

G-231

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ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803 CHICAGO

MICROFILMED

APR 13 1965

1-56 Grada Mission Valley Trunk Sewer Construction
SIX Pacific Hwy to City Line

57-79 City Line East

Grades Mission Valley Trunk Sewer #3
Southwest of Pacific Hwy to City Line

Stakes offset 10' R for South of 2 of Sewer

Alignment # 1786
2 Levels # 1788
H.O. 60131

July 9-47
S. S. Coy
McCoy
Waddel
Williams

INDEXED
WK

NOV 26 1948

Station	Description	Invert	Grade	Cuts	TP	BM	Notes	Top Rail	Other
+25		18.57 10.01 c8.56	-4.53	18.16 10.12 c9.04	TP 6.61	10.02	11.22	3.41 10.02	Top Rail 12.53
						10+43.7	For Jack	-3.98	-4.31
						40+337		-4.01	-4.34 12.56
					BM 4.81	8.22		3.41	on cut plus 10+30
38+0		18.64 9.94 c8.70	-4.60	19.23 10.74 c8.77		10+30	Fly Sacking	-4.62	18.65 11.22 c7.73
37+82	For Crotch		-4.64	12.66 -4.97					
37+70			-4.67	12.37 -5.00					
TP	3.06	7.67	9.43	4.61				-1.58	18.79 7.46 c11.53
BM	1.34	14.04		12.70					
37+70			-4.67	19.20 10.01 c9.29					
TP	6.20	14.63	12.17	8.43				18.26 8.55 c11.71	-4.22
TP	7.30	20.60	1.22	12.30					
36+10	Wly Sacking		-6.51	19.69 10.85 c8.74				18.32 4.18 c13.92	-4.28
	Drift on North fork line		-5.07						
	" 1/2 Below Grade		-6.60	Bottom Steel Pipe					
35+85	Grades pt.		-5.13	19.65 10.91 c8.74				18.39 11.02 c7.37	-4.35
35+45.88	Resisting Man Hole		-8.51	22.79 10.64 c12.15				18.45 11.14 c7.31	-4.41
	Invert Full		-8.27	on Rim					
BM	9.82	14.52	4.70	107 55795 55 9386 From Old Town Bridge				18.31 10.16 8.35	-4.47
									19.10 10.30 c8.80

14.63

+50

-3.56

13.38
5.76
8.22

+25

-3.70

13.71
5.63
8.07

+25

-3.40

13.42
4.97
8.45

42+0

18.75
16.76
27.99

-3.73

13.73
5.77
7.98

44+0

-3.43

13.45
4.59
8.06

+75

18.79
10.26
8.53

-3.77

13.79
5.26
8.53

+75

-3.47

13.46
4.64
8.95

+50

18.83
9.87
8.96

-3.81

13.83
4.88
8.95

+50

-3.51

13.53
4.64
8.89

+25

18.87
7.84
9.03

-3.85

13.87
4.84
9.03

+25

-3.55

13.57
4.64
8.93

41+0

18.90
10.07
8.87

-3.88

13.90
4.87
9.12

43+0

36"7

-3.58

13.60
4.64
8.64

+75

18.94
10.24
8.90

-3.92

13.94
5.24
8.90

+75

-3.62

13.64
5.04
8.60

40+55.13

A 3'49" 30" R.L.V.H. #1

18.97
14.24
9.73

-3.95

13.97
5.24
8.73

42+50

-3.66

13.68
5.04
8.68

8.M. 23

2.32 15.02

10.02

12.70

Santa Fe Br.

+75				-3.02	13.27 5.28 c7.77	49+0		-2.68	12.92 5.22 c7.71
+50				-3.06	13.31 5.22 c8.09	+75		-2.72	12.97 5.25 c7.41
+25				-3.09	13.34 5.21 c7.63	+50		-2.76	13.01 5.25 c7.55
46+0	POT MH#2			-3.13	13.38 5.20 c7.48	+25		-2.79	13.04 5.17 c8.57
TP	5.33	10.25	5.10	4.92	13.19 5.10 c8.09	48+0	=6" T	-2.83	13.08 5.21 c8.37
+75				-3.17					
+50				-3.21	13.33 5.25 c7.78	+75		-2.87	13.19 5.23 c7.97
+25				-3.25	13.37 5.27 c8.00	+50		-2.91	13.11 5.23 c7.70
45+0				-3.28	13.30 5.26 c7.77	+30		-2.93	13.18 5.23 c7.75
44+75				-3.32	13.34 5.27 c7.77	47+0		-2.98	13.23 5.20 c7.83

10.02

10.25

51±00	Equation				14.62			
51+38.42	Δ 2°30' 45" LT MH #3			-2.32	2.84 c8.78			
	T=0.22					+25		14.28 5.20 c9.68
TP	7.05	12.30	4.98	5.27				
51+0				-2.32	12.63 4.98 c7.65			
						53+0		-2.02
								14.37 5.32 c9.02
+75				-2.42	12.67 4.84 c7.83			
						+75		-2.06
								14.36 5.26 c9.70
+50				-2.46	12.71 5.03 c7.58			
						+50		-2.10
								14.40 4.94 c9.46
+25				-2.49	12.74 5.01 c7.53			
						+25		-2.13
								14.43 4.91 c9.52
50+0				-2.52	12.78 5.02 c7.26			
						52+0		-2.17
								14.47 4.85 c9.64
+75				-2.57	12.81 5.27 c7.67			
						+75		-2.21
								14.51 4.90 c9.61
+50				-2.61	12.86 5.07 c7.79			
						+50		-2.25
								14.55 5.40 c9.15
49+25				-2.64	12.88 5.09 c7.80			
						51+25		-2.28
								14.58 5.17 c8.47
	10.25							
						12.30		

Grades Mission Valley Trunk Sewer

Aug. 6-47
 8:55 AM
 McCoy Lumber
 Start 56+48.22

+75				-1.53	24.90 4.86 c26.04	58+0				-1.12	15.57 4.10 c11.44
+50				-1.60	24.97 4.99 c19.98	TP	2.76	14.45	12.65	11.69	15.50 12.55 c128.5
+25				-1.66	25.03 11.47 c13.56						25.54 11.78 c138.4
TP	11.93	23.37	0.86	11.44							
55+0	A 17° 26' MH #4			-1.72	14.02 1.31 c12.31						25.58 11.77 c138.1
+75				-1.76	14.06 2.36 c11.50						25.61 10.84 c150.7
						57+05		Fly Bridge			
+50				-1.80	14.10 3.33 c10.57						25.66 10.58 c152.0
						77'		Wly Bridge			25.66 30.00 20.01 old Town Br. 20.00
+25				-1.83	14.13 4.60 c9.53	BM	4.34	24.34	3.36		
						7+48.42		A 14° 10' MH #5			24.72 14.11 c13.61
54+0				-1.87	14.17 4.88 c9.27						
+25				-1.91	14.21 4.96 c9.23						24.78 0.52 c18.48
53+50				-1.95	14.25 4.81 c9.44	56+0					24.84 4.90 c19.94

12.30

23.37

0.0015

0.025

60+05.00 Equations
 60+06.467 = $\Delta 10^\circ 25' \text{ at } \text{MH} \#6$
 T=0.91

-0.81

15.26
 11.07
 c 4.25

+75 -0.86

15.31
 10.51
 c 4.80

+50 -0.90

15.33
 9.33
 c 6.00

59+27 x 02 Rip Rap -0.94

15.39
 8.23
 c 7.16

58+97 x 07 Rip Rap -0.97

15.42
 7.41
 c 8.01

+75 -1.01

15.46
 7.20
 c 8.26

+50 -1.05

15.50
 7.20
 c 8.30

58+25 -1.09

15.54
 5.19
 c 10.35

14.45

+2.7 x 07 Rip Rap

-0.48
 9.66
 6.09
 c 9.51

62+0 Stubs

-0.52
 9.64
 1.29
 c 8.75

+75 x

-0.56
 9.68
 1.20
 c 8.28

+52 x

-0.59
 9.71
 6.19
 c 9.54

+27

-0.63
 9.75
 2.09
 c 7.66

TP 249 9.12 782 6.63

60+97 x 07 Rip Rap -0.67

15.19
 8.19
 c 7.01

+76 x 07 Rip Rap

-0.71
 15.11
 8.27
 c 6.87

+18.5

-0.74
 15.19
 10.74
 c 7.45

60+25

-0.72
 15.33
 10.33
 c 4.90

14.45

		15' line		10' line		15' line		10' line	
+54	x	17.91 6.50 c11.41	-0.14	16.25 7.70 c8.55		17.83 5.38 c12.45	+0.20	15.98 6.88 c9.23	
TP	7.99	16.11	1.00	8.12					
+25	x	17.95 7.43 c11.52	-0.18	9.30 8.10 c9.20		17.87 5.02 c12.85	+0.16	15.95 5.79 c10.76	
					TP 15' line	5.41	18.03	5.15	12.62
6440	x	47.99 63.7 c11.62	-0.22	9.34 1.35 c7.99		17.65 5.16 c12.49	+0.12	15.99 6.18 c9.81	
RM Fork	12.02	17.77		5.75	oz stub MH '47				
+75	stas		-0.26	9.38 2.06 c7.32		17.69 5.29 c12.40	+0.08	16.01 6.44 c9.57	
+51	stas		-0.29	9.41 2.55 c6.86		17.72 5.00 c12.72	+0.05	16.06 6.15 c9.91	
+32.56	A 7° 03' R / MH '47		-0.52	9.44 3.87 c5.57		17.76 5.13 c12.63	+0.01	16.10 6.37 c9.73	
63+93	stas		-0.37	9.49 2.43 c7.06		17.80 4.86 c12.94	-0.03	16.14 6.37 c9.77	
+78	stas		-0.41	9.53 1.52 c7.97		17.84 4.72 c13.12	-0.07	16.18 6.80 c9.38	
62+50	x		-0.44	9.56 0.62 c8.94		17.88 5.27 c12.61	-0.11	16.22 6.94 c9.28	
		9.12			64+72	stas			
					17.97 Forks				
					16.11 Forks				

Sept 10.47
For 15' line
Sisson
Jr Cory Hanson

7

69+0			0.54	15.57 5.00 c10.57	+25	0.87	15.27 5.89 c9.38
T							
+75			0.50	15.61 4.91 c10.70	71+0	0.83	15.31 5.35 c9.96
6	+56.67	$\Delta 0^\circ 45' 11''$ MH #8 T=0.07	0.47	17.55 4.71 98.5 70	+75	0.80	15.31 4.75 c10.56
R							
+25			0.42	17.61 4.80 c12.78 75	+50	0.76	15.38 4.87 c11.01
68+0	Elev. 14.36	C 14.18 For Church	0.38	17.65 8.23 c14.42 5100	+25	0.72	15.42 4.13 c11.29
+78	a Ramp		0.35	17.68 3.49 c14.19	70+0	0.68	15.46 4.49 c10.97
63	+55		0.32	17.71 4.51 c12.60	+75	0.65	15.49 4.30 c10.69
+25			0.27	17.76 3.33 c12.44	TP	1.80	16.14
				15.84 5.25 c9.87	4.77	11.34	15.49 5.26 c10.03
62-67+0			0.23	17.80 4.84 c12.96	+44	Gas xing 12"	
				15.88 5.61 c10.27	69+24	0.57	15.51 5.03 c10.27
	16.11	18.02 For 18.02			16.11		

+50

1.21

14.93
4.18
c/10.75.

+75

1.51

15.67
6.83
c/9.04.

+25

1.17

14.09
4.93
c/10.04.

+50

1.51

15.70
6.04
c/9.66.

73+0

1.13

15.01
5.26
c/9.63.

+25

1.47

15.74
5.29
c/10.45.

+75

1.10

15.04
4.24
c/10.80.

75+0

1.43

15.78
4.24
c/11.04.

+50

1.06

15.08
5.73
c/9.35.

+75

1.39

15.82
3.83
c/12.74.

.0015

.0015

+25

1.02

15.11
5.92
c/9.22.

TP

427

17.21

3.20

12.94

+60

P.O.T

M.H #9
c/11.58 Fordbeck

1.37

14.77
3.20
c/11.57.

62 72+0

0.98

15.16
5.78
c/9.38.

+30

1.33

14.81
5.78
c/9.63.

+75

0.95

15.11
6.02
c/9.11.

74+0

1.28

14.81
5.22
c/9.64.

62 71+50

c/9.14 Fordbeck

0.91

15.23
6.13
c/9.10.

73+75

1.25

14.89
5.31
c/9.68.

