G-189

FIELD BOOK

No 385[illegible]

G-189

Fairmont 44+

1st Curve 50+53.17 N
50+36.69 S

52+69.93 B.C.

55+03.65 E.C.

59+53.36 B.C.

MADE IN U.S.A.

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK.	Left and Right Hand Page the same as Left Hand Page of this Book.
No. 382 FIELD BOOK.	Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.
No. 384 MINING TRANSIT BOOK.	Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
No. 385 FIELD BOOK.	Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book,) which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803 **CHICAGO**

La Jolla Cove 6-21-38

E/y steps

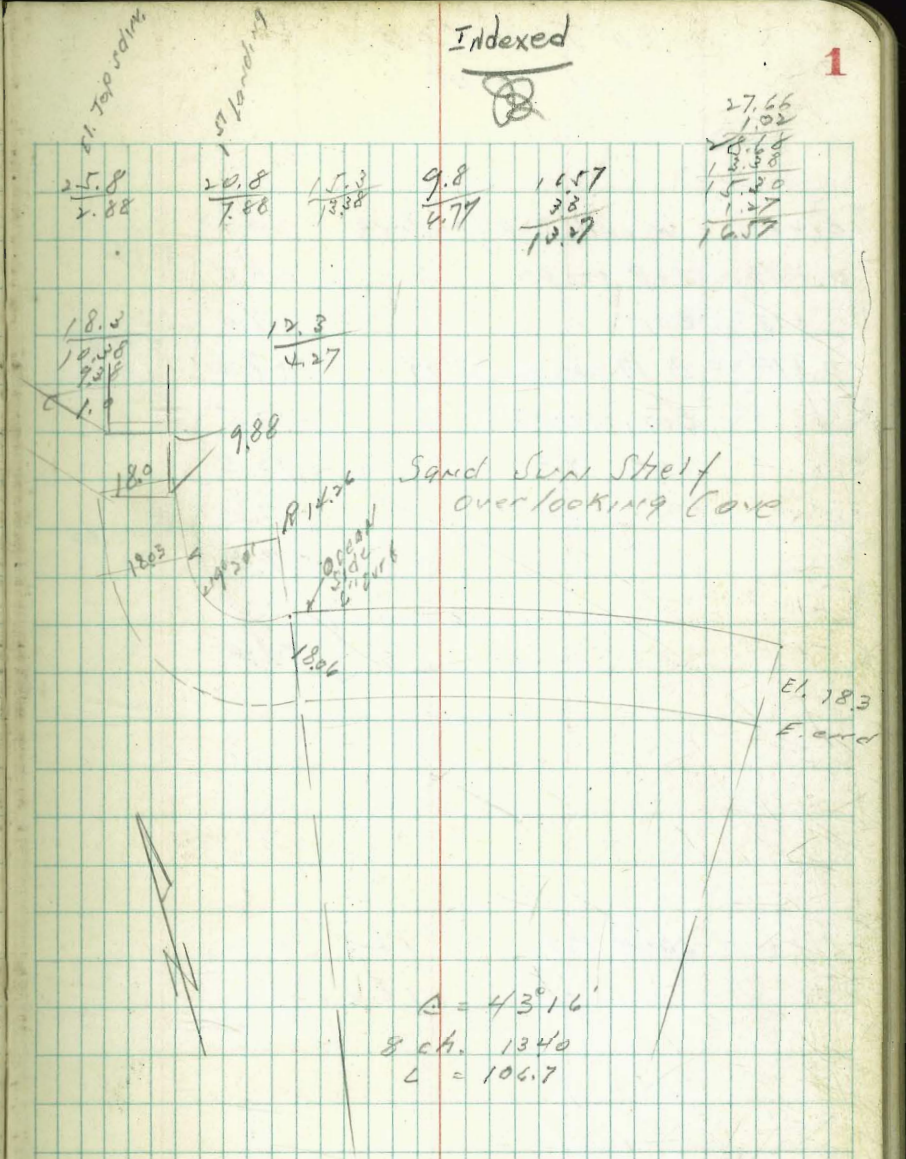
E/y stairs

0+00 =	Top sdwk.	25.8
0+09 =	Landing	20.8
0+15	"	20.8
0+21	"	20.8
0+31 =	Steps bot.	15.8 ✓
0+35	Landing	15.8 ✓
0+45 =	steps bot.	10.3 ✓
0+49	Landing	10.3 ✓
0+61	Steps bot.	3.8
0+64	Landing	3.8

Top steps to sand beach 20.8
+04 18.3

Indexed

1



La Jolla Cove.
Wly steps

0 + 00	= W. end Top Landing	24.0	} F 1.0
0 + 02	Top steps	24.0	
0 + 13	Bot. "	18.0	} c 4.96
0 + 14	= △ Pt. inside 37°29'	18.0	
	Bot. steps	12.5	} c 8.02
	Top step	12.5	
		7.0	} c 13.80
		7.0	
		7.0	
	} ~1.0		

3' 15 + 10 4 10

Ely end	sand Pit	18.3
Wly "	" "	18.0

28.68
5.17
23.51 nail T.P. Post.

23.51
.21
23.72
11.82
T.P. spike 11.90
1.03
12.93

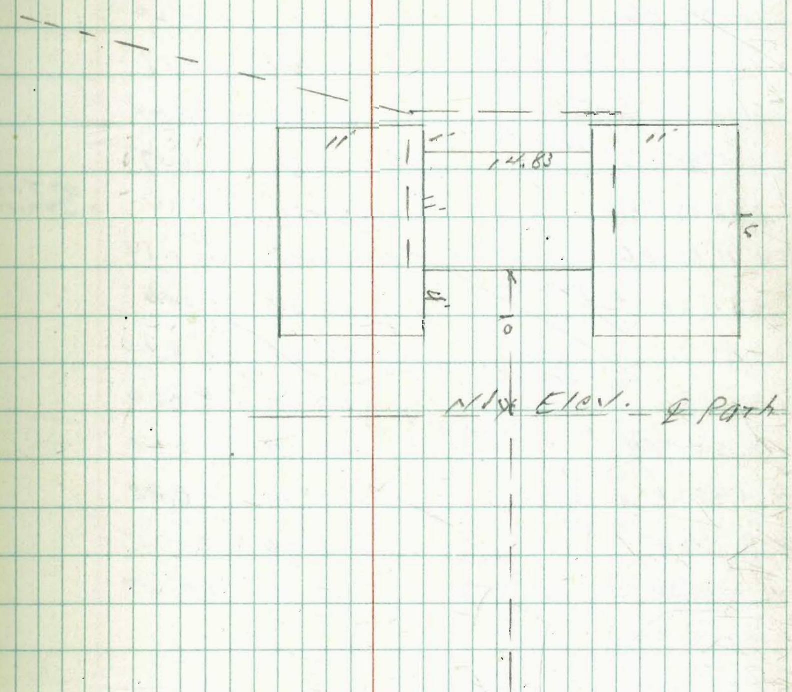
La Jolla Cove Conf. Sta | B.M.

B.M. B.P. in E cb Coast Blvd 5' N of F.H.

					B.M.
					27.66
					3.28
					30.94
					5.72
Fl. el.			27.25		25.22
					4.24
					29.46

			F.L.	CUTS
0+00	Ex. M.H. #92		24.23 ✓	O.K.
0+00	"	"	24.50 ✓	3.56
+28			24.73 ✓	1.69
+64			25.10	0.67
+92.4 = Conf. Sta.			25.25	0.58

Indexed



La Jolla Cove

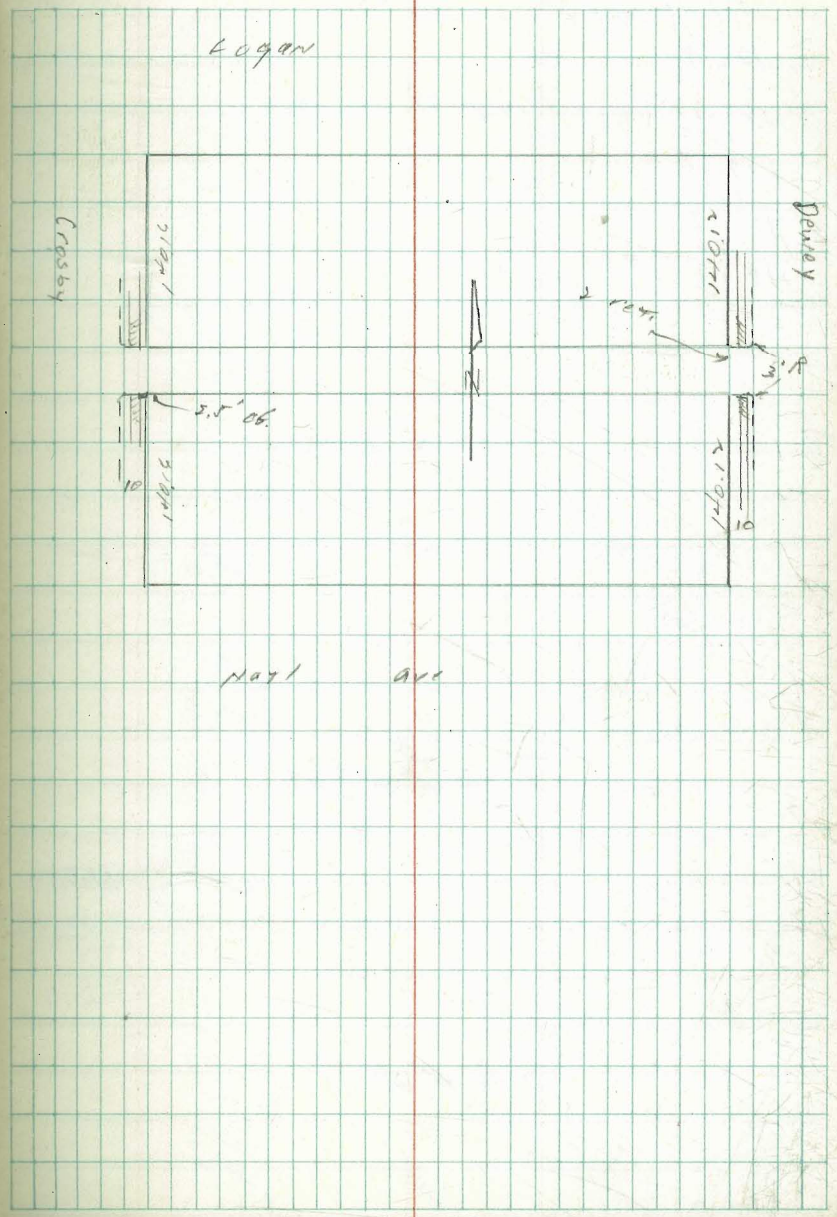
Grades = F.L. of Rock Gutter.
Align. on 3' offset to Ocean face of wall

		F.L.	CUTS	
00 =	Cent. Wall = El. 25.97	24.0	+ 1.90	23.51
				4.48
+ 48.2		23.50	− 0.25	= 7.99
+ 96.4 B.C.		23.0	+ 0.24	
1 + 13.57	Δ = 58° 40' Rt	22.87	+ 0.07	
+ 30.74	R = 67 T = 37.70	22.75	+ 0.24	
+ 47.91	L = 68.68	22.62	+ 0.37	
1 + 65.08 E.C.		22.50	+ 0.49	= 97 TO P STAIRS
1 + 71.85 B.C.		22.45	+ 0.34	
+ 82.20	Δ 19° 46' Rt R 120	22.39	+ 0.46	
+ 92.55	T 20.90 L 41.40	22.28	+ 0.40	
2 + 02.90		22.19	+ 0.50	
2 + 13.25 P.R.C.		22.10	+ 0.68	
2 + 37.60	Δ 124° 00' R 45	21.90	+ 0.88	
2 + 61.95		21.20	+ 0.75	
2 + 86.30	end wall here	20.40	+ 0.27	
2 + 10.65 E.C.				

Indexed

Alley Return Const.

7-27-38



Plum St. Paving
Browning to Dumas

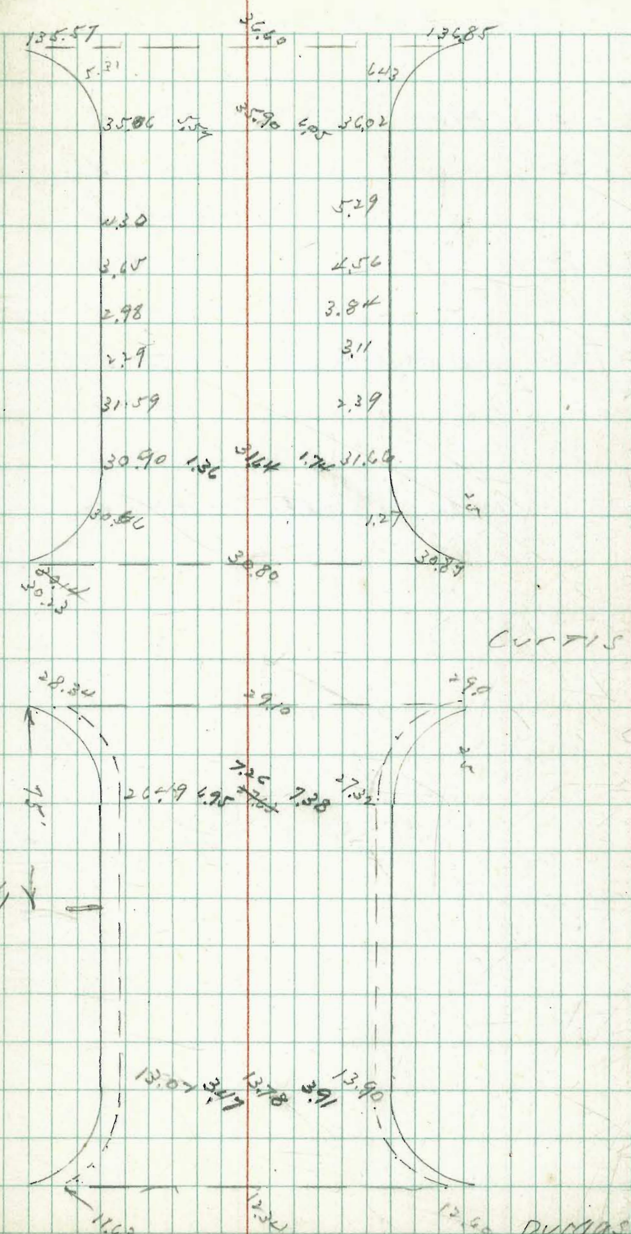
Moore
7-12-38

131.34 S.W.B.P. Curtis + Plum.

131.34
7.62
138.96
12.64
126.32
3.36
129.68
12.40
117.28
1.76
119.04

117.26

Indexed



Sew. Lat #1

117.70
11.98
5.78
C 6.2

W.P.H.
7-28-38

Redondo Ct. Sdw. Const.

-0.32
4.30
3.98

00 = Ely Blvd.		-0.32 ✓
+50		-0.41 ✓
1		-0.49 ✓
+50		-0.58 ✓
2		-0.67 ✓
+17.02	WL Bayside Lane	-0.70 ✓
16.15 ↑		
00 ↓	EL " "	-0.70 ✓
		-0.55 ✓
	WL " Walk	-0.40 ✓

Indexed

Private Contract

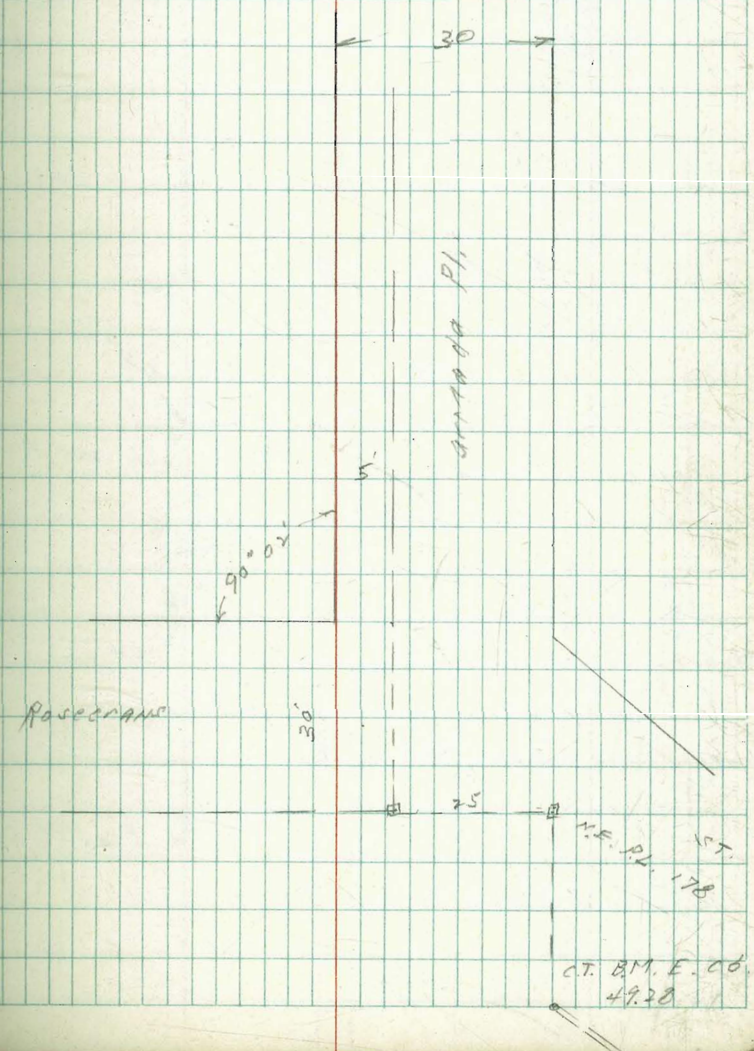
Grades on Armada Pl. 8-3-38

		S		N	
0+00 N.E. Rosecrans		52.10	C 1.1		C 4.3
0+20		57.34	C 7.1		C 7.8
0+40		62.58	C 3.8		C 4.7
0+75		71.75	F 0.7		C 2.0

+26.2 %

Indexed

49.28
11.83
61.11
0.08
61.03
12.34
73.37

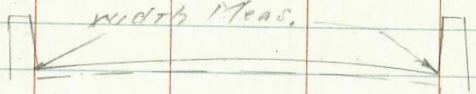


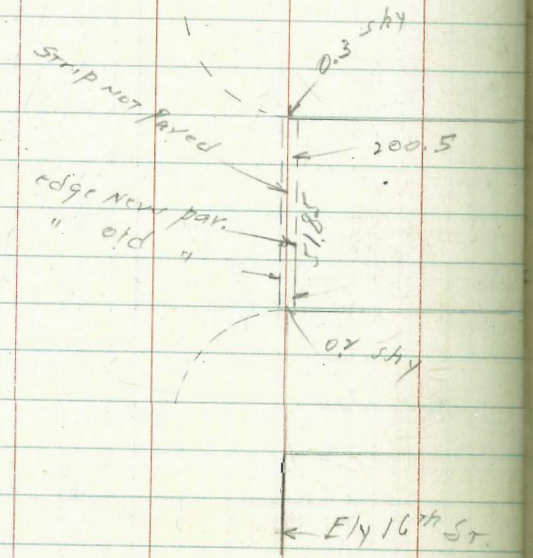
Moore 8-10-38.

