

G-223



G-223

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MADE IN U. S. A.

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2-63 Const Grades, Location of Bldgs, streets
etc Riverlawn Housing Project

64-67 Sewer Const on National Ave west
of 43rd St and in Carruther Add south
of Logan Ave

68 Curb Grades Collier Ave from W Line 54th

69-73 8th & Robinson (Calvert Grades & Location)

77 43rd & Market (Grades Proposed Calvert)

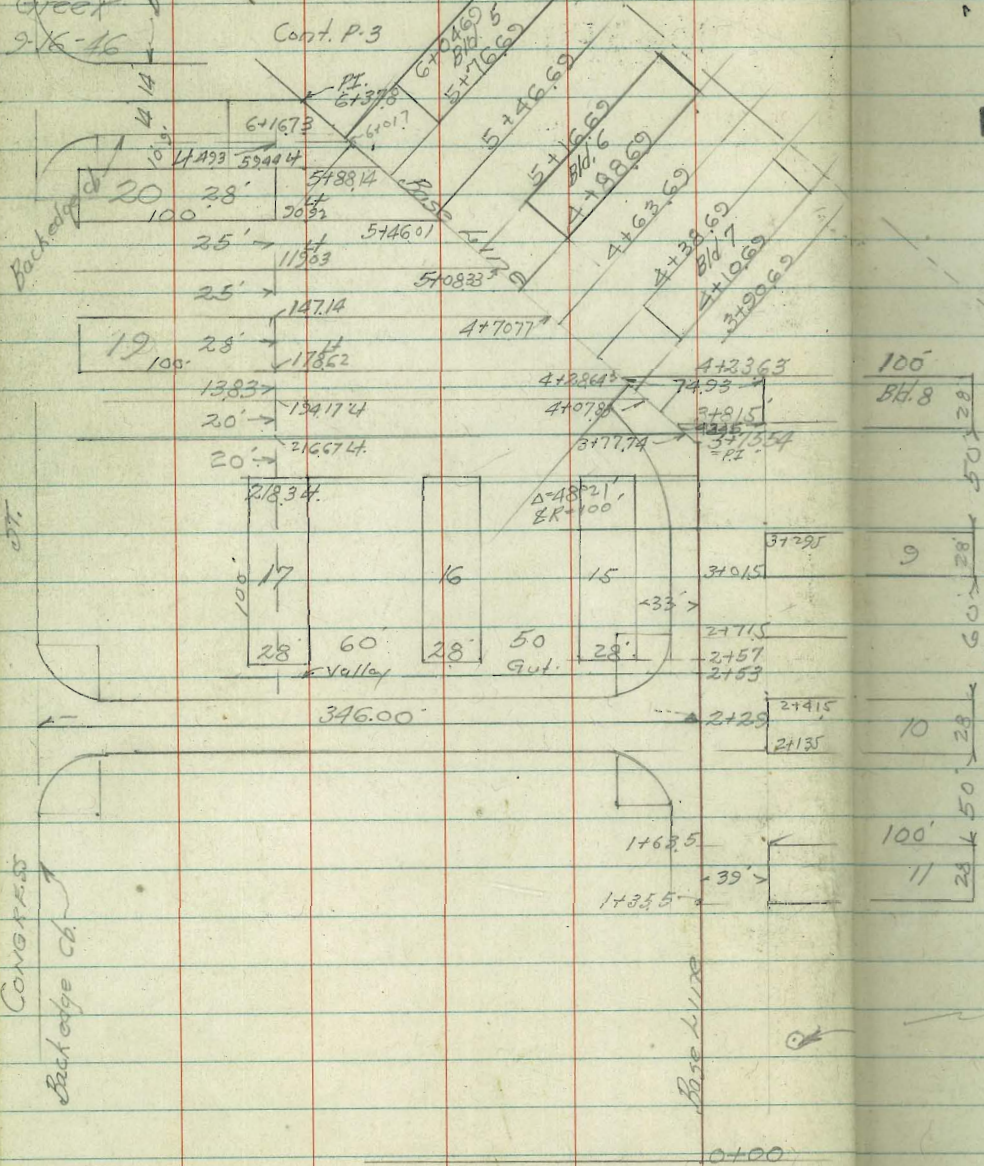
78 Grades for Topping existing curb on
W side 30th St from S Line G to Alley

79 Law St Ingraham to Jewell
(Grades for 6" Water Main)

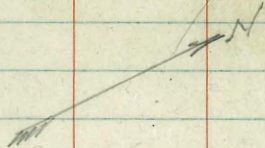
Walker
Hendricks
Becker
Greer
9/6-16

RIVER LAWN - Const. Grades
Veteran's Housing Project.

Cont. P. 3



INDEXED
WK
NOV 18 1949



CONGR. 1.55
Back edge cd

FB 1734-4

Corr. B.M. = Base of Flag Pole Elev = 5.79

River Lowry - Const. Grades
for Grounds.

Station	1.80	9.26	7.46	Fire B.M. Top Hwy Fleet + Congress Elev. Grade	cut & Fills
~0+00~			El. Stakes		
29'R		4.34	4.92	4.55	+0.37
E		5.60	3.66	4.37	-0.21
21'Lt		5.06	4.20	4.59	-0.39
71'Lt		5.20	4.06	4.63	-0.57
111'Lt		4.56	4.70	4.65	+0.05
~0+20~					
111'Lt		4.09	6.17	4.60	+0.57
71'Lt		4.76	4.50	4.70	-0.20
21'Lt		3.82	5.44	4.65	+0.79
E		5.09	4.17	4.63	-0.46
29'R		4.54	4.72	4.60	+0.12
~0+48~					
29'R		4.19	5.07	4.60	+0.47
E		4.72	4.54	4.62	-0.08
21'Lt		4.57	4.69	4.63	+0.06
71'Lt		4.67	4.59	4.65	-0.06
111'Lt		4.25	5.01	4.57	+0.44
~0+73~					
111'Lt		4.18	5.08	4.55	+0.53
61'Lt		4.90	4.36	4.50	-0.14
33'Lt		4.77	4.49	4.47	+0.02
E		4.48	4.78	4.44	+0.31
29'R		4.10	5.15	4.92	+0.73

	Rods				
27.28					
29'R	4.09	5.17	4.38		+0.79
L	4.31	4.95	4.48		+0.47
33' L	4.84	4.42	4.60		-0.18
61' L	4.80	4.46	4.60		-0.14
86' L			4.58		
111' L	4.12	5.14	4.60		+0.54
<u>1+17.5</u>					
L	4.39	4.87	4.40		+0.47
29'R	3.91	5.35	4.35		+1.00
89'R	4.22	5.04	4.28		+0.76
139'R	4.74	4.52	4.20		+0.32
<u>1+30</u>					
L	4.25	5.01	4.73		+0.28
23' L			4.50		
33' L	5.18	4.08	4.63		-0.55
61' L	5.04	4.22	4.65		-0.43
111' L	4.30	4.96	4.60		+0.36
161' L	3.69	5.57	4.66		+0.91
231' L	3.49	5.83	4.75		+1.08
<u>1+35.5</u>					
L	4.28	4.98			
39'R	4.18	5.08	4.45		+0.63
89'R	4.30	4.96	4.33		+0.63
139'R	4.56	4.70	4.20		+0.50
<u>1+49.5</u>					
33'R	4.24	5.02	4.30		+0.72

~ 1463.5 ~

139'R	4.85	4.41	4.20	+0.21
89'R	4.61	4.65	4.27	+0.38
39'R	4.33	4.93	4.35	+0.58

~ 1470 ~

33'L	4.88	4.38	4.67	-0.29
61'L	4.77	4.49	4.70	-0.21
111'L	4.42	4.84	4.70	+0.14
161'L	3.85	5.41	4.80	+0.61
211'L	3.70	5.56	4.90	+0.66
231'L	3.56	5.70	4.80	+0.90

~ 1488.5 ~

39'R	5.44	3.82	4.25	-0.43
89'R	4.62	4.57	4.18	+0.39
139'R	4.24	4.32	4.10	+0.22

~ 1498 ~

33'L	4.49	4.77	4.70	+0.07
61'L	4.52	4.74	4.75	-0.01
86'L	4.58	4.68	4.65	+0.03
111'L	4.44	4.82	4.80	+0.02
161'L	4.09	5.17	4.87	+0.30
211'L	3.91	5.35	4.95	+0.40

~ 2406 ~

231'L	3.79	5.47	4.85	+0.62
211'L	3.96	5.30	4.85	+0.45

2+06					
161'4	4.12	5.14	4.78	+0.36	
111'4	4.42	4.84	4.70	+0.14	
86'4	4.40	4.86	4.68	+0.18	
47'4	4.78	4.48	4.65	-0.17	
2+13.5					
39'R	4.59	4.67	4.35	+0.32	
89'R	4.81	4.45	4.28	+0.17	
139'R	4.83	4.43	4.20	+0.23	
2+27.5					
33'R	4.53	4.73	4.20	+0.53	
2+41.5					
139'R	4.52	4.74	4.10	+0.64	
89'R	4.82	4.14	4.18	+0.26	
39'R	4.66	4.60	4.25	+0.35	
2+53					
47'4	4.92	4.34	4.70	-0.36	
86'4	4.78	4.48	4.65	-0.17	
125'4	4.42	4.84	4.60	+0.24	
169'4	4.34	4.92	4.55	+0.37	
213'4	4.23	5.03	4.50	+0.53	
2+57					
262'4	4.12	5.14	4.45	+0.69	
227'4	4.31	4.95	4.55	+0.40	
199'4	4.19	5.07	4.65	+0.42	
169'4	4.34	4.92	4.65	+0.27	

~ 2+57 ~

139' L	4.22	5.04	4.65	+0.39
111' L	4.50	4.76	4.75	+0.01
86' L	4.72	4.47	4.75	-0.28
61' L	4.56	4.70	4.76	-0.05
33' L	4.86	4.40	4.70	-0.30

~ 2+71.5 ~

39' R	4.79	4.47	4.15	+0.32
89' R	4.72	4.54	4.08	+0.46
139' R	4.90	4.36	4.00	+0.36

~ 3+01.5 ~

139' R	4.83	4.43	4.10	+0.33
89' R	5.04	4.22	4.18	+0.04
39' R	4.84	4.42	4.25	+0.17

~ 3+07 ~

33' L	4.91	4.35	4.67	-0.32
61' L	4.87	4.39	4.67	-0.28
86' L	4.80	4.46	4.57	-0.11
111' L	4.56	4.70	4.67	+0.03
139' L	4.64	4.62	4.57	+0.05
169' L	4.64	4.62	4.47	+0.15
199' L	4.49	4.77	4.57	+0.20
227' L	4.59	4.72	4.50	+0.22
262' L	4.30	4.96	4.40	+0.56

~ 3+15.5 ~

33' R	4.23	5.03	4.10	+0.93
-------	------	------	------	-------

π
9.26

 $\sim 3+295 \sim$

33R

4.90 4.36 4.15 +0.21

89R

5.07 4.19 4.07 +0.12

139R

5.11 4.15 4.00 +0.15

 $\sim 3+545 \sim$

139R

5.45 3.81 3.90 -0.09

89R

5.17 4.09 3.97 +0.12

39R

5.00 4.26 4.05 +0.21

 $\sim 3+57 \sim$

33H

4.95 4.31 4.65 -0.34

61H

5.09 4.17 4.60 -0.43

86H

5.02 4.24 4.50 -0.26

111H

4.93 4.33 4.60 -0.27

139H

4.90 4.36 4.50 -0.14

169H

4.90 4.36 4.40 -0.04

199H

4.82 4.44 4.50 -0.06

237H

4.66 4.60 4.45 +0.15

262H

4.62 4.64 4.35 +0.29

 $\sim 3+7774 \sim$

316.67H

4.66 5.20 4.25 +0.95

266.67H

4.63 4.63 4.30 +0.33

216.67H

4.80 4.46 4.35 +0.11

168H

5.01 4.25 4.40 -0.15

108H

5.07 4.19 4.45 -0.26

54H

5.24 4.02 4.50 -0.48

~34813~

435'R

5.04 4.22 4.15 +0.07

935'R

5.09 4.17 4.07 +0.10

1435'R

5.54 3.72 4.00 -0.28

~470783~

8878'4

5.24 4.02 4.55 -0.53

145.5'4

5.13 4.13 4.35 -0.22

194.17'4

4.99 4.27 4.40 -0.13

244.17'4

4.66 4.60 4.34 +0.26

294.17'4

4.18 5.08 4.28 +0.80

~472864~

28262'4 = cut

4.16 5.10 4.20 +0.90

27862'4

4.06 5.20 4.30 +0.90

22862'4

4.81 4.45 4.37 +0.08

17862'4

5.06 4.20 4.45 -0.25

~472363~

749'R

5.04 4.22 4.00 +0.22

1249'R

5.19 4.07 3.95 +0.12

1749'R

5.08 4.18 3.90 +0.28

~349069~

46'R

5.08 4.18 3.90 +0.28

87'R

5.15 4.11 3.82 +0.29

128'

5.14 4.12 3.75 +0.37

~471069~

28'R

5.01 4.25 4.00 +0.25

78'R

5.22 4.04 3.90 +0.14

128'R

5.32 3.94 3.80 +0.14

~4+3869~

28'R

528 3.98 3.90 +0.08

78'R

547 3.79 3.85 -0.06

128'R

560 3.66 3.80 -0.14

~4+6369

28'R

541 3.85 3.80 +0.05

78'R

568 3.58 3.72 -0.14

128'R

536 3.90 3.65 +0.25

~4+70.77~

147.14'L

529 3.97 4.35 -0.38

197.14'L

492 4.34 4.30 +0.04

247.14'L

428 4.98 4.25 +0.73

251.14'L = Gutter

428 4.98 4.15 +0.83

~4+8869~

28'R

559 3.67 3.90 -0.23

78'R

584 3.42 3.85 -0.43

128'R

542 3.84 3.80 +0.04

~5+0838~

119.03'L

544 3.82 4.25 -0.43

162.03'L

501 4.25 4.18 +0.07

219.03'L

436 4.90 4.10 +0.80

227.03'L

440

~5+1669~

28'R

576 3.50 3.80 -0.30

78'R

575 3.51 3.75 -0.24

128'R

557 3.69 3.70 -0.01

~ 5446.01 ~

9092' Lt.	5.73	3.53	4.35	-0.82
14092' Lt.	5.11	4.15	4.25	-0.10
19092' Lt.	4.45	4.81	4.15	+0.66
19492	4.47	4.79	4.05	+0.74

