

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.
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INDEXED

*Completely
except page 76 & 79*

MICROFILMED

APR 13 1965

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

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Volley Ball Courts Community Center
Laudis + 44th St.

INDEXED
WK
DEC 15 1948

1

BM 6.28 35979

35351
NXBP
Laudis
Highland
172643

LET
3

N.Y. Community Center 2

100

LET

Footline 117251

FdHos 28

Hilly

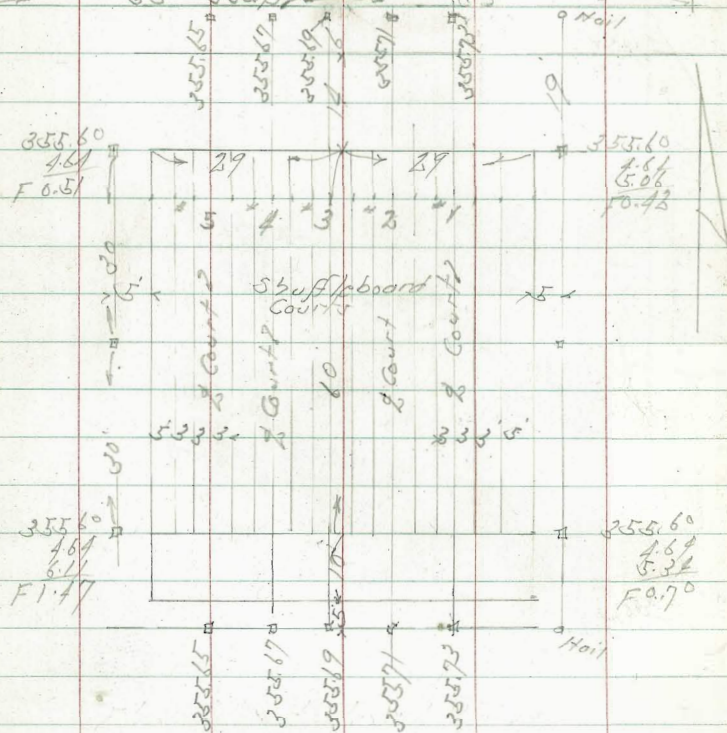
35350 4.48 4.76 5.04 5.32 5.60	35350 4.48 4.76 5.04 5.32 5.60
35350 4.48 4.76 5.04 5.32 5.60	35350 4.48 4.76 5.04 5.32 5.60
35350 4.48 4.76 5.04 5.32 5.60	35350 4.48 4.76 5.04 5.32 5.60

Grades
Laudis 0.10
Volley Ball
Courts
10
10
10
10

Grades Tennis Courts Land N + 4415 St.

Shuffboard
 B.M. Court 6.73 360.34 353.51
 Tennis
 B.M. Court 6.87 360.38 353.51

6.79 360.30 353.51
 Existing Tennis Court

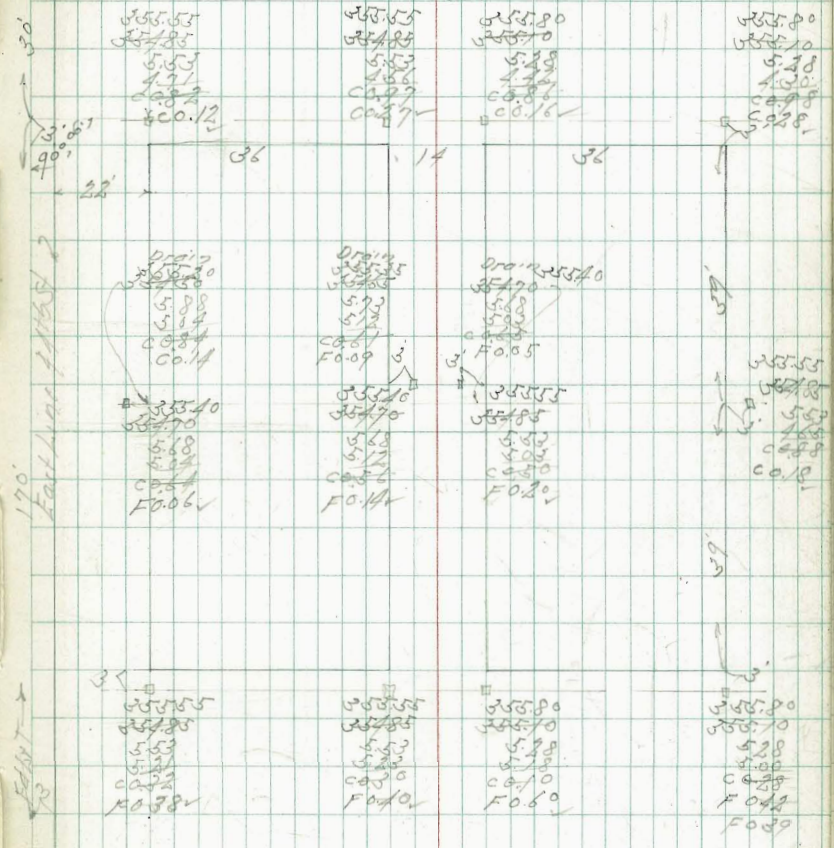


For Grades Page 44

Shuffboard
 Sept 7-48
 5.55.48
 Smith
 3rd Cr. Cross Sec. 1726-13
 1675-20
 Tennis Court Feb 27-48
 5.55.00
 Smith
 Johnson
 H.O. 50/50

2

INDEXED
 WK
 DEC 15 1948
 N.Y. Community Center?



Grades Tennis Courts + Volley Ball Courts
445 St North of Landis

Lat 3 N.Y. Community Center 2

10 355.40 55 355.70
5.10 1.80
5.24 1.36
FO.12 ca. 71

Tennis Courts

355.20
5.30
5.42
FO.17

355.55
1.95
5.29
FO.14

355.70
1.80
5.20
FO.10

Lat 3 BM 699 360.50

355.51 NW. 8P
Landis
Highland

March 1-18
5.55.00
5.55.10
5.55.20
5.55.30

3

355.40
5.10
5.19
FO.09
355.90
4.60
1.58
ca. 0.2

Volley
Ball
Courts

Out.
See Page 1

355.40
5.10
4.94
ca. 0.6

355.40
5.10
5.57
FO.17

355.55
1.95
4.71
ca. 0.19

355.40
5.10
5.10
ca.

