

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

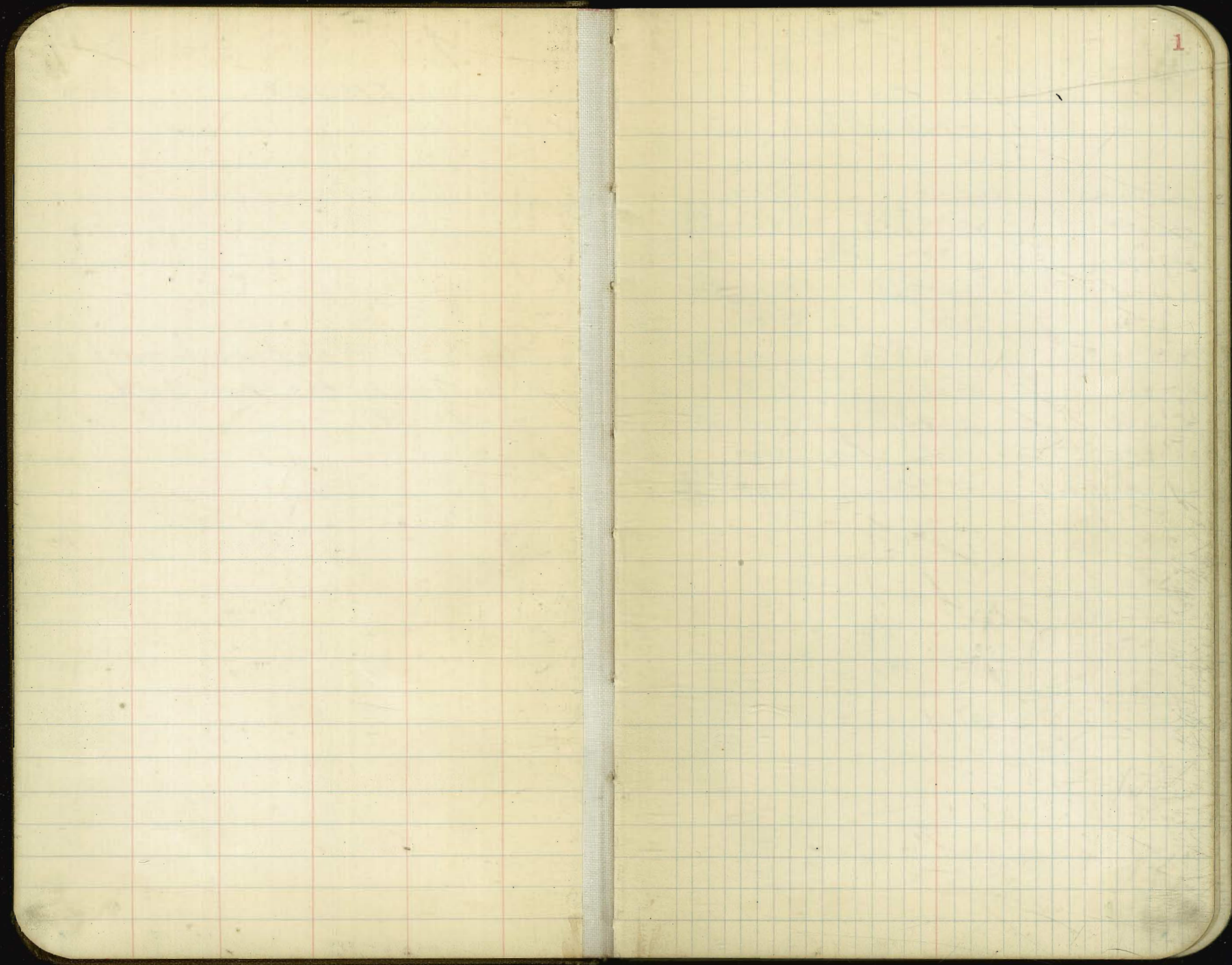
MICROFILMED

APR 12 1965

INDEX

Pages

Upas St. Pipe Line-Grades
& constr. notes, Park Brld.
to 5th St. — — 7-26



Alley Pav. 15' wide
Blk 9 Wilshire Pl.

	W	E
S.L. Monroe	365.40	365.24
0 + 20	✓ 65.59 ^{4.55} _{4.55} ^{4.04} _{4.04}	65.39 ^{4.27} _{4.27} ^{4.24} _{4.24}
0 + 70	^{4.03} _{4.17} 66.05 ^{4.04} _{4.04} ^{4.23} _{4.23}	65.85 ^{4.23} _{4.23} ^{4.24} _{4.24}
1 + 20	^{4.57} _{4.57} 66.51 ^{4.59} _{4.59} ^{4.28} _{4.28}	66.31 ^{4.28} _{4.28} ^{4.27} _{4.27}
1 + 70	66.97 ^{4.13} _{4.13} ^{4.13} _{4.13}	66.77 ^{4.33} _{4.33} ^{4.33} _{4.33}
2 + 20 PVC	✓ 67.43 ^{2.67} _{2.67} ^{2.67} _{2.67}	67.23 ^{2.87} _{2.87} ^{2.87} _{2.87}
+ 40	67.58 ^{1.76} _{1.76} ^{1.76} _{1.76}	67.38 ^{2.78} _{2.78} ^{2.78} _{2.78}
+ 60	67.67 ^{2.56} _{2.56} ^{2.56} _{2.56}	67.47 ^{2.76} _{2.76} ^{2.76} _{2.76}
+ 80	67.69 ^{4.54} _{4.54} ^{4.54} _{4.54}	67.49 ^{4.74} _{4.74} ^{4.74} _{4.74}
+ 95.75 end	67.65 ^{4.58} _{4.58} ^{4.58} _{4.58}	67.45 ^{4.78} _{4.78} ^{4.78} _{4.78}

Sewer Lat.

#1	341.39 ^{8.71} _{8.71} ^{8.71} _{8.71}
#2	341.19 ^{8.91} _{8.91} ^{8.91} _{8.91}

Indexed

Oct 26-39

Moore
Sisson
Northrup

365.40 on Pav 121
4.70 S.L. Monroe 0.0714
370.10 T
1.88
368.22
2.01
373.23 T

65.55 on stub 0 + 20
4.53
70.08 T

13+92	10.18 8.73 9.15 8.06	+2.30	$\frac{7.2}{c3.3}$	20+94	12.70	$\frac{10.9}{c4.2}$
14+46	17.51 1.12 16.34 7.81	3.10	$\frac{7.1}{c3.6}$	21+48 = 45 S of N L Byron	13.50	$\frac{10.5}{c4.5}$
15+2	23.65	3.90	$\frac{6.3}{c4.2}$	22+02	13.80	$\frac{9.8}{c4.1}$
15+54		4.70	$\frac{5.5}{c4.0}$	22+56	14.10	$\frac{9.5}{c4.2}$
16+0.8 = 45 S of N L Dixon	14.7 F 5.50 N 2.80 c3.3	5.50	$\frac{4.7}{c3.4}$	22+10	14.40	$\frac{9.2}{c4.2}$
16+62		6.30	$\frac{11.2}{c3.7}$	23+64	14.70	$\frac{8.9}{c4.2}$
17+16		7.10	$\frac{10.4}{c4.4}$	24+18 = 45 S of N L Addison	15.00	$\frac{8.6}{c4.7}$
17+70		7.90	$\frac{9.6}{c4.6}$	24+64.25		$\frac{8.6}{c4.4}$
18+24		8.70	$\frac{8.8}{c4.7}$	25+10.50		$\frac{8.6}{c4.5}$
18+78 = 45 S of N L Carleton	F 9.50 N 8.10	9.50	$\frac{8.9}{c4.7}$	25+56.75		$\frac{8.6}{c4.3}$
19+32		10.30	$\frac{7.7}{c4.1}$	26+02	15.00	$\frac{8.6}{c4.2}$
19+86		11.10	$\frac{8.4}{c4.3}$			
20+40		11.90	$\frac{5.6}{c4.4}$			

Upas Street 30" Pipe Line
30th St to 5th St.

Reference Points Page 7-12

Grades Page 13-26

Indexed

Q

Nov 9-37
S.W. 505
Northrup
Cotton

29th St

30" Water Line

St

29th St

29th St

Upas

30th St

30th St

0100

Ray St

$14 + 20.75$
 $14 + 22.60$
 $\Delta 22.57$

190° RP RP
 120° 30' Cross on Yolk
 120° 30'

28th St.

RP RP
 25' 20' 90°
 18 + 25 Δ 22° 30'
 Nail in Post

Utah

22

Granada

30' Stake Line P.
 Upas St.

Granada

8

Arnold Ave

Upas St.

Villa Ter.

46

• C.T.

Pershing Ave

Georgia

Upas St

Louisiana

46

Upas St

Texas

Arizona

24+70.50 R.O.T.

R.P. R.P.
20 20
Stub 90
X GRON
WaltR.P. R.P.
20 20
Stub 90
16.12

44+52.39 Florida

41+51.69
23.23R.P. R.P.
20 20
Stub 90
X GRON
WaltR.P. R.P.
Stub 20 Stub 20
90

40+31.22 30

Alabama

do" Water Line

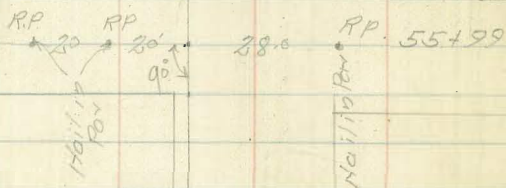
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CT.

Mississippi

Herbert

Upas St.



RP. nail in lot.
5-20'--20' 5-2+21.60

RP Hub 20' RP E.C. 69+71.15
20' 69+69.79
Cross on Cb.

$\Delta 7^{\circ} 04' 30''$
R 1200
T 74.17
L 148.18

RP Hub 20' RP E.C. 67+94.01
20' 68+21.51
Cross on Cb.

$\Delta 7^{\circ} 04' 30''$
R 1200
T 74.17
L 148.18

Richmond

Park Blvd

RP Hub 20' RP 20' 66+45.83
Hub

30' water lined

Upas St.

Albert

B.M. 188.52 075 Stub

P.O.T. 84+48.18

20' 20' 90°
RP
StubCanyado
Way

P.O.T. 79+38.20

20' 18.5' 90°
RP
Cross Wall

EC 78+44.53

20' 20' 90°
RP
Stub

B.M. 260.88

587 Page 43

RP
Stub
Line only

Δ 50°00'

R 1000'

T 43.66

L 87.26

220'

74+32

90°
19.50' RP 48.20
Cross
CurbR.P. Cross
X on M.H. Road
Vermont

B.C. 77+57.29

20' 20' 90°
RP
StubRP
Stub
Line only
50' on Pepper Tree

EC 77+44.33

Δ 50°05'

R 1000'

T 44.39

L 88.22

R.P. 406

B.C. 76+55.61

Line on M
Just Eo. Brd. Path18' 0"
90°

5th Flc

EC 88+75.95 $\frac{90^\circ}{20'}$ RP Stub RP Stub

 $\Delta 7^\circ 24'$

R 700

T 45.26

L 90.41

BC 87+85.54

RP Stub $\frac{20'}{20'}$ RP Stub

87+74.84 EC

 $\Delta 7^\circ 41'$

R 700

T 47.01

L 93.87

RP Hub $\frac{20'}{20'}$ RP Hub $\frac{20'}{20'}$

86+80.97 BC

< 30' >

Upas St

RP * $\frac{20'}{20'}$ RP * $\frac{20'}{20'}$
Crown Wall Crown Wall

93+49.62 $\Delta 45^\circ 00'$

6th Flc

RP Stub $\frac{20'}{20'}$ RP Stub $\frac{20'}{20'}$
 90°

92+44.70 $\Delta 45^\circ 00'$

Cobble Wall →

Upas Street 30" Pipe Line
Grades

13

0+0

+50

1+0

+50

2+0

+50

3+0

+40 oBrk

3+90

4+40 oBrk

4+80

5+20

5+60 oBrk

6+12.5

6+65 oBrk

7+06.67

7+48.33

4.67

7+90 o Brk

11+80

8+50 o Brk

12+25 o Brk $\Delta 22^{\circ}30'$

4-32.5

8+87.5

12+75

9+25 o Brk

13+25 o Brk

2-48.8

9+62.5

13+73.8

10+0 o Brk

14+22.6 $\Delta 22^{\circ}57'$

5-45

14+20.75

2-39.62

10+45

14+60.37

10+90

15+0 o Brk

4-48.75

11+35

15+48.75

15+97.50

16+46.25

16+95 o Brk
4-35

17+30

17+65

18+0

18+35 o Brk
3-45

18+80

19+25

19+70 o Brk

20+20 o Brk

20+50

20+80 o Brk

21+10 o Brk

21+50 o Brk

21+90 o Brk

22+40

23+90 o Brk
5-49

23+39

23+88

24+37

24+86

25+35 o Brk

2-47.5

25+82.5

26+30 o Brk

26+90 o Brk

4-40

27+30

27+70

28+10

28+50 o Brk

29+0 o Brk

3-41.67

29+41.67

29+83.34

30+35 o Brk

3-45

30+70

31+15

31+50 o Bk
5-48

32+08

32+56

33+04

33+52

34+0 o Bk
1

+50

35+0

+50

36+0

+50

36+90 o Bk
4-52.5

37+42.5

37+9.5

38+47.5

39+0 o Bk
2-35.5

39+95.5

39+91 o Bk
5-00

40+01

40+31 o Brk 42230

40+71

41+11

41+51.69 Δ 23°22'

41+90 o Brk

5-46

42+36

42+82

43+28

43+74

44+20 o Brk

2-30

44+50

44+80 o Brk

45+25

45+90 o Brk

46+6

+40 P.V.C

+70

47+0 E.V.C.
1-31.25

+31.25

+62.50

+93.75

48+25 o.Brk

+50 o.Brk

48+95 o.Brk
3-35

49+38

49+65

50+0 o.Brk

+50

51+0 o.Brk

+50 o.Brk

2-37.5

51+27.5

52+25 o.Brk

8-37.5

52+62.5

53+0 o.Brk

+50

$54+0$ $+50$ $55+0$ $+50$ $55+75 \text{ oBrk}$ $56+75 \text{ oBrk}$ $+43.75$ $57+18.75$ $57+62.50$ $58+06.25$ $58+50 \text{ oBrk}$ $59+0$ $+50$ $60+0 \text{ oBrk}$ $+50$

61+0

+50

+75

o Bt

4.50

62+25

+75

63+25

63 + 75

o Bt

64+25

64+75

65+25

65+75

66+25

66+45.83 B.C.

