



# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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# G-191

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

*San Louis Rey* } M.E.B.P.  
*MISSION BIND* } - 0.85

MICROFILMED

APR 12 1965

Wash. ST. EXT. Grader

+75

NW 8P 9th &  
UNIV.

283.76

497

+50

1° 27.27

288.73

538

283.35

2.06

285.43 X 93

**INDEXED**

W.K.

**OCT 19 1948**

9

0° 58.72

288.28 X

3.82

284.46 T.P.

4.77

289.23 X

4.77

284.46 T.P.

4.04

288.50 X

11.92

276.58

4.58

281.16

+50

0° 30.07

8

0° 01.42

7+97.51 B.C. LT.

+60

E. end of 6th St. Bridge

7+50

1

LT.

E

RT.

62  
27  
+3.5

282.11

OUT

281.91

7.3  
6.4  
+0.77.0  
3.2  
+3.2

281.51

7.7  
7.1  
+0.27.3  
4.5  
+2.8

281.72

8.0  
5.0  
+3.07.4  
5.0  
+2.4

281.14

8.1  
5.8  
+2.30.0  
0.0 ✓  
0.0

281.28

+50

$$\begin{array}{r}
 287.00 \times \\
 3.67 \\
 \hline
 283.33 \text{ T.P.} \\
 4.93 \\
 \hline
 288.28 \times
 \end{array}$$

$$\begin{array}{r}
 4.0 \\
 5.0 \\
 \hline
 -1.0
 \end{array}$$

LY.      283.04

2

RY  
OUT

2

12

$$\begin{array}{r}
 4.7 \\
 5.7 \\
 \hline
 -1.0
 \end{array}$$

283.59

$$\begin{array}{r}
 3.4 \\
 1.9 \\
 \hline
 +1.5
 \end{array}$$

+50

$$\begin{array}{r}
 4.8 \\
 4.3 \\
 \hline
 +0.5
 \end{array}$$

283.51

$$\begin{array}{r}
 4.8 \\
 3.4 \\
 \hline
 +1.4
 \end{array}$$

+20.83 F.C.    3° 05.25

11

2° 53.34

$$\begin{array}{r}
 5.2 \\
 3.9 \\
 \hline
 +1.3
 \end{array}$$

283.11

$$\begin{array}{r}
 5.2 \\
 3.3 \\
 \hline
 +1.7
 \end{array}$$

+50

2° 24.67

$$\begin{array}{r}
 5.4 \\
 3.3 \\
 \hline
 +2.3
 \end{array}$$

282.71

$$\begin{array}{r}
 5.4 \\
 3.3 \\
 \hline
 +3.3
 \end{array}$$

10

1° 56.02

$$\begin{array}{r}
 6.0 \\
 2.2 \\
 \hline
 +3.8
 \end{array}$$

284.31

$$\begin{array}{r}
 6.0 \\
 1.8 \\
 \hline
 +4.2
 \end{array}$$

LT

↓

RT

14. W. end 10th Ave. Bridge

P1  
 285.43 x  
 2.08  
 283.35 T.P.  
 3.67  
 287.02

6.6  
 4.4  
 + 0.8  
 278.86

OUT

+50

5.0  
 4.4  
 + 0.8  
 280.36

5.0  
 3.4  
 + 1.7

13

5.1  
 6.3  
 - 1.2  
 281.86

3.6  
 2.5  
 + 1.1

3-8-39

Peterbaugh St grades

S of Pringle St

INDEXED

W.K.

OCT 19 1948

	E	W
50 Pringle = 00	228.02	225.20
+ 30	222.71	220.47
+ 60	217.41	215.75
+ 90	212.10	211.02
1 + 00		209.45
1 + 20	206.80	206.30

225.29  
 3.00  
 ✓ 228.89  
 11.39  
 ✓ 217.50  
 1.22  
 ✓ 218.94  
 4.84  
 ✓ 14.12

13 CT. Pringle + Peterbaugh 225.29

4

2.05  
 227.34  
 13.20

NASH

214.14 T.P.

2.52 Post

214.66

E 228.02 22.7 17.4 12.10 206.80  
 0.87 6.7 11.5 6.8 7.9  
 3.4 7.1 7.7 11.3  
 C 2.4 C 1.4 0.9 -3.4  
 ✓ ✓

W 225.20 20.7 15.75 11.02 206.30  
 2.1 6.9 11.6 3.7 8.4  
 4.4 9.8 3.0 15.9  
 + 2.5 + 1.8 + 0.7 - 7.5  
 ✓ ✓ ✓ ✓

209.45  
 9.4  
 13.2  
 - 4.0

Pay. Alley 53 La Jolla Park

	S	N
Wly Wall	106.80	107.0
+50	106.67	
1	106.55	
+50	106.42	
2	106.30	
+50	106.17	
3	106.05	
+50	105.92	
4 Break	105.80	106.0
+20 "	105.69	105.81
+40 "	105.18	105.32
+40 "	104.19	104.60
+72.70 Pay. Ely Prospect	103.32	103.67

**INDEXED**  
WK.  
**OCT 19 1948**

105.73 SWBP Wall + Harschel 2/3/39. 5

105.73				
4.25				
111.98				
5.20				
106.78	S	4.80	4.67	6.55
4.79				6.22
111.57		5.18	5.81	5.43
4.60			5.36	5.85
104.97			0.05	6.07
3.71				6.50
108.68				6.70
	N	7.0	6.87	6.75
		4.98	5.11	4.95
			5.01	4.95
			6.10	6.78
				6.70
				6.70
	S	6.17	6.05	5.92
		5.40	5.54	5.65
		3.40	4.76	3.65
		6.0	6.78	6.0
				6.85
	N	6.37	6.25	6.12
		5.20	5.32	5.45
		4.20	4.45	4.62
		6.0	6.67	6.88
				6.40
	S	5.69	5.18	4.19
		5.88	6.39	4.49
		4.88	4.39	2.49
		6.0	6.0	3.32
				5.86
	N	5.81	5.34	4.10
		5.76	6.53	4.08
		5.48	5.27	2.88
		6.58	6.96	6.20

2 Paving Silverado

Moore  
4-4-39

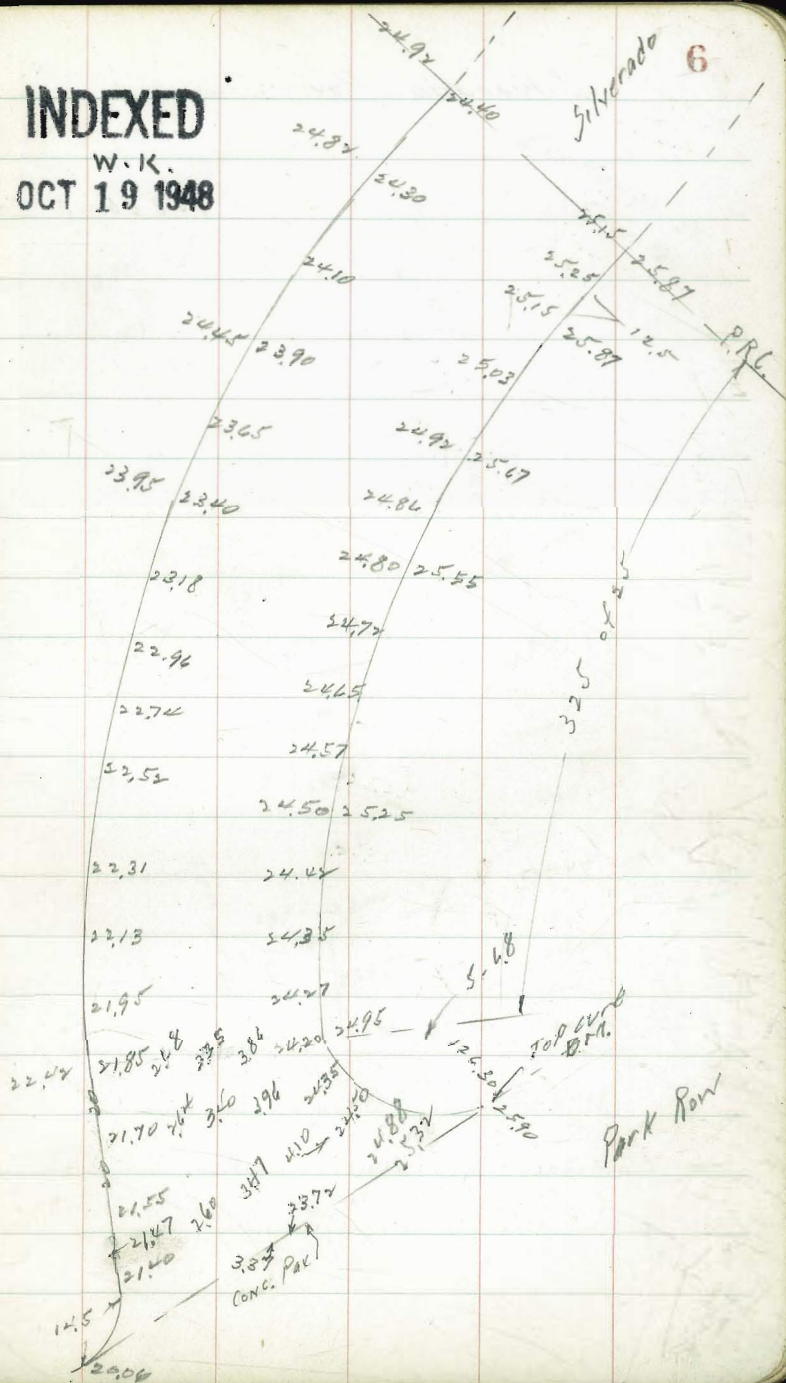
Park Row to Exchange

Silverado  
N.E. TOP curb Park Row

136.30	*
2.20	
128.50	*
3.58	
124.92	
3.94	
128.86	*

INDEXED

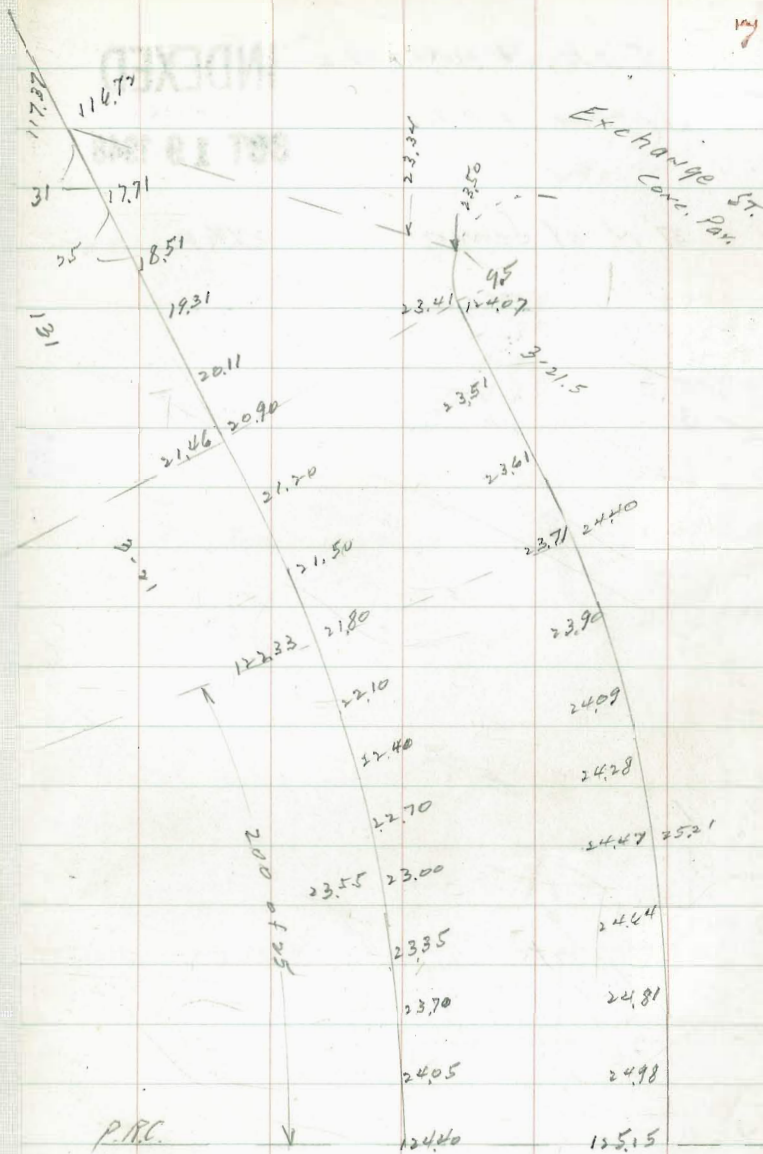
W.K.  
OCT 19 1948





Silverado Pav. 2" oil Rock

128.86 X Fwd.



5th & Wash.  
Sewer LAT.

INDEXED

W.I.C.

OCT 19 1948

# 2 37' N of Sewer 277.0

# 4 31 " " 277.70

XWBP 4th + Wash

8

284.01  
3.89  
292.90

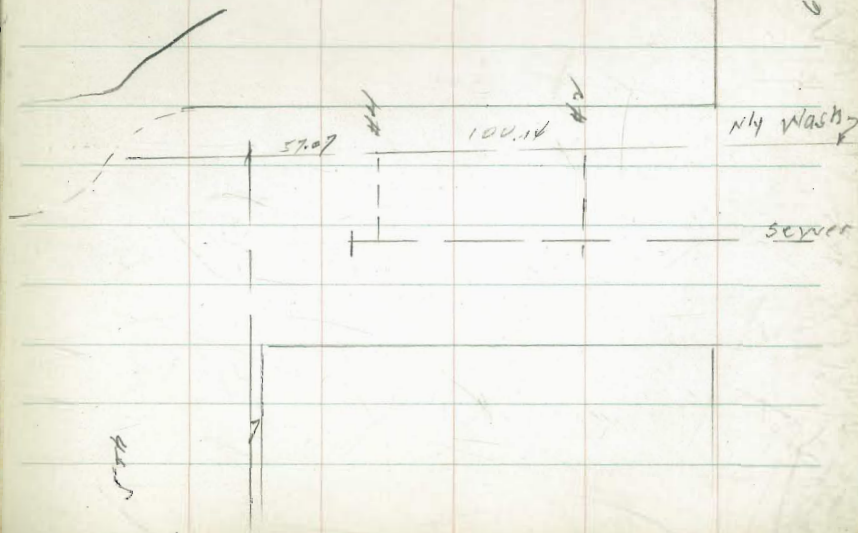
LOT 15 + 14

277.70	277.0
15.70	15.90
10.85	11.50
C 4.35	C 2.50

LOT 13 + 14

M.H. Rim = 12.10  
5.72  
17.82

274.90 = M.H. Gr.  
18.00  
17.82  
High .18 wedge



Alley grades Lot 13 U. H.  
for R.E. Holmes <sup>31</sup> No charge

INDEXED

W.K.  
OCT 19 1948

N.L. Mad.