16.14

16.14

Grades Mirror Valley Trunk Sewer #3

78+0		1.88	15.83 5.07 c10.32.	+25		2.22	14.99 2.14 c12.85.
+75		1.84	15.87 5.22 c10.17.	80+0		2.18	15.03 2.13 c12.70.
+50		1.81	15.40 5.86 c10.87.	+75		2.14	15.07 2.16 c12.97.
+25		1.77	15.44 5.51 c9.93.	+50		2.11	15.10 2.27 c12.83.
77+0		1.73	15.48 5.27 c10.21.	B.M.	571	11.50	14.07 10.41 79+21.11 11.53
	0.015			+25		2.07	15.14 2.28 c12.86.
+75		1.69	15.57 5.62 c9.88.	79+0		2.03	15.18 2.42 c11.76.
+50		1.66	15.58 6.00 c9.53.	+75		1.99	15.22 4.82 c10.60.
+25		1.62	15.59 6.22 c9.36.	+50		1.96	15.25 4.85 c10.40.
76+0	c9.14 for check	1.58	15.63 6.30 c9.13.	78+25		1.92	15.29 5.00 c10.26.
	17.21				17.21		

450				2.56	1786 218 c 10.72	
+25				2.57	1786 218 c 10.58.	
82+0				2.48	1790 211 c 10.77	
+75				2.41	1794 216 c 10.57	
+50				2.41	1797 214 c 10.50	
+25				2.37	1801 212 c 10.88.	
TP	7.17	20.38	4.00	1521	1804 210 81.50	
60 81+0	Δ	$3^{\circ}29'20''$	Δ	MH # 10	2.33	1788 210 c 10.88.
+75				2.29	1790 209 c 9.9	
62 80+50				2.26	1795 209 c 12.75.	

1721

+75				2.89	1786 218 c 10.72	Sept 19-47 S. 5000 McCoy #1180 8140 to 89406
+46.05	Δ	$3^{\circ}50'$	Δ	MH # 11	2.85	1753 218 c 12.77.
+25				2.82	1756 214 c 12.42.	
84+0				2.78	1760 218 c 12.52.	
+75				2.74	1764 216 c 11.94.	
+50				2.71	1767 214 c 11.78.	
+25				2.67	1771 212 c 11.54.	
85+0				2.63	1775 212 c 11.08.	
82+75				2.59	1779 212 c 11.05.	

2058

Page	Station	Notes	Reading	Correction	Sum	Station	Notes	Reading	Correction	Sum	Page
87	+0		3.23	20.07 8.61 c11.96		89	+06 to	3.57	19.31 2.99 c10.97		12
					+25						
	+75		3.19	20.11 8.02 c12.09	TP	89	+06	3.54	19.76 2.85 c11.91	3.22 16.93 9.59 13.91	
										$\Delta 17^{\circ}00'N$ MH #12 T=1.49	
	+50		3.16	20.14 7.24 c12.9				3.49	19.81 3.12 c11.69		
					+75						
	+25		3.12	20.18 7.42 c12.76				3.46	19.84 8.25 c11.99		
					+50						
	86	+0	3.08	20.22 7.41 c12.81				3.42	19.88 8.89 c10.97		
					+25						
	+75		3.04	20.28 8.22 c12.07				3.38	19.97 8.58 c11.34		
					+50						
	TP	8.89	23.30	5.97	14.41						
	+50		3.00	17.38 5.97 c11.41				3.34	19.96 8.52 c11.24		
					+75						
	+25		2.97	17.41 8.42 c10.99				3.31	19.99 8.86 c11.17		
					+50						
	85	+0	2.93	17.45 8.81 c11.27				3.27	20.03 8.86 c11.17		
					+25						

Sept 22-17
Sisson
Hille
Johnson
89+06 to

20.58

23.50

+50

3.91

13.02
3.10
c9.92.

9440

4.28

14.68
3.55
c11.13.

+25

3.87

13.01
3.12
c9.92.

TP

5.91

18.96

5.88

13.05

+65.00

10.19.30 "RT"
A 2 41.81 MH 13
T = 0.23

4.23

13.70
2.73
c10.97.

91+0

3.83

13.10
4.61
c8.49.

+22.5

4.18

13.75
1.46
c11.29.

+75

3.79

13.14
4.64
c8.48.

92+0

4.13

12.80
2.57
c10.23.

+50

3.76

.0015

13.17
4.66
c8.51.

+75

.0015

4.09

12.84
2.50
c10.34.

+25

3.72

13.21
3.68
c9.53.

+50

4.06

12.87
2.51
c10.36.

6 90+0

3.68

13.25
1.99
c11.26.

+25

4.02

12.91
2.87
c10.04.

+75

3.64

13.20
3.32
c10.46.

92+0

3.98

12.95
2.66
c10.29.

6 89+50

3.61

13.22
3.10
c10.22.

91+75

3.94

12.99
4.02
c8.96.

16.93

16.93

+25

4.62

14.31
6.68
c7.66
8

+25

4.92

10.49
5.26
c6.03

96+0

4.58

14.38
4.64
c9.74
8

8.17

5.02

10.59

54.630.34 Pt
97+87.02
10.63
10.73
5.79
c5.54

98+0

4.88

+75

4.55

14.41
3.64
c10.77
9

TP

5.18

15.61

8.53

10.43

0770 Pt
97+87.02
1.10
8.53
c5.57

+87.02

17°22'15" Pt M.H. 14
T 1.53

4.86

+50

4.51

14.45
3.67
c10.82
10

+75

4.85

14.11
8.42
c6.69

+25

4.47

14.40
1.29
c13.20

+50

4.81

14.15
8.07
c6.68

95+0

4.43

14.53
2.78
c11.80

+25

4.77

14.19
7.83
c6.36

+75

4.40

14.54
2.97
c11.65

97+0

4.73

14.23
7.76
c6.51

+50

4.36

14.60
3.32
c11.32

+75

4.70

14.66
7.68
c6.58

94+25

4.32

14.74
3.89
c10.95

96+50

4.66

14.36
7.53
c6.77
10

750	POT on 10' Pt	5.26	10.38 3.00 c7.38
725		5.22	10.39 3.16 c7.23
100+0		5.18	10.43 1.28 c9.15
+75		5.14	10.47 1.20 c9.27
+50		5.11	10.50 3.73 c6.77
+25		5.07	10.54 3.70 c7.84
6 99+0		5.03	10.58 3.60 c6.98
+75		4.99	10.61 4.04 c6.57
6 98+50		4.96	10.65 5.76 c4.89

15.61

+75				5.59	18.41 3.53 c13.88
+50				5.56	18.44 3.30 c15.14
+25				5.52	18.48 3.84 c14.64
TP	10.16	24.00	1.77	13.84	005705 10.19 102+0
102+0				5.48	19.13 1.78 c17.35
+75				5.44	19.17 1.61 c17.56
+50				5.41	19.20 1.76 c17.44
+25				5.37	19.24 2.34 c16.90
101+0				5.23	19.28 3.89 c15.39
100+75				5.29	19.32 3.86 c15.46

15.61

Grades Mission Valley Truck Sector 45

10540		5.93	18.87 8.26 c11.27	+25				6.26	14.51 7.89 c6.67
+75		5.89	18.11 1.84 c16.47	10710				6.23	14.54 8.26 c7.87
+50		5.85	18.15 1.98 c16.27	+75				6.19	14.58 7.53 c7.2
+25		5.81	18.19 0.21 c17.43	+50				6.15	14.62 7.43 c7.17
10410		5.78	18.21 1.12 c17.10	+25				6.11	14.66 7.44 c7.22
+75		5.74	18.24 1.5 c16.74	10640				6.08	14.69 7.50 c7.19
+50		5.70	18.30 3.12 c15.18	+75				6.04	14.73 8.26 c6.38
+33.32 +28.29	A 22° 52' N. M.H. 15 T=2.02	5.67	18.33 5.04 c13.27	+50				6.00	14.77 7.21 c7.35
10540		5.63	18.37 4.94 c13.43	TP	5.35	20.77	8.58	15.42	00540610 R 105435
				105425				5.96	18.07 8.58 c9.46
	24.00								
						24.00			

TP 2.96 18.67 5.06 15.71

+50.00 A 21° 06' 30" 44 MH #16
T=1.86

14.17
5.06
c9.11

6.60

+75

6.94

2.06
2.87
c10.99

+25

6.56

14.21
5.20
c8.81

TP

10.19

27.60

1.26

17.41

+50

6.90

11.77
1.26
c10.51

109+0

6.53

14.21
5.34
c8.90

+25

6.86

11.81
2.96
c9.69

+75

6.49

14.21
5.34
c8.97

111+0

6.83

11.84
2.87
c9.28

+50

6.45

14.37
4.77
c9.55

+75

6.79

11.88
2.89
c8.89

+25

6.41

14.31
6.39
c7.87

+50

6.75

11.92
3.28
c8.52

108+0

6.38

14.30
5.54
c8.72

+25

6.71

11.91
3.18
c8.86

+75

6.34

14.41
6.30
c8.10

110+0

6.68

11.99
3.58
c8.51

107+50

6.30

14.47
7.27
c7.20

109+75

6.64

12.03
3.61
c8.42

20.77

18.67

Oct. 6-47
 S. 1100
 M = Col
 Allen
 113+9070 to 127+91 =

+9376 $\Delta 66^{\circ} 22' 30''$ Lt. MH #18
 T = 6.54

7.27
 16.51
 5.52
 c 10.87

+25

7.62
 15.01
 5.02
 c 10.04

+68.1

7.23

116+0

7.58

15.10
 4.89
 c 10.21

B.M. 4.35 23.79

19.44
 on stub
 MH #17

+42.5 = 5/4 F Board Cape Strip

7.19

+75

7.54

15.14
 4.62
 c 10.52

23.1

113+19.4 = NY F Board " "

7.16

+50

7.51

15.19
 5.06
 c 10.17

20.1

+89.5 = NY F Board " "

0.015

7.11

+25

0.015

7.47

15.31
 3.89
 c 11.42

22.3

+66 = NY F Board Cape Strip

7.07

116+0

7.43

15.25
 4.91
 c 10.34

22.41

B.M. 2.33 25.27

20.54
 8.96
 c 11.58

+43.59 $\Delta 67^{\circ} 17' 30''$ Rt. MH #17
 T = 6.66

7.04

+75

7.39

15.29
 4.56
 c 10.74

+25

7.01

20.54
 7.87
 c 12.67

+50

7.36

15.34
 4.60
 c 10.74

112+0

6.98

20.62
 8.96
 c 11.66

TP

3.71

22.68

4.8

18.97

114+25

7.32

16.47
 5.62
 c 10.85

27.60

+60				7.97	16.15 8.86 c 7.89
+30				7.93	16.12 7.63 c 8.37
TP	7.49	24.12	6.05	16.63	16.12 7.63 c 8.37 11.87 9.85 16.65 17.88
118+0				7.88	16.80 7.70 c 10.18
+25				7.84	14.82 4.93 c 9.71
+50				7.81	14.87 5.82 c 9.05
+25				7.77	14.9 5.81 c 9.08
117+0				7.73	14.95 5.78 c 9.17
+25				7.69	14.91 5.74 c 9.17
116+50	" branch of T			7.66	15.07 5.90 c 9.72

22.68

121+0					8.33	15.79 5.81 c 10.18
+75					8.29	15.83 5.86 c 10.48
+50					8.26	15.86 5.89 c 10.57
+25					8.22	15.90 5.91 c 10.87
120+0					8.18	15.94 5.94 c 11.27
+75					8.14	15.98 5.97 c 11.63
+50					8.11	16.01 5.98 c 12.17
119+25					8.07	16.05 6.01 c 11.74
118+92.56	A 18° 10' 44" M H * 19 T = 1.60 24.12				8.02	16.10 6.03 c 9.57

Oct 8-47
S. Johnson
McCoy
F. Lee
25+46.68 to 47+15
20

+30
8.58
1541
416
c11.28

+25
9.04
1338
207
c8.81

123+0
8.68
1540
478
c10.7

27+0
9.00
1337
207
c8.85

+75
8.59
1533
502
c10.52

+75
8.96
1336
206
c9.41

+50
8.56
1534
462
c10.87

+50
8.93
1339
206
c9.82

+25
8.52
1569
523
c10.37

0015

+25
8.89
1343
207
c11.21

0015

122+0
8.48
1544
521
c10.42

26+0
8.85
1342
208
c11.39

+75
8.44
1568
522
c10.29

+75
8.81
1351
206
c11.86

+50 = 1" T
8.41
1571
523
c10.7

RM 175 2232
2850000
25+46.68 Equation
22+91.91 A 2° 36' 41" MH " 20
T = 0.25
576
8.81
20.57
18.31
8.77
18.40 17.88 W
1335
207
c11.80