~ 5446.69 ~

28'R	5.85	3.41	3.70	-0.29
78'R	5.88	3.38	3.62	-0.24
128'R	5.98	3.28	3.55	-0.27

~ 5476.69 ~

28'R	5.72	3.54	3.80	-0.26
78'R	6.06	3.20	3.70	-0.50
128'R	5.95	3.31	3.60	-0.29

~ 5488.4 ~

5944' Lt.	5.75	3.51	4.25	-0.74
10944' Lt.	5.28	3.98	4.18	-0.20
15944' Lt.	4.56	4.70	4.10	+0.60
16344' Lt.	4.53	4.73	4.00	+0.73

~ 6401.7 = Valley Gutter

1493' Lt.	4.68	4.58	4.00	+0.58
993' Lt.	5.45	3.81	4.08	-0.27
493' Lt.	5.72	3.54	4.15	-0.61

~ 6404.69 ~

28'R	5.68	3.58	3.70	-0.12
78'R	5.94	3.32	3.65	-0.33
128'R	6.06	3.20	3.60	-0.40

$\frac{x}{2.26}$
~~612969~~

28'R	5.88	3.38	3.60	-0.22
78'R	6.40	2.86	3.52	-0.66
128'R	6.04	3.22	3.45	-0.23

Valley Gutter

4+28.69=24'R	4' from 864	5.23	4.03	3.85	4.18	
5+02.69=24'R	" " " 6	5.73	3.53	3.75	-0.22	
5+90.69=24'R	" " " 5	5.86	3.40	3.65	-0.25	
6+	=24'R	" " 4	6.30	2.96	3.55	-0.59
T.P.	6.47	9.47	6.26	3.00	61378 = 8 P.P. Station	
chk. starting B.M.	2.01	7.46	Page 5			

Sept. 23, 1946 Riverlawn Const. Grades
 Hendricks for Grounds
 Becker
 Greer

Station	+ H.L.	-	Elev. 3 Stakes	Grade Elev.	TOP OF HUB 5/16" AT 50" 3.214
	461	8.05			
-6+60.40-					
42.01 RT		490	3.15	3.70	F0.55
93.01 RT		481	3.24	3.60	F0.34
143.01 RT		468	3.37	3.50	F0.13
6+98.38					
58.88 RT		490	3.15	3.60	F0.45
108.88 RT		489	3.16	3.55	F0.39
158.88 RT		497	3.08	3.50	F0.42
-71.28.48-					
70.66 RT		506	2.99	3.45	F0.46
71.58.58					
48.17 RT		491	3.14	3.60	F0.46
71.94.58					
4 RT		469	3.36	3.70	F0.34

Const. Grades for Grounds

Contd.

Station	+ H.I	-	Elev. Stakes	Elev. Gr.
	8.05			
-8+157-				
36 Lt	4.47	3.58	G 3.65	F 0.07
75 Lt	4.08	3.97	3.70	C 0.27
95 Lt	4.34	3.71	3.75	F 0.04
119 Lt	4.14	3.91	3.75	C 0.16
139 Lt	3.90	4.15	3.80	C 0.35
171 Lt	3.84	4.21	3.84	C 0.37
186 Lt	3.80	4.25	3.90	C 0.35
214 Lt	3.77	4.28	3.90	C 0.38
8+70.7				
36 Lt	4.60	3.45	3.53	F 0.08
103.5 Lt	4.41	3.61	3.60	C 0.01
171 Lt	4.40	3.65	3.68	F 0.03
186 Lt	4.33	3.72	3.75	F 0.03
214 Lt	4.25	3.80	3.80	C 0.00
8+85.7				
36 Lt	4.56	3.49	3.50	F 0.01
86 Lt	4.53	3.52	3.50	C 0.02
136 Lt	4.47	3.58	3.50	C 0.08

Const Grades for Grounds
Cont'd.

Station	H.I.		Elev	Elev Gr	
	8.05				
8+94.58					
4 RT		4.61	3.44	3.40	0.04
32 RT		3.63	4.42	3.40	1.02
9+13.7					
36 LT		5.38	2.67	3.50	0.83
86 LT		5.08	2.97	3.50	0.53
136 LT		4.77	3.28	3.50	0.22
9+15.7					
186 LT		4.48	3.57	3.60	0.03
				3.70	
214 LT		4.71	3.24	3.70	0.36
			3.24	3.70	
		4.77	3.28	3.28	

Sept 25-46
 Hendricks
 Becker
 Greer

Restake Const. Grades
 Riverland

Station	+	#1	-	Elev	BM Top of Right 7.46	Fleet & Mallet
	1.94	9.40				
0+00				Stakes	Elev	Grade
29 Rt			450	4.90	4.55	C 0.35
☒			5.09	4.31	4.57	F 0.26
21 Lt			488	4.52	4.59	F 0.07
71 Lt			532	4.08	4.63	F 0.55
111 Lt			468	4.72	4.65	C 0.07
0+48						
29 Rt			431	5.09	4.60	C 0.49
☒			4.91	4.49	4.62	F 0.13
21 Lt			487	4.53	4.63	F 0.10
71 Lt			481	4.59	4.65	F 0.06
111 Lt			472	4.68	4.57	C 0.11
0+98						
29 Rt			424	5.16	4.38	C 0.78
☒			5.19	4.21	4.48	F 0.27
33 Lt			478	4.62	4.60	C 0.02
61 Lt			478	4.62	4.60	C 0.02
111 Lt			471	4.69	4.60	C 0.09

Restake Const. Grades
Riverlawn

Station +	HI -	Elev stakes	Elev Grade	
- 1430 -	940			
111 L4		4.41	4.99	4.60 C.O.39
61 L4		4.67	4.73	4.65 C.O.08
33 L1		4.95	4.45	4.63 F.O.18
☐		4.66	4.74	4.73 C.O.01
29 Rt.		124	7.46	7.46
		CK. B.M.	C	

Walker River-Lynn - Rough Grades

Hendricks

Becker Fleet St. from Congress

Greer

9-20-46 to Moffet Street.

Sketch P. 20

+B.M. on

Fleet & Congress

Stations 2.60 10.06 7.46 Ch. Elev.

Lt. 0+00

Cut & Fill

B.C. Ch. on Congress

4.93 5.13 4.98 +0.15

①

4.79 5.27 5.00 +0.27

②

4.86 5.20 5.03 +0.17

③

4.83 5.23 5.05 +0.18

Ch. E.C.

④ = 0+29

4.78 5.28 5.08 +0.20

0+50

Rt.

B.C. on Congress

4.68 5.38 5.20 +0.18

①

4.63 5.43 5.18 +0.25

②

4.67 5.39 5.17 +0.22

③

4.70 5.36 5.19 +0.17

④ = E.C. = 0+29

4.58 5.48 5.21 +0.27

~0+50~

Lt.

4.74 5.32 5.13 +0.19

Rt.

4.40 5.66 5.25 +0.41

~0+75~

Lt.

4.88 5.18 5.18 00

Rt.

4.50 5.56 5.29 +0.27

~1+00~

Lt.

4.62 5.44 5.24 +0.20

Rt.

4.53 5.53 5.33 +0.20

\bar{x}
10.06

~1725-				
Lt	5.10	4.96	5.29	-0.33
Rt	4.80	5.26	5.38	-0.12
1750				
Lt	4.96	5.10	5.35	-0.25
Rt	4.79	5.27	5.42	-0.15
1775				
Lt	5.08	4.98	5.41	-0.43
Rt	4.84	5.22	5.46	-0.24
~2100 ~				
Lt	5.06	5.00	5.47	-0.47
Rt	4.82	5.24	5.50	-0.26
~2125-				
Lt	5.23	4.83	5.52	-0.69
Rt	5.18	4.88	5.54	-0.66
2146=Bik				
Lt	5.36	4.70	5.57	-0.87
Rt	5.39	4.67	5.57	-0.90
~2174.5-				
Lt	5.47	4.59	5.50	-0.91
Rt	5.35	4.71	5.46	-0.75
~3103=BC. 30'cb R				
Lt=BC	5.93	4.11	5.43	-1.32
Lt ①	5.70	4.36	5.40	-1.04
Lt ②	5.61	4.45	5.37	-0.92

10.06

23

3403 Left Return

Cut & Fills

4③ 5.75 4.31 5.34 -1.03

11② = EC. on Moffet st. 5.77 4.29 5.31 -1.02

3403 R. Return

BC. 5.52 4.54 5.35 -0.81

1 5.74 4.32 5.37 -1.05

2 5.58 4.48 5.40 -0.92

3 5.57 4.49 5.43 -0.94

4 = EC. on Moffet 5.58 4.48 5.45 -0.97

TP. 4.55 8.91 5.70 4.36

Note: Moffet Street on p 24

> Levels Cont p-24

River Lowry - Rough Grades
on Moffet St.

Drawing Misc. # 7357

Sketch P-20

Taken from P-23

8.91

Stations

0+00

INDEXED

Cuts & Fills

Lt

WK

4.06 4.85 5.56

-0.71

Rt

NOV 18 1948

3.90 5.01 5.62

-0.61

0+25.25

Lt

4.30 4.61 5.50

-0.89

Rt

3.97 4.94 5.57

-0.63

0+50.5 = B.C. Ret. on Lt.

Lt

4.42 4.49 5.45

-0.96

Rt

4.00 4.91 5.52

-0.61

0+93.5 = E. of Ret. on Lt.

Rt

4.26 4.65 5.43

-0.78

1+36.5 = E.C. Cb Ret. on Lt.

Lt

4.62 4.29 5.31

-1.02

Rt

4.43 4.48 5.34

-0.86

1+65.82 = 1/2 x 10' from Cb Ret. to B.C.

Lt

4.59 4.32 5.24

-0.92

Rt

4.50 4.41 5.28

-0.87

1+95.15 = B.C. ^{Note:} Curve on Lt. in 5 Parts

Lt.

4.68 4.23 5.17

-0.94

Rt

4.42 4.49 5.22

-0.73

2+26.85 = B.C. 10' Cb R

R

4.70 4.21 5.15

-0.94

Moffet Street
Cont. from P-24

Stations	891				
2+30.34 Rt = EC 10' CR	4.62	4.29	5.10	-0.81	
2+53.36 Rt = 1/2 way from 10' CR to EC on Lt	4.08 4.83	4.83	5.05	-0.22	
2+12.03 Lt	4.80	4.11	5.14	-1.03	
+28.91 Lt	4.82	4.09	5.11	-1.02	
+45.79 Lt	4.63	4.28	5.08	-0.80	
+62.67 Lt	4.65	4.26	5.05	-0.79	
2+79.54 = EC	4.86	4.05	5.01	-0.96	
" Rt	4.92	3.99	5.01	-1.02	
3+00					
Lt	5.10	3.81	4.96	-1.15	
Rt	4.94	3.97	4.96	-0.99	
3+25					
Lt	5.08	3.83	4.91	-1.08	
Rt	5.30	3.61	4.91	-1.30	
3+50					
Lt	5.20	3.71	4.86	-1.15	
Rt	5.30	3.61	4.86	-1.25	
3+75					
Lt	5.16	3.75	4.81	-1.06	
Rt	5.56	3.35	4.81	-1.46	
4+00					
Lt	5.11	3.80	4.76	-0.96	
Rt	5.35	3.56	4.76	-1.20	

Fire Hyd
399 = 1st stake 2+79.54 on Rt.
521
9.20 A
497 = 2+96.5 = FH.
423

Moffet Street

26

Cont. from p. 25

Stations	8.91				
4+25 Lt		5.12	3.79	4.71	-0.92
Rt		5.40	3.51	4.71	-1.20
4+58.89 = B.C.	Note: Curve on Lt = 6 Parts				
Lt		5.47	3.44	4.65	-1.21
Rt		5.53	3.38	4.65	-1.27
4+71.00					
Lt		5.47	3.44	4.62	-1.18
Rt		5.57	3.34	4.62	-1.23
4+83.11					
Lt		5.40	3.51	4.59	-1.09
R		5.77	3.14	4.59	-1.45
4+95.22					
Lt		5.47	3.44	4.56	-1.12
Rt		5.79	3.12	4.55	-1.43
~5+07.33~					
Lt		5.37	3.54	4.53	-0.99
Rt		5.66	3.25	4.52	-1.27
~5+14.18 = P.R.C. 15' C.B. R on Rt		5.51	3.40	4.50	-1.10
Return on Rt		5.44	3.47	4.52	-1.05
E.C. Ret on Rt		5.49	3.42	4.54	-1.12
693' West of E.C. = End of Curve		5.39	3.52	4.55	-1.03
5+19.44 on Lt		5.50	3.41	4.50	-1.09
5+31.55 = E.C.					
Lt		5.63	3.28	4.48	-1.20

Mottet Street

Corit. from P-26

Stations

8.91

~5+4243~

Lt 5.36 3.55 4.46 -0.91

Rt - E Roadway to West

~5+7443~ 4.97 3.94

Lt 4.97 3.94 4.43 -0.49

Rt 5' West of BC 15'cb Return 4.97 3.94 4.42 -0.48

Rt BC Ret 4.97 3.94 4.40 -0.46

1/2 Way cb Return 4.97 3.94 4.38 -0.44

~5+8943~ - EC 15'cb Ret on Rt 4.78 4.13 4.41 -0.28

Lt 4.84 4.07 4.37 -0.30

6+1443 - BC 30'cb R on Rt 4.48 4.43 4.30 +0.13

① 4.56 4.35 4.28 +0.07

② } cb Ret on Rt 4.58 4.33 4.26 +0.07

③ } 4.61 4.30 4.24 +0.06

④ - EC 30'cb R on Rt 4.62 4.29 4.21 +0.08

6+3443 - BC 10'cb Ret on Lt 4.67 4.24 4.34 -0.10

① 4.86 4.05 4.34 -0.29

② - EC 10'cb Ret on Lt 4.67 4.24 4.34 -0.10

chk starting BIM P-21 1.44

7.47
7.46
0.01

Sept. 27, 1946

State Out for Bldgs

Hendricks
Becker
Greer

Osborne
Hardin
Norrell

8, 9, 10, & 11

Riverlawn Housing Proj

Station	+	H.I.	-	State Elev	Floor Elev.	Top. First Floor Elev. & Cont.
	2.17	9.63				7.46

Note: All Hubs set on 10' offset.