355.40
5.10
5.50
FO.10

355.80
1.90
5.25
FO.35

0+25 12.30 11.80
 (2.23) 5.39
 11.80
 12.06
 12.30 12.80 (2.75 Cont)

0+07 11.12 11.57
 11.10 6.62
 11.35 10.85
 10.57 11.07
 7.17 6.67

Locust 10.52 10.87
 7.22 6.87
 11.17 11.02
 6.57 6.72
 11.27 11.27
 6.57 6.57

3+0 9.97 10.57
 7.77 7.12
 10.15
 10.57 10.77
 7.12 6.87
 10.92 10.92
 6.82 6.82
 11.00 11.00

2+75 10.30 9.80
 7.88 7.79
 10.39 10.06
 7.68 7.61
 10.30 10.80
 7.35 7.35

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0+50 6.84 6.95
 10.25 10.71
 7.21 7.45
 10.25 10.25

0+27 7.27 6.69
 10.99 10.52
 7.16 7.77
 10.52 10.52

0+09

Gutter
 BM 6.66
 11.02
 17.68
 6.23
 17.43
 10.07
 27.47 Major

Paving
 BM 6.66
 11.02
 17.74
 6.32
 17.43
 11.84
 29.26A

Rosecrans

Paving Grader Keok St.
 Rosecrans St. to W. 11th St.

4

0+25 26.00 25.50
 1.97 3.74
 26.00 26.50
 1.47 3.46

0+07 23.77 24.27
 5.49 4.99
 23.90 23.40
 4.09 23.77
 23.17 23.57
 6.09 5.82

Evergreen 22.67 22.67
 6.59 6.59
 22.92 22.77
 6.32 6.42

3+0 22.07 22.17
 7.19 7.09
 22.37 22.17
 6.89 7.09

2+0 21.80 21.37
 7.89 7.49
 21.77 21.57
 7.49 5.99

2+75 21.10 20.60
 6.87 8.21
 21.19 20.86
 8.40 8.21
 21.10 21.10 (21.90)

0+25 12.30 11.80 12.30 12.80

Paving Grades Keats St
 Rosecrans St. to Hilliers

Gutter BM	190	1628	4438	J.F. D Hilliers Road
--------------	-----	------	------	----------------------------

Paving	6.82	51.20	4738
--------	------	-------	------

Hilliers

270.7	14.20	13.50	4458	45.35
		2.68		

43.45	43.05	8.74	8.48	8.45	43.75	44.50
	3.32				2.50	

27.95	42.80	42.30	22.73	42.75	42.88	43.50	43.58
		3.98				3.42	

27.60	41.82	41.35	41.94	41.61	41.85	42.35
		4.15		9.59		4.42
			9.80		9.55	

0+25

Paving Grader Jarvin St.
Rosecrans St. to Willow St.

BM 2.06 14.50 12.44
TP 12.35 26.71 0.14 14.36

Paving
BM 6.79 10.08 3.29
TP 8.91 16.63 2.36 7.72

BM 5.88 10.75

BM 5.57 16.32 10.75

INDEXED
WK
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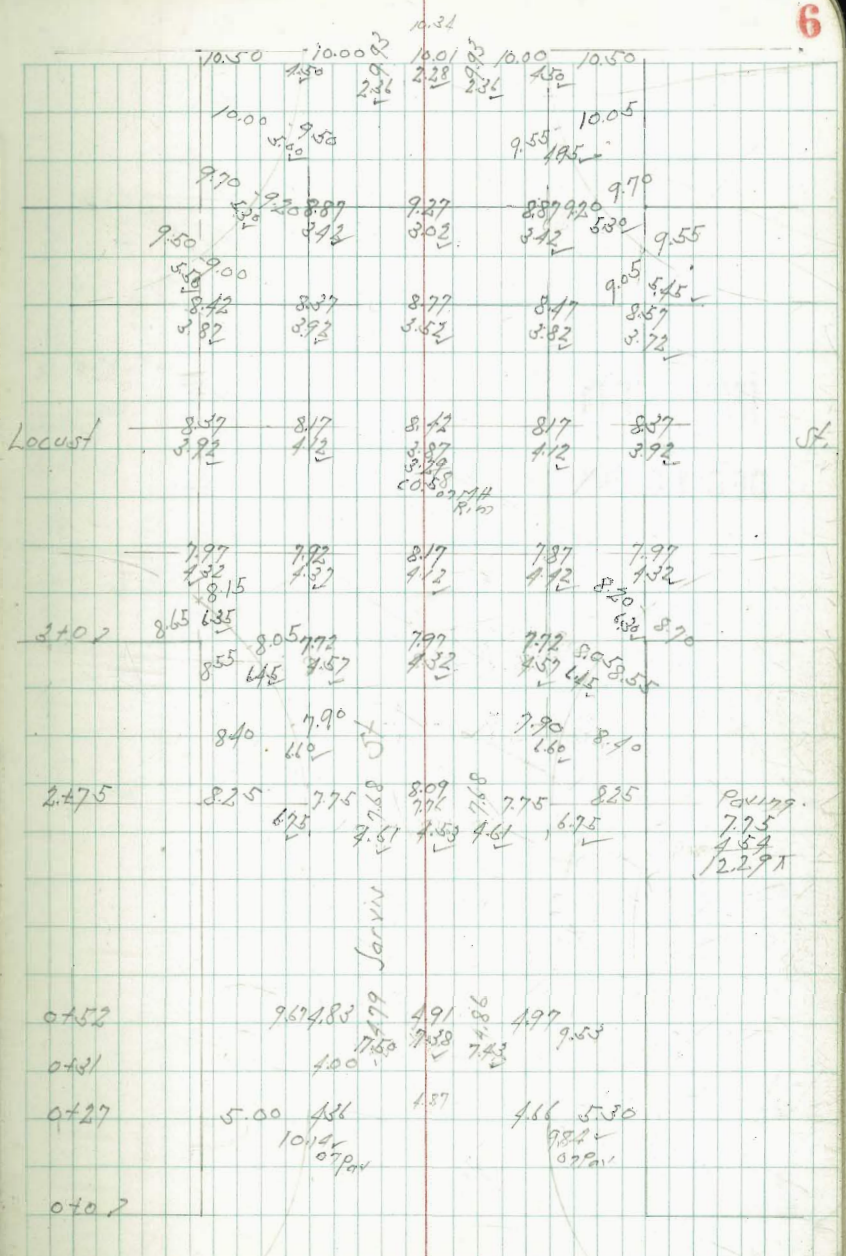
Paving Grades
May 5-18
Sisson
Smith
Riley
Salmonson