121+25
8.37
1575
520
c10.45

122+60
8.72
1540
528
c11.92

2412

2412

+50

9.38
12.96
2.86
c 6.74

+70

9.71
11.19
2.16
c 6.77

+25

9.34
12.91
2.68
c 6.55

+40 P.O.T. MH "21

9.66
11.74
2.20
c 6.84

29+0

9.30
13.02
2.02
c 7.27

+20

9.63
11.27
4.12
c 7.15

+75

9.26
13.06
5.26
c 7.54

TP 4.39 20.90 5.81

16.51

31+0

9.60
12.72
5.81
c 6.91

+50

9.23
13.09
2.09
c 7.5

+75

9.56
12.76
6.12
c 6.59

+40 -6" T

+25

9.19
13.13
6.24
c 6.71

+50

9.53
12.99
2.19
c 6.5

28+0 P.O.T. 10' RT

9.15
13.17
2.02
c 10.19

+25

9.49
12.83
2.41
c 6.52

+75

9.11
13.21
2.21
c 11.00

30+0

9.45
12.97
2.22
c 6.75

27+50

9.08
13.24
1.24
c 12.03

29+75

9.41
12.91
2.25
c 5.96

22.32

22.32

3410		10.05	10.85 4.80 C 6.05	+25		10.39	10.56 4.75 C 6.36
+75		10.01	10.89 4.80 C 6.09	3610		10.35	10.55 4.50 C 6.29
+50		9.98	10.99 4.74 C 6.25	+75		10.31	10.50 4.80 C 6.96
+25		9.94	10.96 4.62 C 6.34	+50		10.28	10.62 4.50 C 6.06
3310	0015	9.90	11.00 4.52 C 6.48	+25		10.24	10.66 4.00 C 6.37
+75		9.86	11.04 4.21 C 6.83	3510	POTON 10' 6" 170	10.20	10.90 4.80 C 6.33
+50		9.83	11.07 4.20 C 6.87	+75		10.16	10.94 4.40 C 6.03
+25		9.79	11.11 4.20 C 6.91	+50	6" T	10.13	10.97 4.50 C 6.97
3210		9.75	11.15 4.21 C 6.94	34125		10.09	10.81 4.81 C 6.30
	20.90				20.90		

+75				10.77	11.60 1.38 c 10.22
+50				10.73	11.64 5.16 c 6.48
+25				10.69	11.68 4.94 c 6.74
38+0				10.65	11.74 4.96 c 6.78
+66				10.60	11.72 4.92 c 6.80
+32	P.O.T.	M.H. # 22		10.55	11.82 5.26 c 6.56
37+0				10.50	11.87 5.22 c 6.65
TP	5.45	22.37	3.98	16.92	02.54 36.75
+75				10.46	10.12 3.98 c 6.14
36+50				10.43	10.12 4.16 c 6.32

20.90

11+0

+75

+50

+25

10+0 -LIT

+75

+50

+25

39+0

22.37

11.10

11.07

11.03

10.99

10.95

10.92

10.88

10.84

10.80

0015

11.27
4.78
c 7.09

11.30
4.18
c 9.12

11.37
4.83
c 6.54

11.38
4.92
c 6.46

11.42
4.67
c 6.75

11.45
5.04
c 6.41

11.49
4.92
c 6.57

11.53
5.16
c 6.37

11.57
4.66
c 6.91

724	P.O.T.	MH #23		11.44	10.90 4.75 c 5.75	+50		11.28	10.56 5.09 c 5.77
4340				11.40	10.94 5.12 c 5.82	+25		11.74	10.60 5.02 c 5.58
775				11.37	10.97 5.00 c 5.97	+50		11.71	10.63 4.79 c 5.70
750				11.33	11.01 4.85 c 5.71	+75		11.67	10.67 4.77 c 5.70
725				11.29	11.05 4.45 c 5.70	+50		11.63	10.71 5.37 c 5.84
TP	441	22.34	441	1793					
4240			0.00	11.25	11.12 4.62 c 5.70	+25		11.59	10.75 5.07 c 5.78
775				11.22	11.15 4.16 c 5.99	+40		11.56	10.78 4.98 c 5.80
750				11.18	11.10 3.74 c 5.75	+75		11.52	10.88 5.09 c 5.75
41425				11.14	11.23 4.07 c 5.76	+350		11.48	10.86 4.63 c 5.83
		22.37							
							22.34		

Grade 5 Minnow Valley Trunk Section #3

Oct. 15-17 25

49+15 Lc

+75				12.12	11.91 6.88 c5.03							
						50+0				12.46	12.88 5.80 c7.08	
+50				12.08	12.01 6.96 c5.04					12.42	12.92 5.62 c7.30	
+25				12.04	12.04 6.65 c5.39							
TP	6.90	24.08	5/6	17.18		+50	on Ramp			12.38	12.91 5.68 c7.23	
47+0				12.01	12.33 5.22 c5.11	TP	6.10	25.34		19.24	07.54 to 10.91 49+15	
										19.86	07.8 to 10.3 19+15 19.24	
						+15	A 0° 34' 30" Rt. T 2.05		4.22	12.33	11.75 4.84 c6.91	
+75				11.97	12.37 4.36 c4.95							
						49+0				12.31	11.22 4.26 c6.98	
+50 = 6" T				11.93	10.44 4.32 c5.12							
						+75				12.27	11.86 4.88 c6.98	
+25				11.89	10.45 4.55 c5.90							
						+50				12.23	11.85 4.97 c6.88	
46+0				11.86	10.48 5.03 c5.45							
						+25	Ramp			12.19	11.88 4.80 c6.81	
45+75				11.82	10.52 5.09 c5.43							
						48+0				12.16	11.92 5.61 c6.31	
		22.34						24.08				

0015

+25			12.80	12.54 8.71 c5.83
52+0	- 1" Branch of T		12.76	12.58 8.79 c5.79
B.M.		6.96	18.38	1407.99 M 514.89 96 18.47
+75			12.72	12.62 8.66 c5.97
+50			12.68	12.66 8.46 c6.20
+25		2.00	12.65	12.69 8.29 c10.4 for force
51+0			12.61	12.70 8.19 c6.60
+75			12.57	12.77 8.16 c6.61
+50			12.53	12.81 8.06 c6.77
50+25			12.50	12.84 8.00 c6.84

2534

				For check		6.28	19.06	002 Hub 54+15.78 19.10 419.88
				+15.98	A 17° 22' 30" PL MH #25 T 1.53		13.08	12.56 8.33 c5.93
				54+0			13.06	12.28 8.22 c5.86
				+75			13.02	12.33 8.07 c6.01
				+50			12.98	12.36 8.22 c6.14
				+25			12.95	12.37 8.19 c6.96
				53+0			12.91	12.43 8.20 c6.73
				+75			12.87	12.47 8.46 c6.81
				52+50			12.83	12.51 8.57 c6.94

2534

7P		341	21.43	02 25/46 61406.48 21.47 H1981
61406.48	= Existing Sewer to Lateral Grades Page 54	9.66 2.69 68.97 15.18 Fat #2 Lateral	13.90 14.42	10.72 2.69 c 8.03 c 8.25
+75			13.87 14.07	10.77 2.92 c 7.79 7.79
+50			13.85 14.07	10.81 3.35 c 7.44 7.64
+25			13.82 14.00	10.86 3.35 c 7.47 7.47
60+0			13.79 13.96	10.88 3.44 c 7.44 7.61
+75		5100 20100	13.77 13.72	10.91 3.82 c 7.70 7.25
+50			13.74 13.88	10.96 3.90 c 7.07 7.20
+25			13.72 13.85	10.99 4.24 c 6.75 c 6.83
59+0			13.68 13.81	11.03 4.41 c 6.62 6.75

24.84

Grades Mission Valley Trunk Sewer #3
East of 6th St.

Rt -
Lt +

Oct 23-27
S. 5500
H. 600
H. 1100
18+75 to 90+84

29

Stakes offset 10 ft or South of Sewer

+50			15.64	$\begin{array}{r} 11.93 \\ 5.02 \\ \hline 6.88 \end{array}$	+75	16.09	$\begin{array}{r} 11.47 \\ 4.73 \\ \hline 6.74 \end{array}$
+25			15.59	$\begin{array}{r} 11.97 \\ 5.16 \\ \hline 6.72 \end{array}$	+50	16.04	$\begin{array}{r} 11.53 \\ 5.07 \\ \hline 6.45 \end{array}$
18+0			15.54	$\begin{array}{r} 12.02 \\ 5.16 \\ \hline 6.86 \end{array}$	+25	15.99	$\begin{array}{r} 11.57 \\ 5.08 \\ \hline 6.54 \end{array}$
+75			15.49	$\begin{array}{r} 12.07 \\ 5.16 \\ \hline 6.97 \end{array}$	70+0	15.94	$\begin{array}{r} 11.57 \\ 4.86 \\ \hline 6.96 \end{array}$
+51.86	A 12° 05' Rt T=100	M.H. #28	15.44	$\begin{array}{r} 12.12 \\ 3.23 \\ \hline 6.89 \end{array}$	+75	15.89	$\begin{array}{r} 11.67 \\ 4.91 \\ \hline 6.76 \end{array}$
+25			15.37	$\begin{array}{r} 12.19 \\ 5.63 \\ \hline 6.76 \end{array}$	+50	15.84	$\begin{array}{r} 11.72 \\ 4.73 \\ \hline 6.97 \end{array}$
67+0			15.31	$\begin{array}{r} 12.25 \\ 5.00 \\ \hline 6.95 \end{array}$	+25	15.79	$\begin{array}{r} 11.77 \\ 3.91 \\ \hline 6.86 \end{array}$
66+75.29	Exist. Sewer		15.25	$\begin{array}{r} 12.31 \\ 3.20 \\ \hline 6.72 \end{array}$	69+0	15.74	$\begin{array}{r} 11.82 \\ 4.53 \\ \hline 6.73 \end{array}$
B.M. Set		2.18	24.38	$\begin{array}{r} 5.15 \text{ offset} \\ 2.18 \text{ offset} \\ \hline 2.18 \end{array}$			
B.M.	5.67	27.56	21.89	$\begin{array}{r} 0.725 \text{ offset} \\ 67+57.86 \\ \hline 41703-59 \end{array}$	68+75	15.69	$\begin{array}{r} 11.87 \\ 4.77 \\ \hline 6.96 \end{array}$

2756

					+25				16.79	12.41 2.62 c 6.39
+75		16.49	11.07 4.66 c 6.71		74+0				16.74	12.46 3.92 c 6.54
+50		16.44	11.12 4.92 c 6.20		+66		6.05	23.15	0.25/04 23.12 1788	
					+66.00	P.O.T.	M.H. # 29		16.67	12.53 3.19 c 6.34
+25		16.39	11.17 4.82 c 6.33		+50				16.64	12.56 3.23 c 6.33
					TP	6.16	29.20	4.52	23.04	
72+0		16.34	11.24 4.72 c 6.50		+25				16.59	10.97 4.52 c 6.45
+75		16.29	11.37 4.87 c 6.40		73+0				16.54	11.02 4.91 c 6.31
+50		16.24	11.32 4.92 c 6.62							
+25		16.19	11.37 4.92 c 6.45							
71+0		16.14	11.42 4.92 c 6.44							

+50 17.24 $\begin{matrix} 11.96 \\ 4.89 \\ \hline c7.07 \end{matrix}$

+25 17.19 $\begin{matrix} 12.01 \\ 5.09 \\ \hline c6.92 \end{matrix}$

76+0 17.14 $\begin{matrix} 12.06 \\ 4.89 \\ \hline c7.17 \end{matrix}$

+75 17.09 $\begin{matrix} 12.11 \\ 5.36 \\ \hline c6.75 \end{matrix}$

+50 17.04 $\begin{matrix} 12.16 \\ 5.63 \\ \hline c6.53 \end{matrix}$

+25 16.99 $\begin{matrix} 12.21 \\ 5.46 \\ \hline c6.75 \end{matrix}$

75+0 16.94 $\begin{matrix} 12.26 \\ 5.69 \\ \hline c6.57 \end{matrix}$

+75 16.89 $\begin{matrix} 12.31 \\ 5.62 \\ \hline c6.69 \end{matrix}$

74+50 16.84 $\begin{matrix} 12.36 \\ 5.90 \\ \hline c6.46 \end{matrix}$

29.20

+75

+50

+25

78+0

+75

+50

+25

77+0

76+75

29.20

17.69 $\begin{matrix} 11.51 \\ 4.85 \\ \hline c6.66 \end{matrix}$

17.64 $\begin{matrix} 11.56 \\ 4.85 \\ \hline c6.71 \end{matrix}$

17.59 $\begin{matrix} 11.61 \\ 4.87 \\ \hline c6.74 \end{matrix}$

17.54 $\begin{matrix} 11.66 \\ 4.85 \\ \hline c6.81 \end{matrix}$

17.49 $\begin{matrix} 11.71 \\ 4.97 \\ \hline c6.74 \end{matrix}$

17.44 $\begin{matrix} 11.76 \\ 4.92 \\ \hline c6.84 \end{matrix}$

17.39 $\begin{matrix} 11.81 \\ 4.37 \\ \hline c7.44 \end{matrix}$

17.34 $\begin{matrix} 11.86 \\ 4.83 \\ \hline c7.03 \end{matrix}$

17.29 $\begin{matrix} 11.91 \\ 4.36 \\ \hline c7.55 \end{matrix}$

+25				18.15	12.44 4.59 c7.85
81+0				18.10	12.49 5.59 c6.90
+75				18.05	12.54 5.78 c6.76
+50				18.00	12.59 5.83 c6.76
80+25				17.95	12.64 5.88 c6.76
TP	5.29	30.59	3.90	25.30	02 2 stub 19.80.19 25.27.17.83
+99.93	Equation			17.90	11.30 4.03 c7.27
79+80.69	A 16.52 Rh M.H. 30 T=11.48				
+50				17.84	11.36 4.21 c7.15
+25				17.79	11.41 4.26 c7.15
79+0				17.74	11.46 4.51 c6.95

