

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100 00	0 44	100 00	0 87	99 09	1 31	89
1	99 98	1 75	99 98	0 44	99 97	0 87	99 05	1 31	88
2	99 94	3 49	99 92	3 93	99 91	4 36	99 88	4 80	87
3	99 86	5 23	99 84	5 67	99 81	6 10	99 79	6 54	86
4	99 76	6 98	99 73	7 41	99 69	7 85	99 66	8 28	85
5	99 62	8 72	99 58	9 15	99 54	9 58	99 50	10 02	84
6	99 45	10 45	99 41	10 89	99 36	11 32	99 31	11 75	83
7	99 25	12 19	99 20	12 02	99 14	13 05	99 09	13 49	82
8	99 03	13 92	98 97	14 35	98 90	14 78	98 84	15 21	81
9	98 77	15 64	98 70	16 07	98 63	16 50	98 56	16 93	80
10	98 48	17 36	98 40	17 79	98 33	18 22	98 25	18 65	79
11	98 16	19 08	98 08	19 54	97 99	19 94	97 90	20 36	78
12	97 81	20 79	97 72	21 22	97 63	21 64	97 53	22 07	77
13	97 44	22 50	97 34	22 92	97 24	23 34	97 13	23 77	76
14	97 03	24 19	96 92	24 62	96 81	25 04	96 70	25 46	75
15	96 59	25 88	96 48	25 50	96 36	25 72	96 25	27 14	74
16	96 13	27 56	96 00	27 98	95 88	28 40	95 76	28 82	73
17	95 63	29 24	95 50	29 45	95 37	30 07	95 24	30 49	72
18	95 11	30 90	94 97	31 32	94 83	31 73	94 69	32 14	71
19	94 55	32 56	94 41	32 97	94 26	33 38	94 12	33 79	70
20	93 97	34 20	93 82	34 61	93 67	35 02	93 51	35 43	69
21	93 36	35 84	93 20	36 24	93 04	36 65	92 88	37 06	68
22	92 72	37 46	92 55	37 86	92 39	38 27	92 22	38 67	67
23	92 05	39 07	91 88	39 47	91 71	39 57	91 53	40 27	66
24	91 35	40 67	91 18	41 07	91 00	41 47	90 81	41 87	65
25	90 63	42 26	90 45	42 66	90 26	43 05	90 07	43 44	64
26	89 88	43 84	89 69	44 23	89 40	44 62	89 30	45 01	63
27	89 10	45 40	88 90	45 79	88 70	46 17	88 50	46 56	62
28	88 29	46 95	88 09	47 33	87 88	47 72	87 67	48 10	61
29	87 46	48 48	87 25	48 86	87 04	49 24	86 82	49 62	60
30	86 60	50 00	86 38	50 38	86 16	50 75	85 94	51 13	59
31	85 72	51 50	85 49	51 88	85 26	52 25	85 04	52 62	58
32	84 80	52 99	84 57	53 36	84 34	53 73	84 10	54 10	57
33	83 87	54 46	83 63	54 83	83 39	55 19	83 15	55 56	56
34	82 90	55 92	82 66	56 28	82 41	56 64	82 16	57 00	55
35	81 92	57 36	81 66	57 71	81 41	58 07	81 16	58 42	54
36	80 90	58 78	80 64	59 13	80 39	59 48	80 13	59 83	53
37	79 86	60 18	79 60	60 53	79 34	60 88	79 07	61 22	52
38	78 80	61 57	78 53	61 91	78 26	62 25	77 99	62 59	51
39	77 71	62 93	77 44	63 27	77 16	63 61	76 88	63 94	50
40	76 60	64 28	76 32	64 61	76 04	64 94	75 76	65 28	49
41	75 47	65 61	75 18	65 93	74 90	66 26	74 61	66 59	48
42	74 31	66 91	74 02	67 24	73 73	67 56	73 43	67 88	47
43	73 14	68 20	72 84	68 52	72 54	68 84	72 24	69 15	46
44	71 93	69 47	71 63	69 78	71 33	70 09	71 02	70 40	45
45	70 71	70 71							

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MADE IN
U. S. A.



LIETZ STANDARD ENGINEERS' TRANSIT
With U Shaped Standards

No. 5E with 6¼" limb.

No. 11E with 5" limb.

Furnished with either Internal or External
Focusing Telescope.

5.7
7.0
12.92
54.0
7.59

Quality Evidenced Since 1882

15.20 = 8050
3+2580
13.80 = 124 1.2 907
3+29.2
107

Standard Tripod Connection

MICR
AP

MICROFILMED

APR 12 1965

CITY ENGINEER

G-208

TABLE OF STADIA REDUCTIONS
For a Constant of 100.
ROD VERTICAL.

Min.	0°		1°		2°		3°		4°		5°		6°		7°	
	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.	Hor. Dist.	Dif. Elev.
0	100.00	00	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.98	99.24	8.68	98.91	10.40	98.51	12.10
2	100.00	00	99.97	1.80	99.87	3.55	99.72	5.28	99.50	7.07	99.23	8.79	98.88	10.51	98.48	12.21
4	100.00	00	99.96	1.86	99.87	3.60	99.71	5.34	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.28
6	100.00	00	99.95	1.92	99.86	3.65	99.70	5.40	99.48	7.19	99.20	8.91	98.86	10.62	98.46	12.35
8	100.00	00	99.94	1.98	99.85	3.70	99.69	5.46	99.47	7.25	99.19	8.97	98.85	10.68	98.45	12.42
10	100.00	00	99.93	2.04	99.84	3.75	99.68	5.52	99.46	7.30	99.18	9.03	98.84	10.74	98.44	12.49
12	100.00	00	99.92	2.10	99.83	3.80	99.67	5.57	99.45	7.36	99.17	9.09	98.83	10.80	98.43	12.56
14	100.00	00	99.91	2.16	99.82	3.85	99.66	5.63	99.44	7.41	99.16	9.15	98.82	10.86	98.42	12.63
16	100.00	00	99.90	2.21	99.81	3.90	99.65	5.69	99.43	7.46	99.15	9.20	98.81	10.91	98.41	12.70
18	100.00	00	99.89	2.27	99.80	3.95	99.64	5.75	99.42	7.51	99.14	9.25	98.80	10.96	98.40	12.77
20	100.00	00	99.88	2.33	99.79	4.00	99.63	5.80	99.41	7.56	99.13	9.31	98.79	11.01	98.39	12.84
22	100.00	00	99.87	2.38	99.78	4.05	99.62	5.85	99.40	7.61	99.12	9.36	98.78	11.06	98.38	12.91
24	100.00	00	99.86	2.44	99.77	4.10	99.61	5.91	99.39	7.66	99.11	9.41	98.77	11.11	98.37	12.98
26	100.00	00	99.85	2.49	99.76	4.15	99.60	5.96	99.38	7.71	99.10	9.46	98.76	11.16	98.36	13.05
28	100.00	00	99.84	2.55	99.75	4.20	99.59	6.02	99.37	7.76	99.09	9.51	98.75	11.21	98.35	13.12
30	100.00	00	99.83	2.60	99.74	4.25	99.58	6.07	99.36	7.81	99.08	9.56	98.74	11.26	98.34	13.19
32	100.00	00	99.82	2.66	99.73	4.30	99.57	6.13	99.35	7.86	99.07	9.61	98.73	11.31	98.33	13.26
34	100.00	00	99.81	2.71	99.72	4.35	99.56	6.18	99.34	7.91	99.06	9.66	98.72	11.36	98.32	13.33
36	100.00	00	99.80	2.77	99.71	4.40	99.55	6.24	99.33	7.96	99.05	9.71	98.71	11.41	98.31	13.40
38	100.00	00	99.79	2.82	99.70	4.45	99.54	6.29	99.32	8.01	99.04	9.76	98.70	11.46	98.30	13.47
40	100.00	00	99.78	2.88	99.69	4.50	99.53	6.35	99.31	8.06	99.03	9.81	98.69	11.51	98.29	13.54
42	100.00	00	99.77	2.93	99.68	4.55	99.52	6.40	99.30	8.11	99.02	9.86	98.68	11.56	98.28	13.61
44	100.00	00	99.76	2.99	99.67	4.60	99.51	6.46	99.29	8.16	99.01	9.91	98.67	11.61	98.27	13.68
46	100.00	00	99.75	3.04	99.66	4.65	99.50	6.51	99.28	8.21	99.00	9.96	98.66	11.66	98.26	13.75
48	100.00	00	99.74	3.10	99.65	4.70	99.49	6.57	99.27	8.26	98.99	10.01	98.65	11.71	98.25	13.82
50	100.00	00	99.73	3.15	99.64	4.75	99.48	6.62	99.26	8.31	98.98	10.06	98.64	11.76	98.24	13.89
52	100.00	00	99.72	3.21	99.63	4.80	99.47	6.68	99.25	8.36	98.97	10.11	98.63	11.81	98.23	13.96
54	100.00	00	99.71	3.26	99.62	4.85	99.46	6.73	99.24	8.41	98.96	10.16	98.62	11.86	98.22	14.03
56	100.00	00	99.70	3.32	99.61	4.90	99.45	6.79	99.23	8.46	98.95	10.21	98.61	11.91	98.21	14.10
58	100.00	00	99.69	3.37	99.60	4.95	99.44	6.84	99.22	8.51	98.94	10.26	98.60	11.96	98.20	14.17
60	100.00	00	99.68	3.43	99.59	5.00	99.43	6.89	99.21	8.56	98.93	10.31	98.59	12.01	98.19	14.24
c=75...			.75	.01	.75	.02	.75	.03	.75	.04	.75	.05	.75	.06	.75	.07
c=1.15...			1.15	.01	1.15	.03	1.15	.05	1.15	.09	1.14	.11	1.14	.13	1.14	.15
c=1.90...			1.90	.02	1.90	.05	1.90	.08	1.90	.15	1.89	.18	1.89	.21	1.89	.25

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74+49⁸⁹ & Yme

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East along Broadway To Tunnel Portal 96+00

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of Elm. check levels. Page 60

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Page 24-26 East San Diego Sewer. 0+00 Wabash, +
Redwood to M.H. # 2 32+13¹²

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" 30-33 32+13¹² M.H. # 9. to 70' of End of Job N. of Elkton

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Page 34 Grade change from 41+50 to 42+57. Necessitated
by. Elec. Conduit. N. Side of Univ

Page 41. Grades from M.H. # 16. Orange + 38⁷³. 190+2
East to ex. M.H. # of Orange + Alley East of 38⁷³

Bliss
Sommermyer
Begg
4/9/42

Grades Pacific Ave. Sewer
from Sta 11+00 S. of Elm to

74+93.89 H. & Vine St Elev. Sides Elev. Grade

BM. 4.95 9.97 5.02 SE BP 4.95 Beech Poles Cuts

Ties see FB 1604 Alignment notes

INDEXED

2

W. K.

OCT 25 1948

see FB 1604 P 25 also FB 1317 P 41C check levels used on cast

Sta	BM	Left	Right	Elev	Grade	Cuts	Notes
TP	3.82	8.83	4.96	5.01			State Hwy BM. NE Cedar Poles Iron Bolt in cb
11+00			4.91	3.92	-10.19	14.11	20.5 ft x in cb
TP	5.08	9.11	4.80	4.03			
11+50			5.40	3.71	-10.15	13.86	24' RT x in walk
12+00			6.37	2.74	-10.11	12.85	20' RT stake
+50			5.48	3.63	-10.07	13.70	24' " x in cb Ret NE Elm Poles
13+00			5.20	3.91	-10.03	13.94	24' " x in walk
+50			4.88	4.23	-9.99	14.22	24' " " " "
14+00			4.51	4.60	-9.95	14.55	24' " " " "
+50			4.29	4.82	-9.91	14.73	20.5 ft x in cb
15+00			3.98	5.13	-9.87	15.00	20.5 " " " "
TP	5.97	11.12	3.96	5.15		14.28	
+50			5.72	5.40	-9.83	15.23	20' RT x in cb
16+00			5.88	5.24	-9.79	15.03	" " " " "
+50			5.16	5.96	-9.75	15.71	20.5 ft " " "
+73	74	MH	4.79	6.33	-9.73	16.06	25' RT x in walk
		L. Lt # 41					See FB 1604 Page
		used to be					
		Check SE Corner Pacific a brass plug	4.51	6.61			
17+00			4.90	6.22	-9.71	15.93	25' RT. R Head Spike in paving
+50			4.58	6.54	-9.67	16.21	" " x in walk
		State Iron Pin					
		Check BM. NE Corner Pacific	4.68	6.44			
18+00			4.22	6.90	-9.63	16.53	25' RT x in walk