Bldg. 11	INDEXED	483	480	7.30	F 2.50
----------	----------------	-----	-----	------	--------

INDEXED
WK
NOV 18 1948

Bldg. 10		493	470	7.20	F 2.50
----------	--	-----	-----	------	--------

Bldg. 9		503	4.60	7.10	F 2.50
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Bldg. 8		5.13	4.50	7.00	F 2.50
---------	--	------	------	------	--------

2.17

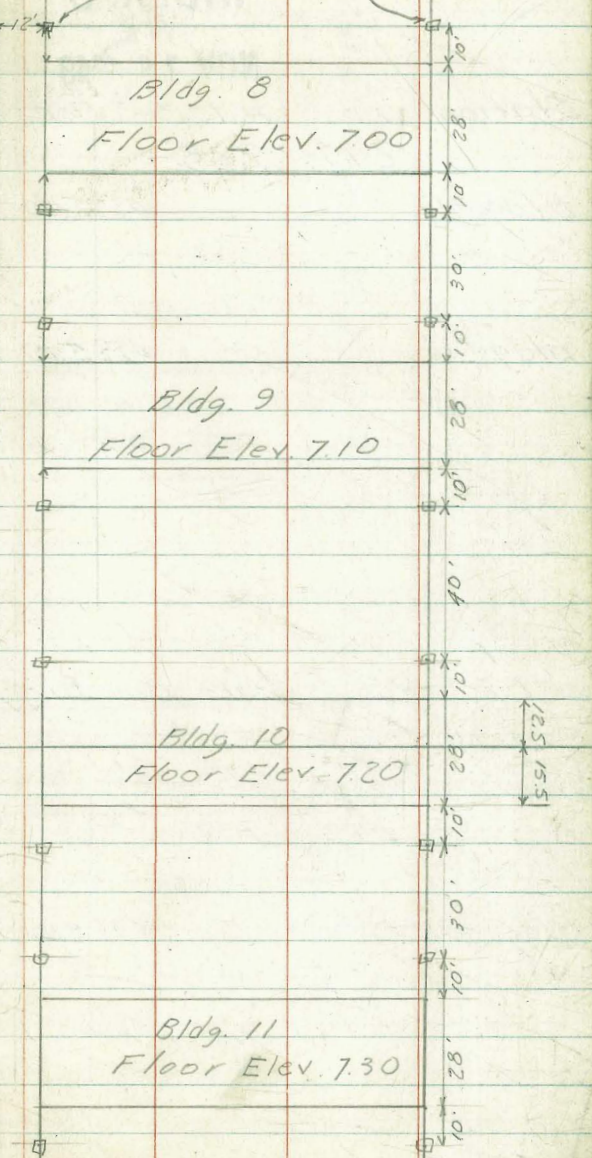
7.46
CK B.M.

All Grade Stakes Set 2.5 below Floor Elev

Floor St

13 27 12

E. Moffat St



Sept. 27, 1946 State Out for Bldgs. 16 & 17
 Hendricks Osborn
 Becker Hardin
 Greer Worrell
 Riverlawn Housing Project

INDEXED

WK

NOV. 1st 1948

Top Fire Ht
 Fleet & Comp

Station	H.I.	Elev	State	Floor	Elev	7.46
---------	------	------	-------	-------	------	------

Bldg #17	2.17	9.63	463	5.00	7.50	F 2.50
----------	------	------	-----	------	------	--------

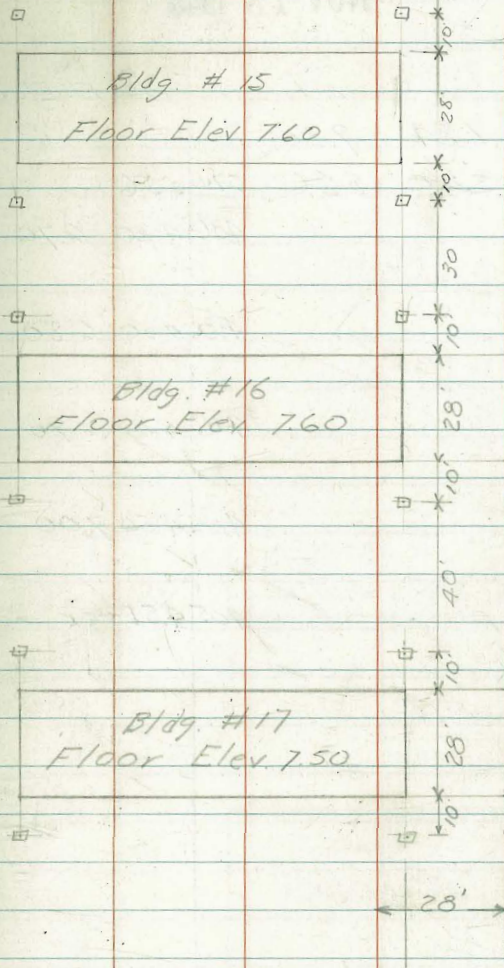
Bldg #16			453	5.10	7.60	F 2.50
			217			7.46 CL RM.

Oct 8, 1946 State Out Bldg #15

Station	H.I.	Elev	State	Floor	Elev	7.46
---------	------	------	-------	-------	------	------

Bldg #15	1.86	9.32	422	5.10	7.60	
			186		7.46	↔ 7.46

to Moffet St

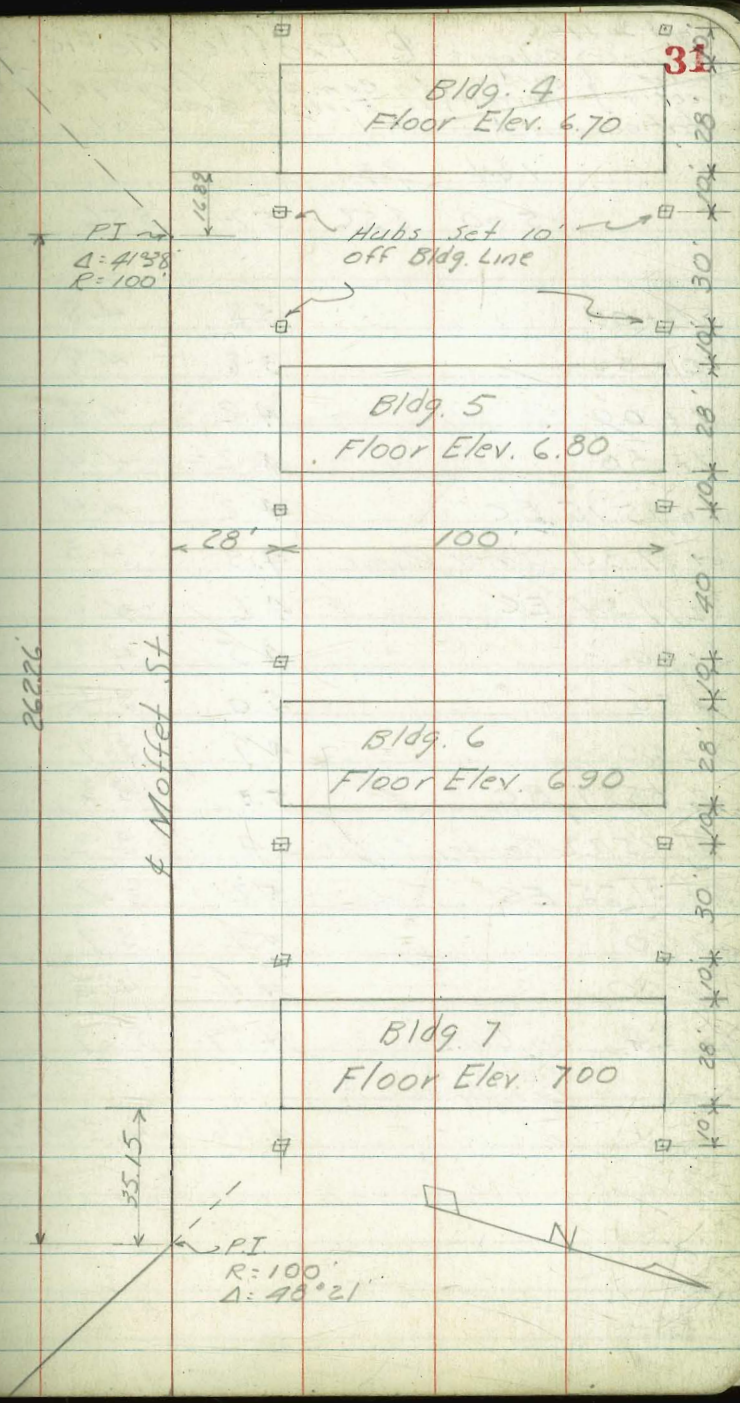


Sept 30, 1946 Stake out Bldgs. 4, 5, 6, & 7
 Hendricks Osberne
 Becker Hardin
 Greer Worrell

INDEXED

WK
 NOV 18 1948

Station	+	H.I.	-	Elev Stake	Fl. Elev	Top Fin. Ht Feet & Comp.
	1.84	9.30				7.46
	5.00	8.56	574	3.56		
Bldg 4			436	4.20	6.70	F 2.50
Bldg 5			426	4.30	6.80	F 2.50
Bldg 6			416	4.40	6.90	F 2.50
Bldg 7			406	4.50	7.00	F 2.50
			405	4.51	← CK →	4.50



31

Sept. 30, 1946

Hendricks }
Becker }
Greer }Osborne }
Hordin }
Worrell }E Profile Moffet St.
To compute Yardage needed
to Finish grade

Station	+	H.I.	Elev	Top Fire Height Fleet & Comps
	184	9.30		7.46
	5.00	8.56	5.74	3.56
0+00			3.8	4.8
0+50			3.8	4.8
1+00			4.2	4.4
1+50			4.2	4.4
1+95.15	BC		4.2	4.4
2+37.34	Center Curve		4.3	4.3
2+79.54	EC		4.6	4.0
3+00			4.5	4.1
3+50			5.0	3.6
4+00			4.9	3.7
4+58.89	BC		5.3	3.3
4+95.22	Center Curve		5.4	3.2
5+31.55	EC		5.2	3.4
5+60			4.9	3.7
6+00			4.4	4.2
6+24	on Curb Moffet & Congress		4.87	3.69
			4.06	4.50 ^{Grade Stake 5/11/7} 4.50

For sketch See page 20
of this Book

Sept 30, 1946. Profile Fleet St
 Hendricks Osborne to Compute yardage Needed
 Becker Hardin to Finish Grade
 Greer Worrell

Station	+	H.L.	-	Elev.	B.M.
	242	9.88			7.46
					Top Fire Hydt Fleet & Congress
0+00	Back Edge of Curb	4.77		5.11	
0+50		4.6		5.3	
1+00		4.5		5.4	
1+50		4.6		5.3	
2+00		5.0		4.9	
2+46		5.1		4.8	
3+00		5.4		4.5	
3+46	= ϕ Moffet & Fleet	5.5		4.4	
		2.42		7.46	7.46