4.37.045

66+82.87

67+19.92

67+56.96

67+94.01 B.C.

68+0

o Bt

68+21.61 B.C.

4-87045

68+58.65

68+96.70

69+33.74

↑
69+69.79

69+71.15

F.C.

↓
70+0

oBrt

+50

71+0

oBrt

+50

72+0

+50

73+0

+50

74+0 oBrt

74+40 oBrt

74+70 oBrt

74+85 oBrt

2-25

75+10

75+35 oB-k

76+15

76+55.61 BC

3-29.57

76+85.18

77+0 oB-k od

77+14.75

77+44.33 LC

77+57.27 BC

3-29.09

77+86.36

78+15.45 oB-k

78+44.53 oB-k

78+85 oB-k

79+15

79+40

79+70

80+0 oB-k

+50

81+0 oB-k

+50

82+0

82+150 o Brk

2-33.5

82+225

82+15 o Brk

2-33.33

82+52.33

83+91.66

84+30 o Brk

2-27.5

84+57.5

84+85 o Brk

85+10 o Brk

85+40 o Brk

85+75 o

85+85 o Brk

2-32.5

86+17.5

86+50 o Brk

+75 o Brk out

86+80.97 Brk

2-31.29

87+0 o Brk out

87+12.26

87+43.55

272.49 A

12.01

260.48

0.71

261.19 A

12.68

248.51

0.22

248.78 A

12.81

235.97

0.76

236.73 A

12.83

223.90

0.15

224.05 A

12.41

211.64

0.66

212.30 A

13.04

199.26

0.46

199.66 A

11.12

BM 188.52 o 2506.20 A

84+48.18

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

188.52

0.52

194.50 12.0

13.0

C 4.7

207.00 12.0

13.4

C 4.6

220.50 16.2

9.3

C 6.9

228.50 8.2

7.3

C 3.7

241.50 7.3

1.3

C 6.0

254.50 6.7

3.4

C 2.3

0 259.50

260.22 12.0

8.0

C 4.3

0 262.50

262.84 2.7

2.2

C 4.5

263.72 2.8

5.0

C 3.8

Nov. 14-39
S. S. 507
Northboro
Osborne

25

87+74.89 E.C. 2°50'30" 264.59 $\frac{79}{4.2}$
C 3.6 91+0 o Brl

87+85.54 B.C. 2-30.14 288.8 ^{SIX BP} 4 par + 64
 $\frac{4.12}{293.00X}$ 264.89 $\frac{7.6}{4.5}$
 $\frac{10.27}{282.73}$ C 3.1 +50
 $\frac{1.38}{284.11X}$ 0.28

88+15.68 1°14' 284.11X 265.74 $\frac{5.8}{2.2}$
 $\frac{12.85}{271.26}$ C 4.3 92+0 o Brl

88+25 o Brl out 272.49X 266.00

88+45.82 2°28' 268.08 $\frac{16.0}{10.8}$
C 5.2 92+4470 Δ 45°00'
4-2623

88+75.95 E.C. 3°42' 271.09 $\frac{12.0}{7.2}$
C 5.1 +50 o Brl out
92+70.93

89+0 o Brl 273.50 $\frac{10.6}{5.9}$
C 4.7 92+9716

+50 276.25 $\frac{2.8}{2.2}$
C 5.0 93+23.39

90+0 o Brl 279.00 $\frac{5.1}{1.3}$
C 3.8 on par 93+49.62 Δ 45°00'

+50 93+50 o Brl

94+05

94+60

95+15

95+70

Levels over bench line
Vermont St. to 7th.

Hill 11/15/39
Soper Clear
Ramen

27

Sta. +S H.I. -S E/cr Grade Cut

B.M. 4.12 280.53 276.71

73+0.0 1.5 77.0

73+90 5.1 77.1

74+10 x 272.00

74+14 4.1 76.1 271.20 4.9

+32 -20.00% -21.25% 7.1 73.1 267.60 5.8

+45 9.9 70.6 265.00 x 5.6

+50 264.00 263.5 ve

T.P. 2.00 269.63 12.90 267.63

+60 -67.50% -68% 5.0 61.6 257.25 7.3

+70 x 250.50

T.P. 0.46 257.45 12.69 256.99

+83 -18.33% 2.8 54.7 248.12 6.6

75 7.2 50.3 244.00 6.3

+20 -5.0% 248.3 243.00 5.3

+25 9.6 47.9 243.06 4.8

+50 +1.24% 9.7 47.8 243.37 4.7

76 8.3 49.2 244.00 5.2

+20 x 49.4 244.24 5.2

Curb at C.B. 74+38 - 20'R

77.5
73.0
4.5

78.6
67.6
11.0

73.0
65.0
8.0

69.8
63.5
6.3

64.6
7.3

60.7
50.5
9.1

250.3
8.2
258.5
250.5
C.B. 274+70

50.1
49.1
0.9
6.1

48.8
43.1
5.7

247.9
+4
248.3

48.7
43.4
5.3

50.3
44.0
6.3

50.3
44.2
6.1

249.2
+2
247.4

26455.6130	257.45	7.9	49.6	244.13	5.5	50.1 ✓ 40.1 60
+75	-0.30%	7.7	49.8	244.08	5.7	50.7 ✓ 44.1 6.6
77	x	8.1	49.1	244.00	5.1	51.4 ✓ 44.0 7.4
+25	-3.3333%	9.8	47.7	243.17	4.5	48.8 ✓ 43.2 5.6
TP	219	256.79	2.85	247.60		
77+44.33 EC		11.0	45.8	242.52	3.3	47.9 ✓ 42.5 5.4
+17.2780		12.2	44.6	242.09	2.5	45.3 ✓ 42.1 3.2
+60x			44.5	242.00	2.5	44.7 ✓ 2.7
+75		12.9	43.9	242.00	1.9	
78	Level	11.1	45.7			45.7 ✓ 42.0 3.7
+06	x		46.6	242.00	4.6	46.6 ✓ 42.0 4.6
+25	+15.27%	7.3	49.5	244.91	4.6	49.5 ✓ 45.0 4.5
+40	x		51.5	247.20	4.3	51.5 ✓ 47.0 4.5
+12.667%						51.5 ✓ 47.0 4.5
+44.53 EC		9.8	52.0	247.77	4.2	51.7 ✓ 47.3 4.4
+70	x		54.8	251.00	3.8	54.8 ✓ 51.0 3.8
TP	256.23	261.92	0.10	256.69		
+95	+6.3333%	3.2	58.7	253.08	5.6	60.2 ✓ 53.1 7.1
79	x		59.1	253.50	5.6	61.4 ✓ 53.1 8.3
79+15		2.0	259.9	254.06	5.9	63.5 ✓ 54.1 9.4

244.00 4) 3.333
243.17

242.10 23331
16665
243.17 3333
242.00 23331
242.09 097991

12.667
247.20 38001
247.77 50668
247.20 38001

$$\begin{array}{r} 185.3 \\ - 185.4 \\ \hline \end{array}$$

$\begin{array}{l} 84+20 \text{ B.t} \\ 84+30 \\ \hline \end{array} \times +3.913\%$
 B.M. 189.06[✓] 185.4 177.00 8.4[✓] 85.2[✓]
 3.2 185.9[✓] 181.00 4.9[✓] 6.2[✓]
 0.48 188.57[✓] S. side Canyon Way
 R.P. hub 20 V. 8.4 + 48.18 (Sisson E. 188.52)

$+13.636\%$
 84+37.5+T.P. 12.96 201.60[✓] 0.41 188.64[✓] 184.75 3.8[✓] Offset hub - 84+37.5
 $\begin{array}{r} 888 \\ 845 \\ \hline 40 \end{array}$

84+85 8.7 192.9[✓] 188.50 4.4[✓] 92.6[✓]
 $\begin{array}{l} 85+10 \\ \hline \end{array} \times +24.00\%$ 2.3 199.3[✓] 194.50 7.8[✓] 4.1[✓] 99.5[✓]
 5.0[✓]

$\begin{array}{l} 85+40 \\ \hline \end{array} \times +41.667\%$
 T.P. 12.36 213.96[✓] 0.00 201.60[✓]

85+40 2.3 211.7[✓] 207.00[✓] 4.7[✓]

T.P. 13.05 226.95[✓] 0.06 213.90[✓]

$\begin{array}{l} 85+75 \\ \hline \end{array} \times +43.75\%$
 T.P. 13.09[✓] 239.55[✓] 0.49 226.46[✓]

85+75 12.0 227.6[✓] 222.31[✓] 5.3[✓] 25.6[✓]
 $\begin{array}{r} 25.6 \\ 22.3 \\ \hline 3.3 \end{array}$

85+85 7.3 32.3[✓] 226.69.5[✓] 5.6[✓] 3.7[✓]

T.P. 12.61 252.14[✓] 0.02 239.53[✓]

$\begin{array}{l} 86+17.5 \\ +20 \\ \hline \end{array} \times +38.333\%$
 T.P. 12.88 264.98[✓] 0.01 252.13[✓] 6.6[✓] 247.5[✓]
 $\begin{array}{r} 247.5 \\ 241.7 \\ \hline 5.8 \end{array}$
 $\begin{array}{r} 46.6 \\ 40.9 \\ \hline 5.7 \end{array}$
 7.1 257.9[✓] 253.50[✓] 4.4[✓] 5.3[✓]

		+20.00%							
		264.98 ✓							
86+80.97	x	3.0	2.4	264.6	259.56	5.1	✓		
		+9.333%							
T.P.	x	9.23	0.45	264.53	262.30	5.0	✓		
+10	x		6.4	267.3	262.36	5.0	✓		
87+12				267.4	262.36	5.0	✓		
		Reset							
		267.4		263.28		4.1			
+43.5		6.2		267.6	263.28	4.3	✓		
+74.04 EC		5.5		268.3	264.19	4.1	✓		
BC		5.6		268.2	264.50	3.7	✓		
+15.6		3.7		270.1	265.37	4.7	✓		
+20	x			270.6	265.50	5.1	✓		
88+46		0.1		273.4	268.1	5.3	✓		
T.P.		12.42	0.60	273.16					
		EC							
+76		2.1		276.3	271.1	5.2	✓		
89		7.5		278.3	273.5	4.8	✓		
+50		4.2		281.4	276.2	5.2	✓		
T.P.		9.33	0.19	285.39					
BM.		6.34		288.39					

Preble lot cor. 6th & Upas

Grades Park Blvd to Vermont

32

Ground Grade Cut

Brass plug S.W. cor. Upass P. Blvd.