	W	E	
	339.75	39.67	339.88 +.48 ✓
0+20	340.0		340.0
0+40	340.05		
0+70			
1	339.7		339.50
+20	339.35		339.20
+40	338.70		338.55
+55.51 Golden S.L. Gate	338.15		337.95
+76.74 " "	337.60		

339.67 E Pav  
- 0.89  
338.78

4-26-39  
Pavement

39.50	39.20	38.55	37.95
5.06	5.36	6.01	6.41
4.91	5.36	5.53	5.95
0.15	0.0	0.42	0.46

Tie PT. check

on 5th bet F & G St

on West side 5th

**INDEXED**  
W.K.  
OCT 19 1948

Moore

4-28-39

F



G

St.

200.38

Ed. C. T.  
checked 200  
5/4 of C.T.

69

150.90

314.40

Ed. C.T.

57h

Ed. C.T.

Ed. C.T. Good for line

Ed. C.T. 57

10

10

Ed. C.T. 57

Survey  $\frac{6-7}{83}$  Univ. Hous.

for Ed. Brooks

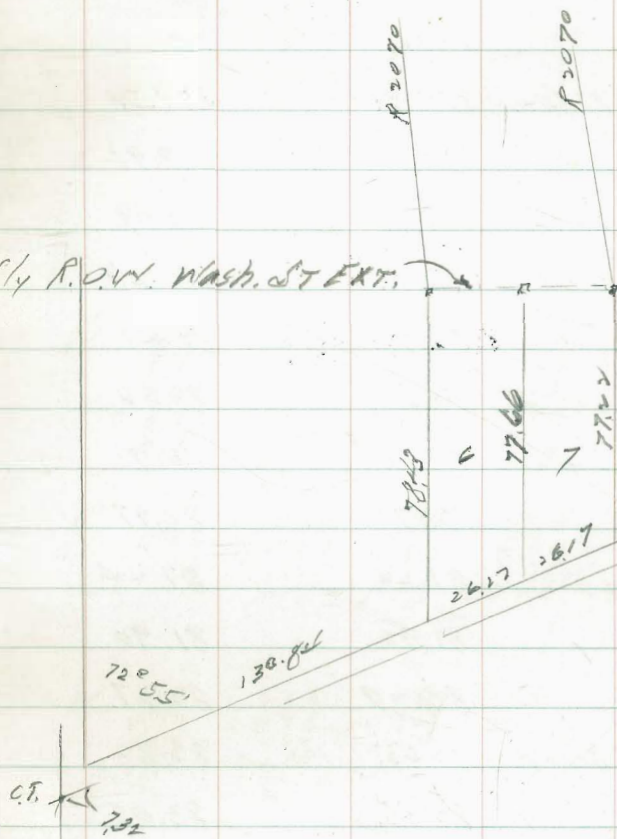
CITY P.O. & DEPT.

Moore  
5-1-39

INDEXED  
W.K.  
OCT 20 1948

11

Sly P.O.W. Wash. ST EXT.



Moore  
5-J-39 Alley Paving Griffith Co.  
Blk B Steadingworth 20' wide

	W	E
0 to N 6 El Canyon	379.52	379.74
+33.3	79.71	79.91
+66.7	79.89	80.09
1 + 100 Break	80.08	80.28
+20 "	80.21	80.41
+40 "	80.36	80.56
+60 "	80.55	80.75
1 + 80 "	80.77	80.97
2 + 20	81.24	81.44
+60	81.70	81.90
3	82.17	82.37
3 + 40 Break	82.63	82.83
+60 "	82.85	83.05
+80 "	83.05	83.25
4	83.22	83.42
4 + 20 "	83.35	83.55

P 13

SW El Canyon + 20' W

INDEXED

12

W.K.

OCT 20 1948

378.92					
<sup>8.56</sup> 387.48	W	9.52	9.11	7.87	0.08
<sup>3.24</sup> 380.82		7.96	7.77	7.59	7.40
<sup>4.64</sup> 385.50			4.27	4.18	3.40
<sup>3.57</sup> 381.93			6.75	6.01	6.10
<sup>5.28</sup> 387.61	E	9.72	9.91	0.09	0.28
<sup>3.94</sup> 383.67		7.76	7.57	7.39	7.20
<sup>6.21</sup> 389.88			6.03	3.86	3.02
			6.53	6.53	6.31
	W	0.36	0.55	0.77	1.24
		5.14	4.95	4.73	4.26
		4.97	4.50	4.19	4.03
		6.17	6.45	6.54	6.53
					TR
	E	0.56	0.75	0.97	1.44
		4.94	4.75	4.53	4.06
		4.46	3.75	3.53	3.78
		6.48	6.10	6.10	6.28
					6.55
	W	2.17	2.43	2.85	3.05
		5.44	4.98	4.72	4.56
		5.39	4.20	4.65	4.67
		6.15	6.78	6.11	6.11
					6.68
	E	2.37	2.83	3.05	3.25
		5.24	4.78	4.56	4.36
		4.66	3.78	4.14	4.11
		6.58	6.10	6.42	6.55
					6.39
	W	3.35			
		6.53			
		6.32			
		6.21			
	E	3.55			
		6.33			
		6.18			
		6.15			

	W	E
4+60	83.60	83.80
5+00	83.86	84.06
5+40 Break	84.11	84.31
+60	84.00	84.22
+80	83.77	84.05
6+00	83.14	83.53
6+07 Sky Mende	82.87	83.30

W	3.60	3.86	4.11	4.00
	<u>1.28</u>	<u>1.02</u>	<u>5.77</u>	<u>5.88</u>
	<u>6.08</u>	<u>5.75</u>	<u>5.53</u>	<u>5.10</u>
	<u>0.70</u>	<u>0.27</u>	<u>0.24</u>	<u>0.78</u>

E	3.80	4.04	4.31	4.22
	<u>1.08</u>	<u>5.87</u>	<u>5.57</u>	<u>5.66</u>
	<u>5.14</u>	<u>4.84</u>	<u>5.38</u>	<u>3.64</u>
	<u>0.46</u>	<u>0.10</u>	<u>0.19</u>	<u>0.10</u>

W	3.77	3.16	2.87
	<u>6.11</u>	<u>6.74</u>	<u>7.01</u> Par
	<u>5.24</u>	<u>5.84</u>	
	<u>0.87</u>	<u>0.90</u>	

E	4.05	3.53	3.30
	<u>5.83</u>	<u>6.35</u>	<u>6.58</u> Par
	<u>3.83</u>	<u>5.56</u>	<u>6.57</u>
	<u>0.10</u>	<u>0.79</u>	<u>0.01</u>

# INDEXED

WK.  
OCT 20 1948

Cabrillo Ave. grading & offsets

W curb grades E

Sly Pear 100	156.0	157.0	
+50	156.44 ✓	157.44 ✓	
1	156.88 ✓	157.88 ✓	
+50	157.32 ✓	158.32 ✓	
+70 Break	157.50 ✓	158.50 ✓	
+90 "	157.80 ✓	158.80 ✓	
2 +10 "	158.40 ✓	159.40 ✓	
+30 "	159.30 ✓	160.30 ✓	
+50 "	160.40 ✓	161.40 ✓	
+70 "	161.90 ✓	162.90 ✓	
+90 "	163.50 ✓	164.50 ✓	
3 +40	168.0	165.9 ✓	169.0
+50	168.85	169.85	
+70	170.35	167.7 ✓	171.35
+90	171.55	172.55	
+ Pueblo Line	172.0	169.5 ✓	173.0
+34	on oil Pav.	71.60	

5-5-39

156.00  
10.24  
166.30  
1.77  
164.53  
13.03  
177.56  
0.39  
177.17  
6.35  
183.52

	W	56.4	56.9	57.3	57.5	57.8
		9.9	7.4	9.0	8.8	8.5
		4.3	4.5	11.8	11.9	11.8
		C 0.1	F 0.1	F 2.8	F 2.1	F 3.3
	E	57.4	57.9	58.3	58.5	58.8
		8.9	8.2	8.0	7.8	7.5
		1.6	3.9	2.8	3.0	3.6
		C 7.1	C 3.5	C 5.2	C 4.8	C 3.9
	W	58.4	59.3	60.4	61.9	63.5
		7.9	7.0	5.9	4.2	2.8
		11.3	10.7	9.8	8.5	6.8
		F 3.2	F 3.7	F 3.9	F 4.1	F 4.0
	E	59.4	60.3	61.4	62.9	64.5
		18.2	17.3	16.2	14.7	13.1
		11.1	11.8	13.8	10.5	8.6
		C 7.1	C 5.5	C 2.4	C 6.2	C 4.7
	W	68.0	68.9	70.4	71.6	72.0
		1.7	2.6	7.2	6.0	5.6
		4.2	1.8	11.2	9.8	9.0
		F 3.9	F 4.4	F 4.0	F 3.8	F 3.4
	E	69.0	69.9	71.4	72.6	73.0
		8.6	7.7	12.1	10.9	10.5
		0.6	0.6	5.5	3.5	0.6
		C 8.0	C 7.3	C 6.6	C 8.4	C 9.9

14

Parl

Cabrillo

Mon

50

20

40

R.P. 2 x 2

R.P. 2 x 2



SEE  
ALSO PAGE  
17

Alley 40 La Jolla Park  
Pav. grades

	S	E	N
Ely Wall - 00	107.78	107.45	107.77
0 + 32	107.96		
0 + 40 Break	108.0	107.80	108.0
0 + 75	108.56		108.64
1 + 25	109.37		109.50
4 + 20 Break	110.90		111.20

105.73

6.34

112.07

3.47

108.60

7.96

8.0

8.56

9.37

4.45

4.59

4.07

3.51

113.05

0.0

3.47

+ 0.02

N 7.77

4.30

✓

8.0

8.62

9.50

4.07

3.45

4.34

3.45

- 0.27

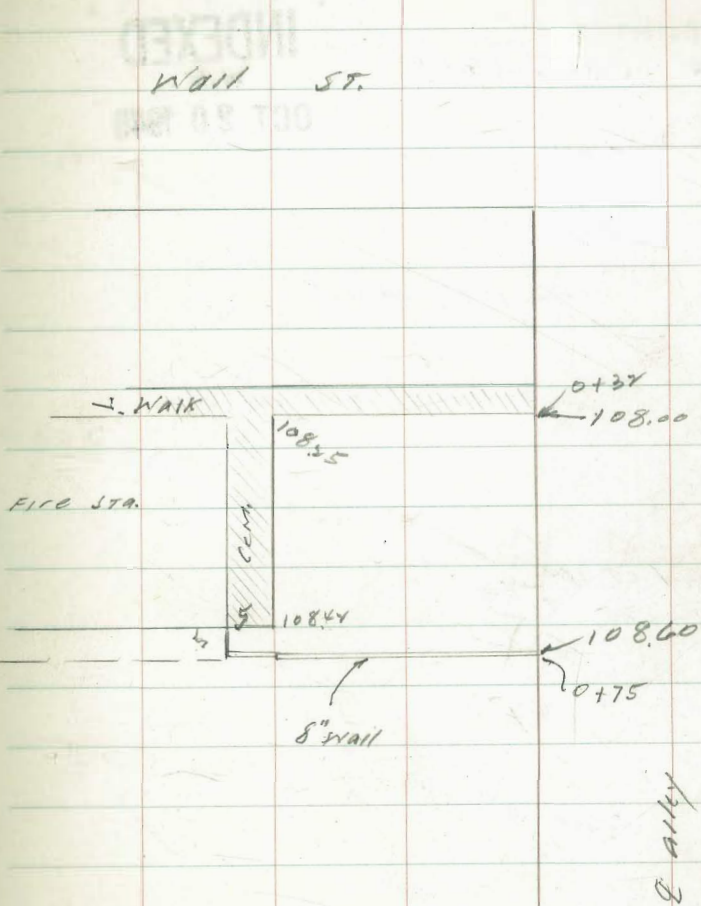
+ 1.0

INDEXED

W.K.

OCT 20 1948

15



S.S.

Alley

Bayside Walk Const.

at Allerton Ct.

NEBP 6.99 6.14

San Louis Rey  
-0.85 M. Blvd.

Avalon 5.00 1.14

Balboa Ct.

+80 0.05 Gr. 1.04

INDEXED

W.K.

OCT 20 1948

0.0

0.0

0.0 3467 Gr. 1.11

Avalon Ct. 1.04  
+80

0.0

3400

0.0

0.0

0.0

0.0

5-29-39

16

San Louis Rey

F0.8

0.0

-2.0

allerton Ct

#1

F 3.0

ch 35.09

1° 00' 40"

#2

F 2.0

2° 01' 30"

#3

#4

0.0 Mole Pier

3° 04'

#5

F 2.0

4° 04' 40"

Anacapa

#6

F 2.0

5° 03' 20"

#7

0.0

6° 04' 00"

RRE

7° 04' 00"

8° 05' 20"

SEE  
ALSO PAGE  
15

alley Pav. 40 L.J. Park, St. Dept.

	S	N
0 + 00 Ely Wall		
0 + 40 Brk	108.0	108.0
0 + 75	108.54	108.64
1 + 25	109.37	109.50
1 + 75	110.18	110.40
2 + 20 Brk	110.90	111.20
2 + 60	111.81	112.11
3 + 00	112.74	113.04
3 + 50	113.80	114.10
4 + 00	115.0	115.20
4 + 40	115.94	116.14
4 + 80 Brk	116.83	117.13
5 + 00 wh/curb	117.46	117.48

TOPWALL

67-37

17

108.10						
10.87						
118.97	S	9.37	10.18	10.90	11.81	12.72
4.10		9.64	8.81	8.09	7.18	6.27
114.87		9.90	9.11	8.37	7.48	6.57
4.17		-0.08	-0.08	-0.08	0.50	1.50
121.06						

	N	9.50	10.40	11.20	12.11	13.02
		9.49	8.59	7.79	6.88	5.97
		9.85	8.65	7.81	6.63	5.10
		0.14	-0.06	-0.02	0.02	0.87

	S	15.0	15.92	16.83	17.40
		6.00	5.14	4.23	3.60
		5.34	5.30	3.23	
		0.74	-0.16	0.10	

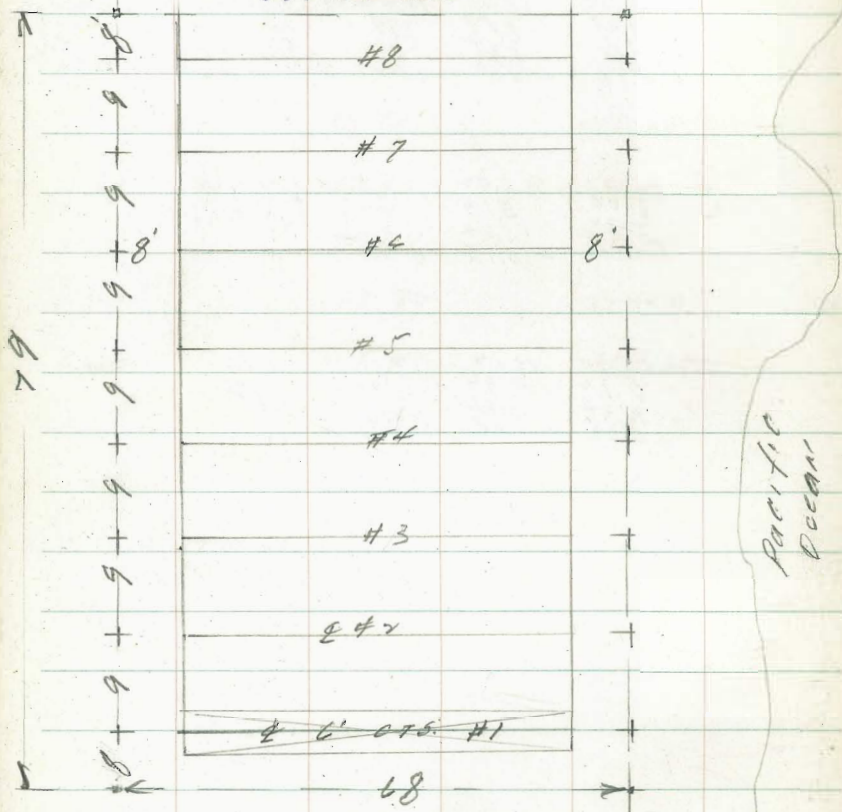
	N	15.30	16.12	17.13	17.48
		5.76	4.94	3.93	3.58
		5.38	4.84	3.81	
		0.38	0.06	0.12	

6-9-39

Shuffle Bds

La Jolla Swim Cove

INDEXED

W.K.  
OCT 20 1948B.P. B.R. SWIM  
COVE  
S'N. FH.