For sketch See page 20
 off this Book

INDEXED

WK

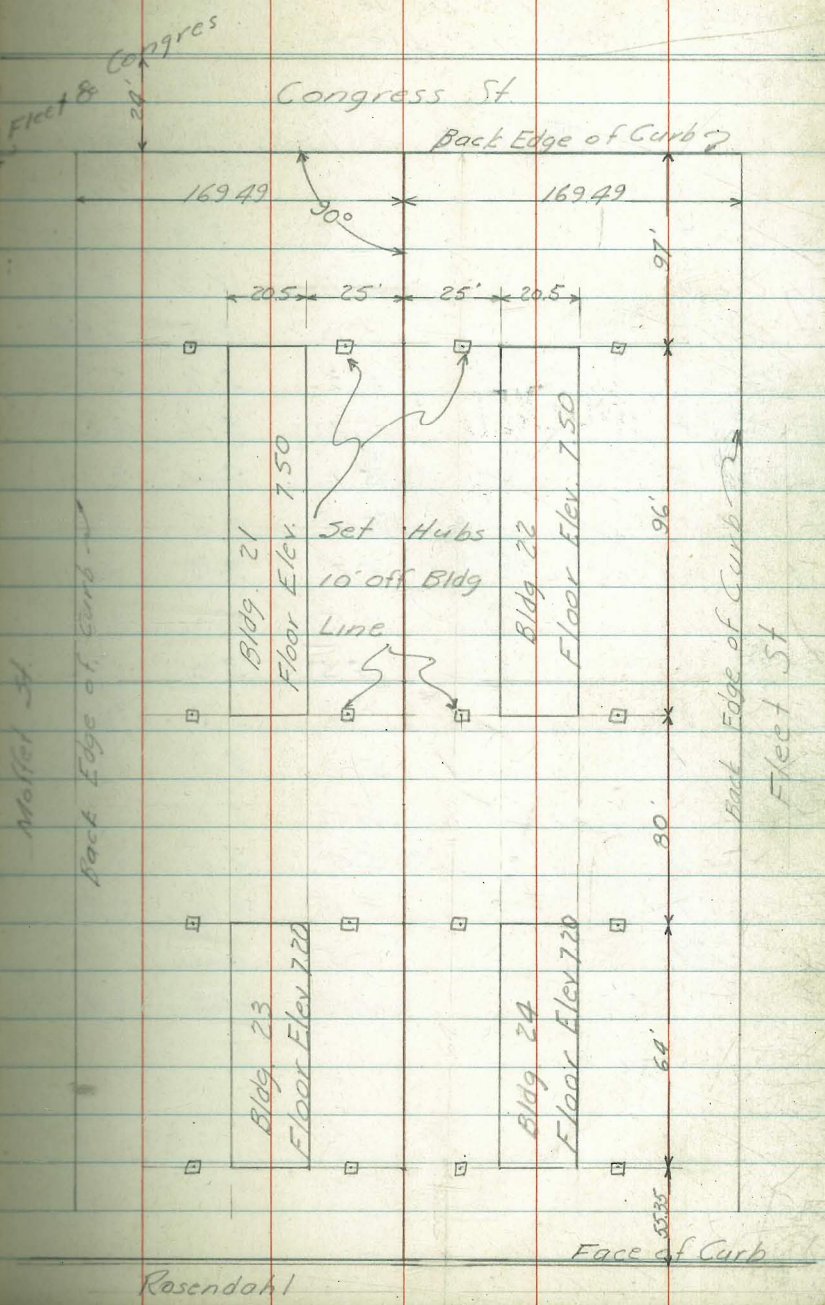
NOV 18 1948

Oct 2, 1946
 Hendricks
 Osborne
 Hardin
 Greer

State Out Bldgs 21, 22,
 23, & 24 Riverlawn
 Housing Project

Station	+ -	H.I.	-	Elev Stake	Floor Elev	BM Top Fire Hdr
		2.32		9.78		7.46
Bldg 21	No. Side			4.78	5.00	7.50 F. 2.50
	So. Side			5.28	4.50	7.50 F. 3.00
Bldg 22				4.78	5.00	7.50 F. 2.50
				5.28	4.50	7.50 F. 3.00
Bldg 23				5.58	4.20	7.20 F. 3.00
Bldg 24				5.58	4.20	7.20 F. 3.00
		2.32		7.46	CF	→ 7.46

INDEXED
 WK
 NOV 18 1948



Oct 14, 1946 Grades to Compute additional
Walker Yardage needed For Riverlawn
Hendricks Housing Project
Becker
Greer

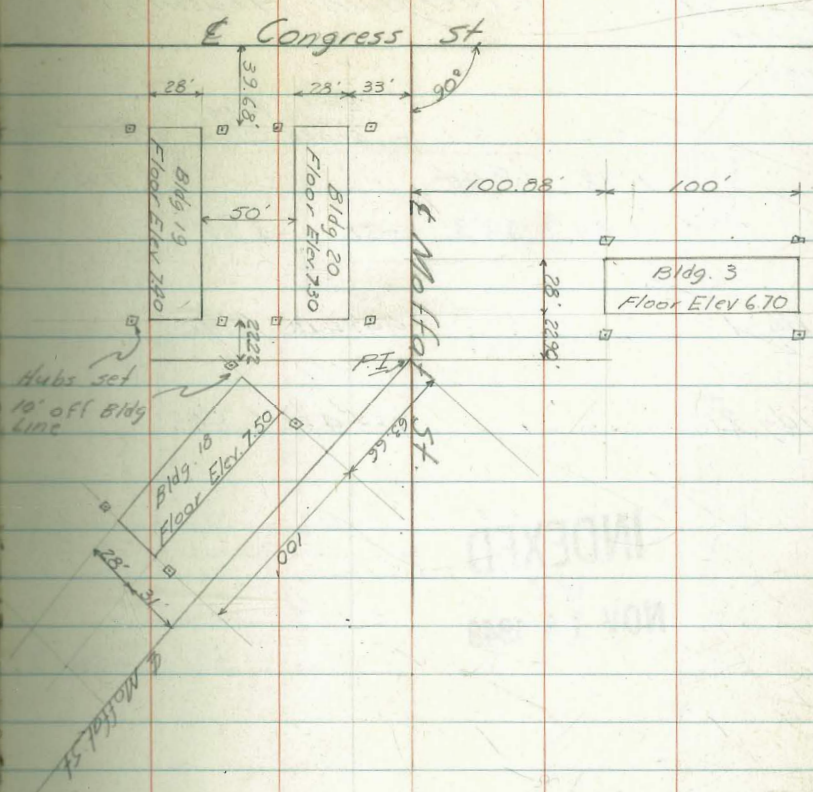
	4.23	8.53		4.30	Grade Stake 2.5 Below Floor Elev. Bldg. 5
			Ground Elev	(Plan) Ground Elev	
SE Cor 7		4.6	3.9	4.00	
SW Cor 7		4.7	3.8	3.90	Bldg. 4
SE Cor 6		5.0	3.5	3.90	
SW Cor 6		5.3	3.2	3.80	
SE Cor 5		5.1	3.4	3.80	
SW Cor 5		5.1	3.4	3.70	Bldg. 5
SE Cor 4		5.0	3.5	3.70	
SW Cor 4		5.2	3.3	3.60	
NW Cor 4		5.5	3.0	3.50	
NE Cor 4		5.5	3.0	3.50	Bldg. 6
NW Cor 5		5.4	3.1	3.60	
NE Cor 5		5.4	3.1	3.60	
NW Cor 6		5.4	3.1	3.70	
NE Cor 6		5.0	3.5	3.80	Bldg. 7
NW Cor 7		5.1	3.4	3.80	
NE Cor 7		4.5	4.0	3.80	
		4.33	4.20	4.20	ck Grade Stake Bldg. 4.



Oct. 18, 1946 Stakeout Bldgs 18, 19, 20, &
 3 Riverlawn Housing Proj.
 Walter
 Hendricks
 Becker
 Greer

	H.I.	Elev Grade Stake	F.I. Elev	B.M. Top of Fict & Comp
1.79	9.25		7.46	

Bldg 18	INDEXED WK	425.500	7.50
Bldg 19	NOV 18 1948	435.490	7.40
Bldg 20		445.480	7.30
Bldg 3		5.05	4.20 6.70



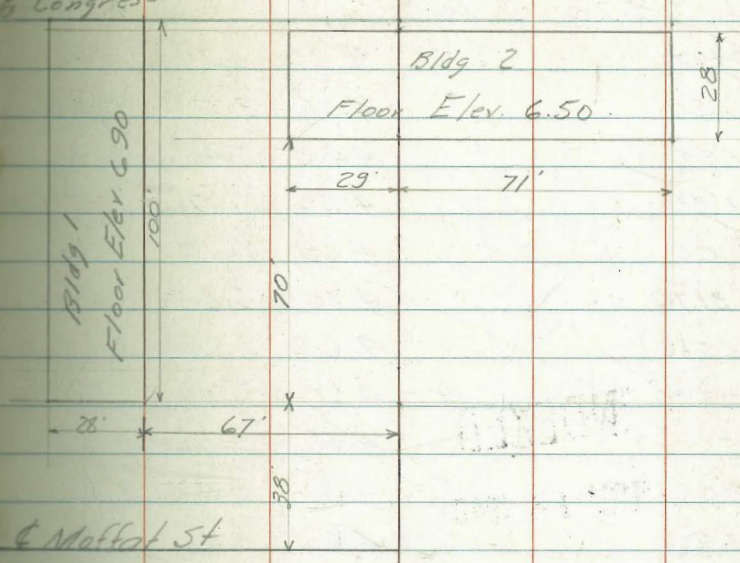
Oct 18, 1946
Walker
Hendricks
Becker
Greer

Stake out Bldgs. 1 & 2
Riverlawn Housing Proj

	H.I.	Elev. Grade Stake	Floor Elev	BM Floor Congress
1.98.	944			7.46
4.90	883	5.51	3.93	

Bldg 1	443	4.40	6.90
Bldg 2	483	4.00	6.50

INDEXED
WK
NOV 18 1948



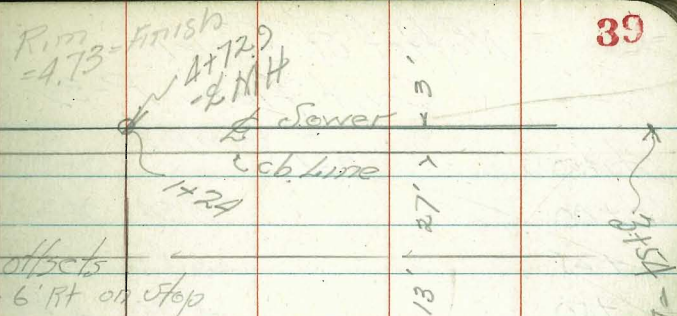
E Congress St.

Oct 24, 1946 Grades for Finish Grading
Walker
Hendricks. Riverlawn Housing Project
Becker
Greer

Station	+ H.I.	-	Elev.	Grade
	3.70	7.90		4.20 ← Grade Stake Bldg # 3
0+00			4.20	3.70
+50			4.31	3.59
1+00			4.42	3.48
+50			4.53	3.37
2+00			4.64	3.26
2+31.70			4.70	3.20
2+65.86			4.65	3.25
3+00			4.61	3.29
+50			4.55	3.35
4+00			4.48	3.42
+50			4.42	3.48
5+00			4.35	3.55
+50			4.29	3.61
6+00			4.22	3.68
+44.36			4.15	3.75
7+00			4.10	3.80

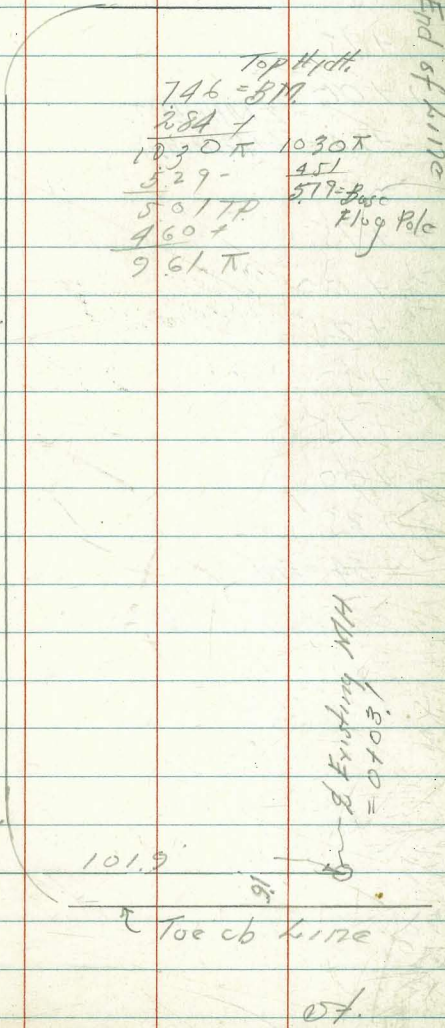


Walker
Handricks
Gieck
Becker
11-8-46
Riverbawn Housing Project
Grades - Sewer Construction
on Congress, Fleet, & Moffet Sts



Station	Elev. 1030	Elev. 1076	Elev. 1076	Elev. 1076	Cuts	offsets
8 East MH on Congress St = 0+03.1	377	6.53	-0.46	-0.40	+593	6' RT on step
+25	455	5.75	-0.31	-0.31	+606	2 6' RT
+50	469	5.61	-0.21	-0.21	+582	6' RT
+75	501	5.29	-0.11	-0.11	+540	6' RT
1+05 = $\Delta 90^\circ$ RT MH	503	5.27	0.00	0.00	+527	10' L
+25	514	5.16	0.07	0.07	+509	6' RT
+50	499	5.31	0.16	0.16	+515	6' RT
+75	509	5.21	0.25	0.25	+496	6' RT
2+00	492	5.38	0.34	0.34	+504	6' RT
+25	504	5.26	0.43	0.43	+483	6' RT
+50	520	5.10	0.52	0.52	+458	"
+75	463	4.98	0.61	0.61	+477	"
3+00	459	5.02	0.70	0.70	+432	"
+25	490	4.71	0.79	0.79	+392	"
+50	507	4.54	0.87	0.87	+367	"
3+75	505	4.56	0.96	0.96	+360	"
4+00	528	4.33	1.05	1.05	+328	"
+25	524	4.37	1.14	1.14	+323	"
+50	498	4.63	1.22	1.22	+341	"
4+72.9 4+77.5 MH	489	4.72	1.30	1.30	+342	"
		4.30 = Rim				
		0.42 = cut to Rim				

INDEXED
WK
NOV 18 1948



Cont. Page 40

Congress

07.

