



# G-225

## CITY ENGINEER'S OFFICE

MADE IN U. S. A.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- |                              |   |
|------------------------------|---|
| No. 380 LEVEL BOOK.          | Left and Right Hand Page the same as Left Hand Page of this Book.   |
| No. 382 FIELD BOOK.          | Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.                               |
| No. 384 MINING TRANSIT BOOK. | Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.                               |
| No. 385 FIELD BOOK.          | Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red. |

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### THE FREDERICK POST CO.

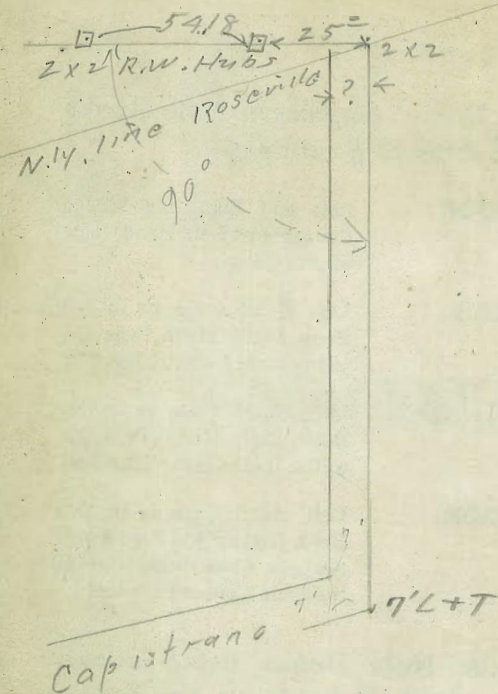
ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

Completely  
INDEXED  
MK  
FEB 16 1949

MICROFILMED  
APR 13 1985



Law St. Gresham to Hains { Meter- } 73-78  
Boxes

Capistrano Pl. Pump house	Mission Beach	6 to 10
Quimby + Poe. S. Ely Firm	Capistrano	2-4
Frontier Sowers		3-
47+Market Culvert		5
Harbor Dr. Traffic Islands		11
Mission Valley Golf Club - Culvert + check		12
Blk 3. Las Alturas Sewer		13
Haines La Playa Water line		14
Alley Blk 60. Ocean Beach		15
Newtown park Blood Center		16
Reed + Daley Sub. Alley Blk 322		17-18 <sup>53+54</sup>
" " " " " 319		19-20 <sup>51+52</sup>
Meade - Resurface Fairmount to 32 <sup>nd</sup>		21-49 <sup>+58</sup>
Oakmore Sewer		50
Meade Resurface 32 <sup>nd</sup> to Georgia		55 to 58
30 <sup>th</sup> + Landis Curb Grades		59
Front + Quince Culvert	64+	60
Water Grades (Dalbergia) Vactata yama		61
(Yama) Dalbergia to Cottonwood		62
Bearslay + Harbor Dr. Sewer		63
Valencia Park Culvert Blk 3-		65
32 <sup>nd</sup> + Univ Returns		66
Bramson Pl. Storm Drain		67 to 68
Blks 3+5 Nettleship Tye Sewer	tract #1	71 + 72
Bangor {Sewer Grades Lucinda to Jennings}		69
Harbor Dr. + Bangor Locate Sewer D.E.S		79

Capistrano Place Pump House  
2-3-47

B.M. = Nail in fence. S. Side  
Capistrano Place & Bayside walk.  
Brot. from San Diego Place See Book

INDEXED

WK  
NOV 22 1948

2.75      3.33      —      0.58

0+83.77 W. Edge M.H.      -8.10

0+89.10 E. Edge M.H.      -8.60  
11.93      12" line to pump house  
8.02      + in paving  
C 8.91      8' RT.

1+12 = 12" line at pump house      -12.00      + in pump house.  
15.33      on line  
2.33  
C 13.00

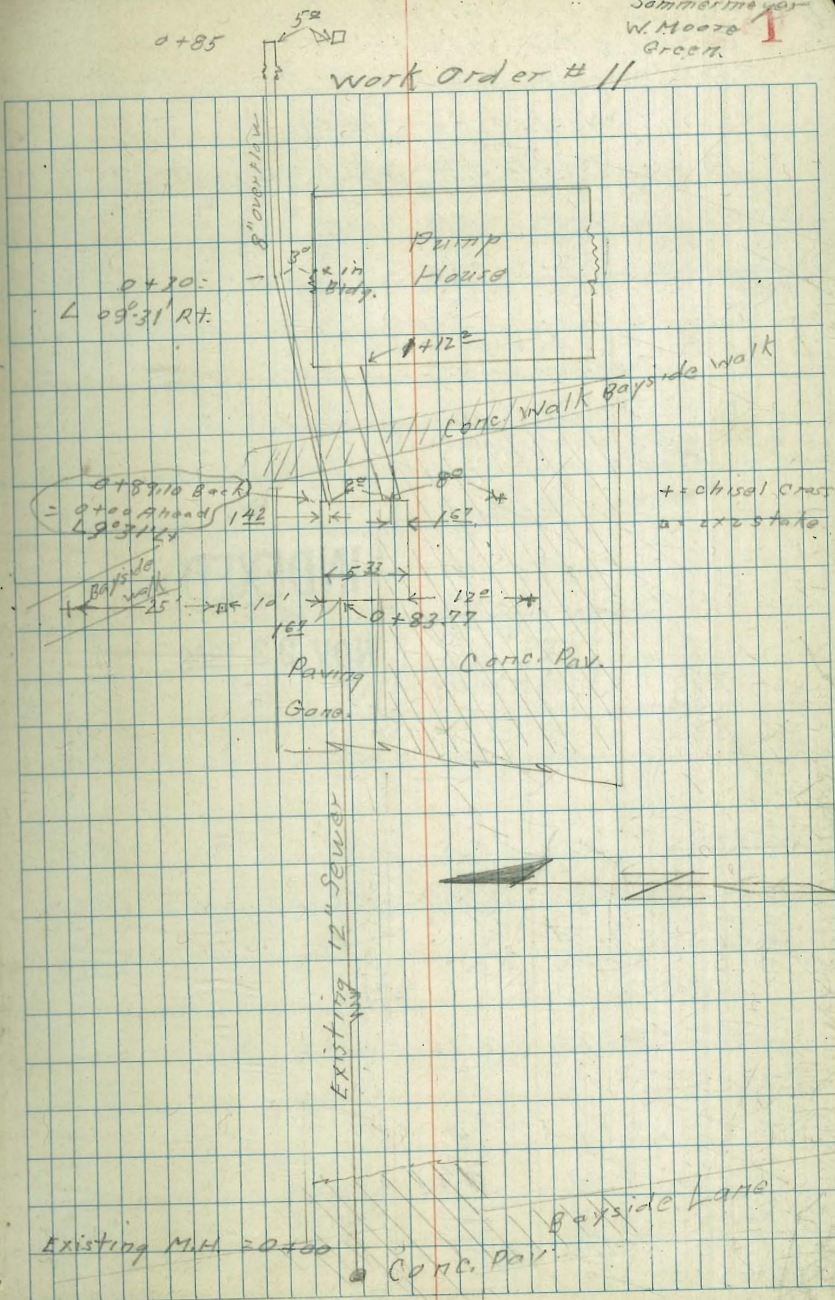
0+00 (8" over flow)      -3.00      + in Pav.  
6.33      10' RT  
3.02  
C 3.31

0+30 (L 9° 31' RT)      -3.35      Rate = .01177  
6.68      \*3' RT  
3.68  
C 3.00

0+85 End pipe      -4.00  
7.33      D 6' RT.  
8.57  
F 1.24

Summer for  
W. Moore  
Green

Work Order # 11



2-4-46 Sewer lateral Grades  
 Quimby + Poe streets  
 Capistrano to Wly line Roseville

Work order 1019

B.M. S.E. B.P. Chatsworth + Poe

	1.37	77.58	-	78.21	BM #1
T.P.	7.10	77.40	9.28	70.30	
S.S.	N.W. B.P. (shown as 71.70) Poe + Capistrano		5.66	71.74	BM #2
T.P.	9.63	86.41	0.62	76.78	
S.S.	SWRR, Quimby (shown as) + Capistrano (81.21)		5.27	81.14	BM #2
	<u>86.41</u>				

INDEXED  
 WK  
 NOV 22 1948

LAT. #1	<u>78.12</u>				
	8.29				
	<u>3.21</u>				
	C 5.08				
T.P.	13.16	99.31	0.26	86.15	

LAT #2	#3	#4	#5	#6	#7
83.21	85.35	87.49	87.63	91.70	93.50
16.10	13.76	11.82	9.68	7.61	5.81
10.93	8.76	6.53	4.30	2.32	0.45
C 5.17	C 5.20	C 5.29	C 5.38	C 5.29	C 5.36

T.P.	12.22	<u>110.35</u>	1.18	98.13	
------	-------	---------------	------	-------	--

#8	#9	#10	#11	#12	#13
95.10	96.40	97.50	98.42	97.83	101.24
Stub 15.25	13.95	12.85	11.93	10.52	9.11
2' Back 9.37	8.62	7.65	6.77	5.23	3.86
C 5.88	C 5.33	C 5.20	C 5.16	C 5.19	C 5.27

W.O. 1019

2

X  
110.35

Sewer Laterals Quimby St.						
#14	#15	#16	#17	#18	#19	#20
95.21	94.74	98.86	99.58	100.50	101.47	102.78
15.14	12.61	12.69	10.77	9.85	8.88	7.57
13.94	7.00	6.44	5.72	5.31	4.37	3.19
C 1.70	C 5.63	C 5.25	C 5.05	C 4.54	C 4.51	C 4.44

T.P.	0.97	78.85	12.47	97.88
T.R.	0.82	86.66	13.01	85.84
X.P.	1.88	<u>75.76</u>	12.78	73.88

Sewer Laterals Poe St.

#31	#30 2x2 stub	#29	#28	#27
60.24	59.09	59.53	59.88	60.22
15.52	16.67	16.23	15.88	15.54
10.74	6.81	11.01	10.56	10.34
C 4.78	C 9.86	C 5.22	C 5.32	C 5.20

#26	#25	#24		
60.57	61.26	61.94		
15.19	14.50	13.82		
10.04	7.29	8.67		
C 5.15	C 5.21	C 5.21		
	7.72	<u>74.32</u>	9.16	66.60

#23	#22	#21
64.91	65.05	65.40
9.61	9.27	8.92
4.38	4.22	3.78
C 5.23	C 5.45	C 5.14

See page  
 4

T.P.	3.76	75.49	2.59	71.73	13 M. #2 opposite page
T.R.	6.80	77.67	2.62	72.87	
			1.45	78.22	original B.M.
				<u>77.21</u>	0.01 Error

2-5-47  
Sammemoja  
W Moore  
J. Green

W.O. 11267  
Frontier St  
So. of M.H. 57 O.B. Sewer Line

B.M. = M.H. Invert - 0+00 = -4.40

11.10    6.70    -    -4.40

0+00	0+25	+50	+75
-4.40	-4.23	-4.05	-3.88
11.10	10.93	10.75	10.58
✓	4.63	4.63	4.62
	C 6.30	C 6.12	C 5.96

1+00	+25	+50	+75
-3.70	-3.53	-3.35	-3.18
10.40	10.23	10.05	9.88
4.60	4.69	4.73	4.66
C 5.80	C 5.54	C 5.32	C 5.22

2+00	+25	+50 Dead End
-3.00	-2.83	-2.65
9.70	9.53	9.35
4.60	4.62	4.53
C 5.06	C 4.91	C 4.82

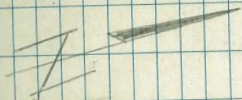
Stake Sewer P.L. 242 For  
W.J. Crower.

3

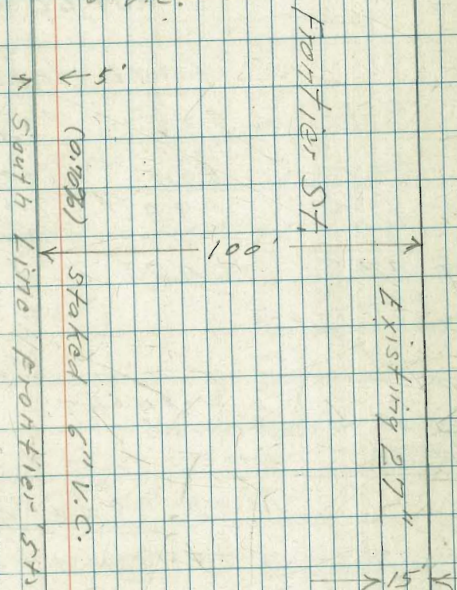
Work Order # 11267  
☉ stakes set 4' Pt.

INDEXED

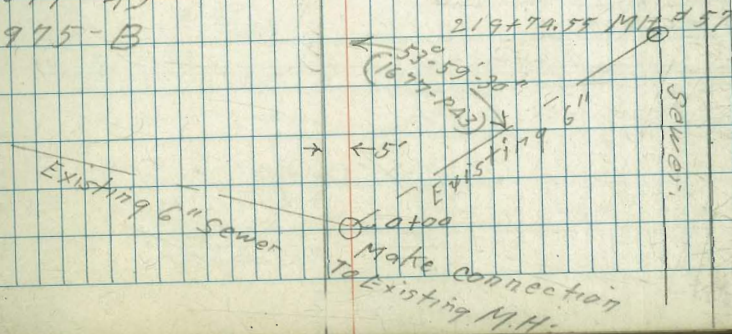
WK  
NOV 22 1948



2+50 = D.E.  
6" V.C.



See P.B.  
1677-A3  
2975-B



2-5-47

W.O. # 1019

P.O.E. St.

Additional Sewer Laterals

#16 Lat. stake				60.57
page 2	2:88	68.60	—	65.72
				<u>5.15</u>
				65.72

omit  
#364 #38

INDEXED  
WK  
NOV 22 1948

Set 2x2 stakes A' Back

#32	#33	#34	#36	#37
59.97	59.52	59.07	58.44	58.08
8.63	9.08	9.53	10.16	10.52
3.96	4.35	4.90	5.21	5.86
C 4.67	C 4.73	C 4.63	C 4.25	C 4.66

2-14-47

Quimby & Capistrano				page 2
S.E.B.P.	11.02	92.16	—	81.14

10.48	98.44	4.20	87.96
-------	-------	------	-------

Opposite 3775	5.78	103.44	0.78	97.66
T.P. in Drive	6.90	104.56	5.78	97.66

check to Lateral cut			2.82	101.74
Lat # 9				98.101.72

Grade 96.40				97.66
cut 5.33				5.75

El. Cross = 101.73

Pop Lat # 9				T.P. in Dr. opposite 3475
				97.66
				5.75
				103.41 K

100	4.88
180	2.17

2-14-47

Curb Stakes Quimby wa. 1019

Capistrano South

W. Side Quimby

98.44

1485	2+30	2+75	81K	Meet curb
			3+20	3+26
2nd. Curb				
98.44	90.13	92.57	95.00	95.30
10.75 Rod	8.31	5.87	3.44	2.14 1/4
87.69				3.12
IN.				1.02

INDEXED

WK  
NOV 22 1948

104.56				
Void	Set to plan	grade		
500 Below				
4+12	+20	4+40	+60	+62.5
99.07	99.30	100.00	100.60	100.67
98.75	99.04	99.73	100.42	100.52
5.81	5.82	4.83	4.14	4.04

104.56  
East Curb Quimby

4+45	4+50	4+70	4+80
99.90	100.10	100.80	101.10
4.66	4.46	3.76	3.46
4.09			OK

West Curb Quimby

4+00	+20	+40	+60	+80	103.41
98.60	99.30	100.00	100.60	101.20	
4.81	4.11	3.41	2.81	2.21	
stake set				stake set	
curb 0.07				curb 0.04 High	
Low					

Stake 18" Culvert, N.W. Cor.

Work order # 30

Stakes set 8' So. of E.

0+00 R.P. stake set 8' E. of 0+00

INDEXED

WK  
NOV 22 1948

B.M. =  $\Phi$  L+T, Market + 47.

8.92 129.88 — 120.96

9.10 138.71 0.27 129.61

2.96 129.22 12.45 126.26

8.27 120.75

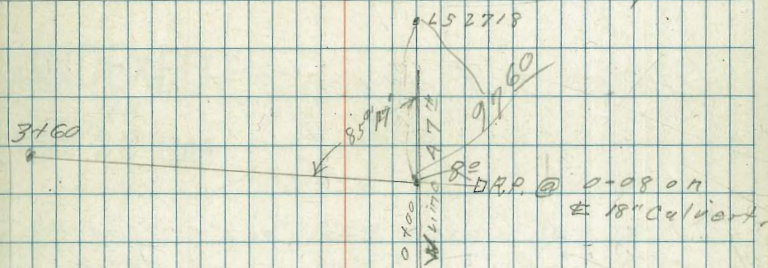
orig BM —  $\frac{120.96}{-0.01}$

A7<sup>th</sup> & Market,

Sommermeier  
W Moore  
J Green

5

2-19-47



N. Line Market

129.88

Start Pipe

F.L.  
Cleanup

$\frac{115.20}{14.68}$   
 $\frac{10.80}{C 3.88}$

0+00

0+50

$\frac{115.40}{14.48}$   
 $\frac{10.80}{C 3.68}$

$\frac{117.40}{12.48}$   
 $\frac{6.56}{C 5.92}$

1+00

1+50

2+00

$\frac{119.40}{10.48}$   
 $\frac{5.10}{C 5.38}$

$\frac{121.40}{8.48}$   
 $\frac{4.41}{C 4.07}$

$\frac{123.40}{6.48}$   
 $\frac{1.57}{C 4.89}$

138.71

End pipe

2+50

3+00

3+30

3+60

$\frac{125.40}{13.31}$   
 $\frac{7.10}{C 4.21}$

$\frac{127.40}{11.31}$   
 $\frac{6.57}{C 4.72}$

$\frac{129.60}{10.11}$   
 $\frac{4.99}{C 5.13}$

$\frac{129.80}{8.91}$   
 $\frac{2.69}{C 6.27}$



20-Feb. 1947  
Sommermeier

STAKE CULVERT IN  
W.O. # 209

Stakes set as per "B" sheet # 3188  
and "L" " # 6820 L

0+00 = L-Connection to Existing 24"  
drain 4 1/2 No. No. Line E. St 78° 16' off <sup>Prop</sup> Line  
1+49.1 = Ctr. type "D" Catch Basin + L <sup>2-57'</sup> LT  
1+59.3 = End of pipe.

Stakes set 8' L + C.

S.W.B.P.	1.17	181.18	—	180.01	27 + E
	1.66	170.11	12.73	168.45	
	1.27	159.05	12.33	157.78	
	0.91	147.59	12.37	146.68	
End of Existing 24" 0+00 - 1'			10.11	137.48	O.K.

Alley BIK 2 - Parish + Loomis Sub 6  
E. to Broadway - 26 to 27th

INDEXED

WK  
NOV 22 1948

0+00	0+50	1+00
137.52	138.59	139.66
10.07	9.00	7.93
6.16	7.70	6.81
C 3.91	C 1.30	C 1.32

INVERT C.B.	TAP C.B.	End Job
1+49.1	144.5	1+59.3
140.71	3.09	140.93
6.88	2.80	6.66
2.80	C 0.27	2.74
C 4.08		C 3.92



Paving Grades Poe St.