11/12

INDEXED

cts

18+50			3.78	7.34	-9.59	16.93	25' RT. X in CB
19+00			3.40	7.72	-9.55	17.27	" " RH Spike in A.C. Work
TP.	6.96	14.64	3.44	7.68			
+50	* Note This Grade pt is under heavy Truck Traffic		6.62	8.02	-9.51	17.53	25' RT RH Spike in A.C. Work or Forming
20+00			5.96	8.68	-9.47	18.15	" " " " " " " "
+50			5.33	9.31	-9.43	18.74	" " " " " " " "
21+00			5.17	9.47	-9.39	18.86	" " " " " " 8' H.H. Handicap
+50			5.25	9.39	-9.35	18.74	" " " " " " AC Work
22+00			5.17	9.47	-9.31	18.78	25' RT RH Spike " " " "
+50			4.76	9.88	-9.27	19.15	" " " " " " " "
23+00			5.24	9.40	-9.23	18.63	" " " " " " " "
+50			4.42	10.22	-9.19	19.41	" " " " " " " "
24+00			4.80	9.84	-9.15	18.99	" " RH Nail " " " "
+50			4.63	10.01	-9.11	19.12	RH Nail 25' RT in A.C. Work
+70	5.61	15.69	4.56	10.08	-9.09	19.17	" " Spike 25' RT M.H.H. E of Trv
25+00			³⁸ 5.42	10.31	-9.07	19.38	
+50			³⁴ 5.37	10.35	-9.03	19.38	
26+00			³² 5.35	10.37	-8.99	19.36	
+50			⁶⁰ 5.64	10.09	-8.95	19.04	
27+00			³⁸ 5.41	10.31	-8.91	19.22	
+50			³⁹ 5.42	10.30	-8.87	19.17	
28+00	4.23	14.36	⁵⁴ 5.56	10.15	-8.83	18.98	
+50			⁸⁹ 4.90	9.47	-8.79	18.26	
29+00			¹⁹ 4.20	10.17	-8.75	18.32	
			4.50	9.86			

5 late
check point
8M

X
1436

check BM	NW				Jun. p.c. 1	
29+50			5.52	8.84	8.71	18.09
30+00			4.94	9.45	8.67	18.12
+50			5.10	9.26	8.63	17.89
31+00			5.41	8.98	8.59	17.57
+50			5.63	8.70	8.55	17.25
32+00	4.29	12.66	5.99	8.39	8.51	16.90
+50			4.44	8.25	8.47	16.72
33+00			4.64	8.05	8.43	16.48
+ 4.26 / 1. Pt 8.33					8.39	
check BM			4.57	8.09	8.39	60/100
1 1/4 City			4.72	7.94		
St. Binny Pacific + Laurel	5.16	13.28		8.12		
33+50			5.72	7.56	8.39	15.95 25' st
34+02.65			6.14	7.14	8.35	15.49 20' Lt x. in p. 170
+50			6.00	7.28	8.31	15.59 " " " "
35			5.68	7.60	8.27	15.87 " " " "
12" 11" 00 Lt + 59"			5.24	8.04	8.23	16.27 14.7' Lt x. in cb
36+00			5.60	7.68	8.19	15.87 " " in p. 170
+50			5.07	8.21	8.15	16.36 " x. in p. 170
37	6.35	15.50	4.13	9.15	8.11	17.26 " x. in cb
+50			6.04	9.46	8.07	17.53 " " " "
38			5.23	10.27	8.03	18.30 " " " "
+50			4.71	10.79	7.99	18.78 " " " "
39			4.79	10.71	7.95	18.66 " " " "
+50			3.66	11.84	7.31	12.75 " " " "

4

32 XXH 39+37 #44			3.13	12.37	-7.87	20.24	X in cb 14.7 ft of d
+50	649	19.40	2.59	12.91	-7.83	20.74	" " " " " "
41			6.00	13.96	-7.79	21.19	" " " " " "
+50			5.51	13.89	-7.75	21.64	" " " " " "
42			5.00	14.40	-7.71	22.11	" " " " " "
+50			4.51	14.89	-7.67	22.56	" " " " " "
43			4.07	15.33	-7.63	22.96	" " " " " "
Top F.A. 150+ N-5 91m Set BM N. Line. N. 11m	2.36	20.74	1.02	18.38			
TP	3.96	18.22	6.48	14.26			
Close BM. B.P. in ch Sept 18, 92			6.05	12.77			
	1.71	20.09		12.77			
				10.38	BM Top of d		X in cb 10.5 ft of d
+50			5.15	14.94	-7.59	22.53	" " " " " "
44			4.42	15.67	-7.55	23.22	" " " " " "
+50			4.25	15.84	-7.51	23.35	" " " " " "
45			4.13	15.96	-7.47	23.43	" " " " " "
+50			3.97	16.12	-7.43	23.55	" " " " " "
46			4.10	15.99	-7.39	23.38	" " " " " "
M.H. & White #95 714.30	268	18.58	4.19	15.90	-7.37	23.28	" " " " " "
+50 ²⁵			2.90	15.68	-7.35	23.03	" " " " " "
47			3.78	14.80	-7.31	22.11	" " " " " "
+50			3.61	14.97	-7.26	22.23	" " " " " "
48			3.91	14.67	-7.22	21.89	" " " " " "
+50			4.87	13.71	-7.18	20.89	X in ch Paring 10.5 ft of d
49			4.78	13.80	-7.15	20.95	" " " " " "
+50			5.20	13.38	-7.13	20.51	" " " " " "

T
1858

offsets

5880
218

6

T
1964
257 -
12.07 F.H.

cc's

10524

50	+00		6.26	12.32	-7.10	+ 1942	"
	+50		6.13	12.45	-7.07	+ 1952	"
51			6.56	12.02	-7.03	+ 1905	"
	+50	3.08	14.64	7.02	11.56	-6.99	+ 1855
52			3.53	11.11	-6.95	+ 1806	"
	+33	15 MH - 46	3.72	10.92	-6.93	+ 1785	"
	+50		3.76	10.88	-6.92	+ 1780	"
53			4.74	9.90	-6.89	+ 1679	"
	+50		4.87	9.77	-6.85	+ 1662	"
54			4.57	10.07	-6.82	+ 1689	"
	+50		4.83	9.81	-6.99	+ 1660	"
55			5.14	9.50	-6.75	+ 1625	"
	+50		5.34	9.30	-6.71	+ 1609	"
56		4.22	13.25	5.61	9.03	-6.88	+ 1571
	+50		7.29	8.96	-6.65	+ 1561	" X ch-1 here
57			5.00	8.25	-6.61	+ 14.86	" X in paring
	+50		5.11	8.14	-6.58	+ 14.72	"
58			4.79	8.46	-6.59	+ 15.00	"
	+50	3.88	12.19	4.94	8.31	-6.51	+ 14.82
	+80		3.97	8.22	-6.49		

59+11. Pipe in place
MH & Splice. exact with
#47 + 95 ³⁰ ? Phelps on final placing of this M.H.

60+63. Pipe in place See page 76

+ 98 Pipe was stored to here 3.97 8.22 - 6.28

Continued Page 9

0.1070

9712

Grades Pac. Ave Server From

514

-12.53
-5.14
+7.39
5.02

7.39
2.85
-5.14
8.14
5.00
6.74 X
7.08
7.22

2.90
4.5
3.35
12.53
7.22
5.31

98+82⁹⁴ East Along Broadway

23.34

11.01
2.36
-8.65 X
13.51
8.65
3.86
1.12
4.98

10.87
-7.4
11.61
12.53
+1.52
15.2
2.36
3.88

BM	NN	524	9.92	4.68			
98+82 ⁹⁴				5.61	9.31	-12.53	+16.84
98+50				5.87	4.05	-12.56	+16.61
98				5.36	4.56	-12.60	+17.16
+50				9.20	5.72	-12.64	+18.36
Tunnel Portal							
+12	6.96	12.85	4.03	5.89	-12.65		+18.54
97	out						
+50 out							
East Tunnel Portal							
36				5.28	7.57	-12.75	+20.32
BM		4.50	8.81		9.31		
				9.78	-0.97	-12.53	
				5.96	+2.85		
					7.99		
98+50							
BM		5.57	11.29	5.72			
				5.05	6.24	-12.65	+18.89
1st/2nd Tunnel Portal Cut W Side							
98+11		5.23	11.12		5.89		
98+12				9.77	6.35	-12.65	+19.00
98+82.94		4.88	9.19		4.31		
				12.06	-2.87	-12.53	

1854

541

11.12
5.40
5.72

-12.53
2.87
9.66
4.67
4.99

Grade at 145⁵ *

M.H. N. Line of Broadway

940 908

468

1685 - 7.77 - 12.94 + 467

top of pipe

970 L of timber

715 Rod

1685 Rod to Top of pipe

Continued
from page 6π
12-19

cwt

9

61	150		3.76	8.43	-6.20	+14.63		
62	100		3.66	8.53	-6.12	+14.65		
	150	7.82	13.51	3.50	8.69	-6.04	+14.73	
63			4.68	8.83	-5.96	+14.73		
	150		4.81	8.70	-5.88	+14.58		
64			4.81	8.70	-5.80	+14.50		
	150		5.21	8.30	-5.72	+14.02		
65			4.89	8.62	-5.64	+14.76		
	150		5.01	8.50	-5.56	+14.06		
66		4.56	12.42	5.65	7.86	-5.48	+13.34	
	150		4.18	8.30	-5.40	+13.70		
67			4.82	7.60	-5.32	+12.92		
M.H. 2700 #48	155 ³⁰		4.98	7.44	-5.24	+12.68		
68			4.34	8.08	-5.13	+13.27		
X in 45.74 cb Pico BC	5.54	13.73	4.23	8.19	-5.15	+13.34		
69			5.34	8.39	-5.10	+13.49	11' Lt X mcb	
	150		5.77	7.96	-5.05	+13.01	11' " X in Diversey	
70			4.96	8.77	-5.00	+13.77	11' Lt X " walk	
	126 ^{55 800}		4.91	8.82	-4.97	+13.73	11' Lt X " "	
150			4.85	8.88	-4.95	+13.83	11' Lt X " "	
71			4.67	9.06	-4.90	+13.96	12' " X " "	
	150		4.53	9.20	-4.85	+14.05	13' Lt X " "	
72		5.88	15.19	4.42	9.31	-4.80	+14.11	14' " X " "
	150		5.93	9.26	-4.75	+14.01	12' Lt Took in packing	
73			5.70	9.49	-4.70	+14.19	" " " " "	

+ 98. ^{of} EC

5.43 9.76 - 4.65

214.91

cut
12' 4" Tk. in Paring

74

S. on Pac

see FB

1625 p. 26

5.45 9.74 - 4.60

214.34

" " " " "

+ 99.88

M.H. & Vic. See Grade

- 9.54

7414381

BOOK. 207. Page 15.

+ Non Pac.

INDEXED

OCT 22 1918

Set BM ^{TK} in cb. N. Side of ^{EC} near ^{near} Lamp Post

5.18 10.01

check BM. to Tack 741438 ^{of} EC

5.08 10.11

Sec. Grade Book 207. Page 16 for
Continuation of Grades North to Bear.

65th St Sewer Grades
Akins Ave to Broadway

offset 6' lt of *

+40.63 = $\Delta 60^\circ 12' R$ = MH #34
R.P. 90' 6' 46' 27"

5664-68 For Location

223.00

+50

254.44

INDEXED
W.K.
OCT 25 1948

2+0

219.67

7+0

251.29

+50

215.57

+50

248.15

2+0

211.47

6+0 = MH #36

245.00

+50

207.37

+50

241.05

1+0 = Break

203.27

5+0

237.10

+50

201.63

+50

233.15

0+0 = Siting MH & Akins

199.99

4+0

229.20

276.43 = $\Delta 60^\circ 00' L$ = MH #35

227.34

225.94

Circle 410 on split

Transferred 9 218-2

0.0582

+ 85.00 = MH # 38

270.51

+ 50

286.62

+ 50

269.01

+ 40

283.79

+ 10

266.87

+ 50

280.95

+ 50

264.73

+ 32.29 = 1/2 Hundredth MH # 39

279.98

0.0428

+ 9

262.59

+ 30

278.72

+ 50

260.45

+ 50

276.81

+ 36.83 = 1/2 Brooklyn MH # 37

259.89

+ 40

274.90

0.0382

+ 8

257.58

+ 50

272.99

0.0629

+ 40

271.08

INDEXED
OCT 25 1988

17+77.76

304.00

2-37.76

17+40.0 = Break

302.00

17+0

300.75

16+60

298.49

0.563

16+20

296.24

15+80.00 = Δ 1° 03' RT = MH " 40

293.99

+50

292.29

5 South of
18+52.28 = MH " 41 N.E. of Broadway
R.P. 10 + 10.8 to 2.57

305.99

15+0

289.46

0.567

18+15.57

304.99

64th St Sewer Grader
Hkins H to under 110

offset 6' Right

1660-69 Locating

370

INDEXED

W.K.
OCT 25 1948

1940
201.41

2+87.50 A 1° 44' 20" RL - MH # 31
R.P. 67 + 6' Rf on Split A

198.99

+50

198.44

270

197.71

+50

196.98

170

196.25

+50

195.52

0+0 = Existing M.H. & Hkins

194.79

Transferred 9 218-5

14

770 = A 22° 50' RL MH # 31
R.P. 10 + 10 Rf on Split A

225.81

+50

225.61

640

225.41

+50

225.21

540

225.01

+50

224.81

4120 - MH # 31 7'