Moffet of Sewer
Cont. from P-39

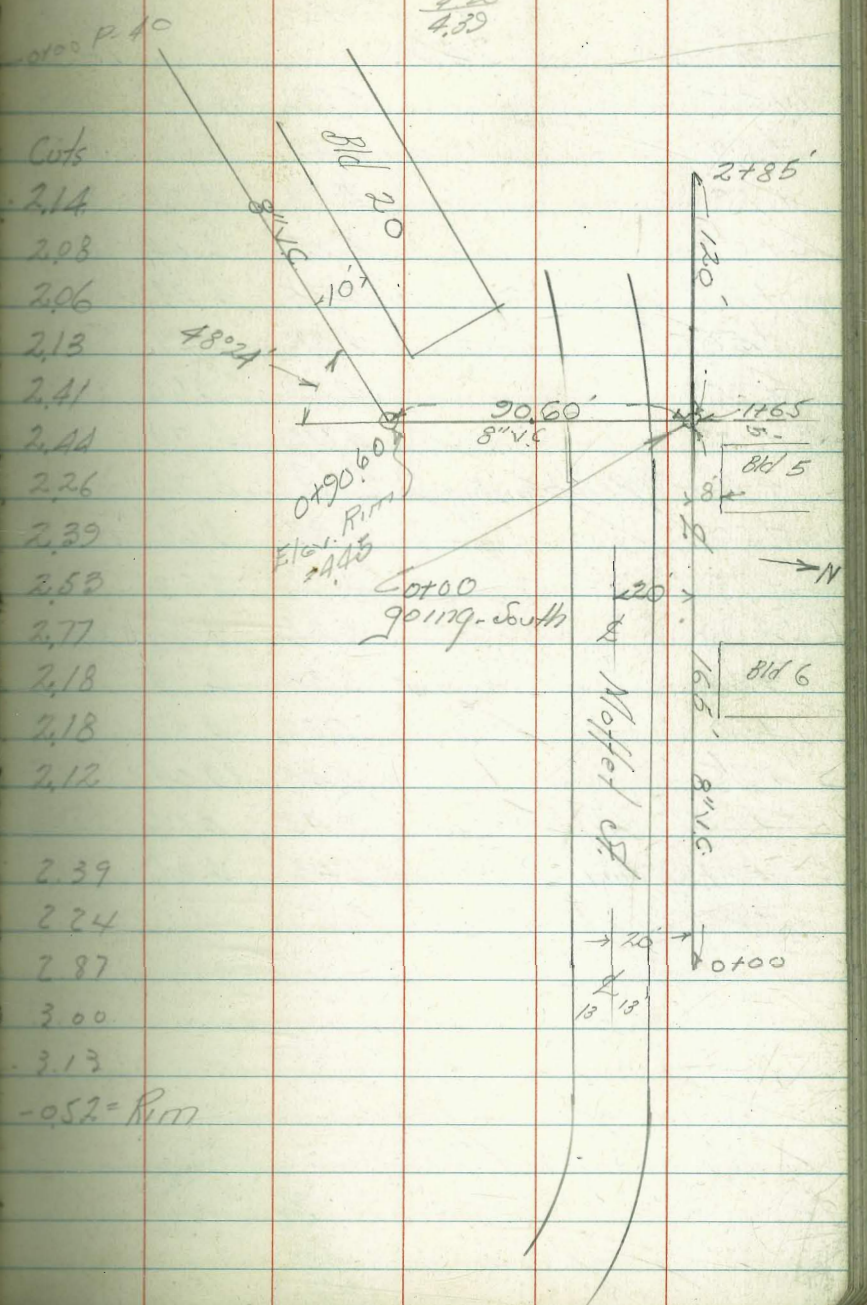
Station	π from P-39 26		Elev. Flowline	Cuts	Offsets
0+00		5.34	4.27	1.73	2.54 6' Lt.
+25		5.23	4.38	1.64	2.74 "
+50		5.20	4.41	1.56	2.85 "
+75		5.24	4.37	1.47	2.90 "
1+00		5.10	4.51	1.38	3.13 "
+24 = 2 NH = DOT. (4+729 P-39)		4.89	4.72	1.30	3.42 "
+50		4.82	4.79	1.39	3.40 6' Rt.
+75		4.76	4.85	1.48	3.37 "
2+00		4.90	4.71	1.58	3.15 "
+25		4.89	4.72	1.65	3.07 "
+50		5.07	4.54	1.74	2.80 "
+75		5.31	4.30	1.82	2.48 "
3+00		5.01	4.60	1.91	2.69 "
+25		5.14	4.47	2.00	2.47 "
+54 = End		5.25	4.36	2.10	2.26 "
chk starting B.M.		246	7.15		
			7.46		
			0.01		

Walker
Hendricks
Becker
Green
11-18-46
River Basin Sewer Construction
Along SLY End Bldg. 4, 5, 6

Station	Elev	Flow Line	Cuts
0+00 going West	4.77	3.82	1.68
+25	4.92	3.67	1.59
+50	5.03	3.56	1.50
+75	5.05	3.54	1.41
1+00	4.86	3.73	1.32
+25	4.91	3.68	1.24
+45	5.16	3.43	1.17
+65=M.H.	5.10	3.49	1.10
+90	4.87	3.72	1.19
2+15	4.54	4.05	1.28
+40	5.05	3.54	1.36
+65=	4.96	3.63	1.45
+85=End	4.95	3.64	1.52
TP 5.01 8.83	4.77	3.82	
0+00 going South	5.24	3.49	1.10
+25	5.57	3.26	1.02
+46.24	5.01	3.82	0.95
+67.48	4.95	3.88	0.88
+90.60=M.H.	4.90	3.99	0.80
+90.6 Rim Elev	4.45		
TP 5.37 9.90	4.30	4.59	on ch
(Chk S.M. Fire Hyd)	2.44	7.46	✓

Cont P-42

8.59
4.20
4.39



River Lower Sewer

Station	π from P 43 249		Feet Flow Line	Cuts
1+25	5.52	3.97	0.68	3.29
+50	5.40	4.09	0.59	3.50
+75	5.28	4.21	0.50	3.71
2+00	5.05	4.44	0.41	4.03
+25	5.15	4.34	0.32	4.02
+50	4.88	4.61	0.23	4.38
+75	4.89	4.60	0.14	4.46
3+00	4.79	4.70	0.05	4.65
+162 = MH. Int. Existing Sewer	4.73	4.76	0.00	4.76
+50	4.83	4.66	0.25	4.41
+75	4.76	4.53	0.43	4.10
4+00	5.21	4.28	0.61	3.67
+25	5.30	4.19	0.79	3.40
+50	5.32	4.17	0.97	3.20
+75	5.45	4.04	1.15	2.89
5+00	5.43	4.06	1.35	2.71
+212 = End	5.43	4.06	1.50	2.56
T.P.				

River Basin Sewer
to Serve Bld 1

43

Station	π 9.00			Elev Flow Line	Cuts
\pm First MH -0+00		8.64	0.36	0.35	0.01 chk Flow
+25		4.76	4.24	0.47	3.77
+50		4.87	4.13	0.60	3.53
+69.6 = Δ 21° 38'		2.95	6.05	0.70	5.35
1+00		2.95	6.05	0.85	5.20
+25		2.86	6.14	0.97	5.17
+50		2.90	6.10	1.10	5.00
1+62.6		3.07	5.23	1.20	4.73
chk Nail 0+00-P-47		4.94	4.06		

2.94	π 10.40			7.46	2nd up from flow & center
chk Flow Line MH Note N-Side is Higher		11.44	-1.04		
			-0.93		
2.05	2.51			7.46	Above BM
		5.55	3.96		
		4.96	4.55		
4.26	π 2.49			4.53	TP cb P-21
TP 4.30	9.00	4.79	4.70		
chk Flow Above MH	0+00	8.64	0.36		

Fr

No

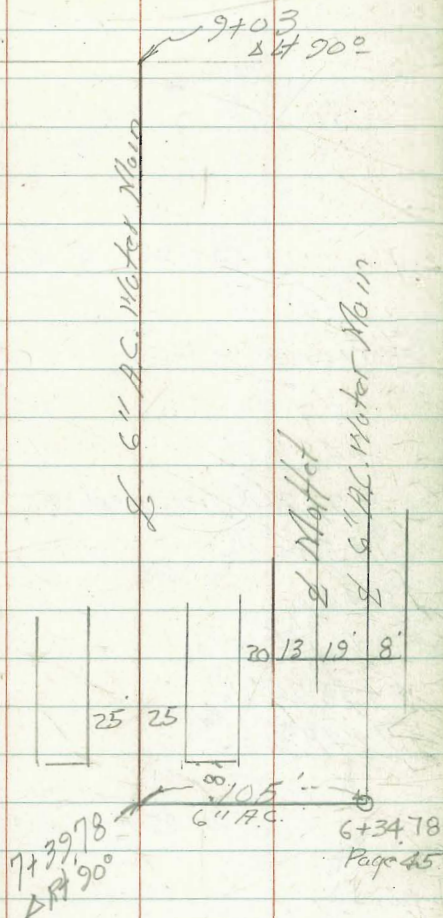
RECHNUNG
VON

9.69 from P-45

				Elev Trench	
2	9+03 = Bk	4.84	4.85	1.60	3.25
	+55	2.81	6.88	1.42	5.46
	10+20	2.77	6.92	1.20	5.7
	+43 = Bk	2.77	6.92	1.10	5.8
	11+14	4.27	5.42	1.31	4.1
	11+80.18 = 5' South of Congress	4.82	4.87	1.50	3.4
	BM Top Fire Hyd	2.25	7.44		
	Fleet + Congress		7.46		
			0.02		

Reset 9+03

				BM 5'
	4.74	2.53	4.79	
9+03		5.11	4.42	1.60
9+55 chk		2.66	6.87	4.28
			6.87	
			0.01	



Walker
H

River Lower - Water Main Grades

Mis. Drawing No 7358

483 8.50

367

BM 244
1+48.39
P-45

Moffet St

522

55'

Congress

5'

Stations

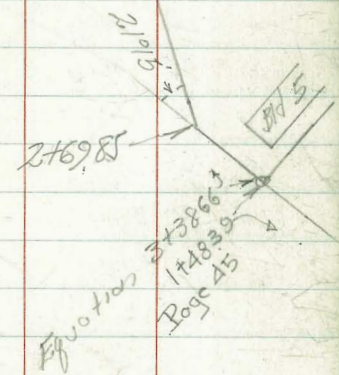
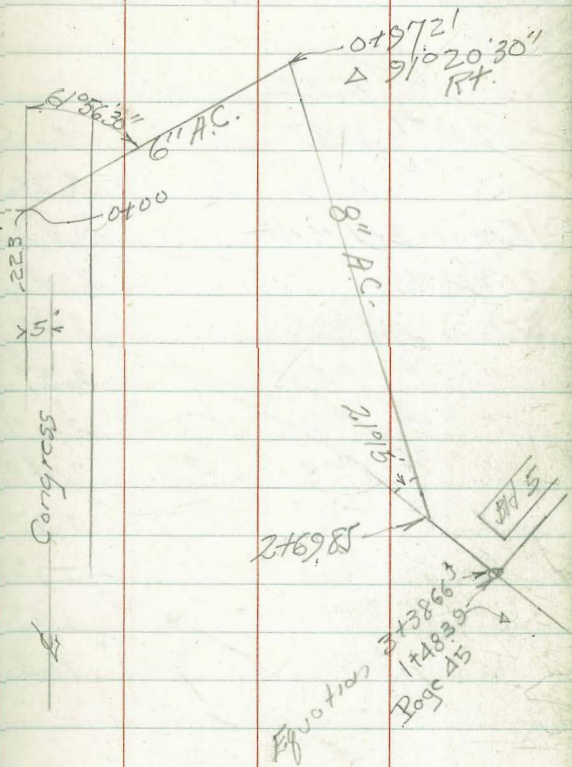
Files
Trans Cuts

0+00	4.46	4.04	0.8	3.24
+48.6	4.66	3.84	0.5	3.34
+97.2 / Δ 91°20'30" Rt.	4.91	3.59	0.2	3.4
1+50	5.24	3.26	0.4	2.8
2+00	4.94	3.56	0.5	2.9
+62.85 Δ	5.20	3.30	1.0	2.3
3+38.66 } = 1+48.39 } Equations	4.83	3.67	1.1	2.6
(Chk Sinar 2+85 P-41.)	4.88	3.62		
		3.64		
		0.02		

For
This size
See P-45

3+2.617

Existing
Water Main



Walker
Hendricks
Becker
Greer

River Lower Housing Project
Check Floor Elevations
of Buildings

	4.22	10.01		5.79	5.79
TP #1	4.37	9.28	5.10	4.91	
TP #11	4.99	9.01	5.26	4.02	
Floor Bld #19			2.37	6.64	
SVL Stake			1.04	4.97	
Floor Bld #20			2.42	6.59	0.71
" " #5			2.97	6.04	0.76
" " #4			2.07	5.94	0.76
" " #18			2.42	6.59	0.91
" " #15			1.97	7.04	0.56
" " #16			2.02	6.99	0.61
" " #17			1.97	7.04	0.46
" " #14			1.64	7.37	

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WIK
NOV 18 1948

Walker
Hendricks
Becker
Greer
12-5-46
Grades for Conc. Stubs at
Bottom Steps of Bldg.
117 River Lawn

X
9.38

El. Stakes El. Grade

			El.	El. Grade					
	9.01-T from P 48		4.48	4.48	SW 15			4.78	4.60 4.60
NW Bld #19		4.66	4.35	4.35	SE 15			4.63	4.75 4.75
E "		4.71	4.30	4.30	SW 13			4.63	4.75 4.75
SW "		4.76	4.25	4.25	SE 13			4.78	4.60 4.60
SE #20		4.86	4.15	4.15	TP	5.05	9.65	4.78	4.60
E #20		4.76	4.25	4.25	NW 14			4.85	4.80 4.80
NE #20		4.66	4.35	4.35	SW 14			4.70	4.95 4.95
SE #18		4.66	4.35	4.35	TP	6.08	10.68	5.05	4.60
NE #18		4.46	4.55	4.55	NE 14			5.98	4.70 4.70
					SE 14			5.78	4.90 4.90
	2.14	9.60	7.46	7.46	SW 12			6.03	4.65 4.65
SE #17		5.05	4.55	4.55	NW 12			6.13	4.55 4.55
SW #17		5.15	4.45	4.45	TP	6.00	10.60	6.08	4.60
NE #19		5.15	4.45	4.45	SE 12			5.90	4.70 4.70
SE 19		5.30	4.30	4.30	NE 12			6.00	4.60 4.60
TP	4.51	9.42	4.69	4.91	TP	5.27	9.87	6.00	4.60
chk Floor Stake		4.37	5.05	8.17	NE 13			5.27	4.60 4.60
NW 17		4.92	4.50	4.50	NW 13			5.17	4.70 4.70
NE 17		4.77	4.65	4.65	SE 11			5.42	4.45 4.45
SE 16		4.77	4.65	4.65	NE 11			5.67	4.20 4.20
SW 16		4.92	4.50	4.50	Pov.			5.28	4.59
TP	4.47	9.38	4.51	4.91	Pov 100' N NE #11			5.62	4.25
NW 16		4.78	4.60	4.60	TP	4.86	9.56	5.17	4.70
NE 16		4.63	4.75	4.75					

INDEXED
WK
NOV 18 1948

Cont. Page 50

Grades for Conc slabs bottom
of steps Contd.