29.20

+50				18.60	11.99 5.05 c6.94
+25				18.55	12.04 5.00 c6.94
83+0				18.50	12.09 4.93 c7.16
+75				18.45	12.14 4.81 c7.33
+50				18.40	12.19 4.88 c7.31
+25				18.35	12.24 4.83 c7.41
82+0			P.O.T. on side here	18.30	12.29 5.01 c7.28
+51				18.22	12.37 4.91 c7.46
81+50			30.59	18.20	12.39 4.74 c7.65

+75				19.05	12.04 5.52 c 6.50				
TP	5.63	51.09	5.13	25.46	075705704 8.5770	88+0		19.50	11.59 5.12 c 6.47
+40.00	P.O.T.	M.H. 21		18.98	11.61 5.20 c 6.48				
+20				18.94	11.65 5.20 c 6.45	+75		19.45	11.64 4.79 c 6.85
85+0				18.90	11.60 5.20 c 6.41	+50		19.40	11.69 5.21 c 6.42
+75				18.85	11.74 5.16 c 6.58	+25		19.35	11.74 5.20 c 6.54
+50			0.02	18.80	11.79 5.12 c 6.67	87+0		19.30	11.79 5.15 c 6.64
+25				18.75	11.84 4.93 c 6.91	+75		19.25	11.84 5.20 c 6.64
84+0				18.70	11.89 4.98 c 6.91	+50		19.20	11.89 5.25 c 6.64
88+75				18.65	11.94 4.84 c 7.10	+25		19.15	11.94 5.20 c 6.74
						86+0		19.10	11.99 5.16 c 6.83
		50.59					81.09		

Oct 27-47
SUNCO
10000
7116
90+88 40 101+70

34

+25

1995

11.14
3.99
c7.15

+50

20.40

10.95
4.55
c6.36

90+0

1990

11.19
2.42
c8.57

+25

20.35

10.96
4.33
c6.55

+75
BM

325

1985
27.81

11.24
4.74
c7.70
SP 10 Pk.
1-4 RB 80+70
27.80 Pk.

92+0

20.30

11.01
4.46
c6.57

+50

1980

11.30
4.20
c6.80

+75

20.25

11.06
4.51
c6.55

+25

007

1975

11.34
4.22
c6.55

+50

007

20.20

11.11
4.50
c6.58

89+0

1970

11.39
4.10
c6.29

+25

20.15

11.16
4.48
c6.97

+75

1965

11.44
4.18
c6.26

91+0

20.10

11.21
4.24
c6.80

+50

1960

11.40
4.22
c6.27

TP

4.31 31.31 4.09
30.51.67
30.51.67
4.00.00
1.0.35
MH 32

27.00

00 8.57.66
90.7.87.03
26.91.1788-57

+81.03

20.07

11.08
4.28
c6.58

88+25

1955

11.54
5.22
c6.38

90+50

20.00

11.09
4.21
c6.88

31.09

31.09

+75		20.85	10.46 4.80 c5.66	TP	4.90	3129	4.82	26.49	
				97+0				21.30	10.01 4.82 c5.19
+50		20.80	10.57 4.82 c5.75	+75				21.25	10.66 4.74 c5.32
+25		20.75	10.56 4.80 c5.76	+50				21.20	10.46 4.70 c5.41
94+0		20.70	10.51 4.72 c5.57	+25				21.15	10.16 4.58 c5.48
+75		20.65	10.66 4.72 c5.92					0.02	
B.M.	4.59	26.62	02.00 35.11 26.62 02.00	9620153	4° 14' Δ 5° 05' RT MH #33 T=0.44			21.11	10.20 4.80 c5.40
+50		20.60	10.71 4.70 c5.01	+75				21.05	10.46 4.72 c5.54
+25		20.55	10.76 4.53 c5.88	+50				21.00	10.51 4.66 c5.75
93+0		20.50	10.81 4.53 c6.01	+25				20.95	10.56 4.81 c5.55
92+75		20.45	10.86 4.73 c5.72	95+0				20.90	10.41 4.84 c5.57

31.01

31.01

125	21.75	9.64 7.55 c5.69	TP	7.28	34.41	4.26	27.13	072.01031 161+70 2708-1788-71
			170	$\Delta 0^{\circ} 24' N$ P.O.T. MH *34			22.24	9.05 4.25 c4.97
99+0	21.70	9.19 4.89 c8.12	+50				22.20	9.19 4.07 c5.12
			+25				22.15	9.34 4.27 c4.97
+75	21.65	9.74 5.06 c4.74	101+0				22.10	9.39 4.36 c4.90
+50	21.60	9.79 4.85 c4.74	+75				22.05	9.31 4.02 c4.92
+25	21.55	9.84 5.28 c4.5	+50				22.00	9.39 4.55 c4.84
98+0	21.50	9.89 5.06 c4.53	+25				21.95	9.14 4.69 c4.84
+75	21.45	9.94 4.63 c5.31	100+0				21.90	9.19 4.66 c4.53
+50	21.40	9.99 4.24 c5.29	+75				21.85	9.54 4.86 c4.83
97+25	21.35	10.04 4.25 c5.29	99+50				21.80	9.53 4.22 c4.77

3139

3139

104+0

22.70

11.71
5.96
c 5.75

+25

23.15

11.56
4.83
c 6.61

+75

22.65

11.76
6.29
c 5.47

106+0

23.10

11.56
4.77
c 6.52

+50

22.60

11.81
6.75
c 5.66

+75

23.05

11.56
4.80
c 6.56

+25

22.55

11.86
6.64
c 5.22

+50

23.00

11.41
4.82
c 6.59

103+0

22.50

11.91
6.73
c 5.18

+25

22.95

11.46
4.91
c 6.52

+75

22.45

11.96
6.74
c 5.21

105+0

22.90

11.51
4.89
c 6.60

+50

22.40

12.01
6.78
c 5.23

+75

22.85

11.56
4.82
c 6.72

+25

22.35

12.06
6.78
c 5.28

+50

22.80

11.51
5.36
c 6.25

102+0

22.30

12.11
7.02
c 5.09

104+25

22.75

11.66
5.86
c 5.70

34.41

34.41

Oct 30-17 38
101+70 + 0.118+50

+75

23.66

11.56
5.28
0.6.28

111+0

24.11

10.91
4.68
0.6.23

+50

23.61

11.41
5.12
0.6.27

+75

24.06

10.96
4.71
0.6.25

+25

23.56

11.46
5.17
0.6.32

+50

24.01

11.01
4.67
0.6.34

108+0

23.51

11.51
5.22
0.6.34

+25

23.96

11.06
4.69
0.6.37

+65

23.44

11.58
5.09
0.6.36

TP

5.05

35.02

4.44

0.02

29.97

on stub
10.97 10.74 10

110+0

0.02

23.91

11.11
4.85
0.6.26

+30

P.O.T. MH #35

23.37

11.01
4.94
0.6.60

+75

23.86

11.16
4.90
0.6.22

107+0

23.30

11.11
4.87
0.6.62

+50

23.81

11.21
4.89
0.6.32

+75

23.25

11.16
4.89
0.6.67

+25

23.76

11.26
4.82
0.6.44

106+50

23.20

11.21
4.84
0.6.59

109+0

23.71

11.31
4.83
0.6.43

34.41

35.02

+25 24.56 ^{10.46}_{4.38} c6.08

113+0 24.51 out

+90.00 POT MH # 36 24.49 ^{10.53}_{4.24} c6.09

+60 24.43 ^{10.59}_{4.47} c6.12

+30 24.37 ^{10.65}_{4.52} c6.12

112+0 24.31 ^{10.71}_{4.58} c6.13

+75 24.26 ^{10.76}_{4.59} c6.17

+50 24.21 ^{10.81}_{4.62} c6.17

111+25 24.16 ^{10.86}_{4.59} c6.27

55.02

+50 25.01 ^{10.78}_{4.83} c6.95

+25 24.96 ^{10.83}_{4.85} c6.88

115+0 24.91 ^{10.88}_{4.82} c6.84

+75 24.86 ^{10.93}_{4.85} c6.88

+50 24.81 ^{10.98}_{4.89} c6.79

+25 24.76 ^{11.03}_{5.00} c6.03

TP 4.90 35.79 4.13 30.89 ^{0.7545}_{10.81} 11410

114+0 24.71 ^{10.81}_{4.73} c6.18

+75 24.66 ^{10.86}_{4.68} c6.27

113+50 24.61 ^{10.91}_{4.71} c6.24

55.02

+75		25.46	10.33 4.33 c 6.00
+50		25.41	10.33 4.33 c 5.99
+25		25.36	10.43 4.43 c 5.87
117+0		25.31	10.43 4.43 c 5.86
+75		25.26	10.53 4.53 c 5.84
BM	2.38	33.41	CHINA D. HAN CULTURE 59/11/16/19 33.37
+50		25.21	10.63 4.63 c 5.82
+25		25.16	10.63 4.63 c 5.78
116+0		25.11	10.63 4.63 c 5.75
115+75		25.06	10.73 4.73 c 5.87

3579

				120+0				110.327 118+50	40
				+75				25.91	11.27 4.27 c 6.30
				+50				25.86	11.37 5.37 c 6.72
				+25				25.81	11.37 5.35 c 6.02
				+75				25.76	11.47 5.47 c 6.28
				119+0				25.71	11.47 5.36 c 6.77
				+75				25.66	11.57 5.30 c 6.24
				TP	4.85	37.18	3.46	32.33	07.57+6 10.18/118+50
				+50.00	A 12° 22' 41"	MH 437		25.61	10.18 4.18 c 5.92
					T=1.08				
				+25				25.56	10.28 4.27 c 5.96
				118+0				25.51	10.28 4.28 c 5.88

3579

Grades Mission Valley Truck Service

+25	26.36	10.82 4.86 c5.96
122+0	26.31	10.87 4.87 c5.00
+75	26.26	10.91 4.82 c6.08
+50	26.21	10.97 4.76 c6.21
+25	26.16	11.02 4.73 c6.29
121+0	26.11	11.07 4.72 c6.35
+75	26.06	11.12 4.68 c6.44
+50	26.01	11.17 4.67 c6.50
120+25	25.96	11.21 4.63 c6.58

3718

TP	13.03	46.71	3.50	33.68	41
+50				26.81	10.57 4.56 c6.87
+25				26.76	10.42 4.64 c6.38
121+0				26.71	10.17 4.35 c6.22
+75.00	POT	MH #38		26.66	10.52 4.53 c5.97
+50				26.61	10.57 4.54 c6.03
+25				26.56	10.62 4.81 c6.01
123+0				26.51	10.67 4.65 c6.02
+75				26.46	10.72 4.78 c5.94
122+50				26.41	10.77 4.66 c5.97

3718

+75			2439	2726	26.06 11.02 c15.02	TP	149	46.67	12.08	45.18	005406 42 10 ft 129+00
							129+00	$\Delta 6^{\circ} 17' 30''$ RT MH " 39 T=0.57		27.71	29.55 27.28 c19.77
+50			2444	2721	26.11 9.27 c16.84						
							175	Re-Station	23.99 5.12 c18.85	27.66	29.60 10.00 c19.60
+25				2716	26.16 28.04 c28.72			45.18 6.47 51.65T			
TP	754	53.32	0.93	45.78	0.70405 10 ft 126+00		+50			27.61	29.65 9.23 c19.73
126+0	= 6" Chimney		2454 5.87 c18.57	27.11	19.60 6.92 c18.58						
							+25		21.09 2.86 c20.23	27.56	29.70 9.50 c20.20
+75				27.06	19.65 6.49 c19.74						
							128+0	= 6" Chimney		27.51	29.75 9.68 c21.67
+50				27.01	19.79 6.91 c18.77						
							+75		24.19 5.21 c20.78	27.46	29.80 5.22 c20.78
+25				26.96	19.75 5.69 c14.76						
							+50		24.34 4.79 c19.75	27.41	29.85 5.58 c20.27
125+0				26.91	19.80 11.10 c8.9						
							+28		24.28 6.37 c19.91	27.37	29.89 5.86 c20.93
124+75				26.86	19.85 11.65 c8.20		TP	762	57.26	368	49.64
							127+0				
									24.39 8.00 c16.39	27.31	28.01 10.04 c15.97
			46.71					5232			

+25		2816	1851 6.49 c11.57
131+0		2811	1851 5.21 c13.33
+75		2806	1861 21.50 c14.5
+50		2807	1866 38.80 c15.11
+25		2796	1871 3.22 c15.72
130+0	003	2791	1876 3.33 c15.43
+75		2786	1881 3.15 c15.66
+50	6" Chimney	2781	1886 2.71 c15.15
129+30		2777	1896 1.98 c15.12