East	West
28.46	0+00
70.28	0-5.18
4.40V	69.50
	67.52
	5.18V
	5.16L

INDEXED  
WK  
NOV 22 1948

67.85	62.38
	5.47V
63.50	
4.35V	
	63.16
	61.50 catch basin
63.50	
4.35V	
	67.03
	62.10
	5.53V
	62.18
	5.45V

Set to subgrade

63.16
4.47
3.3
4.89V
63.16
4.47
4.80V
63.28
4.35
3.3
2.68V

N.W. B.P. Poe. 2.7A 74.68 — 71.7A  
+ Capistrano

So. Line Capistrano

So Line Capistrano

0+00 = Prop. W. Line Poe

BM #1 Page 7 3.68 67.85 — 64.17

7+28.92

7+40

7+44.5

+ 48.92 also ~~7~~ 7+58.92

+ 77.A En Curb on west

7+78.92 Brk on west 63.50 Brk on East  
4.13

67.63

+ 95.3 End West Pav.

7+44.5

7+69.5

7+85.1

Paving Grades Quimby

East      †      west

Breaks	BM#3 Page 2	81.14
		7.34
0-28.46		88.48
		0.30
0-17.07		88.18
		11.47
0-5.18		99.65
		2.00
		77.65 (97.60)
		6.72
	BM#3 - Page 2	103.87
0+00		81.14
		5.10
		86.34
		0.18
1+00		86.16
		12.73
		98.89
		0.37
1+15.85 Bk		98.52
		9.24
		107.76
1+85		
Rk		
3+15.85 P.V.C. East.		
3+20 P.V.C. West.		
3+35.85		
3+40		
3+55.85		
3+60		
3+75.85		
3+80		
3+95.85		
4+00		

**INDEXED**  
WK  
**NOV 22 1948**

Capistrano - South

25-Feb-1949

East	1/4	1/4	West
88.48		86.34	88.48
81.87		84.40	
7.11		sub grade	
		81.30	
		5.04	
		5.37	80.44
		Sub. Gr.	8.04
		81.62	80.50
		4.72	79.84
		3.58	
		3.29	
		83.90	83.00
		2.49	5.48
		2.77	
		84.48	
		1.86	
		2.19	
			87.33
			1.15
			0.36 cut-off
			103.87
			94.99
			8.89
			95.21
			3.58
			2.01
			96.23
			2.66
			2.99
			96.98
			6.89
			97.17
			1.72
			2.05
			97.88
			0.84
			7.17
			98.70
			5.17
			98.85
			0.04
			0.37

4+15.85

4+20

4+35.85

4+40

4+55.85

4+60

4+75.85

4+80

4+95.85

5+00

5+15.85 E.V.C. East

5+20 E.V.C. West

BM#A page A

6+93 Mid Curve on East

6+88<sup>2</sup> Mid Curve - West8+11<sup>2</sup> End Cb. East

8+39 " " West

109 108

$$\begin{array}{r} \pi \\ 107.76 \\ 2.77 \\ \hline 104.99 \\ 6.77 \\ \hline 111.68 \end{array}$$

$$\begin{array}{r} 27.66 \\ 9.92 \\ \hline 107.58 \\ 2.60 \\ \hline 104.98 \\ 7.10 \\ \hline 112.08 \\ 9.10 \\ \hline 104.98 \\ 6.77 \\ \hline 111.75 \end{array}$$

$$\begin{array}{r} \pi \\ 103.97 \end{array}$$

EAST

$$\begin{array}{r} 99.47 \\ 4.40 \\ \hline 100.16 \\ 3.71 \\ \hline 100.78 \\ 3.07 \\ \hline 101.34 \\ 2.53 \\ \hline 101.82 \\ 2.05 \\ \hline 102.25 \\ 1.62 \\ \hline 111.75 \end{array}$$

1/4

1/4

1/4

West

$$\begin{array}{r} 107.76 \\ 99.60 \\ 8.16 \\ 3.77 \\ \hline 8.47 \\ \hline 100.26 \\ 7.50 \\ 3.77 \\ \hline 7.83 \\ \hline 100.87 \\ 6.88 \\ 3.77 \\ \hline 7.22 \\ \hline 101.40 \\ 6.36 \\ 3.77 \\ \hline 6.69 \\ \hline 101.86 \\ 5.90 \\ 3.77 \\ \hline 6.23 \\ \hline 102.22 \\ 5.54 \\ 3.77 \\ \hline 5.87 \\ \hline 111.69 \\ 105.80 \\ 5.95 \\ 0.99 \text{ Curb Edge} \\ \hline 108.17 \\ 3.49 \\ 3.77 \\ \hline 3.82 \\ 1.82 \\ \hline 0.104 \\ \text{From top cb.} \\ \hline 0.2100 \end{array}$$

$$\begin{array}{r} 103.87 \\ 98.78 \\ 5.09 \\ \hline 99.44 \\ 4.43 \\ \hline 104.02 \\ 3.85 \\ \hline 100.53 \\ 3.31 \\ \hline 100.98 \\ 2.87 \\ \hline 101.42 \\ 2.45 \\ \hline 111.95 \\ 104.55 \\ 7.20 \\ \hline 107.12 \\ 4.38 \end{array}$$

Work Order  
288

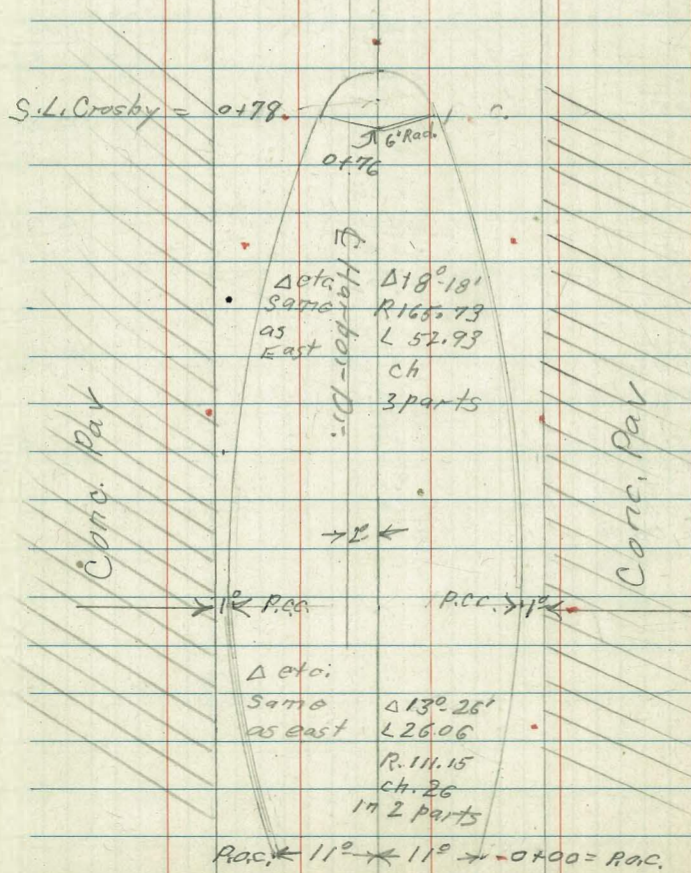
Island

Sommermeier  
W. Moore  
J Green

Mar. 7, 1947

INDEXED

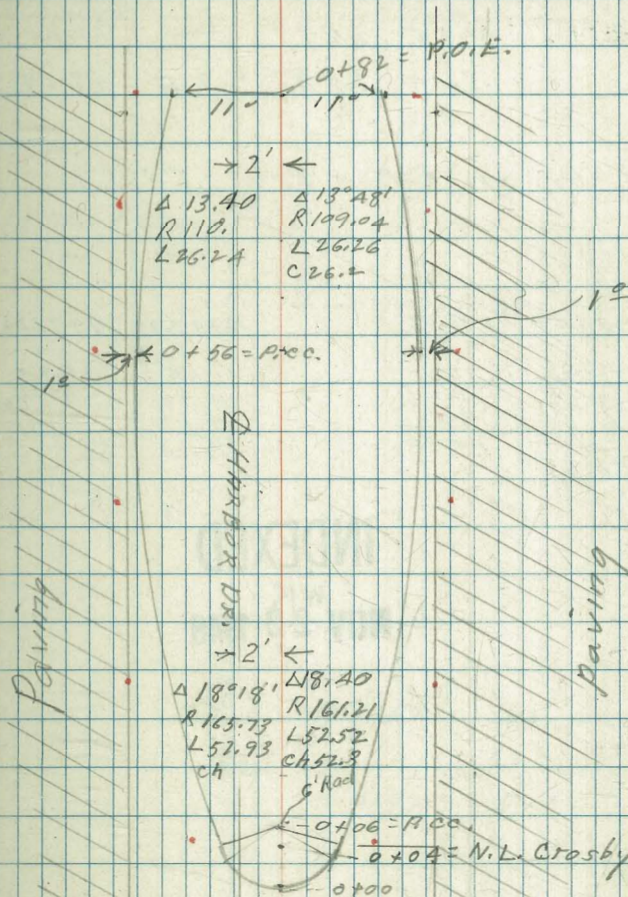
WK  
NOV 22 1948



Trafic Islands Crosby + Harbor Dr. 11

150' Rad. does not pass thru the 3 points noted on plan.

Therefore Islands staked as shown.



3/13/47 W.O. 262  
Check Culvert grades  
Mission Valley Golf Course

B.M. = 2x2 Hub F.B. 1670-48  
10.55 26.77 — 16.24  
3.14 20.83 9.10 17.69

Grades taken from 6875 L

1+14.29	1+86.29	4+57.29	4+97.29
12.61	12.35	11.06	10.94
8.22	8.48	9.77	7.87
8.47	8.56	9.57	Grade
80.25	80.08	80.20	

INDEXED  
WK  
NOV 22 1948

P.L. 1105

↓ Culverts

P.L. Line ————— 0+00

↑ 15 ↓

1+50.29 & Road

1+14.29 Beg. 63" cond. pipe

1+86.29 = End. 63" " "

M Line Camino Del Rio

4+57.29 - Beg. 60" corr. pipe

4+97.29 = End 60" " "

4-17-47  
 Sommermayer  
 W Moore  
 J Green

Stake sewer. BIK 3  
 Los Altos # 2 (54 ft. to East  
 150 So. Imperial)

B.M. =  $\Phi$ L+T

54 Imperial

FB17A7-20

		$\pi$ 165.64		
0+00	0+50	1+00	1+50	2+00
154.20	154.55	154.90	155.25	155.60
11.44	11.07	10.79	10.59	10.04
5.62	5.20	4.97	4.89	4.76
C 5.82V	C 5.89V	C 5.95V	C 5.50V	C 5.28V

$\pi$  165.44

		M.H. #1		M.H. #2
2+50	3+00	3+10	3+47.66	3+85.31
155.95	156.30	156.37	156.63	156.90
9.69	9.34	9.27	9.01	8.74
4.09	3.75	4.03	4.45	4.43
C 5.62V	C 5.59V	C 5.24V	C 4.56V	C 4.31V

T.P. 5.25 166.46 4.43 161.21

4+35.31 4+85.31 5+31.31 = D.E.

157.25	157.60	157.92
9.21	8.86	8.59
5.36	4.67	4.15
C 5.85V	C 4.19V	C 4.39V

orig B.M. 3.45 165.39 4.52 161.94  
 6.19 159.20 OK

Work Order 251 13

INDEXED  
 WIK  
 NOV 22 1948

B. sheet 3228

5+31.31 = D.E.

stakes set  
 6" So. sewer  $\Phi$

M.H. #2 = 3+85.31  
 $\Delta 10' 41" 48" \pi$

3+10 =  
 M.H. #1  
 $\Delta 10' 41" 48" \pi$

Imperial

$\Phi$ L+T 1505  
 54 1/2 St  
 M.H. = 0+00 1749/20



Mar. 31-47  
 Sommermejer  
 W. Moore  
 L. Melten  
 S. Bain

Stake change

S.L. La Playa = Sta. 296 + 53 ±

BM = N.E. P. R. Frontera + La Playa.

13.03 32.48

19.45

**INDEXED**

WIK

NOV 22 1948

Check on pipe as laid 4-7-47

12.87 32.32

19.45

Water Line Haines + La Playa.

14

B.M.					296
294 + 87.5	- 295 + 12.5	+ 37.5	+ 62.5	+ 87.5	+ 12.5
24.14	24.05	23.97	23.89	23.80	23.72
8.39	8.43	8.51	8.59	8.68	8.76
2.91	3.05	3.06	3.19	3.25	2.90
C 5.43	C 5.38	C 5.45	C 5.40	C 5.73	C 5.86

B.M.				B.M. - Join pipe
296 + 37.5	+ 50.2	+ 81.25	+ 12.00	297 + 37.5
23.64	23.60	23.92	24.20	25.29
8.84	8.88	8.58	8.28	7.79
2.61	2.47	3.86	3.68	5.51
C 6.23	C 6.39	C 4.72	C 4.60	C 5.68

Stakes set 10' E of pipe.

294 + 87.5	95 + 12.5	+ 37.5	+ 62.5	+ 87.5	+ 12.5
24.14	24.05	23.97	23.89	23.80	23.72
8.19	8.27	8.35	8.43	8.51	8.60
6.76	6.91	7.08	7.21	7.32	7.55
C 1.42	C 1.86	C 1.27	C 1.22	C 1.30	C 1.25

296					296
+ 37.5	+ 50	+ 81.25	+ 12.5	+ 37.5	+ 79.5
23.64	23.60	23.90	24.20	25.29	25.69
8.58	8.72	8.42	8.12	7.63	6.83
3.59	3.60	7.17	6.08	6.22	5.59
C 1.11	C 1.12	C 1.25	C 1.44	C 0.81	C 1.24
					5.07
					C 1.56

Stake Paving Alley BIK. CO. D.B.  
Bacon to Cable - Bet. Santa Monica + Newport.

0+00 = Elyline Bacon.

NE. B.P. Bacon + Newport		11.05	
		3.71	
		14.76	
		3.57	
2+80	$\frac{13.75}{5.09}$ 7.81 C 0.28	18.84	$\frac{13.75}{5.09}$ 3.09 C 2.00
			16.97
			2.57
			14.38
2+40	$\frac{13.35}{4.56}$ 4.28 F 0.02	17.71	$\frac{13.35}{4.56}$ 3.56 C 1.00
			3.57
			17.91
			19.38
			4.06
			18.84
			2.07
B.K. 2+00	$\frac{12.95}{4.96}$ 5.25 F 0.32	6.28	$\frac{12.95}{4.96}$ 4.96 C 0.96
			2.09
			3.17
			17.81
			3.81
			21.62
			5.17
1+50	$\frac{12.37}{5.52}$ 5.42 C 0.10	17.71	$\frac{12.38}{5.53}$ 5.57 F 0.06
			16.15
			4.70
			20.85
			4.92
			16.03
			5.01
1+00	$\frac{11.82}{5.15}$ 4.60 C 0.55	2.58	$\frac{11.81}{5.16}$ 3.16 C 2.00
			NE Cable
			Newport
0+50	$\frac{11.25}{5.72}$ 4.92 C 1.00 mail		$\frac{11.24}{5.73}$ 4.97 C 1.00 mail
0+00	$\frac{10.68}{4.28}$ 4.25 1.03		$\frac{10.66}{4.30}$ 4.28 1.02
			10.96

N.      ♀      S

6+00	$\frac{16.06}{5.78}$	15.78	$\frac{16.10}{5.52}$
5+80	$\frac{16.22}{5.40}$ 4.60 C 0.80	16.01	$\frac{15.93}{4.96}$ 4.96 C 1.00
			20.87
5+60	$\frac{16.31}{5.31}$ A 1.17 C 0.84	16.01	$\frac{16.01}{4.96}$ 4.96 C 1.00
			16.15
			2.75
5+40	$\frac{16.29}{5.53}$ 4.13 C 0.74	18.93	$\frac{15.97}{4.88}$ 4.88
			16.29
			5.33
			10.82
			C 1.00
5+20	$\frac{16.15}{5.47}$ 4.44 C 1.03	15.85	$\frac{16.15}{5.02}$ 5.02
			16.15
			5.47
			4.44
			C 1.00
4+80	$\frac{15.75}{5.23}$ 4.23 C 0.95		$\frac{15.75}{5.23}$ 5.23 C 1.00
			15.75
			5.23
			4.23
			C 1.00
4+40	$\frac{15.35}{5.63}$ 4.20 C 1.23		$\frac{15.35}{5.63}$ 5.63 C 1.07
			15.35
			5.63
			4.20
			C 1.07
4+00	$\frac{14.95}{6.03}$ 4.03 C 2.00	20.98	$\frac{14.95}{6.03}$ 6.03 5.04 C 0.94
			14.95
			6.03
			5.04
			C 0.94
3+60	$\frac{14.55}{4.27}$ 4.27 C 2.00		$\frac{14.55}{4.27}$ 4.27 3.22 C 1.07
			14.55
			4.27
			3.22
			C 1.07
3+20	$\frac{14.15}{4.67}$ 3.67 C 1.00	18.84	$\frac{14.15}{4.67}$ 4.67 3.96 C 0.77
			14.15
			4.67
			3.96
			C 0.77

N      ♀      S

INDEXED  
WK  
NOV 22 1948

New Town Park

Sommermejer  
W Moore  
L Melton

16

Blood Donor Center A-15-47

W.O #

SW.B.P. (1/2")  
+ Columbia 3.28 15.75 — 12.47

X-sec. Ground

N.E. Cor 3.5 12.25

SE Cor 3.8 11.95

NW Cor 5.5 10.25

S.W. Cor 5.8 9.95

**INDEXED**

WIK  
**NOV 22 1948**

Stakes set 3° off lines as shown on sketch.