BM 3.65 299.45 295.80

56+50-60 ft. 14 3.8 295.7

56+75 " 3.6 95.9 289.5 6.4

57+00 " 4.0 95.5 289.2 6.3

57+50 " 4.5 95.0 288.6 6.4

58+00 " 5.1 94.4 288.1 6.3

58+50 " 5.8 93.7 287.5 6.2

59+00 " 6.3 93.2 287.0 6.2

TP 2.83 296.08 6.20 293.25

59+50 " 3.5 92.6 286.5 6.1

60+00 4.0 92.1 286.0 6.1

60+50 4.6 91.5 284.9 6.6

61+00 5.1 91.0 283.9 7.1

95.7
58.8
6.9

95.1
59.5
6.0

95.3
6.1

94.5
5.9

94.6
58.1
6.1

93.3
5.8

93.4
67.0
6.6

92.3
5.5

92.3
66.0
6.3

91.0
6.1

91.2
62.9
7.3

296.08

61+50 6.0 H. Lt.

5.7

290.4 ✓ 282.8

7.6

89.7
82.8
6.9

61+75 "

6.0

90.1 ✓ 282.3

7.8

89.5
7.2

TP

1.71

291.64

6.15

289.93

62+00 "

1.8

89.8 ✓ 282.2

7.6

90.1
82.2
7.9

62+50 "

2.4

89.2 ✓ 282.1

7.1

88.8
6.8

63+00 "

2.9

88.7 ✓ 281.9

6.8

89.0
81.9
7.1

63+50 6.0 H. Lt.

3.5

88.1 ✓ 281.8

6.3

87.6
81.8
5.8

63+50 8.0 H. Lt.

3.6

88.0 ✓ 281.8

6.2

63+75 "

3.8

87.8 ✓ 281.7

6.1

87.4
5.7

64+00 "

4.2

87.4 ✓ 281.5

5.9

87.5
81.5
6.0

64+50 "

4.8

86.8 ✓ 281.0

5.8

86.5
5.5

65+00

5.2

86.4 ✓ 280.4

6.0

86.8
80.4
6.4

N.B. Excav. carried
as below grade
from 64+50 to 79+50
for sand backfill

29164

65+50 8' H RT

5.8 285.8 ✓ 279.9

5.9

85.5
5.6

66+00 "

6.4 85.2 ✓ 279.4

5.8

86.2
79.4
6.866+45⁸³ " B.C.

6.8 84.8 ✓ 278.8

6.0

84.4
5.6check on
66+45⁹³

7.32 84.32 ✓

66+75 8' H RT

7.1 84.5 ✓ 278.6

5.9

84.0
5.4

67+00 "

7.4 84.2 ✓ 278.3

5.9

84.2
78.9
5.3

67+25 "

7.8 83.8 ✓ 278.0

5.8

85.5
78.0
7.5

67+50 "

8.3 83.3 ✓ 277.8

5.5

85.4
77.8
7.6

67+75 "

8.9 82.7 ✓ 277.5

5.2

82.8
5.367+94⁰¹ " E.C.

8.6 83.0 ✓ 277.3

5.7

83.5
6.2

B.M. 9.50 285.91

276.41

68+21.6⁶ B.C. (8' H RT)

3.2 82.7 ✓ 277.1

5.6

82.6
5.3check on
67+94⁰¹

2.9 83.0 ✓

68+50 "

3.5 82.4 ✓ 276.5

5.6

82.7
76.5
6.2

69+00 "

4.1 81.8 ✓ 276.4

5.4

82.0
76.4
5.6

Corbat CB 20R 74+38

285.91

69+50 (R.H. Rd)

4.7

281.2 ✓ 275.9

5.3

81.3
75.9
5.469+69.79 Back
69+71.15 Ahead E.C.

5.0

80.9 ✓ 276.7

5.2

81.0
5.3

70+00 "

5.4

80.5 ✓ 276.5

5.0

80.7
75.4
5.3

+50 "

5.7

80.2 ✓ 274.6

5.6

80.0
5.4

71+00 "

5.2

80.7 ✓ 273.8

6.9

80.4
6.6

71+50 "

5.1

80.8 ✓ 273.5

7.3

80.8
7.4

72+00 "

5.2

80.7 ✓ 273.2

7.5

80.9
7.7
7.7

72+50 "

5.6

80.3 ✓ 272.9

7.4

80.4
7.4272.0
6.4
6.4

73+00 "

6.4

79.5 ✓ 272.6

6.9

78.9
7.6
7.677.4
6.2
71.0

73+50 "

7.7

78.2 ✓ 272.3

5.9

78.0
5.7

74+10 "

8.3

77.6 ✓ 272.0

5.6

77.5 ✓
5.5

74+50

12.64
1.9
14.5

14.5

71.4 ✓ 264.0

7.4

Grades Park Blvd to Balboa Park Carline 293.18

Hill
Soper
Remmen

36

			Elev.	Grade	Cut	
B.M.	7.45	300.25	295.80		95.5	Brass plug S.W. cor. Upas & Park Blvd.
56+30.5		4.2	296.1	290.4	5.7	W. side corner box Park Blvd.
56+13		4.3	96.0	290.4	5.6	95.8 5.4
56+7.5		4.2	96.1	290.25	5.8	96.0 5.7
55+50		4.4	95.9	290.2	5.7	95.9 90.2 5.7
55+00		4.7	95.6	290.0	5.6	95.4 90.0 5.4
54+50		5.0	295.3	289.8	5.5	95.0 89.8 5.2
54+00		5.3	295.0	289.6	5.4	94.7 89.6 5.1
53+50		5.7	94.6	289.4	5.2	94.5 89.4 5.1
53+00		6.1	94.2	289.25	5.0	94.0 89.3 4.7
52+50		6.4	93.9	288.6	5.3	93.9 88.7 5.2
52+25		6.5	93.8	287.8	6.0	94.0 88.7 5.3

Emil E. Kirk

7.0 C 293.17

Elevs in Canyonada Way - after heavy rain late PM. 11/27/38

Elevs, taken 9 AM 11/28/39

Hill
Brochmann

80th peg 89+00 4.25 189.7

185.4

83+70 18'N

3.5

186.2

High water mark

83+35 ♀

3.3

186.4

"

"

"

84+65 ♀

3.0

186.7

"

"

"

83+70 sluff in trench 4.0 below nat. grd.

83+35

"

"

"

3.0

"

"

"

83+22

"

"

"

5.0

"

"

"

			Elev.	Grade	Pipe grade to exist 16" M.	
B.M.	87.7	301.47	298.80			B.P. S.W. cor Upas & Park
Top 16" pipe	8.75		292.72			
	6.2				grade at 16" cross	292.7
	<u>5.5</u>	289.8	290.3	290.7	Trench at 55+99	<u>0.7</u>
	11.7					292.00
	<u>5.35</u>				grade at 16" cross	<u>1.35</u>
	<u>7.65</u>					290.65
	13.00	288.47	290.2	290.7	" " 56+42	
	12.2	289.3	289.5			
	6.7	295.8	289.5	6.3		
55+75	11.4	290.1	290.25			

Coffs 56+75 4.9 300.8 295.9
 2.2 399.3 8.7 392.1
 4.9 389.4
 290.6 3.7

Top 16" pipe 1.5 294.2 292.7
 3.9 290.3
 0.8 293.5 292.7
 290.6 2.9
 3.3 290.2

292.7
 1.3
 294.0
 3.4
 290.6
 292.7
 3.2
 269.5
 292.7
 2.1
 2.4
 290.6
 2.1
 2.4
 290.6

12/9/90

Hill
Brachmann

40

Levels over portion backfilled with sand - Sta. 74+50 to Sta. 64+50

B.M.	9.10	285.51	276.41
74+50		17.6	267.9
74+10		11.7	74.1
73+50		10.2	75.3
73		9.5	76.0
72+50		9.4	76.1
72		8.9	76.6
71+50		8.6	76.9
71		8.3	77.2
70+50		7.7	77.8
70		6.9	78.6
69+71.15			
69+69.79 E.C.		6.5	79.0
69+50		6.0	79.5
69		5.6	79.9
68+50		5.1	80.4
T.P.	8.14	290.86	279 282.72
68+21.6 B.C.		10.2	80.7
67+94		10.0	80.9
67+75		9.7	81.2
67+50		9.5	81.4
67+25		9.3	81.6
67		9.2	81.7
66+75		9.1	81.8
66+45.8 B.C.		8.9	82.0
66		8.3	82.6

Curb at C.B. 20' R 74+38

290.86

65+50	7.7	283.2
65	7.1	83.8
64+50	7.0	83.9
" R.H. 80 ft	4.12	286.74

Sand Backfill at car tracks

B.M.	5.8	299.0	293.2
52+68	7.0	292.0	
T.P.	3.3	297.0	5.3 293.7
52+50	5.6	291.4	
52+25	6.1	290.9	
52+00	5.6	291.4	
51+46	7.4	289.6	
51+75	7.0	290.0	

E. rail / E. track

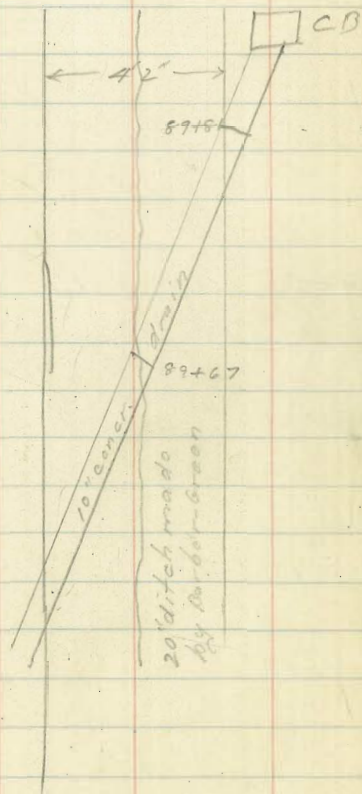
Loc. 10" drain at 7th St.

4.3	285.7	281.4	6' offset plug 29+50
E. end 10" pipe	5.6	280.1	
W. " " "	5.2	280.5	

2.6

5.5

5.9



Photos

1/11/40 Repairing tel. cable cut by jack-hammer at 28th St.

1/11/40 Material encountered in trench near 28th St.

1/12/40 Gate valve chamber at Park Blvd.

1/17/40 Placing & compacting sand backfill near 28th St. (4, 5, & 6)

1/18/40 Placing rubber insulation on pipe

1/19/40 Trench showing sec. too hard for trench machine at about sta. 6+00.

1/27/40 172 shooting in trench on westerly side of 5th St.

Levels over 8' offset pts. 5th Ave to end of pipe sta 87+03

B.M.	3.90	292.76		288.86		Brass plug S.W. cor. 6th & Upas
96+49.75			8.0	84.8	280.0	4.8 6.2
96+09.75			7.6	85.2	280.3	4.9 6.4
95+69.75			7.0	85.8	280.50	5.3 6.9
95+50			6.8	86.0	280.7	5.3 7.0
95			6.0	86.8	281.2	5.6 7.0
94+50			5.3	87.5	280.6	5.9 6.9
94			4.4	88.4	281.3	6.3 7.1
93+49.62 Δ pt.			3.6	89.2	282.50	6.7 7.1
93			3.3	89.5	282.8	5.5 5.7
92+44.70 Δ pt.			2.9	89.9	285.50	4.4
T.P.	0.85	290.78	2.83	289.93		
89+80			8.3	82.5	277.3	5.2
11' line culvert Sta 89+80			10.3	80.5		
11' line culvert Sta 89+67			10.9	79.9		
89+50			9.5	81.3	270.2	5.1
89+00			12.8	78.0	272.3	4.7
P	1.10	278.99	12.89	277.89		
88+76			2.8	76.2	271.1	5.1
88+46			5.6	73.4	268.3	5.1
88+20			8.2	70.8	266.3	4.5
87+85 ± B.C.			11.0	68.0	264.6	3.4
87+74 ± E.C.			11.5	67.5	264.2	3.3
87+43 ±			11.5	67.5	63.3	
P	4.41	272.49	10.91	268.08		
Tap off pipe 87+03			8.60	63.9	261.2	5.0 + 8.3
" " 86+87 ±			9.70	62.8		
						7.86 264.63

Note Grade dropped for connection

with 16" main on 5th st

2.0
283.2 top 16" main
at sta. 96+00

Set B.M. C.4.2
Rail in tree 87th Sta 86+74

Sand Backfill

Sta 45+12 to sta. 45+92 to spring line of pipe (2) cut 0.5 below grade

Sta. 48+20

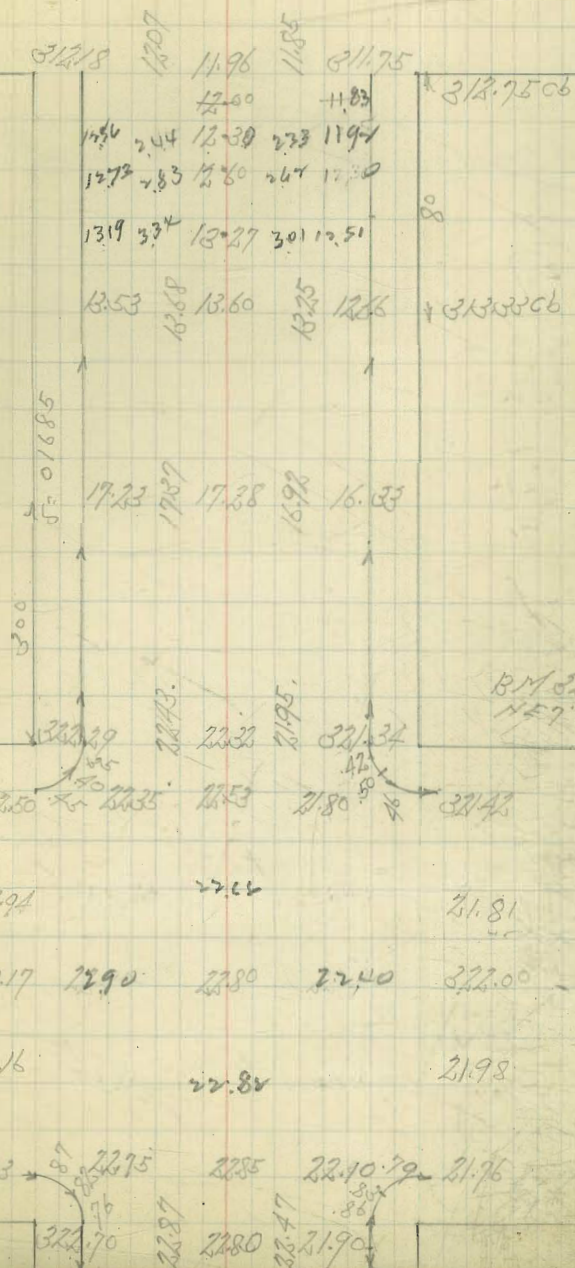
Elev. of 24" pipe at W. end of line

B.M.	2.48	291.34	288.86
96+66.4		10.75	280.59

Lead plug S.W. cor 6th & Upas
Top of 24" C.I. Pipe at W. end

BM 3/4.46
NE 3' CT.