46.67

+50		2861	1832 2.03 c7.50
+25		2856	1857 2.19 c7.71
133+0		2851	1862 2.38 c7.24
+75		2846	1867 3.83 c7.85
TP	7.90	42.12	12.44
+50		2841	1826 12.44 c5.82
+25		2836	1851 11.08 c7.23
132+0		2831	1856 10.27 c8.75
+75		2826	1841 8.98 c9.13
131+50		2821	1846 7.69 c10.77

46.67

+75			29.32	12.81 7.10 c8.71
+50			29.22	12.91 7.11 c8.60
+25			29.12	13.01 7.12 c8.55
13540			29.02	13.11 7.13 c8.44
+725			28.91	13.22 7.14 c8.33
+15.00	P.O.T.	M.H. 40	28.80	13.33 7.15 c8.22
+22.5			28.75	13.43 7.16 c8.11
13440			28.71	13.53 7.17 c8.00
133475			28.66	13.63 7.18 c7.89

42.13

13840

+75

+60

+25

13740

TP

+75

+50

+25

13640

12.39 53.79 0.72

30.22

30.12

30.02

29.92

29.82

41.40

29.72

29.62

29.52

29.42

23.57
6.94
c16.63

23.67
7.82
c15.85

23.77
8.72
c15.05

23.87
9.62
c14.25

23.97
10.52
c13.45

24.07
11.42
c12.65

24.17
12.32
c11.85

24.27
13.22
c11.05

24.37
14.12
c10.25

42.13

+2.5				31.12	21.39 5.39 c16.00
140+0				31.02	21.49 5.57 c15.92
TP	5.66	52.51	6.94	46.85	
+88.50	A 14°26' Pt. MH # 41 T=1.37			30.97	22.82 6.95 c15.87
+50				30.82	22.99 6.15 c16.84
+2.5				30.72	23.07 6.37 c16.70
139+0				30.62	23.17 6.57 c16.60
+7.5				30.52	23.27 6.77 c16.50
+50				30.42	23.37 6.97 c16.40
138+25				30.32	23.47 7.17 c16.30

53.79

+50				32.02	20.48 1.58 c18.81
+2.5				31.92	20.59 1.78 c18.81
				2.78	Point A HW Ck 26 ft 122+150 ft 49.73
142+0				31.82	20.69 1.98 c18.71
+7.5				31.72	20.79 2.18 c18.61
+50				31.62	20.89 2.38 c18.51
+2.5				31.52	20.99 2.58 c18.41
141+0				31.42	21.09 2.78 c18.31
+7.5				31.32	21.19 2.98 c18.21
140+50				31.22	21.29 3.18 c18.11

52.51

.004

.004

sand Rock Grade
B.M. + Camino Del Rio

+25 33.67 $\frac{13.39}{2.94}$
 -8.45

+75

34.07 $\frac{16.26}{8.55}$
 -7.71

149+0 33.62 $\frac{13.44}{6.26}$
 -7.24

+50

34.02 $\frac{16.31}{8.54}$
 -7.77

+75 33.57 $\frac{13.49}{6.23}$
 -7.26

+25

33.97 $\frac{16.36}{8.15}$
 -8.21

+50 33.52 $\frac{13.54}{6.20}$
 -6.74

150+01.32 J
149+99.967

33.92 $\frac{16.41}{8.03}$
 -8.38

+25 33.47 $\frac{13.59}{6.25}$
 -6.58

20.16

179.20

33.88 $\frac{16.45}{8.13}$
 -8.33

100

TP

8.49 50.55 5.22

41.84 $\frac{16.50}{8.05}$
 $-150+119.0$

148+0 33.42 $\frac{13.64}{6.32}$
 -7.26

149+58.64 J
150+119.07

$\Delta 16^{\circ}08'30''$ 11.43
 $T=1.41$

33.84 $\frac{16.53}{8.02}$
 -8.72

+75 33.37 $\frac{13.69}{6.09}$
 -7.66

150+0

33.82 $\frac{16.54}{8.00}$
 -8.34

+50 33.32 $\frac{13.74}{5.76}$
 -6.38

+75

33.77 $\frac{16.59}{5.27}$
 -8.08

147+25 33.27 $\frac{13.79}{5.49}$
 -6.30

149+50

33.72 $\frac{16.61}{5.19}$
 -8.14

47.06

47.06

153+0		34.52	$\frac{15.81}{5.25}$ c10.56	+25		34.99	$\frac{15.31}{1.89}$ c13.45		48
+75		34.47	$\frac{15.86}{6.91}$ c9.95	155+0		34.92	$\frac{15.11}{3.10}$ c12.01		
+50		34.42	$\frac{15.91}{7.01}$ c8.90	+75		34.87	$\frac{15.46}{3.87}$ c12.09		
+25		34.37	$\frac{15.96}{7.92}$ c8.24	+50		34.82	$\frac{15.51}{3.84}$ c11.67		
152+0		34.32	$\frac{16.01}{8.00}$ c8.01	+25		34.77	$\frac{15.56}{7.28}$ c11.28		
+75	0.05	34.27	$\frac{16.06}{7.51}$ c8.55	154+0		34.72	$\frac{15.61}{4.72}$ c10.89		
+50		34.22	$\frac{16.11}{8.01}$ c7.80	+75		34.67	$\frac{15.66}{4.76}$ c10.90		
+25		34.17	$\frac{16.16}{8.28}$ c7.88	+50		34.62	$\frac{15.71}{4.68}$ c11.03		
151+0		34.12	$\frac{16.21}{8.25}$ c8.18	153+25		34.57	$\frac{15.76}{4.87}$ c10.89		

50.83

50.83

+75				35.47	19.46 4.17 c 15.29	16040	35.92	19.01 4.56 c 14.45
+56				35.42	19.51 4.21 c 15.30	+75	35.87	19.06 4.39 c 14.67
+25				35.37	19.56 4.38 c 15.18	+50	35.82	19.11 4.81 c 14.30
15740				35.32	19.54 4.29 c 15.25	+25	35.77	19.16 4.88 c 14.28
+75				35.27	19.66 4.56 c 15.10	15940	35.72	19.21 4.89 c 14.32
+50				35.22	19.71 4.76 c 14.95	+75	35.67	19.26 5.12 c 14.14
+25				35.17	19.76 5.29 c 14.47	+50	35.62	19.31 4.96 c 14.35
15640				35.12	19.81 5.29 c 14.52			
TP	6.10	54.93	1.50	48.83	0.0506 10.8118520	+25	35.57	19.36 4.78 c 14.58
155470.00	P.O.T	M.H # 44		35.06	13.27 1.50 c 11.77	15340	35.52	19.41 4.40 c 14.92
		50.33						
						5493		

+25

36.37

14.93
2.57
c12.36

+50

36.82

14.48
2.55
c7.93

162+0

36.32

14.91
2.58
c12.33
on 5/10/1074
161+90

+25

36.77

14.53
2.03
c7.50

TP

2.87

57.30

6.50

48.43

+90.00

A 42° 55' L
7-393

MH 45

36.30

18.63
6.50
c12.13

164+0

36.72

14.58
7.10
c7.48

+60

36.24

18.69
6.45
c12.24

+75

36.67

14.63
7.31
c7.32

+30

36.18

18.75
6.47
c12.28

+50

36.62

14.68
7.18
c7.50

161+0

36.12

18.81
6.46
c12.35

+25

36.57

14.72
7.06
c7.66

+75

36.07

18.86
6.32
c12.54

163+0

36.52

14.78
3.18
c11.60

+50

36.02

18.91
6.50
c12.41

+75

36.47

14.83
7.32
c7.51

160+25

35.97

18.96
4.27
c14.69

162+50

36.42

14.88
7.14
c7.74

54.93

51.30

Nov. 17-17
5:50
7°C
71100

51

+75 37.27 $\frac{18.95}{2.87}$
c 12.08

+62 = E Wall Spillway 0710 line 37.64

18.38
9.67
c 8.91

+50 37.22 $\frac{19.00}{2.08}$
c 10.92

+55 = W Wall Spillway 0710 line 37.63

18.59
9.78
c 8.97

+25 37.17 $\frac{19.05}{3.71}$
c 10.34

B.M. #43 9.93 46.29

8. P. W. 1907
Spillway caln.
1.571 16.153
46.21

166+0 37.12 $\frac{19.10}{9.30}$
c 9.78

+46 37.61

18.61
3.57
c 15.04

TP 10.20 56.22 5.28 46.02 $\frac{0.75 \text{ total pt}}{1.65 + 76.18}$

+25 37.57

18.65
3.98
c 14.77

+75.68 A 13° 21' 30" Rt M.H. #46 37.07 $\frac{14.33}{5.44}$
c 8.92

168+0 37.52

18.78
2.48
c 14.31

+50 37.02 $\frac{14.41}{5.40}$
c 8.88

Note: Levels checked
From Wood Post Stone to B.M. #43
46.29 - 46.27

0.02

+75 37.47

18.75
5.06
c 13.69

+25 36.97 $\frac{14.33}{5.65}$
c 8.68

+50 37.42

18.80
5.28
c 13.52

165+0 36.92 $\frac{14.38}{6.28}$
c 8.76

+25 37.37

18.88
5.00
c 13.88

164+75 36.87 $\frac{14.43}{6.57}$
c 8.74

167+0 37.32

18.90
6.47
c 12.43

51.50

56.22

169 + 46.73 = Fly Expt Ppc 13.88 37.83 Nov. 26.47

BY 501 2.42 51.71 166 49.29
C540/110/100
Cone P. 10/10
H. Fed. Capital
F. J. O. H. R. 01

TP 4.10 50.95 40.5 46.85

+ 48.73 37.82 13.08
10.05
09.03

+ 40.73 A 30.13 R 20 H # 47 37.80 13.10
4.11
08.77

+ 20 37.76 13.14
4.11
08.77

169 + 0 37.72 13.18
4.11
08.77

TP 4.61 50.90 9.93 46.29
56.22

Grader Senter Material #1
 Mission Valley Trunk #3
 Stakes off set 10' R of 2 or 4

Oct 7-47
 S: 5607
 McCoy
 Filled

For Check 317 4711 00 R 100
 1457.04
 47.08 Pa.

+57.04 - First M.H. 4238 79°
 360
 0 4.8°

TP 7.86 50.28 112 4242 8.33
 +25 35.22 172
 07.8°

140 2963 1391
 568
 08.2°

INDEXED
 WIC
 NOV 26 1948

+75 24.04 19.50
 10.53
 08.91

TP 12.55 43.54 0.50 30.99 13.04
 +50 18.45 582
 08.8°

+25 12.86 18.63
 13.67
 08.8°

040 = 113+93.70 M.H. #18 7.27

BM 13.56 31.49 18.23 0754610
 113+93.70
 Page 18

INDEXED
 NOV 26 1948

Grader Sewer Lateral #2
 Mission Valley Trunk #3
 Stakes offset 10 ft or more of 2

Oct 15-47
 S. Siro
 McCoy
 7/1/57

INDEXED
 WK
 NOV 26 1948

+50		20.58	15.32 7.32 c6.00	+45				27.97	17.88 9.94 c7.94
+25		19.68	14.23 7.24 c6.28	+35	MH 26 H. P.O.T.			27.24	18.61 10.47 c8.14
+10		18.78	15.12 8.12 c6.94	TP	12.19	15.85	0.24	33.66	7.93 1.22 c6.71
+75		17.88	16.02 10.22 c5.32	+30				25.98	
+50		16.98	16.92 12.21 c5.71	+75				15.08	8.83 4.22 c4.61
+25		16.08	17.82 11.82 c5.94	+50				24.18	9.72 5.68 c4.04
0+0	614 06.48 MH #26	15.18	c6.94 P.O.T. 25	+25				23.28	10.62 6.78 c4.52
BM	1247 33.90	21.43	0.72 Stak 81+06.48 P.O.T. 28	+10				22.38	11.52 6.58 c4.94
				+75				21.48	12.42 7.02 c5.36