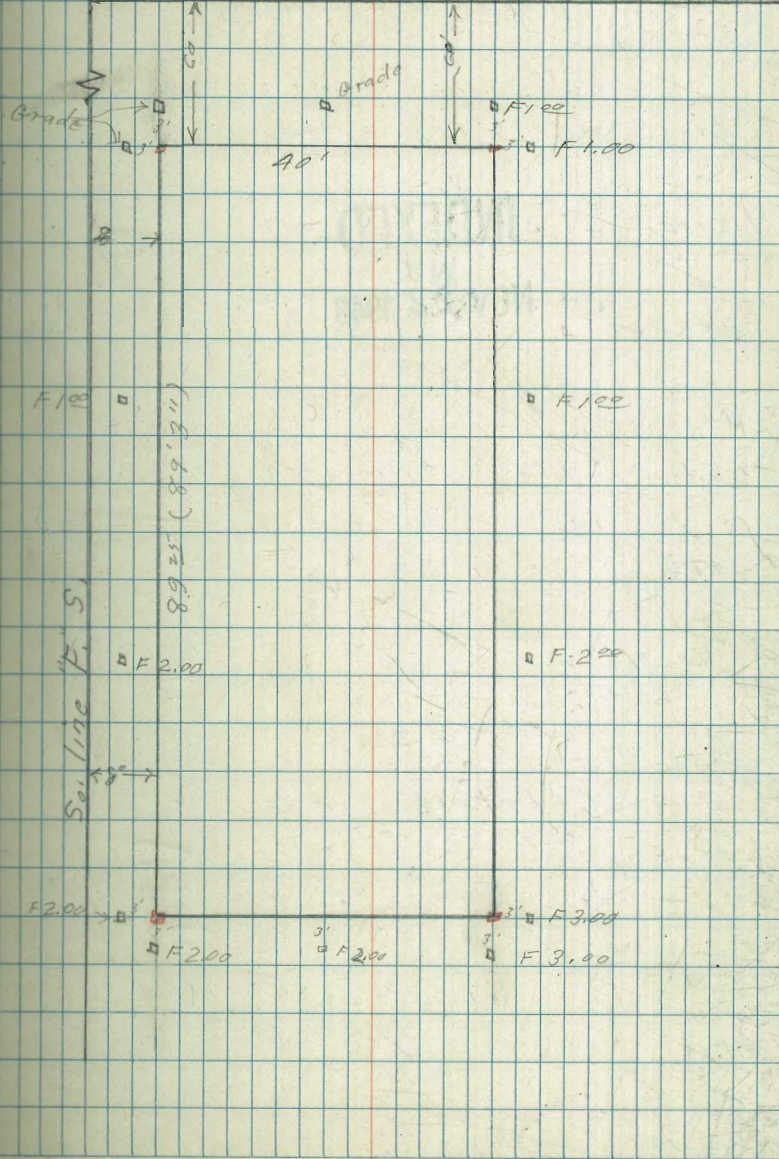
Also 2x2 R.W. Hubs set on Bldg. Corners.

Grade Est. 6" Above ground at N.E. Cor

Cuts + Fills as shown on sketch.

X 15.75  
Grade 12.75  
Gr. rod 3.00

W. Line Columbia



Alley BIK 322 Reed + Daley Add.  
 From 29 to 30 Bet. Clay + Webster  
 Orig grades @ 221-P. 55

Orig. Stakes - @ 221-55

3+00				
2+85	Sewer. lat. #3 N + #2-S.			
2+50				
2+00				
1+50				
T.P.	5.86	79.16	4.43	73.80
1+00				
+80	E.V.C.			
0+60				
T.P.	3.89	78.23	4.13	74.34
0+40				
0+33				
0+00	EL. 29 <sup>th</sup> St.			
SE.B.R	Clay + 29 <sup>th</sup>	0.42	78.47	78.05

INDEXED  
 WK  
 NOV 22 1948

5/19/47 Paving Grades BIK 322 Reed + Daley 17  
 N. S.

N.O. 31045

4.62 3.93 C 0.67	74.54	74.39 4.77 25 5.02	74.84	4.32 4.32 0.00
8.54 4.13 C 4.41	70.62 #3		#2 70.62	8.54 4.13 C 4.41
4.77 3.97 C 1.00	74.39	74.24 4.77 25 5.17	74.69	4.47 4.21 C 0.26
4.92 5.25 F 0.28	74.24	74.09 5.09 25 5.32 sub.G.	74.54	4.62 4.81 F 0.19
5.09 5.01 C 0.06	74.09	73.94 5.22 25 5.47	74.39	4.79 4.79 x
4.29 3.29 C 1.00	73.94 Nail	73.79 5.37 25 5.62	74.24 Nail	3.99 2.99 C 1.00
4.35 4.57 F 0.22	73.88	73.73 5.34 25 5.68	74.18	4.05 3.19 C 0.92
4.45 3.45 C 1.00 mil	73.78	73.63 5.58 25 5.78	74.08	4.15 4.15 0.00
4.93 4.67 C 0.26	73.54	73.46 5.70 25 5.95	73.91	4.56 4.36 0.00
5.27	73.30	73.10 6.05 25 6.36	73.50	4.97

6+20.05 W.L. 30<sup>th</sup> Pak

6+00

+ 80

+ 60 Sewer Lat. # 4 - South

5+40

T.P.

3.41 79.31  
2.17 78.09 3.57 75.90

5+20 P.V.C.

4+80 Sewer Lat. # 4

4+40 E.V.C.

+35 Sewer Lat. # 1/2 So.

+ 20

4+00 P.V.C.

3+50

4.65 79.47 4.34 74.82  
79.16

L.H.N.

4

Rt. 50.

18

7.06  
7.08  
72.25

71.63

72.21  
7.10  
7.14  
6.09 Rev.

6.32  
4.91  
72.79

72.48  
6.83 V

73.07  
6.24  
4.97  
6.12 V

5.66  
5.09  
6.66  
73.65

73.22  
6.09 V

73.83  
5.48  
4.67  
6.79 C

5.17  
4.19  
60.99  
74.14

73.21  
5.60 out

74.38  
4.93  
4.57  
6.01

4.86  
3.85  
6.00  
74.45

74.09  
5.27 V

74.74  
4.57  
4.15  
6.07

4.87  
3.92  
6.10  
74.60

74.20  
5.71 V

74.90  
4.57  
3.57  
6.40

4.75  
4.52  
6.10  
74.72

74.32  
4.99 V

75.02  
4.45  
3.11  
6.10

4.63  
4.41  
6.21  
74.84

74.44  
4.87 V

75.14  
4.33  
4.14  
6.19

4.60  
4.60  
6.21  
74.87

74.72  
4.75 V  
2.5  
5.00

75.17  
4.30  
3.94  
6.36

4.63  
4.27  
6.36  
74.84

74.69  
4.78 V  
2.5  
5.03

75.14  
4.33  
4.22  
6.10

4.78  
3.9  
6.30  
74.69

74.54  
4.73  
2.5  
5.18

74.99  
4.48  
3.60  
6.88

71.10  
5.37  
3.45  
6.47 V

Paving Grades Alley BIK 319 - Reed + Daleys Adol.  
 From 28<sup>th</sup> to 29<sup>th</sup> Bet. Clay + Webster.

Orig stakes @ 221- 53

+50

**INDEXED**

WK

NOV 22 1948

3 +00

T.P.

5.51

78.62

4.50

73.11

+50

2 +00

+50

1 +00

+80

EVC

+60

+40

+20

0 +00 E line 28<sup>th</sup>

B.M. - Top. Cl.  
 S. Line Alley  
 E Line 28<sup>th</sup>

171A-A1

5.66

77.61

71.95

N. Pav Gr

Sub  
 grade

S. Pav. Grade **1.9**

XXO.31045

73.42  
 5.19

74.13

4.49

3.49

C 1.00

73.28  
 5.34

73.98

4.64

3.28

C 1.36

73.13  
 4.48

73.83

3.78

1.78

C 2.22

72.98  
 4.63

73.68

3.73

2.54

C 1.07

72.88  
 4.78

73.53

4.08

3.08

C 1.00

72.68  
 4.93

73.38

4.23

3.76

C 0.47

72.62  
 4.97

73.32

4.29

3.51

C 0.77

72.42  
 5.17

73.17

4.49

3.82

C 0.64

72.15  
 5.96

72.85

4.76

3.30

C 0.86

71.66  
 5.95

72.36

5.25

3.97

C 1.28

71.00  
 6.61

71.70

5.91

73.83

4.79

4.40

C 0.99

73.68

4.84

3.28

C 1.11

73.53

4.08

2.96

C 1.12

73.38

4.23

C 1.12

73.23

4.38

3.38

C 1.00

73.08

4.53

3.02

C 1.51

73.02

4.57

4.11

C 0.48

72.87

4.74

3.74

C 1.00

72.55

5.05

3.83

C 1.23

72.06

5.55

4.31

C 1.24

71.40

6.21

S.E. B.P. Clay  
+2941.82 78.05 <sup>5.8</sup> 78.05

597. 79.87 5.01 73.90

5+99.50 W.L. 29<sup>th</sup>

+80

+60

+40

+20

5+00 P.V.C

T.R. 5.18 78.71 4.89 73.73

+50

+100

78.62

73.00

5.71  
5.41  
C 0.30

73.47

5.44  
4.90  
C 0.54

73.87

5.09  
4.52  
C 0.57

74.14

4.87  
4.80  
C 0.03

74.27

4.69  
3.64  
C 1.06

74.28

4.63  
4.82  
F 0.19

74.13

4.49  
4.77  
C 0.28

73.78

4.64  
4.64  
X

72.60

6.31  
2.1  
C 0.6

73.07

5.84  
C 0.6 = 5.7. B. -  
4.12. H.

73.47

5.44  
C 0.70

73.74

5.17  
C 0.73

73.87

5.04  
C 2.00

73.88

5.03  
C 1.00

73.73

4.87  
C 0.21

73.58

5.04  
C 1.01

73.30

5.61  
5.01  
C 0.60

73.77

5.14  
4.24  
C 0.90

74.17

4.74  
4.01  
C 0.73

74.44

4.47  
3.47  
C 2.00

74.57

4.34  
3.34  
C 1.00

74.58

4.33  
4.12  
C 0.21

74.43

4.19  
3.18  
C 1.01

74.28

4.34  
3.34  
C 1.00

Resurface Meade Fairmount  
to 32<sup>nd</sup> St. (Backed in) W.O. 60108

N.W.B.R.  
Bancroft + Meade  
FB 1296-79

6.53 377.45 377.44

INDEXED

0+00 = W.L. Bancroft,

WK

NOV 22 1948

Field books { 1746 - 15

1768 6-

1740 61-

1767 - 17

1296 - 79

0+40 =

1+07 = E.L. Alley to No. West of Bancroft.

2+46<sup>2</sup> = E.L. 32<sup>nd</sup>

2+58<sup>2</sup> = E.C. 32<sup>nd</sup>

2+67<sup>2</sup> = E 1/4 32<sup>nd</sup>

2+76<sup>2</sup> = 1/4 32<sup>nd</sup> Meet Pav.

FB 1296

1297

352

383.98

380.46

N.W.B.R.

Meade

32

N. 1/4 1/4 S. 1/4 S. 1/4 21

377.18 6.85 6.85 0.00	377.33 6.65 6.67 F0.02	377.30 6.68 6.73 F0.07	377.10 6.89 6.92 F0.04	376.65 7.33 7.31 6.02 Meet
377.70 6.28 6.28 0.00	377.89 6.09 6.18 F0.09	377.87 6.11 6.18 F0.07	377.63 6.35 6.40 F0.05	377.15 6.83 6.77 6.06 Meet
378.38 5.60 5.60	378.65 5.33 5.45 F0.12	378.67 5.31 5.39 F0.02	378.45 5.53 5.60 F0.07	378.98 6.00 5.99 6.01 Meet
379.71 4.27	380.07 3.91 4.01 F0.10	380.19 3.77 3.72 F0.13	380.07 3.91 4.11 F0.20	379.73 4.25
379.84 4.18 4.18 X	380.15 3.83 4.06 F0.23	380.20 3.78 4.09 F0.19	380.10 3.88 4.08 F0.15	379.86 4.12 4.09 4.1 Meet



Re-surfacing grades Meade Ave  
Fairmount to 32<sup>nd</sup>

INDEXED

2+50

2+00

1+50

1+00

0+50

0+10

0+00 W.L. Fairmount

0-10 W.Cb. Fairmount Meet Exist. Pav

T.P. P9023 4.15 353.09

348.94

Meade Ave  
S. 06. S 1/4 E N. 1/4 N.C. 22

<u>348.00</u> 5.09	348.23	348.22	347.82	<u>347.35</u> 5.74 ✓
-----------------------	--------	--------	--------	-------------------------

<u>348.23</u> 4.86 ✓		348.47	348.19	<u>347.09</u> 5.42 ✓
-------------------------	--	--------	--------	-------------------------

<u>348.46</u> 4.63 ✓		348.72	348.45	<u>347.94</u> 5.15 ✓
-------------------------	--	--------	--------	-------------------------

<u>348.69</u> 4.40 ✓		348.97	348.71	<u>348.21</u> 4.88 ✓
-------------------------	--	--------	--------	-------------------------

<u>348.92</u> 4.17 ✓	349.20	349.22	348.97	<u>348.48</u> 4.61 ✓
-------------------------	--------	--------	--------	-------------------------

<u>349.40</u> 3.69 3.84 F0.15	349.40 3.69 3.86 F0.23	<u>349.15</u> 3.97 4.14 F0.20
--	---------------------------------	--

<u>349.15</u> 3.94 ✓		<u>348.25</u> 4.34 ✓
-------------------------	--	-------------------------

S. 6.

S 1/4

4

N 1/4

N 66

0+20

3+26<sup>0</sup> = W.L. 43<sup>rd</sup> = 0+00

3+16<sup>0</sup> = W. Ch.L. 43<sup>rd</sup>

3+06<sup>0</sup> = W. 1/4-43<sup>rd</sup>

+96<sup>0</sup> = 4 43<sup>rd</sup>

+86<sup>0</sup> E 1/4-43<sup>rd</sup>

+76<sup>0</sup> = E. Ch. 43<sup>rd</sup>

2+66<sup>0</sup> = E.L. 43<sup>rd</sup>

T.P.	4.00	353.14	4.20	348.94	
			12.48	349.14	
2 W. 1/4 1/4 T.					
V. 1/4 Dyko +	2.47	361.62	-	359.15	F.R. 1/4 AC
Mead					P. 21

347.80				347.50
5.34L				5.64L
5.32				5.60
2.01L				
347.50	348.00	348.15	347.88	347.37
5.64L	5.14	4.99	5.26	5.77L
	5.25	5.19	5.38	
	F0.11	F0.15	F0.12	
347.47	348.02	348.15	347.85	347.28
5.67L	5.12	4.99	5.27	5.86L
	5.25	5.10	5.25	
	F0.13	F0.17	F0.17	
347.75R	348.04	348.15	347.81	347.21
5.39L	5.10	4.99	5.33	5.78L
	5.24	5.23	5.00	
	F0.11	F0.24	F0.27	
347.90	348.07	348.15	347.78	347.15
5.24	5.07	4.99	5.36	5.79L
5.25L	5.07	5.00	5.30	
	F0.12	F0.21	F0.20	
347.88R	348.10	348.15	347.74	347.08
5.26	5.04	4.99	5.40	6.06L
F0.04	5.17	5.22	5.36	
	F0.13	F0.22	F0.16	
347.77R	348.12	348.15	347.72	347.00
5.27L	5.02	4.99	5.42	6.14L
	5.13	5.20	5.61	
	F0.13	F0.21	F0.19	
347.72	348.18	348.15	347.70	346.90
5.21	4.96	4.99	5.44	6.27L
	5.10	5.12	5.59	
	F0.14	F0.13	F0.15	

			S. 06.	S 1/4	±	N 1/4	N. 06.
2+44 <sup>2</sup>			356.82 3.67 ✓	357.10	357.10	356.85	356.45 4.04 ✓
1+7A <sup>2</sup>			353.19 7.30 ✓		353.50	353.23	352.80 7.69 ✓
S.W. 1/4 Via Dyke + Meade	1.34	360.49	359.15	FB1746 P 21			
1+40 = W. L. Alley to So			351.35 1.79 1.94 Fo.15		351.80 1.34 1.56 Fo.22		351.29 1.85 ✓
1+25 E. line Alley to So			350.45 2.69 2.79 Fo.10		351.02 2.12 2.24 Fo.12		350.62 2.52 ✓
1+00			349.28 3.86 3.86 ✓		349.90 3.24 ✓		349.90 3.34 ✓
0+80			348.71 4.43 4.43 ✓		349.35 3.79 3.85 Fo.06		349.12 4.02 4.02 ✓
0+60			348.35 4.79 4.79 ✓		348.80 4.34 4.37 Fo.03		348.41 4.70 ✓
0+40			348.09 5.05 5.05 ✓				347.90 5.24 ✓

353.14

Sch. S 1/4. \$ N 1/4 N. Ch.

3424<sup>I</sup> = 0+00 W. Line Van Dyke

358.92	359.38	359.40	359.16	358.56 C
2.72V	2.24	2.22	2.96	3.06
	2.55	2.30	2.68	3.04
	F0.31	F0.28	F0.22	

3414<sup>I</sup> W. Ch. line Van Dyke

358.77	359.10	359.12	358.92	358.42 C
2.85	2.52	2.50	2.70	3.20 L
2.97	2.72	2.67	2.85	
F0.12	F0.20	F0.17	F0.18	

3404<sup>I</sup> = W. 1/4 Van Dyke

358.60	358.84	358.85	358.70	358.50 C
3.02	2.78	2.77	2.92	2.32 L
3.10	2.97	2.90	3.10	
F0.08	F0.19	F0.13	F0.18	

2494<sup>I</sup> = \$ Van Dyke

358.45	358.59	358.60	358.45	358.18 C
3.17	3.03	3.02	3.17	3.44 L
3.24	3.20	3.17	3.30	
F0.07	F0.17	F0.17	F0.13	

2484<sup>I</sup> = E. 1/4 Van Dyke

358.22	358.33	358.31	358.22	357.92 C
3.40	3.29	3.31	3.40	3.70 L
3.48	3.41	3.43	3.55	3.68
F0.04	F0.12	F0.12	F0.15	

2474<sup>I</sup> = E. Ch. Van Dyke

358.00	358.07	358.06	358.00	357.70 C
3.02	3.53	3.56	3.62	3.72 L
2.77	2.67	3.67	3.77	
F0.10	F0.12	F0.13	F0.15	

2464<sup>I</sup> = E. L. Van Dyke

357.77	357.82	357.81	357.78	357.37 C
3.85 L	3.50	3.51	3.84	4.25 L
	3.70	3.90	4.04	
	F0.10	F0.15	F0.20	

S.W. 7/4 +  
Van Dyke +  
Meads  
1746-11

2454<sup>I</sup>

357.90				357.00
--------	--	--	--	--------

Sid S/A  $\Phi$  N/A N/d.