224.69

440

220.81

2150

211.12

+50 231.16

14102.97 - 9 Wunderlin MH # 28
RP 10 410 N 90° of Wunderlin 240.00

10+0 230.06

12+12.64 238.67

+50 228.96

12+16.32 237.33

+06.54 Δ 14° 41' 11" MH # 30
RP 15 410 R Brook 228.00
226.647

12+16.32

12+70.3 = Δ 27° 42' 11"
RP 10-10-10° 00' R + SP 17 A 236.00

9+0 226.61

+50 235.56

+50 226.41

12+0 234.46

8+0 226.21

+50 233.36

7+50 226.01

11+0 232.26

Grades Pacific Ave Sewer
from Sta 111+00 N. of A. to 111+00 South of B. Lots

SE 8 P BM Pac Beach	4.47	9.99		5.02			
TP	4.55	8.81	5.23	4.26			
111+00			5.83	2.98	-11.34	14.32	x in walk 19' pt of & N of A
+50			5.53	3.28	-11.30	14.58	" " " " " "
112+00			5.26	3.55	-11.26	14.81	" " " " " "
+50			5.04	3.77	-11.22	14.99	" " " " " "
113+00			4.84	3.97	-11.18	15.15	" " " " " "
+50			4.58	4.23	-11.14	15.37	x in walk 19' pt of &
114+00 ³⁴	M.H.L. Pt 1'-11'-00"		4.93	3.88	-11.10	14.98	Roofing Tack 20' x Bit & Ash. pt of &
+50			4.30	4.51	-11.06	15.57	x in walk 20' pt of &
115	5.53	10.09	4.25	4.56	-11.02	15.58	" " " " " "
+50			5.52	4.57	-10.98	15.55	" " " " " "
116+00			5.85	4.24	-10.94	15.18	" " " " " "
+50			5.72	4.37	-10.90	15.27	" " " " " "
117+00			5.19	4.90	-10.86	15.76	" " " " " "
check BM Sta 115			5.07	5.02			
+50			5.94	4.15	-10.82	14.97	" " " " " "
+80 ⁰⁹	M.H.L. Pt 1'-11'-00"		5.64	4.45	10.80	15.25	20' x 100ft Roofing Tack in Pavement
118+00			5.58	4.51	-10.76	15.29	20' Pt of & Roofing Tack
+50			4.95	5.14	-10.74	15.88	x in cb 20' pt of &
egestion 118+79.62 = 4+39.23			4.65	5.44	-10.72	16.16	30' pt of & Roofing Tack
5+00			4.86 ²	5.27	-10.67	15.94	x in cb 20' pt of &
+50	4.83	10.34	4.58	5.51	-10.63	16.14	x in walk 24' pt of &
6+00			5.44	4.90	-10.59	15.49	x in cb 20.5' pt of &
+50			5.69 ⁷¹	4.63	-10.55	15.78	x in Driveway 20.5' pt of &
7+00			5.65	4.69	-10.51	15.20	x in Paving of Curb 20.5' pt of &

X
16.34

+57.31	MH. #	5.27	5.07	-10.97	15.54 ok
8400		5.48 ^{5.4}	4.84	-10.43	15.27
+50		6.14 ^{6.1}	4.18	-10.39	14.57
9400		5.74 ^{5.7}	4.58	-10.35	14.33
+50		5.94 ^{5.9}	4.36	-10.31	14.67
10400		6.14 ^{6.1}	4.19	-10.27	14.46
+50		6.28 ^{6.2}	4.04	-10.23	14.27
11400		6.48 ^{6.4}	3.92	-10.19	14.11 ✓

Cuts

21

Grades Pac Ave Sewer from 0+00

Note Grades were equated because
+s had been cut on original line
see page 63 check levels

Station	Grade	Grade	Grade	Grade	Grade	Grade
93' N of So. line of Broadway to 12+32 ¹² NW of New St SM NW Broadway sp	4.10	8.78	4.68			
0+00			9.45	4.33	-12.53	
0+25			9.55	4.23	-12.51	16.74
0+50			9.6	4.16	-12.49	16.65
0+75			9.72	4.06	-12.47	16.53
1+15 ⁵⁰ L Pt.			9.74	4.04	-12.49	16.48
1+61.45 = 1+62 ²⁵ original line			9.25	4.53	-12.40	16.33
2+00			9.30	4.48	-12.37	16.25
2+50			9.59	4.19	-12.34	16.53
3+00	4.21	8.27	9.72 9.58	4.06	-12.30	16.36
3+50			9.25	4.02	-12.26	16.28
4+00			9.33	3.94	-12.22	16.16
4+50			9.37	3.90	-12.18	16.08
5+00			9.40	3.87	-12.14	16.01
5+50			9.41	3.86	-12.10	15.96
6+00			9.29	4.03	-12.06	16.09
1+4+50 = 6+42 ^{4.64} L		8.89	4.02	4.25	-12.02	16.27
7+00			9.35	4.54	-11.98	16.52
7+50			9.13	4.76	-11.94	16.70
7+78 ⁶⁰ = 7+70 ^{Pat} 82			9.07	4.82	-11.92	16.74
8+12 ^{M.H} = 8+09 ²			9.06	4.83	-11.89	16.72
8+50			9.12	4.77	-11.87	16.64
9+00			9.43	4.46	-11.83	16.29
9+50			9.68	4.21	-11.73	16.00

\$
 \$
 \$
 \$
 X 10.17
 X 10.17
 X 10.27
 X 10.75
 X 10.55
 X 10.25
 X 11.0
 X 10.7
 X 10.5
 X 10.2
 X 9.95
 X 10.7
 X 11.95
 X 12.25

7
8.89

10^{next} 04.23 = 10^{3.53} 12.01 7.45 4.97 3.92 - 11.74 15.65

+50 3.69 3.76 - 11.70 15.46

11+00 3.90 3.55 - 11.66 15.21

+50 4.16 3.29 - 11.62 14.91

+57⁵⁹ = 11+65 46 4.20 3.25 - 11.61 14.86

12+00 4.46 2.99

+32⁰³ = 12+39 90 4.01 - 11.54 14.86

check 11 to 12 of A 4.46 2.99
2.98
0.01

7.37 3.05 4.68

0400 4.24 4.81 - 12.53 + 17.34

1+15 4.54 4.51 - 12.44 + 16.95

305
270
405

23

Bliss Notes
Sommerwyer
Begg Rod.
1/15/44
Fairway

East San Diego Senior Nabash

Grade Elev. + cont

INDEXED

24

W.K.
OCT 25 1948

+ Redwood to M.H. #9

BM #1	6.90	206.74		200.34	Can Men & Redwood Nabash	
0700			6.00	200.74	192.12	8.62 From Run
+50			6.98	199.81	193.37	6.44
1			5.05	201.69	194.62	7.07
+50			7.31	202.43	195.87	6.56
2			2.52	209.22	197.12	7.10
+50	10.76	216.55	0.95	205.79	198.37	7.42
3			9.67	206.88	199.62	7.26
+50			9.12	207.43	200.87	6.56
4			7.61	208.94	202.12	6.82
+50			5.43	211.12	203.37	7.75
MH #1 + 74 ⁰⁷			4.63	211.92	204.00	7.92
checkmen			5.87	210.58		6.14
5			4.88	211.67	204.65	7.02
+50			4.77	211.78	205.90	5.88
6			2.52	214.03	207.15	6.88
+50	10.26	224.71	2.10	214.45	208.40	6.05
7			7.85	216.86	209.65	7.21
+50			7.67	217.04	210.90	6.14
8			6.64	218.07	212.15	5.92
MH #2 + 87 ⁰⁹			4.83	219.88	213.07	6.81
+50			5.38	219.33	213.40	5.93
9			4.12	220.59	214.65	5.94
+50	9.47	232.68	1.50	223.21	215.90	7.31
10			7.47	225.21	217.15	8.06
check #3			6.65	226.03		

6.14

6.07

T
232.68

INDEXED

2400

25

				6.53	226.15	218.90	7.75	
11				5.39	227.29	219.65	7.64	
+50				4.96	228.22	220.30	7.32	
M.H.#3								
12	1.11			4.62	228.06	222.18	5.32	
+50	11.82	243.30		1.20	231.98	223.33	8.09	
13				10.03	233.27	224.64	8.63	
+50				8.92	234.38	225.59	8.49	
14				7.70	235.60	227.14	8.46	
+50				5.92	237.38	228.89	8.99	stake was low on recheck 0.06
15				3.83	239.47	229.60	9.83	
+50				4.46	238.84	230.83	7.95	
16				2.39	240.91	232.14	8.77	
88) +38 88	M.H.#4							
+36 76	6.00	248.31		0.99	248.31	233.12	9.19	stake was 0.06 low
check M.H.#4				3.98	244.83			
+50				5.37	242.94	233.56	9.38	Original Stake Destroyed - Reset
17				3.82	244.49	235.25	9.24	
+50				2.09	246.27	236.93	9.34	
18	12.54	258.83		2.02	246.29	238.61	7.68	
+55				10.79	248.04	240.29	7.78	Stake 0.06 low
19				9.33	249.50	241.98	7.52	
+50				7.42	251.41	243.66	7.75	
M.H.								
45 +84 ¹⁸				6.62	252.21	244.81	7.40	
20 +50				4.32	254.51	247.00	7.51	
21		260.64		3.57	255.26	248.63	6.57	
+50				4.19	256.55	250.37	6.08	
22 +00	10.28	268.90		2.28	256.55	250.37	6.08	
				2.08	258.62	252.06	6.54	stake 0.06 low on recheck

all stakes
6' Rt of d except
Where noted

		T 268.90		Elev Stake	Elev Grade	Cuts	
		266.77					
22	+50		5.31	260.86	253.75	+7.24	
			7.91	260.99			
23			4.67	262.74	255.94	+6.76	
			6.76				
MH#6			3.75	262.38			
	+31.52		5.90	263.00	256.50	+6.50	6.43 Rt
close MH#6			4.32	264.58			
	+50		5.54	263.36	257.12	+6.24	
24			5.71	263.13	258.80	+4.33	
	+50		3.66	265.84	260.98	+5.36	
25	9.81	277.02	1.69	267.21	262.17	+5.04	
	+50		7.95	269.07	263.85	+5.22	
26			6.08	270.98	265.58	+5.40	
MH							
27	+48.13		4.06	272.96	267.15	+5.81	
		276.75	2.90	274.12	267.89	+6.23	
	+50	12.83	1.72	275.30	269.56	+5.74	Recheck
28		287.74	10.29	277.84	272.23	+5.61	
MH			3.75				
28	+59.42	12.79	4.17	283.98	274.23	+9.73	10.75 Rt
29			5.11	291.64	277.92	+13.72	
	+50	12.10	0.13	296.62	282.98	+14.14	
30			3.90	298.82	287.04	+11.78	
	+50		7.04	301.65	291.60	+10.65	
31	13.11	319.15	2.68	306.04	296.16	+9.88	
	+50		8.75	310.40	300.12	+10.68	7 Rt
32			5.09	314.06	305.29	+8.79	
M.H							
#7	+13.72		4.26	314.89	306.53	+8.86	0.07 of in Grade

Bliss Notes
 Bepp N
 Summer Mgr. Rod.