Layered
S.E. Top of Hill
Locust & Jarvin
228.70

S.W. 745' Dike
Rosecrans
+ 129/5W

S.E. Top of Hill
Locust & Jarvin

Used Gutter
Grades for
Paving



Rosecrans

Paving Grades Jarvis & Evergreen

Paving 29.55 LT Page 9

29.87 LT Page 9

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25.47
446 28.00

25.92
1849 487
25.00

24.68
24.51
5.05
24.18

Evergreen

24.58 2.10
24.58 2.10
24.58 2.10
5.82

23.89
2442 104
24.02

14.75

1790/600

7

0+25	21.40	23.98	23.99	23.66	23.40	23.90
0+30	20.90	23.40	23.60	23.40	23.90	26.71
0+35	20.40	23.90	23.90	23.60	23.90	23.90
0+40	20.00	23.90	23.90	23.60	23.90	23.90
0+45	19.50	23.90	23.90	23.60	23.90	23.90
0+50	19.00	23.90	23.90	23.60	23.90	23.90
0+55	18.50	23.90	23.90	23.60	23.90	23.90
0+60	18.00	23.90	23.90	23.60	23.90	23.90
0+65	17.50	23.90	23.90	23.60	23.90	23.90
0+70	17.00	23.90	23.90	23.60	23.90	23.90
0+75	16.50	23.90	23.90	23.60	23.90	23.90
0+80	16.00	23.90	23.90	23.60	23.90	23.90
0+85	15.50	23.90	23.90	23.60	23.90	23.90
0+90	15.00	23.90	23.90	23.60	23.90	23.90
0+95	14.50	23.90	23.90	23.60	23.90	23.90
1+00	14.00	23.90	23.90	23.60	23.90	23.90
1+05	13.50	23.90	23.90	23.60	23.90	23.90
1+10	13.00	23.90	23.90	23.60	23.90	23.90
1+15	12.50	23.90	23.90	23.60	23.90	23.90
1+20	12.00	23.90	23.90	23.60	23.90	23.90
1+25	11.50	23.90	23.90	23.60	23.90	23.90
1+30	11.00	23.90	23.90	23.60	23.90	23.90
1+35	10.50	23.90	23.90	23.60	23.90	23.90
1+40	10.00	23.90	23.90	23.60	23.90	23.90
1+45	9.50	23.90	23.90	23.60	23.90	23.90
1+50	9.00	23.90	23.90	23.60	23.90	23.90
1+55	8.50	23.90	23.90	23.60	23.90	23.90
1+60	8.00	23.90	23.90	23.60	23.90	23.90
1+65	7.50	23.90	23.90	23.60	23.90	23.90
1+70	7.00	23.90	23.90	23.60	23.90	23.90
1+75	6.50	23.90	23.90	23.60	23.90	23.90
1+80	6.00	23.90	23.90	23.60	23.90	23.90
1+85	5.50	23.90	23.90	23.60	23.90	23.90
1+90	5.00	23.90	23.90	23.60	23.90	23.90
1+95	4.50	23.90	23.90	23.60	23.90	23.90
2+00	4.00	23.90	23.90	23.60	23.90	23.90

Jarvis St

Paving
19.60
6.30
25.80

Jarvis St.

BM 0.18 3908 3890

Top of Hill

0.32 3922 3890

Willow

JF

3702 36.00 38.5 35.23 36.75 36.50

3570 35.60 34.90 35.25 35.85

2473 35.15 34.80 4.8 34.90 34.59 34.85 35.30

2450 34.10 33.60 3.8 34.04 34.71 34.80 34.30

3.8 3.5 4.3 4.3 4.3 4.3

5.0 5.1 5.55 5.28

Jarvis St

Paving Grades Evergreen

B/M 5.27 29.87 24.50

Paving 5.06 29.56 24.50

SE Section 417
Evergreen
1199000

1090 St.

2407 2540 24.89
198

2625 2735
315

2570 - 2520
467

2658 2708
337

1475

2590 2540 25.96
142 396

2629 2650 2700
366 331 332

1455

2589 out.

2689

140
Gutter Bit
on street

2505
427

2569 2630
387 335

2686 AS Cont.

0425

2520 2470 25.54
312 468

2521 2570 2620
435 418 417

2510 2460
507

2575 2625
412

0407

2482 2434
548

2585 2640
102

1090/00 St.

Alley Block 1 Chester Park 4 Add. Water Grader
 Polk Ave to Orange Ave 4644 West

Stakes Set
 on Property Lines
 2' x 2' South of lateral

M.O. 60138

For 15-18

S. 5889
 S. 5896
 7167
 5052507

10

	West		East
1451 Lt	553.22	⁴¹⁵ _{3.59} Co. 21	⁴¹⁵ _{3.63} Co. 21
1432 Rt			^S 4.39 ^N 4.25 Co. 16
1403 Lt	553.33	⁴⁰⁴ _{3.42} Co. 21	⁴⁰⁴ _{3.38} Co. 21
0498 Lt	553.50	^S 4.07 _{3.65} Co. 12	
0491 Rt	557.37	^S 0.83 _{1.73} Fo. 30	^N 4.45 4.51 Co. 11
+76	52.91		
0474 Lt	552.85		
+72	52.79	^S 0.85 _{1.57} Fo. 34	
0473 = Corner 1074	346.82	^S 1.66 _{1.25} Co. 22	^S 2.31 _{0.38} 96
0442 Rt			^N +44
0432	351.10	^S 2.14 _{2.82} Co. 52	^S 2.42 _{1.77} 96
0430 Lt	out 350.97		^N +40
+28	350.80	^S 2.91 _{2.22} Co. 72	
+03			^S 5.90 _{4.92} Co. 18
0401 Rt			
040 = 1/2 Polk Ave.			^S 6.26 _{6.37} on Pav.
TP	5.42	353.74	8.87
BN	3.25	357.19	353.94

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	West		East
3431 Lt	350.94	^S 6.43 _{6.77} Fo. 04	^N 6.43 _{6.61} Fo. 18
2412 Rt			^S 6.49 _{7.28} Fo. 99
340 Lt	351.01	^S 6.36 _{6.89} Co. 27	^N 6.36 _{6.20} Co. 07
2484 Rt			^S 6.34 _{6.35} Co. 06
2448 Lt	351.76	^S 5.11 _{5.06} Co. 87	^N 5.11 _{5.03} Co. 58
2432 Rt			^S 5.43 _{4.97} Co. 76
2402 Lt	352.78	^S 4.59 _{5.12} Co. 13	^N 4.59 _{3.66} Co. 13
1476 Rt			^S 4.53 _{3.81} Fo. 26

35737

Water Laterals Hilley Block 1 Chester Park Add

		At. W		Rt. E
TP	5.28	353.99	1.66	350.71
5+03	Rt.			350.49 ^{6.86} _{6.81} ^{6.88} _{6.83}
4+71	Lt.	350.66	^{6.76} _{6.96} ^{6.71} _{6.84}	^{6.85} _{6.73}
4+67	Rt.			350.57 ^{6.80} _{7.28} ^{6.80} _{6.90}
4+21	Lt.	350.76	^{6.61} _{6.82} ^{6.61} _{6.74}	^{6.74} _{6.73}
3+95	Lt.	350.81	^{6.56} _{6.79} ^{6.56} _{6.88}	^{6.88} _{6.80}
3+90	Rt.			350.72 ^{6.15} _{7.30} ^{6.15} _{7.55}
3+67	Rt.			350.77 ⁵ _{6.10} ^{7.17} _{7.72}
3+86	Lt.	350.89	⁵ _{6.48} ^{7.18} _{6.48}	^{7.18} _{6.67}
		357.37		

11

BM		2.08	353.91	^{11.4} _{11.8} ^{11.8} _{11.1}
5+42	Rt.		350.42	^{5.57} _{5.05} ^{5.57} _{4.82}
5+38	Lt.	350.64	^{5.93} _{5.14} ^{5.35} _{5.08}	^{5.35} _{5.20}
5+32	Lt.	350.58	^{5.21} _{5.14} ^{5.11} _{5.05}	^{5.11} _{5.06}
5+29	Lt.	350.56	^{5.18} _{5.18} ^{5.18} _{5.05}	^{5.18} _{5.07}
		355.99		

Culvert Grades Churchyard St &
Santa Margarita St.