NW. 42<sup>nd</sup> 4.  
Meade 5.19 369.79 4.69 364.60

1+25

364.00	364.70	364.40	364.27	363.92
5.29	4.79	4.89	5.02	5.37
	F 1.14	4.95	5.21	5.37
	F 0.13	10.07	F 0.19	

0+15 = 15' W. W.L. Copeland

363.62	363.91	364.00	363.90	363.36
5.67	5.38	5.29	5.29	5.73
	5.51	F 0.22	5.52	
	F 0.13		F 0.23	

3+25<sup>L</sup> W.L. Copeland

363.53	363.85	363.93	363.82	363.50
5.76	5.44	5.36	5.47	5.77
	5.50	5.57	5.68	
	F 0.13	F 0.21	F 0.21	

Rake Intersection  
Except N. cb. line. meet pav. there

2+65<sup>L</sup> = E.L. Copeland

363.32	363.43	363.70	363.50	363.20
5.97	5.86	5.59	5.79	6.09
	5.86	5.94	5.94	
	F 0.15	F 0.15	F 0.20	

Copeland + Meade 4.84 369.29 364.65 NW. B.R. 1746-24

2+50<sup>L</sup>

Rake

364.01	362.50	363.58	363.37	362.91
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1+50

Rake

361.80	362.07	362.07	361.84	361.35
--------	--------	--------	--------	--------

0+20

361.62

359.62	359.90	359.92	359.65	359.12
2.00	1.72	1.70	1.77	2.50
2.00	1.90	1.93	2.25	
	F 0.10	F 0.23	F 0.29	

Copeland + Meade 361.62 362.45 NW. B.R. 1746-24

2+65<sup>2</sup> = E.L. Marlborough  
 NWBR {  
 FB1745-28Pake 527 371.29 366.02 Marlboro + Maale  
 {  
 = 0400  
 3+30<sup>2</sup> = W.L. 42<sup>nd</sup>

+15<sup>2</sup> = W. Cl. line 42

3+02<sup>2</sup> = W. 1/4 - 42<sup>nd</sup>

+90<sup>2</sup> =  $\phi$  - 42<sup>nd</sup>

+77<sup>2</sup> = E. 1/4 - 42<sup>nd</sup>

+65<sup>2</sup> = E. Cl. 42<sup>nd</sup>

2+50<sup>2</sup> = E.L. 42<sup>nd</sup>

369.77

S. cl.	S 1/4	$\phi$	N 1/4	N. cl.
365.60 5.69 L	365.90 5.39 5.34 C 0.05 L	365.90 5.39 5.34 C 0.04 L	365.75 5.54 5.65 F 0.11	365.85 5.79 L
364.90 5.09 5.06 L	365.17 4.62 4.59 L	365.22 4.57 4.58 L	364.94 4.83 4.70 F 0.05	364.38 5.71 L
G	365.10 4.69 4.66 C 0.03 L	365.16 4.63 4.67 F 0.04	364.90 4.89 4.85 F 0.16	364.30 5.49 5.47 L
G	365.06 4.73 4.68 F 0.04	365.09 4.70 4.72 F 0.03	364.95 4.94 4.86 F 0.12	364.26 5.53 5.57 F 0.05
G	365.02 4.77 4.72 F 0.06	365.02 4.77 4.84 F 0.05	364.90 4.97 4.92 F 0.13	364.22 5.57 5.54 F 0.03
B	364.95 4.84 4.82 L	364.96 4.83 4.84 F 0.06	364.95 5.04 5.17 F 0.13	364.20 5.59 F 0.01
G	364.88 4.71 4.71 L	364.70 4.69 4.75 F 0.03	364.70 5.09 5.22 F 0.17	364.18 5.61 3.61 L
364.42 5.57 L	364.78 5.01 5.07 F 0.06	364.83 4.96 5.00 F 0.04	364.63 5.16 5.24 F 0.03	364.20 5.59

2+50 = 15' E. E. Line 41<sup>st</sup>.  
 Meads  
 + Central 3.01 372.31 — 368.70 N.W.B.P.  
 F.B. 1946  
 R. 32

0+70

0100  
 3+25<sup>2</sup> = W. L. Marlborough

+15<sup>3</sup> = W. Cl. Marl.3+05<sup>3</sup> = N. 1/4 Marl+95<sup>3</sup> ♀+85<sup>3</sup> E. 1/4 Marl2+75<sup>3</sup> E. Cl. Marl.

371.29

S. Cl	S 1/4	♀	N 1/4	N. Cl.
367.60 4.71 ✓	367.84 4.47 4.37 F 0.10	367.84 4.47 4.47 F 0.01	367.58 4.73 4.21 F 0.18	367.06 5.25 ✓
366.40 4.87	366.70 4.59 4.22 F 0.15	366.72 4.57 4.72 F 0.13	366.50 4.79 5.00 F 0.21	366.00 5.29 ✓
365.68 = ♀	366.28 3.01 3.12 F 0.11	366.28 3.01 3.16 F 0.15	366.10 3.14 3.27 F 0.19	365.60 = ♀ 5.09
♀	366.21 5.08 5.10 F 0.10	366.21 5.08 5.22 F 0.14	366.05 5.24 5.03 F 0.19	♀
♀	366.15 5.14 5.18 F 0.04	366.15 5.14 5.23 F 0.09	365.99 5.30 5.46 F 0.16	♀
♀	366.09 5.20 5.25 F 0.02	366.09 5.20 5.23 F 0.03	365.93 5.36 5.48 F 0.12	♀
♀	366.02 5.27 5.33 F 0.09	366.02 5.27 5.24 F 0.09	365.87 5.42 5.28 F 0.16	♀
♀	365.96 5.33 5.33 x	365.96 5.33 5.39 F 0.06	365.81 5.48 5.62 F 0.15	♀

S.C.	S 1/4	E	N 1/4	N.C.
367.40 4.71	367.98 4.53 4.81 F0.28	367.95 4.36 4.42 F0.11	367.82 4.47 4.67 F0.18	367.50 4.81 4.86 F0.05
367.20 5.11	367.32 4.77 5.08 F0.09	367.53 4.78 4.89 F0.11	367.44 4.87 4.83 C0.02	367.24 5.07
367.18 5.13 2.27 F0.24	367.19 5.12 3.34 F0.22	367.20 5.11 5.24 F0.13	367.21 5.10 3.22 F0.12	367.22 5.09 5.13 F0.04
367.32 4.97 4.95 X	367.37 4.84 4.91 X	367.37 4.94 4.92 X	367.40 4.91 4.91 X	367.39 4.72 4.87 F0.11
G	357.70 4.61 4.69 F0.02	357.68 4.63 4.62 X	357.64 4.67 4.67 X	357.62 4.69 4.69 X
G	367.81 4.57 4.54 F0.04	367.75 4.56 4.56 X	367.72 4.59 4.66 F0.07	367.64 4.67 4.67 X
G	367.82 4.47 4.47 C0.02	367.80 4.51 4.51 C	367.65 4.66 4.66 C0.01	G
367.68 4.63	367.80 4.51 4.50 C .11	367.82 4.51 4.59 C0.12	367.60 4.71 4.68 X	367.14 5.17

0+45

-0400  
3+25 W. Line 41<sup>st</sup>

+15 = W.C.

3+05 = W 1/4

+95 = E 41<sup>st</sup>

+85 = E. 1/4

+75 = E.C.

3770 N. Gut. of Meade only

2+65 = E. L. 41<sup>st</sup>

372.31



= 0+00

3+25<sup>10</sup> = Vx. line Central3+13<sup>10</sup> = W. Cb. Line Central+95<sup>L</sup> =  $\Phi$  Central+77<sup>L</sup> = E. Cb. Central2+65<sup>10</sup> = East. Line Central2+45<sup>10</sup> = 20'E. K.L. Cent.

4.32 373.02 3 61 368,70

1+35

372.31

S.Cb.	S 1/4	$\Phi$	N 1/4	N.Cb.
<u>367.85</u> 5.17 ✓	<u>368.10</u> 4.92 4.94 F0.02	<u>368.26</u> 4.76 4.73 C0.03 X	<u>367.90</u> 4.72 4.80 F0.08	<u>368.27</u> 4.75 ✓
<u>367.80</u> 5.22 5.42 F0.20	<u>367.90</u> 5.12 5.37 F0.25	<u>368.00</u> 5.02 5.17 F0.15	<u>368.10</u> 4.92 5.08 F0.12	<u>368.20</u> 4.82 4.90 F0.08
<u>368.00</u> 5.02 5.43 F0.41	<u>368.00</u> 5.02 4.97 C0.05 X	<u>368.00</u> 5.02 4.87 C0.15 X	<u>368.20</u> 4.82 4.77 C0.05 X	<u>368.30</u> $\Phi$ 4.72 4.80 C0.06 X
<u>367.40</u> 5.62 5.60 F0.19	<u>367.70</u> 5.22 5.20 F0.24	<u>367.80</u> 5.22 5.27 F0.27	<u>367.90</u> 5.12 5.58 F0.26	<u>367.92</u> 5.10 5.21 F0.11
<u>367.43</u> 5.59 ✓	<u>367.80</u> 5.22 5.26 F0.19	<u>367.95</u> 5.07 5.05 C0.05 X	<u>368.02</u> 5.00 5.20 F0.10	<u>368.00</u> 5.02 ✓
<u>367.50</u> 5.52 ✓	<u>367.95</u> 5.07 5.31 F0.24	<u>368.20</u> 4.82 5.04 F0.22	<u>368.20</u> 4.82 5.08 F0.26	<u>367.95</u> 5.07 ✓
<u>367.70</u> 4.61 4.71 F0.10	<u>368.00</u> 4.31 4.50 F0.19	<u>368.15</u> 4.16 4.39 F0.23	<u>368.03</u> 4.28 4.42 F0.21	<u>367.68</u> 4.68 4.71 F0.08

S. Cl.    S 1/4    E    N. 1/4    N. Cl.

3+20 = W. 1/4 40th

3+05 = E. 40th

+90 E. 1/4

2+75 = E. Cl. 40th

2+65 = E. L. 40th

N.W. 1/4 L+T  
Meadow 40th

272 372.60

369.88

F.B. 1768  
P. 6

1+25 = E. L. Alley

1+25 out

0+20 = 20' W. W. L. Central

373.02

G 4.26 Rod	G 4.22 Rod	368.88 3.72 <u>3.12</u> X	G 3.39 Rod	G 3.18 Rod
G 4.03 Rod	G 3.77 Rod	G 3.57 Rod	G 3.25 Rod	G 3.04 Rod
G 4.10 Rod	368.76 F 3.89	369.10 3.56 3.62 F 0.12	369.278 3.33 X	369.47 3.13 3.12 X
367.95 4.65 4.97 F 0.12	368.70 3.70 4.41 F 0.51	369.19 3.47 4.00 F 0.53	369.26 3.34 3.76 F 0.22	367.10 3.50 3.60 F 0.16
367.90 4.70	368.69 3.97 4.44 F 0.53	369.15 3.45 3.81 F 0.36	369.25 3.35 3.01 F 0.26	367.05 3.55
369.28 4.74	368.75 4.27 4.43 F 0.16	369.00 4.02 4.19 F 0.08	368.93 4.09 4.43 F 0.14	368.66 4.36
367.95 5.07	368.46 4.56 4.89 F 0.28	368.72 4.30 4.54 F 0.24	368.71 4.31 4.60 F 0.29	368.46 4.57

		S. cl.	S 1/4	¢	N. 1/4	N. cl.
2+95 = E - 3974	Rod. Readings	4.75 G	4.57 G	4.53 G	4.45 G	4.34 G
2+85 E 1/4	Rod. Readings	4.84 - G	4.82 G	4.75 G	4.63 G	4.53 G
2+75 E. cl.		368.45 5.43 5.41 0.01	368.75 5.13 5.25 F0.13	368.92 4.96 5.02 F0.09	368.95 4.93 5.01 F0.08	368.99 4.94 4.91 x
2+65 = E.L. 3974		368.46 5.42	368.85 5.03 5.05 F0.02	369.05 4.83 4.87	369.03 4.85 4.86	369.20 4.88
2+50 Brk NW8P39+ meade 1768-7	A.13 373.88	368.42 5.46	368.85 5.03 5.12 F0.19	369.10 4.78 4.88 F0.14	369.15 4.73 4.81 F0.08	369.22 4.86
1+00 Brk		367.90 4.70	368.65 3.95 4.26 F0.31	369.08 3.52 3.77 F0.19	369.25 3.35 3.58 F0.28	369.13 3.47
0+00 3+45 = W.L. 4074		367.70 4.70	368.40 4.20 4.50 F0.30	368.95 3.65 3.89 F0.24	369.17 3.43 3.59 F0.16	369.05 G 3.55
3+35 = W. cl. 4074	372.60	367.73 4.87 5.00 F0.13	368.20 4.40 4.57 F0.11	368.75 3.85 4.09 F0.24	369.00 3.60 3.72 F0.12	G 357 Rod.

(See page 58  
for restake on  
New patch fill)

2+65 = E.L. 38th

2+50

N.W. B.P. Meade + 38  
F.R. 1768-10

374.30

1+25 = E.L. Alley - W. of 39th

0+50

0+25

= 0+00

3+25 = W. Line 39th

3+15

W. Cb. 39th

N.L.	N-50B+K	N-100
369.28	369.61	369.81
4.60L	4.2%	4.07L

3+05

W 1/4

5.36	5.10	5L
368.50	368.63	368.77
5.38	5.25	5.11
5.40	5.35	5.30
F0.02	F0.10	F0.19

W. Cb. line sd. of  
Meade

373.88

S cb.	S 1/4	4	N 1/4	N Cb.
372.25 7.17L	372.80 6.62 6.70 F0.08	373.22 6.20 6.27 F0.07	373.25 6.17 6.24 F0.07	373.22 6.20L
372.07 7.35L	372.65 6.77 6.85 F0.08	373.07 6.35 6.45 F0.10	373.10 6.32 6.32 F0.10	373.00 6.42L
				371.14 274 274L
		370.15 3.77 3.86 F0.13	370.20 3.68 3.81 F0.13	
				369.30 4.38 4.30 F0.08L
368.90 4.98L	369.10 4.78 4.88 F0.10	369.30 4.58 4.68 F0.10	369.23 4.65 4.76 F0.11	369.25 4.63L
368.85 4.43 5.16 F0.13	369.00 4.88 5.09 F0.21	369.15 4.73 4.95 F0.26	369.18 4.70 4.95 F0.25	369.41 4.67 4.89 F0.22
369.00 4.88 4.93 x	369.16 4.72 4.79 F0.07	369.22 4.66 4.78 F0.07	369.28 4.60 4.65 F0.05	369.38 4.50 4.59 F0.09

S.C.

S 1/4

E

N 1/4

N.C. 84

2+00 N 1/4 only

$$\begin{array}{r} 375.75 \\ 3.63 \\ 3.87 \\ \hline 70.24 \end{array}$$

1+00 N 1/4 only

$$\begin{array}{r} 374.88 \\ 4.54 \\ 4.00 \\ \hline 80.06 \end{array}$$

$$\begin{array}{r} 0+00 \\ 3725^L = \text{W. Line } 38^{\text{th}} \end{array}$$

$\begin{array}{r} 372.95 \\ 6.47 \\ \hline \end{array}$	$\begin{array}{r} 373.46 \\ 5.96 \\ 6.17 \\ \hline 12.13 \end{array}$	$\begin{array}{r} 373.83 \\ 5.57 \\ 5.93 \\ \hline 11.50 \end{array}$	$\begin{array}{r} 373.90 \\ 5.52 \\ 5.02 \\ \hline 10.54 \end{array}$	$\begin{array}{r} 373.87 \\ 5.55 \\ \hline \end{array}$
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2+13<sup>L</sup> W. cb.

$\begin{array}{r} 372.80 \\ 6.72 \\ 6.62 \\ \hline \end{array}$	$\begin{array}{r} 373.33 \\ 6.09 \\ 6.34 \\ \hline 12.43 \end{array}$	$\begin{array}{r} 373.13 \\ 5.69 \\ 6.07 \\ \hline 11.76 \end{array}$	$\begin{array}{r} 373.78 \\ 5.69 \\ 5.27 \\ \hline 10.96 \end{array}$	$\begin{array}{r} 373.72 \\ 5.70 \\ 5.84 \\ \hline 11.54 \end{array}$
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3+03<sup>E</sup> W. 1/4 roadway

6.70 G	$\begin{array}{r} 373.22 \\ 6.20 \\ 6.25 \\ \hline 12.45 \end{array}$	$\begin{array}{r} 373.63 \\ 5.79 \\ 5.93 \\ \hline 11.72 \end{array}$	$\begin{array}{r} 373.67 \\ 5.74 \\ 5.90 \\ \hline 11.64 \end{array}$	$\begin{array}{r} 373.70 \\ 5.72 \\ 5.92 \\ \hline 11.64 \end{array}$
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2+94<sup>L</sup> E - 38<sup>th</sup> roadway

6.77 G	$\begin{array}{r} 373.10 \\ 6.32 \\ 6.22 \\ \hline 12.54 \end{array}$	$\begin{array}{r} 373.53 \\ 5.89 \\ 5.90 \\ \hline 11.79 \end{array}$	$\begin{array}{r} 373.56 \\ 5.86 \\ 5.89 \\ \hline 11.75 \end{array}$	5.77 G
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2+84<sup>E</sup> E 1/4 Roadway

6.62 G	$\begin{array}{r} 373.01 \\ 6.41 \\ 6.40 \\ \hline 12.81 \end{array}$	$\begin{array}{r} 373.43 \\ 5.99 \\ 6.10 \\ \hline 12.09 \end{array}$	$\begin{array}{r} 373.45 \\ 5.97 \\ 6.00 \\ \hline 12.07 \end{array}$	5.82 G
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2+75<sup>L</sup> = E. cb. 38<sup>th</sup>

6.74 G	$\begin{array}{r} 372.94 \\ 6.48 \\ 6.58 \\ \hline 13.06 \end{array}$	$\begin{array}{r} 373.33 \\ 6.09 \\ 6.20 \\ \hline 12.29 \end{array}$	$\begin{array}{r} 373.35 \\ 6.07 \\ 6.18 \\ \hline 12.25 \end{array}$	6.03 G
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= 0400  
3+25 = W.L. McClintock

S 1/4	S 1/4	E	N 1/4	IVC.
376.62 5.64	376.90 5.39 5.47 F0.08	377.17 5.12 5.17 F0.05	377.17 5.12 5.19 F0.07	376.87 5.42

3+13 W. Cb.

376.45 5.84 5.84 x	376.98 5.51 5.87 F0.06	377.05 5.24 5.45 F0.21	377.03 5.26 5.47 F0.21	376.77 5.52 5.50 6.02
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3+04 = W 1/4

G 5.73 5.60 5.65 F0.05	376.89 5.37 5.46 F0.09	376.92 5.37 5.46 F0.09	376.89 5.40 5.58 F0.18	376.70 5.39 5.59 F0.20
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2+95 = E McClintock

G 5.76 5.77 5.75 F0.02	376.86 5.49 5.63 F0.16	376.90 5.49 5.63 F0.16	376.75 5.54 5.69 F0.15	376.64 5.65 5.67 F0.02
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2+86 = E 1/4

G 6.03 5.85 5.70 F0.05	376.44 5.61 5.78 F0.12	376.68 5.61 5.78 F0.12	376.62 5.67 5.88 F0.13	376.43 5.86 5.84
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2+77 = E. Cb.

G 6.24 5.96 6.10 F0.14	376.33 5.77 5.88 F0.16	376.57 5.77 5.88 F0.16	376.49 5.80 5.94 F0.14	376.22 6.07 6.04
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2+65 = E.L. McClintock

375.80 6.49	376.22 6.07 6.26 F0.19	376.45 6.84 6.93 F0.19	376.35 5.94 6.10 F0.16	376.00 6.29
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2+50 out

N.W.B.P. Meade  
McClintock 4.99 382.29 — 377.30

3.41 384.25  
3+33L = W. Cb. 37 to So

+19L = V 1/4 to So

3+05L = E 37th to So.

2+65L = E.L. 37th to South.  
BM - NWBR Cherokee + Meade 3A1 387.66 — 384.25 PR 1769 P 16

1+89 W. W. Line 37th to No. (N. Out. ...)

1+73  
1+71 W Cb. to North.