Check Levels for Grades 0 to 100 Wabasha Redwood to Mth 100
 Mon. 2. Redwood to Mth 100

JM #1	6.17	206.51		200.34	
0+00			5.76	200.75	192.12
+50			6.68	199.83	
1			7.81	201.70	
+50			4.07	202.44	
2			2.28	204.23	
TP	11.75	217.44	0.82	205.69	
+50			11.67	205.77	
3			10.55	206.89	
+50			10.99	207.44	
4			8.48	208.76	
+50			6.31	211.13	
M th #1			5.50	211.94	204.00
5			5.75	211.69	
+50			5.65	211.79	
6			3.90	214.04	
+50	10.73	225.18	2.99	214.45	
7			8.32	216.86	
+50			8.14	217.04	
8			7.11	218.07	
M th #2			5.29	219.89	213.07
+50			5.85	219.33	
9			7.58	220.60	
+50	12.47	235.69	1.96	223.22	
10+00			10.48	223.21	

10	150		955	226.14	
11			839	227.30	
	150		745	228.24	
	MH #3				
12			761	228.08	
	150		420	231.49	
13			240	233.29	
	150		128	234.41	
14	10.69	246.31	0.07	235.62	
	150		893	237.38	
15			684	239.47	
	150		747	238.84	
16			540	240.91	
9 ^o +					
MH #5			401	242.30	
	150		337	242.94	
17	10.18	254.66	1.83	244.48	
	150		840	246.26	
18			838	246.28	
	150		634	248.32	
19			518	249.48	
	150		328	251.38	
MH					
16	+ 84 ¹⁸		248	252.18	
20	out				
	150	12.41	266.90	0.17	254.49
21			1166	255.24	
	150		1037	256.53	

T
266.90

29

22			8.31	258.50
+50			5.93	260.97
23			4.78	262.12
+31.52			3.92	262.98
check BM #			2.39	264.56
+50			3.56	263.34
24			3.73	263.17
+50	11.25	277.07	1.08	265.82
25			9.88	267.19
+50			8.02	269.05
26			6.12	270.95
MH #7 148 ¹³			4.13	272.94
27			2.96	274.11
+50	12.03	287.30	1.80	275.27
28			9.49	277.81
MH #8 +53.47			3.86	283.94
TP	11.96	298.49	0.77	286.53
29			6.87	291.62
+50			1.89	296.60
TP	11.33	308.74	1.08	297.41
30			9.94	298.80
+50			7.09	301.65
31	11.52	317.54	2.72	306.02
+50			7.15	310.39
32			3.49	314.05
MH #13 49			2.66	319.88

Sewer Grades East San Diego

Sorter from M.H. #9 sta 32+13⁷² to End of job

BM.						cuts
	387	322.22	318.35	SE 1/4 W1/4 T100 #382		
32+13 ⁷² M.H. #9			7.40	314.82	306.53	+8.29 ✓
+50			6.05	316.17	306.89	+9.28 ✓
33			5.20	317.02	307.39	+9.63 ✓
+50			4.58	317.64	307.83	+9.75 ✓
34			4.23	317.99	308.39	+9.60 ✓
+50			3.90	318.32	308.89	+9.43 ✓
35			3.76	318.46	309.39	+9.07 ✓
M.H. #10 +60 ⁶⁴	11.9	330.68	2.96	319.26	310.00	+9.26 ✓
36			10.45	320.23	312.70	+7.53 ✓
+50			6.57	324.11	316.12	+7.99 ✓
37		343.11	2.69	328.04	317.55	+8.49 ✓
+50			11.86	331.25	322.97	+8.28 ✓
38			9.35	333.76	326.40	+7.36 ✓
+50			7.04	336.07	329.81	+6.26 ✓
M.H. #11 +67 ⁶⁴			6.91	336.70	331.02	+5.68 ✓
39			5.36	337.75	331.86	+5.89 ✓
+50			3.83	339.28	333.16	+6.12 ✓
40			2.61	340.50	334.46	+6.04 ✓
+50		350.35	1.36	341.75	335.76	+5.99 ✓
41			7.27	343.08	337.06	+5.02 ✓
+50			5.95	344.40	338.36	+6.04 ✓
M.H. #12 +79 ⁶⁴			5.18	345.17	339.00	+6.17 ✓

BM.

318.35
3.87 +
322.22 x
2.96 -
319.26
11.9 +
330.68 x
6.16 -
330.52 +
12.59 +
343.11 +
1.36 -
341.75 +
8.60 +
350.35

42+00		4.56	345.79	339.44	+6.35 ✓
+50	353.39	4.13	346.22	340.31	+5.91 ✓
43		6.90	346.49	341.19	+5.30 ✓
+50		6.01	347.38	342.06	+5.32 ✓
44		5.01	348.38	342.94	+5.44 ✓
+50		4.09	349.30	343.81	+5.49 ✓
45		3.10	350.29	344.69	+5.60 ✓
+50		2.18	351.21	345.56	+5.65 ✓
MH 43+75	359.91	1.59	351.80	346.00	+5.80 ✓
46		7.13	352.22	346.29	+5.93 ✓
+50		6.16	353.25	346.72	+6.53 ✓
47		5.05	354.26	347.21	+7.05 ✓
+50		4.13	355.22	347.63	+7.59 ✓
48+00		3.24	356.17	348.18	+7.99 ✓
+50		2.26	357.15	348.66	+8.49 ✓
M.H. #14 43+69	369.92	1.54	357.87	349.19	+8.68 ✓
+50		6.33	358.59	349.63	+8.96 ✓
50		5.40	359.52	350.11	+9.41 ✓
+50		4.69	360.23	350.59	+9.64 ✓
51		3.98	360.94	351.08	+9.86 ✓
+50		3.23	361.69	351.57	+10.12 ✓
52		2.54	362.38	352.06	+10.32 ✓
MH #15 +15		2.25	362.67	352.24	+10.43 ✓

350.357
4.75
84 MHBP 345.60
302 Unit 7.79
353.397
1.59
351.807
7.63
359.42
1.63
357.72
7.20
364.94
2.25
362.69
7.11
369.80

52 + 50		6.62	363.16	352.53	+10.63	✓
53		5.78	364.00	353.01	+10.99	✓
+ 50		7.99	364.79	353.50	+11.29	✓
54		7.16	365.62	353.98	+11.64	✓
+ 50		3.95	362.33	354.47	+11.86	✓
55		2.70	367.08	354.95	+12.03	✓
MH #16 + 35.15		2.29	367.49	355.29	+12.20	✓
+ 50	372.13	2.16	367.62	355.58	+12.04	✓
56		4.26	367.87	356.49	+11.38	✓
+ 50		4.19	367.94	357.40	+10.54	✓
57		4.00	368.13	358.31	+9.82	✓
+ 50		3.91	368.22	359.22	+9.00	✓
58		3.77	368.36	360.13	+8.23	✓
+ 12.95 MH #17		3.68	368.45	360.37	+8.08	✓
+ 50		3.56	368.57	360.63	+7.94	✓
59	373.41	3.91	368.72	360.98	+7.74	✓
+ 50		4.39	368.92	361.32	+7.60	✓
60		4.41	369.00	361.68	+7.32	✓
+ 50		4.11	369.29	362.03	+7.26	✓
+ 91.25 MH #18		3.72	369.68	362.32	+7.36	✓
61		3.99	369.42	362.38	+7.04	✓
+ 50	374.80	4.85	369.95	362.73	+7.22	✓
62		4.73	370.07	363.08	+6.99	✓
+ 50		4.41	370.39	363.43	+6.96	✓
63		4.23	370.57	363.78	+6.79	✓
+ 50	? Check this	3	370.85	364.13	6.72	✓
MH + 19 + 94 #3	377.08	3.64	371.16	364.44	6.72	✓

369.80
 1.69 -
 368.11 TP
 4.04 +
 372.15 x
 3.41 -
 368.74 TP
 4.63 +
 373.43 x
 3.20 -
 370.23 TP
 4.75 +
 374.98 x
 3.64 -
 TP 377.18
 5.82
 377.10

32
T
377.08

64+50		5.98	371.60	364.83	+6.77
65		5.15	371.93	365.18	+6.75
+50		4.91	372.17	365.53	+6.64
66		4.58	372.50	365.88	+6.62
+50		4.18	372.90	366.23	+6.67
MH#20 31					
+97		3.95	373.13	366.56	+6.57
67+50	380.48	3.20	373.88	366.91	+6.97
67+80		5.81	374.67	367.12	+7.55
68+00		5.45	375.03	367.26	+7.77
pvc					
8x +90		5.14	375.34	367.55	+7.79
8x +60		4.93	375.55	367.73	+7.82
8x +80		4.90	375.58	368.01	+7.57
8x					
69		4.78	375.70	368.37	+7.33
+20		4.62	375.86	368.82	+7.04
70+40		4.42	376.06	369.35	+6.71
EXC					
+60		4.20	376.28	369.98	+6.30
70+01		3.66	376.82	371.36	+5.46

33

cuts

377.08
358
373.52 B17
SWIFT
210/22
2275
378.50
298
380.48

Grade Change from 41+50 to

42+57. Necessitated by Elec. Conduit

cuts

N. Side of Univ.

Elev. Stake

Elev. Profile

BM

NW Univ 38

395.60

48.21

350.92

41+50

350.92

344.90

338.26

+ 6.04

M.H.

#12 +74.64

Elevs of cut

stakes copied

from original

Notes

page 30

345.17

338.65

+ 6.52

42+00

345.79

338.95

+ 6.84

+57. Ch. Conduit

423

346.19

332.63

+ 6.56

Check Levels on Grade Stakes East San Diego
Sewer

BM.					
	4.95	322.80		318.35	5.57 [±] 4.6 N 61° 40' 30"
M.H. #9			7.98	314.82	
+50			6.63	316.17	
33			5.78	317.02	
+50			5.17	317.63	
34			4.81	317.99	
+50			4.49	318.31	
35			4.33	318.47	
M.H. #10	11.03	330.29	3.54	319.26	
+60 [±]					
36			10.05	320.24	
+50			6.17	324.12	
37			2.25	328.04	
T.P.	12.01	341.86	0.94	329.85	
+50			10.61	331.25	
38			8.10	333.76	
+50			5.79	336.07	
M.H. #11			5.16	336.70	
+67 [±]					
39			4.11	337.75	
+50			2.57	339.29	
40			1.36	340.50	
T.P.	8.11	349.70	0.27	341.59	
+50			7.95	341.75	
41			6.62	343.09	
+50			5.37	344.39	
M.H. #12			4.54	345.16	
+74 [±]					

42			392	345.78	
	+50		3.98	346.22	
check	#10 #11 #12 #13 #14 #15 #16 #17 #18 #19 #20 #21 #22 #23 #24 #25 #26 #27 #28 #29 #30 #31 #32 #33 #34 #35 #36 #37 #38 #39 #40 #41 #42 #43 #44 #45 #46 #47 #48 #49 #50 #51 #52 #53 #54 #55 #56 #57 #58 #59 #60 #61 #62 #63 #64 #65 #66 #67 #68 #69 #70 #71 #72 #73 #74 #75 #76 #77 #78 #79 #80 #81 #82 #83 #84 #85 #86 #87 #88 #89 #90 #91 #92 #93 #94 #95 #96 #97 #98 #99 #100	8.24	353.84	910	345.60
43			7.35	346.49	
	+50		6.46	347.36	
44			5.97	348.37	
	+50		4.54	349.30	
45			3.55	350.29	
	+50		2.62	351.22	
	+75	MH4	2.05	351.79	
46	7.63	359.86	1.61	352.23	
	+50		6.61	353.25	
47			5.49	354.37	
	+50		4.64	355.22	
48			3.69	356.17	
	+50		2.70	357.16	
	MH4		1.99	357.87	
49	7.60	365.32	2.14	357.72	
	+50		6.72	358.60	
50			5.80	359.52	
	+50		5.08	360.24	
51			4.36	360.96	
	50		3.62	361.70	
52			2.94	362.38	
	MH #12	+19.15	2.65	362.67	

7
365.32

39

52	1.50		2.17	363.15	
53	7.78	371.76	1.34	363.98	
	1.50		6.99	364.77	
54			6.16	365.60	
	1.50		5.45	366.31	
55			4.70	367.06	
M.H	10' Diagonally NE				
	+34.15		4.29	367.47	
	+50		4.16	367.40	
56			3.90	367.86	
B.M.			3.68	368.08	NW BP Corner 30'
	1.50		3.85	367.91	
57			3.65	368.11	
	1.50		3.57	368.19	
58			3.42	368.34	
M.H					
#	112.05	5.68	3.34	368.42	
	1.50		5.55	368.55	
59			5.39	368.71	
	1.50		5.69	368.41	
60			5.11	368.99	
	1.50		4.82	369.28	
	+91.75		4.45	369.65	
61			4.68	369.42	
B.M.			4.10	370.00	N.W. 757K 37' 10' 00" H
	1.50		4.16	369.94	
62			4.05	370.05	

+50			3.73	370.37	
63			3.56	370.54	
+50	5.88	376.80	3.28	376.82	
M.H +94.83			5.66	371.14	
64+50			5.22	371.58	
65			4.89	371.91	
+50			4.66	372.14	
66			4.34	372.96	
+50			3.93	372.87	
M.H # +97.21			3.70	373.10	
67+50			2.94	373.86	
check 8M	697	380.47	3.33	373.50 373.47	SWBP H/Gap 37 ²
+80			5.80	374.67	
68			5.45	375.02	
D.V.C. +90			5.14	375.33	
+60			4.92	375.55	
+80			4.90	375.57	
69			4.78	375.69	
+20			4.62	375.85	
+90			4.41	376.06	
R.V.C. +60			4.20	376.27	
Total			365	376.82	

East San Diego Sewer Grades from
 M.H. # 16 Orange 438th 190.2 East to
 Existing M.H. # of Orange + Alley East
 of 38th 8" Sewer

c/s

	376	371.84		368.08		
0+00			4.36	367.48	355.23	+12.19
0+50			4.41	367.43	355.77	+11.66
1+00			4.84	367.00	356.26	+10.74
1+50			5.02	366.82	356.74	+10.08
1+90.2	EX.M.H.	cut on rim of M.H.	5.22	366.62	357.13	+9.49
	NWBP					
BM 38 th Orange	376	371.84		368.08		
	M.H. #					
0+00			4.35	367.48		
+50			4.91	367.43		
1			4.84	367.00		
+50			5.02	366.82		
+90.2	EX.M.H.		5.22	366.62		