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1+44 = 14 18" Culv.	165.00	16.58 14.54 c1.94
1+04	166.80	14.98 11.97 c2.81
0+64	168.60	12.98 10.23 c2.75
0+32	170.04	11.54 8.45 c3.09
0+0 = 14 Existing 18" Culv.	171.48	10.10 5.54 c4.56
TP	3.78	181.58
BM	0.80	190.25
		177.80
		189.45

April 6-48

S. 1100

Sm 26

Plan

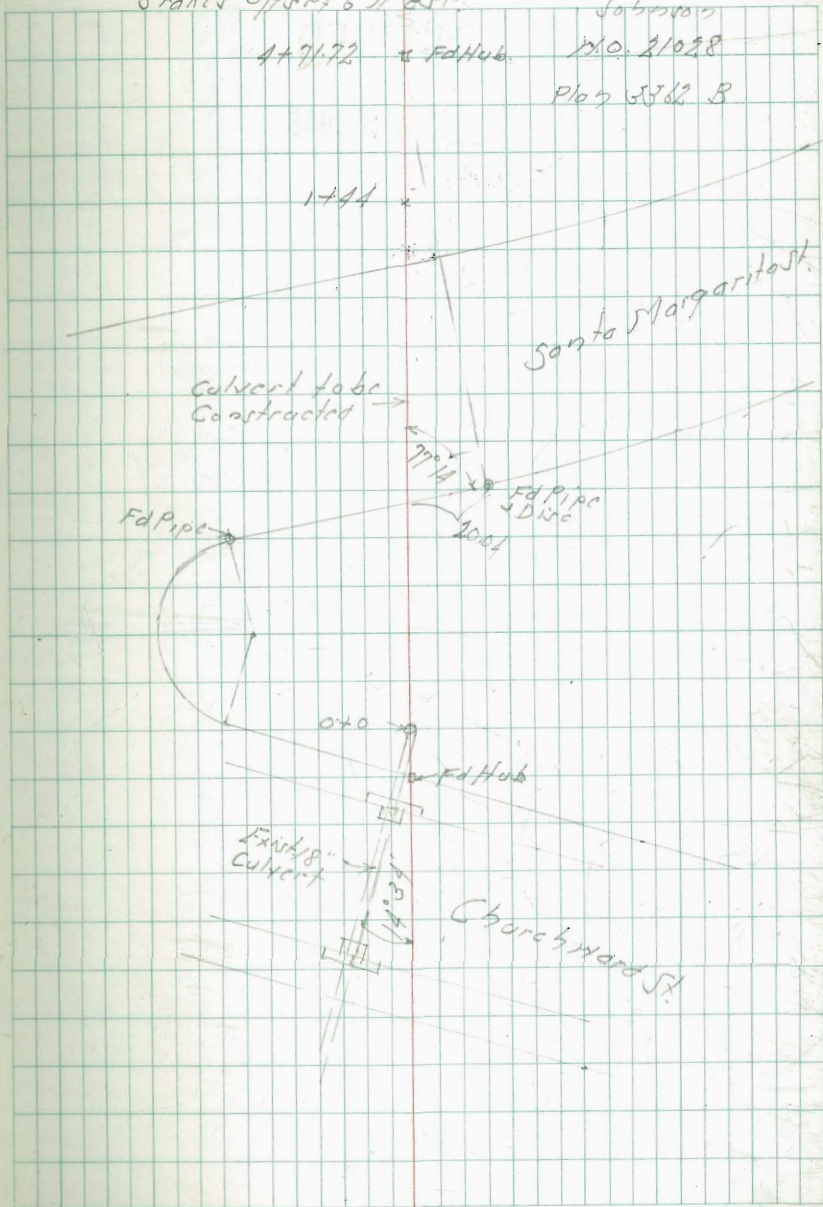
10.21028

Plan 3382 B

12

stakes offset 6' out

4+71.72 = Fd Hub

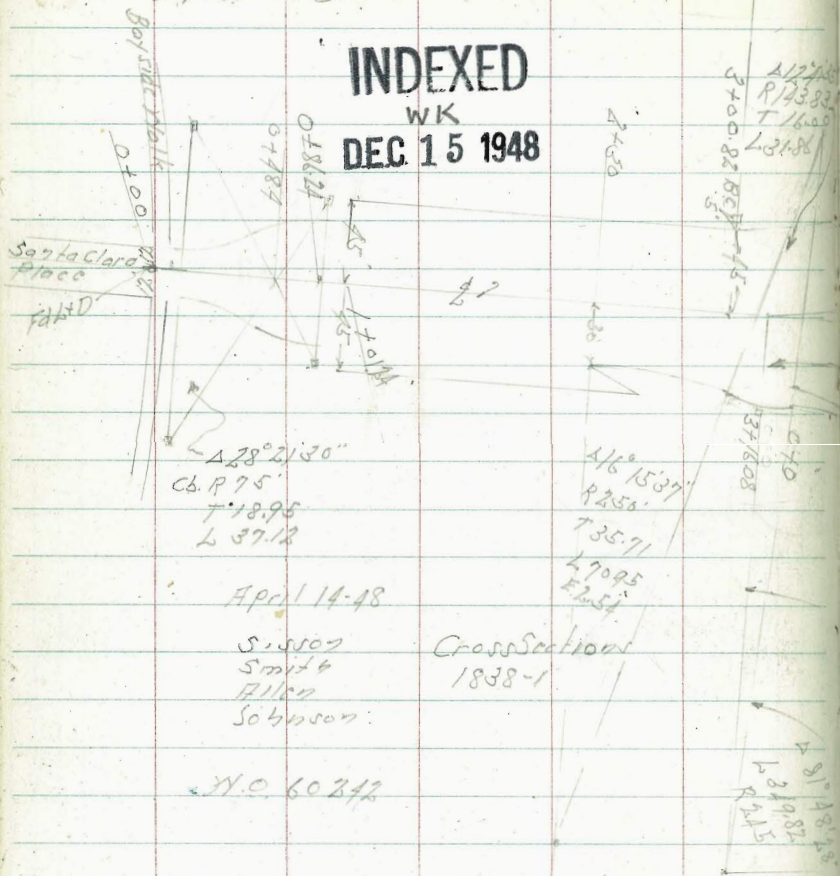


Paving Grades Santa Clara Point
Mission Beach

INDEXED

WK

DEC 15 1948



$\Delta 28^{\circ} 21' 30''$
Cb. R 75
T 18.95
L 37.12

April 14-48

S. Sisson
Smith
Ellen
Solomon

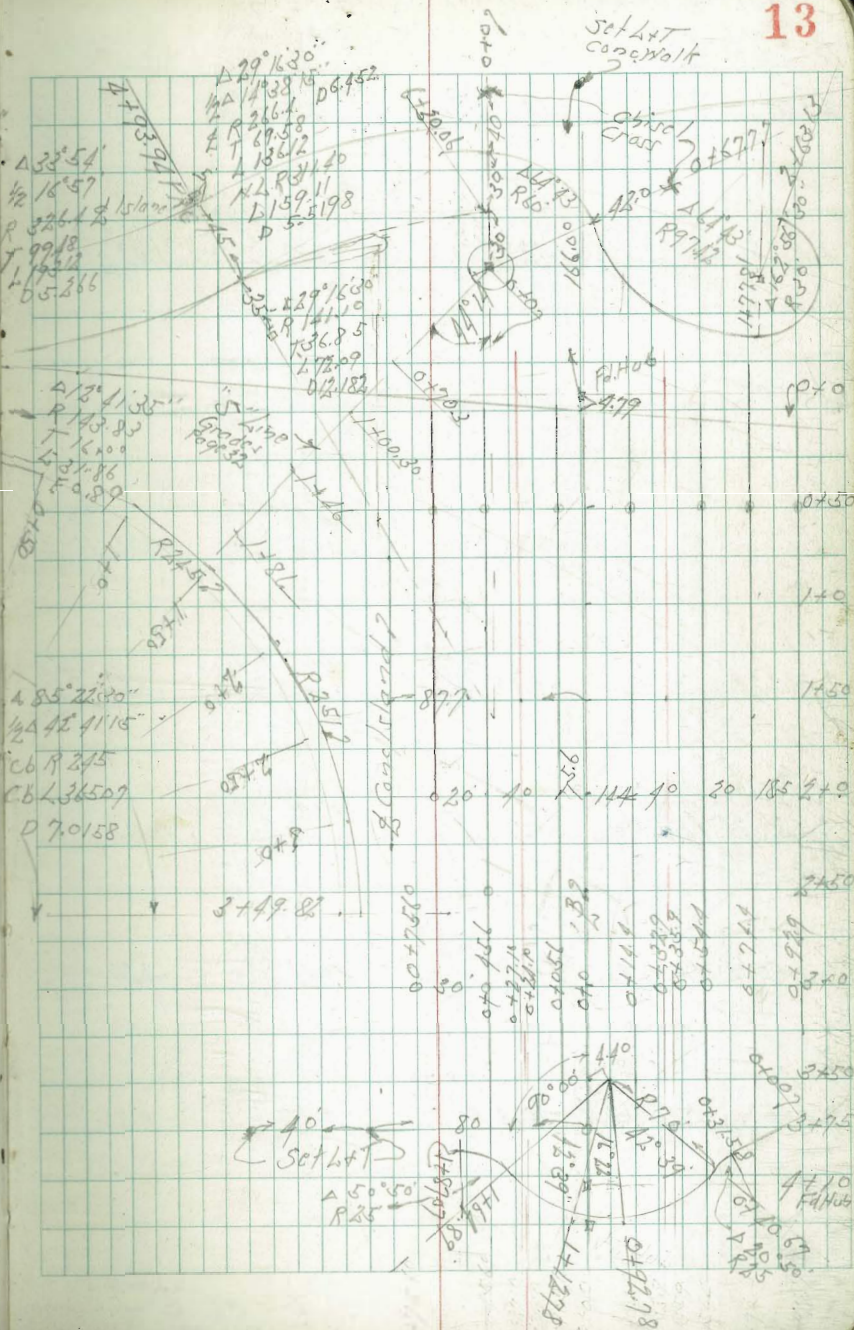
Cross Sections
1838-1

N.C. 60242

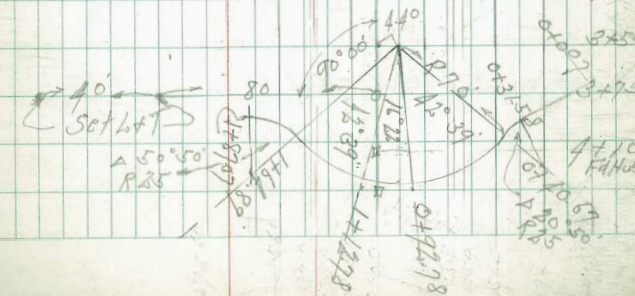
July 29-48

S. Sisson
Smith
Becker