1+53 = E 37th to No

1+23 E.L. 37 to No

0+50

382.29

S.Cb.	S 1/4	E	N 1/4	N.Cb.
G 597	381.95 5.71 5.91 FR.20	382.27 5.39 5.48 FR.09	382.13 5.51 5.66 FR.15	381.97 5.89 5.95 FR.06
G 601	381.80 5.86 6.03 FR.22	382.20 5.46 5.80 FR.34	382.05 5.61 5.97 FR.36	G 605
G 635	381.63 6.03 6.31 FR.27	381.84 5.82 6.13 FR.31	381.77 5.89 6.11 FR.28	G 631
380.25 7.38 7.53 FR.15	380.95 6.71 7.10 FR.39	381.25 6.41 6.60 FR.19	381.27 6.39 6.65 FR.26	380.70 6.76 6.80 FR.04
379.10 5.79	379.80 2.49 2.30 FR.35	380.15 2.14 2.36 FR.22	380.22 2.07 2.34 FR.23	379.90 2.39
378.97 3.32	379.65 2.64 3.03 FR.37	380.00 2.29 2.44 FR.15	380.05 2.22 2.40 FR.16	379.80 2.79 2.48 FR.01
378.75 3.54	379.38 2.71 3.27 FR.32	379.75 2.54 2.67 FR.08	379.80 2.49 2.76 FR.21	G 258
378.35 3.94	378.97 3.32 3.50 FR.24	379.38 2.66 2.84 FR.17	379.54 2.65 2.82 FR.20	379.33 2.76
377.30 4.99	377.75 4.54 4.90 FR.06	378.17 4.12 4.17 FR.05	378.25 4.04 4.19 FR.10	378.07 4.22

T.P.

+77<sup>2</sup> L. Cb21  
2+65<sup>2</sup> E.L. Cherokee to So

5.77 390.02 4.17 384.25

1462<sup>E</sup> W.L. Cherokee to No

1735 B.K

1+23<sup>E</sup> B.K E 1/4 cher. to No1+02<sup>E</sup> E.L. Cherokee to No

0+50 So Cb. B.K.

= 0+00

3+45<sup>L</sup> = W.L. 37<sup>th</sup>. to South4.17 388.42

384.25

384.60 5.42 <u>3.80</u> F0.08	384.82 5.24 5.22 <u>5.22</u> F0.22	384.91 5.11 5.18 <u>5.18</u> F0.07	384.85 5.17 5.24 <u>5.24</u> F0.07	384.47 5.55
384.53 5.49	384.75 5.27 5.50 <u>5.27</u> F0.27	384.84 5.18 5.27 <u>5.27</u> F0.07	384.79 5.23 5.42 <u>5.42</u> F0.19	384.40 5.62
383.25 5.17	383.72 4.70 4.81 <u>4.81</u> F0.21	383.90 4.52 4.58 <u>4.58</u> F0.06	383.99 4.49 4.68 <u>4.68</u> F0.19	383.80 4.62
383.00 5.42 5.48 <u>5.48</u> F0.06	383.47 4.95 5.21 <u>5.21</u> F0.26	383.63 4.77 4.82 <u>4.82</u> F0.10	383.72 4.70 4.88 <u>4.88</u> F0.19	G 497
382.95 5.47	383.43 4.99 5.27 <u>5.27</u> F0.30	383.61 4.81 5.01 <u>5.01</u> F0.22	383.67 4.75 4.98 <u>4.98</u> F0.23	5.04 5.10 <u>5.10</u> F0.06
382.60 5.82	383.10 5.32 5.53 <u>5.53</u> F0.21	383.32 5.10 5.27 <u>5.27</u> F0.07	383.33 5.09 5.26 <u>5.26</u> F0.17	383.10 5.32
381.65 6.77	382.10 6.32 6.54 <u>6.54</u> F0.22	382.34 6.58 6.19 <u>6.19</u> F0.11	382.25 6.17 6.30 <u>6.30</u> F0.13	381.85 6.87

388.42



2465 = E.L. 36<sup>th</sup> to SouthT.P. 543 391.71 3.74 386.281432<sup>E</sup> =  $\Phi$  36<sup>th</sup> st. to North

= 0400

3425<sup>W</sup> W.L. Cherokee to So.3413<sup>W</sup> W cl. Cherokee to So3404<sup>W</sup> W 1/42495<sup>W</sup>  $\Phi$ 2486<sup>E</sup> E 1/4 Cherokee to So.390.02

386.43 5.28L	386.80 4.71 5.25 F0.34	387.00 4.71 4.74 F0.23	386.90 4.81 4.78 F0.17	386.65 5.06L
385.65 4.37 4.36 F0.01L	385.91 4.11 4.37 F0.26	386.13 3.89 4.08 F0.19	386.02 4.00 4.06 F0.06	385.80 4.22L
384.83 5.19L	385.15 4.87 5.12 F0.25	385.25 4.77 4.88 F0.11	385.17 4.85 5.01 F0.16	384.80 5.22L
384.85 5.17 5.23 F0.06	385.109 4.93 5.13 F0.20	385.19 4.83 4.93 F0.10	385.11 4.91 5.00 F0.09	384.74 5.28L
G 5.15	385.02 5.00 5.23 F0.23	385.42 4.90 4.97 F0.05	385.05 4.97 4.97 F0.02	384.67 5.35 5.39 F0.04
384.78 5.24 5.33 F0.09	384.95 5.07 5.20 F0.23	385.05 4.97 5.05 F0.08	384.98 5.04 5.14 F0.10	384.60 5.42 5.51 F0.09
384.70 5.32 5.37 F0.05	384.89 5.11 5.33 F0.22	384.98 5.04 5.09 F0.03	384.91 5.11 5.18 F0.07	384.54 5.48L



0-68 E.C.B 35<sup>th</sup> to No

S 06.	S 1/4	Q	N 1/4	N 40
386.42	386.60	386.75	386.77	386.89
5.61	5.48	5.28	5.26	5.23
5.64	5.64	5.39	5.28	3.38
F0.03	F0.21	F0.11	F0.02	F0.10

0-80 2+65 E.L. 35<sup>th</sup> to No

386.40	386.84	387.05	387.05	386.82
5.63	5.19	4.98	4.98	5.21
	5.40	5.00	4.98	
	F0.21	F0.06	X	

NW 1/4 35<sup>th</sup>  
+ Meade  
FB 1740 AC 4.86 392.03 - 387.17

		392.03		
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1+40 Brk

386.81	387.22	387.43	387.44	387.25
5.17	4.76	4.55	4.54	4.73
	5.05	4.66	4.57	
	F0.29	F0.11	F0.05	

468 391.98 5.24 387.30

0+00 3+25 W.L. Wilson to South

387.11	387.70	387.95	387.88	387.50
5.43	4.84	4.59	4.66	5.04
	5.16	4.65	4.66	
	F0.32	F0.06		

2+95 Q Wilson to South

387.60	387.87	388.05	387.91	387.56
4.74	4.67	4.49	4.63	4.98
	5.02	4.72	4.83	5.04
	F0.35	F0.23	F0.20	F0.04

2+65 E.L. Wilson to South

387.45	387.83	388.00	387.94	387.52
5.09	4.71	4.54	4.64	5.02
	4.94	4.67	4.63	5.00
	F0.23	F0.13	L	0.02

392.54

	S 06.	S 1/4.	☒	N 1/4.	N 06.
0+15 = 15' W. W.L. 35 <sup>th</sup>	386.45 5.58	386.84 5.19 5.44 F0.25	387.05 4.98 5.23 F0.25	387.08 4.95 5.34 F0.39	386.92 5.11
0+00 W.L. 35 <sup>th</sup> <span style="border: 1px solid black; border-radius: 50%; padding: 2px;">OMIT</span> →	386.40 5.63 5.67	386.65 5.38 5.50 F0.12	386.82 5.71 5.20 C0.01	386.90 5.13 5.20 F0.07	386.88 5.18 5.14 C0.01
0-12 W 06.35	386.37 5.66 5.75 F0.09	386.60 5.43 5.67 F0.11	386.75 5.28 5.57 F0.27	386.80 5.23 5.44 F0.21	386.85 5.18 5.35 F0.17
0-26 W 1/4 35	G <sup>5.15</sup>	G <sup>5.07</sup>	G <sup>4.96</sup>	G <sup>4.86</sup>	G <sup>4.76</sup>
0-40 ☒ 35 <sup>th</sup> to	G <sup>5.09</sup>	G <sup>5.02</sup>	387.17 4.86 4.75 F0.09	G <sup>4.78</sup>	G <sup>4.67</sup>
0-54 E 1/4	G <sup>5.14</sup>	G <sup>5.08</sup>	G <sup>4.98</sup>	G <sup>4.87</sup>	G <sup>4.84</sup>

S. ob. S 1/4 § N 1/4 N. ob.

3713 W ob. Swift to So

G	387.30 4.11 4.41 Fo.30	387.45 3.70 4.31 Fo.35	387.32 4.19 4.53 Fo.14	387.10 G 4.81 4.58 Fo.07
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3704 W 1/4

G	387.40 4.21 4.17 Fo.20	387.53 3.88 4.12 Fo.24	387.50 3.91 4.02 Fo.13	387.42 G 3.99 4.09 Fo.05
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2795 § Swift

G	387.25 2.16 2.11 Fo.105	387.50 F 0.91 4.17 Fo.26	387.60 3.81 4.00 Fo.19	387.65 3.70 3.92 Fo.16	387.68 G 3.93 3.99 Fo.06
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+86 E 1/4

G	387.53 3.88 4.17 Fo.25	387.65 3.70 3.93 Fo.17	387.71 3.70 3.92 Fo.22	387.73 G 3.68
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+77 E. ob.

G	387.23 4.18	387.55 3.86 3.95 Fo.09	387.70 3.71 3.89 Fo.29	387.76 3.65 3.85 Fo.20	387.75 G 3.66 3.62 Fo.04
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+65 East Line Swift to So.

G	387.20 4.21	387.53 3.88 3.97 Fo.09	387.75 3.68 3.84 Fo.16	387.75 3.66 3.80 Fo.14	387.60 3.81
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NWBR34th  
f/leade 7.19 391.41 — 384.22  
FB1740-66

1733 § Hilley "Brk"

G	386.90 5.13 5.12 Fo.01	387.38 4.65 4.95 Fo.31	387.60 4.43 4.70 Fo.28	387.54 4.49 4.49	387.20 4.87 4.82 Fo.05
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				S 06	S 1/4	☐	N 1/4	N 06
3413 <sup>65</sup>	W cb.	3417	To. No	389.88 5.29	384.08 5.04 5.17 Fo.13	384.25 4.87 5.05 Fo.18	384.15 4.97 5.15 Fo.18	383.83 5.29 5.25
3404 <sup>65</sup>	W 1/4	✓	✓	384.00 5.12 5.08	384.18 4.94 5.06 Fo.12	384.33 4.79 4.95 Fo.16	384.22 4.90 4.94 Fo.104	383.97 5.15 5.13
2495 <sup>65</sup>	☐	✓	✓	384.17 4.95	384.27 4.85 4.93 Fo.10	384.42 4.70 4.87 Fo.17	384.37 4.75 4.93 Fo.18	384.03 5.09 5.07
2477	E 1/4	✓	✓	384.25 4.87	384.43 4.69 4.78 Fo.09	384.60 4.52 4.61 Fo.09	384.50 4.62 4.71 Fo.09	384.23 4.89 4.97 Fo.08
2467	E 06 to No.	✓	to North	384.22 4.85	384.40 4.42 4.50 Fo.130	384.85 4.27 4.42 Fo.22	384.78 4.34 4.42 Fo.38	384.20 4.92
2450	E.L. 3415 to No			384.30 4.82	384.70 4.42 4.50 Fo.08	384.85 4.27 4.30 Fo.03	384.77 4.35 4.42 Fo.09	384.35 4.77
N.V.B.P. 3415 + Meade FB1740-66	4.90	389.12	384.22					
1733	☐ Alley			385.14 5.94 5.90 Fo.104	385.88 5.53 5.76 Fo.23	386.05 5.36 5.59 Fo.23	385.90 5.51 5.69 Fo.18	385.87 5.74
0400 3425	V.L. Swift to South			386.77 4.64	387.20 4.21 4.50 Fo.29	387.35 4.06 4.38 Fo.32	387.20 4.21 4.41 Fo.20	386.75 4.66

S. ch    S. 1/4    ♀    N. 1/4    N. ch

2+04 W 1/4

380.95	381.15	381.28	381.15	380.670
5.27	5.07	4.94	5.07	5.55 ✓
5.23	5.22	5.10	5.17	
80.02 ✓	F0.15	F0.16	F0.10	

2+94<sup>8</sup> ♀

381.05	381.20	381.33	381.20	380.700
5.17	5.02	4.89	5.02	5.52
5.15	5.15	5.07	5.21	5.52 ✓
80.00 ✓	F0.13	F0.18	F0.19	X

2+86 E. 1/4 To South

381.030	381.23	381.35	381.25	380.730
5.19 ✓	4.99	4.87	4.97	5.49
	5.21	5.15	5.23	5.50
	F0.22	F0.29	F0.26	F0.01 ✓

2+72 E. ch. To North.

381.000	381.30	381.41	381.30	380.820
5.22 ✓	4.92	4.81	4.92	5.40
	5.10	4.95	5.07	5.58 ✓
	F0.18	F0.14	F0.15	

2+64<sup>8</sup> E.L. Felton To South

381.040	381.35	381.48	381.35	380.76
5.18	4.87	4.74	4.87	5.26 ✓
5.15 ✓	5.08	4.85	5.01	
	F0.21	F0.11	F0.14	

330    386.22    6.26    382.86

1+23 E.L. Alley

382.500	382.85	382.95	382.80	382.42
6.02 ✓	6.27	6.17	6.32	6.70
	6.53	6.26	6.37	6.70
	F0.28	F0.09	F0.09	X

0+00 W.L. 34<sup>14</sup>

383.680	384.00	384.19	384.00	383.650
5.49	5.12	4.99	5.12	5.47 ✓
5.47	5.27	5.17	5.37	5.48
X	F0.15	F0.18	F0.25	F0.01

389.12

S. 1/4	S. 1/4	E	N. 1/4	N. 1/4
378.43 x 5.12 ✓	378.55 x 5.00 ✓ 4.97 ✓ C 0.04	378.85 ✓ 4.70 4.69 ✓ C 0.01	378.72 4.83 4.90 F 0.07	378.62 4.83 ✓ 4.92 ✓
378.87 4.68 ✓ 4.67 C 0.01	379.35 4.20 4.37 F 0.17	379.55 4.00 4.00 x	379.45 4.10 4.20 F 0.10	379.08 4.97 ✓
NW 1/4 P. 33 <sup>rd</sup> Meade	452 383.55 — 7.18	17A-71 NW 1/4 33 <sup>rd</sup>	339.03 339.04	5B.337.03
1+33 <sup>rd</sup> E Alley				
379.53 6.67 6.76 F 0.09	380.00 6.22 6.57 F 0.35	380.17 6.05 6.16 F 0.11	380.07 6.15 6.29 F 0.14	379.70 6.52 ✓
380.51 5.67 ✓	380.95 5.27 5.53 F 0.30	381.10 5.12 5.12 x	380.97 5.25 5.24 L	380.55 5.67 ✓
380.67 5.55 ✓	381.03 5.19 5.47 F 0.28	381.17 5.05 5.21 F 0.20	381.05 5.17 5.28 F 0.11	380.62 ✓ 5.60 ✓
380.77 ✓ 5.45 ✓	381.10 5.12 5.31 F 0.17	381.23 4.99 5.13 F 0.16	381.10 5.12 5.21 F 0.09	380.65 5.57 ✓

2+50 = 15 E. E.L. 33<sup>rd</sup>

2+00 Brk

NW 1/4 P.  
33<sup>rd</sup> Meade 452 383.55 — 7.18 339.03 339.04 5B.337.03

1+33<sup>rd</sup> E Alley

0+14 = 14' W. W.L. Felton

0+00  
3+25 W.L. Felton

13+13 W. cb. Felton

386.22



040  
3+45<sup>15</sup> W. Line 33<sup>rd</sup>

3+93<sup>15</sup> W. Ch.

3+19<sup>15</sup> W 1/4

3+05<sup>15</sup> E

2+91<sup>15</sup> E 1/4

2+77<sup>11</sup> E. Ch.

2+65<sup>15</sup> E.L. 33<sup>rd</sup>

383.55

S. 06.	E. 1/4	E	N. 1/4	N. Ch.
378.12 5.43 5.43 ✓	378.49 5.06 5.43 F0.39	378.62 4.93 5.11 F0.18	378.63 4.92 5.16 F0.24	378.28 5.27 5.25 ✓ 00.02
378.15 5.40 5.57 F0.17	378.45 5.07 5.63 F0.56	378.60 4.95 5.41 F0.54	378.63 4.92 5.38 F0.54	378.33 5.22 5.37 F0.09
378.35 5.20 ✓	378.45 5.10 5.24 F0.14	378.57 4.99 5.04 F0.06	378.62 4.93 5.01 F0.08	378.58 4.97 ✓
378.47 5.08 ✓	378.45 5.10 ✓	378.55 5.00 ✓	378.61 4.93 ✓	378.72 4.83 ✓
378.35 5.20 5.20 ✓	378.30 5.25 5.29 F0.04	378.45 5.10 ✓	378.40 5.15 ✓	378.60 4.95 ✓
378.07 5.48 5.30 F0.02	378.16 5.39 5.46 F0.07	378.20 5.35 5.42 F0.07	378.26 5.29 5.40 F0.11	378.30 5.25 ✓
378.30 5.25 ✓	378.25 5.30 5.38 F0.08	378.45 5.10 5.13 F0.03	378.45 5.10 5.12 F0.02	378.45 5.10 5.09 00.01 ✓

3402 W. 1/4 33<sup>rd</sup> Place to No.

S. 06.	S 1/4	♀	N 1/4	N 06.
377.32	377.80	378.05	378.05	377.70
5.40 ✓	3.98	4.67	4.57	5.02
	5.11	4.83	4.81	5.08
	F0.20	F0.16	F0.24	F0.01

24899 ♀ 33<sup>rd</sup> PL. to No

377.87	377.87	378.10	378.12	377.76
5.35 ✓	4.85	4.62	4.60	4.96
	5.03	4.83	4.86	5.09
	F0.18	F0.23	F0.26	F0.13

2479 E. 1/4 33<sup>rd</sup> place to North

377.43	377.93	378.17	378.18	377.82
5.29 ✓	4.79	4.55	4.54	4.90
	4.99	4.81	4.90	4.77
	F0.19	F0.26	F0.16	F0.09

2466 E. Cb 33<sup>rd</sup> <sup>Place</sup> to No. W. Cb to South

377.47	378.00	378.25	378.24	377.87
5.25	4.72	4.47	4.48	4.85
5.45	4.98	4.74	4.57	4.93 ✓
F0.20	F0.26	F0.27	F0.09	

24549 = E.L. 33<sup>rd</sup> Place North

377.52	378.05	378.31	378.30	378.01
5.20	4.67	4.71	4.42	4.71 ✓
5.40	4.97	4.60	4.48	
F0.20	F0.30	F0.23	F0.06	

T.P. 4.66 382.72 5.49 378.06

382.72

0450 = 50' W. W.L. 33<sup>rd</sup> St.