Hightman



E 0.46

22.94

22.26

21.81

E 0.41

Landis

22.17

22.90

22.80

22.40

322.00

23.16

22.82

21.98

22.93

22.75

22.85

22.40

21.76

322.70

22.87

22.80

22.47

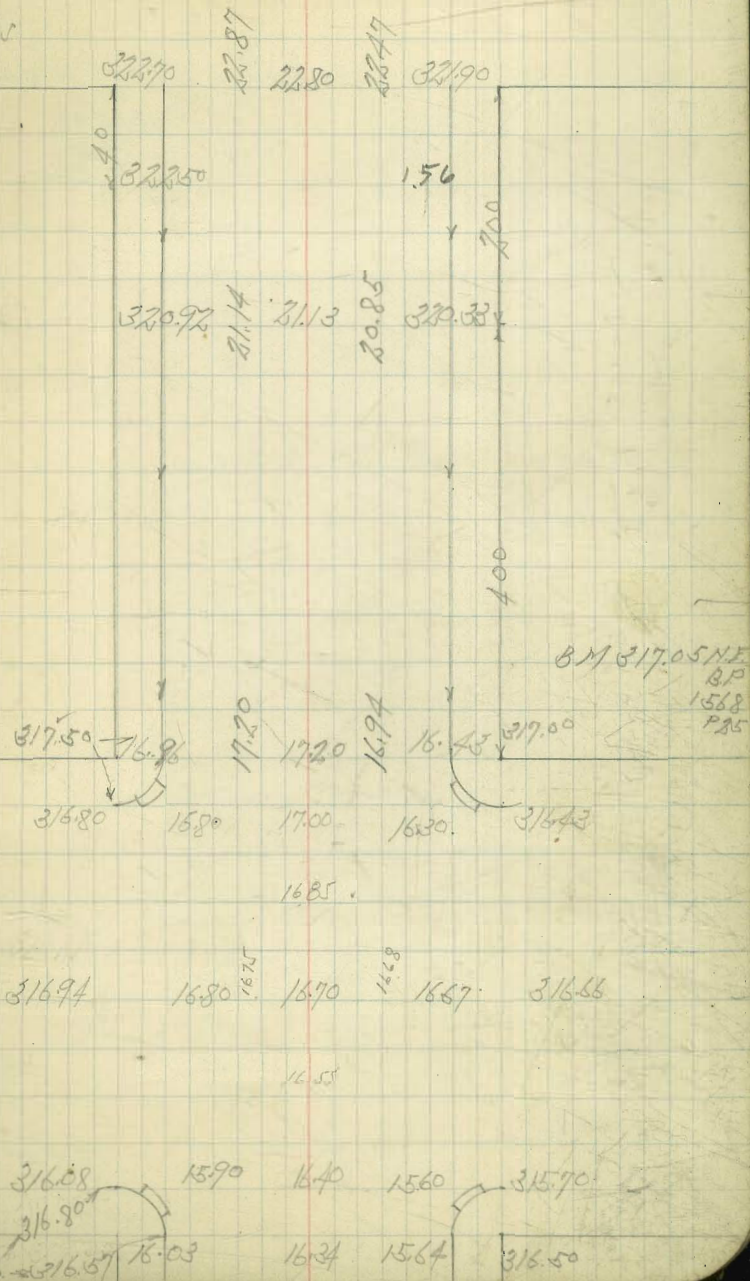
21.90

Hile St. Por 149

47

BM 365 520.70 317.05 HFBP
 S.H. Return HFBP SFBP
 317.00
 3.70

Londis



88'50m 961	129'5	170'5	211'50m 1961	261'5
316.28	316.18	316.08	315.97	15.85
4.91	5.01	5.11	5.22	5.31
		✓	5.38 on C6	5.23 on C6
C3 19 ONC1				

321.1705 NE
 4.14 DR
 321.19 T

$$0 \times 0.2$$

Prk

Next cb. on Next

0748

CB3/6.03

Myrtle

BM 3/4 5455

Hila St. Paving

Myrtle

14.48 Pav

14.02 Pav

344.33

14.57

14.58

14.32

313.82

250

11.83

12.19

12.28

12.14

11.74

50

11.08

11.46

11.58

11.46

11.08

50

9.73

10.16

10.24

10.25

9.90

240

304.63

31.16

303.37

3.36

303.11

B.M. 1128P
303.69

3028.6 Pav

3029.5 Pav

T. born

Paving Grades Alley Block 1 City Heights
Between Fairmount & 44th St.
University to Polk

Indexed

Sept 28-40
Sisson
Northbury
N. H.

51

4452	556.90	5.09 3.61 1.48	556.90	5.09 3.61 1.48
------	--------	----------------------	--------	----------------------

3×98

$$\begin{array}{r} 6.13 \\ 4.58 \\ \hline 57.06 \\ 51.55 \end{array}$$

$$\begin{array}{r} 6.13 \\ 6.11 \\ \hline 20.02 \end{array}$$

3+44	357.21	5.98 5.60 FO.38	5.98 5.60 CO.34
------	--------	-----------------------	-----------------------

2490 357.36 $\frac{5.83}{6.02}$ $\frac{5.83}{6.02}$

2436	357.51	5.68 5.76 5.96 FO.48	5.68 5.76 5.96 FO.48
------	--------	-------------------------------	-------------------------------

1 + 82	357.66	$\begin{array}{r} 5.53 \\ 5.07 \\ \hline 10.60 \end{array}$	$\begin{array}{r} 5.53 \\ 8.77 \\ \hline 14.30 \end{array}$
		50.57	10.64

1+28 557.82 5.37
 3.28
 7.59 5.37
 4.39
 0.98

0x74	357.99	$\begin{array}{r} 5.22 \\ 2.48 \\ \hline 7.70 \end{array}$	$\begin{array}{r} 5.51 \\ 5.05 \\ \hline 10.56 \end{array}$
------	--------	--	---

$0 + 20 = F.V.C.$
 $358 \frac{1}{2} \circ$
 $\begin{array}{r} 536 \\ 116 \\ \hline 120 \end{array}$
 $358 \frac{1}{2}$
 $\begin{array}{r} 536 \\ 116 \\ \hline 650 \end{array}$

07/10 $258.15 \overset{5.33}{\overset{2.25}{\underset{0.58}{\text{c}}}}$ $258.12 \overset{5.06}{\overset{5.26}{\underset{0.10}{\text{c}}}}$

0+0	342.61	358.16	532	358.06	5.42
			✓		5.41

BM 357.75 LIT. A/1/1/6'5
H.L. Univ.

65.73
263.48x

358.85

$$\begin{array}{r} 4.37 \\ 253.19 \end{array}$$

3 5 7 8 9

$$\begin{array}{r} 4.13 \\ 261.99 \pi \end{array}$$

0.571
 4.845
 357.1

506
362.17

5198.85 = 52 Polk 556.58 ^{5.59} ✓

$$5 \times 80 = 400$$
$$5760 = P.V.C. \quad 356.60 \quad \begin{array}{r} 5.39 \\ 0.85 \\ \hline 61.59 \end{array}$$

57.06 356.75 5.34
437
6087

556.05 6.12

556.56

556.60 5.39
4.36

356.75

Paving Grader Alley Block 25 Terra to
Between Marlborough & 42nd St
From Orange to E. Cajon Blvd

N

E

3+50 $\frac{4.54}{4.13}$ 364.27 364.27 $\frac{4.54}{3.85}$
CO.41 CO.59

3+0 $\frac{4.66}{4.51}$ 364.15 $\frac{4.66}{4.07}$
CO.15 CO.62

2+50 $\frac{4.79}{4.70}$ 364.02 $\frac{4.79}{4.78}$
CO.09 CO.61

2+0 $\frac{3.90}{3.85}$ 363.90 $\frac{3.90}{3.96}$
CO.06 CO.44

1+50 $\frac{4.03}{3.78}$ 363.77 $\frac{4.03}{4.31}$
CO.25 FO.31

1+0 $\frac{4.15}{3.78}$ 363.65 $\frac{4.15}{4.30}$
CO.37 FO.05

0+50 $\frac{4.28}{3.85}$ 363.52 $\frac{4.28}{4.01}$
CO.63 CO.27

0+0 N. Orange 363.40 363.40 $\frac{4.40}{4.39}$
4.40 on Pav

Indexed

B/M 362.78 NW BP
5.02 Orange
Marlborough

367.80 X

3.88

363.92

4.89

368.81 X

4.11

364.70

4.93

369.63 X

N

July 2-40
Survey
Northway 52
Winters

6+07 E. Cajon 364.80 4.83
4.81 on Pav

364.70 4.93
4.98 on Pav

5+80 B. L. 364.85 4.78
4.82

364.85 4.78
4.82

5+40 $\frac{4.88}{5.03}$ 364.75
FO.15

$\frac{4.88}{5.03}$
CO.05

5+0 $\frac{4.98}{5.15}$ 364.65
CO.23

$\frac{4.98}{5.15}$
FO.11

4+60 - Sewer Location F

259.55 10.08
5.20
4.88

4+50 $\frac{5.16}{5.08}$ 364.52
CO.03

$\frac{5.16}{5.08}$
CO.03

4+0 $\frac{4.41}{4.44}$ 364.40
FO.03

$\frac{4.41}{4.44}$
CO.57

Bridge For National Avenue
East of 41st Street

BM	1.06	36.31		35.25
TP	4.99	29.64	11.66	24.65
BM			10.48	19.16

Deck Grade 27.92

BM	0.84	36.09		12.92
TP	4.17	30.16	10.40	25.69
W End Bridge on Pavement			2.23	27.93
E " " " "			2.07	28.09