888

El. Grade

SW # 3

5.18

3.70

3.70

NW # 3

5.48

3.40

3.40

3.90

4.98

4.95

4.98

0.03

Nail in 1st Pole west of Congress St EB 1734-4
on Moffett St.

Walker
Hendricks
Becker
Greer
12-16-46

River-Lawn
Curb Finish Grades
for Fleet Street
Sketch on Page 20

B.M. Conc. Base Flag Pole - Page 2 = 579
451
10.30*

10.30

Stations	Ret in 6 Parts	Elev. Top of	Cuts and Fills	Offsets	
Lt. 0+00 = B.C. cb Ret on Congress	5.14	5.16	4.98	+0.18	4' to Back edge cb
①	5.09	5.21	5.00	+0.21	
②	5.12	5.18	5.02	+0.16	
③	5.39	4.91	5.03	-0.12	
④	5.31	4.99	5.05	-0.06	
⑤	5.26	5.04	5.07	-0.03	
⑥	5.07	5.23	5.08	+0.15	
~ 0+00 ~					
Rt. B.C. cb Ret on Congress	5.12	5.18	5.20	-0.02	
①	5.12	5.18	5.19	-0.01	
②	5.02	5.28	5.18	+0.10	
③	4.92	5.38	5.17	+0.21	
④	4.95	5.35	5.18	+0.17	
⑤	4.94	5.36	5.19	+0.17	
⑥ = E.C. = 0+29	4.86	5.44	5.21	+0.23	
~ 0+50 ~					
Lt	5.29	5.01	5.13	-0.12	
Rt	4.69	5.61	5.25	+0.36	
~ 0+75 ~					
Lt	5.09	5.21	5.18	+0.03	
Rt	4.78	5.52	5.29	+0.23	

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WIK
NOV 18 1948

Cont. p. 53

River Lowry Curb Grades

Cont. from P. 52

Stations	π 10.30		Elev Top cb	Cuts/ill	Offsets
1+00 Lt.	5.20	5.10	5.24	-0.14	
Rt.	5.07	5.23	5.33	-0.10	
~1+25~					
Lt.	5.16	5.14	5.29	-0.15	
Rt.	5.66	4.64	5.38	-0.74	
~1+50~					
Lt.	5.27	5.03	5.35	-0.32	
Rt.	5.60	4.70	5.42	-0.72	
~1+75~					
Lt.	5.38	5.02	5.41	-0.39	
Rt.	5.31	4.99	5.46	-0.47	
~2+00~					
Lt.	5.47	4.83	5.47	-0.64	
Rt.	5.19	5.11	5.50	-0.39	
2+25					
Lt.	5.77	4.53	5.52	-0.99	
Rt.	5.40	4.90	5.51	-0.64	
~2+50~					
Here Acct. Service Ditch					
Lt.	5.77	4.53	5.56	-1.03	
Rt.	5.70	4.60	5.56	-0.96	
~2+77~					
π 9.19					
Lt.	4.75	4.44	5.49	-1.05	
Rt.	4.75	4.44	5.45	-1.01	

Cont. P. 54

10.30 π
5.70
4.60 T.P.
4.59 +
9.19 π

River Lower Curb Grades
Cont from p 53

54

Stations	T			Elev	
	9.19			Top of	
~3+03=BC. 30'cbR~					
Lf BC		5.06	4.13	5.43	-1.30'
" ①		4.96	4.23	5.41	-1.18'
" ②		4.90	4.29	5.39	-1.10'
" ③		4.91	4.28	5.37	-1.09'
" ④		4.94	4.25	5.35	-1.10'
" ⑤		4.98	4.21	5.33	-1.12'
" ⑥ = F.C.		5.02	4.17	5.31	-1.14'
~3+03=BC. 30'cbR~					
Rf = BC.		4.98	4.21	5.35	-1.14'
" ①		4.88	4.31	5.37	-1.06'
" ②		4.89	4.30	5.39	-1.09'
" ③		4.77	4.42	5.40	-0.98'
" ④		4.75	4.44	5.42	-0.98'
" ⑤		4.70	4.49	5.44	-0.95'
" ⑥ = F.C.		4.76	4.43	5.46	-1.02'

Note: Mottel A Grades
on p 55

Riser Lovin Curb Grades
Mottet street

Grades from P-24 sketch P-20

Stations 279 Elev Top cb Cut & Fill

~ 0+00 ~

Lt	INDEXED	4.77	4.42	5.56	-1.14	/
E		4.61	4.58	5.59	-1.01	/
Rt		4.50	4.69	5.62	-0.93	/

~ 0+25.25 ~

Lt		4.90	4.29	5.50	-1.21	/
Rt		4.44	4.75	5.57	-0.82	/

0+50.50 = B.C. 30' cb Rd on Lt.

Lt		4.76	4.43	5.45	-1.02	/
Rt		4.55	4.64	5.52	-0.88	/

0+93.5 = E. Fleet St on Lt.

Rt		4.48	4.71	5.43	-0.72	/
----	--	------	------	------	-------	---

1+36.5 = E.C. cb Rd on Lt.

Lt		5.02	4.17	5.31	-1.14	/
Rt		4.93	4.26	5.34	-1.08	/

1+65.82 = 1/2 way from cb Rd. to B.C. on Lt.

Lt		4.91	4.28	5.24	-0.96	/
Rt		4.83	4.36	5.28	-0.92	/

1+95.15 = B.C. on Lt. Curve in S. Park

Lt		4.92	4.27	5.17	-0.90	/
Rt		4.90	4.29	5.22	-0.93	/

2+26.85 = Station = B.C. 10' cb R on Rt.

Rt		5.19	4.00	5.15	-1.16	/ 4' Rt of West end Vertical Curb.
----	--	------	------	------	-------	------------------------------------

River Lower - Curb Grades
 Mallet St. Cont. from p. 55

Stations	919			Flev. Top cb	Cuts - Fill	
2+2685 ^{off} Rt.		4.94	4.25	5.15	-0.90	4' to Back edge Rolled Curb
2+3034 ^{off} Rt. = F.C. 10'cb R		4.98	4.21	5.10	-0.89	
+5336 on Rt. - 1/2 way from 10'cb R to F.C. with		4.93	4.26	5.05	-0.79	
2+1203 on Lt.		4.68	4.51	5.14	-0.63	
+2891 " "		4.96	4.23	5.11	-0.88	
+4579 " "		4.93	4.26	5.08	-0.82	
+6267 " "		4.81	4.38	5.05	-0.67	
2+7954 F.C. " "	8.53	4.47	4.06	5.05	-0.95	
2+7954 DN Rt.		4.55	3.98	5.01	-1.03	
~ 3+00 ~						
Lt.		4.69	3.84	4.96	-1.12	
Rt.		4.77	3.76	4.96	-1.20	
~ 3+25 ~						
Lt.		5.45	3.98	4.91	-0.93	see Note →
Rt.		4.92	3.61	4.91	-1.30	
~ 3+50 ~						
Lt.		4.58	3.95	4.86	-0.91	
Rt.		5.14	3.39	4.86	-1.47	
~ 3+75 ~						
Lt.		4.76	3.77	4.81	-1.04	
Rt.		5.11	3.42	4.81	-1.39	
~ 4+00 ~						
Lt.		4.86	3.67	4.76	-1.09	
Rt.		5.27	3.26	4.76	-1.50	

Note - Reset stake

3+25 on Lt.

RM-stake Rt 2+7954

Elev. 3.98

+5.45

H.I. 9.43

CK-stake Rt 5.67

3+00 → 3.76

919 T
 4.92 -
 4.27 TP
 4.26 T
 8.53 T

River Lawn - Curb Grades

Moffet St.
Cont. from p. 56

Stations	8.53			Elev. Top	
~4+25~					
Lt	4.82	3.71	4.71	-100	✓
Rt.	5.08	3.45	4.71	-126	✓
~4+5889=BC. 4.~					
Lt.	5.06	3.47	4.65	-118	✓
Rt.	4.88	3.65	4.65	-100	✓
~4+7100~					
Lt	5.12	3.41	4.62	-121	✓
Rt.	5.05	3.48	4.62	-114	✓
~4+8311~					
Lt.	5.10	3.43	4.59	-116	✓
Rt.	5.30	3.23	4.59	-136	✓
~4+9522~					
Lt	5.28	3.25	4.56	-131	✓
Rt.	5.46	3.07	4.56	-148	✓
5+07.33					
Lt	5.25	3.28	4.53	-125	✓
Rt.	5.28	3.25	4.52	-127	✓
5+1418 = PRC. on Rt. 15' cb R.	5.38	3.15	4.50	-135	✓
± 15' cb Ret.	5.10	3.43	4.52	-109	✓
E.C. " " "	5.10	3.43	4.54	-111	✓
693 West of 15' cb R.	4.92	3.61	4.55	-094	✓
5+1944 on Lt.	5.36	3.17	4.50	-133	✓
5+3155 = E.C. on Lt.	5.31	3.22	4.41	-126	✓

River Lewis
Moffet St. Curb Grades

Stations	8.53		El. Top of	
~54943~				
Lt	4.98	3.55	4.46	-0.91'
Rt = E. Roadway to West	5.15	3.38	4.48	-1.10'
~547443~				
Lt	4.46	4.07	4.43	-0.36'
Rt. 5' West of 15' cb R	4.64	3.89	4.42	-0.53'
Rt. BC 15' cb Ret	4.58	3.95	4.40	-0.45'
1/2 way " " "	4.53	4.00	4.38	-0.38'
~548943 = E.C. 15' cb R on Rt ~				
Rt	4.45	4.08	4.41	-0.33'
Lt.	4.37	4.16	4.37	-0.21'
6+1443				
Lt.	3.92	4.61	4.35	+0.26'
Rt. = BC. 30' cb R	4.25	4.28	4.30	-0.02'
①	4.15	4.38	4.28	+0.10'
②	4.22	4.31	4.27	+0.04'
③	4.20	4.33	4.25	+0.08'
④	4.21	4.32	4.23	+0.09'
⑤	4.27	4.26	4.22	+0.04'
⑥ = E.C. 30' cb R. on Rt	4.25	4.28	4.21	+0.07'
6+3443 on Lt. BC. 10' cb Ret.	4.26	4.27	4.24	-0.07'
E 10' cb R on Lt	4.46	4.07	4.34	-0.27'
E.C. " " " "	4.27	4.26	4.34	-0.08'

chk next in Pole P-51

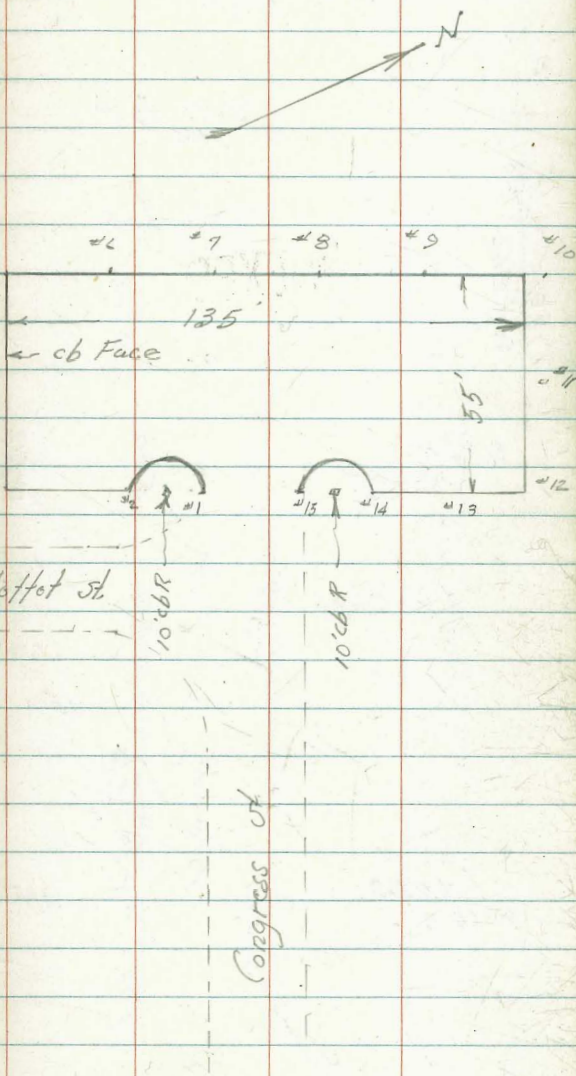
8.53 x
3.78 -
4.75 TP
4.63
8.78 x
3.82
4.96
4.25 001

Walker
Hendricks
Becker
Greer
12-18-56

River lawn - Curb Grades
For Parking Area
on West end Congress St

59

Stations	8.78		Elev. Top cb	Cuts & Fills	offsets
# 1		4.62	4.16	4.00	+0.16 /
# 2		4.80	3.98	4.13	-0.15 /
# 3		4.59	4.19	4.17	+0.02 /
# 4	INDEXED WIK NOV 18 1959	5.03	3.75	4.09	-0.34 /
# 5		5.09	3.67	4.01	-0.32 /
# 6		5.18	3.60	3.98	-0.38 /
# 7		5.10	3.68	3.95	-0.27 /
# 8		5.16	3.62	3.92	-0.30 /
# 9		5.15	3.63	3.89	-0.26 /
# 10		5.28	3.50	3.86	-0.36 /
# 11		4.93	3.85	3.92	-0.07 /
# 12		5.12	3.66	3.98	-0.32 /
# 13		4.96	3.82	4.00	-0.18 /
# 14		4.74	4.04	4.03	+0.01 /
# 15		4.70	4.08	4.03	Grade



12

valley

Gutter

cb=562
G=529

13

Moffet

G=523

13
1436
Cont. 1462

5.04
3+46

G=549

G=505

G=523
cb=556

NEGRO

30' cb R
3+03

G=510

5.30

G=512

2+50=84

cb=556
G=523

OT

G=523
cb=556

13'

Flect

13'

0+2.9
30' cb R

G=476

5.10 5.16

488

Uniform Grade

30' 17.83

20

4.80

CONGRESS ST.