378.07	378.53	378.72	378.63	378.27
5.48 ✓	5.02	4.83	4.92	5.28 ✓
5.41 ✓	5.17	4.86	4.99	
F0.01	F0.15	F0.09	F0.09	

38355

	S. cb.	S 1/4	E	N 1/4	N. cb.
E. 1/4	376.59 6.03 6.11 FO.08	376.56 6.06 6.04 6.02	376.80 5.94 5.97 FO.03	376.80 5.82 5.87 FO.05	376.87 5.75 5.77 FO.02
1+7A E Gutter line	376.40 6.22 6.22 L	376.48 6.14 6.14 L	376.55 6.07 6.07 L	376.65 5.97 5.98 FO.01	376.75 5.87 5.96 5.01
1+53 <sup>2</sup> E.L. Bancroft. to No.	376.53 6.09	376.90 5.72 5.83 FO.11	377.10 5.52 5.68 FO.16	377.10 5.52 5.64 FO.12	376.92 5.70
1+40 B-K NW Bancroft + Meade	5.20 382.62	377.02 5.67 6.04 6.07 6.02 FO.11	377.15 5.47 5.47 FO.16	377.15 5.47 5.47 FO.16	376.97 5.65
3+24 <sup>2</sup> W.L. 33 <sup>rd</sup> Place to North	377.21 5.51	377.68 5.04 5.00 FO.22	377.90 4.77 5.00 FO.23	377.93 4.79 4.70 FO.11	377.63 5.09
3+13 W. Cb. 33 <sup>rd</sup> Place to North	377.26 5.46	377.75 4.97 5.18 FO.21	378.00 4.92 4.96 FO.24	377.98 4.74 4.90 FO.16	377.65 5.07 5.07
	381.72				

1+40 B-K  
NW Bancroft  
+ Meade

377A2

BR.  
EA. 1740  
P. 74

381.62

W.L. Bancroft (Page 21)

W. Cutter Bancroft.

376.54	376.60	376.70	376.80	376.92
6.07	6.07	5.92	5.82	5.90
5.90	6.01	5.96	5.92	
EO.01	EO.01	EO.04	EO.10	

W. 1/4

376.65 Q	376.60 Q	376.78 G	376.80 S	376.88 Q
5.97	6.02	5.84	5.78	5.74
5.98	5.98	5.8		
EO.01	EO.02	EO.06		

E Bancroft

376.70	376.65	376.85	376.86	376.95
5.92	5.97	5.77	5.76	5.67
5.93	5.92	5.81	5.74	5.87
EO.03	EO.05	EO.04		

382.62

# INDEXED

Oakemere Sewer grades  
Lots 39 to 52 + 55 to 62

6-2-47  
Sommerville  
W. Moore  
Hutton  
Sherman

NW 1/4 63 <sup>rd</sup> El Cajon	A.16	469.82	—	456.66
T.P.	3.67	467.37	6.12	463.70
T.P.	5.45	466.97	5.85	461.52

17<sup>th</sup> Grade MH#1

0-96 <sup>th</sup> Exist. M.H. Rod 13.74 A53.23	0+00 E1. 454.19	0+45 454.64	0+90 455.09	1+36.8 Δ AA 52.87 455.56
		12.33	11.88	11.41
		8.04	8.28	7.83
		C 4.29	C 3.60	C 3.53

T.P.	3.67	466.52	A.12	462.85
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## 0.7% Grade

1+50 2+00 +50 +82<sup>8</sup> = M.H. #2

455.65	456.00	456.35	456.58
10.87	10.52	10.17	9.94
6.60	6.39	5.15	5.03
C 4.27	C 4.13	C 5.02	C 4.91

3+00 +50 A+00 +45 +61.8 = M.H. #3

456.70	457.05	457.40	457.72	457.84
7.82	7.47	7.12	6.80	6.68
4.77	5.01	4.11	4.08	4.36
C 5.03	C 4.46	C 5.01	C 4.72	C 4.32

### North Line

5+07<sup>16</sup> DE. to South MH#3  
DE CH  
+79.

458.16	458.12	458.40
8.36	8.40	8.12
4.08	3.59	3.79
C 4.28	C 4.81	C 4.33

Indexed  
csik.

50

Alley  
 Grades A BIK 319 Reed + Daleys  
 W.O. 31045

+20

INDEXED

5+00

BM 526.6  
 Clay + 27" 0.70 78.75 - 78.05

Rake

0+80 E.V.C.

0+60

0+40

0+20

0+00 - E. Line 28<sup>th</sup>

BM - top Curb.  
 E.L. 29 South Curb.  
 Alley 4.06 76.01 - 71.95  
 FB 1714-41

Finish grades

51

74.12  
 4.63 ✓

74.13  
 4.62 ✓

72.87  
 3.74 ✓

72.72  
 3.79 ✓

72.40  
 3.61 ✓

71.81  
 4.10 ✓

71.25  
 4.76 ✓

Alley BIK 319 Reed & Daleys  
Finish grade

INDEXED

51995 West Line 29th

+80

+60

5140

78.75

72.85  
5.90 ✓

73.32  
5.43 ✓

73.72  
5.03 ✓

73.99  
4.76 ✓

INDEXED

4100

}

Rake

TR. 5.98 19.98 4.87 14.03

0+80 Brk.

+60

+40

+20

0+00 = E. Line 29<sup>th</sup>

S.F.R. Clay + 19<sup>th</sup> 0.95 78.90 78.05

74.69  
- 5.29 ✓

73.73  
- 5.17 ✓

73.63  
- 5.27 ✓

73.46  
- 5.44 ✓

73.26  
- 5.64 ✓

73.05  
- 5.85 ✓



Finish grades BIK 322. Reed & Daleys Sub

6+20 Meet Paving W.O. 31045

6+00

INDEXED

+80

+60

+40

5+20

}

Rake

3.27 79.68 3.57 76.91

}

4+40

4+20

79.98

4

54

~~72.85~~  
~~7.43~~  
~~7.41~~  
~~7.42~~

71.93

72.78  
6.95 ✓

73.47

6.21 ✓

73.96

5.72 ✓

74.30

5.58 ✓

74.45

5.23 ✓

74.69

5.29 ✓

74.72

5.26 ✓

~~72.21~~  
~~7.47~~  
~~7.48~~  
~~7.49~~



Iowa  
+  
Meade

~~Z~~

N.W. R. 3204

Meade 7.44 387.90. — 380.46

S 1/4

N 1/4

0.125 5.99 5.62 5.17 5.06 5.81

Meade

INDEXED  
WK  
FEB 16 1949

W.L. Iowa

0.100 5.78 5.53 5.21 5.10 5.124

25  
6.11 5.98 5.76 5.50 5.32 5.29 5.25 5.30 25 4.94

5.37 5.33 5.20 4.98 5.03 4.89 4.71 W 1/4

4.99 5.10 4.95 4.78 4.72 4.51 4.55 4.50 Iowa

E 1/4 4.94 4.93 4.74 4.58 4.52 4.40 4.34

25  
5.19 4.76 4.90 4.71 4.67 4.67 4.50 4.44

5.41 5.16

Rod readings not reduced  
Leave intersection as is.

OHIO  
+  
Meade

56

~~Z~~

S.E. R. 0112 +  
Meade

CC 3/4 Meade N 1/4 CC  
5.80 379.32 — 373.52

INDEXED  
WK  
FEB 16 1949

Leave West Gutter

5.85

5.89

5.80 5.89

W 1/4

5.44

OHIO

E 1/4

6.35 6.50 Eliminate E. Gutter 5.30 5.17 4.93

25 6.33

EL 01110 6.27

25

5.94

25

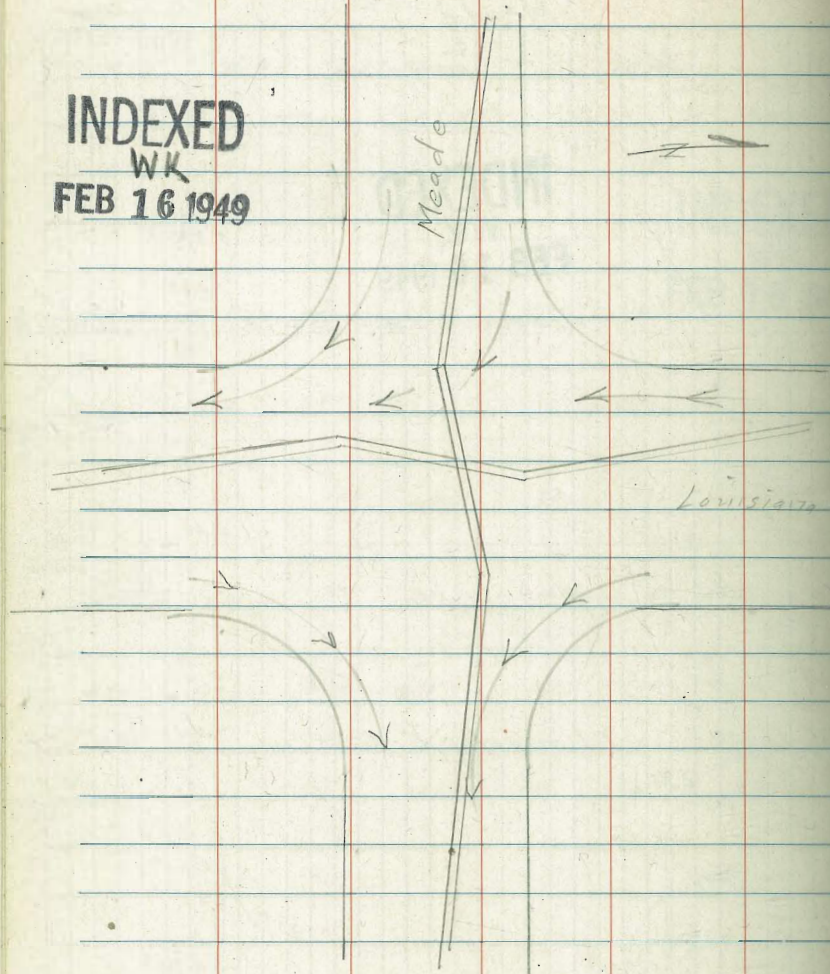
5.25

4.85

Rod readings not reduced

Louisiana + Meade

INDEXED  
WK  
FEB 16 1949

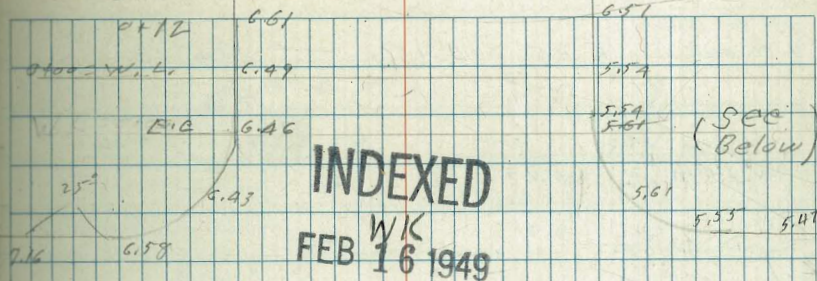


(↖) = direction off flow.  
No change in intersection

S.E. BP = 318.87 Alabama + Meade

57

$\frac{5.03}{323.907}$



INDEXED  
WK  
FEB 16 1949

Rods not reduced

Alabama \* 5.50

\* 5.10

\* 5.30

\* 4.79

$\frac{318.76}{5.92 \text{ set}}$

$\frac{318.44}{5.65 \text{ set}}$

$\frac{318.59}{5.40 \text{ set}}$

$\frac{318.56}{5.54 \text{ set}}$

$\frac{318.64}{5.26 \text{ set}}$

$\frac{318.71}{5.5 \text{ set}}$

New grade  
gutter. N.W. Return  
+ 50' N. on Alabama  
Eliminate gutters

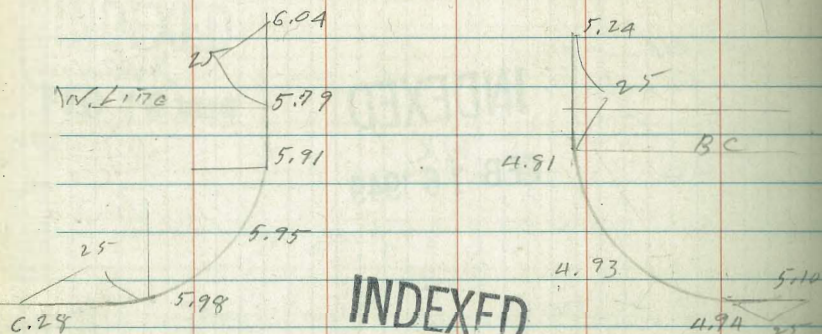
# Georgia & Meade

B.M. Hole

1 SE. Top Qu. 10

B.M. out

6.25 349.85 — 343.60



INDEXED

WK

FEB 16 1949

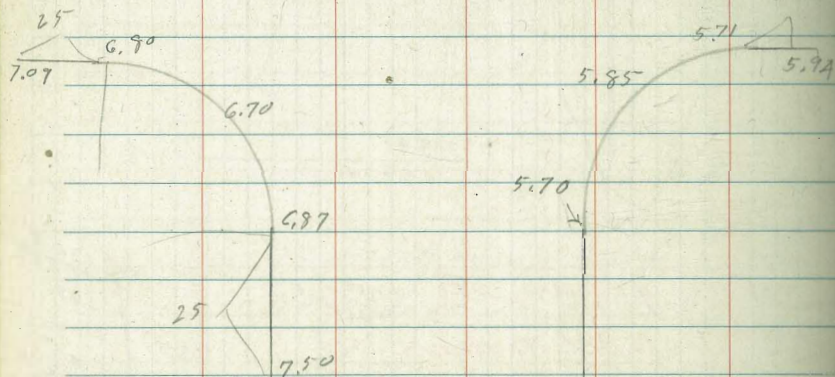
• 5.56

Intersection is

High spots

Eliminate gutters

1/4 x 5.93



# Restake W. gutter line 58

40th at Meade

NW. 7/4 + 40th + Meade = B.M. =

4.90 374.78 — 369.89

S.L. Meade	S C/L	V <sub>A</sub>	N 1/4	N.O.	20' N. N.O.
367.37	367.73	68.20	68.75	69.78	69.03
OK	705	619	823	575	571
	717	OK	609	576	OK
	Ed. 10		Ed. 06	Ed. 09	

50' Not N.O.

67.47

581

2 on par.

INDEXED

WK

FEB 16 1949

Stake Driveway N.E. Cor.  
30th at Landis

Stake 30th  
+ Landis 338.99 out  
S.W. B.P. 30th  
+ Corn 3.06 346.99 — 343.93

Set B.M.  
NE B.P. 30th. 6.92 340.07  
+ Landis  
orig B.M. 3.06 343.93

**INDEXED**

WK  
NOV 23 1948

Established Grade

0+50.6 = N. End drive 6.32  
Meet Existing Ch. 6.92 OK 340.67 Meet B.B.  
6.01

0+20.6 = S. End Drive 6.72 set. 340.27

0+00 = N. L. Landis 6.99  
Meet Existing Ch. 6.99 OK 340.00 Meet  
Exist Ch.

Stake 30th

→ 14 ← 26 → 26 → 14 ←

4.8  
5.8  
1.0  
Conc. walk

0+50.8

0+20.9

0+00

4.8  
5.8  
1.0  
Conc. walk

Stake Landis

# Stake Culvert Quince & Front

Sommermeys 6-12-47

Stakes set 4' Lt of  $\Phi$

Inlet - 0+00

FB 1693 P. 76	1.51	180.91	-	179.40	
		Intersect # of Imp.			
0+00	0+30	0+60	0+90	1+20	1+60
176.70	171.85	167.00	164.00	161.00	157.00
4.21	9.06	13.91			
4.01	8.74	13.23			
C 0.20	C 0.32	C 0.68			

	0.10	167.78	13.23	167.68	
1 1/2 Bost on Lath.			13.62	154.16	FB. 1693 P. 76

**INDEXED**

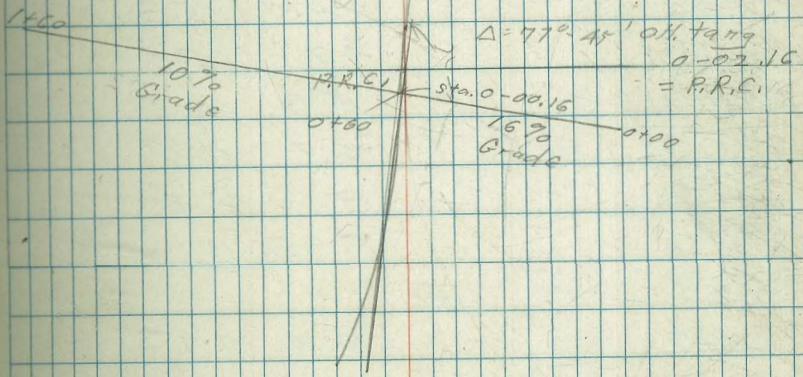
WK

NOV 23 1948

Not Used

See page 64.

164.00	161.00	157.00
3.78	6.78	10.78
3.05	6.78	10.78
C 0.73	Gr.	Gr.









Summer moyer  
W. Moore  
Sherman

Beardsley + Harbor Drive  
Sewer Grades

7-28-47

Stakes set. 10' Lt. ♀.

W.O. 90011

N.W. 7' Lt. Main  
+ Beardsley

	1.04	22.17	-	21.13	
	2.23	15.90	8.50	13.67	M.H.#1
0+00	+25	+50	+75	1+00	1+25.92
+0.35	+0.09	-0.16	-0.41	-0.66	-0.92
15.56	15.81	16.06	16.31	16.56	16.82
8.30	7.83	7.27	6.70	6.13	4.95
C 7.26	C 7.78	C 8.49	C 9.61	C 10.93	C 11.97
	Δ	M.H.#2	Cuts on 40' offset.		
1+45.08	1+64.23		M.H.#1	M.H.#2	
-1.30	-1.68	-0.38	-0.92	-0.38	
17.20	17.58	16.28	16.82	16.28	
4.33	3.44	4.85	3.54	3.50	
12.87	C 14.14	11.43	C 13.28	C 12.74	

Check.