Note - Changed See Next Page

N.H.B.P.
National
+410

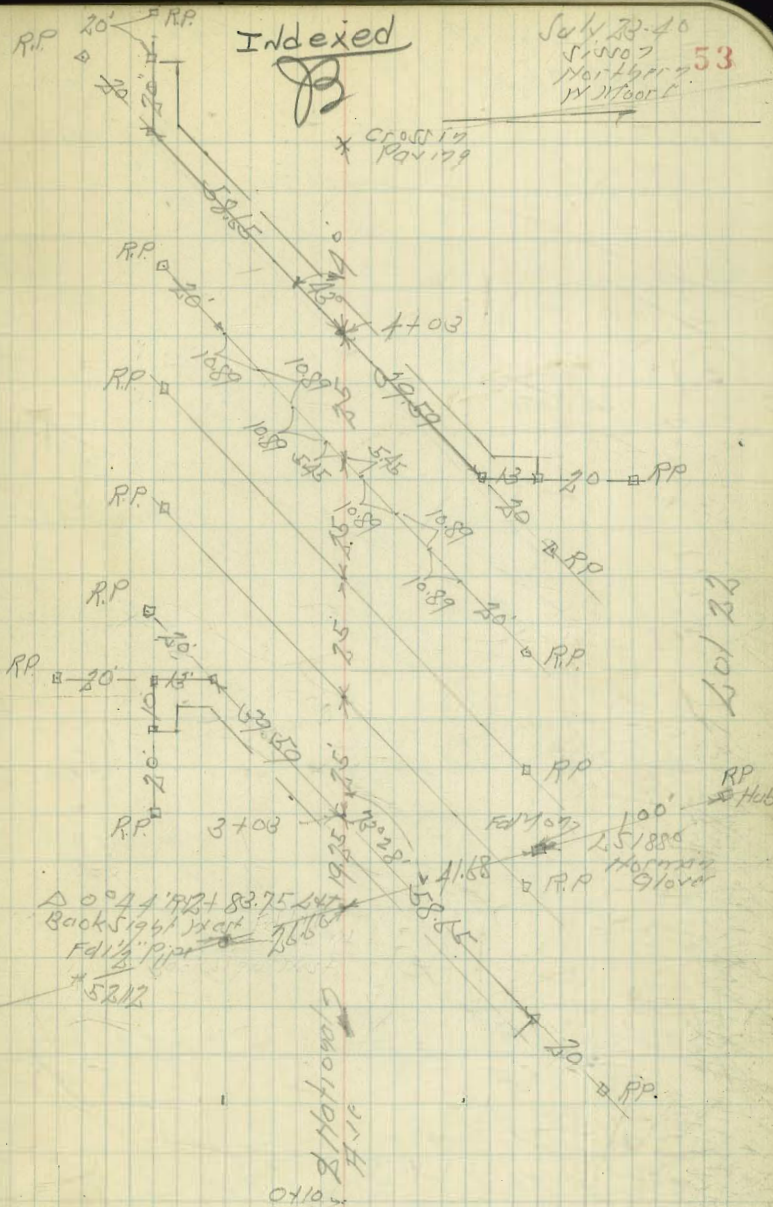
Mon 5th
Cor. Bridge
on Broadway

N.H.B.P.
National
+410

Lot 31 Caruthers Add

Indexed

July 23-40
S. 10007
North 10007
W. 10007
53



N.L. 41st St

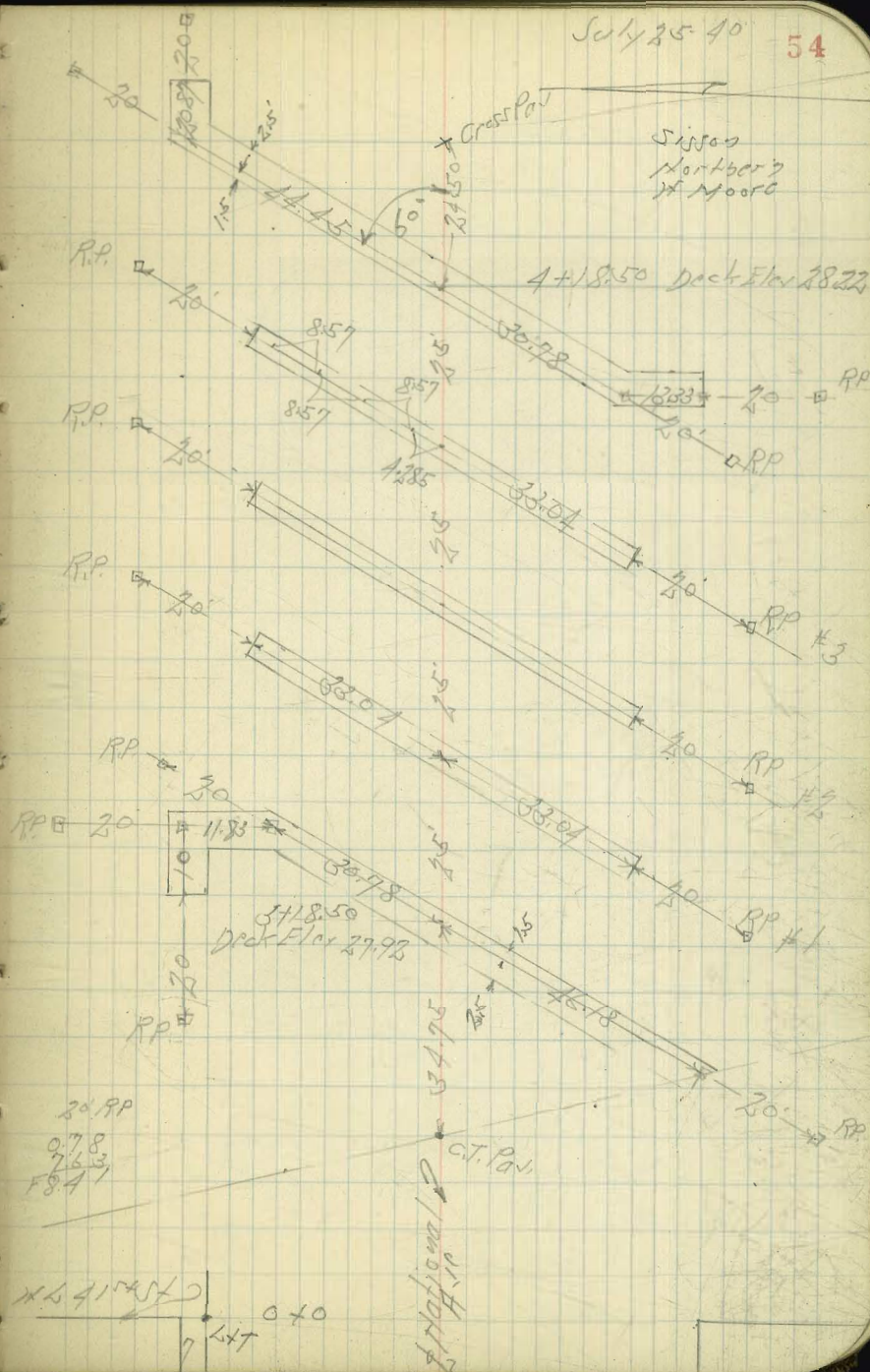
NT

7 33 40

National Avenue Bridge
East of 41st St.

July 25-40 54

	0220 RP	Jack Grader S	0220 RP
4+18.5 = E Abut.	-1.08 6.61 F 6.69	28.22	-1.08 6.62 F 6.30
3+93.5 = Bent #3	-1.01 6.57 F 7.58	28.15	-1.01 6.62 F 6.70
3+68.5 = Bent #2	-0.93 6.02 F 7.01	28.07	-0.93 6.66 F 7.59
3+43.5 = Bent #1	-0.86 4.66 F 5.52	28.00	-0.86 8.62 F 9.45
3+18.5 = W Abut.	-0.78 4.21 F 5.99	27.92	-0.78 7.83 F 8.60
BM	798	27.14	19.16



Grades 6.33 below Deck Grade
or 2' below Hatches

or 2' below Hensch

Grades 6.33 6e/ox Deft Grade

BM 19% Moss 100%
BM 19% Moss 100%

22/19/6

Grades 6.33 6e/ox Deft Grade

This image shows a blank, aged, cream-colored page, likely an endpaper or flyleaf of a book. The paper has a slightly textured appearance with some faint horizontal lines and minor discoloration or foxing, characteristic of old paper. The page is oriented vertically and appears to be part of a bound volume.

DATE	TIME	TEMP.	WIND	WAVE	SEA	WIND	WAVE	SEA
2096	21.40	21.49	21.58	21.57	21.45	21.32	20.88	
2099	21.45	21.46	21.37	21.38	21.50	21.32	20.88	
						2.73	3.07	

Box #	21.04	21.36	21.57	21.66	21.65	21.53	21.40	20.96
	2.59	2.38	2.29	2.30	2.43	2.65	2.90	2.99

Bout #7	21.11 884.
	21.43
	.3164
	3173
	2160
	21.87
	21.02

Boat #	3.19	3.15	3.17	3.18	3.18	3.145	3.11
	2.96	3.44	2.33	2.1	2.1	2.50	2.01

Sept 25/88

Haunch: 4.336 below Finish Grade

3729	27.27	27.44	27.52	27.59
------	-------	-------	-------	-------

27.61	27.69	27.76	27.84	27.91
-------	-------	-------	-------	-------

27.82	27/90	27/97	28.05	28/12
-------	-------	-------	-------	-------

37/9	27/99	28/06	28/14	28/21
------	-------	-------	-------	-------

27.92	28.00	28.07	28.15	28.23	28.31
1054					1055

157/90	2798	2805	2813	2820
--------	------	------	------	------

37/78	37/88	37/93	38/01	38.08
-------	-------	-------	-------	-------

27/55	27/63	27/70	27/78	27/83
-------	-------	-------	-------	-------

2721	2729	2736	2744	2751
------	------	------	------	------

WCSX.

15.14

18.6

26.0

East

Paving Grader Alley Block 5 N 16 1/2 W 10 E Place
Between Mor/borough + 42nd St.
100' N of N 16 E / Coyote Blvd.

BM 462 369.76 365.14
N S F
SW BP
F / Coyote
Mor/borough

Indexed
Jy

July 31 40
Sunny
North 3/4 W
by Moore 56

1+0 = N 1/4 mp 364.60 364.40 364.60
5.16
4.82
C 0.59
5.16
4.82
C 0.28

0+62.5 364.52 364.52
5.24
4.82
C 0.57
5.24
5.04
C 0.20

0+27 = 8 1/4 mp 364.45 364.25 364.45
5.31
4.82
C 0.76
5.31
5.14
C 0.17

0+0 N 16 E / Coyote 364.59 364.19 364.59
5.17
4.82
C 0.45 Top CB
5.17
4.82
C 0.55 Top CB

0-25 N 16 E / Coyote 364.14
5.62
5.64 on Pav

Sewer Grades 60th St
 Estelle St North 375 to DE
 offset 6' West

Indexed
 JB

Aug. 12, 40
 Survey
 North 375
 to 2nd St
 8/1/40

57

0+0	= N.H. of Estelle From E	414.00	11.46 11.45
0+41.25		415.98	9.48 3.21 0.5.57
0+82.50		417.96	18.17 12.50 0.5.67
1+23.75		419.94	16.19 10.12 0.6.69
1+65	= Grk	421.92	14.81 7.83 0.6.93
2+20		426.04	10.09 3.05 0.7.04
2+75	= DE	430.17	17.34 9.59 0.7.75

B.M.	7.20	478.48	471.28	N.W. 8 P E. 1/4 1/4 1/4 1/4
TP	0.87	470.99	7.86	470.62
B.M.		4.87	466.12	N.W. 100 E. 1/4 1/4 1/4 1/4
TP	6.22	470.84	6.37	464.62
TP	0.58	459.45	11.97	458.87
TP	0.14	447.51	12.08	447.37
TP	0.97	436.13	12.35	435.16
TP	1.83	425.46	12.50	423.62
B.M. Set		6.80	418.66	N.W. 8 P Estelle 460th St

Paving Grader Alley Block 189 Clon. Hts
Lincoln Ave to Polk Ave
Between Hamilton & Oregon

W

E

2+80 = E.V.C.	351.74	^{3.00} F0.36	352.04	^{3.70} C0.61
B.M. 350.93	^{S.F.R.P.} 351.26	^{3.48} F1.16	351.56	^{3.18} C0.79
2+60	352.55	^{4.02} F1.48	350.66	^{3.78} C0.70
2+40	339.62	^{4.78} F0.61	349.96	^{4.10} C1.54
2+20	345.81	^{5.59} F1.73	349.15	^{5.29} C1.16
2+0	352.41	^{6.31} F1.17	348.23	^{6.31} C2.32
1+80	356.90	^{7.52} F0.96	347.20	^{7.74} C0.43
1+60	P.V.C.	^{8.56} F1.86	345.03	^{9.41} C0.20
1+20		^{3.66} F0.35	342.87	^{3.36} C0.95
0+80		^{5.83} F1.11	340.70	^{5.53} C0.27
0+40	= E.V.C.	^{7.06} F0.66	339.47	^{6.55} C0.77
0+20			339.98	
0+0 = H.L. Lincoln	337.95		339.10	

Indexed
JH W

Aug. 20-40 58
S. 1007
North 1007
Bluff
E. W. Moore

6+0 = S.L. Polk	357.60	^{4.47} F0.17	358.08	^{3.98} C1.29
5+80 = P.V.C.	357.40	^{5.08} F0.17	357.29	^{4.78} C1.43
5+50	356.99	^{5.49} F0.04	356.58	^{5.19} C1.28
5+20 = E.V.C.	356.58	^{5.78} F0.22	356.29	^{5.48} C0.60
5+0	356.29	^{6.11} F0.61	355.96	^{5.90} C0.64
4+80	355.96	^{6.57} F0.44	355.18	^{6.27} C0.57
4+60	355.59	^{6.84} F1.05	354.32	^{6.26} C1.42
4+40 P.V.C.	355.18	^{5.70} F1.01	353.46	^{5.40} C0.49
4+20	354.32	^{6.14} F1.50	352.60	^{6.26} C1.20
3+60	353.46		352.90	
3+20	352.60		352.90	