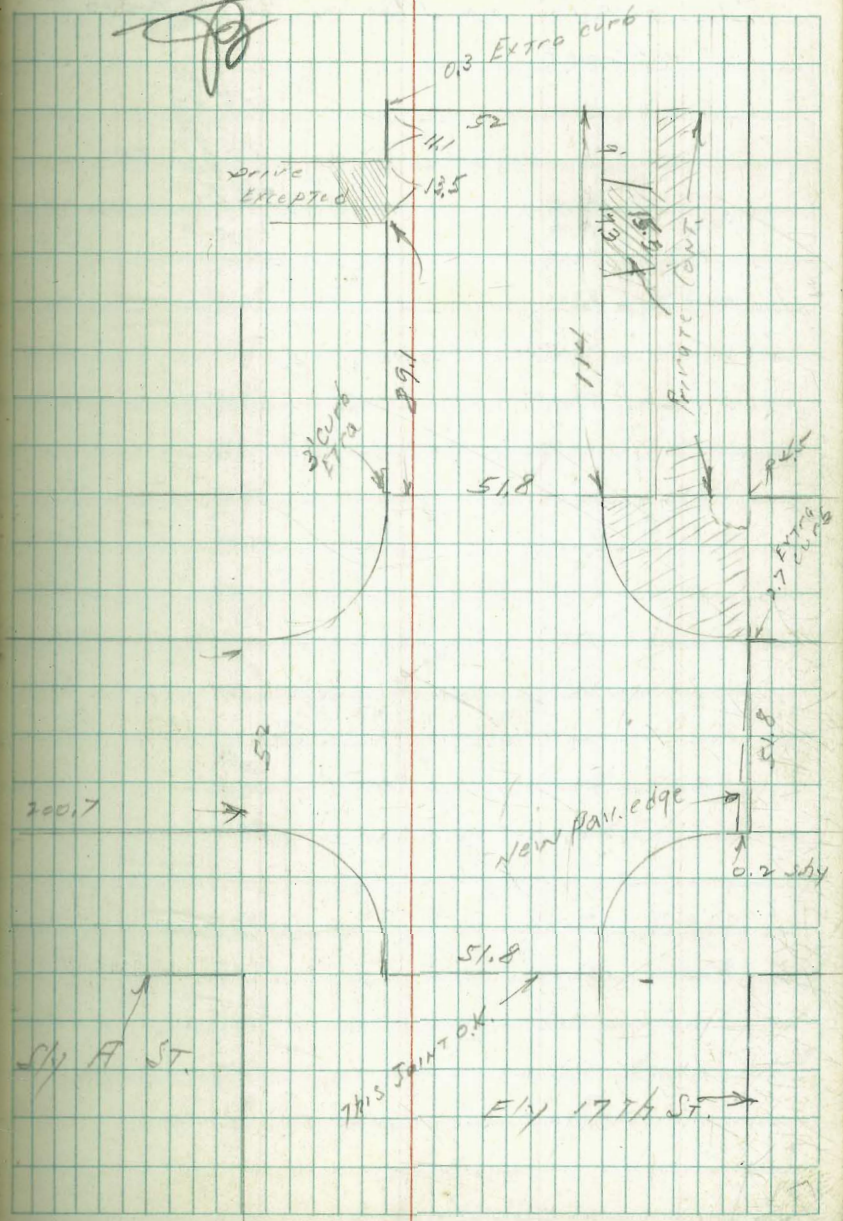
9

Indexed

Slope Meas. of Imprints at 17th & A Sts.







Moore
Sisson
9-28-38

Pav. Grades on Marcey 28th to 500 E

2" oil rock

66.02
8.38
74.40
1.53
72.87 T.P.
3.94
76.81

66.02 N.W. B.P. 28th & Logan

Indexed

Marcey

29th St
69.30
69.80 ℄ 6+00

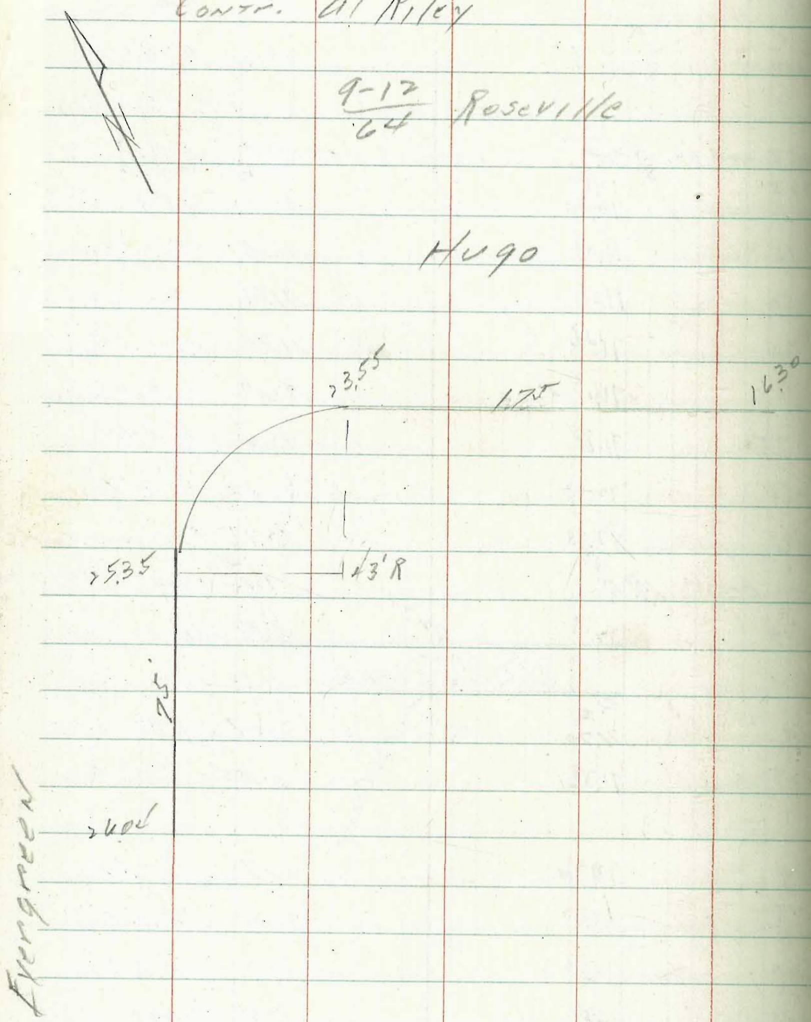
Station		West	East	
5+00	70.84	70.5 C 0.75	70.22	C 0.92
4+55 end cb.	71.16	70.49	70.64	C 0.77
+25		70.70	70.94	C 0.67
✓		70.90	71.15	0.0
+75		71.09	71.38	F 0.42
+50		71.27	71.61	F 0.50
+25		71.46	71.84	F 0.55
3		71.65 ✓	72.07	F 0.60
+75		71.84	72.30	F 0.40
+50		72.02	72.53	C 0.17
+25		72.21	72.77	F 0.11 no curb
2+00 Break	73.03	72.40	73.0	F 0.14 on South
1+79		72.19	72.87	TP
1+65			72.82	
1+50		71.2 / 71.70	72.47	F 0.20
1+25		71.33	71.88	C 0.13
1+00		70.96	71.27	C 0.67
+75		70.60	70.68	C 0.78
+50		70.23	70.10	C 1.0
+25		69.86	69.50 Break	C 1.37
0+00	70.02	69.50	69.10	

72.74
Cem. cross walk
72.64
0.26 Crown

28th St.

Curb Stakes
S. Cor. of Hugo + Evergreen
Permit # 499
Contr. Al Riley

9-12
64 Roseville



Evergreen + Garrison
SWBP

Moore
9-29-38.

Indexed

30.10
1.78
31.88
6.41
25.47
2.82
28.29

Return
5
13.5

16.		P.C.		
26.04	25.58	25.35	25.15	24.90
5.84	6.30	6.53	3.14	3.39
			2.46	2.90
			C 0.68	C 0.49

		P.C.		
24.50	24.10	23.55	22.52	20.45
3.79	4.19	4.74	5.77	7.82
3.72	0.0	4.67	5.10	6.89
C 0.07		C 0.07	C 0.67	C 0.93

18.38	16.30
9.91	11.99
9.01	10.82
C 0.90	C 1.17

Curb checked O.K. 10-21-38.

Cont. Rep. promises to remove dirt in gutter & St.

Alley Pav. Blk 8 C.N. Ad. #2

Griffith Co.

Station		W		E	
00 = S.L. Dwight		336.40 ✓		335.10	✓
+20	BK.	39.55	C 2.0	39.25	C 2.12
+30	"	41.37	C 1.44	41.07	C 0.83
+40	"	42.69	C 1.27	42.39	F 0.52
+50	"	43.50	C 0.05	43.20	F 1.12
+60	"	43.80	C 0.17	43.50	F 1.42
1 +00	"	44.0	C 1.0	43.70	0.0
+20	"	44.06	C 1.0	43.76	C 1.0
+40	"	44.03	F 0.02	43.73	C 1.0
+60	"	43.93	C 0.34	43.63	F 0.71
1 +80	"	43.74	C 0.21	43.44	C 1.0
2 +30		43.17	C 2.0	42.87	C 1.0
2 +80	"	42.60	F 0.06	42.30	C 1.0
3		42.42	C 0.15	42.12	C 0.25
+50		41.97	C 0.38	41.67	C 1.0
4		41.53	C 0.12	41.23	F 0.21
+50		41.08	C 0.18	40.78	F 0.26
5		40.64	F 0.24	40.34	F 0.50
+20	"	40.46	F 0.30	40.16	F 0.45
+40	"	40.18	C 0.22	39.89	F 0.46
+60	"	39.69	C 0.22	39.44	F 0.11
+80	"	39.0	C 0.97	38.81	C 0.81

332.00
10.67
334.67
0.94
333.73
11.90
345.63
1.59
344.04
4.34
348.40
8.17
340.23
4.17
344.40

NWBP Dwight Charmoune

Moore
10-3-38-

Indexed

W. Ser.		Sewer Lat. El.				Line Cuts
✓ 0+30	E.L.	✓ 0+50	E.L.	#1	335.38	C 4.70
✓ 0+80	E.L.	✓ 3+90	E.L.	#2	36.34	C 4.66
✓ 3+70	E.L.	✓ 4+15	W.L.	#5	36.41	C 5.20
✓ 3+95	W.L.	✓ 4+50	E.L.	#3	35.80	4.72
✓ 4+20	E.L.	✓ 5+50	E.L.	#4	34.67	4.88
✓ 4+70	E.L.					
✓ 5+20	E.L.					
✓ 5+70	E.L.					

6+01.36 338.11 ✓ Pav 337.99 - Pav

Pine St. Pav. 2" Oil Rock St. Dept.
Arista to Conde

		S		N	
00 EL Conde		247.40	F 0.40	47.90	C 0.40
+20		47.65	C 0.30	48.15	C 0.35
+40		47.70	C 0.40	48.20	C 0.43
+60		47.50	C 0.51	48.0	C 0.56
+80		47.10	C 0.40	47.60	C 0.60
1+00		46.45	C 0.20	46.95	C 0.40
+20		45.70	C 0.05	46.20	F 0.10
+40		44.70	C 0.04	45.20	F 0.16
+60		43.80	C 0.13	44.30	C 0.25
+80		43.10	C 0.27	43.60	C 0.34
2+00		42.50	0.0	43.90	C 0.70
+20		42.65	C 0.47	43.15	C 0.64
+40		42.85	C 0.45	43.35	C 0.48
+70		43.18	C 0.40	43.82	C 0.22
3+00 WL Arista		43.50	C 0.42	44.30	C 0.40
3+50 EL "		45.50 ✓		45.50 ✓	

Curve Grades

00 = EL Conde B.C.		247.40 ✓		247.90 ✓	
1		46.20	F 0.35	47.20	C 0.10
2		44.20	C 0.20	45.20	0.0
3		42.70	0.0	43.20	F 0.30
4				41.06	0.0
5 = E.C. on Pav.					

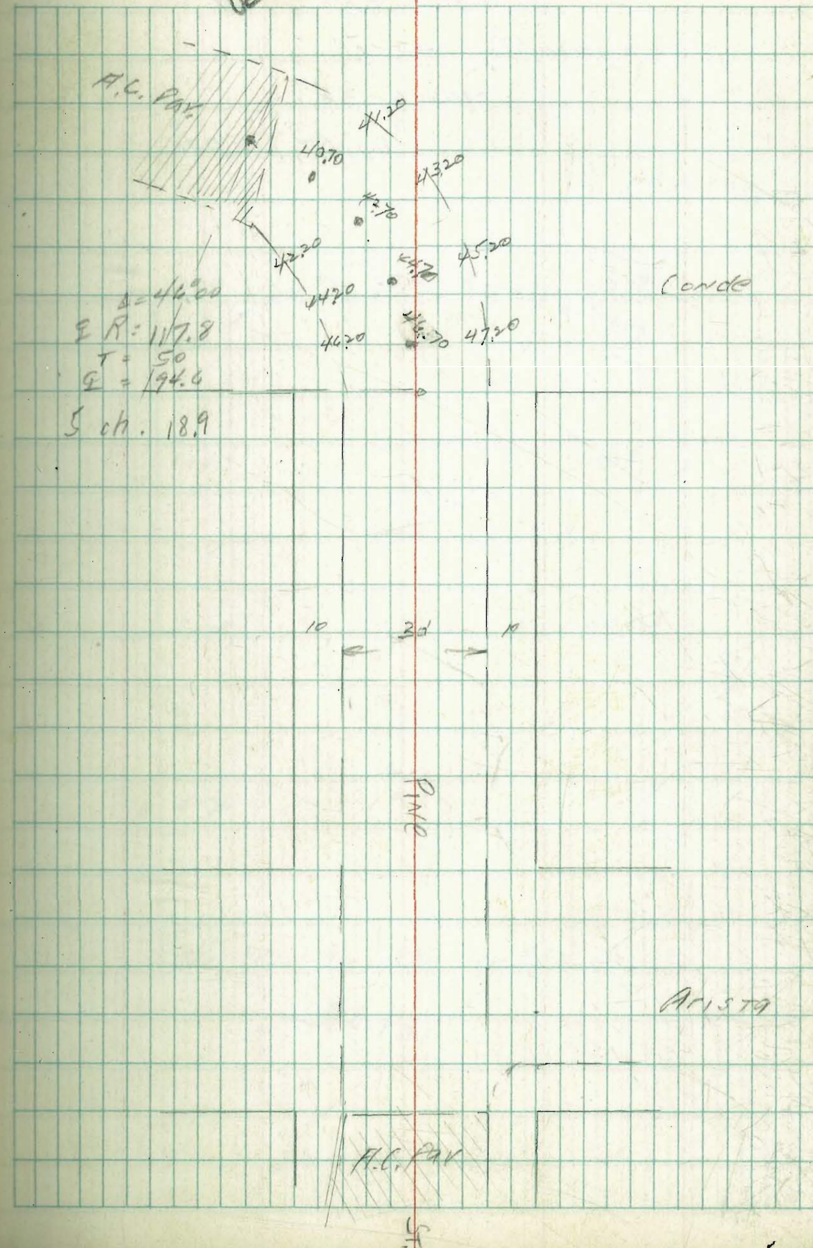
5 Parts 18.90

246.83
3.20
250.03

S.E. Mon. Pine & Conde.

Moore
10-5-38

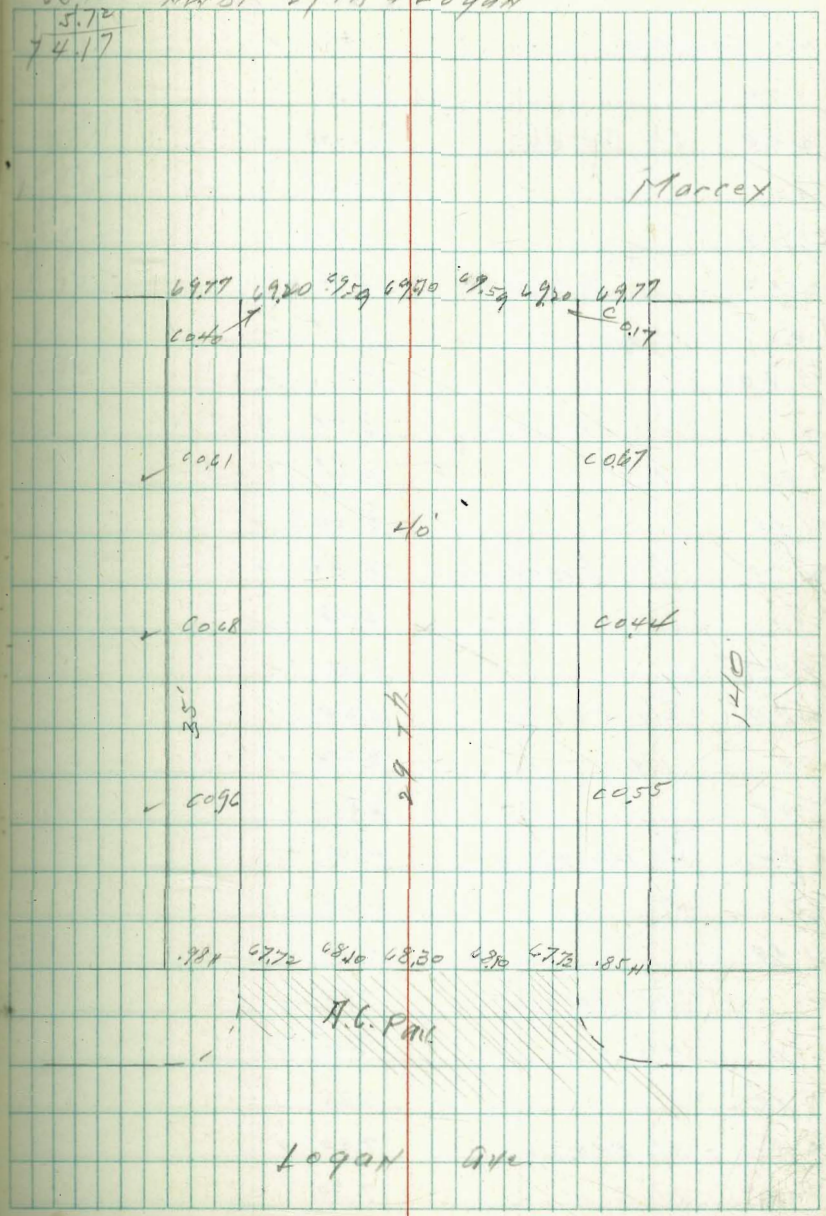
Indexed



Indexed

Pav. Grades on 29th
Logan to 140' N.
10-6-38.
by ST. Dept.