Lee

13



$\Delta 85^{\circ} 21' 30''$
 $\Delta 44^{\circ} 41' 15''$
Cb. R 245
Cb. L 36507
D 7.0158



Paving Grades Santa Clara Point
East West Roadway

	North	SubGrade	South
2+0	6.23 6.23 6.23 1.64	cb 3.27 5.22 2.54 FO.62	6.23 1.64 7.87 71.64
1+75	6.45 6.45 6.00 1.42	cb 3.05 4.82 2.82 FO.63	6.45 1.42 7.75 71.30
1+50	6.71 6.65 6.06 1.16	cb 2.79 5.08 2.66 FO.25	6.71 1.16 7.39 FO.68
1+25	7.03 6.91 6.07 0.84	cb 2.47 5.40 1.74 FO.82	7.03 0.84 7.53 FO.50
1+01.21	7.39 7.13 6.26 +0.48	cb 2.11 5.76 1.38 FO.20	7.39 +0.48 7.83 FO.44
0+86.24	7.14 6.83 6.03 0.73	cb 1.86 6.91 1.13 FO.26	7.14 0.73 6.89 6.25
0+50.62	7.63 7.63 6.00 +0.24	7.43 7.30 6.03 +0.44	7.63 +0.24 7.38 6.07
0+15	8.22 8.22 8.22 -0.35	8.22 7.99 6.03 -0.35	8.22 -0.35 8.04 6.08
0+0	8.82 7.87	2+0.00 Santa Clara W. Bay side	-0.96 7.87