Guy St Grader
Hortensia East

Costa Rica
Sept 17-40

Indexed
S

Sept 2-40
Simoes
Hortensia
W Moore
S 59

BM 195.78 H.E. Top
12.23 Hortensia
Guy
208.01 K
205.1
207.50
7.66
215.16 X

195.78 BM
10.75
206.53 X
1.42
205.11
8.74
211.85 X

HCB

S

3+0 = W.L. 1603

22590

22540

3+60

3+20

1+80 = E.V.C.	209.10	308.66
1+75 End ch.	208.44	307.94
1+60	206.45	305.95
1+40	204.11	303.61
1+20	202.06	301.56
1+0	200.32	199.82
0+80	198.89	198.39
0+60	197.75	197.35
0+40	196.92	196.42
0+10	195.90	195.40
0+0 = F.L. Hortensia	195.65	195.20
C.B.F.C.	195.68	1058

209.10	308.66
206.45	305.95
202.06	301.56
198.89	198.39
196.92	196.42
195.65	195.20

Paving Alley Block 8 Altadena
From Thorne to Cedar Bay on Bancroft Road

Indexed

Spot 17.10
Sutton 60
Northcott
H Moore
E

	N	E
3+70	315.69 5.23 4.54 c0.57	315.78 5.41 4.42 c2.73
3+20 = EVC	314.04 6.88 6.21 c0.17	314.20 6.72 5.50 c1.22
3+0	313.42 7.44 6.42 c1.02	313.66 7.36 5.92 c1.34
2+80	313.12 5.86 4.03 c1.23	313.32 5.66 4.21 c1.37
2+60 = P.V.C.	312.96 4.21 3.59 c0.22	313.16 5.02 4.01 c1.16
2+10	312.81 4.36 3.57 F1.21	313.01 5.07 4.16 c1.52
1+60	312.66 4.35 3.75 c0.60	312.86 4.15 3.07 c2.08
1+10	312.51 4.56 3.46 c0.64	312.71 6.22 3.89 c2.67
+60	312.36 4.40 1.62 c2.78	312.56 6.62 3.82 c1.74
+40	312.27 4.49 3.89 c0.60	312.49 4.68 3.82 c0.86
+20	312.13 4.63 3.67 c0.96	312.40 4.36 3.91 c1.45
0+0 = N.B.T. Loc 2	311.96 5.25 5.06 c0.19	312.29 4.69 3.97 c0.72

BM 314.69	318.59 6.15 324.74X
317.17X	318.59 6.15 324.74X
314.01	318.59 6.15 324.74X
318.98X	318.59 6.15 324.74X
313.59	318.59 6.15 324.74X
323.93X	318.59 6.15 324.74X
318.59	318.59 6.15 324.74X
5+98.15 = S.L. Up on 320.36	4.38 4.40 on P.V.C.
5+80	320.59 4.15 3.21 c0.94
5+60	320.61 4.13 3.32 c0.87
5+40 = P.V.C.	320.31 4.43 3.45 c0.78
5+0	319.38 5.36 4.76 c0.60
4+60 = E.V.C.	318.46 6.28 5.37 c0.41
4+40	317.95 2.97 1.26 c1.61
4+20 = P.V.C.	317.34 3.58 2.07 c1.51

314.69	4.68 4.76 c0.02
316.76X	4.68 4.76 c0.02
315.14	4.68 4.76 c0.02
317.01X	4.68 4.76 c0.02
313.52	4.68 4.76 c0.02
317.17X	4.68 4.76 c0.02
320.06	4.68 4.76 c0.02
320.51	4.68 4.76 c0.02
320.59	4.68 4.76 c0.02
320.31	4.68 4.76 c0.02
319.38	4.68 4.76 c0.02
318.46	4.68 4.76 c0.02
317.96	4.68 4.76 c0.02
317.37	4.68 4.76 c0.02

	X	F
5470.8: 52 019291375.60	548 5470.8	543 375.65 5420.8
5450.8	375.84 544 4.62 C0.72	376.00 548 3.57 C1.47
5430.8 - PIC	375.74 542 3.02 C0.86	375.94 544 4.41 C0.70
4482.23	375.15 541 3.05 C0.56	375.25 541 3.16 C0.15
4460 DONT	8.67 543 3.24 C5.43	370.09
4433.66	374.57 542 4.12 C0.19	374.77 540 3.87 C0.12
3785.09	373.98 548 4.27 C0.01	374.18 548 4.68 F0.10

Paving Alley Block 27 Res K+L Teratto
From Orange Ave to F/Cajon Blvd.
Between Central Ave + 4th St.

Indexed

Oct 8-10
Sinner
Northrup
Hale

62

8th 362.81 NW BP
Orange Ave

3+90 = P.V. 365.12 ^{5.61}_{5.07} 365.02 ^{4.79}_{3.77}
C.V. 5.54 C.V. 5.04

3+45 364.90 ^{4.91}_{4.06} 364.80 ^{5.01}_{4.06}
C.V. 5.09 C.V. 5.09

3+10 359.63 ^{10.68}_{5.87}
C.V. 5.87

3+0 364.69 ^{5.12}_{4.37} 364.59 ^{5.22}_{4.37}
C.V. 5.68 C.V. 5.85

2+50 364.45 ^{5.36}_{4.51} 364.35 ^{5.46}_{4.51}
C.V. 5.24 C.V. 5.59

2+10 = 359.25 ^{10.56}_{5.44}
C.V. 5.44

2+0 364.31 ^{5.66}_{4.81} 364.11 ^{5.70}_{4.81}
C.V. 5.68 C.V. 5.75

1+50 363.97 ^{5.84}_{4.99} 363.87 ^{5.94}_{4.99}
C.V. 5.56 C.V. 5.52

1+0 363.73 ^{4.48}_{3.63} 363.63 ^{6.18}_{5.33}
C.V. 5.47 C.V. 5.67

0+50 363.49 ^{4.72}_{3.87} 363.39 ^{4.82}_{3.87}
C.V. 5.45 C.V. 5.38

0+0 = 363.25 ^{4.96}_{4.11} 363.15 ^{5.66}_{4.81}
C.V. 5.19 C.V. 5.13

368.21 T
3.82
364.33
3.49

369.81 T
3.49
365.11
5.32

370.73 T

370.73 T

6+07 - SLF Cajon 364.76 ^{5.97}_{5.02} 364.64 ^{6.09}_{5.14}
C.V. 5.97 C.V. 6.09

6+0 = Brk 364.80 ^{5.93}_{5.08} 364.70 ^{6.03}_{5.08}
C.V. 5.93 C.V. 5.95

5+55 364.98 ^{5.75}_{4.90} 364.88 ^{5.85}_{4.90}
C.V. 5.38 C.V. 5.38

5+10 = F.V.C. 365.16 ^{5.57}_{4.72} 365.06 ^{5.67}_{4.72}
C.V. 5.99 C.V. 5.85

4+90 365.23 ^{5.50}_{4.65} 365.13 ^{5.60}_{4.65}
C.V. 5.55 C.V. 5.59

4+70 365.26 ^{5.47}_{4.62} 365.16 ^{5.57}_{4.62}
C.V. 5.47 C.V. 5.41

4+50 365.27 ^{5.46}_{4.61} 365.17 ^{5.56}_{4.61}
C.V. 5.46 C.V. 5.49

4+30 365.27 ^{5.46}_{4.61} 365.17 ^{5.56}_{4.61}
C.V. 5.46 C.V. 5.41

4+10 365.20 ^{5.53}_{4.68} 365.10 ^{5.63}_{4.68}
C.V. 5.53 C.V. 5.51

Curb Stakes Surfton Place + Monte Visto

Indexed

63

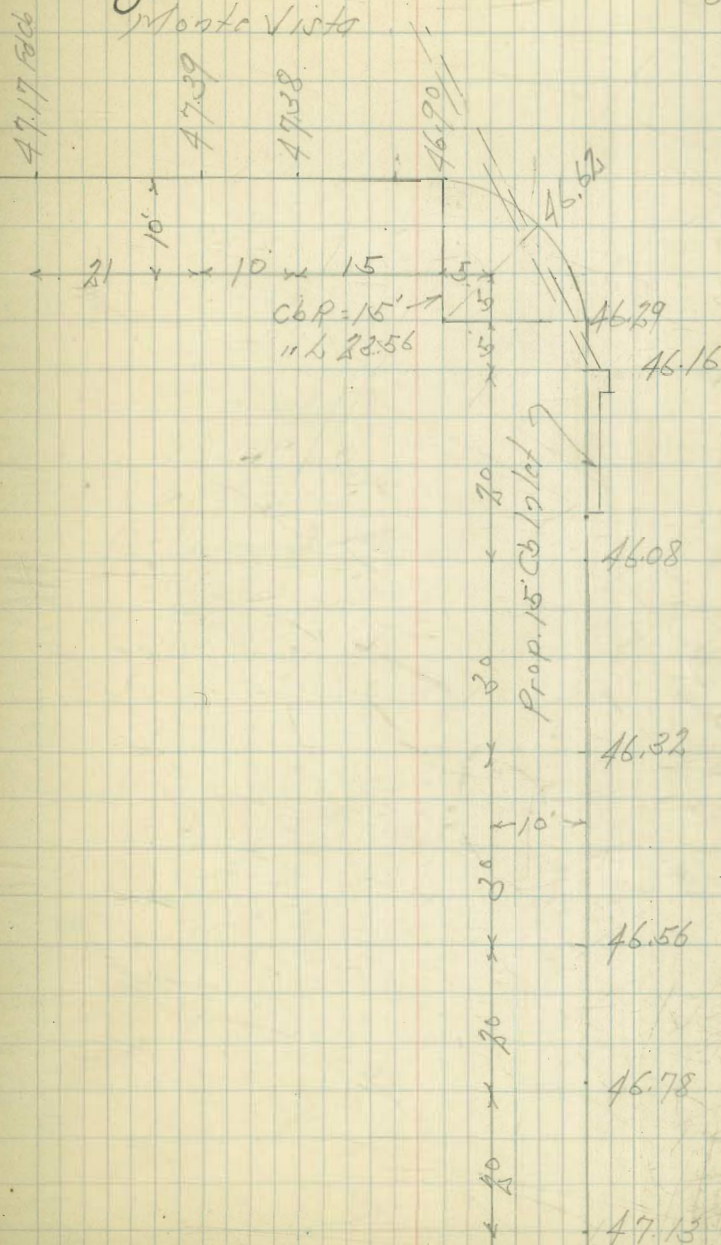
Oct. 11-10
Sunny
Hort. Hrs.
at Mont

BM 2.12 61.64 59.52 ^{Sw. BP} _{Ben Visto}
_{11/10/10/10/10}

TP 1.44 52.21 10.87 50.77

47.39	47.38	46.90	46.62	46.29	46.16
4.82	4.83	5.61	5.59	5.92	6.05
4.82	4.83	5.01	5.12	5.52	5.25
0.0	0.0	0.030	0.040	0.040	0.080

46.08	46.32	46.56	46.78	47.13
6.13	5.89	5.65	5.43	5.08
5.92	5.89	5.65	5.23	4.68
0.030	0.0	0.0	0.030	0.050



Vine St. Imp. Kettner to Pacific

Indexed

65

Culvert No 1

Dec. 18.40

Kettner

St. 1.00

Plid

0+0 = End open ditch

Florlin

21.60

9.67
8.72
08.90

0+70 = End 24" Conc Pipe

21.20

10.02
8.82
08.40

1+20

20.95

10.37
8.86
08.21

1+70 = End 24" Conc Pipe

20.70

10.52
8.22
08.26

2+50 = End open

10.92
9.72
01.20

20.30

PP Hub
50'

PP Hub
50'

100.00

PP Hub
50'

PP Hub
50'

PP Hub
50'

PP Hub
50'

PP Hub
50'

BM

390

43.48

39.58

S.F. RP
Kettner

California

TP

0.00

31.22

12.26

31.22

PP Hub
50'

PP Hub
50'

40.59
20'
40'

40.59
20'
40'

13.13

PP Hub
50'

PP Hub
50'

50' 90° 4" 4"

10.40

Pacific Highway

S F H M BM 39.58
 4.12
 43.77
 1499.80 N L Calif 24.40
 8.9 6.8
 22.66
 10.3 COB 24.90
 8.4 14.15
 22.62
 8.66
 33.28
 9.37
 1479.80 25.20
 8.1
 8.7
 0.7 25.70
 7.6 24.01
 7.1 1.82
 0.5 1.583
 3.60
 8.223
 1459.80 -PVC 26.40
 6.9
 0.5
 0.4 26.90
 6.4
 0.1
 0.3
 1449.86 PVC 29.54
 3.7
 2.4
 0.7 30.04
 12.7
 2.4
 0.8
 0+79.93 32.69
 11.1
 1.6
 0.0 33.19
 10.6
 6.9
 0.7
 0+40 = Exc 35.83
 7.9
 9.1
 1.2 36.33
 2.4
 0.7
 0+20 37.19
 6.6
 9.3
 2.7 37.61
 6.2
 5.2
 0.9
 0+0 = S L Kettner 38.13
 5.64
 5.65016 38.32
 5.45
 5.47016

S F B P
 Vine St
 Kettner

1+50

BM 22.23

1+30

1+10 = PVC

0+70 = F16

0+40

0+20

S L Calif = 0+0
 Stations

0 L Calif

S F

H M

12.57
 8.3
 9.7
 F1.4

13.92
 7.0
 9.3
 F2.3

20.87 A Ford

15.70
 5.3
 9.1
 F3.9

19.70
 1.3
 3.4
 -6.3

22.05
 2.7
 2.3
 F6.0

22.90
 2.9
 3.5
 F2.2 22.75

23.20
 10.1
 10.7
 F0.6 F0.6

23.80
 9.5
 10.7
 F1.2 F0.7

12.57
 11.7
 13.0
 F1.3

13.92
 10.3
 11.3
 F1.0

15.70
 8.6
 9.9
 F1.3

19.70
 4.6
 8.9
 F4.3

22.05
 2.2
 2.3
 -6.8

22.90
 2.9
 4.2
 F2.0

23.50
 9.8
 9.6
 0.5

24.20
 10.1
 9.0
 0.1

5 L

N 14

20.877 N 84. Ford

41.7 = BC NW
 2 + 42.3 = BC Pacific ?