18

	ELY	WH	
#1	23.15 <u>4.65</u> 3.90 C 0.64	4.55 <u>5.73</u> -1.18	27.66 4.38 32.04 8.52 23.52 4.18 27.70
#2	23.20 <u>4.80</u> 3.74 C 0.74	4.50 <u>5.07</u> -0.57	
#3	23.25 <u>4.48</u> 3.81 C 0.64	4.45 <u>4.81</u> -0.36	
#4	23.30 <u>4.40</u> 3.96 C 0.46	4.40 <u>4.82</u> -0.42	
#5	23.35 <u>4.35</u> 3.57 C 0.78	4.35 <u>4.71</u> -0.36	
#6	23.40 <u>4.30</u> 3.56 C 0.74	4.30 <u>4.65</u> -0.35	
#7	23.45 <u>4.25</u> 3.31 C 0.94	4.25 <u>4.82</u> -0.57	
#8	23.50 <u>4.20</u> 3.11 C 1.09	4.20 <u>4.45</u> -0.25	

23.25  
4.55  
27.80

S	24.60 <u>3.20</u> 5.88 <u>-2.68</u> 3.20 5.13 <u>-1.93</u>	24.57 <u>3.22</u> 5.88 <u>-2.64</u> 3.20 5.08 <u>-1.97</u>	24.54 <u>3.26</u> 4.52 <u>-1.50</u> 3.26 5.87 <u>-1.61</u>	24.50 <u>3.30</u> 4.30 <u>-1.06</u> 3.30 5.21 <u>-1.91</u>
N				

INDEXED

W.K.

OCT 20 1948

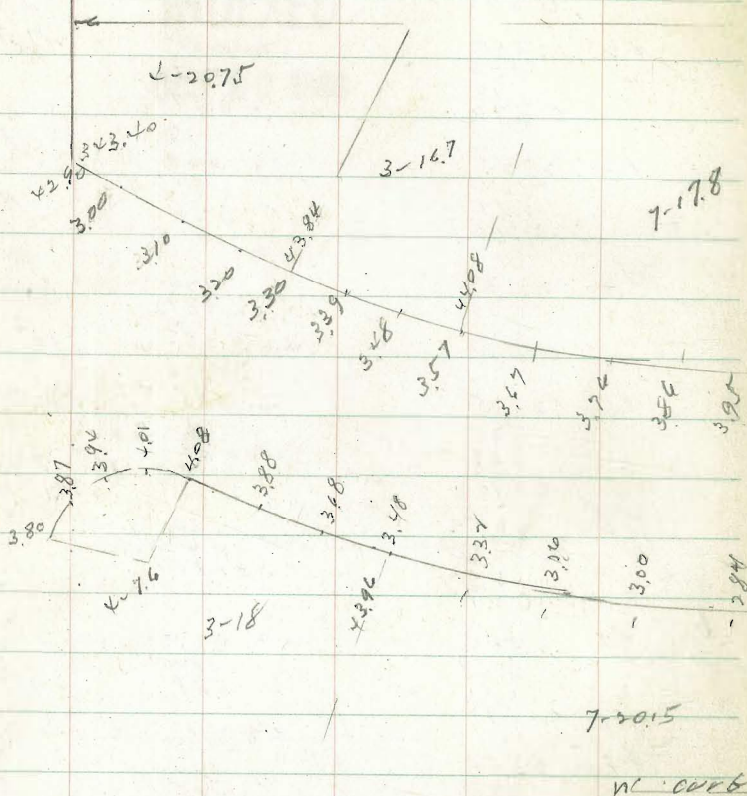
POV. MISSION AVE

Madison to Texas

1140.  
SEBP LA

342.31  
2.15  
348.46

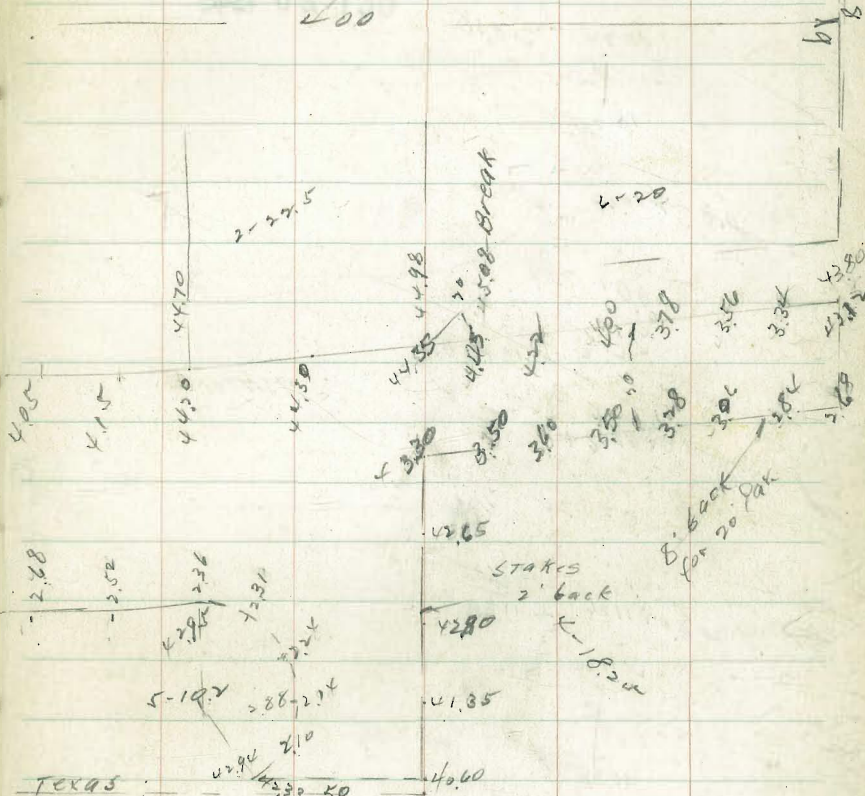
Madison



7-18-39

by St. Dept.

100



846	846	846	846	846	846
380	370	370	370	370	388
476	476	498	570	570	570
10.10	+0.2	+0.90	+0.35	507	60.60
		+0.30	+0.05		
466	846		42.85	42.10	41.35
10.2	340		5.61	6.86	7.11
	570	-0.5	6.31	7.06	7.61
	0.80		0.74	0.80	0.50
			0.5	0.6	



8-2-39

Set curb stakes for 10' sidewalk

N. Side Roseland Dr. opposite Hypatia Dr

**INDEXED**

ob grade

B.C. = 00

W.K.

OCT 20 1948

53.23 Not Set

0 + 26 Ely Grandall line 51.29

0 + 70.67 = Break = E <sup>edge</sup> gar. 49.68

0 + 86.24 Wedge gar. 49.03

1 + 23.24 47.48

1 + 60.24 Wly Grandall line 45.93

1 + 66.26 = Break 45.68 Not Set

Note! Grades set are  
4 ft below Glover Profile

37.38

SE BP Spindrift T Newport

0.36

37.74

5.08

32.66

12.68

45.34

0.20

45.14

9.38

54.52

10' Cor. approx  
edge = 1 + 45.24  
OR LINE

45.14  
9.67  
54.81

51.29	49.68	49.03
35	5.13	5.78

47.48	45.93
7.33	8.88

9.67  
44.90 = El Wedge 20' Cor approx

5.67  
48.90 El. Edge Grandall gar. fl. 3' back  
fl. Level  
= 0 + 70.67

45.14					
8.21					
53.35	51.29	49.68	49.03	47.48	45.93
	4.06	3.67	4.32	5.87	7.14

Reset 4-16-40.  
Moore

Cedar St Grades  
Pac. to Cal.

**INDEXED**  
W.K.  
**OCT 20 1948**

00 = Ek. Pac. 5.06 N 06

9.07

0 + 12 E.C. 06. 5.50 4.83 5.50

0 + 50 7.28

1 + 00 9.62

+ 50 11.96

2 W.K. Cal. 14.30 13.43 14.30

+ 50 B 15.73 15.92

4.94  
8.47  
13.41  
1.20  
17.81  
6.84  
18.65

B.M. C.T. P.I. Pac. & Cedar.

22

S	5.50	7.28	9.62	11.96	14.30
	7.91	6.13	3.8	1.05	4.4
	7.93	5.4	3.8	0.45	3.4
	LOW .02	+ 0.7	0.0	+ 1.0	+ 1.0
				nd	nd

N	7.91	6.13	3.8	4.7	4.4
	7.90	7.0	3.8	7.2	5.6
	LOW .06	- 0.9	0.0	- 0.5	- 1.1

	4.94	
	10.18	
S	15.73	15.12

	2.9					
	3.7					
	- 0.8					
		5.50	7.28	9.62	11.96	14.30
		9.62	7.82	5.50	3.16	0.82

N	15.92
	2.7
	3.6
	- 0.9

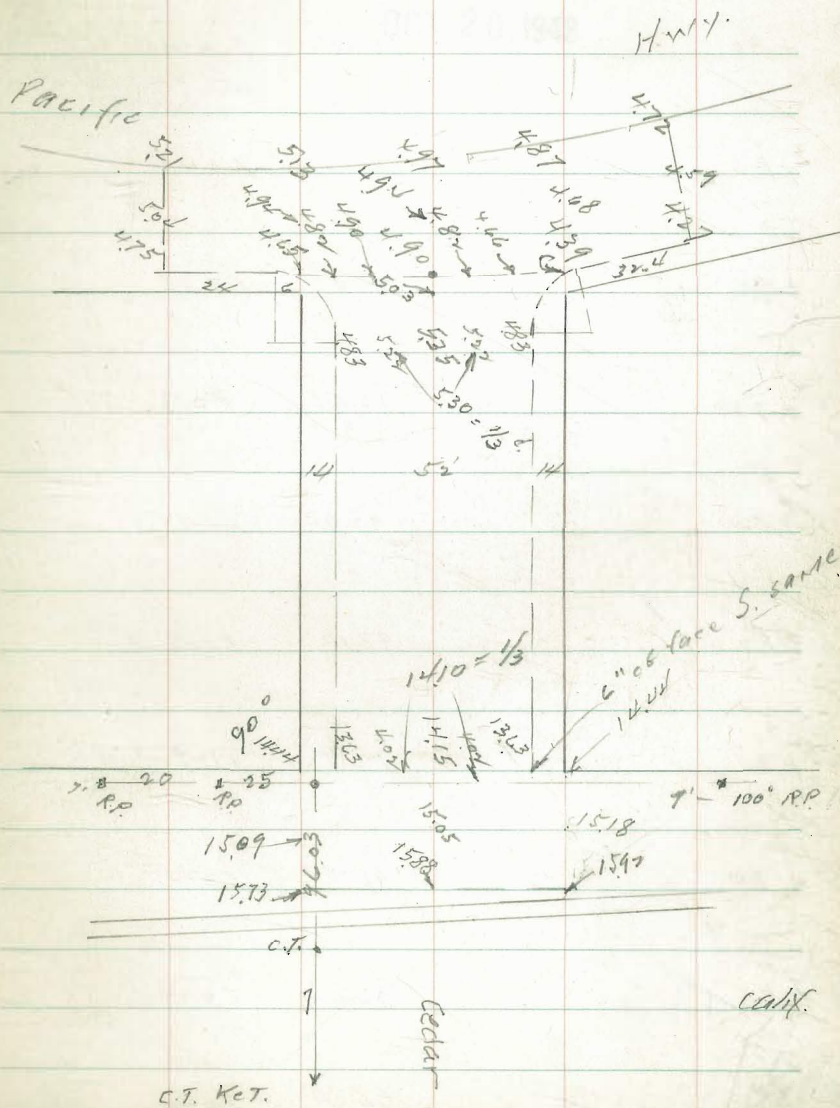


Cedar Pav grades

P.I. C.T. B.M. 494

12.30
17.52

4.94
3.85
8.77



8-14-39

S. side Pershing Dr.

00 = P.C.C.	91.34	C045
+ 30	91.88	C063
+ 60	92.33	C046
+ 90	92.61	F0.53
1 + 20	92.56	F0.33
1 + 50	92.94	C043
1 + 80 = F.C.	93.13	F107
+ 30	94.30	F129
+ 80	95.10	F020
3 + 30	96.04	C034
3 + 80	96.80	F040

68.07 N.E.B.P. 18th + B. Str.

24

12.23	
80.80	
0.13	
80.17	
12.45	
92.62	E 06 18th
2.50	
90.12	P.C.B. Part Line
90.15	
99.46	
3.94	
95.54	B.M. Nail 5100
2.12	Acc Pole
97.66	

INDEXED

WK

OCT 20 1948

N side Pershing Dr. widening

00 + 80 C.

91.28

+0.90

0 + 28

92.31

-0.18

0 + 56

92.96

+0.06

0 + 84

93.68

+1.03

1 + 12

94.20

+1.05

1 + 40

94.60

+0.05

1 + 68

94.71

-0.20

1 + 96

94.46

+0.48

2 + 24 = E.C.

94.20

+0.10

2 + 54

94.20

+0.36

INDEXED  
WK  
OCT 20 1948

2 + 84	94.00	+ 0.00	99.00 x
3 + 14	94.26	+ 0.40	
3 + 44 = BC. 38	94.60	+ 1.08	
3 + 82	94.80	+ 0.80	
4 + 20	95.04	- 0.09	97.40 x
4 + 58	94.74	- 0.50	
4 + 96 38	94.16	- 0.31	
5 + 34	93.41	- 0.14	
5 + 72	94.66	+ 0.79	
6 + 10	94.76	- 0.03 ✓	
6 + 48	94.96	0.0 ✓	

50700	4 + 38	44" Con. pipe C/W. Fl.	
	Wedge Par. etc	E. edge Par. 0 + 58	0 + 88
	89.0	87.9	86.40
	8.9	10.0	11.5
	4.1	4.4	3.6
	C 7.8	C 5.6	C 7.9
			85.0
			12.9
			9.0
			C 3.9

				97.46 X 5.93	
6 + 86	✓ 93.24	+ 0.55	91.73 =	92.42	97.92 X
			0.69		
7 + 2X E.C.	✓ 93.06	- 0.5X			
7 + 66	✓ 92.56	0.0			
8 + 08	✓ 92.30	0.0			
8 + 50	✓ 91.86	0.0			
8 + 92	✓ 91.46	- 0.15			
9 + 34	✓ 90.96	0.0			
9 + 76	✓ 90.56	- 0.00			
10 + 18	90.00	- 0.30			
10 + 60	89.10	- 0.30			
11 + 02	88.30	- 0.20			

COULD RECT  
SPINWAY

11 + 44 = B.C.