45'11 North

45'11	North	21'N	Gutter	South	South
	6.29 Sub	2.54 Sub	2.71 5.16	2.34 5.53	5.39 6.01
	1.86 6.01	2.54 5.53	2.71 5.16	2.34 5.53	5.39 6.01
	1.84 6.83	2.12 5.75	2.49 5.38	2.12 5.75	1.14 6.83
	1.38 6.49	1.86 6.01	2.23 5.64	1.86 6.01	1.38 6.49
	1.06 6.81	1.54 6.37	1.91 5.96	1.54 6.37	1.06 6.81
	0.70 7.17	1.18 6.62	1.55 6.32	1.18 6.62	0.70 7.12
	0.95 6.92	Gut. 1.30 6.57			0.95 6.92
	6.57 7.55	Sub 1.44 7.43			+0.33 7.45
	-0.35 8.22	Sub 6.35 8.22			-0.35 8.22
					7.87

Aug 8-48

East + West Roadway

Santa Clara Point

4+50 13° 05.58' North 4.19
 3.68 4.73
 FO.54
 cb 5.31 2.56
 4.58 3.72
 FI.76

4+30 11° 20.26' 4.31
 3.56 4.37
 FO.06
 cb 5.19 2.18
 4.46 3.82
 FI.74

4+10 9° 34.96' 4.45
 3.42 4.04
 cb 5.05 2.82
 4.32 3.39
 FO.57

3+90 7° 49.6' 4.62
 3.25 4.18
 cb 4.88 2.99
 4.45 3.90
 FO.81
 c 5.64 16.93

3+70 6° 04.3' 4.19
 3.08 4.22
 cb 4.71 3.16
 3.98 3.85
 FO.69
 c 5.64 24.55

3+11 3° 31.59' 3.50
 2.82 3.55
 cb 4.46 3.41
 3.93 4.11
 FO.70
 c 5.04 34.00

3+00.82 8.54 5.37
 2.50 3.62
 FO.25
 Suss. 4.49
 3.40 3.58
 FO.11

2+85 = Fly Island 5.48
 2.39 3.74
 cb 3.99 3.80
 3.26 4.52
 FO.64
 000

2+50 5.81
 2.06 3.75
 cb 3.69 4.18
 2.96 4.70
 FO.52
 6.90

2+45 on Souths
 A in Parving 2.02
 9.87
 8.14
 FI.65
 90LT

4E17	Sub 21H	Sub 21H	2 Gutter 31.5	39.5	15
3.90	4.38	4.75	3.12	4.05	
3.97	3.49	3.12			
3.78	4.26	4.63	4.60		
4.09	3.61	3.24			
3.64	4.12	4.49			
4.23	3.75	3.38			
3.47	3.95	4.32			
4.40	3.92	3.53			
3.30	3.78	4.15			
4.57	4.09	3.72			
3.05	3.53	3.90	3.53	OK 5.43	6.97
4.82	4.34	3.97	4.34		8.92
2.92	3.20	3.40	3.20	6' off edge	9.01
5.15	4.62	4.47	4.67		
2.58	3.06	3.43	3.06	6' off edge	2.95
5.39	4.81	4.44	4.81		4.92
		3.28			
		4.59			
2.28	2.76	3.13	2.76		
5.49	5.11	4.74	5.11		
		2.92		6' off edge	3.15
		4.95			2.60
	2+24				2.61
7.87					5.20
					5.77

East West Roadway

	North Subgrade		South Sub Grade	
B.M.			Top of H/d 21.6 ft of 5+38 6.97	
	For East Page 31			
1+53.05	11°38.25'			
35.68				
6+17.37	11°21.33'	cb 3.90 5.23 3.87 5.02 c-0.21	cb 4.33 3.20 4.50 3.20 8°55'	5+66.04 Top of H/d 11°38.25'
c-49.12 Skline 48.39				
5+68.98	6°54.21'	cb 4.46 4.67 3.79 6.48 F1.81	cb 5.39 3.74 4.65 4.96 F1.76	11°22.9'
c-27.60 27.19				
5+11.79	1°24.13'	cb 4.34 4.59 3.81 5.86 F1.37	cb 5.44 3.69 4.97 5.03 F1.34	7°19.3'
c-27.05 26.64				
5+15.15	1°57.08'	cb 4.56 4.57 3.83 6.19 F1.62	cb 5.46 3.67 4.73 5.05 F1.38	5+10 3°15.6'
c-21.53 Skline 5=21.21				
H.L. Sta 4+93.94	16°57'	3.32 3.81 5.93 F0.61	cb 5.41 3.69 4.91 5.06 F1.37	2 Sta 4+93.94
2 Sta				
4+70	14°50.9'	3.76 5.37 5.35 5.23 F0.98	5.39 3.74 4.66 5.23 F1.41	Top of H/d
TP	2.16	9.13	0.90 6.97	
		7.87		

45'N	39'N	31'N	L	21.5
45'N Gutter	39'N Sub	31'N Sub	L Gutter	21.5
3.48 4.39 ✓	3.53 4.34 +0.05	1.01 3.86 ✓	1.77 3.10 ✓	
3.90 3.97 ✓	3.95 3.92 ✓	4.43 3.44 ✓	4.82 3.04 ✓	
3.98 3.89 ✓	4.03 3.81 ✓	4.51 3.36 ✓	4.88 2.99 ✓	
4.00 3.87 ✓	4.05 3.82 ✓	4.53 3.34 ✓	4.90 2.97 ✓	
4.03 3.84 ✓	4.51 3.35 ✓	4.88 2.99 ✓	4.80 ✓	
3.98 3.89 ✓	4.45 3.41 ✓	4.83 3.04 ✓		
	7.87			89.67

South West Curve

Station	Angle	Subgrade R 251	Subgrade R 245	5.90
3+49.82	EC 40° 54.24	2.85 6.16	3.04 2.83	5.92 5.82 5.87
+25		5.94		
3+0	35° 04.74	5.73 5.72 0.0	3.28 5.73	3.16 5.85 6.03 FO.17
+75		5.68		
2+50	29° 13.95	5.63 5.78 FO.15	3.38 5.63	3.26 5.75 6.45 FO.40
+25		5.61		
2+0	23° 23.16	5.69 5.77 FO.12	3.44 5.69	3.22 5.69 5.99 FO.30
+75		5.52		
1+50	17° 32.37	5.45 5.45 0.0	3.56 5.45	3.34 5.67 5.74 FO.07
+25		5.54		
1+0	11° 41.58	5.63 5.89 FO.25	3.38 5.63	3.27 5.74 6.31 FO.57
+75		5.68		
0+50	5° 56.79	5.74 5.99 FO.25	3.77 5.74	3.12 5.89 6.86 FO.97
c-48.90	5' South of station			
c-49.91	on Pav. Line		5.85	
0+00 = P.R.C.		5.97 5.55 FO.58	3.04 5.97	2.94 6.07 7.25 FO.18
0-31.86 = P.R.C.			2.90 6.11	2.79 6.22 6.59 FO.31
0-67.33 = 250' P.C. Curve			2.70	2.59 6.42 6.00 FO.48
B.M.	2.01 9.01		6.97	6.42 6.71 FO.94 TOP of Hnd