Lindbergh Field Sencer Grader
 Lateral No 3 14+50 MH #9 North East

4119 #1675-1
 Harbor #126-79 For B.M.
 states offset 25 FT 8.46 T For Level
 8.78 T For Grader

Sept. 25-44
 S. 5507
 B. 1151
 C. 5607

42

B.M.	4.44	6.81	2.37	2.37	Top Cone Base Pence For 5.75 Coas 5.90	4+50			13.73 4.66 c9.67	-4.95	
B.M.	3.50	6.75	3.26	3.26	S. E. Top Conch Road 17.11 20.15 22+50	5+0			13.63 4.61 c9.02	-4.85	
	5.05	7.86	3.94	2.81	1.7 2.145 Run way 9.5 11.19 12.00	+50			13.53 4.28 c9.05	-4.75	
	5.20	8.46	4.60	3.26	on 2 St 05 14.50	6+0			13.43 4.18 c9.05	-4.65	
B.M. For Grades	5.49	8.78	3.29	3.29	2.51 0.6 (2.26) 14.50 16.75-11				13.35 4.24 c9.11	-4.57	Flow Line on 07 Rim
2+0 = MH #9 Trunk			14.63 out	-5.85		+38.2 - East MH			07 Rim 3.95	4.51	
+50			14.53 5.20 c9.23	-5.75					15.43	-6.97	Flow Line
1+0			14.47 5.37 c9.87	-5.65							
+50			14.33 5.32 c8.99	-5.55		TP	6.23	9.49		3.26	on 2 St 05 14+50
2+0			14.23 5.19 c9.04	-5.45		B.M.	3.43	8.72	4.20	5.29	H.M. 80 ft Found. plate For Car Wash Hanger 5.130
+50			14.13 4.99 c9.14	-5.25			4.47	10.70	2.49	6.23	
3+0 = MH			14.03 4.92 c9.11	-5.25		B.M.	3.72	11.93	2.49	8.21	Top F Hyd. NECO W. Gate Canopy + Gas 8.155
+50			13.93 4.85 c9.08	-5.15		B.M.			1.16	10.77	Top F Hyd St Laurel + Pacific Hwy 10.735
1+0			13.83 4.73 c9.10	-5.05		B.M.			3.94	7.99	H.M. 80 ft Laurel + Pacific Hwy 7.97

INDEXED
 W.K.
 OCT 25 1948

Lindbergh Field Check Levels
Pacific Hwy + Laurel St to

Sept 27-44
Sisson
81st X
Osborn

BM 3.50 11.44 7.94

N.W. B.P.
Laurel St +
Pacific
#1317-42

INDEXED
OCT 25 1944

BM 2.91 11.08 3.27 8.17

Top Fire Hill
N.E. Westgate
Cannery Laurel

4.70 8.46 7.32 3.76

BM 2.88 8.15 3.19 5.27

N.W. 80th Four
Plate S.W. Car
nest Hanger

3.04 7.40 5.77 2.36

3.18 7.21 3.37 4.03

3.915 6.265 4.86 2.35

BM 2.82 3.445

J.E. Cortez
Head Wall
20th St 22+50
Marker 3-45

Brooklyn A.C. Water Line Grades
 04th St to 66th St.

INDEXED

W.K.
OCT 25 1948

1+14.07		256.51	11 18.0 14.6 6.5 2.7
1+74.07	PXC	258.74	0.1 15.0 13.7 6.5 2.7
1+32.03		260.88	48 18.6 13.5 6.4 2.5
0+0 = 10' E of E 65th St North		262.93 265.03	10.1 9.0 C 7.1 1.5
1+93.73	2x E of E 65th St	263.98 264.38	9.1 5.5 6.5 9.0
1+57.80		265.80	40 6.9 C 3.9
1+17.80		266.74	14 6.7 3.0 C 3.9 4.1
+77.80		266.80 267.00	6.4 3.0 C 3.4 3.8
+37.80		266.57	6.0 3.0 C 3.7 4.3
0+0 = FVC		264.80	10 8.6 3.4 C 3.4 5.6
BM	635	273.41	267.09

2x E of
 Brooklyn
 65th St
 1603-100

stakes offset 15' South of 1st St
 Grades 267.80 to South Curve
 8.07

1+20.53		267.83 268.23	7.8 5.0 C 2.8
BM		590	263.68
1+00.53 = FVC		261.63 262.03	6.0 5.2 C 0.8
TP	1.95	267.98	12.63 266.03
5+57.30		241.54	14 7.4 C 0.7 1.7
TP	0.54	248.66	12.96 248.12
5+14.07 = FVC		250.63 251.03	10.6 4.8 C 5.8 5.7
TP	0.68	261.08	13.04 260.40
4+74.07		257.97 258.37	13.1 11.5 C 3.6 9.0
4+34.07		262.80	40 10.6 8.2 C 2.4 2.8
3+94.07		263.88 264.28	9.2 4.8 C 4.4 2.3
2+54.07 = PXC		262.86	46 10.6 9.2 C 1.4 1.7
3+14.07 = FVC		259.60 260.00	13.2 11.2 C 2.0 2.4
2+74.07		257.54	13 15.0 12.0 C 3.0 3.5
2+32.07		255.76	5.6 17.5 14.2 C 3.3 3.7
1+94.07		254.87 255.27	18.2 15.3 C 2.9 3.3
1+54.07		255.75	18.0 15.0 C 3.0 3.4

Nov 17-44
 S.M.M.
 G.I.S.
 Harbor
 Hazard

44

1700 E
 Brooklyn
 11th St
 232.60

273.41

Brooklyn Ave. Water Line Grader
68th St to 69th St

Stake offset 15' S. of E.S.
Grades 242 Below South Curbs
307

Nov 17-14
Sutton
Bliss
Osborne
Hazard

45

INDEXED

Wly Concess Hall
Brooklyn 69th

12.65 262.03

3+57.25 = F.V.

277.94 ⁵³
81
70
C 1.4
1.8

BM

3+17.25

278.79 ³⁹
76
64
C 1.2
1.2

1+05.22 - 44.69th St

257.10
257.53 out

3+77.25 = P.V.C.

278.62 ²³
83
69
C 1.2
2.2

258.93 15.3
259.33 10.6
C 1.2
3.5

3+21.80

277.77 ⁸²
83
63
C 1.2
2.2

5+90.22

265.91 8.4
266.31 4.2
C 1.2
4.6

1+66.35

277.71 ⁸¹
82
62
C 1.2
2.2

5+37.25

TP 121 279.68 12.90 273.47

270.56 15.8
15.0
C 1.2
3.2

1+10.90

276.85 ⁹¹
90
70
C 1.2
2.5

4+97.25

273.49 12.7
11.7
C 1.2
2.0

0+55.45

276.49 ³⁹
91
76
C 1.2
2.4

4+57.25

275.82 10.5
9.2
C 1.2
1.7

0+0 = F.L. 68th St

275.93 ^{10.0}
80
80
C 1.2
2.4

4+17.25 = P.V.C.

276.88 9.5
7.9
C 1.2
2.0

BM

6.96 286.37

279.41 ^{5.27}
Hus
Brooklyn
68th St

5+87.25

286.37

1915 St. Water Line Grades
 Brooklyn Ave to Imperial
 stakes offset N. East of ²⁵ Grades & Ben E. C.

INDEXED
 W.K.
OCT 25 1948

INDEXED
OCT 26 1948

2+60		251.27 <u>252.06</u> 9700 10.7 8.5 2.2 28.0
2+0		251.67 <u>252.30</u> 10.7 9.1 1.6
1+50 = F.V.C.		252.00 <u>252.50</u> 10.3 7.9 2.4 3.8
1+10		252.33 <u>252.81</u> 9.9 7.1 2.8 2.3
0+70		252.93 <u>252.73</u> 9.3 6.3 3.0 3.5
0+30		254.05 <u>254.56</u> 8.8 8.2 0.6 1.8
0+0 = S.L. Brooklyn		255.26 <u>255.76</u> 7.0 5.2 1.8 3.2
BM	0.72 262.75	262.05 Wilson No 11 Brooklyn 8915st Page 15

BM	4.65	253.45	2nd Pipe 54" Culvert Imperial 10/169 253.44
P	492	252.10	9.57 252.18
3+75		250.50 <u>251.10</u>	11.1 9.4 1.7 2.8
3+75		250.68 <u>251.20</u>	11.0 10.7 0.3 1.3
3+0		251.01 <u>251.90</u>	10.8 8.8 2.0 2.9
		262.75	

Server Grader From Garbage Hopper "P" Line
to Existing Man Hole Under Bridge on Harbor Dr

1664-66

Nov. 24 44
S.V. 807
81148
Osborne
Hayard

47

7.43

8.11 4.11 7.43 332 07 2000
040 P

INDEXED
W.K.
OCT 26 1948

0+0 0.150 6.13 = Flon Line
Faint 42

+50 0.80 7.63
2.58
c 4.05

1+0 0.30 7.13
2.55
c 2.37

+50 -0.20 7.63
5.03
c 2.60

2+0 -0.70 8.13
5.41
c 2.72

+50 -1.20 8.63
5.40
c 3.03

3+0 -1.70 9.13
5.42
c 3.70

+50 -2.20 9.63
5.97
c 3.99

1+0

+50

5+0

+50

+68.3 = Faint, DH

-2.70

-2.20

-2.70

-4.20

-4.28

10.12
6.81
c 3.25

10.63
6.60
c 4.03

11.12
7.78
c 3.37

11.63
6.85
c 4.78

11.86
6.85
c 5.91

Andrew Jackson School Sly Portion
 Grader For Drainage Ditch
 Ditch 375.14 of Sly School Prop. & Seagrove Ditch
 Stake 28.11 "

BM	5.64	378.95		378.29	8.1 9.6 7.4
0+0 = E.L. 54 1/2 St Top Wall			16.71	362.22	
" = Core Gutter			18.25	360.68	
7.15 = Bk. 9.54	372.0	369.4	371.2	370.80	8.1 9.6 7.4
Void See Page 53					
7.40	374.6	376.5	374.9	371.0	7.9 8.0 7.0
1+0	372.5	372.4	371.9	371.87	7.6 7.5 6.7
7.50	372.4	372.3	371.8	371.70	7.2 7.0 6.2
2+0	372.5	372.4	372.4	372.01	6.9 6.2 6.7
7.50	5.6	372.9	372.9	372.87	6.6 6.2 6.2
3+0	373.2	373.0	372.9	372.71	6.4 5.5 5.7

Grades for E. of Ditch

9202-33 Final Grader
 1413-9 Crude
 Re Stake Page 53
 378.93
 Jan. 5 48
 81.55
 48
 05.60

375.0	373.0	372.9	373.0	373.04	5.9 4.9 6.0
140	373.3	373.2	373.2	373.38	5.6 4.2 6.2
7.50	4.2	374.5	373.9	373.71	5.3 4.7 6.5
500	374.1	374.1			
500	374.6	374.4	374.1	374.05	4.9 4.4 6.5
7.50	374.4	374.3	374.4	374.38	4.6 4.3 6.7
600	374.7	374.5	374.6	374.72	4.3 3.8 6.8
7.50	376.0	375.9	375.8	375.05	3.9 4.0 6.1
700	376.4	376.3	376.2	375.39	4.5 3.9 6.1
7.50	376.1	376.0	375.8	375.72	3.3 3.7 6.1

N.	Shine			
	378.93			
8+0	376.2	376.2	376.2	376.06 ^{2.9} / _{0.0}
+50	376.5	376.5	376.5	376.39 ^{2.5} / _{2.6} / _{1.0}
+88	376.7			376.64 ^{2.8} / _{2.1} / _{0.2}
9+0				376.70

5+50	375.5	375.5	375.4	375.5
6+00	375.5	375.4	375.3	375.5
+50	374.9	375.7	375.8	375.9
7+00	375.0	375.8	375.9	376.0
+50	375.8	375.9	376.1	376.2
8+00	376.1	376.2	376.2	376.2
+50	376.3	376.4	376.4	376.4
+88	376.8	376.90	376.95	376.99

X Sections of Ditch

	Elev. at Stake	Elev. at SW of Ditch	Elev. at E of N. Ditch	Elev. at NE of Ditch
--	----------------	----------------------	------------------------	----------------------

0+00				
0+15	369.4	369.8	370.6	370.6
0+40	370.9	371.8	371.4	371.5
1+00	371.5	372.0	372.5	372.6
+50	371.9	372.0	372.5	372.9
2+00	372.7	373.1	373.1	373.2
+50	372.7	373.2	373.3	373.5
3+00	373.4	373.6	373.7	373.9
+50	374.0	374.0	373.9	374.0
4+00	374.6	374.4	374.4	374.5
+50	374.2	374.4	374.7	374.7
5+00	374.5	374.6	374.9	375.1

Main + 32nd Sts
Re-Design of Intersection

INDEXED
W.K.
OCT 26 1948

March 22 45
J. S. S. 07
Bliss
Osborne
Begg

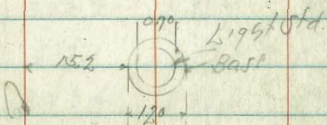
50

Main St.