87.30 + 0.30

11 + 77.4

86.75 + 0.25

12 + 107

86.15 + 0.40

12 + 44 = E.C.

85.75 + 0.40

12 + 94

85.30 + 0.74

13 + 44

84.80 + 0.20

13 + 94

84.72 + 0.74

14 + 44

84.75 + 0.42

14 + 94

84.95 - 0.15

15 + 44

85.35 - 0.70

		N	
15 + 90		85.70	-0.50
16 + 30		85.93	-0.27
		Sly w/ of Bridge	
0.0	width 0.0	87.63	-0.2
+50	1.5	84.87	-0.4
1	2.2	85.87	-7.4
+50	2.0	85.20	-6.7
2	2.7	85.0	-7.3
+50	2.6	84.90	-7.1
3	2.5	84.75	-6.3
+50	2.3	84.54	-4.7
4	2.2	84.67	-4.0
+50	2.2	84.70	-4.3
5	5.4	85.04	+1.0
+33	5.0	Wend Bridge 85.00	0.0
+76	4.8	86.10	0.0
4	4.5	86.20	+0.4
+50	3.1	86.04	+0.1
7	0.0	87.07	-0.1

23

~~88.95~~  
~~2.57~~  
~~91.47~~

88.82  
 2.29  
 91.11  
 1.27  
~~89.84~~

89.98 B.M. S.P. SE Cap of Cobble Bridge

8-1-39

Bridge Ely  
Perching Widening

width x/y

00 0.0 85.96 -0.10

0+54 W. end Bridge v. 85.94 0.0

1+00 E " " 37 86.15 0.0

250 58 86.13 +0.9

v 7.8 86.35 +1.0

+53 B.L. LT. 10

v +90 11

3+27 12

3+66 13

4+01 14

89.84

127

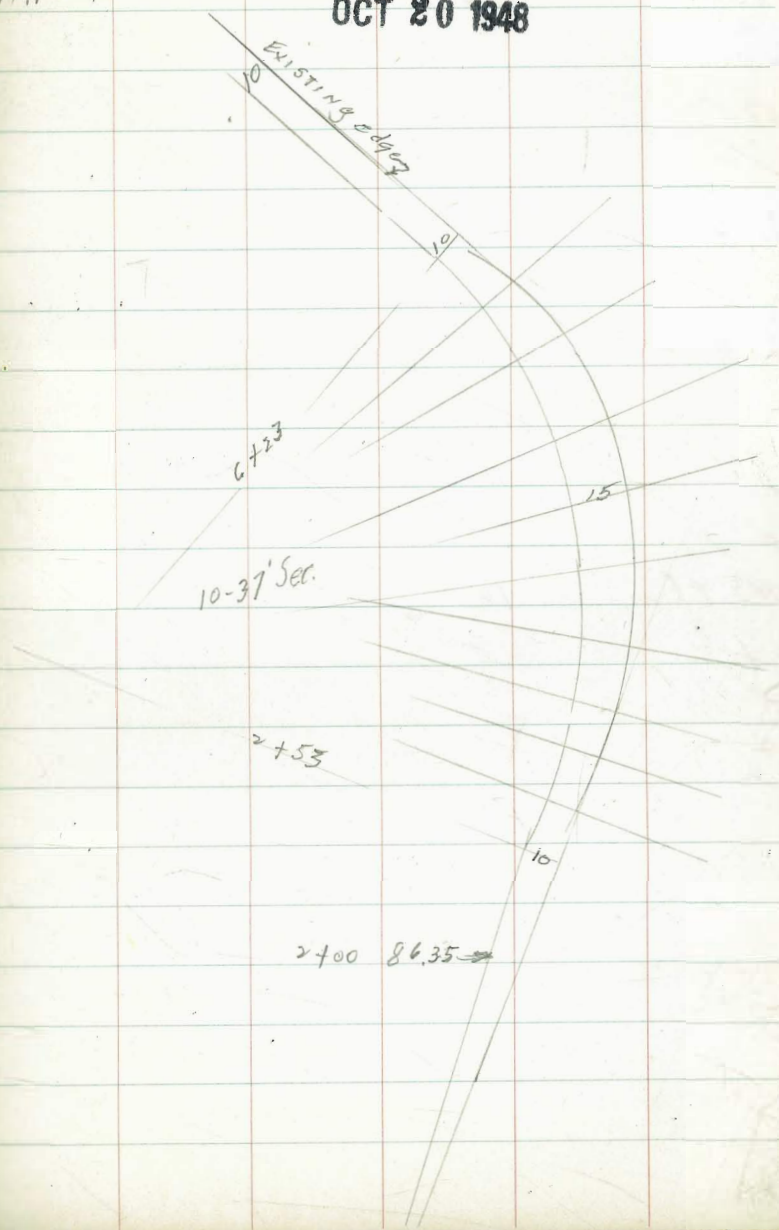
91.11 \*

INDEXED

W.K.

OCT 20 1948

30





width

4+38

15

37

4+75

14

5+12

13

5+49

12

5+86

11

6+23 EC

10









The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. The right page is numbered '36' in the top right corner. The notebook has rounded corners and a dark cover is visible around the edges. The pages are otherwise blank.







INDEXED  
OCT 20 1930

8-17-39

Alley Blk 20 U.H. Pav. Dennis Co

	W	E
0 + 00 N.M.Tad.	341.0	341.15
+ 20 Break	42.55	42.32
+ 40 "	43.37	43.32
+ 60 "	43.94	43.94
1	44.81	
+ 50	45.91	
✓ Break	47.00	47.00
+ 40	47.74	
+ 80	48.45	
3 + 20	49.18	
3 + 40 Break	49.91	49.91
+ 80 "	50.25	
4	50.54	
+ 30 "	50.78	
+ 40 "	50.97	
+ 60 "	51.12	
4 + 80 "	51.22	51.22

**INDEXED**

W.K.

**OCT 20 1948**

over

340.06 SE. MAD. + MISS.

	W	E
340.06	41.60	42.55
340.31	42.37	43.27
340.37	42.90	43.90
340.44	43.81	44.81
340.51	44.72	45.72
340.58	45.63	46.63
340.65	46.54	47.54
340.72	47.45	48.45
340.79	48.36	49.36
340.86	49.27	50.27
340.93	50.18	51.18
341.00	51.09	52.09
341.07	52.00	53.00
341.14	52.91	53.91
341.21	53.82	54.82
341.28	54.73	55.73
341.35	55.64	56.64
341.42	56.55	57.55
341.49	57.46	58.46
341.56	58.37	59.37
341.63	59.28	60.28
341.70	60.19	61.19
341.77	61.10	62.10
341.84	62.01	63.01
341.91	62.92	63.92
341.98	63.83	64.83
342.05	64.74	65.74
342.12	65.65	66.65
342.19	66.56	67.56
342.26	67.47	68.47
342.33	68.38	69.38
342.40	69.29	70.29
342.47	70.20	71.20
342.54	71.11	72.11
342.61	72.02	73.02
342.68	72.93	73.93
342.75	73.84	74.84
342.82	74.75	75.75
342.89	75.66	76.66
342.96	76.57	77.57
343.03	77.48	78.48
343.10	78.39	79.39
343.17	79.30	80.30
343.24	80.21	81.21
343.31	81.12	82.12
343.38	82.03	83.03
343.45	82.94	83.94
343.52	83.85	84.85
343.59	84.76	85.76
343.66	85.67	86.67
343.73	86.58	87.58
343.80	87.49	88.49
343.87	88.40	89.40
343.94	89.31	90.31
344.01	90.22	91.22
344.08	91.13	92.13
344.15	92.04	93.04
344.22	92.95	93.95
344.29	93.86	94.86
344.36	94.77	95.77
344.43	95.68	96.68
344.50	96.59	97.59
344.57	97.50	98.50
344.64	98.41	99.41
344.71	99.32	100.32
344.78	100.23	101.23
344.85	101.14	102.14
344.92	102.05	103.05
344.99	102.96	103.96
345.06	103.87	104.87
345.13	104.78	105.78
345.20	105.69	106.69
345.27	106.60	107.60
345.34	107.51	108.51
345.41	108.42	109.42
345.48	109.33	110.33
345.55	110.24	111.24
345.62	111.15	112.15
345.69	112.06	113.06
345.76	112.97	113.97
345.83	113.88	114.88
345.90	114.79	115.79
345.97	115.70	116.70
346.04	116.61	117.61
346.11	117.52	118.52
346.18	118.43	119.43
346.25	119.34	120.34
346.32	120.25	121.25
346.39	121.16	122.16
346.46	122.07	123.07
346.53	122.98	123.98
346.60	123.89	124.89
346.67	124.80	125.80
346.74	125.71	126.71
346.81	126.62	127.62
346.88	127.53	128.53
346.95	128.44	129.44
347.02	129.35	130.35
347.09	130.26	131.26
347.16	131.17	132.17
347.23	132.08	133.08
347.30	132.99	133.99
347.37	133.90	134.90
347.44	134.81	135.81
347.51	135.72	136.72
347.58	136.63	137.63
347.65	137.54	138.54
347.72	138.45	139.45
347.79	139.36	140.36
347.86	140.27	141.27
347.93	141.18	142.18
348.00	142.09	143.09
348.07	143.00	144.00
348.14	143.91	144.91
348.21	144.82	145.82
348.28	145.73	146.73
348.35	146.64	147.64
348.42	147.55	148.55
348.49	148.46	149.46
348.56	149.37	150.37
348.63	150.28	151.28
348.70	151.19	152.19
348.77	152.10	153.10
348.84	153.01	154.01
348.91	153.92	154.92
348.98	154.83	155.83
349.05	155.74	156.74
349.12	156.65	157.65
349.19	157.56	158.56
349.26	158.47	159.47
349.33	159.38	160.38
349.40	160.29	161.29
349.47	161.20	162.20
349.54	162.11	163.11
349.61	163.02	164.02
349.68	163.93	164.93
349.75	164.84	165.84
349.82	165.75	166.75
349.89	166.66	167.66
349.96	167.57	168.57
350.03	168.48	169.48
350.10	169.39	170.39
350.17	170.30	171.30
350.24	171.21	172.21
350.31	172.12	173.12
350.38	173.03	174.03
350.45	173.94	174.94
350.52	174.85	175.85
350.59	175.76	176.76
350.66	176.67	177.67
350.73	177.58	178.58
350.80	178.49	179.49
350.87	179.40	180.40
350.94	180.31	181.31
351.01	181.22	182.22
351.08	182.13	183.13
351.15	183.04	184.04
351.22	183.95	184.95
351.29	184.86	185.86
351.36	185.77	186.77
351.43	186.68	187.68
351.50	187.59	188.59
351.57	188.50	189.50
351.64	189.41	190.41
351.71	190.32	191.32
351.78	191.23	192.23
351.85	192.14	193.14
351.92	193.05	194.05
351.99	193.96	194.96
352.06	194.87	195.87
352.13	195.78	196.78
352.20	196.69	197.69
352.27	197.60	198.60
352.34	198.51	199.51
352.41	199.42	200.42
352.48	200.33	201.33
352.55	201.24	202.24
352.62	202.15	203.15
352.69	203.06	204.06
352.76	203.97	204.97
352.83	204.88	205.88
352.90	205.79	206.79
352.97	206.70	207.70
353.04	207.61	208.61
353.11	208.52	209.52
353.18	209.43	210.43
353.25	210.34	211.34
353.32	211.25	212.25
353.39	212.16	213.16
353.46	213.07	214.07
353.53	213.98	214.98
353.60	214.89	215.89
353.67	215.80	216.80
353.74	216.71	217.71
353.81	217.62	218.62
353.88	218.53	219.53
353.95	219.44	220.44
354.02	220.35	221.35
354.09	221.26	222.26
354.16	222.17	223.17
354.23	223.08	224.08
354.30	223.99	224.99
354.37	224.90	225.90
354.44	225.81	226.81
354.51	226.72	227.72
354.58	227.63	228.63
354.65	228.54	229.54
354.72	229.45	230.45
354.79	230.36	231.36
354.86	231.27	232.27
354.93	232.18	233.18
355.00	233.09	234.09
355.07	234.00	235.00
355.14	234.91	235.91
355.21	235.82	236.82
355.28	236.73	237.73
355.35	237.64	238.64
355.42	238.55	239.55
355.49	239.46	240.46
355.56	240.37	241.37
355.63	241.28	242.28
355.70	242.19	243.19
355.77	243.10	244.10
355.84	244.01	245.01
355.91	244.92	245.92
355.98	245.83	246.83
356.05	246.74	247.74
356.12	247.65	248.65
356.19	248.56	249.56
356.26	249.47	250.47
356.33	250.38	251.38
356.40	251.29	252.29
356.47	252.20	253.20
356.54	253.11	254.11
356.61	254.02	255.02
356.68	254.93	255.93
356.75	255.84	256.84
356.82	256.75	257.75
356.89	257.66	258.66
356.96	258.57	259.57
357.03	259.48	260.48
357.10	260.39	261.39
357.17	261.30	262.30
357.24	262.21	263.21
357.31	263.12	264.12
357.38	264.03	265.03
357.45	264.94	265.94
357.52	265.85	266.85
357.59	266.76	267.76
357.66	267.67	268.67
357.73	268.58	269.58
357.80	269.49	270.49
357.87	270.40	271.40
357.94	271.31	272.31
358.01	272.22	273.22
358.08	273.13	274.13
358.15	274.04	275.04
358.22	274.95	275.95
358.29	275.86	276.86
358.36	276.77	277.77
358.43	277.68	278.68
358.50	278.59	279.59
358.57	279.50	280.50
358.64	280.41	281.41
358.71	281.32	282.32
358.78	282.23	283.23
358.85	283.14	

	W	F
5+20	51.36	51.34
5+60 Break	51.51	51.47
+80 "	51.58	51.53
6 S.L. Adams "	351.65	351.48

	W	F	PAY.
	51.36	51.51	51.65
	5.29	5.14	5.00
	4.73	4.47	5.00
	C 0.56	C 0.72	C 0.95
			0.02 F
	51.34	51.47	51.53
	5.31	5.18	5.17
	5.27	4.91	4.80
	C 0.04	C 0.27	C 0.34
			5.17
			0.00 Pay

4+97.5 Sewer hat. <sup>W.L.</sup> #1 346.28  
 10.37  
 5.14  
 C 5.23

~~4+100 " " E.W. #2 345.65~~  
~~4+22 Sewer W 9.48~~  
~~4.91~~  
~~C 4.57~~  
 #2 already in.

INDEXED

BAR 03 100

20' Alley Pav. Blk 7 La Jolla Park

Bet. Fay & Girard. Pearl Sly to P.L.