6845 NW SP 29th & Logan
5.72
4.17



W.L. Grades on Rosecrans St.

10-13-38.

Carleton N/y W.L.

N/y Carleton		13.06 ✓
1 +0		12.29 ✓
2 +0	S/y Dickens	10.97 ✓
00	N/y "	9.88 ✓
1 +0		8.50 ✓
2 +0	S/y Emerson	7.12 ✓
00	N/y "	5.91 ✓
1 +00		4.81 ✓
2	S/y Fenelon	3.48 C 1.9
00	N/y "	3.21 C 1.8
1 +0		3.00 ✓
2 +0	S/y Garrison	2.84 ✓
00	N/y "	3.12 ✓
1 +0		3.31 ✓
2 +0	S/y Hugo	3.50 ✓
00	N/y "	3.67 ✓
1 +0		3.81 ✓
2 +0	S/y Ingelow	4.0 ✓
00	N/y "	4.24 ✓
1 +0		4.76 ✓
2	S/y Jarvis	5.87 ✓
00	N/y "	5.85 ✓
1 +0		6.56 ✓
2 +0	S/y Keats	7.20 ✓
00	N/y "	7.90

Indexed

15

9.92 BM Rosecrans

6.43
14.35
8.46
5.91
3.10
9.01
4.74
3.27
5.63
1.90
6.30
4.56
7.40
13.96

Rosecrans St.

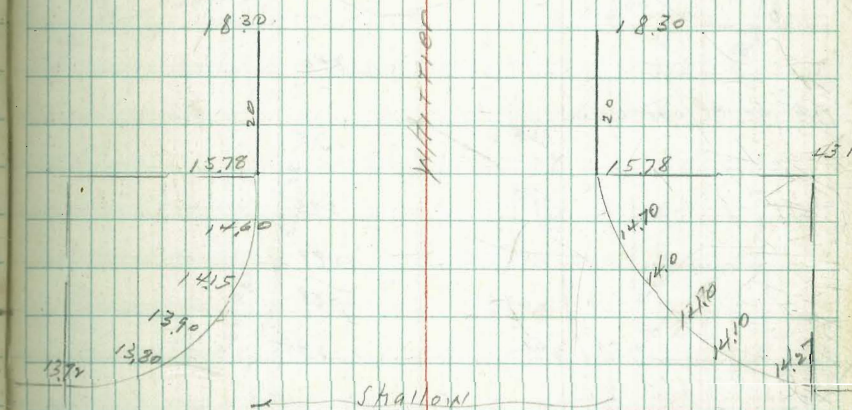
			W.L.	
1+0			8.53	✓
2+0	S'ly Lowell		9.15	–
00	N'ly "		9.63	✓
1+0			9.90	✓
2+0	S'ly Macaulay		10.56	✓
00	N'ly "		10.67	✓
1+0			10.0	✓
2+0	S'ly Newell		9.36	✓
00	N'ly "		8.66	✓
1+0			8.00	✓
2+0	S'ly Oliphant		7.53	✓
00	N'ly "		7.35	✓
1+0			7.10	✓
2+0	S'ly Poe		6.86	✓
00	N'ly "		6.63	✓
1+0			6.46	✓
2+0	S'ly Quimby		6.26	✓
00	N'ly "		6.10	✓
1+0			5.94	⊘ 1.0
2+0	S'ly Russell		5.83	✓
00	N'ly "		5.97	✓
1+0			5.23	✓
2+0	S'ly Sterne		5.16	✓
00	N'ly "		5.40	✓
1+0			6.08	✓
2+0	S'ly Tennyson		7.36	✓

13.96
3.47
10.49
2.26
12.75
6.18
6.57
3.70
10.27
5.83
4.44
6.22
10.66
5.35
5.31 = 5.23 7' Mon Rosecrans + Russell
3.63
8.86

Rosecrans St.

00	Nly Tennyson	8.37	
0+50		9.34	
1+0	"	10.35	
2	Sly Udall	12.36	
00	Nly "	13.16	C.1.6
0+25		12.90	C 2.1
1+0		13.17	C 2.7
1+75		13.34	C 3.3
2	Sly Voltaire	14.07	C 2.5
00	Nly "	14.20	C 0.5
0+25		13.53	
1+0		13.65	
1+75		13.78	
2+0	Sly Whittier	13.88	
00	Nly "	14.42	
0+25		14.84	
1+0		16.15	
1+50		17.40	
2	Sly Xenophon	18.26	

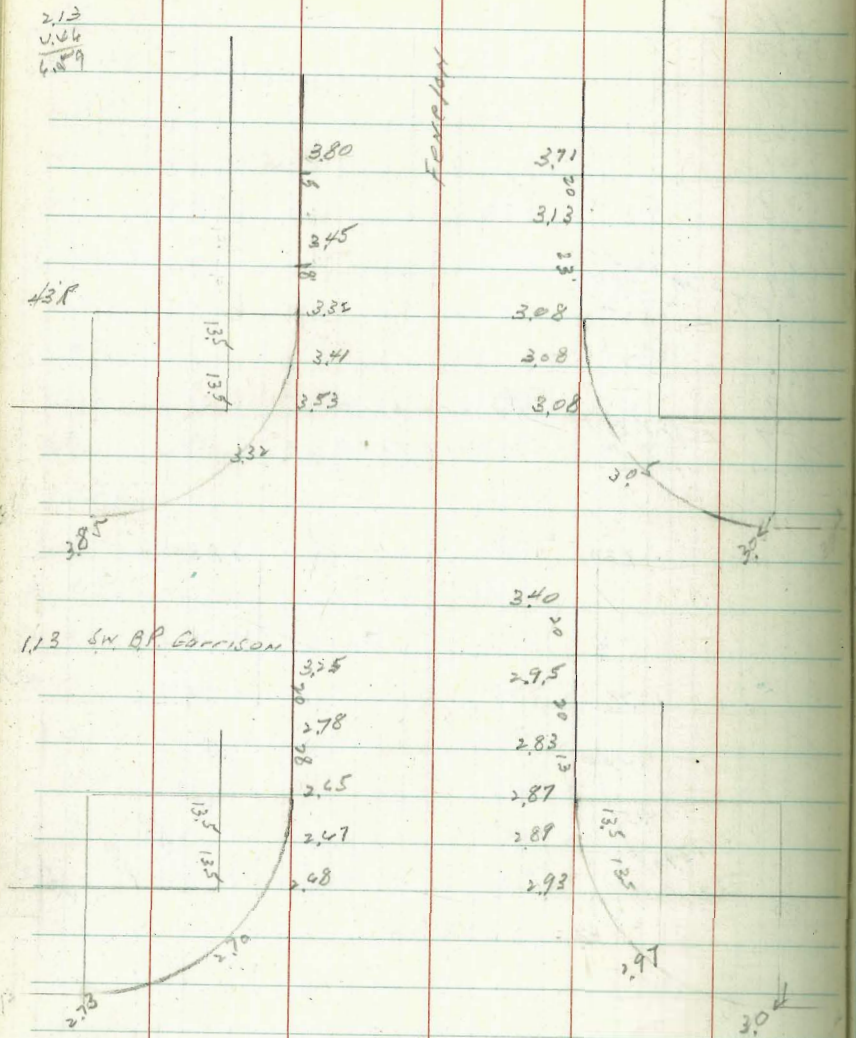
8.84 π
3.84
5.00
11.68
16.68
1.41
15.27
3.57
18.84
6.39
12.45 T.P. → 12.45
5.80
18.25
5.81
18.26
5.49
12.77 NW BP Rosecrans Whittier



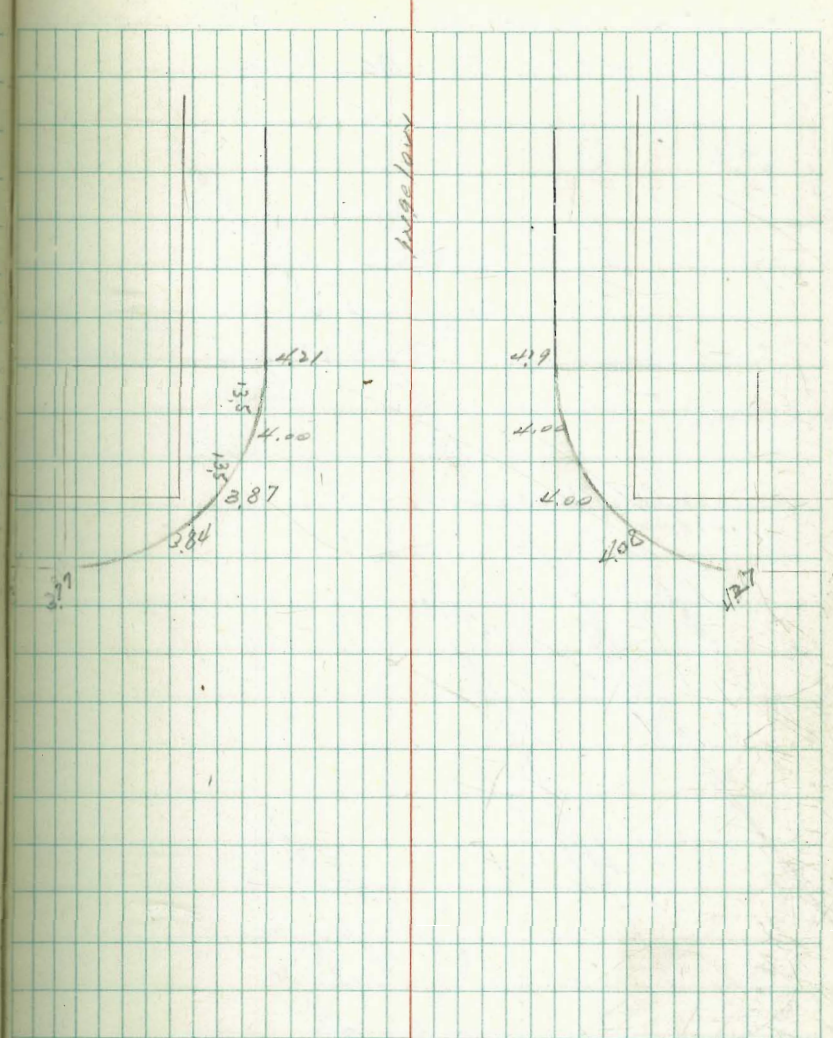
Rosecrans

Rosecrans St.

7' Mon. Fenelon



1.13 SW BP Garrison



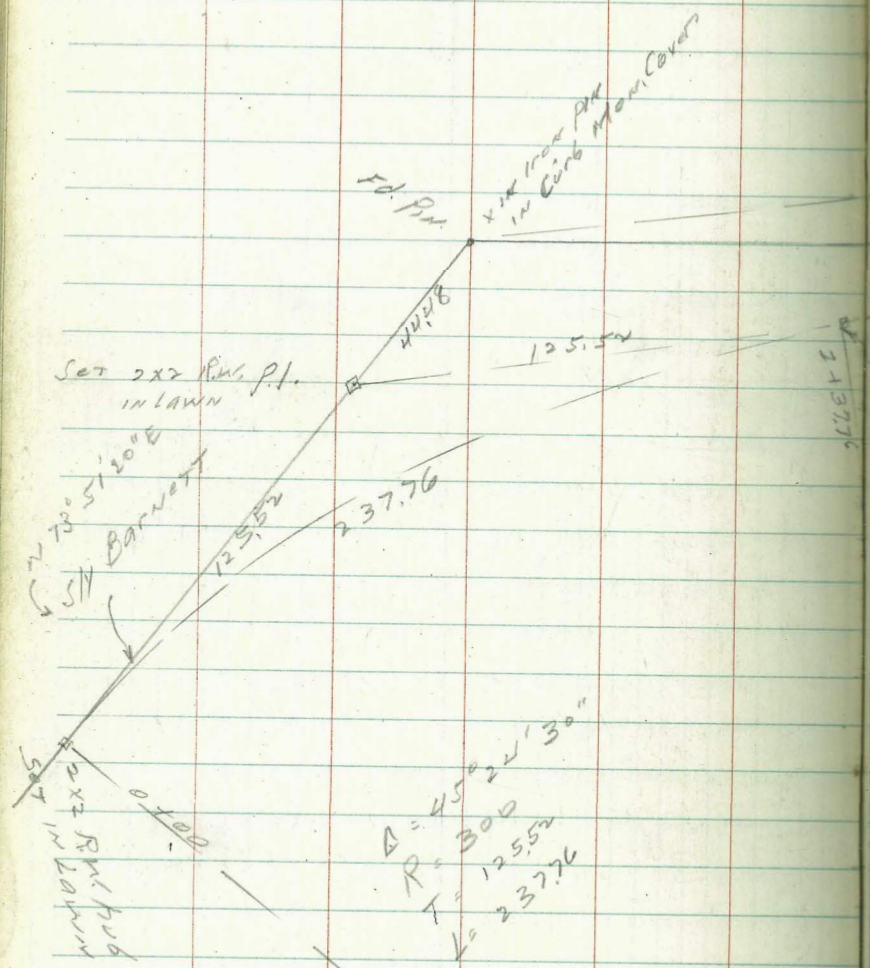
Indexed

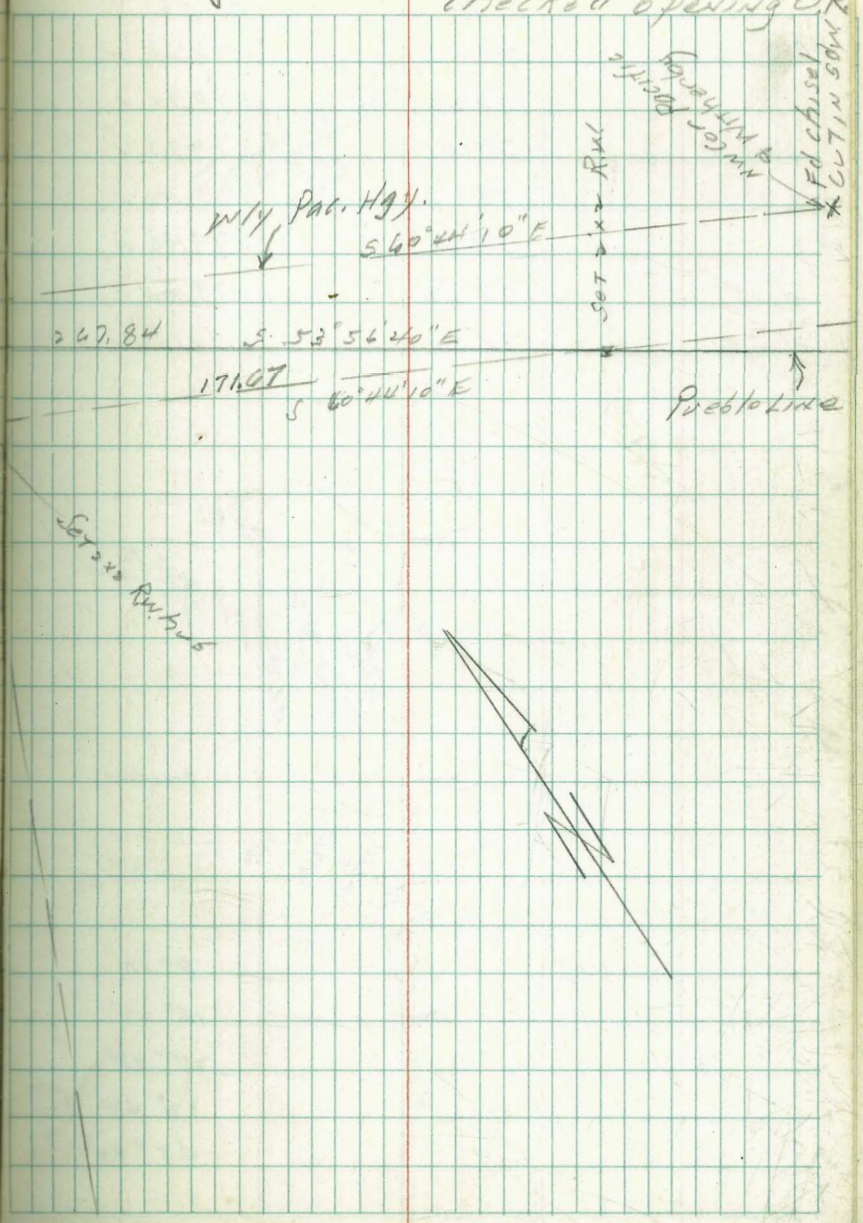
Moore
10-19-86

19

checked opening OK

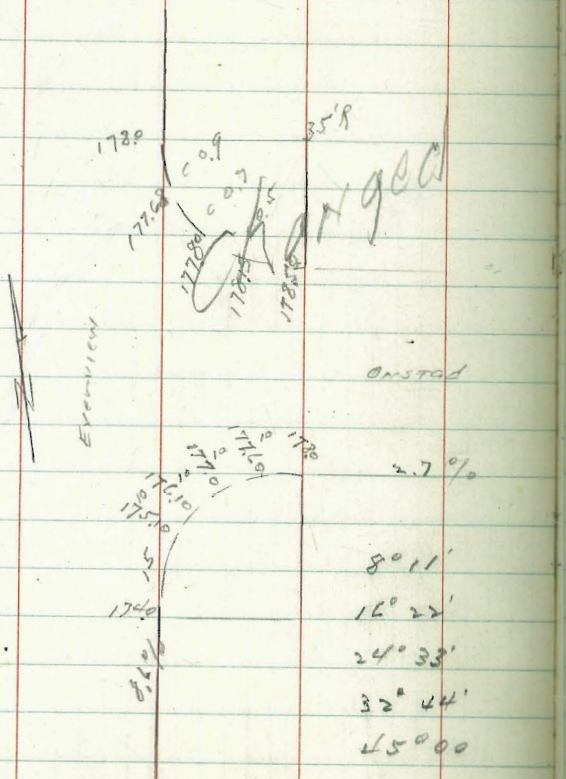
Prop. Opening at SW'ly Cor.
Barnett + Pac. Hgy.