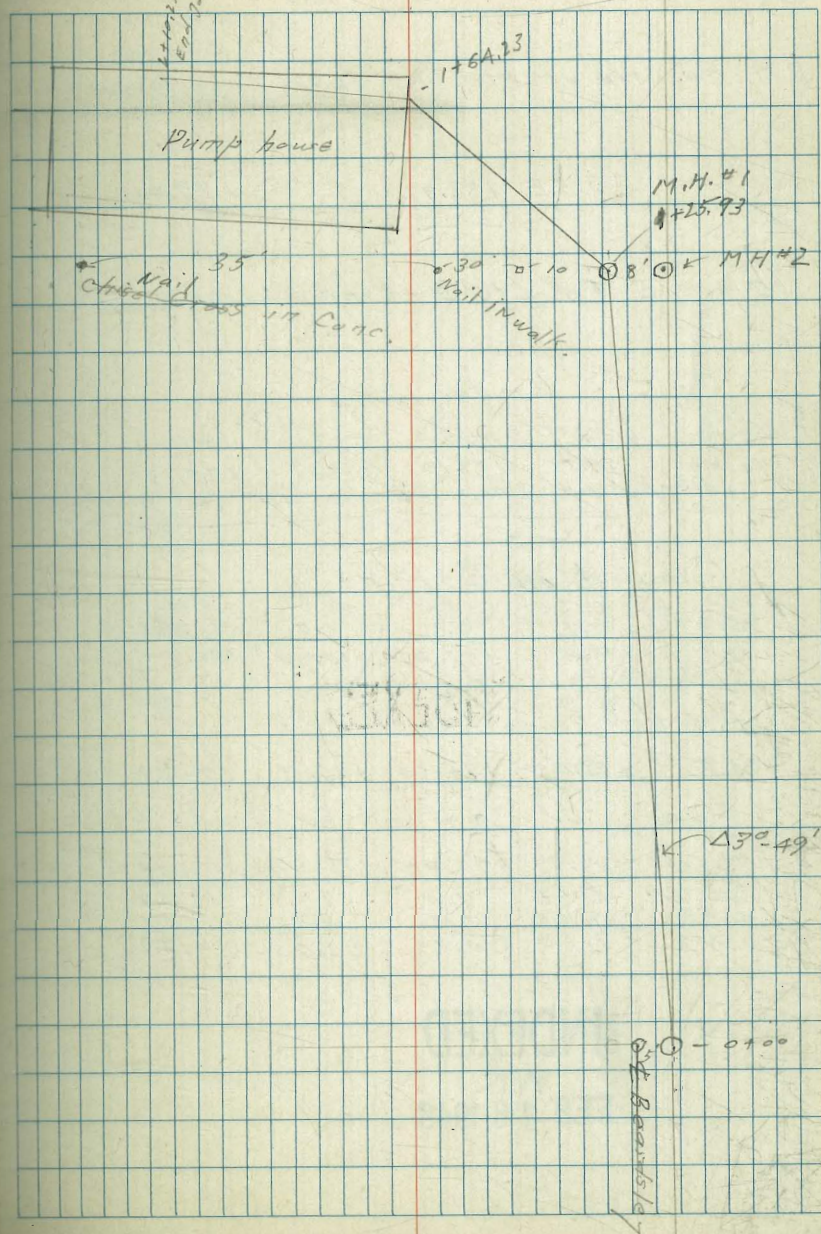
M.H. Rim EL.  
0+00 FB1679-60 (7.65)

8.26 7.64 - 76° OK.

INDEXED  
WK  
NOV 23 1948

63

Harbor Dr.



# Stake Culvert

Frant & Quince

7-30-47

Sommermeier  
Moore  
Sherman

64

B.M. = Cross top of M.H. F.B. 1693 - Page 76 = 179.40

3.52 182.92 179.40

0+00 = 54' Lt. & Improvement.

Grade = 1.67%

0+00	0+27	0+54	0+83	1+12
180.00	179.55	179.10	178.61	178.13

Proposed Imp. Grade is to High

## Ground on Pipe

0+00	1+7	1+14	1+53	1+72
6.8	7.7	9.5	8.9	6.0
176.1	173.2	173.4	174.0	176.9
0.4	3.3	2.5	1.0	2.3

Proposed Grade Lowered 3.50

176.5	176.05	175.60	175.11	174.63	Grade
					1.67%

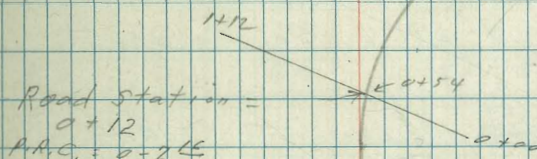
Figure 0<sup>3</sup> Camber So Grade Els. =

176.50	176.27	175.90	175.34	174.63	Set
6.42	6.55	7.02	7.58	8.27	
4.90	7.75	6.66	4.95	3.50	
C 2.02	F 1.10	C 0.36	C 2.63	C 4.79	

INDEXED

WK

FEB 16 1949



Culvert is  
Radial to Curve.

Det. 1:51'-30" =  
Tang. of H. P.R.C.

Culvert Lot #1 BIK#3  
 Valencia Park. 8-19-47  
 Work order 80059

0+00 = E. Line San Jacinto F.B. 1696-P 78  
 B sheet # 3308

B.M. = 0+00 1/2 Hub. F.B. 1696-P. 79  
 E.L. = 170.17

Stakes 9' Lt. & So. Culvert.

~~151~~  
~~169~~ 171.68 — 170.17

INDEXED  
 WK  
 NOV 23 1948

A 179.30' Lt. Divided into 4 parts			
Start Pipe	H.C. Pt.	# 1	# 2
0+108	0+20.02	0+33.76	0+47.51
164.20	164.44	164.72	165.00
7.48	7.24	6.96	6.68
Fix into	7.06	6.87	6.60
Exist Pipe	00.18	00.28	00.08
# 3	EC	EC. Ground at &	
0+61.25	0+75.00	0+75.00 in wash.	
165.128	165.56	169.56	
6.40	6.12	6.12	
5.50	7.14	6.4	
00.90	01.68	F 013 O.K.	

Returns - cut back  
32nd + Univ

W.O. 60146 8-26-47

Sommersmeyer  
W Moore  
Sherman  
Lamore

Grades taken from  
profiles # 885 # 1605 and  
# 1606

N.E. Ret. set to walk

#1	#2	#3	#4	#5	#6
352.55	352.50	352.50	352.50	352.50	352.44
4.56	4.61	4.61	4.61	4.61	4.67
4.38	352.31			352.61	5.0
352.26					
4	80	70	60		

Set. at. Below to meet walk.

352.26	352.51	352.53	352.50	352.37	352.24
	2.60	4.58	4.61	4.74	4.97
	5.14	5.30	5.39	5.23	
	F 0.64	F 0.78	F 0.78	F 0.49	

S.W. Ret. set to profile Grade.

#1	#2	#3	#4	#5	#6	#7
352.10	352.07	352.00	352.00	352.00	352.00	351.90
5.01	5.04	5.11	5.11	5.11	5.11	5.21
5.18	5.21	5.47	5.54	5.68	5.64	
F 0.17	F 0.17	F 0.36	F 0.48	F 0.57	F 0.53	

Set. B.P.P.M.  
N.C. Cor. Univ  
+ 32.42

1.P.	5.90	357.20	5.81	351.30
32nd + Univ	5.20	357.11		351.91

357.11

5.81

351.30 = Temp. B.M.

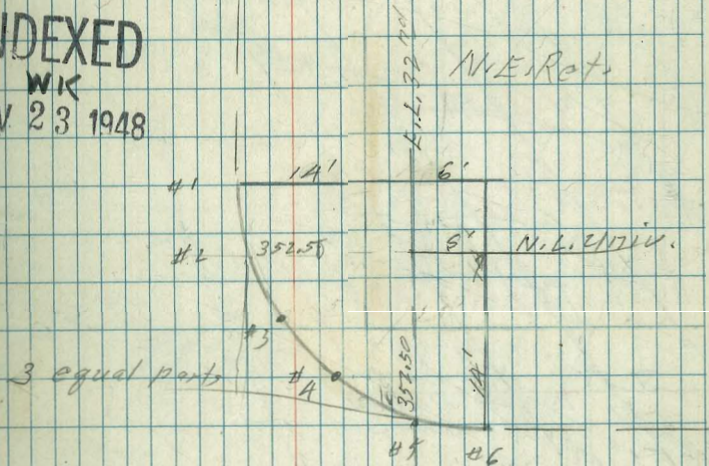
590

66

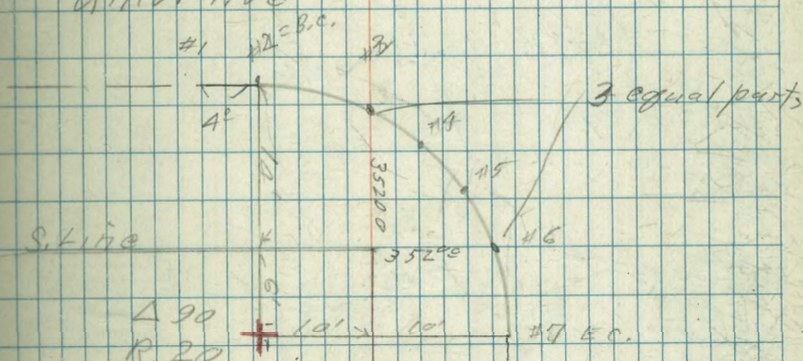
INDEXED

WIK

NOV 23 1948



UNIV. Ave

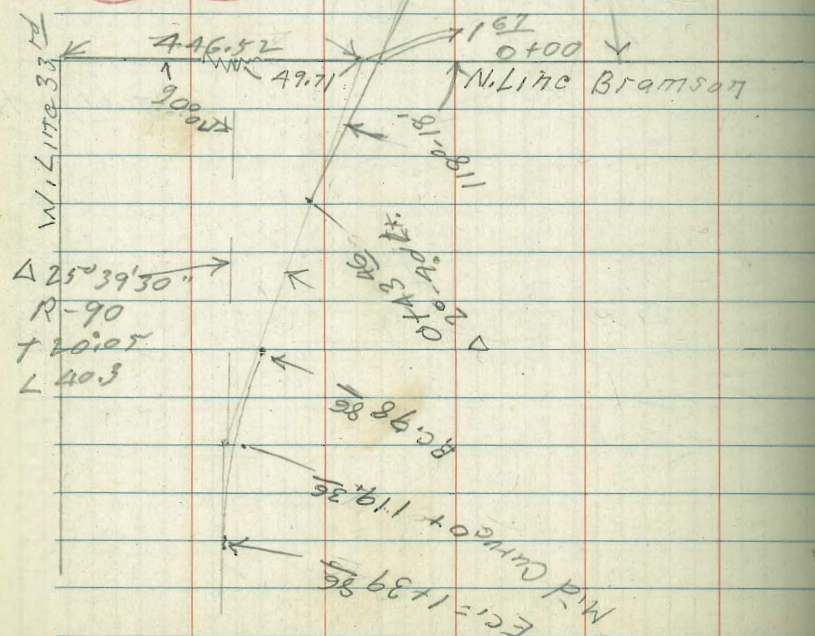
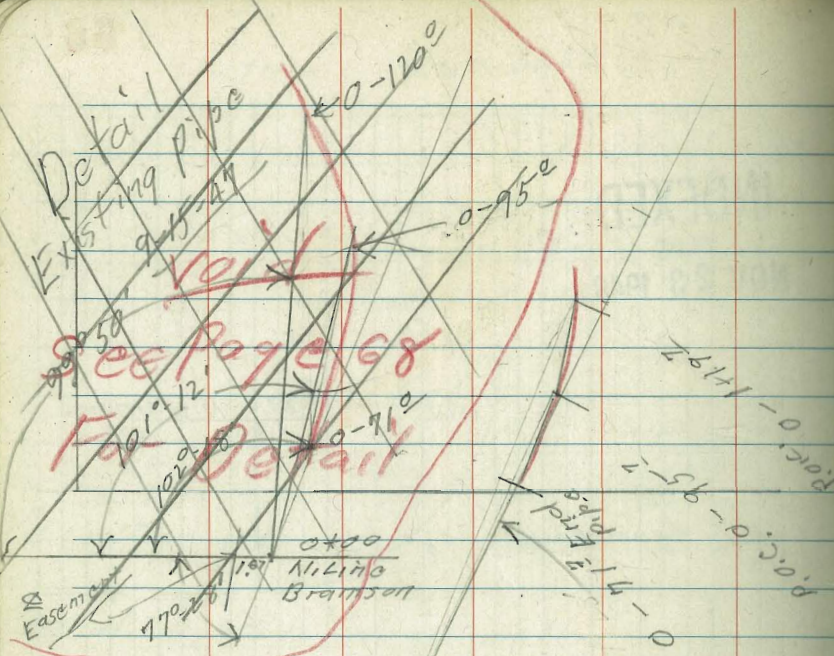


A 90

R. 20

S.W. Ret

Storm Drain Bramson Place 67



INDEXED

9-15-47 WIK  
NOV 23 1948

Sommermeje  
W Moore  
Stierman  
Allen

SW R.R. 33rd + El. Cajon.	374.32
	1.48
	375.80
	.836
	367.94
Moved curb stake	3.79
N. Line Bramson (C2.82)	371.23
Set stake 10'	
East. at	5.78 Ord. Road
old stake	4.61
C 2.32	C 1.17
2.76	
5.77	Ord. + Grade

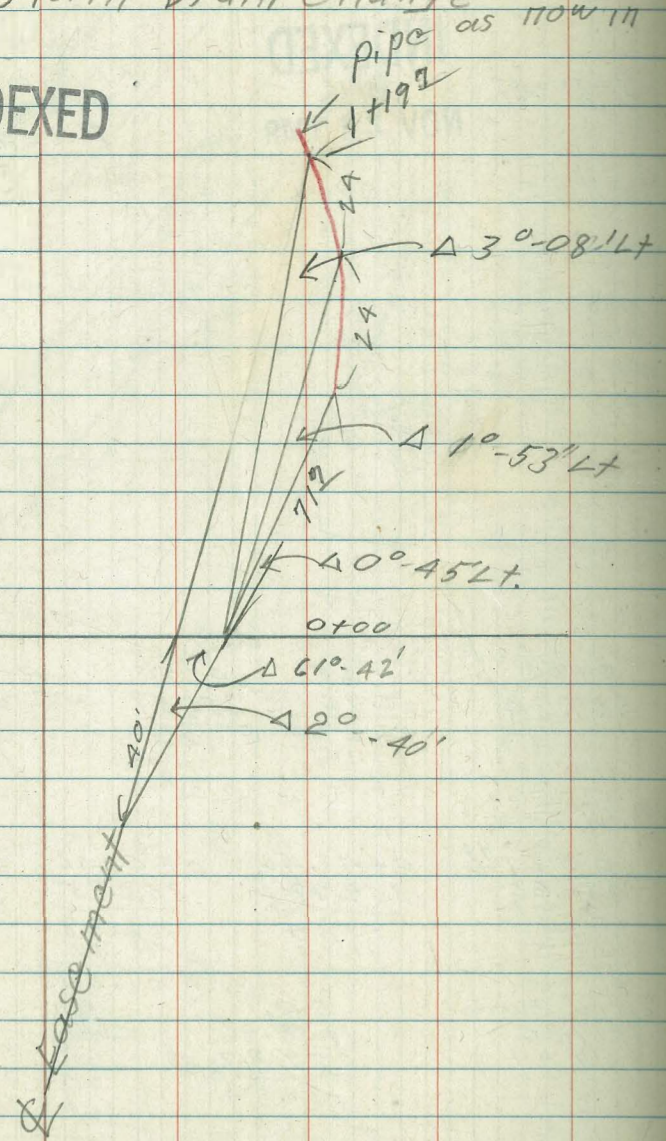
stakes 6' 10 ft.

0+00	0-25	0-50	0-71
357.34	356.96	356.59	356.28
13.89	14.27	14.67	14.95 New
12.92	12.12	11.74	11.72
C 1.07	C 2.15	C 2.70	C 0.003
Ch. stake			P.C.
0+21.73	0+47.46	0+58.46	0+99.86
357.66	357.98	358.35	358.79
13.57	13.28	12.88	12.44
12.37	11.19	11.67	11.65
C 1.24	C 2.06	C 1.21	C 0.79
Mid Curve	E.C.		
119.36	139.86		
359.09	359.39		
12.14	11.84		
9.82	9.32		
C 2.32	C 2.52		

0+00 6' RT
357.34
13.89
12.92
C 1.87

Bramson Place  
Storm Drain Change

INDEXED



Sewer Grades Bangor St.  
From Lucinda - 174.88 South

9-26-47  
W.O. # 60161  
Sommarmayer  
W Moore  
E Sherman  
F.B. 1569-P70 + "B" sheet # 3347-B  
0+00 =  $\Phi$  Lucinda + Bangor } sec. FB 1759  
Rate = 1.72

0+00	+34	+70	1+05	1+40	1+74 <sup>88</sup>
265.68	265.93	266.17	266.42	266.66	266.91
9.10	8.85	8.61	8.36	8.12	7.87
1.58	1.96	2.54	4.23	3.17	3.02
C 4152	C 3.89	C 4.07	C 4.13	C 4.75	C 4.85

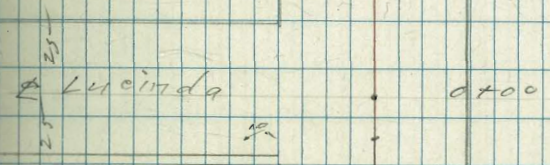
che INDEXED  
WIC  
NOV 23 1948

BM. = N.E. 10' tie back on 7' Line Lt.  
FB 1659  
P. 70 5.30 274.78 — 269.48

check. BM. 5.30 269.48 ✓

stakes set 4' west of  $\Phi$

1+74<sup>88</sup>  $\Phi$  Bangor  
Puck Line  
Ed. 2529 City dist





Stake Culvert Front + Quince

INDEXED

6-6-97

Summerhayes  
W Moore  
Molten  
Sherman

Drawing 6922L

Stakes set 6 North  $\Phi$ .

0+00 = inlet - 54' Ely from  $\Phi$  Improvement

Original cross  
M. H.  
E.G. 1693-76

found

stake

179.40

0+00

+27

+54  $\Phi$

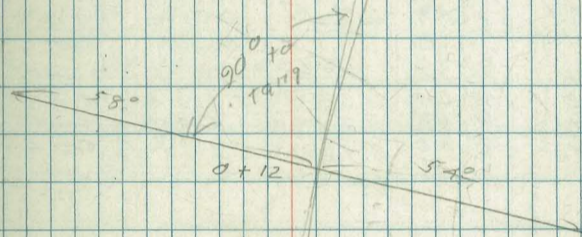
+83

1+12 = outlet

Void

Not used C.H.S. 6-10-97

See Page 64



0-2' E = ARC.

9-24-46 Sewer Grades: Blks 345  
 Nettleship - Tye Tract #1  
 W.D. 80004 (Pacific Beach)

F.B. 1690 P27 + L sheet 6692-L  
 Exist M.H. D.M.H.

0+00	+50	1+00	1+09.4	1+13.1
28.60	29.05	29.50	29.89	31.53
13.53	13.08	12.63	12.24	9.60
13.52	4.58	4.02	4.12	4.12
C 0.101	C 8.50V	C 8.61V	C 8.12V	C 5.48V

OK.

M.H.#2  
 2+00 +50 2+70.5L Δ220.35' RT.