W E

00 Sly Pearl 111.12 110.93 111.30

0 + 20 Break 112.50 112.50

0 + 40 " 113.50 113.50

0 + 70 114.62 0.13  
114.75

1 + 00 115.75 0.25  
116.0

+ 50 117.62 0.46  
118.08

~ 119.50 0.67  
120.17

+ 50 121.37 0.88  
122.25

2 + 85 123.25 1.08  
124.33

3 + 50 125.13 1.30  
126.42

4 = Pueblo Line 127.00 1.50  
128.50

124.33

42

124.75

130.11 x

5.36

4.04

EL. 3710

F 0.68 on 1' Cent Walk

INDEXED

W.K.

OCT 20 1948

2 do. 99.  
cent. fl.

6.41

6.21

0.0

2" Oil Rock by St. Dept.

3" dip on E

11517 5282 Pearl & Girard

11517	W 111.12	112.50	113.50	114.75	116.0
9.73		12.40	11.40	10.15	8.90
124.90		11.50	10.88	9.15	8.04
3.35		C 0.90	C 0.55	C 0.70	C 0.80
171.65				C 1.13	C 1.13
8.46					
130.11					

E 111.23	112.50	113.50	10.15	8.90
	12.40	11.40	9.10	7.12
	11.27	9.59	C 1.05	C 1.80
	C 1.13	C 1.81	1.18	C 3.05

W 118.08 120.17 122.25 124.33

6.82 4.73 4.65 5.78

5.56 4.16 2.88 6.50

C 0.70 C 0.57 F 0.73 F 0.77

C 1.73 C 1.24 C 0.65 C 0.86

E 6.82 4.73 2.65 5.78

6.82 3.73 3.75 6.34

C 0.50 C 0.70 F 0.60 F 0.56

C 0.96 C 1.67 C 0.28 C 0.53

W 126.42 128.50

3.69 1.61

5.37 1.31

F 4.68 C 0.30

F 0.38 C 1.80

E 3.69 128.50

5.29 1.61

F 4.60 2.05

F 0.30 F 0.40

C 1.06

Moore  
8-28-39 42



Overlook HTS

9-20-39

Lot 2 to 9 Incl. BIRB

Solar 57

Cushman 4  
S. C. Brownell

N.C.B.

206.86 X

00 = W/Ly Lot 2	186.30	F 0.90	F 0.4	194.38 12.08 1.11
0 + 36.21	182.40	F 1.13	F 0.63	195.49 1.207
0 + 56.21	180.98	F 0.80	F 0.26	183.42 5.37
0 + 76.21	179.82	F 0.87	F 0.27	188.79 X 1.17
0 + 96.21	179.40	F 0.50	0.00	187.62 X.P. 11.57
1 + 16.21 179.45	179.62	F 0.88	0.01	199.19 1.37
1 + 36.21 P.C. 16	180.50	F 0.45	F 0.75	197.82 X.T.P. 8.37
1	181.50	F 1.04	F 0.99	06.19
2 ob. R = 30	182.90	F 0.83		
3 Parts	184.35	F 0.93		
4 Cushman EC = 0400	185.80	F 0.77		
0 + 55 N.C.B.	191.70	F 0.50		
1 + 10	197.60	F 0.45		
1 + 30	199.60	F 0.88		
1 + 50 P.C. 16	201.35	F 0.98		
1	202.45	F 0.60		
2	203.55	F 0.86		
3	204.30	F 0.98		
3 1/2	204.40	F 0.84		
4 EC Solar	204.30	F 0.80		
				= 0400

S. C. Brownell

44

INDEXED

W.K.

OCT 20 1948

0400 EC	204.30		
0 + 50	203.10		
1	201.90	F 0.62	
+ 50	200.70	F 0.88	
P.C. 16	+ 07.52	199.36	C 0.12
1		198.87	C 1.0
2		198.32	C 1.06
3		197.66	C 1.01
4		197.0	C 0.82
P.C. Elev. Rd.	+ 17.80	196.35	C 0.54
S.L. Lot 9	47.3	194.62	F 0.19
	44.77	192.96	F 0.63
B.C.	44.77	191.30	F 0.75
1		190.89	F 0.81 F 0.77
2		190.32	F 0.64 F 0.85
3		189.43	F 0.77 F 0.44
4 EC		188.47	F 0.85 F 0.35

Plainview Rd.  
Everview to Cushman

N 66

195.12 X

BC	183.90 ✓ F.58
1 7°30'	185.52 ✓ F.55
2 15°00'	187.15 ✓ F.62
3 22°30'	188.66 F0.20
4 30°00'	190.17 ✓ F0.14
5 37°30'	191.41 ✓
6 E.C. 45°00' = 0400	192.65 ✓ C0.27
0+30	193.94 ✓ C.42
0+50	194.68 ✓ C.24
0+70	195.32 ✓
0+90	195.83
1+10 E.V.C.	196.30
1+50	✓ 197.0 ✓
2+00	✓ 197.88 ✓
2+30 P.V.C.	✓ 198.40 ✓
+50	✓ 198.80 ✓
+70	✓ 199.30 - F0.05
+90	✓ 199.90 ✓ F0.36
3+10	✓ 200.60 ✓ F0.50
3+30	✓ 201.40 ✓ F0.96

B11.

201.48

4.13

205.61 X

0.68

204.93 4.2

11.49

216.42 X

INDEXED

WK

N 66.

OCT 20 1948

3+50 E.V.C.

✓ 202.25 ✓ F0.71

4+00

204.55 ✓ C 0.38

+50

206.84

5

209.14

+30

210.52

5+60 P.V.C.

211.90 ✓

+80

212.70 ✓

6

213.30 ✓ F0.07 ✓

+20

213.70 ✓ F0.14 ✓

+40

213.90 ✓ F0.24 ✓

+60

213.80 ✓ F0.30 ✓

6+80 E.V.C.

213.55 ✓ F0.37

7

213.20 ✓ F0.37

LOT 7+8 BIK 9 on Plainview  
S 66

P.C. + 87.8

211.90 F.54

212.70 F.65

5-20

213.30 F0.5

213.70 F0.05

213.90 F0.54

213.80 F0.14

45

KNOX ST. AT EVERVIEW

	N 66		182.60 TP
			2.03
BC	182.15	F 0.30	185.23
1	81.23	F.17	
2	80.45	F.13	
3	79.70	F.30	
4 E.C. 200	79.10	C 0.08	
+ 16.5	78.40	C .35	
+ 36.5	77.30	C.87	
+ 56.5	75.40	C 1.12	
+ 86.5	72.0	C 0.97	

INDEXED  
WK  
OCT 20 1948

ONSTAD ST.  
W of EVERVIEW

LOT 7 BIK 6

5 66

	170.47	F 0.70	- .60
BC	173.50	F 1.12	- 1.14
1	174.65	F 1.28	- 1.41
2	175.0	F 0.97	- 1.15
3	174.27	F 0.86	- 1.0
4 E.C. 200	173.0	F 0.65	
0 + 25	170.57	F 0.65	171.07 F 0.09
0 + 75 = W. 6.7	165.74	F 0.91	166.24 F 0.7

OK.

OK

177.64 BM 80  
1.34 N 20  
178.98 ONSTAD  
EVERVIEW

INDEXED  
WK  
OCT 20 1948  
N 66



N E COR Elev + Brownell

LOT 1 BIK 9

206.89x

B.C.	202.15	0.0
1	201.67	0.18
2	201.20	0.31
3	200.76	0.40
4 E.C. = 0+100	200.48	0.20
0 + 13.06	200.35	0.47
0 + 23.00	200.30	0.20
0 + 33.06	200.35	0.17
0 + 37.81 = E+ LOT 1	200.50	0.08
0 + 43.06	200.70	0.17
0 + 53.06 EYC	201.21	

INDEXED  
WK  
OCT 20 1948

1544-3  
B.M. E.H. 6  
201.48  
528  
206.84x

LOT 5 BIK 9

INDEXED  
WK  
OCT 20 1948  
- 37.81 W.L. 5

B.C.	203.83	F 0.05
1	204.70	F 0.13
2	205.15	F 0.30
3	205.84	F 0.24
4 E.C.	206.50	F 0.25
0 + 20	207.20	F 0.28
0 + 40	208.20	F 0.15
0 + 60	209.10	F 0.13
0 + 75	209.95	F 0.36
0 + 75 = NW LOT 5	210.50	F 0.35

216.42x  
12.94  
203.48 TR  
3.43

E Align.

S. Side Solar St. 190.73

48

curb

P.O.C. E Cushman	182.90	-3.25	
+ 7.85	182.55	-2.81	
+ 15.71 E.C. 30 R	182.10	-2.42	
W.L. Cushman	180.0	<del>-2.38</del>	-2.1
0 + 20	178.75	179.12	<del>-2.04</del> -1.69
0 + 40	178.90	<del>1.82</del>	-1.32
0 + 60	179.32	<del>1.51</del>	-1.01
0 + 80	180.38	<del>2.07</del>	-0.47
1 + 00	182.10	<del>2.08</del>	-0.35
+ 31.95 P.C.C. 185.0	185.35	<del>2.05</del>	-0.20
1 13° 14' 45"	184.55	184.71	-0.22 -0.08
2 26° 29' 30"	187.87	0.0	
3 39° 44' 15"	188.48	0.0	
4 52° 59'	P.R.L. 188.50		

Align.

B.M.C.T.  
APRON

156.88

11.09

Elev. Rd.

167.89

0.96

166.93

1.287

179.80

0.96

178.86

11.87

190.73

0	+197.43	BCLT	155.40	
1	4° 19' 41"	Chords	156.52	
2	8° 39' 22"	249	157.65	-0.49
3	12° 59' 03"		158.77	-0.58
4	17° 18' 44"	PRC=00	159.90	-0.16

0	+18.28	2° 26.2	160.80	-0.65
1		5° 06.0	161.90	-0.72
2		7° 45.7	163.05	-0.68
3	20	10° 25.5	164.35	-0.17
4	4	13° 05.2	165.55	+0.09
5		15° 45.0	167.05	-0.12
6		18° 24.7	168.60	-0.09
	PRC 1032	19° 47.	169.40	-0.06

1		1° 16' ✓	171.95	-0.14
2	29.92	2° 32' ✓	174.50	-0.05
3	4	3° 48' ✓	177.05	+0.31
4	PRC	5° 04' ✓	179.60	-0.04
1		5° 55' ✓	181.20	-0.14
2	20	6° 45.8 ✓	182.70	-0.11
3	7	7° 36.7 ✓	184.0	-0.17

4		8° 27.5 ✓	185.25	-0.17
5		9° 18.4 ✓	186.35	-0.27
6		10° 09.3 ✓	187.30	-0.51
7		11° 00.1 ✓	188.05	-0.14
PRC 06	13.83	11° 35.25 ✓	188.50	-0.07 see P48

INDEXED  
WK  
OCT 20 1948

# INDEXED

WK  
OCT 20 1948

Everview Rd. Line of Wly Curb

beg. 75' S of ONSTAD 1800.2

RUN NAILS ON CB. LINE

B.C.				12.31	
				167.91	
				0.41	
		W.C.B.		148.12	
		- .45	164.40	13.10	
1	2-20.99	3° 44.7 ✓	- .40	161.25	155.02
					0.46
2	PRC	7° 29.5 ✓	- .50	158.10	155.48
1		10° 45.1 ✓	- .48	155.50	0.52
2		14° 00.8 ✓	- .60	153.30	142.49
3		17° 16.5 ✓	- .58	151.40	12.74
4		20° 32.1 ✓	- .57	149.70	0.63
5		23° 47.7 ✓	- .42	148.40	131.38
6	EXC.	27° 03.1 ✓	- .33	147.30	534
1		31° 33.0 ✓	+ .14	146.07	126.04
2		36° 03.2 ✓	+ .15	144.83	12.42
3	PRC	40° 35.75 ✓	- .13	143.60	138.42
1	1-10.26	0° 47.0 ✓	F0.35	143.05	12.04
			- .17	142.90	150.46
1		2° 18.6 ✓	F0.35	141.85	
			+ .40	141.20	
2		3° 50.3 ✓	0.00	140.25	
			+ 1.06	139.0	
3		5° 22.0 ✓	0.189	137.85	
			+ 2.04	136.20	
4		6° 53.6 ✓	F0.35	134.85	
			+ 1.40	133.10	
5		8° 25.3 ✓	F0.50	131.25	
			+ 1.25	129.50	
		9° 33.04 ✓	P.C. Curb	127.80	0.0
			P.C. Ret.	126.40	+ 1.38

NELY RETURN of DORCAS & EVERVIEW

16	P.L. of Ret.	127.80	0.0
		124.40	+ 1.38
1	17° 26 ✓	125.55	F0.19
		124.30	+ 1.06
2	34° 52 ✓	123.15	F0.33
		122.30	+ 0.53
3	52° 18 ✓	121.12	F0.30
		120.70	+ 0.41
4	69° 46 ✓	119.82	0.07
		119.70	+ 0.19
5	87° 11 ✓	119.20	- 0.05
		119.20	+ 0.25
6	104° 37 ✓	119.20	- 0.33
		119.20	+ 0.13
7	122° 03 ✓	119.00	- 0.57
		119.70	- 0.27
8	E.C. Ret. 139° 29' 00	121.00	F0.43
		120.70	- 0.13
	0 + 50	126.96	- 0.44
1		133.22	- 1.14
1	+ 50	139.48	- 0.83
1	+ 93.6 = S.L. LOT 5 BK 6	144.95	- 0.23

# INDEXED

WK  
OCT 20 1948

150.46
0.14
150.32
12.10
162.44
2.04
160.38
7.53
167.91
165.72
2.19
3.04
1.05

SE 1/4 Cor. of  
ONSTAD & Everview

P.C. - 75	179.40 ✓
P.C. - 50	179.0 + .24
P.C. - 25	178.60 + .30
P.C.	178.0 + 0.03

1	11° 15'	Chords 13.45	177.45 - .25
---	---------	--------------	--------------

2	22° 30'	176.60 - .58
---	---------	--------------

3	33° 45'	175.40 - 0.74
---	---------	---------------

4	E.C. 45° 00'	174.0 - 0.59
---	--------------	--------------

5	25	170.97 - .22
---	----	--------------

8.6%

12.13%

177.64  
2.38  
180.02

Ely Curb. on  
Evenview S. of Oxstad

		155.48	
		12.43	
	E. Cb.	142.85	
		0.64	
S.L. DIST.	153.50	- .82	143.49
	151.50	- .93	
	149.70	- .49	
	148.30	- .82	
	147.10	- .56	
	145.77	- .55	
	144.43	- .07	
	143.10	+ .14	
	142.55	0.030	
	142.40	+ .45	
	141.35	0.043	
	140.70	+ .08	
	139.75	0.061	
	138.50	+ 1.86	
	137.35	0.069	
	135.70	+ 2.34	
	134.35	0.087	
	132.60	+ 2.60	
	130.75	0.084	
	129.0	+ 2.59	
	126.40	8.43 2.53 0.70	
	122.35	0.07 0.09 0.02	
	118.09	4.33 2.29 0.36	
	114.12	8.30 8.93 0.63	
	110.42	12.02 12.45 0.43	

	12°13.33'	102.01	
	10°41.67'	102.89	
	9°10.01'	101.04	
	7°38.35'	98.48	
	6°06.69'	96.20	
	4°04.46'	93.35	
	2°02.23'	90.50	
EC V	0°00'	82.65	
		85.16	
		82.67	
		80.19	
		77.70	
		75.80	
		76.00	
		74.52	
		74.88	
		73.90	
		74.29	
		73.92	
		74.58	
		74.62	
		74.82	

07274920  
52

81176364  
9.54  
85.24  
12.03  
98.27  
8.44  
97.83  
12.10  
109.93  
6.20  
109.73  
12.71  
122.44  
0.09  
123.35  
12.48  
134.83  
0.74  
0.86  
0.08  
5.23  
2.86  
0.27  
5.96  
0.26  
9.90  
10.00  
0.10  
11.02  
11.48  
11.62  
12.60  
11.62  
12.61  
11.08  
11.83  
0.98  
0.60  
0.95

BC V curb

4-1262  
Ret

18.50

Rosecrans St.  
Curb Change South of Bassemor

BM	12.71	40.55		27.84	17.18 B.P. Rosecrans Bassemor
TP	12.44	52.03	0.96	39.59	
TP	5.37	54.38	3.02	49.01	

BC Lt. 45.34 0.00

L=248.39  
Curve into 10 Parts

1	Chords 24.83 1° 50.9'		46.35	8.42 8.18 0.24
		Δ 36° 58'		
		R 385'		
		T 128.89		
2	3° 41.8'	L 248.39	47.40	7.37 7.34 0.03
3	5° 32.7'		48.45	6.32 6.90 0.08
4	7° 23.6'		49.28	5.49 5.77 0.28
5	9° 14.5'		50.02	4.75 5.40 0.65
6	11° 05.4'		50.77	4.00 3.93 0.08
7	12° 56.3'		51.51	3.26 3.39 0.03

Oct. 3.39  
S. 15.07  
Nor 4.01  
53  
07 Pav

Top Cb  
Existing

Edge Pav

INDEXED

W.K.