06.90

TP 10.00 91.49 0.97 81.49

+70

66.30

16.16
0.97
15.19

+60

62.24

19.22
3.52
15.70

+98.85 - FRANKLIN

11.96
0.72

79.59

11.90
1.31
10.59

+40

56.52

25.94
9.97
15.97

+75

77.66

13.83
2.87
10.96

TP 12.12 82.46 0.41 70.34

+20

49.80

20.85
5.05
15.80

+50

75.63

15.86
8.15
7.71

+10

43.08

27.88
14.32
13.56

+25

73.60

17.80
8.09
9.71

TP 12.79 70.75 0.14 57.96

+75

34.68

23.11
9.86
13.25

+50

71.58

19.91
7.92
11.99

TP 12.48 58.10 0.23 45.62

+12.39

Δ 5° 03' 30" N
T: 0.24

31.12

14.50
4.97
9.53

+90

70.49

21.00
7.95
13.05

+3+55

29.46

16.89
0.27

+120

68.68

22.81
8.63
14.18

45.85

91.49

ReStake Server Lateral #2
3+0 to 5+98.85

Oct. 21-47
J. W. 100
M. Coy
F. 1/67

+20		-3.69	44.11	49.80	16.28 6.52 c/9.76 5.79 c/15.62	+98.85 - Fric. MH	0.0	79.59	79.59	8.67 +1.92 10.59 Sub	
TP	11.86	65.08	0.30	65.22	10.44 0.30 c/10.74	+75	-2.80	74.86	77.66	10.60 2.60 c/10.80	
1+0		-2.94	40.14	43.08	2.94 c/3.08	+50	-5.72	69.90	75.62	1.53 2.71 c/4.24 5.75 c/3.82	
+75		+0.49	35.17	34.68	18.86 7.99 c/11.55 0.49 c/10.86	+85	-8.66	64.94	73.60	14.66 6.25 c/8.71 3.66 c/17.07	
+62.39	As 0.230%	71.55	32.67	31.12	22.10 11.04 c/11.32 1.55 c/9.81	5+0	-11.60	59.98	71.58	16.68 9.91 c/6.97 11.60 c/18.37	
TP	13.21	53.52	0.48	40.31	11.53 1.42 c/10.55 1.74 c/9.13	TP	11.19	88.26	0.11	77.07	6.60 0.11 c/6.59 12.50 c/17.08
+55		+1.74	31.20	29.46		+90	-12.50	57.99	70.49		
+45		+1.25	29.22	27.97	12.84 2.86 c/10.46 1.33 c/9.21	+80	-12.67	56.01	68.68	8.30 2.00 c/6.30 12.67 c/18.87	
+35	MH 2LH Pot. ties 10+10	0.0	27.24	27.24	13.55 4.00 c/9.55	+70	-12.27	54.03	66.30	10.88 4.57 c/6.31 12.87 c/18.18	
3+0				2598	14.81 8.60 c/6.21	+60	-11.19	52.05	63.24	13.94 2.63 c/6.31 11.78 c/17.15	
B.M.	11.65	40.99		29.14	0.25 2.75 1.95	TP	12.19	77.18	0.07	65.01	8.26 0.31 c/9.95 8.44 c/6.19
						+40	-8.44	48.08	56.52		
							65.08				

Grades Mission Valley Trunk Sewer #3
City Line East

No. 60162.

Sommermeier
McCoy
Moore
Sherman

Jan. 19-48
S. 5502
H. 167
Smith

57

172+3551 ← 38.59 $\frac{14.94}{6.98}$
C 7.96

T.P. 6.98 53.33 3.79 46.35

175+3682 $\Delta 25^{\circ} 51' 30''$ L.M.H. 48
T = +2.30

39.10 $\frac{14.23}{4.46}$
C 9.77

171+9124 38.50 $\frac{11.84}{4.43}$
C 7.41

175+4280

39.02 $\frac{14.31}{5.01}$
C 9.30

171+5314 38.22 $\frac{11.92}{5.22}$
C 6.70

175+1076

38.94 $\frac{14.39}{7.15}$
C 7.24

171+1204 38.14 $\frac{12.00}{5.76}$
C 6.24

174+7272

38.87 $\frac{14.46}{7.18}$
C 7.28

170+7094 38.05 $\frac{12.09}{5.12}$
C 6.97

174+3418

38.79 $\frac{14.54}{7.22}$
C 7.32

170+2984 37.97 $\frac{12.17}{2.14}$
C 10.03

173+9664

38.72 $\frac{14.61}{6.24}$
C 8.37

169+8874 37.88 $\frac{12.26}{3.96}$
C 8.30

6-3804

173+5860 $\Delta 41^{\circ} 20' 00''$ L.M.H. 48
T = +3.77

38.64 $\frac{14.69}{4.29}$
C 10.40

10-4110
169+4764 37.80 $\frac{12.34}{3.32}$
C 9.02

173+1764

38.57 $\frac{14.77}{6.52}$
C 8.25

B.M. From Page 52 0.85 50.14 49.29

72+7164

38.47 $\frac{14.86}{6.30}$
C 8.06

53.33

177+0

3975

12.44

6.55

C 5.89

+60

40.47

11.72
5.59
C 6.13

178+60

7' offset From here

3967

12.52

6.07

C 6.49

182+20

10' offset

40.39

11.80
4.78
C 7.02

T.P. M.H.

12.57 R.P.

3.24

52.19

12.84

48.95

SS M.H. + 10

SS. on nub.

178+2894

Δ 28° 50' P.A. M.H. * 50

39.61

22.18

12.84

C 9.34

+80

End 7' offset

40.31

11.88
3.66
C 8.22

178+4189

T - 2.57

178+0547

39.54

22.25

13.25

C 9.00

+10

40.23

14.96
4.16
C 7.80

177+69.03

39.46

22.33

8.31

C 14.02

181+0

300

40.15

12.04
4.14
C 7.90

T.P.

10.60

61.79

2.14

51.19

177+2259

300

39.39

13.74

1.95

C 19.79

180+60

40.07

12.12
4.10
C 8.02

176+9615

39.32

14.01

4.36

C 9.15

180+20

39.99

12.20
4.33
C 7.87

176+5971

39.25

14.08

6.22

C 7.81

179+80

39.91

12.28
4.71
C 7.57

176+2327

39.17

14.16

6.58

C 7.58

179+60

39.83

12.36
5.48
C 6.88

7-2644

53.33

52.19

BM # 45 - 1629 - 7			0.89	54.41	54.39
TiR 6.05	55.30		3.90	49.25	
280+61				46.20	$\frac{11.95}{4.55}$ C 7.40
280+22.10				41.12	$\frac{12.03}{4.43}$ C 7.60
12-38.9					
279+83.20				41.04	$\frac{12.11}{1.50}$ C 10.61
1857+22.86	Δ 28° 44' 30" = MH # 51				
					T = +2.86
185+10				40.95	$\frac{12.20}{2.27}$ C 9.93
184+60				40.87	$\frac{12.28}{2.77}$ C 9.31
184+20				40.79	$\frac{12.36}{2.77}$ C 9.37
480				40.71	$\frac{12.44}{4.30}$ C 8.14
440				40.63	$\frac{12.52}{5.68}$ C 6.84
183+0				40.55	$\frac{12.60}{7.21}$ C 5.37
	6.55	53.15	5.59	46.60	
		52.19			

							59
284+161						41.89	$\frac{13.38}{2.08}$ C 11.30
283+22.2						41.81	$\frac{13.46}{2.38}$ C 11.08
283+333						41.74	$\frac{13.53}{3.05}$ C 10.48
282+911						41.66	$\frac{13.61}{3.58}$ C 10.03
282+555						41.58	$\frac{13.69}{4.18}$ C 9.51
282+166						41.50	$\frac{13.77}{4.51}$ C 8.96
281+929						41.43	$\frac{13.84}{5.36}$ C 8.48
281+388						41.35	$\frac{13.92}{5.86}$ C 8.06
280+999						41.27	$\frac{14.00}{6.97}$ C 7.03
BM # 45	0.89	55.27				54.38	
18629-7							

+60				42.59	$\frac{12.08}{4.60}$ C 7.44	291+20			43.51	$\frac{16.31}{6.90}$ C 9.37
287+20				42.51	$\frac{12.16}{4.57}$ C 7.59	+80			43.23	$\frac{16.39}{6.25}$ C 10.14
780				42.43	$\frac{12.24}{4.57}$ C 7.67	+10			43.15	$\frac{16.47}{6.27}$ C 10.20
740				42.35	$\frac{12.32}{3.66}$ C 8.66	289+96 290+10 10' road.			43.06	$\frac{16.56}{5.99}$ C 10.62
286+0				42.27	$\frac{12.40}{2.69}$ C 9.72	+60			42.99	$\frac{16.63}{6.37}$ C 10.30
285+60				42.19	$\frac{12.48}{1.13}$ C 11.35	289+20			42.91	$\frac{16.71}{5.98}$ C 10.73
285+20				42.11	$\frac{12.56}{1.25}$ C 11.31	T.P. } 7.97 +80 TR	59.62	3.02	51.65	$\frac{11.84}{3.02}$ C 8.82
284+80				42.03	$\frac{12.64}{1.25}$ C 11.39	+40			42.75	$\frac{11.92}{4.11}$ C 7.71
10' off T.P. A#12	4.00	54.67	4.60	50.67						
staked to here 1-20-28										
284+50.01	$\Delta 19^{\circ} 52' 30''$	RT MH #52		41.97	$\frac{13.30}{4.60}$ C 8.70	288+0			42.67	$\frac{12.00}{4.38}$ C 7.62
							54.67			

$\frac{2 \times 1 \text{ stake}}{T.P. 1061}$	} 7.08	<u>55.80</u>	4.90	48.72	T.P. 11741		
R1.09 M.H.				9.64			
294+55.00				43.98	7.90	298+20	44.71
$\Delta 58^\circ 57' \text{ Alt. - MH}^* 54$					C 4.74		$\frac{11.09}{5.58}$ C 5.51
					T= -354		
294+15.67				43.90	9.72	+80	44.63
					7.86		$\frac{11.17}{4.86}$ C 6.31
					C 4.76		
293+76.34				43.82	9.80	+40	44.55
					4.62		$\frac{11.25}{4.60}$ C 6.65
					C 5.16		
293+57.01				43.75	9.87		44.47
					4.46	297+0	$\frac{11.33}{4.09}$ C 6.84
					C 5.41		
T.P. 2	2.00	<u>53.62</u>	8.00	51.62	15.95		
292+97.68				43.67	8.00	+60	44.39
					C 11.95		$\frac{11.41}{5.42}$ C 5.99
5.39.03							
292+58.85				43.59	16.03	296+20	44.31
$\Delta 11^\circ 07' \text{ Alt. - MH}^* 53$					1.17		$\frac{11.47}{5.93}$ C 5.56
					C 14.86		
					T= +3.75		
+40				43.53	16.07	+80	44.23
					5.23		$\frac{11.57}{6.59}$ C 4.98
					C 10.99		
292+0				43.47	16.15	+40	44.15
					2.31		$\frac{11.65}{7.81}$ C 3.84
					C 9.44		
291+60				43.39	16.23	295+0	44.07
					7.81		$\frac{11.73}{8.17}$ C 3.56
					C 8.40		
		<u>59.62</u>					
						53.80	

+80 47.79 $\frac{10.46}{4.20}$
C 6.26

31410

49.21 $\frac{13.72}{5.36}$
C 8.36

+40 47.63 $\frac{10.66}{4.42}$
C 6.20

+60

49.05 $\frac{13.88}{5.95}$
C 7.73

308+0 47.47 $\frac{10.73}{4.14}$
C 6.64

313120

48.89 $\frac{14.04}{5.44}$
C 7.60

+60 47.31 $\frac{10.94}{3.20}$
C 7.54

+80

48.73 $\frac{14.20}{5.75}$
C 8.25

307+20 47.15 $\frac{11.10}{2.01}$
C 9.09

+40

48.57 $\frac{14.36}{5.10}$
C 8.76

T.R. 1.04 58.25 5.65 57.21

20.11

2.81 66.43

+80 46.99 $\frac{15.87}{5.65}$
C 10.22

M.H. T.R.