Paving Grader Sky End Santa Clara Point
Alignment Page 13
Staker offset 5' South of Paving Edge Aug. 19-48

Station	Subgrade 6' N of Sky	Subgrade 5' S of Pav.	5.84
+89.07 = F.C.		2.80	5.84 5.49 FO.34
+64.89 P.R.C.	2.99	2.94	5.70 5.13 FO.53
+38.80			
26.05			
1+13.78	2.97	2.94	5.70 5.61 FO.14
20			
+92.78 = P.C.	2.97	2.94	5.70 5.52 FO.17
+66.72			
26.05			
+10.69 P.R.C.	2.94	2.91	5.73 5.38 FO.35
+31.58 B.C.T.	2.94	2.91	5.73 5.38 FO.39
0+0 = S.F. Cor. -3+73 to North	2.89	2.86	5.78 5.49 FO.68
B.M.	1.67	2.64	6.97 TOP of Hnd

Paving Grader Santa Clara Point
Parking Area North & South Strip

929E 869E 744E 544E 344E

1450
5.37
5.72 3.74 3.77 3.82 3.90 3.98
FO.45 5.24 5.19 5.11 5.11 5.19 5.03
4.79
c.032

140
5.07
5.72 3.94 3.97 4.02 4.10 4.18
FO.92 5.07 5.04 4.99 4.91 4.91 4.83
4.70
c.0.21

0750
5.17
5.72 3.84 3.90 4.02 4.27 4.36
FO.56 5.17 5.11 4.98 4.91 4.94 4.65
4.74
c.0.20

0700
5.80
5.78 3.81 3.79 3.46 3.94 4.24
FO.02 5.80 5.72 5.55 5.05 5.05 4.77
4.52
c.0.02

0-20
6.07
5.63 2.94
FO.44

41 Rad Pt.
595
5.48 3.06
FO.47

0-36.54
6.17
6.17 2.84
Rad

0-100
8.17 2.04 9.01 6.97
Top of F.H.D.
21.6.1 5.13.8

14.4 F 2 05.677 25.6 M 45.6 M 55.6 M

4.06 4.87 4.71 4.38
4.95 4.14 5.04 4.22 4.30 4.82 4.38
4.87 FO.17 4.79 4.71 FO.16 4.63

4.26 5.26 4.67 4.51 4.58
4.95 c.0.19 4.34 4.72 4.42 4.50 4.99 4.58
4.67 FO.05 4.59 4.51 FO.48 4.43

4.46 4.47 4.31 4.78
4.55 4.54 4.70 4.62 4.70 4.42 4.78
4.47 FO.23 4.39 4.31 FO.11 4.23

5.00 4.31 4.11
4.52 5.21 4.70 4.77 4.50 4.90 4.27 out
4.49 FO.21 4.31 FO.16 4.21 4.11 FO.15

3.68 4.94 4.35 4.81
5.33 4.07 5.10 4.36 4.66 4.26 4.81
4.94 FO.16 4.65 4.33 c.0.09 4.20
3' west

5.14
3.87 5.39 4.09
5.14 FO.25 4.92

9.01

East. 929F ^{89F} 744F 544F 344 144F Z 056 256 15.6 65.6M

3172 2.86

3+50 ^{6.09}
5.75
c0.32 2.94 2.97 3.02 3.10 3.17
6.04 5.99 5.91 5.91 5.81
out c0.77 out

3+0 ^{5.87}
5.81
c0.26 3.14 3.17 3.22 3.30 3.38
5.81 5.79 5.71 5.76 5.63
c0.55 ✓

2+50 ^{5.67}
5.83
F0.16 3.34 3.37 3.42 3.50 3.58
5.64 5.59 5.51 5.51 5.43
c0.52 ✓

2+0 ^{5.47}
5.86
F0.33 3.54 3.57 3.62 3.70 3.78
5.44 5.39 5.31 5.31 5.23
c0.73 ✓

9.52
9.01 ✓

3.25 3.20 3.27 3.25 3.04
5.76 5.71 5.71 5.76 5.97
out out out out ✓

^{6.06}
5.64
c0.72 3.46 3.54 3.57 3.60 3.68
5.85 5.47 5.45 5.41 5.41 5.72
c0.07 ✓ ✓ ✓ ✓ ✓

3.66 3.74 3.80 3.87 3.73
5.35 5.27 5.27 5.21 5.11 5.38
F0.01 ✓ ✓ ✓ ✓ ✓

^{5.66}
5.47
c0.17 3.86 3.94 4.02 4.10 4.18
5.15 5.07 5.07 4.99 4.91 5.33
F0.09 ✓ ✓ ✓ ✓ ✓

9.01 ✓

Curb Grades East Side of Division St.
Island Ave. to 200 North

			Curb	
340	Sly Market	11.50	5.81	
240	Erd	9.33	7.98	
155		8.26	8.95	
1710		6.71	7.38	9.93
190		6.28	6.95	10.26
773	N Y Drive	5.90	6.57	10.71
750		5.41	6.08	11.23 11.77 FOA 900000 Drive
736	Sly Drive	5.19	5.82	11.19
717	N Y Drive	5.04	5.68	11.63
070	N L Island Ave	4.93	5.60	11.71
BM	688	17.31	10.93	5 1/2 BP Market + 471.02