OCT 20 1948

45.34 Top Cb B.C.

9.43

54.77 Measurements to the right of new line  
on East side of Rosecrans.

45.34

9.04

46.39

7.99

0.8'

47.42

6.90

3'

48.57

5.81

7'

49.52

4.86

12'

50.26

4.12

13.5

51.02

3.36

12

51.73

2.65

7'

46.55

8.13

6'

47.42

6.96

8

48.54

5.84

12'

49.35

5.03

16

49.95

4.43

17

50.79

3.59

16

51.64

2.74

12

46.67

7.71

16'

47.80

6.58

18'

48.90

5.48

22

49.76

4.62

21

50.41

3.97

27

51.24

3.14

26

52.19

2.19

22

8	14.472	52.15	$\begin{array}{r} 2.62 \\ 2.90 \\ \hline 5.52 \\ - 0.81 \\ \hline \end{array}$
9	16.381	52.15	$\begin{array}{r} 2.62 \\ 2.90 \\ \hline 5.52 \\ - 0.28 \\ \hline \end{array}$
10	- F.C. 18.29	51.39	$\begin{array}{r} 3.38 \\ 3.09 \\ \hline 6.47 \\ - 0.0 \\ \hline \end{array}$

Top Cb

Edge Part

54

0.12 Part

62.06

2.32

35

52.03

2.35

0.8

51.39

2.99

54.38

51.92

2.46

8

51.87

2.51

5.8

52.41

1.97

18'



Bianca curb grades

N.L. STA.	65.137 Ford PCB	Nly	4.23 4.03 Co.19
P.C.	52.91 0.51	48.70	3.99 3.86 Co.77
19.97	3°49.2 52.92T 4.03	48.70	3.89 3.87 Co.02
	8°46.2 48.89 3.60 52.49T	48.60	4.14 4.05 Fo.11
	13°43.2	48.35	4.89 4.77 Co.12
	18°40.2	47.60	5.74 5.72 Co.02
	23°39.3	46.75	6.99 6.87 Co.42
	28°36.4	45.50	8.44 8.05 Co.89
	33°33.1	44.05	10.19 10.06 Fo.07
	38°30.0	42.30	12.29 12.23 Fo.14
EC.	29.92 44°14.0	Nly Weeks add 40.20	RC. Above 4.05 4.73 Fo.18 4.89 4.83 Co.06
	3-41.18	48.70 =	5.22 4.98 Co.47
	P.C. 180°	48.37	5.17 4.11 Co.06
	5°43.7	48.03	4.73 4.60 Co.78
	11°27.5	47.70	3.87 3.87 Co.45
	17°11.3	48.20	3.63 3.52 Co.08
	22°55.1	49.10	4.00 4.00 Co.08
	28°38.9	50.30	4.94 4.94 Co.08
	34°22.4	51.90	11.43 11.92 Fo.56

INDEXED

W.K.

OCT 21 1948

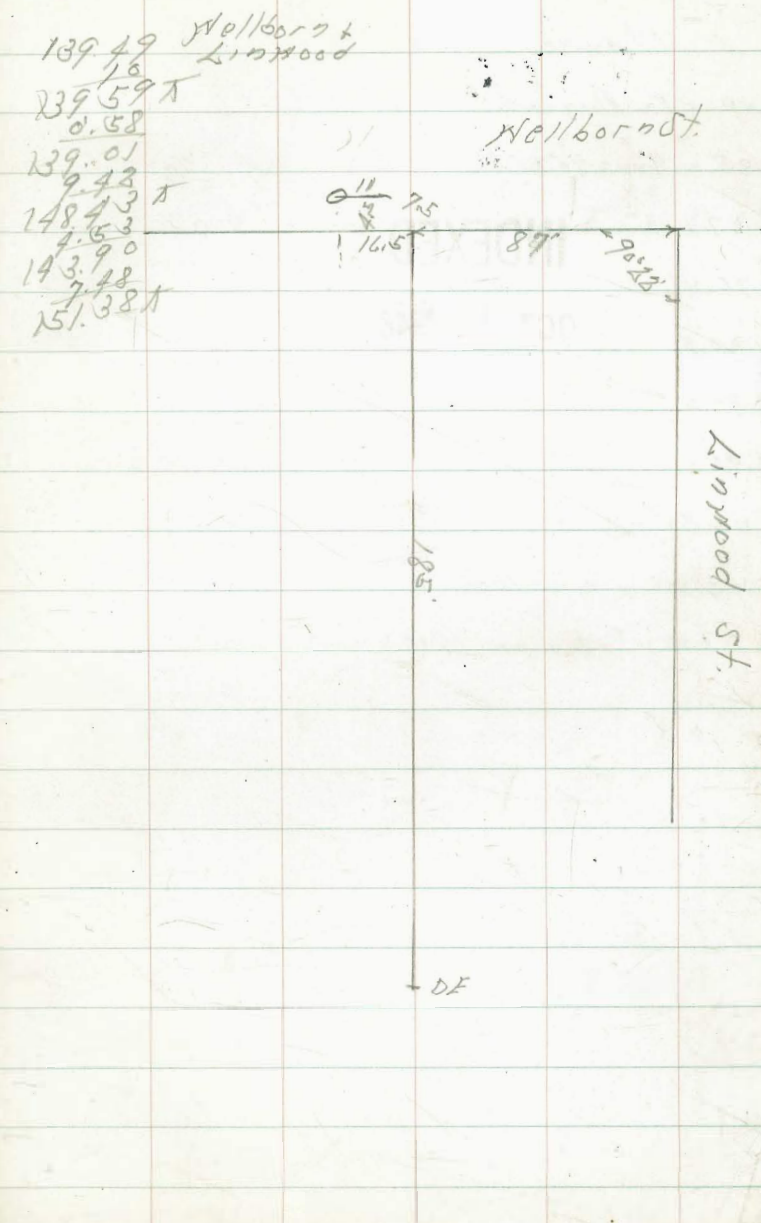
55

7	40°04.4	Nly	55.90	9.23 9.57 Fo.14
1/2 Curve	45°00.0		57.75 ✓	
CONT. PCB				
BIANCA ST				
		Sly	58.92T	
			48.20	
1			47.87	4.62 5.51 Fo.89
2			47.53	5.39 6.09 Fo.70
3	OPP. PC = 0 + 50		47.20	5.72 6.50 Fo.78
	0 + 35		47.0	5.97 6.78 Fo.86
	0 + 55		46.55	6.32 6.59 Fo.22
	0 + 74.91	66 P.C. R. 35	45.80	7.12 7.08 Co.04
1			45.00	7.92 7.84 Co.10
2			44.20	8.72 8.50 Co.33
3			43.10	9.82 9.63 Co.39
4		6 E.C. on Dorcas	42.00	10.92 10.70 Co.80
	0 + 35.5		38.70	14.32 13.96 Co.26
	0 + 69 = 3 Nly Weeks add.		35.68	17.24 16.91 Co.33

Block 19 Middletown Add.  
Sewer Construction

Oct 5-89  
Dustin  
Northport

MH	INDEXED WK OCT 21 1948		
		119.36	20.23 14.40 C 5.83
18.5' F = 0 to E L Wellbor 1		121.05	18.54 12.37 C 6.17
20' F		122.88	16.76 8.59 C 8.18
50' F		125.62	18.97 5.23 C 8.74
74' F		127.82	11.77 15.07 C 6.90
100' F		130.10	18.43 10.02 C 8.35
125' F		132.39	16.04 9.67 C 6.37
150' F		134.68	13.75 5.47 C 8.38
163' F		135.90	12.53 4.58 C 8.00
185' F - D E		138.00	13.38 2.44 C 10.94





Rosecrans ST Grades 10-18-39

for oil Pav.  
Ingraham sly

⊕ STA. STAKES LINED ON 20' offset to Rt.

29 SWBP Ingraham 0.56  
Rosecrans 3.78  
L.49

BM 0.56  
4.30  
48.67

INDEXED

W.K.

OCT 21 1948

+50

BM 0.56  
4.96  
5.537

28

4.55  
5.05  
FO.50 0.31

521 ✓

0.61  
3.69  
4.39  
-0.70

+50

4.71  
5.18  
FO.47 0.15

537 ✓

0.45  
2.85  
4.33  
-0.48

27

4.86  
5.15  
FO.29 0.00

0.30  
2.0  
4.3  
-0.2

26 +77.45 sly Ingraham

Lt.

⊕

Nov. 12. 39  
S. J. 58  
Hortberg  
O. S. Gard

4.24  
5.04  
FO.80 0.62 49.0

0.94  
3.38  
4.70  
-1.3

4.40  
5.05  
FO.65 0.46

5.06 ✓

0.76  
3.54  
4.48  
-0.94

4.55  
5.05  
FO.50 0.31

521 ✓

0.61  
3.69  
4.39  
-0.70

4.71  
5.18  
FO.47 0.15

537 ✓

0.45  
2.85  
4.33  
-0.48

4.86  
5.15  
FO.29 0.00

0.30  
2.0  
4.3  
-0.2

-0.07

0.23  
0.0

+50

$$\begin{array}{r}
 4.29 \text{ T} \\
 4.74 \\
 -0.55 \\
 \hline
 4.14 \\
 3.71 \text{ T}
 \end{array}$$

$$\begin{array}{r}
 4.86 \text{ T} \\
 5.36 \\
 -0.50 \\
 \hline
 5.20 \\
 4.70 \text{ T}
 \end{array}$$

552T

+50

$$\begin{array}{r}
 3.46 \\
 5.06 \\
 \hline
 F1.90
 \end{array}$$

1.40

4.13 ✓

$$\begin{array}{r}
 1.70 \\
 2.50 \\
 4.80 \\
 \hline
 2.20
 \end{array}$$

31

$$\begin{array}{r}
 3.62 \\
 5.38 \\
 \hline
 F1.74
 \end{array}$$

1.24

4.28 ✓

$$\begin{array}{r}
 1.54 \\
 2.76 \\
 4.81 \\
 \hline
 2.05
 \end{array}$$

+50

$$\begin{array}{r}
 3.78 \\
 5.05 \\
 \hline
 F1.27
 \end{array}$$

1.08

4.44 ✓

$$\begin{array}{r}
 1.38 \\
 2.92 \\
 4.47 \\
 \hline
 1.70
 \end{array}$$

30

$$\begin{array}{r}
 3.93 \\
 5.27 \\
 \hline
 F1.34
 \end{array}$$

0.93

4.59 ✓

$$\begin{array}{r}
 1.23 \\
 3.07 \\
 4.64 \\
 \hline
 1.57
 \end{array}$$

29+50

$$\begin{array}{r}
 4.09 \\
 5.35 \\
 \hline
 F1.26
 \end{array}$$

0.77

4.75 ✓

$$\begin{array}{r}
 1.07 \\
 3.43 \\
 4.61 \\
 \hline
 1.38
 \end{array}$$

4+

2

59

$$\begin{array}{r}
 3.00 \\
 4.95 \\
 \hline
 F1.95
 \end{array}$$

1.70

3.88 ✓

$$\begin{array}{r}
 2.0 \text{ T.P.} \\
 2.30 \\
 4.74 \\
 \hline
 2.44
 \end{array}$$

$$\begin{array}{r}
 3.15 \\
 5.06 \\
 \hline
 F1.91
 \end{array}$$

1.55

3.97 ✓

$$\begin{array}{r}
 1.85 \\
 2.45 \\
 4.53 \\
 \hline
 2.08
 \end{array}$$

$$\begin{array}{r}
 3.46 \\
 5.06 \\
 \hline
 F1.90
 \end{array}$$

1.40

4.13 ✓

$$\begin{array}{r}
 1.70 \\
 2.50 \\
 4.80 \\
 \hline
 2.20
 \end{array}$$

$$\begin{array}{r}
 3.62 \\
 5.38 \\
 \hline
 F1.74
 \end{array}$$

1.24

4.28 ✓

$$\begin{array}{r}
 1.54 \\
 2.76 \\
 4.81 \\
 \hline
 2.05
 \end{array}$$

$$\begin{array}{r}
 3.78 \\
 5.05 \\
 \hline
 F1.27
 \end{array}$$

1.08

4.44 ✓

$$\begin{array}{r}
 1.38 \\
 2.92 \\
 4.47 \\
 \hline
 1.70
 \end{array}$$

$$\begin{array}{r}
 3.93 \\
 5.27 \\
 \hline
 F1.34
 \end{array}$$

0.93

4.59 ✓

$$\begin{array}{r}
 1.23 \\
 3.07 \\
 4.64 \\
 \hline
 1.57
 \end{array}$$

$$\begin{array}{r}
 4.09 \\
 5.35 \\
 \hline
 F1.26
 \end{array}$$

0.77

4.75 ✓

$$\begin{array}{r}
 1.07 \\
 3.43 \\
 4.61 \\
 \hline
 1.38
 \end{array}$$

34

3.71  $\pi$ 

$$\begin{array}{r} 4.70 \times \\ 4.96 \\ - 0.26 \text{ of Staboot 24} \\ \hline 5.78 \\ 35+60 \\ \hline 5.52 \pi \end{array}$$

35+60 Break

$$\begin{array}{r} 5.52 \pi \\ 2.66 \\ 1.86 \\ 4.90 \\ \hline 6.78 \pi \end{array}$$

35

+50

34

+50

33

$$\begin{array}{r} 2.97 \\ 5.64 \\ \hline F2.67 \end{array} \quad \begin{array}{r} L+ \\ 2.55 \end{array} \quad \begin{array}{r} 4.21 \\ 2.85 \\ 0.86 \\ 4.41 \\ \hline -3.55 \end{array}$$

$$\begin{array}{r} 2.00 \\ 4.96 \\ \hline F2.96 \end{array} \quad \begin{array}{r} 2.70 \\ 4.06 \end{array} \quad \begin{array}{r} 3.0 \\ 0.71 \\ 4.43 \\ \hline -3.74 \end{array}$$

$$\begin{array}{r} 2.20 \\ 4.24 \\ \hline F2.44 \end{array} \quad \begin{array}{r} 2.50 \\ 4.26 \end{array} \quad \begin{array}{r} 2.80 \\ 0.91 \\ 4.41 \\ \hline -3.50 \end{array}$$

$$\begin{array}{r} 2.37 \\ 4.92 \\ \hline F2.55 \end{array} \quad \begin{array}{r} 2.33 \\ 4.43 \end{array} \quad \begin{array}{r} 2.63 \\ 1.08 \\ 4.30 \\ \hline -3.22 \end{array}$$

$$\begin{array}{r} 2.54 \\ 4.83 \\ \hline F2.29 \end{array} \quad \begin{array}{r} 2.16 \\ 4.60 \end{array} \quad \begin{array}{r} 2.46 \\ 1.55 \\ 4.32 \\ \hline -3.07 \end{array}$$

$$\begin{array}{r} 2.19 \\ 4.95 \\ \hline F2.26 \end{array} \quad \begin{array}{r} 2.01 \\ 4.75 \end{array} \quad \begin{array}{r} 2.31 \\ 1.40 \\ 4.14 \\ \hline -2.74 \end{array}$$

$$\begin{array}{r} 2.85 \\ 4.90 \\ \hline F2.05 \end{array} \quad \begin{array}{r} 1.85 \\ 2.67 \end{array} \quad \begin{array}{r} 2.15 \\ 1.54 \\ 4.26 \\ \hline -2.70 \end{array}$$

39+05 Break 3° 09.4

ch 54.07

+50 1° 50.6

ch 49.13

38 0° 39.0

ch = 24.76

R = 1180

Q = 1200

37+72.83 = BC PT.