ONSTAD ST.
MONITOR to EVERVIEW

	S c6	N c6
P.C. 00	178.20	178.20 ✓
+25	178.80	178.90 ✓
+50	179.10	179.30 ✓
+75	179.20	179.50 ✓
	179.0	179.40 ✓
+25	178.60	179.05 ✓
+50	178.0	178.50 ✓ c ℄



177.64 B.P. Porch NW Cor
5.30
182.94
ONSTAD
EVERVIEW

Enlarged

Everview Rd.
Onstad to Plainview

				E c6	
P.C. E		177.50	+0.05	178.0	C 1.0
3 Points	1° 53.02	178.53	+0.15	179.03	C 0.6
25.47	1° 46.03	179.56	+0.44	180.06	C 0.55
P.V.C.	2° 39.09	180.60	+0.18	181.10	C 0.57
1	3° 20.73	181.30		181.80	C 0.19
2	4° 02.37	181.90	F 0.10	182.40	
3 8-20	4° 44.0	182.30		182.80	
4	5° 25.63	182.50		183.0	
5	6° 07.25	182.50		183.0	
6	6° 48.87	182.30		182.80	C 0.22
7	7° 30.49			182.50	C 0.2
8	8° 12.13			181.80	F 0.13
27.91	9° 10.21			180.90	F 0.40
2-1.5	9° 45.0			180.55	F 0.83
E.C.	10° 19.0			180.20	F 0.8
1				180.0	F 0.87
2 6-25				180.0	
3				180.40	
4				181.20	C 0.38
5				182.20	
6 P.C. Plainview				183.90	

Inland

182.94
1.15
181.79
5.36
187.15

177.64
9.58
187.22
4.62
182.60 T.P. STAKE
17.5
195.1

177.64
4.06
181.70

177.64
9.72
187.36

Plainview Rd.
Everview to Monitor.

				Sc6	
P.C.				183.90	
	15° 00			~~187.20~~ 186.80	
	30° 00			~~190.10~~ 189.55	
EC 300	45° 00			~~192.70~~ ✓ 191.70	
+10				~~193.20~~ ✓ 192.30	
+30				~~194.10~~ ✓ 193.35	
+50				~~194.95~~ ✓ 194.20	
+70				~~195.60~~ ✓ 194.90	
+90				~~196.05~~ ✓ 195.43	
1 +25	℄ P.C. Monitor			~~196.80~~ ✓ 196.14	
Return				~~197.0~~ ✓ 196.40	
4 Parts				~~197.10~~ ✓ 196.65	
	EC	"		~~197.10~~ ✓ 196.90	F 0.6
				197.0 ✓	F 1.0

Indexed
JB

187.36
1.67
~~185.69~~
13.13
~~198.82~~
2.78
~~196.04~~
5.35
201.39

200.52 ⊼

187.22 ⊼

195.1 ⊼

BC						EC.
3.90	5.35	6.80	8.18	9.55	0.63	1.70
11.22 ✓	9.77 ✓	8.32 ✓	6.94	5.57	4.49	3.42 ✓
			6.57	5.27	4.04	
			6.37	6.30	6.45	

Moore
10-18-38

Crown Pt. Sewer Const.
Blk 14 & 15

0+00 = D.M.H. #4		11.66 ~~11.41~~ ✓		EXISTING
+25 = S/y La Mancha		11.76	c 8.00	
+44 B.C.		11.84	c 8.72	
+82.23	Δ = 17°45' Rt.	12.00	c 8.17	
1 +20.46	R = 617	12.14	c 7.60	
+58.69	L = 191.15	12.32	c 7.00	
+96.92		12.48	c 6.82	
2 +35.15 E.C.		12.64	c 6.00	
+50		12.70	c 5.54	
2 +91.80 = M.H. #5		12.87	c 5.00	
3		12.91	c 4.84	
+50	0.417%	13.12	4.24	
4		13.33	3.75	
+50		13.53	3.13	
5		13.74	2.93	
+50		13.95	2.03	
5 +83.6 = M.H. #6		14.09	3.60	
6		14.16	3.59	
+50		14.37	4.21	
7		14.58	5.15	
+50		14.78	6.10	
8		15.00	6.32	
+50 Ex. Stub end		15.21		

Indexed

Note!
℄ Sewer 3' W'ly of ℄ of 10' E-ment.

BM nail Pole
21.32
1.62
22.94
5.19
17.75
7.74
25.49

	℄ LA CIMA		15.32		
8+75.4	= M.H. #7		~~14.97~~		EXISTING
9+00.4			15.60 ✓	STUB	end
9+11	B.C.		15.70	C 6.88	
9+31.57		Δ = 7°07' Rt.	15.92	C 7.34	
9+52.14		R = 497'	16.14	C 7.11	
9+72.77	E.C.	L = 61.72	16.36	C 7.10	
10			16.65	C 7.37	
+35	beg. TUNNEL		16.92	C 7.44	
+63			17.32	OUT	
11	end "		17.72	C 7.60	
+46	M.H. #8		18.21 ✓	C 7.87	
12			18.79	C 8.40	
+50			19.32	C 8.43	
13			19.86	C 8.78	
+50			20.41	C 8.94	
+91.6	end STUB		20.87 ✓	STUB	end
14+16.6	M.H. #9		~~21.10~~ 21.08 ✓		EXISTING

B.M. nail pole 22.61 ✓
Bolt

B.M. nail pole 29.21
3.62
25.43

.15 dip Alley Paving Blk 4 Wilshire Pl. Moore 10-28-38 by V.R. Dennis, Cont.

Indexed

		W		E	
00 = N E1 Cajon		364.13	363.79	363.86	
0+20	C 1.06	64.05	3.74	63.92	C 0.83
0+40	Break C 1.34	63.98	63.78	63.98	C 0.92
+70	C 0.65	64.04	3.85		C 1.31
1	C 1.0	64.10	3.91		C 0.62
+50	C 1.0	64.20	4.02		C 1.0
2	C 0.22	64.30	4.12		C 1.0
+50	C 1.0	64.40	4.22		C 0.12
3	C 1.0	64.50	4.33		C 0.51
+50	F 0.33	64.60	4.44		F 0.06
4	F 0.10	64.70	4.54		F 0.12
+30	C 0.01	64.76	4.60		F 0.03
4+60	Break C 0.11	64.82	64.67	64.82	F 0.02
5	C 0.53	64.72	4.58	64.72	C 0.02
+50	C 2.0	64.63	4.46	64.60	C 2.0
6	C 1.0	64.53	4.35	64.47	C 0.67
+07 SL Meade		64.51	64.33	64.44	

Sewer Lat.				Water	
0+10	W.L.	#3	359.09 / C 5.61	0+30	W.L.
2+60	E.L.	#2	359.42 / C 5.30	2+80	E.L.
3+15	E.L.	#1	359.53 / C 5.30	3+30	E.L.

364.44 NW BP 42nd Meade

364.44
5.14
369.80
5.06
364.74
4.63
369.37
4.76
364.61
4.53
369.14
4.87
364.27
4.87
369.14

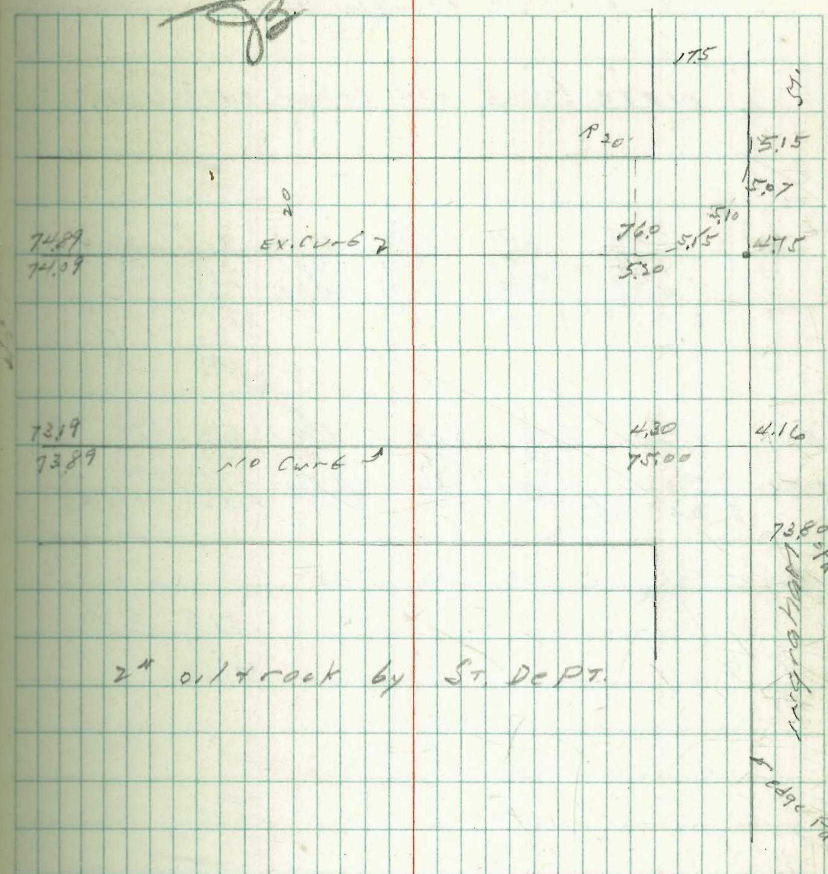
78.11 NW BP in School Porch
1.89 Ingraham & Emerald.
80.00

Moore
11-8-38.

Indexed

Pav. of Emerald W of Ingraham

		N	Pav. grade	S	
0+00 = W.L.	Ingraham	75.20		74.30	C 0.03
+25		75.10 ✓			C 0.57
+50		75.00 ✓			C 0.97
+75		74.90 ✓			C 0.79
1		74.80 ✓			C 0.36
+25		74.70 ✓			F 0.26
+50		74.61 ✓			F 0.18
+75		74.51 ✓			F 0.11
2		74.41 ✓			C 0.09
+25		74.31 ✓			C 0.20
+50		74.21 ✓			C 0.24
+79		74.09 ✓		73.19	C 0.14



Moore
11-3-38

Par. Stranoway
betw. San Juan Pl. & Nantasket
2" oil rock by St. Dept.

NOTE! ℄ 0.20 below east side.

W = 5.52 / 4.99 / 4.27 / C 0.50 ; 5.41 / 4.90 / 4.51 / C 0.39 ; 5.30 / 5.01 / 4.77 / C 0.24 ; 5.26 / 5.05 / 4.88 / C 0.17 ; 5.15 / 5.16 / 5.06 / C 0.10 ; 5.04 / 5.27 / 5.11 / C 0.16

E = 5.37 / 4.94 / 5.24 / F 0.30 ; 5.26 / 5.03 / 4.63 / C 0.40 ; 5.20 / 5.11 / 4.87 / C 0.24 ; 4.90 (℄ alley) / 5.21 / 5.17 / C 0.20 ; 5.16 / 5.15 / 5.13 / F 0.02 ; 5.08 / 5.38 / 2.95 / C 2.30 ; 4.99 / 5.32 / 4.51 / C 0.81

5.16
2.37
7.53

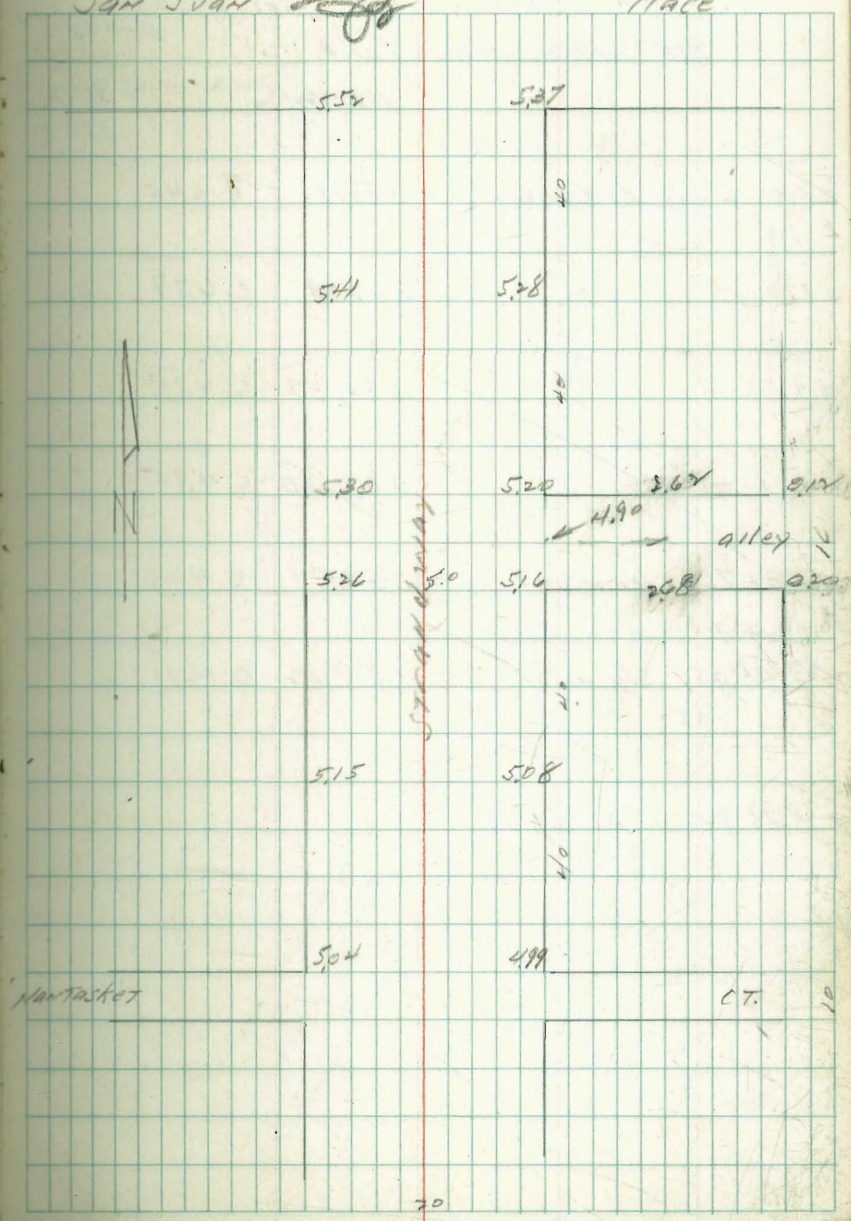
707 SWBP
3.2
10.31

Seawall
San Juan Pl.

27

Indexed

San Juan Place



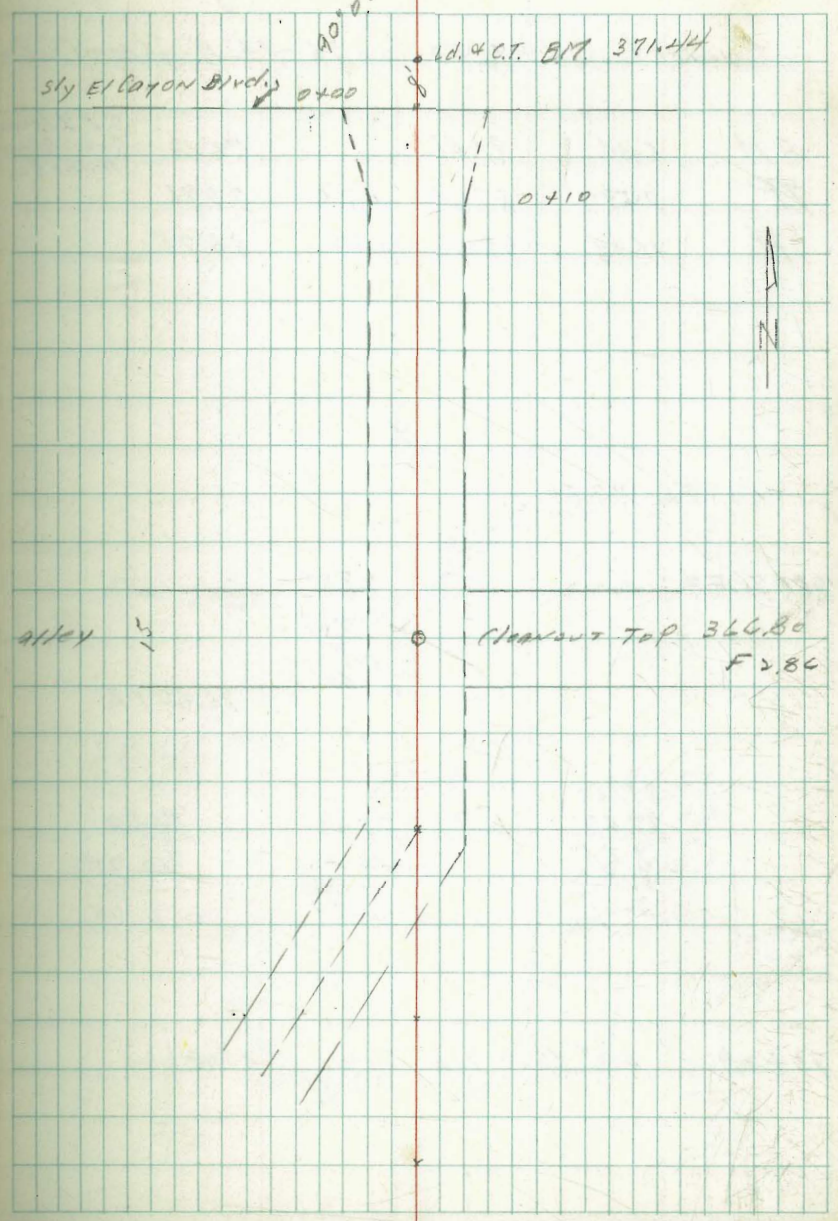
Indexed

See F.B. 1536-79.