2 + 32.3

1490 = E.V.C.

1470 = 19.

2570

10.52 $\frac{10.35}{10.5}$

10.67 $\frac{10.50}{10.35}$

10.76 $\frac{10.1}{10.3}$
 -0.2

10.80 $\frac{10.1}{10.3}$
 F0.9

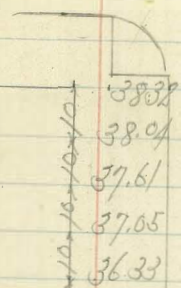
11.25 $\frac{9.6}{9.2}$
 -0.1

11.25 $\frac{9.6}{9.2}$
 F1.0

11.66 $\frac{9.2}{9.2}$
 -0.7

11.66 $\frac{9.2}{9.2}$
 F1.3

Kettner



119.80

26.90

26.22

25.70

25.30

25.00

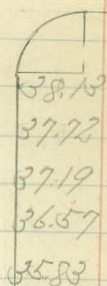
24.70

24.40

8.25

6.09

Calif



26.40

25.72

25.20

24.80

24.60

24.28

24.00

6.09

Vinn St.

BM 3.62 43.20 39.58 S.F.B.P.
V. 200
K. 1000

TP 0.48 31.39 1229 30.91

N.W. Highway 0.50 above
Pav. Gr. 33.25 23.75 7.64

S.E. Highway Cb. Grade 23.79 8.60

Curb States H.E. V. line & Pacific Highway Sp. 11. 41

BM 1.21 40.79 39.58 S.F.B.P.
V. 200
K. 1000

TP 0.30 29.06 12.03 28.76

TP 1.11 18.63 11.54 17.52

10.65 = Cb. E. 11.15 422 F.C. E. E.
7.98 7.48
6.48
0.10

69

23-25 Pav. 2.5

Colif.

36.88

19.5

22.90

22.90

0.20

22.55

22.55

32.79 24.19
Cb

22.05

22.05

21.41

21.41

20.63

20.63

19.70

19.70

15.70

15.70

14.75

14.75

13.92

13.92

13.19

13.19

12.57

12.57

12.06

12.06

11.66

11.66

11.37

11.37

11.25

11.25

9.5

11.15

422

10.67 = Cb. E. C

10.47

Paving Grades Surfton Place
Monte Vista West

Indexed

cc. Gutter Grades

cc.

5 48.50 47.95 47.42 46.75 46.30 46.14 46.14
4.16 4.71 5.24 5.91 6.26 6.52 6.52
0.00 4.12 4.78 5.23 5.28 5.23 6.10
c 4.16 c 6.58 c 0.48 c 6.58 c 6.58 c 6.59 c 0.42

5 46.30 46.55 46.77 47.12
6.36 6.11 5.89 5.54
5.67 5.35 4.21 3.84
c 0.69 c 0.76 c 1.58 c 1.76

H 45.66 45.58 45.82 46.06 46.28 46.63
7.00 7.08 6.84 6.60 6.38 6.03
5.22 6.41 6.37 6.18 5.67 5.06
c 1.28 c 0.67 c 0.47 c 0.60 c 0.77 c 1.01
1.34 0.60

5 47.66 48.01 48.17 48.15 47.86 47.25 46.60
5.06 4.65 4.49 4.51 4.80 5.34 6.06
3.64 3.13 2.67 2.77 2.63 3.24 4.69
c 1.12 c 1.52 c 1.92 c 1.54 c 2.18 c 1.37 c 1.37

H 47.10 47.52 47.73 47.71 47.47 47.01 46.33
5.56 5.14 4.92 4.95 5.10 5.65 6.33
4.36 3.90 3.92 4.12 4.52 4.87 5.20
c 1.18 c 1.24 c 0.98 c 0.83 c 0.67 c 1.28 c 1.13

Nov 13-40 47.10 46.60
Simon
Northway
W Moore 47.85 47.35

46.33 46.83

71

47.01 47.51

46.69 48.36 47.86
597 48.36
52.66

47.47 47.97

48.65 48.15

47.91 48.21

48.67 48.17

47.73 48.23

48.51 48.01

47.52 48.02

48.10 47.60

47.10 47.60

47.62 47.12

46.63 47.13

47.27 46.77

46.28 46.78

47.05 46.55

46.06 46.56

46.80 46.30

45.82 46.32

CR 50 46.64 46.14
46.64 46.14
46.80 46.30
47.25 46.75
48.45 47.95
49.30 48.80

45.65 46.08

45.60 46.16

Monte Vista

BM 36139 Topch. L. P. 1/4 on E N

Indexed

Nov. 20-40 72
Sisson
Hartberry
W Moore

BM	361.39	one M	F
	5.67		
	367.06	4.37	4.37
3+20	4.76	361.85	4.34
	368.30	c 0.41	4.02
	3.87		
	366.17		
	4.15	5.34	4.45
3+70	362.02	361.72	4.15
	4.64	c 0.57	0.80
	368.64		

2+20	361.60	5.46 4.98 0.48	5.46 4.97 0.49
------	--------	----------------------	----------------------

170	559	559
336147	559	487
0008	0008	0073

$1+20$

0+70 36.122 ^{5.81} ~~4.85~~ _{00.92} 5.81 ^{5.81} ~~4.85~~ _{01.64}

$0.20 = 8\% \quad 361.09 \overset{6.15}{\underset{0.55}{\text{C}}} \quad 361.09 \overset{5.91}{\underset{0.66}{\text{C}}}$

0 + 0 = 14	Polk	360.91	361.07	5.99
------------	------	--------	--------	------

$5 + 76.15 = 52$ Orange 1361.76 4.88 36169 4.95
 4.80 on 100 4.93 on 100

5A 56.15 = 81.4 361.80 $\frac{484}{391}$ 361.80 $\frac{484}{391}$
CO93 CO58

$54 \frac{2}{1} / 15$

$\begin{array}{r} 4.24 \\ 86.93 \\ \hline 307 \\ c 0.63 \end{array}$

$\begin{array}{r} 4.24 \\ 2.56 \\ \hline 2.66 \\ FO.02 \end{array}$

4+86.15 F.V.C. 36207 $\frac{4.10}{3.76}$ $\frac{4.10}{3.64}$
CO34 CO34

4 + 46.15 362.12 405
 379
 008 1.03
 4.98
 50.38

4+06.15=PVC. 362.07-^{4.10}_{4.37}
FO.27
on Cond.

3×70
 $\begin{array}{r} 4.19 \\ 36.98 \\ \hline 125.97 \\ \hline 125.97 \end{array}$
 $\begin{array}{r} 4.19 \\ 4.19 \\ \hline 4.19 \\ \hline 4.19 \end{array}$

Alley Grades Block 256 University Hts
From Robinson to University
Between Georgia + Florida

Indexed
B

BM	4.68	341.09	336.41	SW. QP Univ. Georgia
TP	4.24	337.23	8.10	332.99

Stake Set 2' E of NL			7.03
70' S of S.W. Univ. 2nd	330.20		7.20 FO.17

84' S		331.60	5.62 5.85 FO.02
-------	--	--------	-----------------------

104' S		333.30	3.93 3.93 0.00
--------	--	--------	----------------------

124' S		334.80	2.43 1.98 0.45
--------	--	--------	----------------------

Nov 29 40
S. 3809
North 4007
W Moore

Winona Ave Carb Stake 73
West Side
Indexed
B

North of Trojan

BM	2.05	365.15A	363.16	NW Top Curb
----	------	---------	--------	----------------

141.45 - E.V.C. H of NL Trojan	361.05	4.10
--------------------------------	--------	------

183.45 H of NL Trojan	361.39	3.76
-----------------------	--------	------

225.45 H of NL Trojan	361.72	3.43
-----------------------	--------	------

Curb Level 585 P 69

Kolmia & 3rd St.
Grade S.E. Cor + 132' E of F.L. 3rd H.H.

Indexed
B

Jan 7-41 74

BM 2.84 227.79 224.95 NW 80
Kolmia
+ 416.51

222.00
5.79
✓

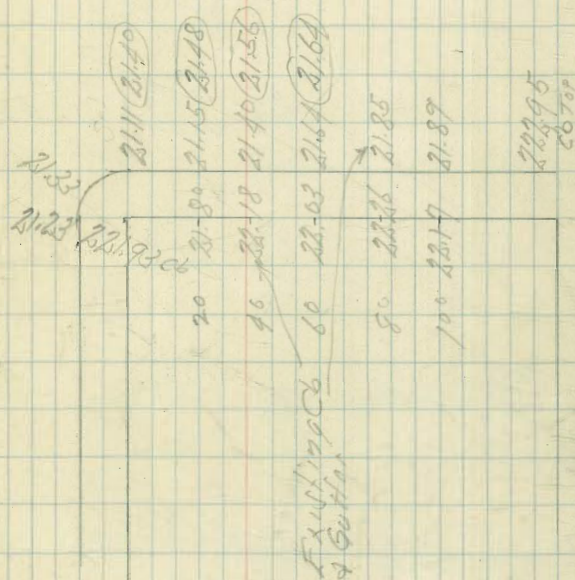
BM 3.41 228.36 224.95 NW 80
Kolmia
+ 416.51

F.L. 3rd H. 30' East 60' E of F.L. 3rd
222.00 222.15 222.30
6.36 6.21 6.06
✓ ✓ ✓

Aug 25-41

BM 3.40 228.35 224.95
Curb Grades Profile
F.L. 3rd 30' East 60' East 91' East 122' East
221.96 222.00 222.15 222.30 222.45 222.61
6.39 6.35 6.20 6.05 5.90 5.74
✓ ✓ ✓ ✓ ✓
5.77 Fadd

Kolmia



3rd St

416.51

Santa Clara Place
Paving Grades
Ocean Front Walk to Bay side Walk

March 11-41
SUSCO
North Side
St. Moor

Indexed
JG

75

1+0 2.28 ^{9.45}_{9.59} FO.14 2.14 ^{9.59}_{9.65} CO.04

0+80 = P.V.C. 3.20 ^{8.53}_{9.23} FO.70 3.05 ^{8.68}_{8.80} FO.12

0+50 4.70 ^{7.03}_{7.39} FO.36 4.55 ^{7.18}_{7.01} CO.17

0+20 = Brk 6.20 ^{5.53}_{5.66} FO.07 6.05 ^{5.68}_{5.80} FO.12

0+0 = F.L. Strandway = F.V. 7.20 ^{4.53}_{4.53 on Pav} 7.05 ^{4.68}_{4.70 on Pav}

0+80 = F.L. Strandway = H.V. Paving 7.20 ^{4.43}_{4.41 on Pav} 7.15 ^{4.58}_{4.58 on Pav}