Exst. Curb ?

$\Delta 39^{\circ}44'$
R 200
T 78.27
L 138.70

$\Delta 30^{\circ}00'$
R 50.00
T 12.00
L 36.18



Light Std.
Base

2070
2110
2140
2170

Prop. 1.2 Diam.

$\Delta 51^{\circ}54'$
CR 28.97
T 14.10
L 23.24

$\Delta 15^{\circ}$
R 93.5
T 12.3
L 22.98

$\Delta 76^{\circ}33'40''$
CR 55.1
T 13.41
L 28.00

$\Delta 15^{\circ}00'$
R 200
T 26.33
L 52.36

$\Delta 54^{\circ}44'$
R 80
T 14
L 29.14

Coll. 07 Fac

38

10'

Main St. Grades South Curb
West of 3rd St
Sketch Page 50

2+69.72 B.C. Pt

+50

2+0

+50

+38.70 = FC. 19° 52'

+25 17° 54' 25"

+10 14° 19' 40"

+75 10° 44' 55"

+50 7° 09' 70"

+25 3° 34' 25"

0+0 = B.C. Pt

51

1+12.43 = H.L. Callen

+50

+10

2+89.05 FC 10° 46' 10"

473.02 7° 10' 46"

1+66.98 3° 35' 20"

+10

2+10.91 B.C. Pt

2+95.90 = FC. 15° 00'

2+82.81 = 1/2 Curve 7° 30'

Main St. Curb Grades
East of 32nd St.

Sketch Page 50

2+08.41 7°39.37'

C=14.70

1+93.71 - P.C.C.

+80.59 - 2 Curve

1+67.47 B.C.Lt

+50.88

1+00.88

+76.81 - 10 7°30'

C=12.23

+64.60 - 2 Curve 5°45'

C=12.23

+52.36 - P.R.C. 7°30'

C=26.16

+26.18 - 2 Curve 5°45'

C=26.16

0+0 - B.C.Lt

2+67.20 F.C. 38°16.83'

+52.51 30°37.16'

+37.81 22°58.10'

2+23.11 15°18.72'

Anders Jackson School Site Portion
Grader For Drainage Ditch

B Sheet 2904
Location + Grader

Sept 21-45
S. J. Iron
81551
O. Garber
8199

53

2 Ditch 375 ft of Site School Prop. Station 46 N of Site School Prop
or 1.0 part 4 of 1.2 Ditch Old Grader Page 48

377.99

BN 4.70 377.99 373.29

Child's
0-7 58
2.5
3.02-23

+50

373.04 ^{4.95}
^{4.17}
c. 0.84

640 = F.L. 54' 1/2" out Corred Concr Gutter

+40

373.37 ^{1.61}
^{3.67}
c. 1.01

425 = grk 370.87

7.12
7.20
Fo. 08

+50

373.70 ^{4.29}
^{5.30}
c. 0.99

440 370.97

7.07
7.49
Fo. 47

+40

374.03 ^{3.96}
^{2.98}
c. 0.98

140 371.37

6.62
5.69
c. 0.93

+50

380.79 2.98 375.01

374.37 ^{6.44}
^{3.92}
c. 1.00

750 371.70

Σ = 00666

6.70
5.78
c. 1.11

+40

374.70 ^{6.09}
^{5.29}
c. 0.80

240 372.04

5.95
4.29
c. 1.76

+50

375.03 ^{5.76}
^{4.82}
c. 0.92

750 372.37

5.62
4.53
c. 1.01

+40

375.37 ^{5.17}
^{4.75}
c. 0.87

240 372.70

5.29
4.23
c. 1.06

380.79

7+50

375.70 ^{5.09}
4.85
co.11

8+0

376.03 ^{4.71}
4.63
co.11

150

376.37 ^{4.41}
4.32
co.10

788 = Conc Hall

376.62 ^{4.19}
4.03
co.37

INDEXED
GET TO READ

Orange Ave. Paving Grades
43rd to 44th St.

Fairmount

INDEXED
WIK
OCT 26 1948

21647

35791

BM 361.01
2.49
363.508
4.87
358.63
4.01
362.64

35795

2159

219657

35795
58.00

2125

58.45

35815
4.87
362.67

Conc Pav

Conc Pav

357.90

Oil & Rock

357.91 Conc Pav

0160

357.55

0176

58.45

0108

357.40

358.15

0107

357.55

357.70

357.40

358.63 Ch

0102

360.19

357.55

357.53

43rd

SX

Fairmount

June 28 45
S. 1100
8/1/51
S. 6000
8/2/51

55

INDEXED
OCT 26 1948

SX
357.95
Paving

357.61
357.67 Paving

Grades Water Main Alley Blk. 14 Toralta
 From Polk to Orange Between 40th & Central
 Stokes offset 4' East of 1/2 Ditch. Grades 3.58 below Fort line

July 19. 15
 5.000
 81.00
 056000
 8099

56

3+55

359.10
 $\frac{99}{59}$
 03.9

INDEXED

W.K.

OCT 26 1948

+ 97.5

358.50
 $\frac{100}{53}$
 04.0

2+40 = Brk

357.90
 $\frac{109}{87}$
 04.2

BM

4.15

364.60

N.M.R.P.
 Orange & 40th
 364.62

TP

7.76

368.84

1.53

361.08

+ 82.5

357.0

$\frac{51}{28}$
 03.6

TP

5.39

368.75

5.48

369.26

1+25

356.2
 $\frac{64}{31}$
 03.3

5+25 = F.L. Orange

360.15

$\frac{8.7}{5.0}$
 03.7

+ 67.5

358.3

$\frac{73}{33}$
 04.0

5+50

360.00

$\frac{8.5}{4.1}$
 04.1

+ 10 = Brk

354.45
 $\frac{8.2}{4.2}$
 04.0

5+10

360.40

$\frac{8.2}{3.9}$
 04.6

0+0 = N.L. Polk

out

1+70 = P.V.C.

360.80

$\frac{8.5}{4.3}$
 04.0

BM

3.84

362.61

358.77

N.M.R.P.
 Polk & 40th

1+25

359.70

$\frac{9.1}{4.9}$
 04.2

368.84

Paving Grades Alley Block 14 Teralta
From Polk to Orange Between 40th & Central

Sold 20-45
S. No
Orange
B. 99 **57**

+86		362.08	$\frac{3.86}{2.23}$ c1.03	361.88	$\frac{3.06}{2.67}$ c1.42
2+40 = B-4		361.60	$\frac{4.34}{3.02}$ c1.00	361.40	$\frac{4.54}{3.57}$ c1.00
+94		360.89	$\frac{5.05}{2.53}$ c0.52 57 cent 100.00	360.69	$\frac{5.35}{4.65}$ c1.00
+48		360.18	$\frac{5.76}{4.76}$ c1.00	359.98	$\frac{5.96}{4.96}$ c1.00
1+02		359.47	$\frac{6.47}{5.47}$ c1.00	359.27	$\frac{6.67}{5.67}$ c1.00
TP	6.39	365.94	3.19	359.55	
+56		358.76	$\frac{3.98}{3.98}$ c0.79	358.56	$\frac{4.18}{3.98}$ c0.79
710 = B-4		358.05	$\frac{4.69}{3.44}$ c0.25	357.85	$\frac{4.89}{4.64}$ c0.33
0+0 = N.L. Polk		357.80	$\frac{4.94}{4.94}$ c0.99	357.80	$\frac{4.94}{4.94}$ c0.99
BM	3.97	362.74		358.77	N.W. 8P Polk + 40th

+95 = 5L Orange					
+50		362.90		362.80	
5+10		364.10	$\frac{5.15}{4.95}$ c0.23	363.90	$\frac{5.35}{3.40}$ old Nail c0.200
+70 = P.V.C		364.00	$\frac{5.25}{4.25}$ c1.00	363.80	$\frac{5.15}{4.62}$ c0.80
4+21		363.52	$\frac{5.73}{3.34}$ c0.89	363.32	$\frac{5.93}{3.73}$ c0.80
+78		362.04	$\frac{6.21}{3.33}$ c0.88	362.24	$\frac{6.41}{5.42}$ c0.98
TP	5.66	369.25	2.25	363.59	
3+32		362.56	$\frac{3.38}{2.58}$ c0.80	362.36	$\frac{3.58}{2.78}$ c0.88
		365.94			

INDEXED
OCT 28 1930

Fairmount Ave Storm Drain Grader
 El Cajon Blvd to Polk Ave

Staked 1/4 East of 1/2 Fairmount Cut on West Curb

Aug 14 1951
 S.W.R.P.
 El Cajon
 0860740 **58**

Cont Page 67

TP 6.93 368.09 2.88 356.07

+50

INDEXED
 W.K.
OCT 26 1948

348.09

13.51
 2.29
 07.97

7+0

350.82

12.18
 2.50
 09.68

8+0

347.69

10.76
 3.21
 07.75

+83 = Clean Out #2

11.77
 3.15
 07.86
 07.11
 10.71

350.75

12.25
 2.22
 09.83

+50

347.29

11.46
 3.52
 07.50

+42 = Clean Out #1

12.04
 3.99
 08.05
 08.07
 10.71

350.42

10.51
 12.58
 2.42
 08.70

2+0

346.89

11.56
 4.20
 07.36

358.52 09 10.55
 3.92
 362.46

6+0

350.09

12.26
 2.83
 08.08

+59

346.49

11.75
 4.79
 07.11

+50

349.69

13.01
 5.12
 08.19

1+0

346.09

12.36
 6.00
 06.36

5+0

349.29

13.71
 5.19
 08.54

+40

= A

345.61

12.81
 6.28
 06.09

+50

348.89

14.11
 5.16
 08.09

0+0

= Existing Curb Inlet
 At El Cajon Fairmount

345.29

13.16
 12.81
 07.11

4+0

348.49

14.61
 6.22
 08.08

BM

642

358.45

352.02

S.W.R.P.
 El Cajon
 Fairmount

363.00

Bliss
 0999 K...
 Sommers for Rod
 4/9/92

Check Levels Pacific Arc. Sewer
 from Sta 11100 to 24170 & of Ivy

PM. NE
 Iron pin site.

3.70 8.64 4.94

Cedar i. H...
 AM. actually
 5.02 See
 paper

11100

4.79 3.85

21100

5.68 9.41

TP.

4.92 8.88 4.68 3.96

22100

5.68 9.41

+50

5.23 3.65

+50

5.28 9.81

12100

6.20 2.68

23100

5.75 9.34

+50

INDEXED

5.31 3.57

+50

4.25 10.14

13100

W.K.
 OCT 26 1948

5.04 3.84

24100

5.31 9.78

+50

4.71 4.17

TP +50 5.11 15.23

4.91 10.18

14100

4.34 4.54

+50

5.36 9.93

TP.

4.71 9.55 4.04 4.84

+70

5.30²³ 10.00

+50

4.80 4.75

check BM 2.56 15.94

1.91 13.38

15100

4.49 5.06

check BM⁴⁴

7.18 8.76

+50

4.21 5.34

5.58 15.66

10.08

16100

4.37 5.18

25100

5.36 10.30

+50

3.65 5.90

+50

5.32 10.34

+ 1 Lt

3.28 6.27

26100

5.29 10.37

17100

3.40 6.15

+50

5.57 10.09

+50

3.07 6.48

27100

5.35 10.31

18100

2.71 6.84

+50

5.34 10.30

+50

2.28 7.27

28100 3.93 14.07

5.52 10.14

19100

1.89 7.66

+50

4.60 9.47

TP.