11-5-38
W.P.H.

Storm Drain Const. Bet. El Cayon & Orange
Blk 1 N. Highland Park

		F.L. Gr.	
			371.44 3.37 374.81
0+00 = Sly El Cayon		363.19	C 6.45
0+10		362.03	C 6.57
0+50	1.64%	361.37	C 6.75
1+00		360.55	C 4.95
1+36.75 Clean out		359.94	C 4.00
1+44.25 Sly alley		359.87	C 4.11
1+76.90 = Δ 29°10'			



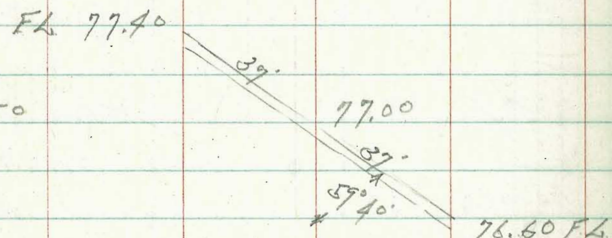
Home Ave Culverts

Indexed

Nov 14-38
Sisson
Northern

Culvert 86+76.50 — 74' 24" Reinforced Con Pipe

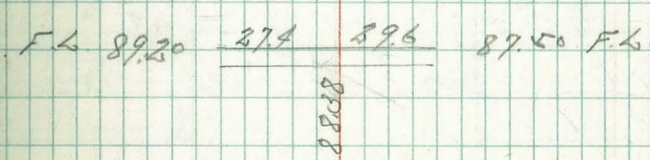
BM	6.34	81.46		75.12	C.T. ℄ Lemon Grove Blvd + Home Ave
TP	7.59	87.35	1.70	79.76	
TP	11.78	98.53	0.60	86.75	



87.35		
77.40	77.00	76.60
9.95	10.35	10.75
8.90	4.82	9.80
C 1.05	C 5.53	C 0.95

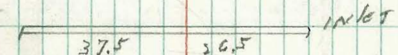
73+74 24" Conc. Pipe Culv. Radial

Culvert 79+77 — 57' - 8'x4' Conc. Box



98.53		
89.20	88.38	87.50
9.33	10.15	11.03
2.61	4.75	8.52
C 6.72	C 5.40	C 2.51

104.96
4.44
109.40



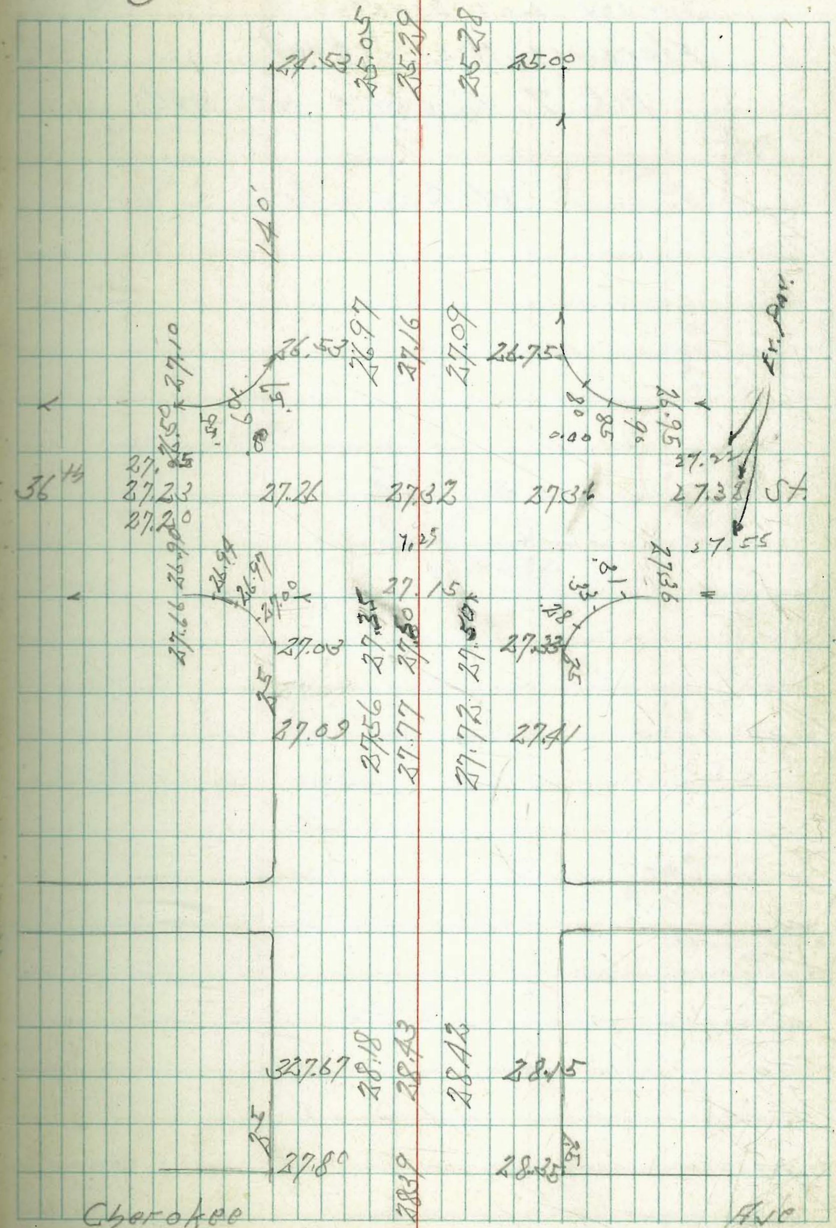
100.6		101.60
8.8	8.3	7.8
3.2	4.5	3.3
C 5.6	C 3.8	C 4.5

Dwight St Paving
Cherokee to 140' N of 36th St.

BM	4.83	332.38		327.55	NW. B.P. Dwight x 36

Indexed

Nov 15-38
S. Sloop
Northern

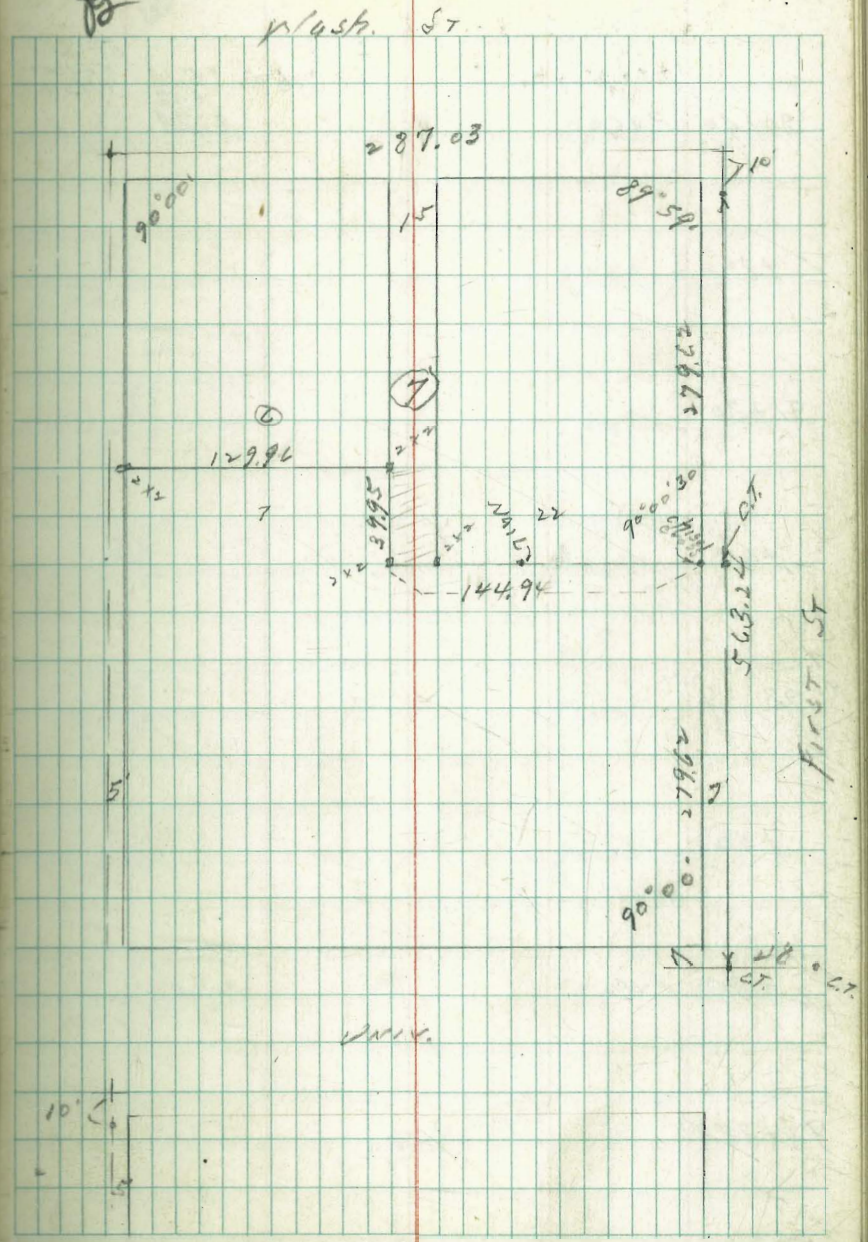


Moore
11-23-28.

Survey - Lot Lines
Florence Hts. School
Blk 7 Florence Hts Add.

Wilson - Frink

Indexed



Home Ave Paving

Indexed

Nov-17-38

32

E

		BM 95.12 6.12 81.24	C.T. & Federal Highway		
90+40	P.V.C.				
+80					
91+30					
+60					
92					
+40					
+80	EVC				
92+38.15					

3.4 / 3.4 / F 0.0	78.15	✓	78.15	3.4 / 3.4 / F 0.0	
3.6 / 4.1 / F 0.5		✓	77.68	3.6 / 4.0 / F 0.4	
4.0 / 4.7 / F 0.7		✓	77.50	4.0 / 4.4 / F 0.4	
4.4 / 5.2 / F 0.8		✓	76.80	4.4 / 4.9 / F 0.5	
4.8 / 5.2 / F 0.4		✓	76.45	4.8 / 5.1 / F 0.3	
5.1 / 5.6 / F 0.5		✓	76.15	5.1 / 5.6 / F 0.5	
5.3 / 5.8 / F 0.5	75.90	✓	75.90	5.3 / 5.8 / F 0.5	
		75.61	5.63		

W

E

		81.24 ↑ 1.21 800.3 9.97 89.97			
86+60			7.1 7.2 F0.1	✓	82.87 7.1 6.7 C0.4
87	E.V.G.		7.6 7.7 F0.1	✓	82.35 7.6 7.4 C0.4
+50			8.2 8.2 8.1	✓	81.73 8.2 7.7 C0.5
88			8.9 8.8 C0.1	✓	81.11 8.9 8.0 F0.1
+50			0.7 0.6 C0.1	✓	80.49 0.7 1.2 F0.5
89			1.4 1.7 F0.3	✓	79.87 1.4 1.7 F0.3
+50			2.0 2.5 F0.5	✓	79.25 2.0 2.3 F0.3
90			2.6 3.2 F0.6	✓	78.63 2.6 3.2 F0.6

Station				W				E
83		89.97 ⊼ 1.35 88.62 10.02 98.64 ⊼		1.1 1.4 F0.3		✓	88.89	1.1 0.3 C0.8
+50				2.0 2.6 F0.6		✓	88.00	2.0 1.4 C0.6
84				3.9 3.3 F0.4		✓	87.11	2.9 2.9 0.0
+60	P.V.C.			3.9 4.5 F0.6	86.05	✓	86.05	3.9 3.9 0.0
85				4.6 5.3 F0.7	85.34	✓	85.84	4.6 4.5 C0.1
+40				5.3 6.0 F0.7		✓	84.66	5.3 5.1 C0.2
+80				6.0 6.6 F0.6		✓	84.02	6.0 5.6 C0.4
86+20				6.6 6.8 F0.2		✓	83.42	6.6 6.6 0.0

Station		Angle			H			E	
	O		98.64 T						
79+20		13°23'		3.7 / 1.7 / C1.0	95.95			95.42	3.2 / 3.6 / F0.4
+60.72 E.C.		13°58'		3.5 / 2.8 / C0.7	95.18			94.74	3.9 / 4.4 / F0.5
		Line only							
		B.M. 2x2 R.P. Lt of E.C. 89.90							
80				4.3 / 5.9 / F1.6	94.36			94.10	4.5 / 4.9 / F0.4
+40				5.1 / 5.7 / F0.6	93.56		0.776	93.45	5.2 / 5.6 / F0.4
+80	×	Transition		5.8 / 5.8 / 0.0	92.81			92.77	5.9 / 5.9 / 0.0
81+20	⊙	⊙		6.6 / 6.8 / F0.2	92.09		✓	92.09	6.6 / 6.7 / F0.1
+50				7.1 / 7.6 / F0.5			✓	91.56	7.1 / 7.6 / F0.5
82				8.0 / 8.4 / F0.4			✓	90.67	8.0 / 8.3 / F0.3
+50				8.9 / 8.9 / 0.0			✓	89.78	8.9 / 8.4 / C0.5

				98.641
				2.00
75+50		8° 05.02'		96.64
				10.25
				106.891
76		8° 48'		
+50		9° 31'		
77		10° 13.93'		
+50		10° 56.90'		
78		11° 39.87'		
+40		12° 14.25'		
+80		12° 48.63'		

W E

5.1 / 5.1 / 0.0	101.83	✓	101.33	5.3 / 5.7 / C0.4
5.8 / 5.7 / F0.1	101.08	✓	100.48	6.4 / 6.6 / C0.8
6.6 / 6.7 / F0.1	100.63	✓	99.73	7.7 / 6.0 / C1.2
7.3 / 7.1 / C0.2	99.59	✓	98.99	7.9 / 7.6 / C0.3
8.1 / 7.9 / C0.2	98.84	✓	98.23	8.7 / 8.7 / 0.0
8.8 / 8.7 / C0.1	98.09	✓	97.48	9.4 / 9.7 / F0.3
1.2 / 0.0 / C1.2	97.48	✓	96.88	1.8 / 2.0 / F0.2
1.9 / 2.5 / F0.6	96.73	✓	96.12	2.5 / 2.9 / F0.4

			106.89 ℄					
			0.15					
72		3°04.33'	106.74					
			7.70					
			114.44 ℄					
			2.69					
		BM	111.75	on RP Hub 40' N 69+86.66 B.C				
+60	P.V.C.	3°55.77'						
73		4°30.15'						
	24" Culv.							
+40		5°04.53'						
+80		5°38.91'						
74+20		6°13.29'						
+60		6°47.67'						
75	P.O.C. E.V.C	7°22.05'						

7.8 / 6.9 / C0.9	107.05	✓	106.45	8.5 / 7.3 / C0.5				
8.8 / 7.6 / C0.7	106.16	✓	105.56	1.3 / 0.1 / C1.2				
1.3 / 0.5 / C0.7	105.56	✓	104.96	1.9 / 0.6 / C1.3				
1.9 / 1.6 / C0.3	104.96	✓	104.36	C 2.1 / 1.5				
2.5 / 2.2 / C0.3	104.36	✓	103.76	C 3.1 / 1.4				
3.1 / 3.1 / 0.0	103.76	✓	103.16	C 3.8 / C0.9				
3.7 / 3.8 / F0.1	103.18	✓	102.58	C 4.3 / C0.7				
4.3 / 4.4 / F0.1	102.58	✓	101.98	C 4.9 / C0.6				

Station		Deflection				W	W Elev.		E Elev.	E
69			B.M.	111.75 / 3.06 / 114.81 H.I.	on R.P. Hub 40' Rt 69+85.66	4.5 / 4.7 / F0.2	110.28		110.31	4.7 / 4.3 / C0.4
69+40						4.9 / 4.9 / 0.0	109.96		109.75	5.1 / 5.9 / F0.8
+80						5.2 / 6.0 / F0.8	109.64		109.28	5.5 / 5.9 / F0.4
+85.66	B.C.						out		out	
70+20		0° 29.51'				5.5 / 6.7 / F1.2	109.30		108.80	6.0 / 6.4 / F0.4
+60		1° 03.88				5.9 / 6.7 / F0.8	108.93		108.37	6.4 / 6.8 / F0.4
71	.8594	1° 38.26				6.3 / 6.3 / 0.0	108.55		107.95	6.9 / 7.0 / F0.1
+50		2° 21.26'				7.0 / 6.9 / C0.1	107.80	✓	107.20	7.6 / 7.3 / C0.3

Station					
65+50				114.81 Λ 1.75 112.06 8.46 121.52 Λ	
66					
+20 = Brk					
+50					
67					
67+23.98					
+72					
68 +20					
+60					

W | Grade Change to 66+20, Corrected .04 | E

W				E	
0.8 / 1.8 / F ~~1.0~~ F0.6			113.97		0.8 / 1.0 / F ~~0.2~~ C0.2
1.4 / 2.2 / F ~~0.8~~ F0.4		113.04	~~113.44~~		1.4 / 1.5 / F ~~0.1~~ C0.3
	112.84	0	112.84		
1.9 / 2.2 / F ~~0.4~~ F0.1		112.61	~~112.91~~		1.9 / 2.3 / F0.4 F0.1
2.4 / 3.2 / F ~~0.8~~ F0.6		112.18 / 2800	~~112.38~~		2.4 / 2.5 / F0.1 C0.1
2.7 / 3.4 / F ~~0.7~~ F0.5	~~112.13~~	111.95	~~112.13~~		2.7 / 2.2 / C ~~0.5~~ C0.7
3.2 / 4.0 / F ~~0.8~~ F0.7	111.62	111.54	~~111.62~~		3.2 / 2.6 / C ~~0.6~~ C0.7
3.6 / 4.0 / F0.4	111.12	✓	111.12		3.6 / 3.6 / 0.0
4.1 / 4.3 / F0.2	110.71		110.69		4.1 / 3.9 / C0.2