+50

37

36 + 50

3.71 T

3.92

- 0.21 T.P.

6.50

6.29 X

5.52 T

6.76 T

4.33

2.43

4.95

7.38 T

of 4500

BC

3.12

5.62

F2.20

Lt.

5.28 ✓

2.10

1.70

2.01

3.91

- 1.91

RT

6.18

1.20

61

4.32

5.81

F1.49

3.14

5.92

F2.78

2.38

5.00 ✓

1.93

1.78

3.90

- 2.14

5.95 ✓

1.43

4.09

5.78

F1.69

3.06

5.82

F2.76

2.46

4.92 ✓

2.11

1.40

3.93

- 2.33

5.74 ✓

1.64

3.88

5.81

F1.93

3.08

5.39

F2.31

2.44

4.23 ✓

2.21

1.50

4.18

- 2.78

5.03 ✓

1.73

3.79

6.15

F2.36

3.12

5.80

F2.62

2.40

4.36 ✓

2.30

1.41

4.44

- 3.03

4.86 ✓

1.90

3.62

6.30

F2.68

3.19

5.87

F2.68

2.33

4.43 ✓

2.48

1.23

4.46

- 3.43

4.63 ✓

2.13

3.39

6.50

F2.91

3.12

5.70

F2.58

2.40

4.36 ✓

2.66

1.05

4.54

- 3.49

4.63 ✓

2.36

4.40

42+60 E.V.C.

6.79 A

5.52 A

42+10

7.38 A

41+60

41+10

40+60

40 + 10.54

39 + 01.06 E.C.

4° 29' 37"

BREAK

ch 55.22

0.92  
3.50  
F2.58

47

3.78

4.60

2

RT

62

4.90

1.39

5.29

- 3.90

1.77  
4.26  
F2.49

3.75

3.63 ✓

4.05

2.24

5.94

- 3.7

3.53  
4.66  
F2.14

3.00

4.38 ✓

3.30 ✓

2.99

4.60

- 3.61

P. 340

3.07  
5.02  
F1.95

2.45

4.93 ✓

2.75

3.54

6.90

- 3.36

3.65  
5.08  
F1.73

1.87

5.51 ✓

2.10

4.19

4.81

- 2.64

5.58 ✓

1.80

3.75  
5.97  
F1.66

1.77

5.61 ✓

1.80

4.49

6.73

- 2.24

5.94 ✓

1.44

4.08

5.01

F1.93

3.77  
5.65  
F1.88

1.75

5.63 ✓

1.50

4.79

6.89

- 2.10

6.33 ✓

1.05

4.47

6.60

F1.93



46

$$\begin{array}{r} 5.527 \\ 2.19 \\ 3.38 \\ 12.57 \\ 15.957 \end{array}$$

+ 50

$$\begin{array}{r} 4.29 \text{ T} \\ 0.37 \\ 5.92 \text{ T.P.} \\ 12.25 \\ 18.17 \end{array}$$

45

$$\begin{array}{r} 7.387 \\ 1.01 \\ 6.37 \\ 11.69 \\ 18.087 \end{array}$$

+ 50 P.O.T.

44

+ 50

43+00

$$\begin{array}{r} 4.62 \\ 3.20 \\ 07.42 \\ 11.33 \\ 6.73 \\ 11.63 \\ 6.54 \\ 2.46 \\ + 2.10 \end{array}$$

$$\begin{array}{r} 5.61 \\ 4.25 \\ 01.36 \\ 10.34 \\ 7.73 \\ 10.64 \\ 7.53 \\ 5.09 \\ + 2.42 \end{array}$$

$$\begin{array}{r} 6.56 \\ 7.84 \\ 170.68 \\ 9.35 \\ 8.71 \\ 9.65 \\ 8.57 \\ 6.22 \\ + 2.30 \end{array}$$

$$\begin{array}{r} 7.59 \\ 8.20 \\ 170.87 \\ 8.36 \\ 9.70 \\ 8.66 \\ 9.51 \\ 7.88 \\ + 1.63 \end{array}$$

$$\begin{array}{r} 8.88 \\ 8.96 \\ 170.88 \\ 7.87 \\ 10.69 \\ 7.67 \\ 10.50 \\ 10.00 \\ + 0.50 \end{array}$$

$$\begin{array}{r} 9.57 \\ 10.46 \\ 170.89 \\ 6.38 \\ 1.00 \\ 6.68 \\ 11.49 \\ 12.35 \\ - 0.76 \end{array}$$

$$\begin{array}{r} 0.18 \\ 2.12 \\ 172.08 \\ 5.10 \\ 1.98 \\ 5.70 \\ 0.54 \\ 3.44 \\ - 2.85 \end{array}$$

T.P. between

+90 4° 41.25

+65 3° 15.35

48+40 P.V.C. 1° 39.3

ch = 30.53  
B.P. = 500

48+08.20 B.C. P.T.

+50

47

46+50

18.17 X  
1.68  
16.49 T.P.  
12.50  
29.01 X

15.95 X  
9.6  
TP 14.99 07 21 Stub  
47+50  
12.25  
27.24 X

18.06 X  
15.10 07 17 07 06  
11.04 48+08.20  
36.14 X

LT	E. J.P.	RT	64
8.54 11.20 F 2.66	7.94	17.50 0.67 1.68 -1.01	10.87 10.76 00.08
9.19 10.92 F 1.73	18.05 8.09	16.90 1.27 2.00 -0.73	10.34 15.80 11.44 11.08 00.36
9.89 11.20 F 1.31	17.35 8.79	16.20 1.77 2.29 -0.50	10.79 15.35 11.89 11.34 00.55
10.79 12.14 F 1.35	16.45 1.61	15.75 2.40 2.92 -0.50	3.21 14.85 12.09 11.98 00.71
1.22 9.6 00.26	14.73 3.33	14.60 2.57 3.33 +0.22	4.01 14.05 13.19 12.37 00.82
2.54 8.6 01.68	13.41 4.65	13.61 2.56 3.80 +0.76	4.88 13.20 14.04 13.22 01.20
2.63 11.03 02.60	12.32 5.74	12.64 5.55 4.10 +1.45	12.32

+83.85 15° 47.5 ✓

ch. of 42.00

50+40 E.V.C. 13° 16.8 ✓ 29.01 X

8-2 ch

27.24 X

50+15 11° 50.9 ✓

26.14 X  
0.68  
25.51  
11.25  
36.76 X

+90 10° 25.0 ✓

+65 8° 59.0 ✓

+40 7° 33.1 ✓

49+15 6° 07.2 ✓

-0.91 0.77 F.1.68	Lt 28.15	8.6 ✓	26.95 2.06 3.26 -1.70	RT 11.01 25.75	65 1.49 2.03 F0.54
-------------------------	-------------	-------	--------------------------------	-------------------	-----------------------------

1.74 3.21 F.1.47	25.50	0.64 ✓	24.30 5.71 7.07 -1.76	23.10	4.14 5.02 F0.88
------------------------	-------	--------	--------------------------------	-------	-----------------------

3.04 5.56 F.2.52	24.20	1.94 ✓	23.0 6.01 7.93 -1.92	21.80	5.44 6.18 F0.74
------------------------	-------	--------	-------------------------------	-------	-----------------------

4.49 7.46 F.2.96	22.75	3.39 ✓	21.55 7.46 9.22 -1.70	5.79 20.35	6.89 7.52 F0.63
------------------------	-------	--------	--------------------------------	------------	-----------------------

5.69 7.87 F.2.18	21.55	4.59 ✓	20.35 8.66 10.22 -1.58	19.15	8.09 8.50 F0.41
------------------------	-------	--------	---------------------------------	-------	-----------------------

6.69 8.68 F.1.89	20.55	5.59 ✓	19.35 9.66 11.39 -1.73	7.99 18.15	9.09 9.64 F0.55
------------------------	-------	--------	---------------------------------	------------	-----------------------

7.64 10.51 F.2.81	19.50	6.54 ✓	18.40 10.61 11.89 -1.28	8.94 17.20	10.04 10.14 F0.10
-------------------------	-------	--------	----------------------------------	------------	-------------------------

~~27.24~~  
~~0.48~~  
~~26.76~~  
~~11.24~~  
~~38.00~~  
~~1.58~~  
~~36.42~~  
~~2.07~~  
~~15.49~~  
~~8.26~~  
 BM 41.63

759.42 = edge par.

Rod crane  
 SWBP LYRON = 41.75

29.01  
 0.46  
~~28.55~~  
 13.12  
 41.67

52 + 40

36.76

52 + 15.42 E.C. 23° 19.91.

+71.56

20° 48.98 ✓

51 + 27.7

18° 18.2 ✓

Lt

Z

Rt

66

INDEXED

NOV 1930

36.79  
~~5.88~~  
~~5.11~~  
~~0.93~~

36.10

35.90

36.25

2.75  
~~3.76~~  
 FO.01

35.25

1.57

34.85

1.71

35.05

2.95  
~~3.17~~  
 FO.22

4.85  
~~5.66~~  
 FO.81

33.15

3.65

32.75

9.42

9.92

20.50

31.55

6.45  
~~6.26~~  
 CO.19

7.30  
~~8.27~~  
 FO.97

30.70

6.06 ✓

29.60

12.07

13.12

11.05

28.40

9.60  
~~9.77~~  
 CO.13

Moore

Priv. Cont.  
Griffiths Co

10- Alley Pav. 15' wide

Blk 23 Terapto

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W.K.

OCT 21 1948

E

0+00	W		
Orange Pvc	361.40	361.40	
+20	41.90	41.90	
+40	42.30	42.30	
+60	42.60	42.60	
+80 PVC	42.80	42.80	
1 +20	43.01	43.01	
1 +60	43.22	43.22	
2 +00	363.44	363.44	

NW Orange + Van Dyke

67

361.03

476

365.79

2.11

367.68

5.23

367.91

4.22

363.49

4.63

368.32

W 361.40

4.39

41.90

4.01

4.80

C 1.21

42.30

42.60

2.80

5.61

5.31

5.11

5.89

4.74

4.88

C 1.72

C 0.55

C 0.23

E 4.39

(7.0)

3.89

4.31

C 0.78

5.61

4.51

C 1.10

5.31

4.54

C 0.75

5.11

4.21

C 0.90

W 3.01

3.22

3.44

(7.0) - 4.90

5.10

4.88

4.22

4.68

3.88

C 0.68

C 0.42

C 1.0

NAIL

E 3.01

5.10

4.88

5.31

4.44

4.55

4.94

C 0.64

C 0.53

C 0.37

Hilda Dr. ROAD  
 Sly curb grades  
 beg. Center of 180° Curve  
 at Dorcas St  
 to end of EXISTING curb  
 at Park (end curb in let.)

To STA.

		Wly	
5+72.87 P.O.C.		57.70	738 746 FO.08
23.57		57.75	496 528 FO.53
5+96.42	5° 23.8	60.17	257 272 CO.70
23.56		62.59	1253 1275 FO.22
6+20	10° 47.7	64.71	1049 1071 CO.57
+40	15° 22.7	66.75	874 884 CO.17
+60	19° 57.7	68.23	757 751 CO.06
+75	23° 24.0	68.50	582 582 0.00
+90	26° 50.7	69.67	1345 1345 FO.37
7+10	31° 25.8	71.42	26 344 1175 1331 FO.56
+30	36° 00.4	73.10	771348 P.C. Dorcas
+50	40° 35.5	74.80	72.92 73.20 74.59 76.06 77.90 78.90 81.15 83.75
7+69.77 E.C. 45° 00		76.45	865 948 FO.83
180		80.20	1040 1110 FO.61
8+00		83.20	590 598 FO.08
+20		83.20	780 850 CO.30

B.M. 2 Hub 7+49.22 E.C.

76.36  
 11.57  
 87.87 \*

INDEXED

W.K.  
 OCT 21 1948

68

76.36  
 0.88  
 77.24 X  
 13.75  
 64.49  
 0.64  
 65.13 X

68.42

B.M. 76.36  
 16.19  
 86.55  
 86.40  
 86.15  
 88.73 X

Ely

Ely  
 upper deck

64.09

66.21

68.25

69.73

71.17

72.92

73.20

74.59

76.06

77.90

78.90

81.15

83.75

73.50

74.59

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

FO.53

Hilda Dr. SW curb grade

8+40		85.80	-0.76
+60		88.50 <sup>40</sup>	-0.35
+80		91.20	-0.28
9		93.85	-0.08
+20		94.13	+0.16
9+52.75 PC		99.65	+0.48
+70	1° 19.1	101.35	+0.21
+90	2° 50.7	103.10	-0.31
10+10 POC	4° 22.4	104.55	-0.49
+30	5° 54.1	105.55	-0.44
+50	7° 25.7	106.50	-0.21X
+70	8° 57.4	107.45	-0.34
+90	10° 29.1	108.07	-0.72
11+10	12° 00.7	108.38	-0.50
+30	13° 32.4	108.40	-0.11
+50	15° 04.1	108.12	+0.12
+70	16° 35.8	107.60	-0.29
+90	18° 07.4	107.15	-0.81
12+10	19° 39.1	106.75	-0.85
+30	21° 10.8	106.30	-0.88
+50	22° 42.5	106.12	-0.59
12+70	24° 14.1	106.0	00
P +86.98 PRE	25° 32.0	105.95	00

	ELY	87.60	1.22 1.57 F0.04	887.21	69
12+70		89.90			106.29 50/100 6.61 112.907
		92.20			
		95.34			
		97.63			
		101.15			
		102.84			
		104.59			
		105.85			
		106.80			
		107.60	5.30 5.25 F0.45		
		108.40			1.50 5.55 F1.05
		109.04	5.86 4.90 F1.09		
		109.38			3.52 3.92 F0.42
		109.40	3.50 3.55 F0.05		
		109.08			3.82 3.89 F0.07
		108.35	4.55 4.76 F0.21		
		107.65			5.25 5.21 F0.41
		107.02	5.88 6.17 F0.23		
		106.50			6.40 6.51 F0.11
		106.12	6.78 6.90 F0.12		
		106.05			6.85
		105.95			6.98 00/100
		105.95			106.04

NE ly Cor. 12.277 = 16 P.C.  
Hilda + Dorcas 13.751 = Q

16. grade

86.557

P.C.