0.86 62.93 7.17 62.07

+40 46.83 $\frac{16.07}{5.20}$
C 10.57

312+00
21073599

$\Delta 8^{\circ} 45' 30''$ T.M.H. 57
T + 0.77 1003

48.41 $\frac{20.83}{7.17}$
C 13.66

306+0 46.67 $\frac{16.19}{7.32}$
C 8.87

T.R. 2
310+0

14.63 69.24 0.64 57.61

48.27 $\frac{9.98}{0.64}$
C 9.34

305+60 46.51 $\frac{16.35}{8.04}$
C 8.31

+60

48.11 $\frac{10.14}{1.42}$
C 8.72

309+20

47.95 $\frac{10.30}{3.36}$
C 6.94

+60				50.65	$\frac{10.97}{5.97}$ C 5.02	+80				53.45	$\frac{10.97}{4.68}$ C 6.29
317+20				50.49	$\frac{11.15}{4.88}$ C 6.27	+40				53.09	$\frac{11.33}{4.81}$ C 6.52
+80				50.33	$\frac{11.21}{5.57}$ C 8.74	320+0				52.73	$\frac{11.69}{4.80}$ C 6.89
+40				50.17	$\frac{11.47}{1.92}$ C 9.55	+60				52.27	$\frac{12.05}{4.24}$ C 7.81
316+0				50.01	$\frac{11.67}{0.13}$ C 14.44	319+20				52.01	$\frac{12.41}{4.74}$ C 7.67
T.P.	3.43	61.6A	4.72	58.21							
+66				49.85	$\frac{13.09}{3.17}$ C 9.84	+80				51.65	$\frac{12.77}{2.97}$ C 9.80
315+20				49.69	$\frac{13.24}{2.26}$ C 10.38	+40				51.29	$\frac{13.13}{5.15}$ C 7.78
+80				49.53	$\frac{13.40}{5.26}$ C 11.18	318+0				50.93	$\frac{13.49}{7.81}$ C 5.68
314+40				49.37	$\frac{13.56}{3.51}$ C 10.65	T.P.	8.27	64.42	5.49	56.15	$\frac{10.92}{5.49}$ C 5.43
		62.93				317+9687	A 37° 22' R	MH # 58		50.72	
							T = -3.38				
								61.6A			

000

324+15.31 $\Delta 21^{\circ} 31' 19''$ MH" 59 Check. 10.25
4.41+
c 6.84 56.47
 BM 11.11 71.51 10.40
 324+10 56.33
 +60 55.97
 323+20 55.61
 +80 55.25
 +10 54.89
 322+0 54.53
 T.P. 2 6.91 67.72 3.61 60.81
 +60 54.17
 321+20 53.81

15.04
 8.24
 c 6.80
 47998
 Sph. 7.07
 20.54
 1629.5
 11.39
 3.95
 c 7.43
 11.75
 4.15
 c 7.60
 12.11
 4.25
 c 7.85
 12.47
 4.67
 c 7.80
 12.83
 5.08
 c 7.75
 13.19
 5.72
 c 7.47
 10.25
 3.61
 c 6.64
 10.61
 4.35
 c 6.27

+60
 +80
 +10
 +60
 +80
 +60
 +80
 325+20
 +80
 324+0
 71.51

507.19-48
 5.4502
 7.1102
 5.0014
 65

13.66
 3.87
 c 9.79
 13.82
 4.20
 c 9.62
 13.98
 4.70
 c 9.28
 14.14
 5.15
 c 8.99
 14.30
 5.53
 c 8.77
 14.42
 5.98
 c 8.45
 14.62
 6.54
 8.68
 14.78
 7.14
 c 7.64
 14.94
 7.86
 c 7.14

57.85
 57.69
 57.53
 57.27
 57.21
 57.05
 56.89
 56.73
 56.57

6A.42

		Reset		Rt.									
331+0	staked	17. RT. 13.53 13.53 6.59 5.31 C 6.94 C 8.22	59.17	12.84 3.11 C 8.23									66
					+60								11.49 3.90 C 7.59
out. stake M.H. 60	1.95	72.70	67.75	21. stake 12.50 2.15 C 8.55									60.61
+60			59.01										11.65 3.77 C 7.88
					334+20								60.45
330+20			58.85	12.66 3.28 C 8.88	T.P. ↓	3.88	72.10	4.48	68.22				12.41 4.25 C 7.93
					+80								60.29
329+90 ↘ 329+80 ↗	Δ 2° 18' RT T = -0.20	M.H. # 60	58.73	12.79 3.52 C 9.52									12.57 4.52 C 8.05
+50			58.61	12.90 3.67 C 9.23			10' RT.						60.13
					333+0		10' LT. & RT.						12.73 12.73 5.42 4.96 C 7.31 C 7.77
			58.49	13.01 3.84 C 9.44									59.97
329+20					+60								12.89 5.54 C 7.35
+80			58.33	13.18 3.67 C 9.51									59.81
					332+20								13.05 5.61 C 7.44
+40			58.17	13.34 3.75 C 9.52									59.65
					+80								13.21 5.62 C 7.54
328+0			58.01	13.60 3.97 C 9.71									59.49
					331+40		10' left.						13.37 5.89 C 7.48
		71.51			out. stake M.H. 60		72.70						59.33

338+0
 $\frac{80.29}{183.0}$
 $\frac{59.4}{59.4}$
 C 12.36

+60
 $\frac{80.29}{61.32}$
 $\frac{18.96}{6.43}$
 C 12.04

337+20
 T.P. 7.14 79.37 2.25 72.23

+80
 $\frac{17.70}{6.12}$
 C 11.58

+40
 $\frac{12.98}{2.35}$
 C 10.73

336+0
 (15/108)
 $\frac{13.31}{6.26}$
 C 7.05

335+60
 $\Delta 20-18'47''$
 P.P. MH #61
 From page 80 (B) 74.48

+30
 $\frac{13.47}{6.21}$
 C 7.06

335+0
 $\frac{11.21}{3.90}$
 C 7.41

61.99
 $\frac{17.98}{5.00}$
 C 12.34

61.83
 $\frac{17.54}{5.50}$
 C 12.04

61.67
 $\frac{17.70}{6.12}$
 C 11.58

61.50
 $\frac{12.98}{2.35}$
 C 10.73

61.34
 $\frac{13.14}{4.12}$
 C 8.97

61.17
 $\frac{13.31}{6.26}$
 C 7.05

61.01
 $\frac{13.47}{6.21}$
 C 7.06

60.89
 $\frac{11.21}{3.90}$
 C 7.41

60.77
 $\frac{11.37}{3.77}$
 C 7.56

341+32.00
 $\Delta 40-37' RT$
 $\Delta 39-25' 30'' RT MH \# 62$
 $500:10.67 T=3.58 T=3.73$

341+20

+80

+40

340+0

+60

T.P. pole
 W. 1/2 Saad
 4.50 80.29 3.58

339+20
 $\frac{17.80}{5.12}$
 C 12.47

338+40
 $\frac{17.97}{5.12}$
 C 12.47

63.49
 $\frac{16.93}{4.36}$
 C 12.57

63.31
 $\frac{16.98}{4.51}$
 C 12.47

63.14
 $\frac{17.15}{5.05}$
 C 12.10

62.98
 $\frac{17.31}{5.18}$
 C 12.13

62.81
 $\frac{17.48}{5.97}$
 C 11.97

62.65
 $\frac{17.64}{4.37}$
 C 12.27

75.79
 T.P. #1
 $\frac{16.58}{4.38}$
 C 12.50

62.32
 $\frac{17.05}{4.21}$
 C 12.84

62.16
 $\frac{17.21}{4.32}$
 C 12.87

79.37

+58	Pier #4	EL Base →	77.22 60.00 17.22 10.17 7.05	65.75	11.47 10.17 C 1.30	+40	66.29	14.71 5.83 C 8.88	
T.P.	7.23	77.22	0.97	69.99					
T.P.	11.15	70.96	6.34	59.81					
+42	Pier #3	EL Top of Base	56.00 10.15 5.85 C 9.58	65.59	0.56 6.13 F 5.57	26+0	66.25	14.75 6.18 C 8.57	
+18	Pier #2	EL Top of Base	56.00 10.15 11.15	65.35	0.80 11.41 F 10.61	+60	66.21	14.79 7.12 C 7.56	
T.P.	6.34	66.15	11.15	59.81					
Piers tied out 10' Each way along E of pier.									
343+02	Pier #1	EL Base	70.96 51.00 9.96 0.92 C 9.0	65.19	5.97 0.92 C 4.80	115+20	66.17	14.93 6.99 C 7.84	
T.P.	2.02	70.96	7.85	68.94					
+68				64.85	13.94 7.85 C 4.09	+80	66.13	14.77 7.72 C 7.15	
+34				64.51	14.25 10.23 C 4.05	+40	66.09	14.91 8.47 C 6.44	
343+0				64.17	14.62 7.55 C 7.07	26+40	66.05	14.75 8.72 C 6.23	
					5.56	81.00	-	75.44	
							180	75.42	
341+66				68.83	14.96 3.79 C 11.18	243+86.13 343+76.77	△ 45° 51' 20" Lt MH #63 T = 4.23	66.04 65.94	
T.P. #1	3.00	78.29		75.79				75.44 75.42 75.44 11.28 3.40 C 5.88	
Back of Head 11.18 Face 5.00 C 5.78									
Page 67 Rt.									
72.41									

349+20

66.57

17.98
6.06
C11.92

+80

66.93

20.89
8.02
C12.87

6.45 84.55 2.90 78.10

348+96.86 Δ 3°16'30" Lt MH "69
T = +0.89

66.55

14.45
2.90
C11.55

+10

66.89

20.93
7.32
C13.61

T.P. 7.23 87.82 3.96 80.59

352+0

66.85

17.70
3.96
C13.74

+80

66.53

14.47
3.12
C11.28

+60

66.81

17.74
8.42
C7.32

+40

66.49

14.51
3.03
C11.99

351+20

66.77

17.78
9.28
C8.50

348+0

66.45

14.54
3.22
C11.79

+80

66.73

17.82
9.15
C8.67

+60

66.41

14.57
3.01
C11.79

+40

66.69

17.86
5.43
C12.43

347+20

66.37

14.63
4.22
C9.84

350+0

66.65

17.90
6.84
C11.06

346+80

66.33

14.67
5.05
C9.62

349+60

66.61

17.94
5.51
C12.43

81.00

T

84.55

Restake
A-15-48

10' Lt.
24.24
4.20
C19.84

10' Rt.

10' Lt

10' Rt.

+40

24.69
4.96
C19.73

67.29

T.A 10' Rt
of 2
+60

2.87

82.70

11.70
23.92
13.05
C10.87

79.83

67.61

23.92
11.70
C12.22

356+0

24.73
4.80
C19.93

24.28
4.23
C19.05

67.25

86.40
5.78
91.98

24.77
4.94
C19.83

24.32
4.66
C19.66

67.21

24.32
5.12
C19.20

359+20

23.96
12.93
C11.03

67.57

23.96
11.49
C12.52

+60

355+20

24.81
5.14
C19.67

24.36
5.20
C19.16

67.17

24.36
5.10
C19.26

+80

24.00
11.72
C12.28

67.53

24.00
11.17
C12.83

+80

24.85
5.79
19.06

67.13

24.40
4.73
C19.67

+40

67.49

24.04
10.47
C13.57

+40

24.97

24.89
6.24
C18.64

67.09

24.44
5.70
C18.74

358+0

67.45

24.08
9.09
C14.99

T.P. 20.10 R.P.
1x1 Hub. dia

5.33

91.53

1.62

86.20

+60

24.12
9.59
C14.53

67.41

24.12
7.29
C16.83

354+0

A 13° 11' 30" Lt. 17 11 45
T = 41.18 500' 10.57
Δ 13° 27' 30" Lt.

67.05

20.97
2.10
C18.87

Restake
A-15-48
91.98

357+20

24.61
6.57
C18.04

24.16
7.52
C16.64

67.37

+60

67.01

20.81
3.00
C17.81

352+20

87.82

66.97

20.85
4.60
C16.25

356+80

24.65
5.93
C19.22

24.20
6.12
C18.08

67.33

91.53

+87.14

67.95

12.93
1.37
C 11.54

T.P.]

1.44

80.88

3.26

77.44

14.79
3.26

+78.52

68.36

12.52
7.89
C 4.63

+51.43

67.91

C 17.53

+40.92

68.28

12.60
7.06
C 5.54

363 + 15.91

67.88

14.72
5.06
C 9.76

0.02

8.35.71

362 + 80.00

$\Delta = 45^\circ - 15' - 10''$ RT

361.788.60

$\Delta 45^\circ - 50' - 9''$ MH #66

10.44 + 10.94 M.

$T = -4.23$

67.84

14.86
5.29
C 8.56

366 + 0.33

68.20

12.68
6.30
C 6.38

5.391

365 + 65.72 $\Delta 52^\circ - 38'$ MH #67
 $T = +2.93$

68.13

12.75
5.23
C 7.52

+60

67.81

14.89
5.14
C 7.63

365 + 30

68.09

12.79
5.75
C 6.84

361 + 20

67.77

14.83
4.30
C 10.63

+94.29

68.06

12.82
5.11
C 7.71

+80

67.73

14.77
4.43
C 10.49

0.01

+40

15.01
5.87
C 7.54

67.69

15.01
3.25
C 11.06

+58.57

68.02

12.86
2.96
C 9.70

360 + 0

15.05
3.93
C 11.12

67.65

15.05
3.46
C 11.59

360 + 22.86

67.99

12.87
7.63
C 11.26

81.70

80.88

6' Rt.

+70

6893

10' Rt.
7.51
6.00
C 1.45

T.P.

10.14

83.41

3.20

73.27

369+30

6885

7.59
5.03
C 2.56

2+0

72.12

4.35
3.20
C 1.15

+90

6877

7.67
6.33
C 1.34

+60
take off
B.M. 3.19

3.19

76.47

check to B.M. □
culvert

3.19

71.59

73.28

4.88
3.44
C 1.44

+50

6869

7.75
8.06
F 0.71

+20

Sec. 10.43

A 82° 07' 30" Lt MH # 69
T = +297 - (1.757 * 69)

71.05

5.39
4.15
C 1.24

368+10.30 - Pier #4

C 9.80 to
Base

7.83
2.04
C 5.79

68.61

+90

70.57

5.87
2.30
C 3.51

T.P.

6.59

76.44

3.98

69.85

E 3.47

+60

70.09

6.35
1.70
C 4.61

+94+30 - Pier #3

C 5.17 to
top of base

5.25
12.66
F 7.41

68.58

5.25
12.35
F 7.11

C 2.61 top of base

E 3.01 top of base

+30

69.61

6.33
3.47
C 3.36

+71.00 - Pier #2

5.30
13.22
F 7.92

68.53

5.30
12.82
F 7.52

T.P. 3.14

73.83
(Long side)
S. Mt.