7.47 15.09 1.93 7.62

29100

3.89 10.18

+50

7.13 7.96

check BM

4.19 9.88

State Hwy

20100

6.48 8.61

+50

4.69 9.38

+50

5.84 9.25

30100

4.62 9.45

T
 1509

+ Note. Range of
 elevation 0.07 - 59
 was 0.07 low

59

Bliss notes
 1899 T
 Summer 1899 Red

Check Levels Pacific Ave Section from 111100

N of A to 11400 South of Elm

	6.71	9.17	2.46
111100		6.20	2.97
+50		5.89	3.28
112100		5.62	3.55
+50		5.40	3.77
113100		5.21	3.96
+50		4.95	4.22
114100 ³⁴	L.M.H & Ash	5.30	3.87
+50		4.68	4.49
115100	5.47 10.02	4.62	4.55
+50		5.45	4.57
116100		5.79	4.23
+50		5.65	4.37
117100		5.13	4.89
BM		5.02	
+50		5.87	4.15
180 ²⁹	M.H.L & Beech	5.58	4.44
118100		5.52	4.50
+50		4.89	5.13
118179.62 = 4120 ²³		4.58	5.44
5100		4.75	5.27
+50	497 10 48	4.51	5.51
6100		5.58	4.90
+50		5.84	4.64
7100		5.80	4.68

Triple check

BM	.493	9.95	5.02	SRBP Beech 18
5100			4.69	5.26
150			4.96	5.49
6100			5.06	4.89
150			5.32	4.63
7100			5.26	4.69
1				
400 BM	3.83	8.84	4.94	5.01 Iron Pin NE Cedar 18
757	M.H.		3.78	5.06
5100			4.00	4.84
150			4.66	4.18
3100			4.26	4.58
150			4.48	4.36
10100			4.65	4.19
10050			4.80	4.04
11100			4.92	3.92
BM	4.03	9.25	5.02	
911			4.52	5.43
11250			4.82	5.13

X
10.98

61

757 ³¹	L.M.H. Mid Cedar	592	5.06
8100		562	4.86
750		628	4.20
9400		589	4.59
750		610	4.38
10400		626	4.22
750		642	4.06
11400		653	3.95

\bar{x}
 14.07
 Check Levels on Grade Pts
 See page 9 original

30+50			4.82	9.25
31+00			5.10	8.97
+50			5.38	8.69
32+00	3.88	12.26	5.69	8.38
+50			4.03	8.23
33+00			4.22	8.00
Check BM			4.17	8.09
			Triple check	
BM	2.31	15.77		13.96
			5.69	10.98
25+00			5.46	10.31
+50			5.42	10.35
26+00			5.40	10.37
+50			5.68	10.09
27+00			5.44	10.31
+50			5.47	10.30
28+00			5.62	10.15
+50			6.30	9.47
29+00			5.60	10.17
TP	3.68	13.55	5.90	9.87
+50			4.17	9.38
30+00			4.10	9.45
+50			4.29	9.26
31+00			4.57	8.98
+50			4.85	8.70

\bar{x}
 13.55

62

32+00				516	8.39
+50				530	8.25
33+00				550	8.05
			4.48	12.60	812
					SE Laurel + Pac. Highway
33+50				505	7.55
34+00				547	7.13
+50				532	7.28
35+00				500	7.60
+50				4.55	8.05
36				492	7.68
+50	6.69	14.90		439	8.21
37				575	9.15
+50				593	9.47
38+00				4.63	10.27
+50				4.11	10.79
39+00				4.19	10.71
+50				3.05	11.85
40+50	5.93	18.84		2.52	12.38
41+00				1.99	12.91
+50				5.45	13.39
42+00				4.95	13.89
+50				4.95	14.39
43+00				3.95	14.89
44+00				2.51	15.33
45+00				0.46	18.38
46+00					130+ Not 9300.00 East of 900

Check Levels Interceptor Sewer
from 0+00 43' Nat Skim Broadway to 11+0
N of A

	4.19	8.87		4.68			
TP on 400 ¹⁵	4.20	8.53	4.54	4.33			
0+00			4.52	4.01	-12.53	16.34	15' 2"
+25			4.30	4.23	-12.51	16.74	
+50			4.37	4.16	-12.43	16.65	
+75			4.47	4.06	-12.47	16.53	
1715 ⁵ L			4.49	4.04	-12.44	16.48	
461745 = 169 45			4.00	4.53	-12.40	16.93	
2+00			4.04	4.49	-12.37	16.86	
+50			4.34	4.19	-12.34	16.53	
3+00	4.14	8.20	4.47	4.06	-12.30	16.36	
+50			4.18	4.02	-12.26	16.28	
4+00			4.26	3.94	-12.22	16.16	
+50			4.30	3.90	-12.18	16.08	
5+00			4.33	3.87	-12.14	16.01	
+50			4.35	3.85	-12.10	15.95	
6+00			4.17	4.03	-12.06	16.09	
+50 L			3.95	4.25	-12.02	16.27	
7+00			3.66	4.54	-11.98	16.52	
+50	3.88	8.63	3.45	4.75	-11.94	16.69	
+78 ⁵⁰ = 7170 ⁸² 707			3.82	4.81	-11.92	16.73	
8+12 MH = 8+01 ²			3.81	4.82	-11.89	16.71	
+50			3.86	4.77	-11.87	16.64	

π
8.53

64

9+00	4.18	4.45	-1183	1628
+50	4.92	4.21	-1173	1600
10+12 ⁰¹ = 10+09 ³³	4.71	3.92	-1174	1566
+50	4.87	3.76	-1170	1566
11+00	⁵ 4 .08	3.55	-1166	1521
+50	5.34	3.23	-1162	1491
+65 ⁴⁶ = 11+57 ⁵⁹	5.38	3.25	-1161	1486

Pac Arc Sewer

Check Levels on Grade Pts 93100 to 56100

TI
14.90

510

65

Station	2.04	20.92	18.38						
93150			548	14.54	54150		5.07	9.83	
44			474	15.68	55100		5.38	9.52	
+50			458	15.84	550		5.58	9.32	
45			446	15.96	56100		5.85	9.05	
+50			429	16.13	FH Check IM	2.35	14.42	2.82	12.08
46			441	16.01	56100		5.38	9.04	
MH #45 +15.75			450	15.92	56150	Void	5.44	8.98	
+50			472	15.70	57	Level out	6.14	8.27	
47	3.48	18.29	561	14.81	+50	of Adjustment	6.26	8.16	
+50			331	14.98	58		5.93	8.49	
48			361	14.68	+50		6.09	8.33	
+50			453	13.76	180		6.16	8.26	
49			447	13.82			6.20	8.22	
+50			489	13.40	FH IM	0.68	12.76	12.08	
50			595	12.34	56100		3.91	9.05	
+50			582	12.47	+50		3.79	8.97	
51			626	12.03	59100		4.50	8.26	
+50	3.32	14.90	671	11.58	+50		4.62	8.14	
52			377	11.13	58		4.30	8.46	
M.H. #46 +33.15			396	10.94	+50		4.45	8.31	
+50			401	10.89	+80		4.54	8.22	
53			498	9.92	61108		4.55	8.21	
+50			512	9.78	+50		4.33	8.43	
54			481	10.09	62100	4.85	13.38	4.23	8.53

Pac. Ave. Check Levels
62150 to

66

62150		13.38	4.68	8.70
63			4.55	8.83
+50			4.68	8.70
64+50			4.68	8.70
+50			5.08	8.30
65			4.75	8.63
+50			4.88	8.50
66			5.50	7.88
+50	A.42	12.73	5.07	8.31
67			5.12	7.61
+53 ³⁰			5.28	7.45
68			4.64	8.09
B.C. ⁷⁴ +45	3.55	13.74	4.53	8.20
69			5.34	8.40
+50			5.78	7.96
70			4.98	8.76
+26 B.C.			4.92	8.82
+50			4.86	8.88
71			4.69	9.05
+50			4.53	9.21
72	5.73	15.04	4.43	9.31
+50			5.78	9.26
73			5.54	9.50
+48 ⁰⁹ E.C.			5.28	9.76
74			5.30	9.74
check gm. ^{CP TK} 10 Post. Ch. Pac. 29' N. of Neb. line			5.05	9.99

Fairmount Hvc Storm Drain Grader
 El Cajon Blvd. to Polk Hvc
 Cont From Page 58

11+0				352.42	11.5 4.84 C6.61
+50				352.22	11.35 4.76 C6.60
10+0				352.02	11.55 4.84 C6.71
+50				351.82	11.55 4.84 C6.71
TP	494	363.57	4.57	358.63	
9+0				351.62	11.38 4.82 C6.73
+50				351.42	11.58 4.84 C6.74
8+0				351.22	11.78 4.82 C6.73
7+45				351.00	12.00 4.78 C6.72

363.00

Cont From Page 58

8.77

4.57 359.00

N.W. 8P
Polk
Fairmount
359.10

7917 - Clear Out #6

358.18

10.39

+50

350.02

10.35
4.61
C6.94

12+0

352.82

10.25
4.52
C6.73

11+50

352.62

10.95
4.69
C6.26

363.57

Polk Ave Storm Drain Grader
 Fairmount to 43rd St.
 Stated 105 South of North Line Polk

Curb Inlet #12

355.02

8.86
 4.28
 c 4.74

3403.2 = Cleanout #7

Curb Inlet #11

355.00

8.86
 4.28
 c 4.58

354.75

9.11
 4.28
 c 4.79

+50

354.47

9.31
 4.28
 c 4.81

210

354.21

9.65
 4.28
 c 5.00

+50

353.95

9.91
 5.12
 c 4.79

110

353.70

10.13
 4.98
 c 5.35

+50

353.41

10.41
 4.28
 c 5.41

040 = Cleanout #1 Fairmount

353.18

10.68
 4.28
 c 5.79

814

486

363.86

359.00

NW Cor
 Polk &
 Fairmount

Fairmount & Polk Curb Inlets &
 Storm Drains

BM 543 364.43

359.00

NW Cor
 Polk & Fairmt.
 Page 67

NW Cor Fairmount & Polk

Curb Inlet #9

354.00

10.43
 5.19
 c 5.24

Cleanout #6

353.70

353.18

S-W Cor Fairmount &

Curb Inlet #10

355.80

8.63
 5.19
 c 5.50

Cleanout #6

355.50

353.18

Orange Hic. Storm Drain Grader
Fairmount to Copeland

Staked 21 Herts of South Line Orange Stake 6 N of 200

Curblet #5 SW 4th 355.50 ^{9.89} 5.01
 +43.4 = Clear Out #3 ^{c 4.88} 352.41 07.72

TP 5.35 365.39 2.99 360.04 ^{10.22} 2.78
 370 352.25 07.80

+50 352.00 ^{11.03} 7.66

370 351.75 ^{11.22} 07.55

+50 351.50 ^{11.53} 07.47

170 351.25 ^{11.75} 07.31

+50 351.00 ^{12.03} 07.23

070 = Clear out #2 Fairmount 250.75

B.M. 7.45 363.03 358.58 ^{07.57} 07.57
 #2 Foye

Aug 17-45
 J. J. J.
 R. J. J.
 Osborne

+50 354.50 ^{10.89} 4.04
 06.85

770 H.W. Vanduyke
 Curblet #6 355.50 ^{9.89} 2.99
 05.42 254.25 ^{11.14} 4.57
 06.77

18' Fols. Vanduyke So.
 +48.8 = Clear Out #4 ^{9.59} 354.00 ^{11.39} 4.76
 S.F. Vanduyke
 Curblet #7 355.80 ^{4.57} 05.62
 07.06 06.69

170 353.75 ^{11.64} 4.28
 07.16

+50 353.50 ^{11.89} 4.93
 07.16

570 353.25 ^{12.14} 4.96
 07.22

150 353.00 ^{12.39} 4.88
 07.51

470 352.75 ^{12.64} 5.00
 07.64

365.39

Orange Ave Storm Drain

B.M.

360

361.79

N.W. Cor
Orange &
Copeland
361.90

N.E. of Copeland
Curb Inlet #8

355.54

9.85
4.78
6.40
6.05

9706.8 = Clean out #5

355.29

10.10
3.80
6.30

750

355.00

10.87
3.80
6.47

870

5=005

354.75

10.64
4.11
6.53

36539

Fairmount + Orange Curb Inlet #2
Storm Drains

B.M.