77.08

2-19.6 { 4° 49.7  
8° 59.5

74.59

P.R.C. - 165 12° 46.5

73.50

13.05  
13.21  
FO.21

1 38° 50.75

73.10

13.95  
13.22  
66.21

2 57° 41.50

73.50

13.05  
12.11  
60.94

3 86° 22.25

74.75

11.80  
10.22  
61.18

4 E.C. 115° 23.00

76.70

9.85  
8.71  
61.14



Monitor N Line

Curb Distances

8+49.22 P.C. Lt Hilda  
= 0+00 Monitor

0+00

1178

0+1178

0+23.56

0+35.34

1178

0+47.12 RT

25

0+72.12

25

0+97.12

1+22.52 P.C. Rt

20.26

1+42.78

1+63.04

1+83.30

Exc. Cb

N.L

88.41

90.20

90.70

91.30

92.00

94.50

94.05

96.90

96.77

101.20

102.90

106.10

105.20

110.26

113.55

116.85

120.26

11.2

12.3

13.7

Co. 1

8.6

7.2

6.3

4.5

3.0

6.15

11.7

10.6

6.7

6.9

5.2

6.7

3.3

3.1

Co. 2

9.3

7.2

Co. 1

6.0

5.5

Co. 2

3.61

3.62

0.0

change to new grades

**INDEXED**

W.K.

**OCT 21 1948**

90.92 0.28 Hilda  
9.69 Hilda  
106.61 K  
0.49  
100.13  
12.52  
112.64 K  
0.20  
105.5  
113.74

Monitor

10 am

71

South line  
0.2 below curb

Curb Distances

10+70 Hilda = 0+00

0+00

+20

+40

+60

+67.28 = 10+22

+93.34

1+18.91

1+44.47

1+70.04

1+95.61

2+21.17

2+46.73

2+62.63

2+78.53

2+94.43

Upper Deck

S.L

10840

10760

10710

10692

107.00

107.40

107.85

108.30

108.70

109.20

110.20

112.10

114.20

116.85

120.25 end curb

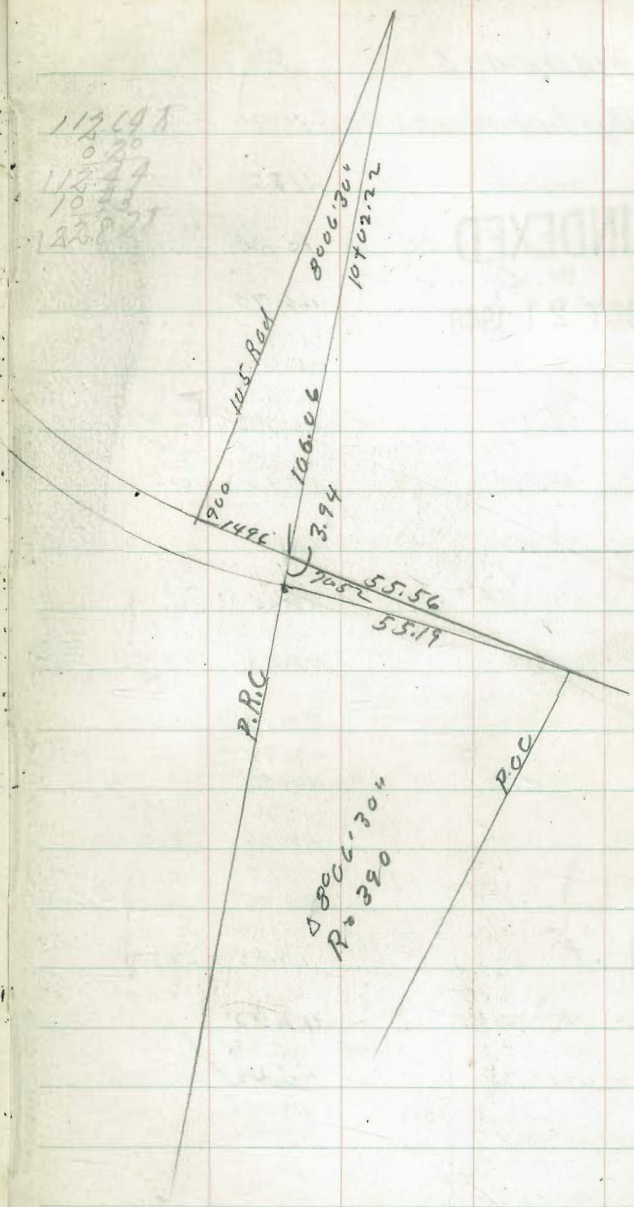
See next page

10 to 5' walk, to 10  
 Curb Distances Upper Dock New Alignment

0+12.43	PT=10157.41	POC	107.70		
+40			107.25		
+60			107.25		
+67.99	=10102.22	opp X	107.38		
+82.95	PC RT.		107.65		
+99.74	16.79 Δ=570 26' 05"		108.00	5.0	
+121.91	R=105.0		108.50	4.5	
+144.09	1-16.79 4-22.17 Parts		108.70	50.3	
+166.26			109.00	4.1	
+188.43	PT		109.50	5.0	
+201.66	PC R1		109.80	3.6	
+214.67	Δ=410 24' 35"		109.80	3.6	
+222.68	R=90.00		110.00	2.9	
+240.69	5-13.01 parts		109.70	2.9	
+253.70			110.40	3.5	
+266.71	PT end Curb		110.50	0.6	
			111.30	1.0	
			111.65	0.2	
			112.70	0.6	
			113.25	0.6	
			114.80	7.7	
			115.15	7.3	
			117.35	5.5	
			120.25	2.8	
			120.18	0.7	

Alignment of 5' curb

change to new grades RFB



Distances	Bianca st	54		
0+00	BC Nly line	Weeks Add	39.80	12.02 12.83 CO.2
0+2493			41.65	11.02 11.3 FO.13
0+46.50			43.10	9.57 9.6 CO.1
0+68.07			44.45 44.70	8.17 8.1 CO.1
0+89.64			45.65 45.80	7.07 7.0 CO.1
1+11.21			46.65 46.75	6.12 5.9 CO.2
1+32.78			47.35 47.40	5.5 5.3 CO.2
1+54.35			47.85	5.0 4.9 CO.1
1+75.92			48.00	4.9 4.8 CO.1
1+92.56	P.T @ North		48.02	4.8 4.0 FO.2
2+53.74	61.22		48.13	4.29 3.97 F1.18
3+14.92	61.28	✓	F1.12 47.94 48.21	1.21 2.0 F1.39
3+76.16	61.25	✓	F1.35 47.76 48.06	1.36 3.0 F1.65
4+01.05	24.93	✓	F1.56 47.68 47.95	1.47 3.0 F1.83
4+26.00	24.95		F0.98 47.30 47.55	1.57 3.0 F1.33
4+50.95	4+51.01 PC		F0.67 46.40 46.60	1.58 3.0 F1.33
4+25.90	4+64.78		F0.75 45.85 45.90	1.58 3.0 F1.33
5+00.85	Nly line 4+78.55	51y line	45.05 45.40	1.58 3.0 F1.33
5+25.80	4+92.32		44.05 44.30	1.58 3.0 F1.33
5+50.25	5+60.9 PT.		43.00	1.58 3.0 F1.33
5+72.87 B	5+77.09 Dorcas	AK	36.40	13.02 13.36 FO.34

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	40.06			114
39	40.10			12.77 12.81 FO.04
41.35	42.40			10.44 10.25 FO.18
42.40	44.20			8.27 8.44 CO.23
44.95	45.90			6.97 6.97 0.00
46.20	47.20			5.67 5.13 CO.55
47.25	48.25			4.63 5.13 FO.54
47.90	48.90			3.97 4.64 FO.67
48.35	49.35			3.52 4.23 FO.75
48.50	49.50			3.37 3.75 FO.38
48.50	49.45			3.42 3.00 FO.58
48.30	48.80			3.85 4.0 FO.23
48.21	48.20			4.05 4.51 FO.26
48.06	48.40			4.11 4.6 FO.33
48.20	48.55			4.07 4.02 CO.27
48.50	48.90			0.77 0.50 CO.26
48.50	48.70			0.77 0.50 CO.26
49.05	49.40			1.07 1.02 CO.35
49.90	50.30			1.32 1.33 CO.07
51.25	51.75			10.02 9.98 CO.73
52.90	53.40			8.37 8.14 FO.27
55.30	55.80			5.97 5.52 CO.45
57.75	57.90			3.57 4.63 FO.25

Nov. 1-39

73

0.75  
0.01  
0.200

Overlook Hts.

✓ Unnumbered Lots BIK 11

ER - 82564 22081 N 06

P.C. - 25 0.540 179.05 179.05 ✓

" - 12.5 0.270 178.20 178.65 C.062

P.C. C.0.55 178.65 178.30 C.0.90

" C.0.10 178.60 178.15 C.0.58

✓ 35' 06 R F.0.05 178.25 178.30 C.0.30

0 F.0.09 178.22 178.50 C.0.23

✓ E.C. = 00 F.0.10 179.40 179.0 F.0.10

+ 25 179.35 F.0.50

+ 50 179.40 Grade

+ 75 179.50 F.0.80

1 179.30 F.0.20

+ 25 178.90 F.0.26

1 + 50 P.C. MONITOR Rd. 178.20

1-8-40

74

177.64 B.P. Ranch

6.27  
183.91

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W.K.

OCT 21 1948

9.05	8.65	8.30	8.15	8.30	8.50	9.00
4.84	5.26	5.41	5.76	5.61	5.41	4.91
✓	4.44	4.91	5.21	5.31	5.18	5.01
	C.0.02	C.0.90	C.0.25	C.30	C.25	F.10

9.35	9.60	9.50	9.30	8.90	8.20	OK
4.56	4.81	4.41	4.61	5.01	5.71	CB
4.61	0.0	4.49	4.81	5.27	✓	
F.05		F.08	F.20	F.26		

LOTS 9-10 BIK 9 Overlook Hts

SE Cor. Elev. + Plainview Rd.

FCB.

-75	NON	204.27	204.27	
-55	C.11	204.85	204.67	C.29
-35	✓ C.35	205.35	205.17	C.53
-15	✓ C.23	205.95	205.60	C.58
PC	✓ C.36	206.35	206.05	C.66
'	✓ C.32	206.85	206.40	C.77
✓ 35' 66R	✓ C.25	207.40	207.85	C.83
✓	✓ C.17	207.95	207.40	C.69
✓ E.C.	C.02	208.50	208.0	C.52
+40	✓ F.47	210.10	209.82	F.21
+85 P.Y.C.		211.90	211.90	
+87.81			212.01	

1-8-40.

75

201.28 & Hub on Elev. Rd. & N.E. Brownell  
 10.70  
 114.18

INDEXED

WK.

OCT 21 1948

ON CB	4.27	4.67	5.17	5.60	6.05	6.40
	7.91	7.51	7.01	6.58	6.13	5.78
	7.82	7.32	6.82	6.20	5.49	5.01
H .09	C.29	C.53	C.58	C.66	C.77	

6.85	7.40	8.00	9.84	11.90	12.01
5.23	4.78	4.18	3.56	0.28	
4.50	4.09	3.66	2.55		
C.53	C.69	C.54	F.21		

Cross Section Rosecrans  
North of Lytton

BM 3.92	42.03	38.11	Top Alley Rd on Rosecrans N of Lytton
A N of Lytton			
E Cb Top	3.02	39.01	<b>INDEXED</b> W.K. OCT 21 1948
Gutter	3.44	38.59	
42.5 N of A			
E Cb Top	3.28	38.25	
Gutter	3.84	38.19	
85.01 N of A = Existing Alley Rd			
E Cb Top	3.93	38.10	
Gutter	4.48	37.55	
105 N of A = S.L. Alley			
E L on Pav 179	4.67	37.36	
E Cb " "	4.77	37.26	
g " "	4.43	37.60	
N Gutter " "	4.37	37.61	
W Cb Top	3.83	38.20	
125 N of A			
W Cb Top	2.85	37.18	
Gutter on Pav	4.57	37.66	
A " "	4.63	37.40	

May 11-26  
5.1962

42.03

Gb on Pav	4.95	37.08
T " "	4.88	37.15
H 20 25 W of BC		
S Edge Pav	5.80	36.23
g " "	5.35	36.67
N Edge " "	5.24	36.79
Opp BC. H 40		
55' N Edge Pav	6.48	35.55
10' g " "	6.35	35.68
25 S Edge " "	6.66	35.37
BC on Ground	6.7	35.3
25 S E BC		
S Edge Pav	7.71	34.32
50 S E BC		
S Edge Pav.	8.81	33.21
75 S E BC		
S Edge Pav	10.10	31.93







INDEXED

WIK  
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79

pg

A St.

6590

6588

TICOUT S.E. CT  
Resort 12-27-41  
Cap. Ask  
X-13-52

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W.K.

OCT 21 1948

NE Tie out 5-9-39

FIRST

65.97

NE 7

Reset 4-17-40

65.97

FIR

SW 7' Tie out

65.97

65.93

A

INDEXED

W.K.

OCT 21 1948

65.89

45.88

Keamy

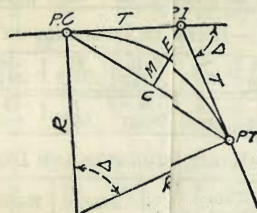
SW 7' Tie out

Reset

4-17-40

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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490 495

## CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)

External= $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div c \cdot \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $=$  Central Angle

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 16+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . In Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $+8\frac{1}{2} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C. = Sta. P. I. —  $T = 11+45.50$ . Also from (4)  $L = 746.00$  and P. T. = Sta. P. C. +  $L = 16+91.50$ .

**Offsets.**—Tangent offsets vary approximately directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance 58 — Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $D$  for 100 ft.,  $\frac{1}{2} D$  for 50 ft., etc. For c ft. = (in minutes)  $.3 \times C \times c$  or = def. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above  $c = .3 \times 54.5 \times 8\frac{1}{2} = 136.2'$  or  $2^\circ 16.2'$ , or  $= 2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26'$  etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$  and from Table V correction = .10 or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and is measured and found to be 42 ft. What is  $D$ ? From Table IV = 230.9 and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be  $41.9 + (20 - 16) \div 2$  or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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