Station				Elev.	W			E
			121.52 T					
61+60					3.4 / 3.8 / F ~~0.4~~ Grade		118.10	3.4 / 3.7 / F ~~0.3~~ C0.1
62					3.8 / 4.6 / F ~~0.8~~ F0.4		117.68	3.8 / 4.3 / F ~~0.5~~ F0.1
+50					4.4 / 5.1 / F ~~0.7~~ F0.3		117.15	4.4 / 4.9 / F ~~0.5~~ F0.1
63					4.9 / 5.8 / F ~~0.9~~ F0.5		116.62	4.9 / 5.2 / F ~~0.3~~ C0.1
+50					5.4 / 6.0 / F ~~0.6~~ F0.2		116.09	5.4 / 5.9 / F ~~0.5~~ F0.1
64					6.0 / 6.3 / F ~~0.3~~ C0.1		115.56	6.0 / 6.2 / F ~~0.2~~ C0.2
+50					6.5 / 7.5 / F ~~1.0~~ F0.6		115.03	6.5 / 6.3 / C0.2 C0.6
65					7.0 / 7.8 / F ~~0.8~~ F0.4		114.50	7.0 / 7.2 / F ~~0.2~~ C0.2

Grade Change Lowered 0.40
55+00 to 66+70
0.1059

Station		Angle				W	W Elev.		E Elev.	E
				121.52 ⊼ 0.95						
58+80		10°46.86'	TP	120.57 8.27 128.84	0.7 F Stub 59+60	8.3 8.1 F ~~0.1~~ C0.3	120.58		122.11	6.7 7.7 F ~~1.0~~ F0.6
59+20		1.7189 11°55.61'				8.7 8.8 F ~~0.1~~ C0.3	120.16		121.51	7.3 8.0 F ~~0.7~~ F0.3
+53.36	E.C.	12°53'					out		out	
+60						1.7 2.6 F ~~0.3~~ C0.1	119.85		120.83	0.7 1.6 F ~~0.3~~ C.01
60						2.0 2.4 F ~~0.4~~ 0.0	119.50		120.15	1.4 1.6 F ~~0.2~~ C0.2
+40						2.2 2.7 F ~~0.5~~ F0.1	119.28		119.46	2.1 2.2 F ~~0.1~~ C0.3
+80						2.6 2.6 ~~0.0~~ 0.0	118.92		118.93	2.6 2.7 F ~~0.1~~ C0.3
61+20	P.V.C.					3.0 3.0 ~~0.0~~ 0.0	118.53	0	118.53	3.0 3.1 F ~~0.1~~ C0.3

Grade Change Lowered 0.40
55+0 to 66+20

01059

						N	E	
				128.84				
55+40		1° 02.48'			F ~~0.6~~ F0.2	125.15	126.55	F ~~1.1~~ F0.8
+80		2° 11.23'			F ~~0.4~~ C0.2	124.55	126.10	F ~~0.9~~ F0.5
56+20	P.C.	3° 20'			F ~~0.1~~ C0.3	124.02	125.61	F ~~1.0~~ F0.6
+60		4° 28.73'			F ~~0.1~~ C0.3	123.49	125.08	F ~~0.7~~ F0.3
57		5° 37.48'			F ~~0.4~~ C0.2	122.96	124.54	F ~~0.5~~ F0.1
+50		7° 03.42'			F ~~0.6~~ F0.2	122.29	123.87	F ~~0.6~~ F0.2
58		8° 29.36'			F ~~0.4~~ 0.0	121.62	123.20	F ~~0.5~~ F0.1
+40	E.C.	9° 38.11			F ~~0.3~~ C0.1	121.09	122.69	F ~~0.9~~ F0.5

1.7189

0.133

Grade Change Lowered 0.40
55+0 56+50

51+80		4°06.40'		
			128.84	A
			3.50	
52+20		5°15.15'	125.34	
			4.14	
			129.48	
			8.09	
			121.39	B.M. R.P. 40' S of
			11.82	
+60		6°22.50'	133.21	B.C. 52+03.65
+69.73	E.C.	6°41'		
53	E.Y.C.			
+50				
54				
+50				
55	E.Y.C.			
55+03.65 B.C.				

N	E	
C0.4 130.99	129.38	C1.7
C0.4 130.38	128.92	C1.7
0.0 129.74	128.52	C0.8
0.0 129.02	128.18	C0.9
0.0 128.12	127.76	C0.7
C0.3 127.22	127.34	C0.5
C0.1 126.32	126.92	C0.2
125.43 out	126.50	out
F0.6 105.80 F0.2	126.85	F0.6

					W	E	
48+60	E.C.			133.21 ft 0.76 132.45 9.15 141.60	C 0.1	134.32	C 0.1
49					F 0.2 133.78	133.76	F 0.2
+40					F 0.6 133.31	133.18	F 0.4
+80					F 0.3 132.98	132.51	F 0.3
50 +20					F 0.3 132.70	131.79	0.0
+36.64	B.C.						
+60		0° 40.15'			F 0.5 132.39	131.08	C 0.4
51		1° 48.90'			F 0.2 131.99	130.46	C 0.8
+40		2° 57.65'			C 0.2 131.53	129.91	C 1.0

					W	E
44+80	T.P. 44+40	on	18' OUT on South	141.60 N. 1.24 / 140.36	F 0.3	139.85 F 0.1
45+30	E.V.C.	Stopped Grade		12-5-38	0.0	138.80 C 0.6
+50					C 0.3	138.40 C 0.2
46					~~C 0.8~~ C 0.3	137.73 ~~C 0.8~~ C 0.3
+50					C 0.2	137.08 (.31) 0.0
47					F 0.1	136.42 F 0.2
+50					F 0.2	135.77 F 0.2
48					F 0.1	135.12 C 0.2

41+80				140.36 T.P. / 12.76 / 153.12 / 4.82 / 148.30	~~148.00~~ 148.30
42	Changed to Fairmount ↓		Sec p 49		BMBP Cubi Fairmount Home
				152.33 / 12.98 / 141.35 / 2.72 / 144.07	
42+40					
42+80					
43+20					
43+60					
44					
+40					

W E

← use for Pav. F 1.8		151.80	F 1.1
F 1.2		150.70	F 1.2
F 1.1		148.50	F 1.1
F 0.5		146.60	F 0.7
F 0.2		144.75	0.0
F 0.4		143.05	C 0.1
F 0.3		141.60	F 0.2
F 0.3		140.66	F 0.4

See p 63

Sta.					W		E	
~~40~~ EVC				3.2 / 3.1 / +0.1	151.80		150.80	4.2 / 0.0
40+40	Pav.	wl	148.22 / 6.11 / 154.33	2.4 / 1.9 / +0.5	152.56		151.15	3.9 / 4.1 / −0.2
40+60	"	wl ✓		✓	153.42		152.19	✓
			148.22 / 6.81 / 155.03 *					
40+80				0.5 / 1 / C 0.4	153.80		152.75	F 0.7
41				F 0.7	154.0		153.15	F 0.8
41+20				F 1.1	153.85		153.10	F 0.6
41+40	-			F 1.5	153.46		153.0	F 0.9
41+60				F 1.6	152.60		152.60	F 1.1

See p 62 & 63

FAIRMONT Ave

Eq. 37+54.81 "B" = 37+37.97 "A"

37+60

38

38+40 P.V.C.

39

39+50

W E

155.03 T

	W			E	
4.6 / 4.9 / -0.3				150.40	4.6 / 4.8 / -0.2
4.7 / 4.9 / -0.2	150.30	OUT		150.30	4.7 / 4.8 / -0.1
4.7 / 4.9 / -0.2	150.30			150.30	4.7 / 4.9 / -0.2
4.5 / 4.7 / -0.2	150.50			150.50	4.5 / 4.2 / -0.7
0.81 % 4.0 / 4.1 / -0.1	151.0			150.62	4.4 / 0.0 0.18 %
3.6 / 3.7 / -0.1	151.40	(1.3)		150.75	4.3 / 0.0

0+00 Home Ave. at Fairmont

Station					LT	℄	RT
42+09 = BC LT	Culv. hd. wall		B.M. B.P.	148.22 11.78 160.00	149.75 ✓		149.75 ✓
41+80					151.05 ✓		151.05 ✓
		LT		RT			
41+60					151.95 ✓		151.95 ✓
41+40					152.47 ✓		152.80 ✓
	42+80	146.55		146.55			
41+20					153.08 ✓		153.40 ✓
	42+40	148.35		148.35			
41					153.10 ✓		153.74 ✓
+80					152.79		153.76 ✓
~~+60~~					~~152.79~~		~~153.76~~
40+~~40~~ = ~~W edge Pav. Fairmont~~					~~152.19~~		~~153.44~~

Home Ave
at Fairmont

160.00

	LT.		RT.	
1+40	C1.3	156.15	157.15	0.0 on Pav.
1+40	C1.7	154.20	155.50	C0.3
1+20	C2.4	152.95	154.45	C0.3
1+00	C0.5	152.50	153.80	0.0
0+83	C0.3	152.30	153.40	
0+71	0.0	152.08	152.80	
0+50	F0.7	151.70	152.05	
0+29 = 41+80	F1.0	151.05	151.05	
0+00 / 42+09 = B.C. Lt. to Fairmont		149.75 ✓	149.75 ✓	

Home Ave.
at Euclid

Note! 4+00 to Fairmont
0.30 below Profile

+60

+40

+20

BM. Ld. & C.T. 229.13 / 0.63 / 229.76

0+00 B.C. on Euclid Ave E Pav.

Home at Fairmont

160.00 T / 0.50 / 159.50 / 7.80 / 167.30

2+48.14 E.C. of Lt. Curve to North on Fairmont

2+20

~~2+00~~

1+80

LT	℄	RT	51
227.13		228.24	1.6 / 1.7 / -0.1
227.41		228.60	1.2 / 0.8 / +0.4
227.82		228.98	0.8
228.42		229.60	
167.48			
0.03	167.0		
	159.80	OUT	
0.03	158.70	159.40	Pav. edge

Δ = 41°13' Rt
R = 1000
L = 719.37
1.7189

R.P. Rt. 39.60 - 25 - 67
" Lt 40

Station					LT		℄	RT	
3+20				0°51.45	12.6 / 12.5 / +0.1	217.24		215.82	14.0 / 13.8 / +0.2
2+90.27	B.C. Rt.				10.8 / 11.0 / -0.2	219.00	1+00 to 4+00 fanned out	217.75	12.1 / 11.9 / +0.2
+40				229.76	8.0 / 8.5 / -0.5	221.77		221.02	8.8 / 9.1 / -0.3
2					5.9 / 6.9 / -1.0	223.93		223.45	6.4 / 7.7 / -1.3
+60					4.3 / 5.3 / -1.0	225.50		225.45	4.4 / 5.5 / -1.1
+20	P.R. V.C.					224.45	Profile 0+00 to 2+00	224.85	3.0 / 3.2 / -0.2
1+00						226.75		227.40	2.4 / 2.3 / +0.1
+80						226.93		227.88	1.9 / 1.8 / +0.1

					LT		RT	
7		11° 44.59	229.76 12.45 217.31 0.66 217.97 T 12.87 205.10 0.51 205.63 R	4.3 4.0 + 0.3	199.35		197.75	7.9 7.9 0.0
	+50	10° 18.65		4.5 4.2 + 0.3	201.15		199.55	6.0 5.3 + 0.7
6		8° 52.71		2.4 2.1 + 0.3	203.25		201.65	4.0 3.2 + 0.8
	+50	7° 26.77		12.4 11.8 + 0.6	205.60		204.00	14.0 13.8 + 0.2
5		6° 00.83		9.9 9.3 + 0.6	208.10		204.50	11.5 11.4 + 0.1
	+50	4° 32.89		7.5 6.5 + 1.0	210.50		208.90	9.1 9.4 - 0.3
4		3° 08.95		5.1 4.5 + 0.6	212.92	lowered 0.3'	211.32	6.7 6.9 - 0.2
	3+60	2° 00.2		2.7 2.5 + 0.2	215.30	raised 0.1' to 2+60	213.74	4.3 4.9 - 0.6

			LT		RT	
	40' Left	193.66				
	Set BM. of 10+09.64	5.46				
	3 x 3 R.W. Hub	188.20				
10+20			1.4 1.2 0.2	192.30	191.85	2.4 2.3 +0.1
10+09.64 E.C.	20° 36.50			—	out	—
+80	19° 45.00		12.5 12.2 +0.3	193.16	191.8	1.3 1.3 +0.3
		205.63 T				
+40	18° 37.00		11.7 11.7 0.0	193.95	192.40	13.2 12.9 +0.3
9	17° 28.35		11.9 0.0	194.67	193.07	12.5 12.2 +0.3
+50	16° 02.41		10.1 9.8 +0.3	195.50	193.90	11.7 11.6 +0.1
8	14° 36.47		9.1 8.8 +0.3	196.50	194.90	10.7 10.4 +0.3
7+50	13° 10.53		7.9 7.6 +0.3	197.75	196.15	9.5 8.9 +0.6

193.66 ±

Station		LT		RT	
+50		7.4 − 7.3 = +0.1		186.33	7.4 − 7.3 = +0.1
18		6.6 / 0.0		187.16	6.6 / 0.0
+50		5.7 − 5.5 = +0.2		187.98	5.7 − 5.8 = −0.1
17		4.9 − 4.7 = +0.2		188.81	4.9 − 4.9 = 0.0
+80	EVC.	4.6 − 4.2 = +0.4		189.44	4.4 − 4.4 = 0.0
+40		4.0 − 3.3 = +0.7	189.78	189.76	4.0 − 3.8 = +0.2
11		3.2 − 2.7 = +0.5	190.55	190.35	3.4 − 3.3 = +0.1
10+60		2.3 − 1.9 = +0.4	191.38	190.87	3.9 − 3.6 = +0.3

1.4532 %

					LT		RT.	
				184.26 BM / 0.04 / 184.22 T.P. / 9.44 / 193.66 BM				
+50					4.3 / 4.8 / −0.5		180.05	4.3 / 0.0
17					3.8 / 3.7 / +0.1	1.432	180.77	3.8 / 3.7 / +0.1
+50					2.8 / 3.1 / −0.3		181.48	2.8 / 3.1 / −0.3
16	Break				2.1 / 2.0 / +0.1		182.20	2.1 / 2.6 / −0.5
+50					1.3 / 1.0 / +0.3		183.03	1.3 / 1.5 / −0.2
15					0.5 / 0.0 / +0.5		183.85	0.5 / 0.7 / −0.2
+50					9.0 / 9.1 / −0.1	1.652	184.68	9.0 / 9.2 / −0.2
14					8.2 / 8.3 / −0.1		185.50	8.2 / 8.4 / −0.2

Station			LT			RT
21+51.55	Break	175.44 ↑ 0.72 174.72 9.54 184.26 ↑	1.1 1.2 -0.1	-1.44	174.30	1.1 1.4 -0.3
21			0.4 0.7 -0.3		175.04	0.4 0.7 -0.3
+50			8.4 8.7 -0.1	-1.432	175.76	8.4 8.6 0.0
20			7.8 8.4 -0.6		176.47	7.8 8.0 -0.2
+50			7.1 7.6 -0.5		177.20	7.1 7.7 -0.6
19			6.4 6.9 -0.5		177.90	6.4 7.1 -0.7
+50			5.7 6.3 -0.6		178.62	5.7 6.4 -0.7
18			5.0 5.2 -0.2		179.34	5.0 5.4 -0.4

175.44 K

+50

25

+50

24

+50

23

+50

22

LT		RT	
4.9 / 4.5 / + 0.4		168.54	6.9 / 7.2 / − 0.3
6.1 / 5.5 / + 0.4		169.27	6.1 / 6.0 / + 0.1
5.4 / 4.7 / + 0.7		169.99	5.4 / 4.9 / + 0.5
4.7 / 4.1 / + 0.6	1.44	170.71	4.7 / 4.3 / + 0.4
4.0 / 3.7 / + 0.3		171.43	4.0 / 3.8 / + 0.2
3.3 / 3.2 / + 0.1		172.15	3.3 / 3.2 / + 0.1
2.5 / 2.4 / + 0.1		172.88	2.5 / 2.5 / 0.0
1.8 / 1.9 / − 0.1		173.60	1.8 / 2.1 / − 0.3

				LT	RT
+50					
29		165.65 ℄ 0.29 165.36 T.P. 10.08 175.44 ℄		162.40	3.3 3.1 + 0.2
+50				163.18	2.5 2.7 − 0.2
28				163.97	1.7 0.0
+50				164.75	1.0 1.1 − 0.1
27				165.54	0.2 0.0 − 0.1
+50	Break			166.31	9.1 9.3 − 0.2
26				167.10	8.3 8.6 − 0.3
				167.92	7.5 7.9 − 0.4

⊼ 165.65

Station						LT			RT	
32+20		Δ = 5°33′ Rt	0°58.7		7.2 / 6.4 / +0.8	158.52		157.91	7.8 / 7.6 / +0.2	
		R = 2000								
		L = 193.73								
31+80		0.8594	0°24.3		6.7 / 5.9 / +0.8	159.00		158.57	7.1 / 7.3 / −0.2	
31+51.62	B.C. Rt.	R.P. 40 Rt + 40 Lt.					OUT			
31+40					6.1 / 5.4 / +0.7	159.62		159.25	6.4 / 6.6 / −0.2	
31					5.5 / 4.9 / +0.6	160.46		159.92	5.8 / 5.9 / −0.1	
30+60					5.0 / 4.5 / +0.5	160.68		160.63	5.1 / 5.2 / −0.1	
30+20					4.4 / 3.9 / +0.5	161.27		161.27	4.4 / 4.5 / −0.1	
29+80	P.V.C.	Break beg. TRANSITION			3.8 / 3.3 / +0.5	161.90		161.90	3.8 / 3.9 / −0.1	