10.19

70.67

(7.25)

04 00

370+50

A 72° 30' Rt MH # 68
T = -7.17

69.13

69.10

6' off
hand
Back
7.31 7.34
4.81 4.50
C 2.50 C 2.80

367+53.90 - Pier #1

C 5.69 to base

68.50

11.38
10.19
C 2.19

370+44

See page 79

370+10

69.01

7.43
5.30
C 2.13

367+16.12

68.43

12.45
9.13
C 3.32

80.88

76.44

												73
+60				7695								
Check. 20 th Lt M.H. #70												
1843 Page 5												
			4.88	84.80								
T.P. 2	10.87	89.68	4.60	78.81								
5720				7641								
+80				75.87								
+40				75.24								
410				74.80								
+60				74.27								
3+20				73.73								
+80				72.19								
2+40				72.66								

83.41

89.68

Check. 20th Lt M.H. #70
1843 Page 5

G'RT.
12.73
9.51
C 3.22
84.80

T.P.

6.88

75.34

1.22

88.46

G'RT.

4.78
1.69
C 6.07

8.49
2.54
C 5.95

9.19
3.45
C 5.74

9.89
4.02
C 5.87

10.60
4.92
C 5.68

11.30
5.48
C 5.82

11.68
6.47
C 5.21

12.20
9.50
C 4.70

6+38.54 Δ 9'32" Rt. M.H. #70
Sec. 10.03 T - 0.83

12+0 8788 $\frac{11.41}{5.04}$
C 6.37

+60 8718 $\frac{12.11}{6.09}$
C 6.04

11+20 8647 $\frac{12.82}{6.55}$
C 5.97
T.R. 20' Lt. C.2A 99.29 2.29 93.05
M.H. #71

10+80 8577 $\frac{9.57}{3.64}$
C 5.73
POT MH #71

+50 8524 $\frac{10.10}{3.74}$
C 6.36

10+20 8471 $\frac{10.63}{4.54}$
C 6.09

+80 8401 $\frac{11.33}{5.35}$
C 5.98

+40 8331 $\frac{12.03}{6.13}$
C 5.90

9+0 8260 $\frac{12.74}{6.89}$
C 5.85

95.3A

check 20' Lt.) 5.65 101.83
15+26.79 Δ 1° 01' 30" R MH #71
Sec. = 19.00 T = 0.35 93.63

+80 92.81 $\frac{14.67}{7.39}$
C 7.28

+40 92.11 $\frac{15.37}{8.02}$
C 7.35

T.R. 9.27 107.48 1.08 98.21

+40 91.40 $\frac{7.89}{1.08}$
C 6.81

+60 90.70 $\frac{8.57}{2.04}$
C 6.55

13+20 8999 $\frac{9.30}{3.53}$
C 5.77

+80 8929 $\frac{10.00}{3.83}$
C 6.17

12+40 8859 $\frac{10.70}{4.60}$
C 6.10

99.29

101.83

$\frac{13.85}{6.27}$
C 7.58

$\frac{14.67}{7.39}$
C 7.28

$\frac{15.37}{8.02}$
C 7.35

$\frac{7.89}{1.08}$
C 6.81

$\frac{8.57}{2.04}$
C 6.55

$\frac{9.30}{3.53}$
C 5.77

$\frac{10.00}{3.83}$
C 6.17

$\frac{10.70}{4.60}$
C 6.10

+80	100.34	7.14 0.59 C 6.56
+40	99.58	7.90 7.07 C 6.83
18+0	98.82	8.56 2.04 C 6.62
+60	98.06	9.42 2.50 C 6.92
17+20	97.20	10.18 3.12 C 7.06
+80	96.54	10.94 3.92 C 6.98
+40	95.78	11.70 4.32 C 7.38
16+0	95.02	12.46 5.42 C 7.04
15+60	94.26	13.22 5.13 C 8.09

107.48

+60	106.44	10.25 4.75 C 5.50		
21+20	105.56	11.13 5.51 C 5.62		
+80	104.68	12.01 6.86 C 5.75		
+40	103.80	13.79 7.37 6.42		
20+0	102.91	13.77 8.24 C 5.53		
+60	102.04	14.65 9.12 C 5.53		
19+20	101.16	15.53 9.21 C 6.32		
21+2 T.P.	9.45	116.69	0.24	107.24
18+98.48	Δ 11° 32' 18" MH # 73			100.69
	Sec. = 10.05	T-101		6.79 8.26 C 6.55

107.48

25+20				6' RT 113.76	10.04 4.07 C 5.97	Chisel D on Head wall	FB 1703 68	4.54	129.05	129.99
+80				113.08	10.92 5.21 C 5.51	28+41.91 2873902 sec. = 11.09	A 51' 15" 30 1/4 MH #25 T + 4.80		119.18	14.41 4.73 C 9.68
+40				112.40	11.40 6.27 C 5.13	28+0			118.52	15.07 5.97 C 9.10
Check 20' Lt. M.H. 74 = 115.35 Page 19 - FB 1843				5.16 118.34		+60			117.84	15.75 7.08 C 8.67
24+0 Sec. = 10.00				111.92	12.08 6.88 C 5.28					
+60				110.84	12.96 7.57 C 5.39	27+20			117.16	16.43 8.76 C 7.67
T.P. ↓	7.86	123.80	0.75	115.94	6.73 0.75 C 5.98	+80			116.48	17.11 9.93 C 7.18
23+20				109.96		T.P. ↓	114.84	133.59	2.05	121.75
+80				109.08	7.61 1.69 C 5.92	+40			115.80	8.00 2.05 C 5.95
+40				108.20	8.49 3.27 C 5.22	26+0			115.12	8.68 2.45 C 6.23
22+0				107.32	9.37 4.24 C 5.13	25+60			114.41	9.20 2.78 C 6.42
		116.69								

31+45

124.25
10.44
6.33
C 4.11

31+0

123.50
11.19
6.21
C 4.28

+60

122.83
11.86
6.65
C 5.21

30+20

122.16
12.53
5.87
C 6.66

+80

121.49
13.20
3.82
C 9.38

+10

120.82
10/10
13.87
3.25
C 10.57

29+0

120.15
14.54
3.87
C 10.67

+80

119.81
14.88
2.50
C 10.38

28+60
Chisel B. Hd. wall
1903-68

5.70 134.69

119.48
15.21
3.70
C 10.51

128.99

G. At.

35+0

T.P. →

12.45 154.23 0.51

137.09
19.14
10.91
C 6.73

+10

141.78
135.53
6.76
0.51
C 6.25

34+20

133.97
8.32
1.89
C 6.43

+80

132.41
9.88
3.15
C 6.73

+40

130.85
11.44
4.11
C 7.33

33+0

129.29
10/20
13.00
6.21
C 6.79

+10

127.93
14.56
9.00
C 5.56

32+20

126.17
16.12
11.60
C 4.52

T.P. CH 12.60 14.229 5.00
10' x 40' LA
1190 PAT MH + 76

129.69
125.00
9.69
5.00
C 4.69

134.69

Grade changed
29+11 to 35+44.56
See G. 238
6

Charged to here to

20 1/2 38 RT
38+36.80
Sec: 10.05

Δ 11° 42' RA MH 478
T: 0.99

141.09

14.37
10.26
0.41

12+0

153.90

78
11.73
6.70
C 5.03

T.P.

9.80

158.46

5.57

148.66

T.P.

8.00

165.63

0.83

157.63

38+0

10.80
5.57
C 5.23

+60

152.82

5.64
0.83
C 4.81

+60

142.71

11.52
5.85
C 6.07

11+20

151.74

6.72
2.42
C 4.30

27+20

141.99

12.24
5.62
C 6.62

+80

150.66

7.80
3.33
C 4.47

+80

141.27

12.96
6.61
C 6.35

+40

149.58

8.58
4.32
C 4.26

+40

140.55

13.68
7.13
C 6.23

10+0

148.50

9.96
4.22
C 5.24

36+0

139.83

14.40
7.42
C 7.00

+60

147.42

11.04
5.77
C 5.27

+60

139.11

15.12
7.56
C 7.86

19+20

146.34

12.12
7.35
C 4.77

Check M.R.R. F 1823-29

Pr. M.H. 77

20.1 + 40.2 LK

354 11.56

Sec: 10.05

Δ 11° 42' RA M.H. 477

T: 0.99

5.96

148.33

145.34

138.83

15.40
7.22
C 7.68

38+20

145.26

13.10
8.25
C 4.45

158146

O.K. From Memo of 154.23

Chisel 38 } 7.45 136.44 128.99
 1703 }
 68 }

Continued in G. 238 - Page 1

Check 20' Rt. M.H. #79 FB 1843-P 37 1.40 164.23 (164.23)

20'+20' Rt. 44+0 Δ 4° 04' 11" M.H. 79 T = 0.35 159.30 C 4.77
 sec = 10.01

0+07 on Alvarado 2.15 69.24 = El. end of stub
 Canyon line.

in headwall Below 5.11 78.39 73.28

460 158.22 C 4.52
 7.41
 2.89

49° 12' Lt. = 18" stub M.H. Grade 69.10 7.20
 to State College line 4.88
 C 2.32

13+20 157.14 C 4.41
 8.49
 4.09

0.27

+80 156.06 C 4.37
 9.57
 5.20

370+44 = 15" wye to Fairmount line 69.13 7.17
 4.67
 C 2.50

42+40 154.98 C 4.49
 10.65
 6.16

in edward Headwall 3.02 76.30 73.28
 6.72

165.63

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00'	0.1	21°-00'	12.8	33°-00'	29.7
3°-00'	0.3	21°-30'	13.4	33°-15'	30.1
4°-00'	0.5	22°-00'	14.0	33°-30'	30.5
5°-00'	0.8	22°-30'	14.7	33°-45'	30.9
6°-00'	1.1	23°-00'	15.3	34°-00'	31.3
7°-00'	1.5	23°-30'	15.9	34°-15'	31.7
8°-00'	1.9	24°-00'	16.5	34°-30'	32.1
9°-00'	2.5	24°-30'	17.2	34°-45'	32.5
10°-00'	3.0	25°-00'	17.9	35°-00'	32.9
10°-30'	3.3	25°-30'	18.6	35°-15'	33.3
11°-00'	3.6	26°-00'	19.2	35°-30'	33.7
11°-30'	4.0	26°-30'	19.9	35°-45'	34.1
12°-00'	4.3	27°-00'	20.6	36°-00'	34.6
12°-30'	4.7	27°-30'	21.3	36°-15'	35.0
13°-00'	5.1	28°-00'	22.0	36°-30'	35.4
13°-30'	5.5	28°-30'	22.8	36°-45'	35.8
14°-00'	5.9	29°-00'	23.5	37°-00'	36.2
14°-30'	6.3	29°-30'	24.3	37°-15'	36.6
15°-00'	6.7	30°-00'	25.0	37°-30'	37.1
15°-30'	7.2	30°-15'	25.4	37°-45'	37.5
16°-00'	7.6	30°-30'	25.8	38°-00'	37.9
16°-30'	8.1	30°-45'	26.2	38°-15'	38.3
17°-00'	8.5	31°-00'	26.5	38°-30'	38.7
17°-30'	9.0	31°-15'	26.9	38°-45'	39.1
18°-00'	9.5	31°-30'	27.3	39°-00'	39.6
18°-30'	10.1	31°-45'	27.7	39°-15'	40.0
19°-00'	10.6	32°-00'	28.1	39°-30'	40.5
19°-30'	11.2	32°-15'	28.5		
20°-00'	11.7	32°-30'	28.9		
20°-30'	12.3	32°-45'	29.3		

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

T.P.	6.77	74.48	3.77	67.71	(B)
331400	8.23	Checked	4.07	59.19	(B) 67.41
160	8.35	These	4.11	59.01	67.37
330420	8.88	For	out.	58.85	67.362
M.H. #60			12.76	58.72	M.H. #60
M.H. #59	3.73	71.48		67.75	58.73
page 66		offset stake E.L.:			67.02
324115.31		actual			67.15
M.H. #59	M.H. Invert		11.43	56.55	
B.M. #231			7.48	60.50	(60.05)
P. 65					
T.P.	8.71	67.98	1.75	59.27	
1X1 cut stake					
1056 AX of N.H.S	S=317476.97		4.92	56.20	B.M. #3
T.P.	2.85	61.02	11.11	58.17	
22 = R1313+72L	(69.11 5R)		0.09	69.19	spike in
= Pole #4343034					take pole
T.P.	11.88	69.28	2.17	57.40	B.M. #1
T.P.	3.12	59.57	9.22	56.45	
28' R of 303+85					
Nail in porch 2/2			12.61	53.06	B.M. #1
T.P.	11.24	65.67	1.04	54.43	
T.P.	4.68	55.47	2.83	50.79	
X from page 61-left	61-left	53.62			

20.1571

17.7687

1.3884

37.22

18.41

92

15

967

9

60

41.91

18.17

27

02.9 ✓

941

~~28~~

915