0+40 6.02 ^{5.71}_{5.82} CO.27 5.95 ^{5.78}_{5.85} CO.25

0+0 = F.L. Ocean Front Walk 4.73 ^{6.98}_{7.18} FO.20 4.75 ^{6.98}_{6.85}

B.M. 4.54 11.73 X 7.19 S.W. BP Santa Clara St. Moor

1+22.10 -0.45 ^{4.65}_{4.63} CO.02 -0.41 ^{4.61}_{5.04} FO.43

0+72.10 -0.32 ^{4.52}_{4.65} FO.13 -0.28 ^{4.48}_{4.68} CO.10

0+22.10 = Brk -0.20 ^{4.40}_{4.49} FO.09 -0.16 ^{4.36}_{4.54} FO.18

0+0 = F.L. Mission = Brk -0.36 ^{4.56}_{4.56 on Pav} -0.30 ^{4.50}_{4.50 on Pav}

TP 3.91 4.20 X 11.42 11.44 0.29 11.44
1+746 = F.L. Mission = Brk Paving 0.21 11.41 on Pav 0.29 11.44 on Pav

1+60 0.55 ^{11.18}_{10.21} CO.27 0.45 ^{11.22}_{10.13} CO.25

1+40 0.96 ^{10.77}_{10.25} CO.02 0.84 ^{10.59}_{10.28} CO.01

1+20 1.54 ^{10.19}_{10.26} FO.07 1.40 ^{10.23}_{9.24} CO.09

11.73 X

17

5

0+80.41 = Conc. Walk -0.40 $\begin{matrix} 4.55 \\ 4.60 \end{matrix}$ on walk -0.40 $\begin{matrix} 4.55 \\ 4.51 \end{matrix}$ on walk
Boyside walk

0+40 -0.60 $\begin{matrix} 4.75 \\ 4.83 \\ 4.08 \end{matrix}$ -0.58 $\begin{matrix} 4.73 \\ 5.15 \\ 4.92 \end{matrix}$

TP 4.95 4.57 5.00 -0.80

0+0 = FL Boyside -0.79 $\begin{matrix} 4.99 \\ 5.21 \\ 4.02 \end{matrix}$ -0.75 $\begin{matrix} 4.95 \\ 5.20 \\ 4.005 \end{matrix}$

2+5790 = FL Boyside -0.79 $\begin{matrix} 4.99 \\ 5.21 \\ 4.02 \end{matrix}$ -0.75 $\begin{matrix} 4.95 \\ 5.20 \\ 4.005 \end{matrix}$

2+2210 -0.69 $\begin{matrix} 4.89 \\ 4.94 \\ 4.05 \end{matrix}$ -0.65 $\begin{matrix} 4.85 \\ 5.26 \\ 4.061 \end{matrix}$

1+72.16 -0.57 $\begin{matrix} 4.77 \\ 5.29 \\ 4.010 \end{matrix}$ -0.53 $\begin{matrix} 4.73 \\ 5.29 \\ 4.058 \end{matrix}$

500245

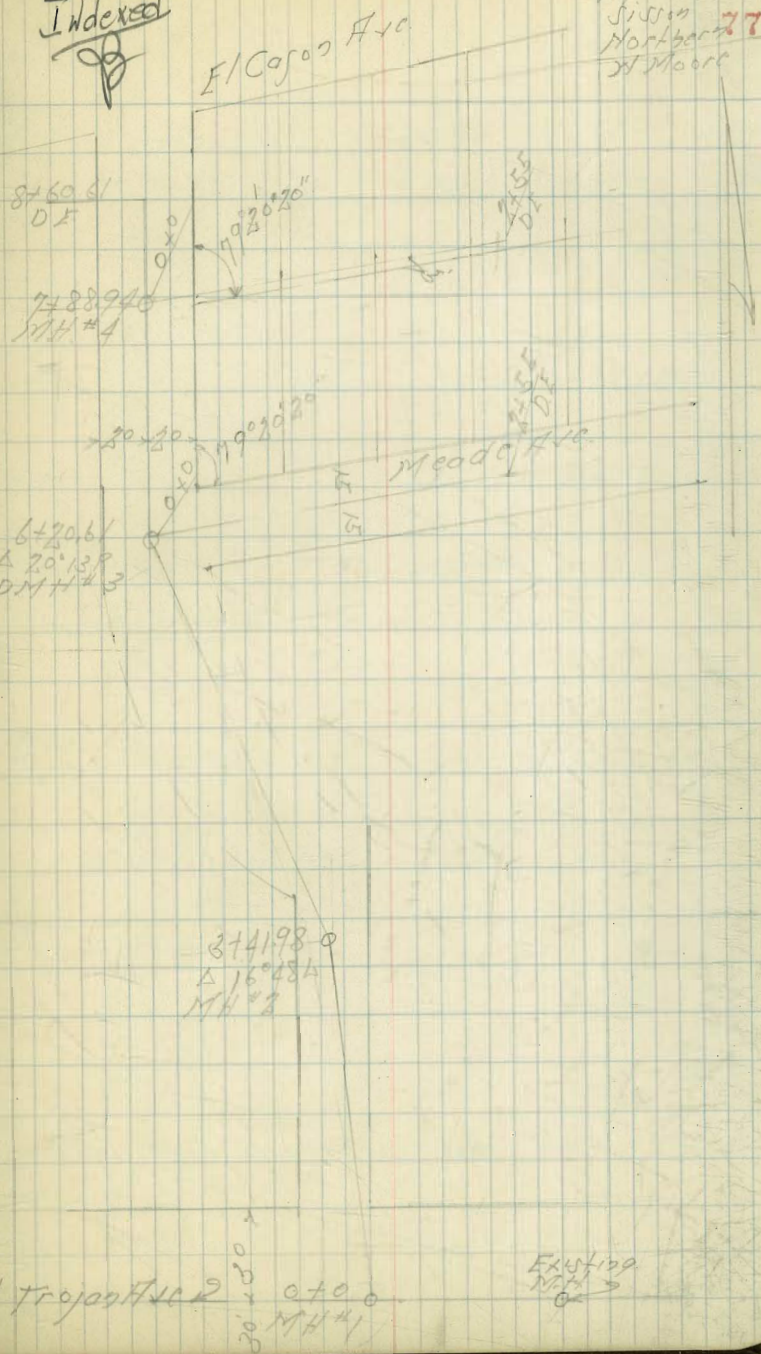
4.20X

Server Grades 53rd St. And
Public Right of Way
Trojan Ave to South of E/Cosmo Ave

Indexed
8

April 11-41
Susan
Northbrook 27
H Moore

		371.08			370.88	20.20 7.76 12.44
5+27.73						8+60.61 DF
TP	0.22	379.66	11.64	379.44		
4+81.29				365.77	13.89 2.13 11.76	7+88.940 MH#4
4+34.26				360.66	19.00 6.16 12.84	
TP	0.92	368.56	12.02	367.64		
3+88.42				355.55	13.01 2.27 10.74	
3+419.8 = MH#2				350.44	18.12 9.34 8.78	6+20.61 Δ 20° 13' 39" DMH#3
TP	0.77	357.66	11.67	356.89		
3+0				347.24	16.42 4.36 6.12	
2+50				343.39	14.27 6.12 8.15	
TP	0.10	345.48	12.28	345.38		
3+0				339.54	5.94 1.84 4.90	
1+50	0.77			335.69	9.79 3.77 6.02	3+419.8 Δ 16° 48' MH#3
1+0	5			331.84	12.64 7.32 6.36	
0+50				327.99	17.49 10.00 7.49	
0+0 = MH#1				324.14	21.34 11.72 9.62	
TP	1.99	325.42	12.05	323.43		2 Trojan Ave
8M 327.43			7.90	327.52	MH#1 Trojan Ave DMH#1	0+0.0 MH#1



Existing
MH#3

BM 768 401.56 393.88
 TP 0.16 391.08 10.64 390.92

JWB.P.
 F/G 100x
 53M

8+60.61 = D.F.

389.56
 12.06
 2.13
 09.93

8+24.77

389.25
 12.01
 3.83
 08.18

7+88.94 = MH⁴

389.00
 12.66
 4.14
 08.48

7+46.86

387.02
 14.51
 1.87
 09.67

7+04.77

386.04
 16.52
 6.35
 09.17

6+62.69

383.07
 13.40
 3.61
 09.88

6+20.61 = DMH³ 2 Moode + 53rd St 10.64 381.09 38700 10.64 38700
 20.47
 9.83

5+74.17

375.99
 13.09
 5.62
 09.47

Moode Ave
 East of 53rd St. 402.63X
 BM 11.71

2+55 = D.F.

2+0

1+50

1+0

0+50

0+0 = DMH³ 3 = 2 Moode + 53rd St 287.00

Across Lot 2-5 Country Paradise

2+55 = D.F.

2+0

TP 4.16 402.17X 4.59

1+50

1+0

0+50

0+0 = 53rd St - MH⁴

BM 5.18

402.60X

390.92 78

391.08 6+20.61

390.20 13.43 2.38 09.03

389.40 13.20 4.95 08.28

388.60 14.03 6.10 07.93

387.80 14.83 7.23 07.60

287.00

391.04 11.13 6.98 05.15

390.60 11.57 6.83 07.74

398.01 12.10 7.37 08.73

389.80 12.80 7.08 08.72

387.40 13.20 6.83 09.38

389.00

397.42

9+88.94

Indexed
Pr

12th St.

June 26 43

51503
51504
51505

79

Вр

5.93

8.83

5.00

NFBP
Imperial
4/13/95

For B

588

$$\begin{array}{r} 542 \\ \hline \end{array}$$

-0.46

592

6.45

10.34

591

5.47

8. 7. 7

1571

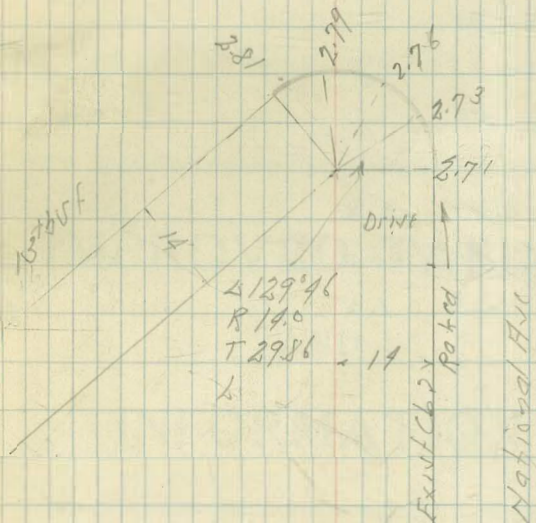
$$\begin{array}{r} 550 \\ 1 \end{array}$$

0.21

Ф.С. М. 1060

2019

21



Sand Backfill

74+50	to 64+50	0.5 above pipe	cas below grade
46+92	" 45+12	to spring line	
47+16	" 47+60	0.5 above pipe	
48+20	" 48+70	"	"
51+46	" 52+68	"	"
43+65	" 44+28	0.3	"
40+31	" 26+50	"	" (0.3 below grade)
26+50	" 19+75	0.5	"
19+75	" 14+07	0.3	" (0.5 below grade)
14+07	" 2+75	to subgr.	0.3
2+75	" 0+00	1.5	" (13+25 to 0+03)

Gr. 272.9

273.8

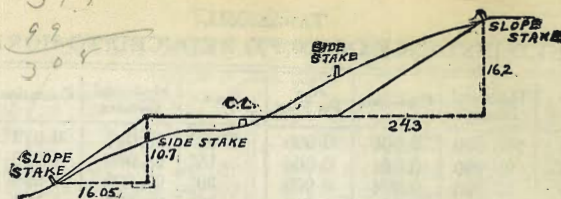
279.0
1.1
277.9

p/vg. 280.3
5.4
285.7
13.3
272.4

273.8
273.0

2" W 11 1/2 32" c. gate

IMPROVED TABLES AND INFORMATION



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

J Isbell
1662 Altadena

92 - 93450 - 2%

93450 - 98460 - -0.91%

$$\begin{array}{r} 251.94 \\ 12.80 \\ \hline 239.14 \end{array}$$

$$\begin{array}{r} 2945.2 \\ 9.64 \\ \hline 285.87 \\ 17.0 \\ \hline 263.37 \end{array}$$

$$\begin{array}{r} 282.5 \\ 3 \\ \hline 282.8 \end{array}$$

$$\begin{array}{r} 292.76 \\ 2.60 \\ \hline 290.16 \end{array}$$

Speed: 1/25/6.2m 45.636

$$\begin{array}{r} 289.3 \\ 0.9 \\ \hline 285.4 \\ 282.8 \\ \hline 2.6 \end{array}$$

$$\begin{array}{r} 11.4 \\ 6.2 \\ \hline 6.2 \end{array}$$

$$\begin{array}{r} 12.4 \\ 4.9 \\ \hline 7.5 \end{array}$$

$$\begin{array}{r} 12.8 \\ 5.0 \\ \hline 7.8 \end{array}$$

$$\begin{array}{r} 3.1 \\ .8 \\ \hline 3.9 \end{array}$$

282.8

.67

16.87

$$\begin{array}{r} 96+4975 \\ \hline 96+66.12 \end{array}$$