Station					LT			RT	
35			1558[illegible] ⊼ 1.03 154.79 10.86 165.65 ⊼		2.1 1.8 +0.3	153.73		153.73	2.1 2.4 −0.3
+60					1.4 1.2 +0.2	154.38		154.34	1.5 0.0
34+20					0.8 0.4 +0.4	155.05		154.94	0.9 1.0 −0.1
33+80					9.9 9.9 0.0	155.79		155.57	10.2 0.0
33+45.35	E.C.	2° 46.5	R.P. 50' + 100' Rt.				OUT		
33+40		2° 41.9			9.2 9.1 +0.1	156.44		156.08	9.1 9.2 −0.1
33		2° 07.5			8.5 8.1 +0.4	157.27		156.66	9.0 9.2 −0.2
32+60		1° 33.1			7.8 7.2 +0.6	157.91		157.28	8.4 0.0

155.87*

Station		LT		RT
38		5.8 / 5.7 / +0.1	150.0	5.8 / 5.6 / +0.2
37+50		5.8 / 5.8 / 0.0	150.0	5.8 / 5.7 / +0.1
37+54.81 = "B" = Eq. 37+37.97 = "A"		5.7 / 5.6 / +0.1	150.10	5.7 / 5.7 / 0.0
37+20		5.5 / 5.4 / +0.1	150.35	5.5 / [illegible] / 0.0
+80	P.V.C.	4.9 / 4.9 / 0.0	150.90	4.9 / 5.2 / −0.3
+50		4.4 / 4.3 / +0.1	151.37	4.4 / 4.8 / −0.4
36		3.6 / 3.6 / +0.0	152.16	3.6 / 3.8 / −0.2
35+50		2.9 / 2.7 / +0.2	152.96	2.9 / 3.0 / −0.1

148.22 BM
7.60
155.82 ✓

Station		LT	℄	RT	
40 + 43.30 E edge Pav. Fairmont Ave		151.15 ✓		152.56	
40	5.0 / 4.7 / + 0.3	150.80		151.40	4.2 / 3.6 / + 0.6
+ 50	5.4 / 5.4 / 0.0	150.60		151.15	4.7 / 4.2 / + 0.5
39	5.4 / 5.0 / + 0.4	150.42		150.72	5.1 / 4.7 / + 0.4
38 + 40 EYC	5.6 / 5.8 / − 0.2	150.20		150.20	5.8 / 5.4 / + 0.4

Note! 38 + 40 E/y, grade
is 0.30 below Profile
38 + 40 to Fairmont Pav. fanned out

Save for home work

2-28-39

Worden St
2" water
Tennyson N'ly 280'

00 NL Tennyson	89.4 ✓
+50	87.2
1	85.1
+50	83.0
2	80.8
+40	79.1
2 +80	77.4

Pav = 5.1 − 3.5 = 1.6; 7.3 − 6.3 = + 1.0; 9.4 − 6.5 = + 2.9; 11.5 − 9.0 = + 2.5; 13.7 − 10.7 = + 3.0; 15.4 − 12.7 = + 2.7; 17.1 − 14.7 = + 2.4

Indexed

Alley Grades
Blk 1 Center Add
Pav. grades

Indexed

	W		E	
N L Pearl	✓113.20	✓	113.20	✓
+40 P.V.C.	✓110.65	C 0.50	110.65	C 0.50
+60	✓109.48	C 0.71	109.48	C 2.02
+80	✓108.51	C 0.67	108.51	C 2.31
+92 = beg. w cb	108.00	C 0.70		
1 +00	✓107.65	C 0.99	107.65	OUT
1 +20 E.V.C.	✓107.20	C 0.79	107.20	C 0.62
1 +32 = end w cb	✓106.93	C 0.52	106.93	C 0.17
1 +70	106.08	C 0.04	106.08	C 0.34
2 +20	104.95	C 0.96	104.95	C 2.0
2 +38	104.55	C 0.74	104.55	C 2.0
2 +65.1	103.44		103.94	

New Cuts 4/3/39. 0+92

W	10.65 / 5.12 / 4.67 / C 0.50	9.48 / 6.79 / 5.58 / C.71	8.51 / 7.26 / 6.67 / C.59	8.0 / 7.77 / 7.07 / C 0.70	7.65 / 8.12 / 7.32 / C.80	7.20 / 8.57 / 7.77 / C 0.80	6.93 / 8.84 / 8.28 / C.56
E	5.12 / 4.36 / C 0.76	6.79 / 4.87 / C 1.92	7.26 / 4.81 / C 2.45			8.57 / 8.31 / C 0.26	8.84 / 8.74 chisel / C.10 +
W	6.08 / 3.63 / 3.60 / C.03 / C 0.35	4.95 / 4.76 / 3.78 / C.98	5.55 / 5.16 / 3.16 / C 2.0	3.94 / 5.77 / 5.77 / 0.0			
Chisel Cut	4.76 / 2.76 / C 2.0	5.16 / 4.41 / C.75	5.77 / 3.77 / C 2.0				

115.17 S.E.B.P. Pearl Girard

Moore
1-2-39.

Note 1 6" dip on ℄ alley

115.17
0.51
115.68
9.26
106.42
3.71
110.13

beg. at 0+40

2-2-39
Check Drain Outlet

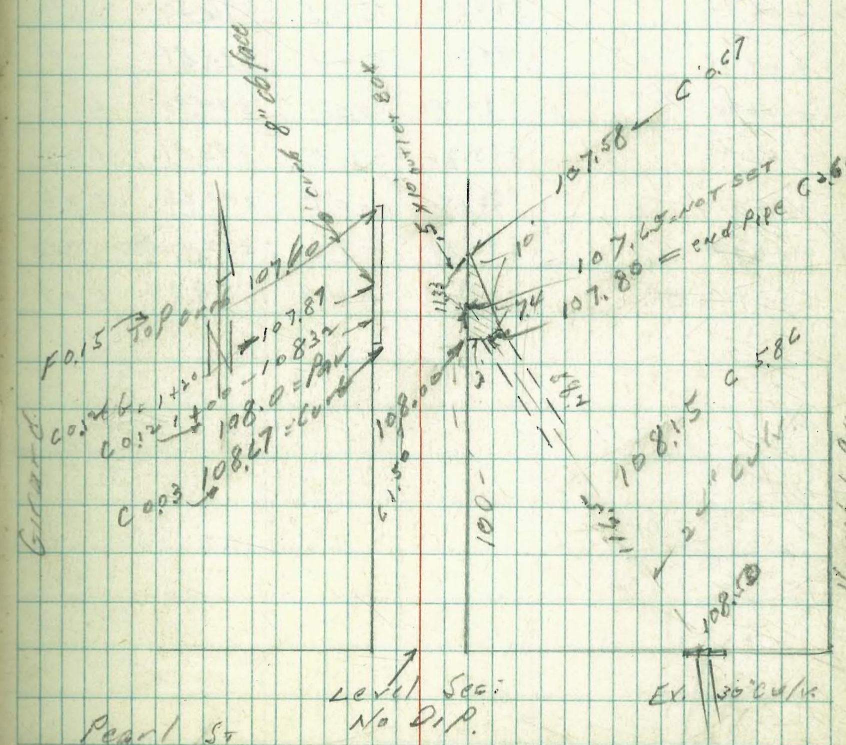
108.70
5.00
113.70

107.58
6.12
6.10
.02 H

108.
5.70
5.75
.05 Low

115.17
0.60
115.77
9.34
106.43
3.28
109.71

See FB 2289-36



Moore
1-4-39

Cut Stakes
53d St. El Cajon S/Y
40' wide

℄ Sta.	W		E	
0+00 ℄ 53d St. & El Cajon	394.02		394.15 = 1.95 / 30 394.76	C 3.2
0 + 26.74	395.66	C 2.0	396.16	C 2.1
0 + 46.74	396.69	C 1.2	397.19	C 1.1
0 + 66.74	397.36	C 0.7	397.86	C 0.6
0 + 86.74	397.67	C 0.3	398.17	C 0.4
1 + 06.74 EVC	397.61	C 0.5	398.11	C 0.4
1 + 66.74 PVC.	396.88	C 0.5	397.38	C 1.1
+ 86.74	396.55	C 0.3	397.05	C 1.2
2 + 06.74	396.02	C 0.5	396.52	C 1.3
+ 26.74	395.31	C 0.5	395.81	C 1.8
+ 46.74	394.40	0.0	394.90	C 1.9
+ 66.74	393.31	-0.8	393.81	C 2.1
+ 86.74	392.12	-0.9	392.62	C 2.3
3 + 06.74	390.81	-3.0	392.0 = Cor.	C 2.5
+ 26.74 = BC.	389.24	-4.8	389.74	C 0.7

393.88 SWBP 53d & El Cajon
8.25
402.13
4.25
397.88
2.57
400.45

Indexed

65th St Pav. 10' cbs.

Imp. South to alley

E.L. STA		E cb		W cb
Sly Imp. = 0+00	cb	221.30 ✓		
0+7.7		221.0 ✓		221.30 = SW Cor ✓
0+50.7	Top cb	227.55 ✓		227.55
1		233.90	C 1.0	233.90
1+37.7		238.77	C 1.4	238.77
1+57.7		241.35	C	241.35

↑ Pav. grade

12.91 %

244.44 S.E. Top Hyd.

8.98

232.62

0.51

232.11

12.34

244.45

1-13-39

Indexed

241.63

4.6

246.23 π

241.35

4.9

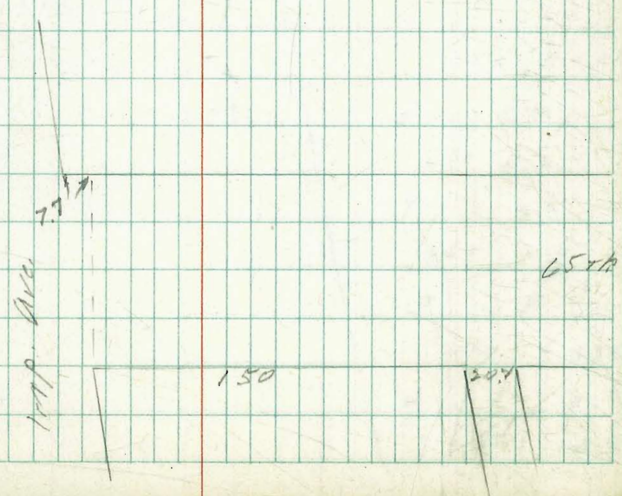
246.25

+0.3

4.9

3.2

1.7



Moore 1-24-39

Bayside Walk Const. Cont'd from 187-39

Grade -0.40

3.66 -0.40 4.06 rod	B.M. Sea wall 7.09 = SWBP El Carmel Pl. 2.46 9.55 4.24 2.30 T.P. nail pole Monterey Ct. Bayside Lane 1.36 3.66 $\bar{x}$ 2.64 1.02 T.P. 2.64 3.66 $\bar{x}$ 4.34 -0.68 = T.P. 4.49 3.81 T

Map

Δ = 39°07'30"

w.L. R = 2400

0.7162 = 1'

0° 35.81 = 50'

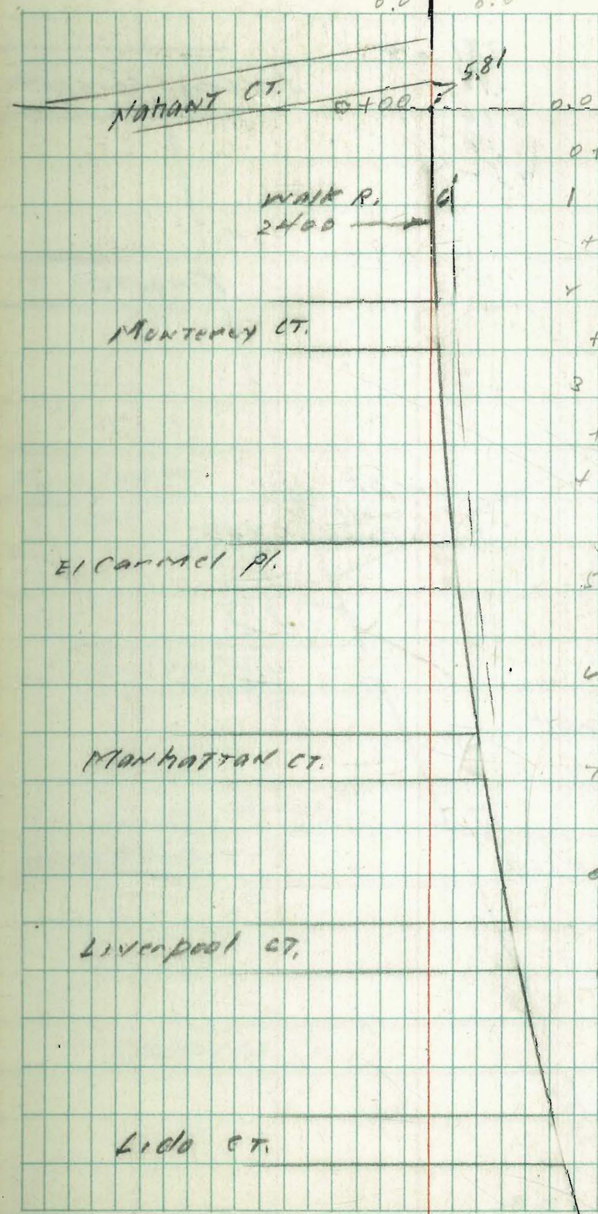
L = 1638.86

defl = 0°35.8 to 50'

Move E'ly 0.04 to 100' to meet Ex. Impmts.

0+00: Old stake grade = E.C. 187 G.B.

C 1.0	C 0.64	F 0.27 = [illegible]
C 1.0	C 0.96	0.0
C 0.80	0.0	F 1.0
C 0.80	0.0	
0.0	0.0	



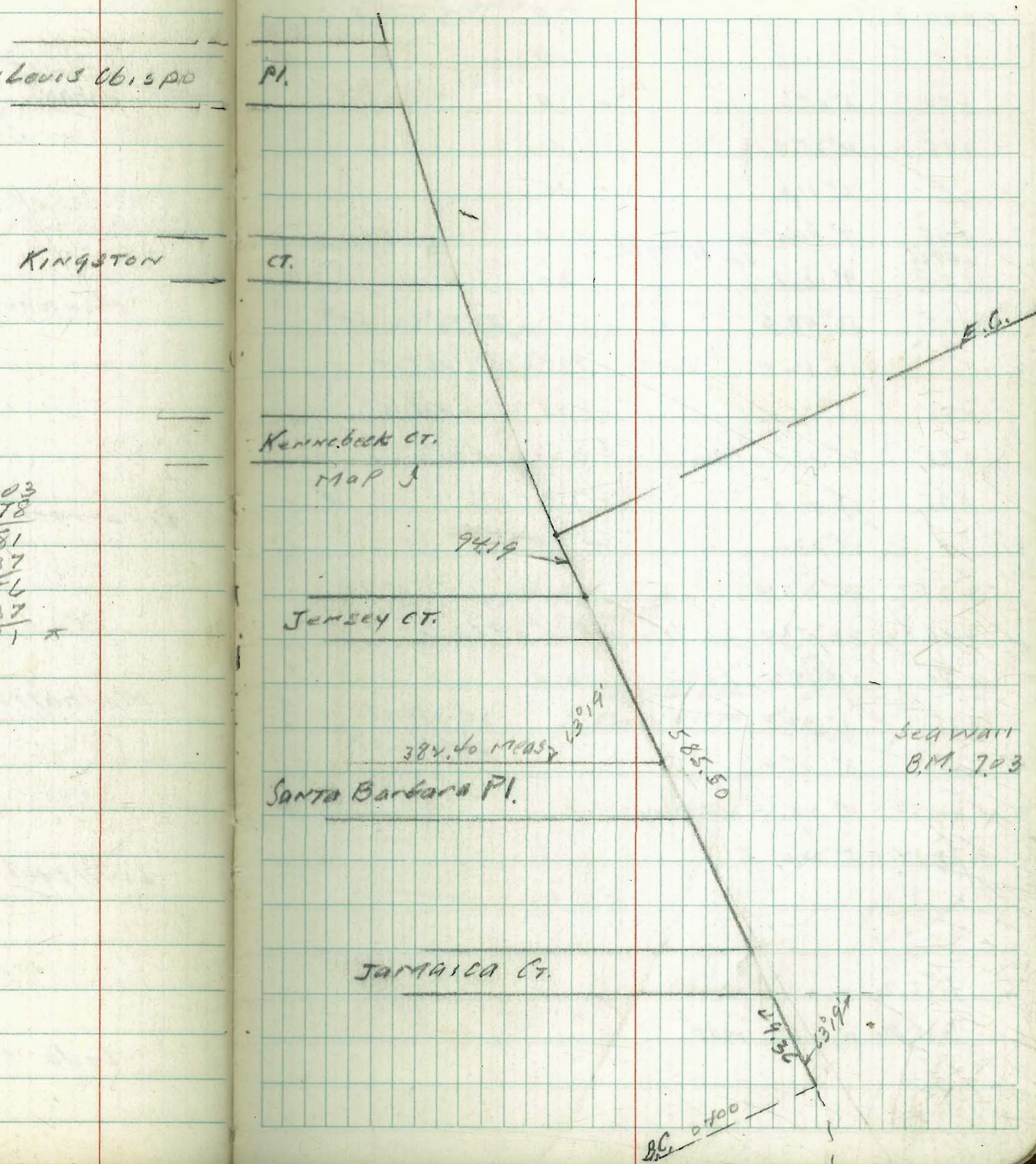
Station		Grade
0+00 = B.C.		0.0
0+50		0.0
1		0.0
+50		0.0
2		0.0
+50		0.0
3		0.0
+50		0.0
4		0.0
+50		0.0
5	on Bd. walk	C 0.30
+50		0.0
6	Porch	C 0.93
+50		0.0
7		0.0
+50		F 0.24
8		0.0
+50		0.0
9		0.0
+50		0.0
10		0.0
+50		C 0.06
11		0.0
+50		0.0

3.81 + ⊼
3.97
-0.16 T.P.
2.68
2.52 ⊼

12	0.0	
+50	-0.17	
13	0.0	
+50	0.0	
14	0.0	
+50	0.0	
15	-1.0	
+50	0.0	
16	0.0	
+40 E.C.	-0.50	
EC	0.0	
+0.17	0+50	on Conc.
0.0	1	on walk
0.0	+50	
-1.0	2	
-0.66	+50	on Conc.
0.0	3	
0.0	+50	
0.0	4	
0.0	+50	
0.0	5	
0.0	+50	
B.C. Rt.	5+85.5	0.0

S.W. B.P.
Seawall
Santa Barbara

7.03
.78
7.81
8.37
-0.56
4.37
3.81 ⊼



Grade = 0.40

				3.81	℄
				5.21	
				1.40	T.P
				3.64	
0+00	B.C.	R.T.		2.24	℄
	+25	1°24.8		-1.0	
	+50	3°05.6		-1.0	
	+75	4°35.6		-1.0	
1		6°11.2		-1.10	
	+25	7°44.0	℄ ISTHMUS	-1.0	
	+49.26				
	+50	9°16.8		-2.0	
	+75	10°49.6		-2.0	Δ = 53°22' 15"
2		12°22.4		-1.0	WLR = 463.05
	+25	13°55.2		-0.75	L = 431.32
	+50	15°28.0	P.O.C.	-0.21	3.712 = 1'
	+75	17°00.8		-1.0	
3		18°33.6		-1.0	
	+25	20°06.4		-1.0	
	+26.86	20°51.0	℄ Island	= 0.9 Low	
	+50	21°39.2	P.O.C.	0.0	
	+75	1°32.8			20' offset
4		3°05.6			ch = 26.07
4	+22.26	4°28.33	N.℄ alley		
4	+31.37	5°07.0	E.C.		