445

363.03

358.58

7.0
07 42 18.7
6100.0 out
#2

N.W. Cor Orange & Fairmount

Curb Inlet #1

353.20 Drop

9.83
4.54
5.19 on 10.6.80

Clean out #1

353.20 Storm Drain

S.W. Cor Orange & Fairmount

Curb Inlet #3

353.50

9.53
4.40
5.13 on 10.6.80

Clean out #2

353.00 Drop

S.E. Cor Orange & Fairmount

Curb Inlet #4

353.50

9.53
4.47
5.04 on 10.6.80

Clean out #2

352.00 Drop

N.E. Cor Orange & Fairmount

Curb Inlet #2

353.20

9.83
4.80
5.00

Clean out #1

352.00 Drop

350.92 Storm Drain

Grader Saranac St Southy Carb
70th St to 300' West

Southy Carb HCL
states set 5' W of Ch

Aug 28-45
S. 2009
81-1-1
S. 2009
81-1-1

240

471.00

7.1
6.6
60.5

450

471.28

6.8
5.8
07.0

INDEXED

WK

OCT 26 1948

240

= FVC

471.55

6.5
5.0
07.5

471.47

7.0
2.8
07.9

460

471.30

6.8
4.5
07.3

471.25

6.1
2.2
07.3
Chas. Stone

1420

470.15

7.9
2.6
03.6

480

468.05

10.9
8.2
02.8

467.90

7.5
0.2
07.3

TP

706

478.06

1.17

471.00

460

460

4664

4.6
0.8
03.8

440

= PVC

465.09

7.1
2.4
03.7

464.80

6.2
2.0
04.2

040

= W.L. 70th

461.64

10.5
10.8
00.7
08.12

BM

11.83

472.17

460.34

2 1/2
Saranac St
1073-66

4 1/2

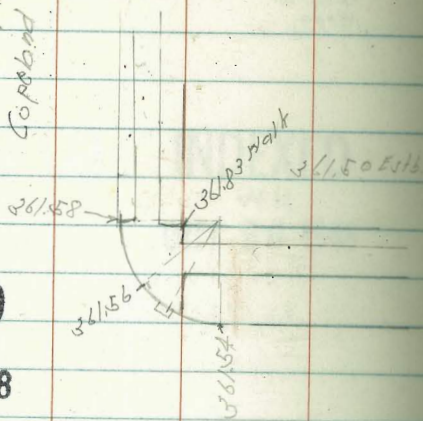
10.70

471.04

460.34

Orange Ave Curb Inlet Grader

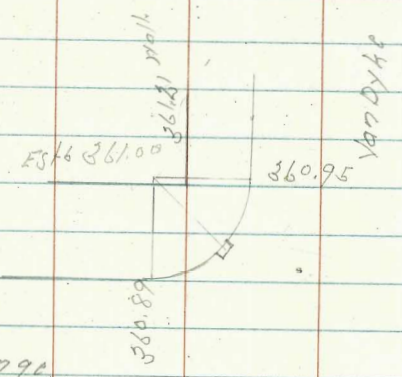
Sept 17-45
 S. J. ...
 B. J. ...
 B. J. ...
 72



INDEXED
 W.K.
 OCT 26 1948

Orange

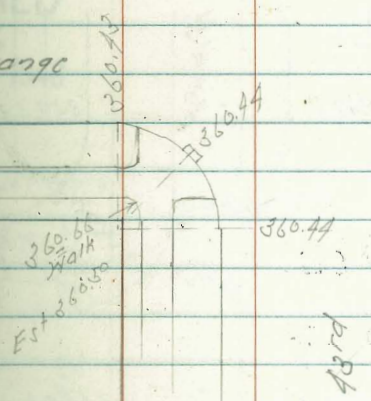
BM	570	367.60	361.90	NXRP Orange Cape Town
Return			361.56	6.04 5.16 0.88 on Rad



Orange

BM	427	366.27	361.90	NXRP Orange Cape Town
Return			360.92	5.35 4.69 0.67 07 Rad.

Orange



BM	473	365.74	361.01	NXRP Orange Cape Town
Return			360.44	5.36 4.86 0.94 on Rad.

Federal Blvd. Gutter Grades South Part
East of 47th St

Sept 22-45
S. 11.50
8.11
8.99

74

42.50 ft 85.50 ft

240 INDEXED
W.K.
OCT 26 1948

750	220.50	4.42 5.72 0.60	220.95	3.91 4.10 F0.22
240	220.50	4.72 4.72	221.19	3.71 3.22 0.0
750	229.75	5.17 5.17 0.0	229.86	4.01 4.22 F0.17
140	229.27	5.65 5.65 0.0	229.27	4.61 4.61 F0.0
750	228.80	6.12 6.12 0.0	229.52	owl
735	228.56	6.36 6.36 0.0	229.47	owl
070	- E. 47th South	6.59 5.22 0.77	228.85	
BM	6.87	224.92	228.05	2.21 Federal 47th St

Curb Grades For Grading
 Laurel St. 33rd St. to Felton

H Stake 5' H of 112
 S " 075 L.

Oct 22-48
 S 18' 00"
 8 1/2"
 056072

75

1+90	144 74 c 7.0 on fence	269.54	269.04	74 77 F 6.3
+20	124 54 c 7.0 on fence	271.51	271.01	74 69 F 5.3
1+0	106 79 c 5.7	272.30	272.80	-0.4 57 F 6.1
TP	123	272.40	1274 271.17	
+80	91 58 c 5.3	274.81	274.31	96 57 F 5.1
+60	78 54 c 4.4	276.09	275.59	83 49 F 3.6
+40	68 32 c 3.2	277.13	276.63	73 32 F 4.1
+20	66 36 c 3.1	277.95	277.45	65 37 F 0.2 on wall
0+0 =	5.0 5.0 on curb	FL 33rd St 278.85	277.90	5.0 5.0 on curb
BM	4.93	283.91	278.98	5.0 5.0 on curb Laurel St 1383-62

INDEXED
 W.K.
 OCT 26 1948

INDEXED
 OCT 26 1948

2+10	114 89 c 7.5	261.00	260.50	119 72 F 5.3
+80	78 58 c 7.0	264.85	264.35	81 50 F 5.7
1+60	166 86 c 8.0 on fence	267.33	266.83	166 83 F 8.7
		283.91	272.40	

5/29/42

Grades Pac Ave Sewer Between
Spruce + Sassafras

5818
5819
5820

76
Front of
BP Adm Bldg 12.175
Ryan 3.69 +
Lindberg 15.86 +

pipe in place

INDEXED
W. K.
OCT 26 1948

13.88

58180 60+90
58160 to 58118
Note error in picture Sp
off plan - Grad changed from
to 1.00 to conform with

pipe in place Seepage 6

58+80	5.64	8.24	-6.95	14.73
+33.95	13.46	1.0.42	-6.462	6.88
+73 21	13.28	0.60	-6.42	7.02
56+14.84	13.56	0.38	-6.38	6.76
+54.03	13.47	0.41	-6.34	6.75
+74.18	13.31	0.57	-6.32	6.83
57+18	5.66	8.22	-6.28	14.50 ✓
	12.94			
55+00	4.70	8.20		
+33.95	12.52	0.42		
+73 21	12.34	0.60		
56+14.84	12.56	0.38		
+54.03	12.53	0.41		
+74.18	12.37	0.57		
57+18	4.72	8.22		

12.07 TP
1.811
13.88 +
3.79 -
10.09 BM
10.15
13.88 +
5.66 -
6.22 TP
4.72
12.94 +
3.74 -
9.20 TP
6.65 +
15.85
3.65
12.17

Grades For Curb Returns
Commercial + Evans

" + 27th .154 FLAT
+ 25 154

Imperial Hill

INDEXED

WIK

OCT 26 1948

Setcb Back 112
to State
25 Roadway
Exit Co 7
63.66
cross
10
125
125
103
69.03
R10
R10

4.99

4.51

Commercial

BM 0.25 77.71 77.46 NEBP
Lst + 27th

TP 3.48 69.50 11.69 66.02

TP 5.51 69.18 5.83 63.67
HM End of
Comm + 27th

BM 3.98 65.20
NE BP
Setcb Back
Commercial
+ 27th

BM 4.86 68.53 63.67

Feb. 15-46
Sutton
asbiron 77
Begg
Wodden

Stakes Set

INDEXED

WIK

OCT 26 1948

FLAT
65.05

4.74

64.71

Commercial

3.98
64.50
R10

4.88

65.00

69.18
65.00
4.18

Curb Grades North Side Commercial
 30th St. to 31st St.
 stakes offset 2' North of N.C. line

Feb 20-46
 S. W. B. P.
 5060 1/2
 Model

78

INDEXED

W K

OCT 26 1948

3+0			72.00	1.87 1.87 0.00				
+50 = Fly Cb + Walk			72.82	5.04 5.02 0.02	BM	3.76	74.10	N.W. B.P. Commercial 30th St.
2+0			72.66	5.26 5.11 0.00	6+0 = W.L. 310th St.		74.00	3.86 3.80 0.06
+50			72.49	5.37 5.34 0.03			73.82	4.84 3.88 0.96
1+10		0.00	72.36	5.50 5.45 0.05	+25 = Fly Cb + Paving		73.73	4.11 4.10 0.01
1+0 = Fly Cb + Walk					5+0		73.66	4.20 4.20 0.00
+50			72.16	5.70 5.70 0.00			73.49	4.58 4.58 0.00
0+0 = Fly 30th St.			72.00	5.86 5.86 0.00			73.32	4.54 4.54 0.00
TP	536	77.86	6.25		4+0			
			72.50				73.16	4.71 4.71 0.00
BM	378	78.75	74.97	N.W. B.P. Imperial 30th St.	3+50			

7786

Indexed
C.R.K.

Lots 11 & 12 Alley, BIK #22, Resub. BIKs. K & L, Terata
 Sommermejer Set. Grades west side Alley
 Begg
 FOX Bet Van Dyke #43 orange + El Cajon
 NWBR orange
 Van Dyke BM. 5.86 366.89 361.03 FB 1256
 Page 58

5.70 369.84 2.75 364.14
 N. Lind orange
 = 0700

3+00 3.70 366.14 364.14

3+25 4.54 365.30 364.30

3+50 4.41 365.43 364.43

T.P. 5.44 364.10

ck.BM. 234 366.74 5.71 361.03 ok

C-2.00 Nail in P. Pole # PA. 4249
 C-1.00 1x1 stake
 C-1.00 ✓ ✓

Levels to check flow line of
Pipe in place N. of "A"

B.M. 19 Tie out for 11100	4.96	7.94	2.98
Flow line			13.48 - 11.54 ✓

Levels To Establish Elev of
Pipe in Place 37th + E. of Cajon

	4.94	378.46	373.52
67+88 Pipe in place Brk		350 + 7.57 11.07	367.39 ✓
68+40 PVC		3.12 7.79 10.91	367.55 ✓

0.73 746 7.79
312 83
737 664
07.112
7.46 87.6
3.52 367.50
1096 1096
367.50
367.50

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00'	0.1	21°-00'	12.3	33°-00'	29.7
3°-00'	0.3	21°-30'	13.4	33°-15'	30.1
4°-00'	0.5	22°-00'	14.0	33°-30'	30.5
5°-00'	0.8	22°-30'	14.7	33°-45'	30.9
6°-00'	1.1	23°-00'	15.3	34°-00'	31.3
7°-00'	1.5	23°-30'	15.9	34°-15'	31.7
8°-00'	1.9	24°-00'	16.5	34°-30'	32.1
9°-00'	2.5	24°-30'	17.2	34°-45'	32.5
10°-00'	3.0	25°-00'	17.9	35°-00'	32.9
10°-30'	3.3	25°-30'	18.6	35°-15'	33.3
11°-00'	3.6	26°-00'	19.2	35°-30'	33.7
11°-30'	4.0	26°-30'	19.9	35°-45'	34.1
12°-00'	4.3	27°-00'	20.6	36°-00'	34.6
12°-30'	4.7	27°-30'	21.3	36°-15'	35.0
13°-00'	5.1	28°-00'	22.0	36°-30'	35.4
13°-30'	5.5	28°-30'	22.8	36°-45'	35.8
14°-00'	5.9	29°-00'	23.5	37°-00'	36.2
14°-30'	6.3	29°-30'	24.3	37°-15'	36.6
15°-00'	6.7	30°-00'	25.0	37°-30'	37.1
15°-30'	7.2	30°-15'	25.4	37°-45'	37.5
16°-00'	7.6	30°-30'	25.8	38°-00'	37.9
16°-30'	8.1	30°-45'	26.2	38°-15'	38.3
17°-00'	8.5	31°-00'	26.5	38°-30'	38.7
17°-30'	9.0	31°-15'	26.9	38°-45'	39.1
18°-00'	9.5	31°-30'	27.3	39°-00'	39.6
18°-30'	10.1	31°-45'	27.7	39°-15'	40.0
19°-00'	10.6	32°-00'	28.1	39°-30'	40.5
19°-30'	11.2	32°-15'	28.5		
20°-00'	11.7	32°-30'	28.9		
20°-30'	12.3	32°-45'	29.3		

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{Mv^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

288
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TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

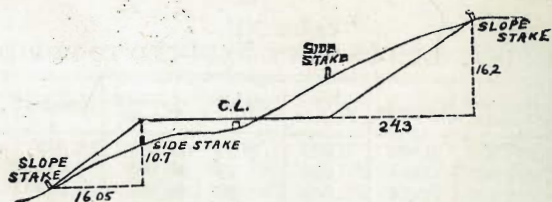
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 30"	.50833	40' 30"	.67500	50' 30"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

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52.33.15

36808

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4.905
3
4.875

Cut 7.46 S of d. El Cajon
To flow.

- 6.78

200 12.74

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09
2+65.40
56

822
7.72
117180.09
100
59

2165.40 - 11.77
1.80
26540.3

282
100.12
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99.53

5.16

1325
8.22
8.03

58880

114 + 3
218
60.48 6150

117180.09
99.53

-6.760
255
-6.495
023
-6.462
020
-6.422

63+75.62

d. Sassefras. 118+79.62

118+79.62 = 4+39.03

118779.62

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4 89.20
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7 77.5
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14 40.29
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73.71
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56+14.84

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111550
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1338
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13.45
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13.46

- MH #1 22°54' 44"
- MH #3 12°02' 40" 44"
- MH #4 12°29' 10" 44"
- MH #6 42°00' 00" 44"
- MH #7 25°15' 44"
- MH #8 50°25' 44"