0+00

Gut
389

91

94

57

400

P = 3.59

Pav = 395

Pav = 396

Congress

Mollet

ST

Rocked

Gut Rocked

518.43

518.43

612.19

408

470

415

414

412

410 = Gut

406 = Gut

408

470

410 = Gut

415

414

412

410 = Gut

408

470

410 = Gut

415

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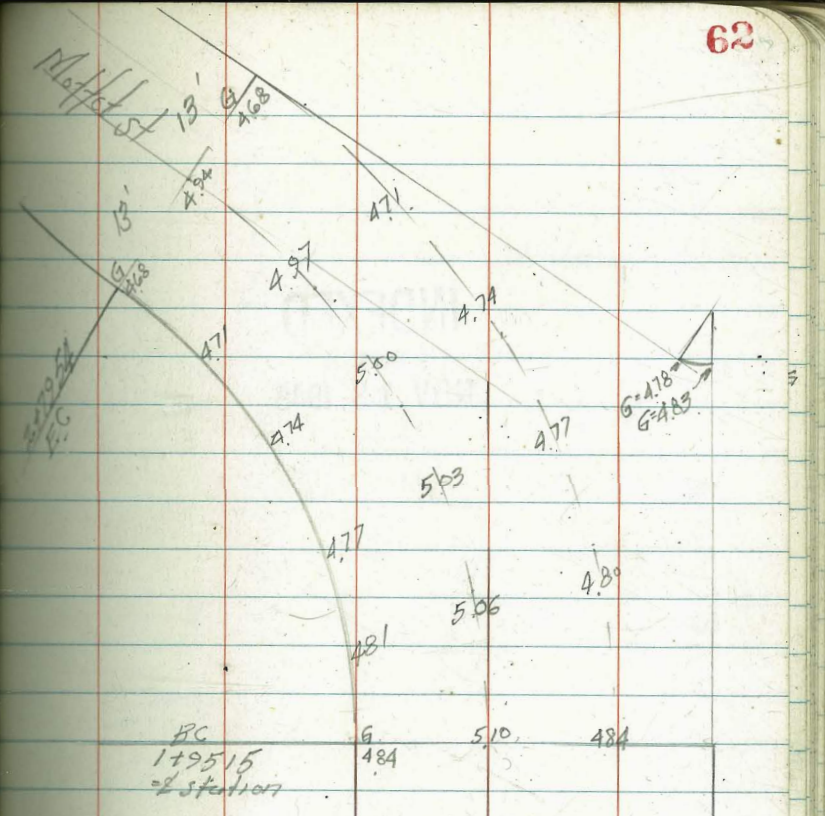
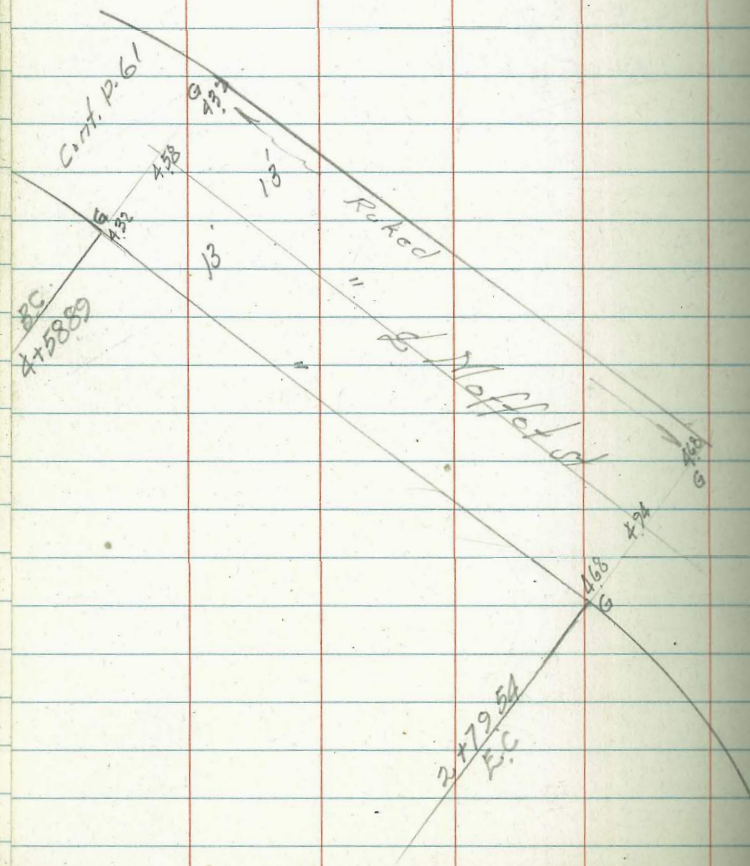
410 = Gut

408

470

410 = Gut

415



13' x 13' x 14'

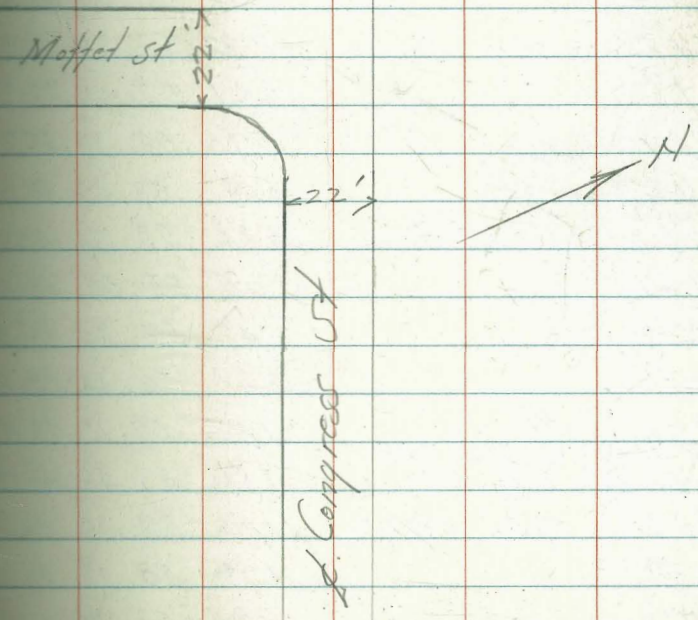
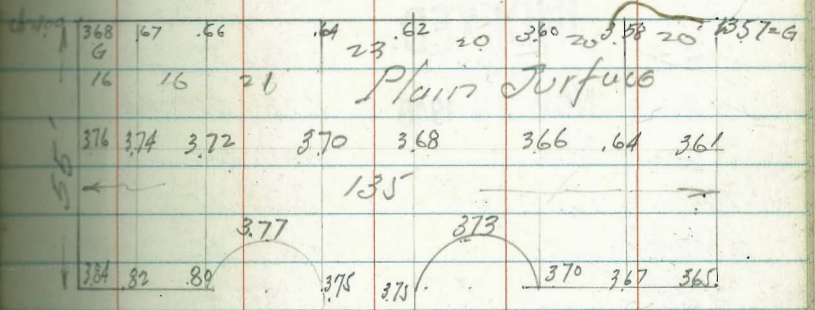
Cont. from P. 60

Walker
Hendricks
Becker
Greer
1-17-47

River Lower Paving
Parking Area

INDEXED
WK
NOV 18 1948

Notched cb



Walker
Becker
Roberts
5-23-47
SEWER CONSTRUCTION
on National Ave West of 43rd St.
And in CARUTHER'S ADD.
South of Logan Ave
Drawing No. C466-L.

Christed Cross on Rim MH	11.79	46.46	34.67	BM FB 1672 22 Pl. Flou...	Cuts	offsets
± Exist MH = 07.00			11.23	35.23	2.957	5.66
+40	INDEXED		2.03	37.43	30.99	6.41
+80	WK		6.70	39.76	32.41	7.35
1+20	NOV 18 1948		4.12	42.34	33.83	8.51
+60			3.03	44.43	35.25	9.18
T.P.	12.65	58.63	0.48	45.98		
2+00			11.89	46.71	36.67	10.07
+40			10.00	48.63	38.09	10.51
+80			8.54	50.09	39.51	10.58
3+20			7.32	51.31	40.93	10.38
+60			6.61	52.02	42.35	7.67
4+00			5.70	52.93	43.77	9.16
+2362 Δ RT MH			5.04	53.59	44.63	8.96
4+29.52 = CHK ± = 51.51 FB 1672 71			5.26	53.37	45.35	
4+61			3.05	55.58	45.10	10.48
+96			2.43	56.20	45.54	10.66
5+31			2.21	56.42	45.95	10.65
+66			1.52	57.11	46.40	10.71
5+98.54 = 5+98.12	Equation = MH Δ RT 8'12"		1.17	57.46	46.80	10.66
5+98.12	5.65	63.00	1.28	57.35	46.80	10.55
6+29.12			4.93	58.07	47.13	10.89
+70			4.26	58.74	47.69	11.05

π from P. 64
63.00

Cuts.

7+10			3.60	59.40	48.19	11.521	6' Lt
7+47.12			3.59	59.41	48.65	10.76	6' Lt
7+80			7.45	55.55	49.06	6.49	6' Rt
8+20			8.26	54.74	49.55	5.19	6' Rt
+60			6.61	56.39	50.05	6.34	6' R
+85	Δ Lt 90° 04'		5.85	57.15	50.36	6.79	6' R
9+05	- 0+00	Alm. #3	5.90	57.10	50.60	6.50	6' Rt
T.P.	12.74	69.84	5.90	57.10			
0+40			9.78	60.06	54.67	5.39	7' Rt
+79			3.64	66.20	58.63	7.57	7' R
T.P.	7.09	76.56	0.37	69.47	62.80	6.67	
1+20			4.53	72.03	62.80	9.23	7' R
1+47.74	Δ 91° 43' Rt	MH #4	5.05	71.51	65.60	5.91	276' Rt on bisector of Angle
1+60			4.90	71.66	65.74	5.92	6' R
2+00			2.73	73.83	66.19	7.64	6' R
+40			2.54	74.02	66.64	7.38	6' R
+80	5.80	79.72	-2.64	73.92	67.09	6.83	6' R
3+20			5.80	73.92	67.54	6.38	6' R
3+60			4.23	74.79	67.99	6.80	6' R
4+00			4.58	75.14	68.46	6.70	6' R
4+40	6.64	82.33	4.03	75.69	68.83	6.80	"
4+72	= MH		6.12	76.21	69.26	6.95	"
5+01			6.37	75.96	69.59	6.37	"
+41			6.14	76.19	70.06	6.15	"
5+81			5.27	77.06	70.45	6.57	489' R = Nail in Barn ←

					lets	offsets
	82.33					
6+21			6.20	76.13	7094	5.19 ✓ 6'R
+61			6.13	76.20	7139	4.81 ✓ "
7+01	Δ 4		5.73	76.60	7184	4.76 ✓ "
+32 = MH#6			5.28	77.05	7219	4.86 ✓ "
+60			5.11	77.22	7250	4.72 ✓ "
8+00			4.18	78.15	7275	5.20 ✓ "
140	666	84.99	4.00	78.33	7341	4.93 ✓ "
+80			5.82	79.17	7385	5.32 ✓ "
9+20			5.49	79.50	7430	5.20 ✓
+60	Δ 90° Rt		4.65	80.34	7475	5.59 ✓
+81 = MH			3.46	81.53	7500	6.53 ✓
10+26			3.24	81.05	7551	5.54 ✓
+71			3.76	81.23	7601	5.22 ✓
0+00			4.01	80.98		
+32.5			4.01	80.98	7539	5.59 ✓
+65			4.50	80.49	7579	4.70 ✓
• Chk 2 Hub 9+81	F.S. 1672 47		3.82	81.17		
				81.18 = Hub		
				2.01 = Error		

SEWER CONST.
on Nat'l. Ave
and in Corrother's add.

T from P-64
63.00

LN#2

0+00 = 4+2362 P-64

2.41 53.59 44.63

El. Elev Luts offsets

8.96

+28

2.74 53.26 44.83

8.43

6' Rt = chisled Cross on Pav

+57.7

10.21 52.79 45.03

7.76

6"

LATERAL #1

(6+2912) Lateral Elev.

4.23 58.07 47.13

10.59 = cut to Lateral. For cut to Main line see p. 64
6' Lt.

39.6 South = Plug.

11.71 51.89 48.00

7.89

= cut to Lateral. For Main line see P-64

39.6 South = Plug.

11.24 51.76 48.00

7.76

6' East

Lateral #2

7+4712 Lateral Elev.

