M.H.
4+77 Y			1.8	342.3	340.0	" " " " " " 2' " Surface
5+30 Y			3.9	340.4	340.0	" " " " " " 1' from Surface <sup>Wat.</sup> 0.5' as B.F.
5+14 M.H. Top			0.36	343.93		W. Rim M.H. #42
3+70 Y						2' from Surface
3+32 Y						2 1/2' " " " "
2+58 Y						1' " " " " 7' from F.L.
2+05 Y						1 1/2' " " " " 4.3' " F.L.
7+14 Y						Schneider Lateral 2' from surface
1-6-36						
M.H. #45	6.30	51.87		45.57	37.54	C. 8.03 38.43 Str Rod 13.44 ✓
1+25 <sup>21</sup>		12.34		41.26	37.4	Top of iron stake
1+49 <sup>22</sup>		13.60		38.27	37.3	String Grade
1+49 <sup>22</sup>		13.70		38.17	37.3	" "
1+49 <sup>22</sup>		12.665				C. 1.035 Top Stake, iron
				45.57		
	2.14	47.71		45.57		
1+			2.47	45.24	45.24	
1+25			9.46	38.25	37.40	Top Bell .02 Low
1+01			9.34	38.37	37.52	

Top Gr 351.7 - 2 = 349.7 = Elev Top Lateral  
 2' Below Surface  
 "A" Line Elev  
 A Y Sta 7+14 ✓ Y 4+35 ✓  
 A Y " " ✓ Y 3+70 ✓ 340.67  
 A Y " 5+92 = Elev 336.70 Y 3+32 ✓ 340.93  
 A Y " 8+00 ✓ Y only Y 2+58 ✓  
 Y Sta 8+71 ✓ 2 Lengths = 6' Y 2+05  
 Y Sta 5+30 ✓ upright Y 1+75 341.35  
 Y Sta 5+06 ✓  
 Y " 4+77 ✓ ✓  
 Y " 14+55 ✓ -1- 3' joint = 3 ft upright  
 337.2 = Elev 0' Below Gr.  
 EI 341.0 Y " 12+31 ✓ -2- 2 1/2 joints = 6 1/2 ft above FL 1 1/2' upright Below  
 Y " 13+36 ✓ 2-2 1/4 = 6 1/2 ft upright

F Y Sta 1+51 = 1-3' joint above Y upright  
 F Y " 1+88 Y only

"C" Line  
 MH 49 47.75' Dist  
 MH 50  
 Portal = 1+93.5  
 2+18.0 = 24.5 = Length of Tunnel.  
 17.8 x 4 x 24.5 =

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of these tables from side or shoulder  
 for any width roadway slope 1:1  
 If ground is nearly level the center line  
 stake is located by the double entry method  
 The number of feet  
 in table in same row and column gives

IMPROVED TABLES  
AND  
INFORMATION

TABLE No. 2.

To find Tangent and External for curves of  
 any other degree, divide by degree of curve and  
 add correction found in column of correction.  
 Degree of curve will give in 1 row below  
 by dividing tangent (or external) by degree of  
 given tangent (or external).  
 The distance from a point on the tangent to  
 the curve is very nearly the square of the tangent  
 length divided by twice the radius.

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

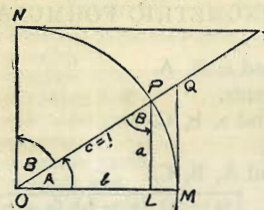


TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

Chas. Walker

7150 - EL CAJON

Box 535 Rente

Thickness of 6" C.I. Pipe = 0.045

02  
Req Adjustment Transit 4-30-36

"A"  
a = 5.09      c = 5.14  
b = 4.68      d = 5.51  
    0.41           0.39

200/100  
4.7  
7.79  
11.49  
11.84  
3.09

Leach Stunglog 4001-3324-54

Lateral - Schneider 15' - 4" pipe