33.61	34.56	34.95
8.52	7.57	7.18
3.40	1.85	2.57
C 5.12V	C 5.72V	C 4.61V

**INDEXED**  
 WK  
 NOV 23 1948  
 42.13

D.M.H. #4

3+10.5L	3+70.5L	4+10.5L	4+70.5L	"
35.90	36.85	37.80	38.75	41.00
18.19	17.24	16.29	15.34	13.09
11.30	9.28	7.01	6.45	6.45
C 6.89V	C 7.76V	C 9.28V	C 8.89V	C 6.64V

5+10.5L 5+70.5L 6+20.5L Connect to Exist Sewer 53.54  
 M.H. R171 57.54

54.09	57.54	41.60	51.77
39.70	40.65	15.94	2.82
14.39	16.89	1.77	2.80
0.80	2.20		0.02 OK
C 13.59V	C 14.69V	C 14.17V	

Line East From DMH #1

0+00	0+39.86	0+77.72	Con. to Exist Sewer
29.89	31.09	32.28	
12.24	11.04	9.85	
4.12	2.70	3.00	
C 8.12	C 8.34V	C 6.85V	

42.13

57.54  
 East From DMH #4

0+02.61	0+50	1+00	1+50.18	61.24
Mar Hole				2101.24
41.00	41.79	42.60	43.40	44.22
	15.75	14.94	14.14	17.02
	7.88	7.15	7.04	5.70
	C 7.95V	C 7.78V	C 7.10V	C 11.32V

DMH #5  
 61.24

2+55.29	3+07.29	3+62.29
2+52.29		
East West + S	North	
45.04	51.50	47.95
16.20	9.74	13.29
3.91	3.91	2.24
C 12.29V	C 5.83V	C 11.05V
		C 8.80V

North From DMH #5  
 DMH #5  
 61.24

0+00	0+40	0+80	1+20	62.73
51.50	52.50	53.50	54.50	0.68
9.74	8.74	7.74	8.28	60.56
3.91	1.62	0.68	1.38	2.17
C 5.83	C 7.12V	C 7.06V	C 6.85V	C 7.73V

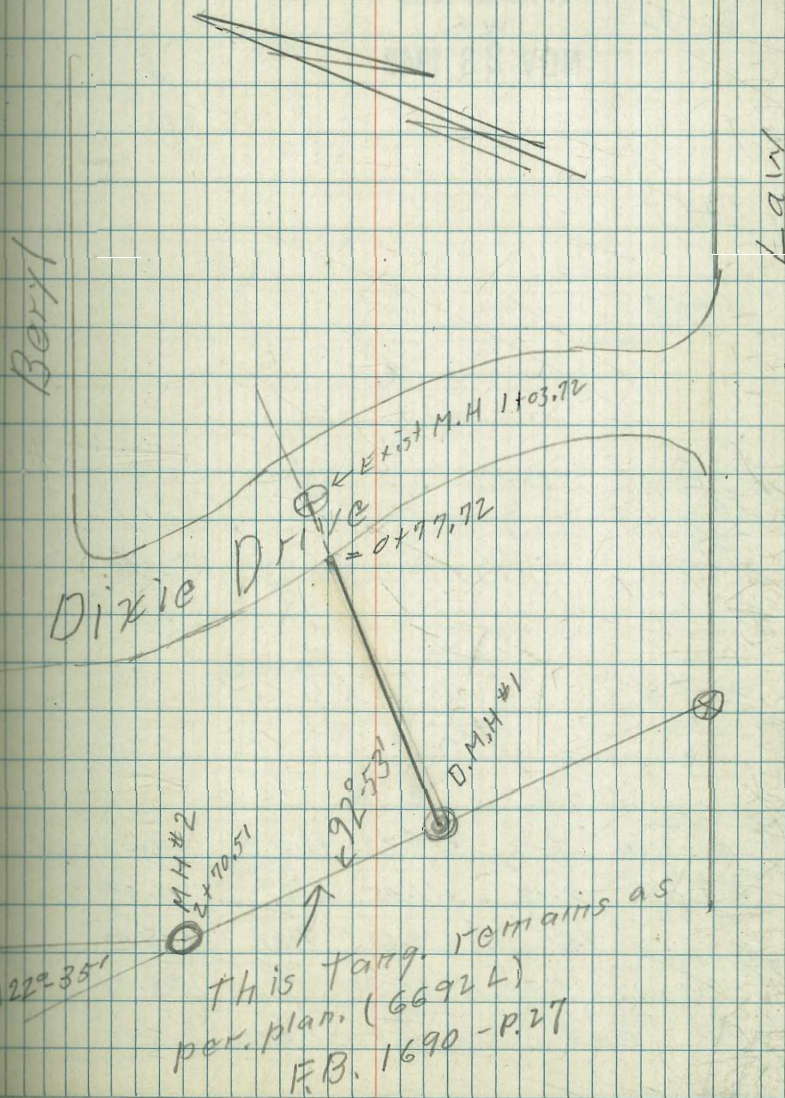
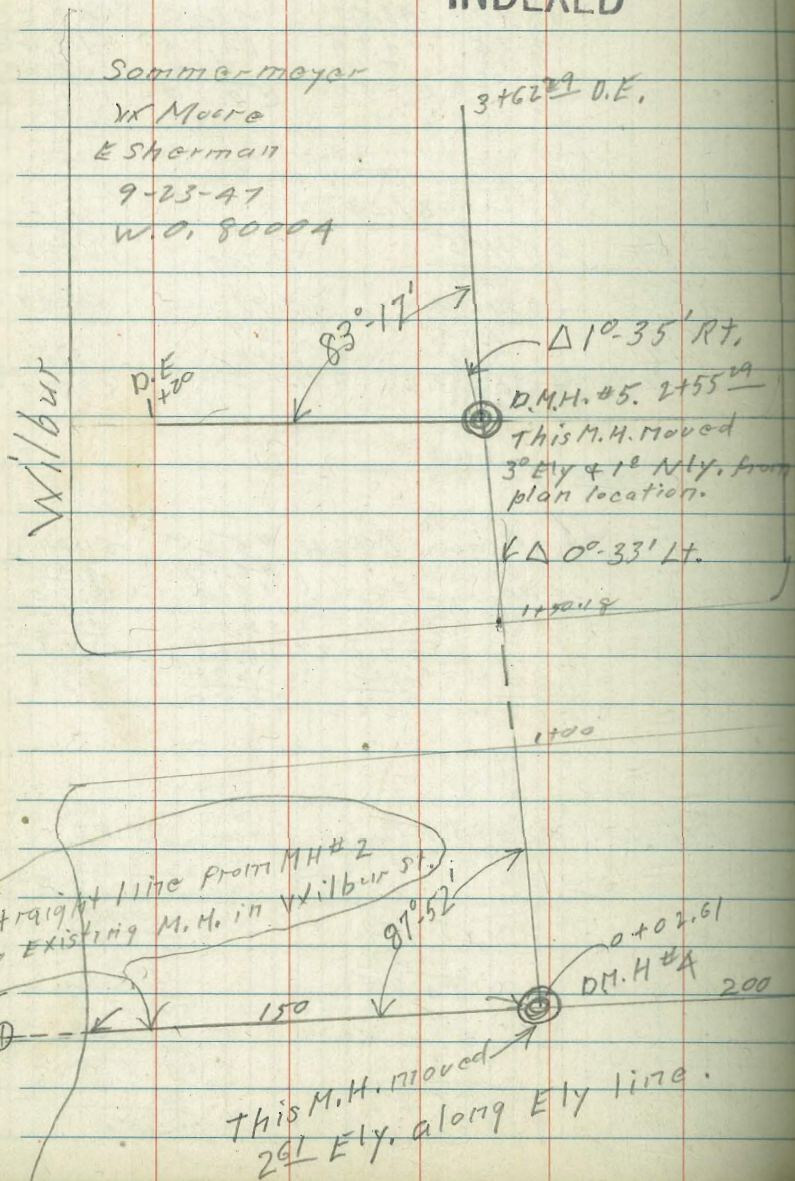
R.M. N.E. Ocean Blvd & Low 33.82

57.54	33.82
2.69	8.71
54.85	42.13
6.39	0.28
61.24	41.85
3.36	12.24
57.88	54.09
	0.55
	53.54
	41.00
	57.54

0.03 OK

Line change  
 BIKs. 3+5 Nettleship Tye  
 Tract #1. INDEXED

Sommermeier  
 vs Moore  
 & Sherman  
 9-23-47  
 W.O. 80004



Law St. Gresham to Ingraham  
Water Meter Box Grades

INDEXED

2+35

WK

NOV 23 1948

1+57

1+53

1+35

0+88

Stakes set 2' East x 2' West x  
of ctr. Meter Box. Stakes 157 back  
of curb face. Fire Hydr. in place

NE 7' track Gresham + Law	6.41	106.77	11.09	100.36
0+35	0.17	111.45	8.35	111.28
	1.61	119.63	7.81	118.02
SW 7' track + Ingraham + Bevel	0.75	125.83	—	125.08

0+00 = East line Gresham

North

South

73

101.50      101.52      100.72      100.74  
C 1.00      C 1.00

101.03      101.05  
C 1.00

100.16      100.18  
C 0.50

100.90      100.92  
C 0.50

100.104      100.06  
6.73      6.71  
6.27      6.21  
C 0.50      C 0.50

100.63      100.65  
C 0.50

100.11      100.13  
6.66      6.64  
6.16      6.14  
C 0.50      C 0.50

106.77

6 1/2 ft.  
100.12

Rate



Temp.

B.M. 4+85

East stake North side = 4.75 103.98

4+85 - W. L. Hairies

5.96 108.73 4.00 102.77

4+25

4+12

3+93

3+85

3+06.5

3+05

2+85

North

South

74

west stake East stake

102.96 102.98

5.77 5.75 109.73

4.77 7.75  
C 1.00 C 1.00

west stake East stake

102.44 102.46

6.29 6.27

5.79 5.77  
C 0.50 C 0.50

102.03 102.05  
Grade

102.53 102.55  
C 1.00

101.80 101.82  
Grade

102.37 102.38  
C 1.00

101.92 101.94  
C 1.00

101.20 101.22  
C 0.50

Rake

101.79 101.81  
5.77 C 1.00 5.75

101.06 101.08  
C 0.50

North

South

West stake	East stake	West stake	East stake
------------	------------	------------	------------

stakes /  $\frac{67}{1}$  back of curb line

1421

103.98	104.00
<del>3.98</del>	<del>3.96</del>
<del>3.98</del>	<del>3.96</del>
x	x

1410 1 stake only

103.46
<del>4.50</del>
<del>5.50</del>
F 1.00

0485

103.35	103.37
<del>4.61</del>	<del>4.59</del>
<del>5.61</del>	<del>5.59</del>
F 1.00	F 1.00

0460

103.73	103.75
<del>4.23</del>	<del>4.21</del>
<del>3.73</del>	<del>3.71</del>
00.50	00.50

0405 = Fixe Hydt. stub in place set grade on our line for Hydt.

106.99	103.01	103.93
<del>4.95</del>	<del>4.95</del>	<del>4.93</del>
<del>4.45</del>	<del>4.45</del>	<del>4.43</del>
00.05	00.05	00.05

0400 = E. Line Haines

398 107.96

107.96

103.98

Law St. Harris to Ingraham.

INDEXED  
WK  
FEB 16 1949

2+86

2+85

2+21

2+15

1+85

T.P. 5.82 110.02 3.76 104.20

1+71

107.96

North

West  
stake

East  
stake

104.64  
5.38  
5.38  
X

104.66  
5.36  
5.36  
X

104.38  
5.64

104.40  
5.62

104.18  
3.78  
3.78  
X

104.20 - T.P.  
3.76  
3.76  
X

107.96

South

76

West  
stake

East  
stake

104.18  
5.84  
7.34  
F 1.50

104.19  
5.83  
7.33  
F 1.50

103.89  
6.13  
7.13  
F 1.00

103.91  
6.11  
7.11  
F 1.00

103.77  
6.25  
7.23  
F 1.00

103.79  
6.23  
7.23  
F 1.00

110.02

North

West  
stakeEast  
stake

South

West  
stakeEast  
stake

77

4+36

$$\begin{array}{r} 106.98 \\ 3.54 \\ 3.54 \\ \hline F 0.50 \end{array}$$

$$\begin{array}{r} 107.10 \\ 2.92 \\ 3.42 \\ \hline F 0.50 \end{array}$$

4+85

$$\begin{array}{r} 106.39 \\ 3.63 \\ 3.63 \\ \hline X \end{array}$$

$$\begin{array}{r} 106.49 \\ 2.53 \\ 3.53 \\ \hline X \end{array}$$

3+96

$$\begin{array}{r} 106.00 \\ 4.02 \\ 4.02 \\ \hline X \end{array}$$

$$\begin{array}{r} 106.08 \\ 3.94 \\ 3.94 \\ \hline X \end{array}$$

3+85

$$\begin{array}{r} 105.29 \\ 4.73 \\ 5.23 \\ \hline F 0.50 \end{array}$$

$$\begin{array}{r} 105.36 \\ 4.66 \\ 5.16 \\ \hline F 0.50 \end{array}$$

3+47

$$\begin{array}{r} 105.18 \\ 4.84 \\ 4.84 \\ \hline X \end{array}$$

$$\begin{array}{r} 105.24 \\ 4.78 \\ 4.78 \\ \hline X \end{array}$$

3+35

$$\begin{array}{r} 104.54 \\ 5.48 \\ 5.98 \\ \hline F 0.50 \end{array}$$

$$\begin{array}{r} 104.55 \\ 5.47 \\ 5.97 \\ \hline F 0.50 \end{array}$$

110.02

110.02



South 78  
West stake East stake

sw. 71247  
Beryl & Ingraham 2.60 125.05 (125.08)

T.P. 10.60 127.65 1.49 117.05

T.P. 11.04 118.54 2.52 107.50

4+85

110.02

T.P.  
$$\begin{array}{r} 107.85 \\ 2.17 \\ \hline 109.97 \\ 10.50 \\ \hline 120.47 \end{array}$$
$$\begin{array}{r} 108.00 \\ 2.02 \\ \hline 110.02 \\ 10.50 \\ \hline 120.52 \end{array}$$

110.02

Locate Dead End  
Bangor + Harbor View Dr.

INDEXED

WIK

NOV 23 1948

Orig B.M. 5.58  $\frac{0.01}{269.47}$  ok

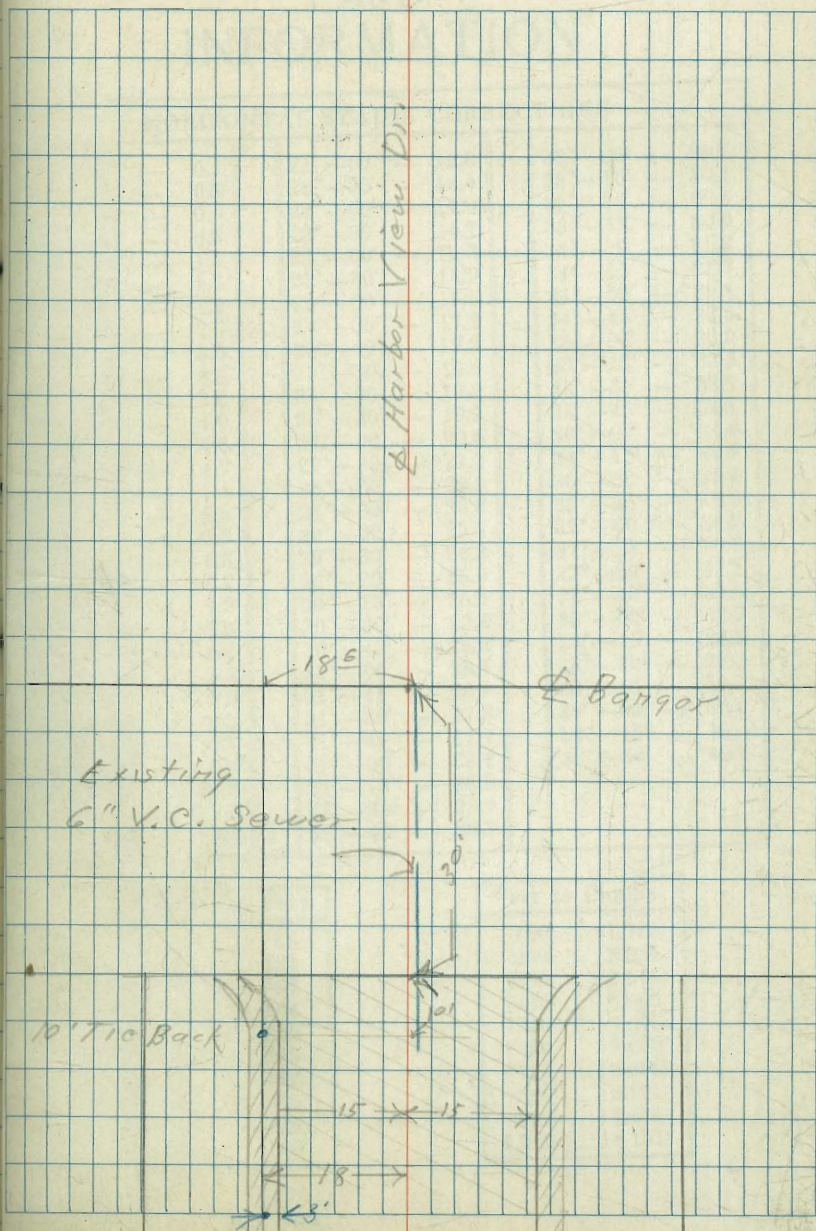
T.P. 12.19 275.05 0.33 262.86

Spike 5' S of D.E. 6.61 256.58 (7.88  
top of pipe)

D.E. of Bangor + Harbor Dr.

Top of 6" V.C. Sewer pipe 14.49 248.70

T.P. 0.68 263.19 12.40 262.51  
N.E. 10' x 8' Beck  
Lucinda +  
Bangor. 5.43 274.97 — 269.48



# IMPROVED TABLES AND INFORMATION

## HORIZONTAL STADIA CORRECTIONS

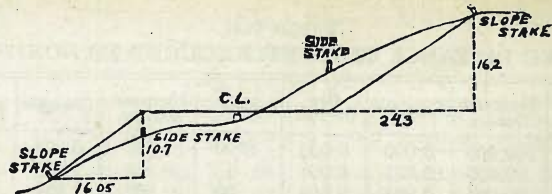
2°-00' — 0.1	21°-00' — 12.3	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

### Chains to Feet

1 .....	66
2 .....	132
3 .....	198
4 .....	264
5 .....	330
6 .....	396
7 .....	462
8 .....	528
9 .....	594
10 .....	660

### Feet to Chains

100 ....	1.515
200 ....	3.030
300 ....	4.545
400 ....	6.060
500 ....	7.575
600 ....	9.090
700 ....	10.606
800 ....	12.121
900 ....	13.636
1,000 ....	15.151



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

5.25  
13  
5.12  
5.07

5.210  
12  
5.21

7664

268.30  
255  
133

Cut stakes So. End Poo

Lat # 30 59.09  
 9.86 - Cut  
68.95  
 1.60 Rod  
70.55 X

4/14/47

15' Back East Ch. End 64.0  
 8+17.33 6.55  
1.37  
 C 5.18 = 5.2

3' Back West Curb End <sup>40</sup> 62.75  
 7+94.6 7.80  
8.20  
 7+41.9 - start Curb 70.10  
 7+48.4 " Walk  
 7+94.6 End Curb & Walk

389.47  
 V.W. Wilson

270  
 80  
 215

598  
 584  
150  
 734

316  
45  
 61  
 30  
 60

<sup>10.00</sup>  
3.37  
 6.65

5.10  
 + 50  
 5.60  
 - 1.00  
 4.60 Rod 5.60 Rod.

107.98  
28.03  
 110.03