415.70 N.℄ alley Meas.

415.56 " " MAP

W'ly Bayside walk

Ventura Pl.
Seawall 7.51

JAMAICA CT.

4.96

0+00

ISTHMUS CT.

486.14 Map
486.32 Meas.

Ely Mission Blvd.

Island Ct.

452.78 = Map
452.92 Meas.

Map = 415.56
Meas. = 415.70

+31.37

alley

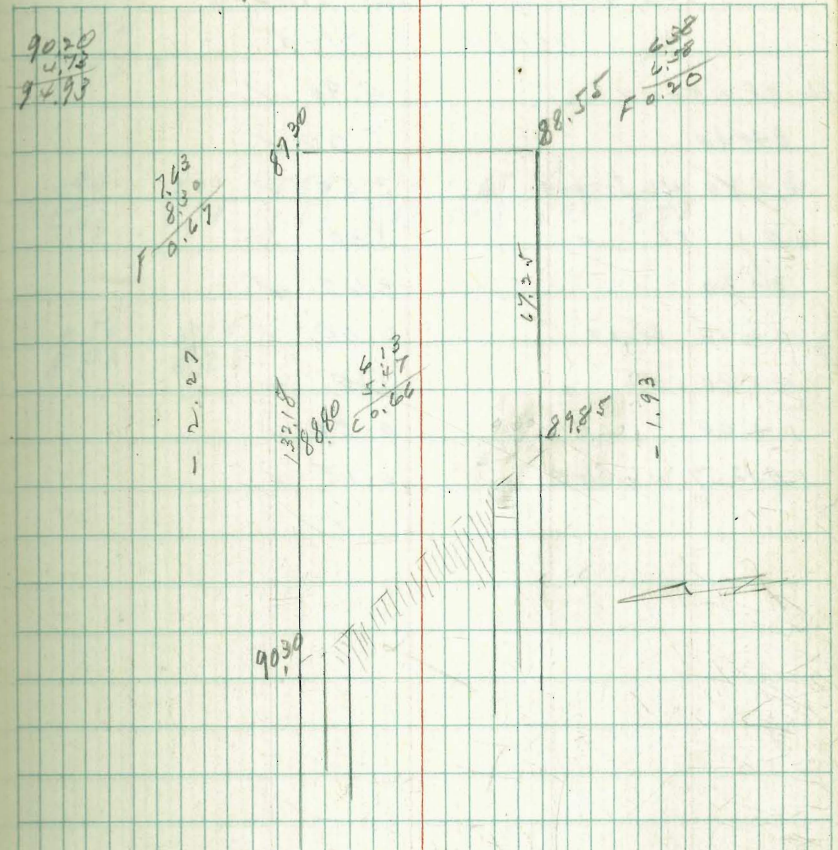
℄

Ventura Pl.

Wisteria Dr. grading 50' wide
for St. Dept.

0 0	90.30
0 + 66.1	88.80
1 + 32.2	87.30

Indexed



Indexed

2-24-39 74

Ormond Ct. Grades
Ocean to Blvd.

EL	O.F.W.K=00	4.90 ✓
	0+40	5.20 ✓
	0+80 W.L. Strand	5.50 ✓
	0.0 EL "	5.30 ✓
	0+30	3.65 ✓
	0+60 Break	2.00 ✓
	0+80 "	1.10 ✓
	1+00	0.50 ✓
	1+32.57 W.L. Blvd	0.15 ✓

7.19 BM BP Santa Clara Pl. & Seawall
1.74
8.93 x

5.90	5.30	5.50	5.30	3.65	2.00	1.10
4.03	3.73	3.43	3.63	5.28	6.93	7.83

0.50 0.15
8.43 8.78

2-27-39.

Niantic Ct. Grades

EL O.F. WK	4.90 ✓
0+40	5.15 ✓
0+80 W.L. Strand	5.40 ✓
00 E.L. "	5.20 ✓
0+56.65	2.72 ✓
1+13.30 W.L. Blvd.	0.25 ✓
00 EL "	-0.35 ✓
0+32.74	-0.87 ✓
0+65.49 Break	-1.40 ✓
1	-1.45
2	-1.50 ✓
3	-1.55 ✓
4 W.L. Bayside Lane	-1.60 ✓
E.L. " "	-1.50 ✓
0+41.07	-0.95
0+82.14 " Walk	-0.40

Indexed

8.93
3.64
5.29 T.P.
4.40
9.69

4.90	5.15	5.20	5.20	2.72	0.25	-0.35	-0.87
4.79	4.54	4.29	4.49	6.97	9.44	10.04	10.56

-1.40
11.09

11.09
-1.40 T.P.
4.02
5.62

-1.45	-1.50	-1.55	-1.60	-1.50	-0.95	-0.40
4.07	4.12	4.17	4.22	4.12	3.57	3.02

3.04
0.02

Nahant Ct. Grades

00 EL OF WK.		4.80 ✓
0+40		5.10 ✓
0+80	WL Strand	5.40 ✓
00	EL "	5.20 OUT
0+328		2.93 "
0+654	WL Blvd	0.67 ✓
00	EL "	0.05 ✓
0+30		-0.48 ✓
0+60	Break	-1.00 ✓
1 2-4/83		-1.32 ✓
2	WL Lane	-1.65 ✓
00	EL "	-1.65 ✓
0+40.92		-1.02 ✓
0+81.84	WL Walk	-0.40 ✓

Indexed

7.09
1.70
8.79

JWBP

San Juan Pl.
Seaward

4.80 / 3.99 — 5.10 / 3.69 — 5.40 / 3.39 — 5.20 / 3.59 — 0.67 / 8.12 — 0.05 / 8.74

8.69
0.10 T.P.
2.82
2.92 *

-0.48 / 3.46 — -1.00 / 3.92 — -1.32 / 0.24 — -1.65 / 4.57 — -1.02 / 3.94 — -0.40 / 3.32 / 3.38 / 0.06

Monterey Ct. Grades
Blvd. to Bay

E.L. M. Blvd.		1.00
1	3-4, 8L	0.17
2		- 0.67
3	W.L. Lane	-1.50
00	E.L. "	-1.50
	0+40.4	-0.95
	0+80.8 W.L. Walk	-0.40

Grade change 3-15-39.

E.L. M. Blvd.	1.00	
0+51 Break	- 0.40	= Sdw on N
1+07	- 1.22	-1.50 = Grade of Sdw. on South side
1+25.52 W.L. Bay.	-1,50	

Can't fix this as -1.50 is grade of Bayside Lane

Indexed B

2.97 T
4.58
-1.61 TR
4.46
2.80 T

1.00 | 0.17 | - 0.67 | -1.50 | -0.95 - 0.40
1.80 | 2.63 | 3.47 | 4.30 | 3.75 | 3.40

-1.50
5.36
3.86

-0.40 | -1.22 | -1.50
4.76 | 5.08 | 5.36
5.53
-0.17

El Carmel Pl. 7.09 / 2.12 / 9.21 / 3.98 / 5.23 / 1.65 / 6.88 x

Manhattan Ct. Grades

Strand to Bay

WL Strandway 18.5			
EL Strandway	5.30	1.58 ✓	
WL Blvd	2.10	4.78 ✓	
EL "	1.50	5.38 ✓	
1 3-40.9	0.53	6.35 ✓	
2	-0.43	7.31 ✓	
3 WL Lane	-1.40	8.28 ✓	
EL " = 0+00	-1.40	8.28 ✓	
+40.01	-0.90	7.78	
+80.02 B.S. wk.	-0.40	7.28	
80.02 Liverpool Ct			6.88 / 5.31 / 1.57 / 4.85 / 6.42 x
EL Strand	5.30	1.12 ✓	
WL Blvd.	1.60	4.82 ✓	
EL "	1.20	5.22 ✓	1.57 T.P. / 3.80 / 5.37
1 41.57	0.33	5.04	
2	-0.53	5.90	
3 WL Lane 1.08	-1.40	6.77 ✓	
EL " 0+00	-1.40	6.77 ✓	
0+40.24	-0.90	~~6.27~~ 6.33 Set	
0+80.48	-0.40	5.77 / 5.91 / 0.14 Low	

Walk

T.P. on W.L. Blvd. Liverpool

Indexed

San Louis Obispo 6.98

Lido Ct.

1.57 T.P. / 3.94 / 5.51 / 0.38 / 5.13 / 1.62 / 6.75

EL of walk	4.70	2.05 ✓
0+40	5.00	1.75 ✓
0+80 WL Strand	5.30	1.45 ✓
0 0 EL "	5.10	1.65 ✓
WL Blvd.	0.70	6.05 ✓
EL "	0.20	6.55 ✓
1	~~-0.33~~	~~7.08~~
2 44.18	~~-0.87~~	~~7.42~~
3 WL Lane 1.622	~~-1.40~~	~~8.15~~
EL "	-1.40	8.15 ✓
0+40.55	-0.90	7.65
0+81.11	-0.40	7.15 ✓

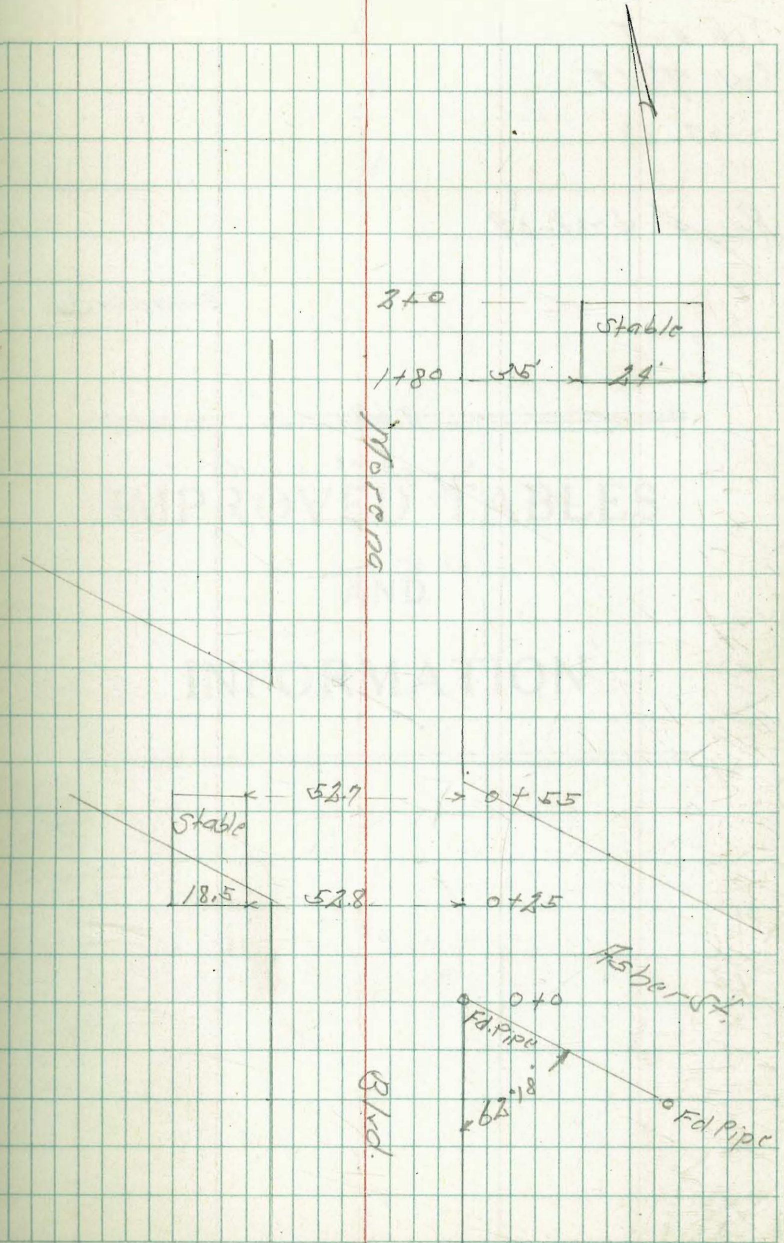
change grade to meet 3-31-39.
grade of Cem. walk on N. side 0+44

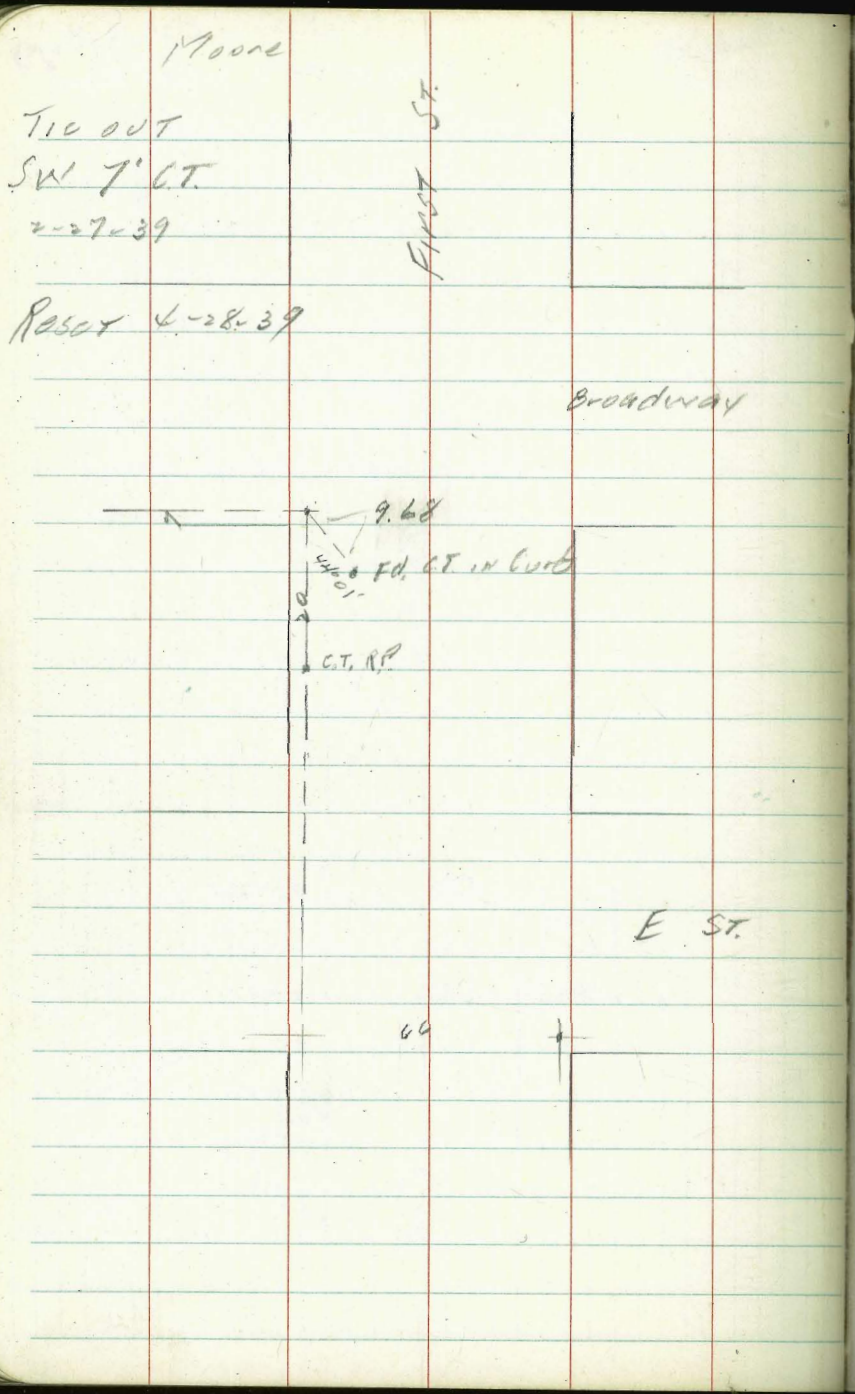
EL Blvd	0.20 ✓	-1.40 / 4.47 / 3.07 x
0+44.18 = Break	-0.60	
0+88.36	-1.00	
1+32.54 WL Lane	-1.40 ✓	

Location Stables
Kenyon Riding Club
Morena Blvd + Asher St

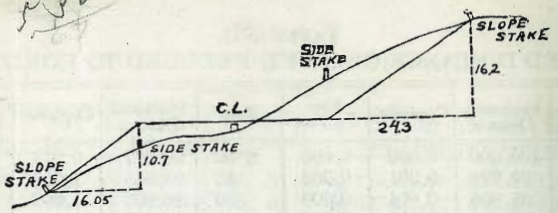
Indexed
C-5.16

Oct. 30. 39
Simson
Nortberg





IMPROVED TABLES
AND
INFORMATION



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5.10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13.65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19.35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54.15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57.75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60.15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70 65	70 80	70 95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.