2.59 59.41 49.00

10.41

36' Lateral

10.46 52.54 49.10

10.71

2.84

5.14

Walker
Becker
Johnson
Meltzer

Curb Grades - Collier Ave.
from W.L. 54th

8-6-47

1+25

INDEXED
WK
NOV 19 1948

1+20

0+90

0+60

0+30

0+00 = W.L. 54th

H

\$

RF 68

413.42

413.42

413.50

413.48

30

413.86

414.00

414.50

414.24

415.00

413.62

415.50

415.00

8M.8P

413.40 NE corner 54th

Don 6648-L

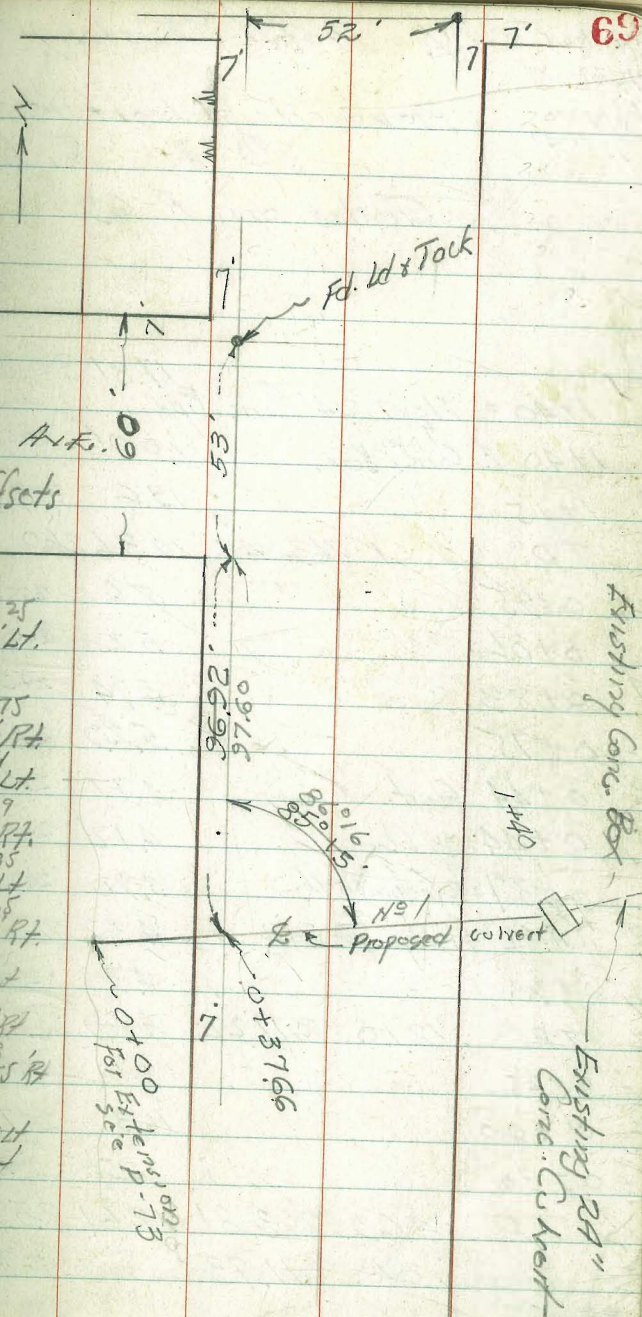
Walker
Hendricks
Becker
Johnson
9-16-47

8TH AVE. And ROBINSON AVE
Grades for Culvert
(Profile sheets P-70)

INDEXED
WK
NOV 19 1948

	Existing	Flow	El. Stakes	El. Flow Line	Cuts	offsets
1+40	Flow 24" Culvert	1781	245.66			
1+40	Box Top Hd	10.06	253.41	246.20	7.21	
1+15		9.41	254.06	246.20	7.86	36' Lt.
TP	2.61	263.47	10.36	260.86		
1+15		10.36	260.86	246.20	14.66	26' Rt.
0+95		4.17	267.05	246.60	20.45	28' Lt.
0+95		7.53	263.69	246.60	17.09	25' Rt.
0+75		3.58	267.64	247.00	20.64	25' Lt.
0+75		6.06	265.16	247.00	18.16	25' Rt.
0+50		3.49	267.73	247.50	20.23	25' Lt.
0+50		5.10	266.12	247.50	18.62	23' Rt.
0+25		4.98	266.24	248.00	18.77	16.25' Rt.
TP	12.10	271.22	4.69	259.12		
0+25		0.83	262.98	248.00	14.98	16' Lt.
0+00		12.88	250.93	248.50	2.43	
		263.81				
		X from P-70				

Robinson Ave. 60



Existing Conc. Box

Existing 24" Conc. Culvert

Proposed

15'

Culvert

0+37.66

0+00 for Ex. P-70

Walker
Hendricks
Johnson
9-16-47

Profile Existing Ground.
Proposed Culvert Location P-69
8th Ave. So. Robinson
Grades on P-69

70

		17.81	245.66
1+40 =	Flow 24" Conc. Pipe		
1+40	Top of Conc. Box.	10.06	253.21
1+15		13.6	249.9
T.P.	2.61	263.47	10.36 260.86
0+95		5.6	265.6
0+86		5.2	266.0
0+83		5.74	265.48
0+75		5.29	265.98
0+44	Gut.	4.71	266.51
0+44	= 14" Cb	4.12	267.10
0+37	= E. edge Walk	3.90	267.32
0+32	= W. edge Sidewalk	4.32	266.90
0+30		4.3	266.9
T.P.	12.10	271.22	4.69 259.12
0+25		1.1	262.7
0+00		16.3	247.5
0-30		15.5	248.3
T.P.	4.69	263.81	12.61 259.12
	1.01	271.73	270.72

B.M. Christed Square W. C. B. 8th³⁵ South of -
Robinson Ave

Grades - Proposed Culvert No 1
 sketch P-72
 8th Ave So. of Robinson.

Cont. P-71

T.P. 0.65 259.77 ✓ 12.24 259.12
 F.P. Chk 0+25 158.84 5.13 266.23
 0.64 271.36 270.72 B.M.

El.
 Flow
 Line

H S #

1+38.5 = West edge exist. Conc. Box.

246.20

C 7.24

1+15

246.59

C 7.47

C 14.27

0+95

246.93

C 20.12

C 16.76

0+75

247.26

26.71

23.29

0+50

247.67

C 20.35

C 17.90

0+25

248.09

26.35

22.65

0+00

248.50

C 20.06

C 18.45

-20

248.83

25.9

22.1

-40

249.16

C 14.89

C 18.15

-60.18 = Beg. Pipe

249.50

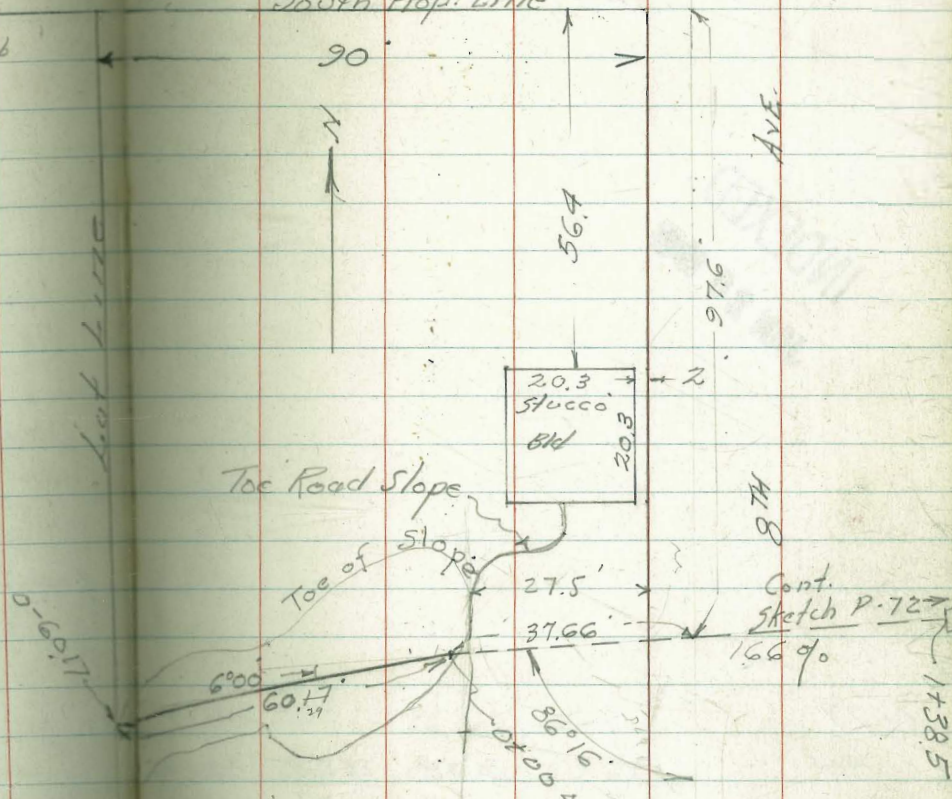
16.45

15.8

Location Toe Slope
8TH And Robinson Ave
And Sketch
Proposed Extension of Culvert
to Lot Line

Robinson Ave
South Prop. Line

1+39 = End Pipe
1+38.5 = West edge Exist. Conc. Inlet Box



97.6

1+38.5

El. Flow Cuts

Station	Flow	Cuts
0+00 = Δ R 6°	8.67	251.10 248.50 2.6
0-20	10.32	249.45 248.83 2.62
0-40	8.82	250.95 249.16 1.79
0-60.17	8.11	251.66 249.50 2.16
0-60.17 on Ground		250.0

259.77 ✓
From P. 71



Scale 1" = 30'

48.5

1-23-48
 Hendricks Stake Curbs on 8th Ave
 Becker
 Johnson

Sta.	+	H.I.	-	Lt Elev. Stake	Elev. Cb.	Cor. F.	-	Elev. Stake Rt	Elev. Cb. Rt	Cor. F.
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INDEXED
 JAN 26 1948

1+79								6.15	269.24	269.20	Meet.
1+74			10.24	265.05	264.97	Meet	8.63	266.76	266.50	CO. 26	
1+14			9.89	265.50	265.50	CO. 8.52	8.52	266.83	266.75	CO. 08	
0+84			9.11	266.28	266.02	8.29	8.29	267.10	267.00	CO. 10	
0+54			7.00	268.39	268.39	Meet	5.92	269.39	269.43	Meet.	
0+00	SW Pk. Cb. 8th & Robinson		1.48						273.91		
BM	4.67	275.39			270.72	Chisel in Cb	P-72				

INDEXED

NOV 19 1918

Walker
Hendricks
1-16-47

Grades for Topping Exist cb
on West Side 30th
from Shine G St to Alley

Plan # 3187-B

153.53

Station
Shine G St
= 0+00

+25

+50

+75

+100

+125

+148

+200

INDEXED

WIK
NOV 19 1948

		Flev. Gmb Top cb	Fills
2.98	150.55	150.80	-0.25
3.76	149.77	150.34	-0.57
4.23	149.30	149.88	-0.58
4.59	148.94	149.42	-0.48
4.81	148.72	148.96	-0.24
5.15	148.38	148.51	-0.13
5.51	148.02	148.09	-0.07
		148.05	-0.03

78

B.M. S.W. B.P. G + 30th = 150.55

2.98

153.53

2.81-

SW. 7' Luck
30th & G → 150.72

Walker
Hendricks
Becker
Greer
12-3-46.
Grades - 6" Water Main
on Law St.
from Ingraham to Jewell St
Drawing # 6737-L

Station			Filey Trench	Cuts	offsets
E Line Ingraham -0+00	12.14	12.19	108.95	106.1	2.85
+18 = Bk		11.63	109.51	106.86	2.65
+59		9.69	111.45	109.46	2.0
1+00 = Bk		6.87	114.27	112.10	2.2
+40 "		4.40	116.74	114.48	2.3
+80 "	130.80	11.82	118.98	116.56	2.4
2+20 "		10.03	120.77	118.3	2.5
+60 "		8.58	122.22	119.7	2.5
3+00 = Bk		7.70	123.10	120.8	2.3
+50		6.30	124.50	122.0	2.5
4+00		5.28	125.52	123.2	2.3
+50		4.36	126.44	124.4	2.0
5+00		3.10	127.70	125.6	2.1
+19.16 = W Line Jewell St		2.60	128.20	126.0	2.2

INDEXED
WK
NOV 19 1948

B.M. B.P. S.W. Diamond ^{And} ~~Locum~~ = 10595

	+ 12.23	
	+ 118.18	
	0.47-	
	TP 117.71	
	+ 11.03	
	TP 128.74	
	0.31-	
	TP 128.43	
	+ 12.65	
	TP 141.08	
	0.20-	
	TP 140.88	
	+ 11.45	
	TP 152.33	
	13.09-	
	TP 139.24	
	1.04	
	140.28	
	11.25	
3 Nails in Pole 35. } →	129.03	
Level = Jewell } →	1.77 +	
	130.80 TP	
	11.81 -	
	118.99 TP	
	2.15 +	
	121.14 TP	
	12.19 -	
	108.95	
	0.57 +	
	109.52 TP	
	11.80 -	
	97.72 TP	
	1.45	
	99.17	
	12.97 -	
	86.20 TP	

130.80
6.06
124.74 dtk ch stake
124.84 3+00 on west
0.10 Profile
diff.

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

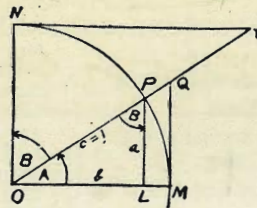


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

$$\begin{array}{r} 373 \\ 48 \\ \hline 857 \\ 98 \\ \hline 131 \end{array}$$

$$\begin{array}{r} 490 \\ 367 \\ \hline 195 \\ 4219 \\ \hline 437.34 \end{array}$$

Rosecrans Ct

25'

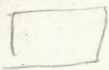
Kentz

35'

67'

Lowroll

67495



$$\begin{array}{r} .6 \\ 959 \\ 6 \\ \hline 1019 \\ 31 \end{array}$$

$$\begin{array}{r} 976 \\ 209 \\ \hline 767 \\ 203 \\ \hline 564 \end{array}$$

$$\begin{array}{r} 2126.70 \\ 417.66 \\ \hline 64436 \end{array}$$

$$\begin{array}{r} 706 \\ 208 \\ \hline 954 \\ 530 \\ \hline 424 \end{array}$$

$$\begin{array}{r} 883 \\ 433 \\ \hline \times 20 \\ 730 \\ 250 \\ \hline 480 \end{array}$$

925

+90.05 20'

$$\begin{array}{r} 90 \\ 34 \\ \hline 56 \\ 2 \\ \hline 8112 \end{array}$$

$$\begin{array}{r} 7266 \\ 3633 \\ \hline 4158.99 \\ 4195.22 \end{array}$$

$$\begin{array}{r} 706 \\ 198 \\ \hline 944 \end{array} \quad \begin{array}{r} 7.46 \\ 1.86 \\ \hline 9.32 \end{array}$$

$$\begin{array}{r} 29.16 \\ 2670 \\ \hline 6586 \end{array}$$

$$\begin{array}{r} 109515 \\ 01935 \\ \hline 10165 \end{array}$$

$$\begin{array}{r} 976 \\ 28 \\ \hline 1252 \end{array}$$