INDEXED
WK
DEC 15 1948

Staker offset 2' Back of
Face of curb

Sept 9-48
S. May
Smith
Becker

20

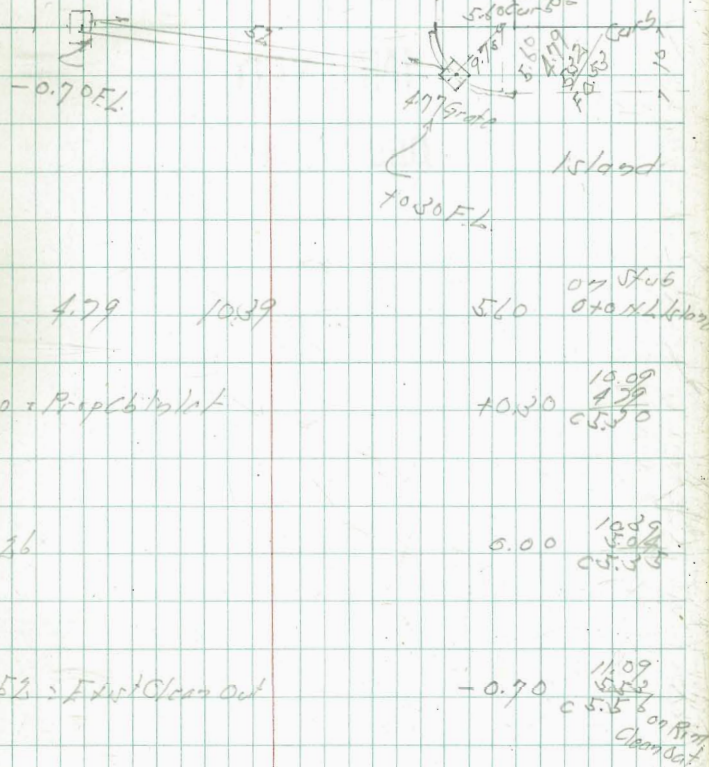
July 1-48

S. May
Smith
Becker
Loc.

Storm Drain

Union

Cross Sec #1842



Sewer Grades Block 120 La Playa

B.M.	11.36	44.96	33.60	X.F.B.P. Rosenblatt Kellogg St
TP	9.41	53.94	0.43	44.53

0+0 = Exist M.H. 9.23 44.71 Invert

INDEXED
WK
DEC 15 1948

+25 44.89 $\begin{matrix} 9.05 \\ 5.26 \\ \hline 2.79 \end{matrix}$

+50 45.06 $\begin{matrix} 8.88 \\ 1.06 \\ \hline 2.82 \end{matrix}$

+75 45.24 $\begin{matrix} 8.70 \\ 1.26 \\ \hline 2.70 \end{matrix}$

+100 = D.F. 45.41 $\begin{matrix} 8.53 \\ 6.21 \\ \hline 7.82 \end{matrix}$

June 25-48
S. S. S. S.
Smith
Lee
Finney

Stakes offset 5' from top of
Sketch #1475-48

Kellogg St
*Edwards Court

San Felipe

Block 120
Exist M.H. @ 0+0

Rosenblatt

← 1+0

Jenkins St

Volley Ball Courts
 Presidio Playground

BM	794	15.76	7.82	SE BP Chapman Taylor
TP	4.54	12.34	6.96	8.80

INDEXED
 WK
 DEC 15 1948

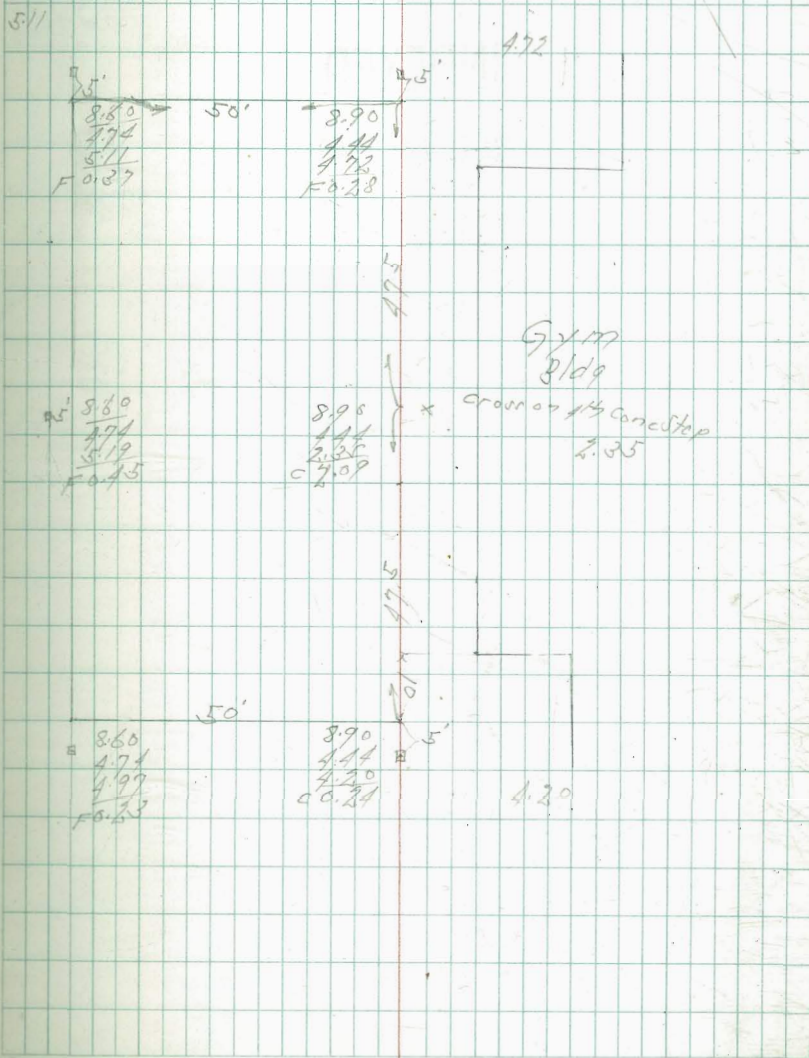
1519

4.97

July 18-48

5.500
 Smith
 Becker
 Lee
 67582

22



Sewer Laterals Alley Block 45
Tract # 1868

BM 0.00 362.83

362.83

NW 8P
Trojan Ave
Winona

0+0 = H.L. Trojan

0+60 ③ on West

353.20

9.63
8.36
3.07
5' W of W.L.

INDEXED

WK
DEC 15 1948

1+10 ① on West

353.59

9.27
6.21
6.27
5'

3+60 ② on West

355.21

7.57
6.33
6.24

Sewer Laterals Alley Block 47
Tract # 1868

July 19, 48
S. S. 02
Smith
Becker
207

23

N.O. 31211

BM 3.36 347.14

344.28

N.E. 8P
Trojan Ave
Winona

TP 8.39 353.67 236

345.28

0+0 = H.L. Trojan

2+85 ⑤ on West

344.54

9.13
4.07
6.06
5'

INDEXED

WK
DEC 15 1948

3+10 ④ on East

345.27

8.10
8.26
4.64
5'

Grader 6" Water Main Stationing A/c.
Trojan A/c to E/Cajon A/c

INDEXED
WK
DEC 15 1948

1+90.5 357.90 $\frac{8.41}{3.26}$

1+43 = F.V.C. 357.50 $\frac{8.81}{3.20}$

1+03 357.50 $\frac{8.81}{3.70}$

+63 = P.V.C. 358.20 $\frac{8.11}{3.25}$

+31.5 358.90 $\frac{7.41}{3.38}$

0+0 = M2 Trojan 359.60 $\frac{6.79}{3.99}$

BM 3+8 366.31 362.83 $\frac{3.48}{3.70}$
Trojan
Stationing

Grade 3.5 Below East Gutter Pencil Grade #2396
offset 5 East of 1/2 Ditch

24

5+50.4 = S.L. E/Cajon 369.70 $\frac{5.77}{3.33}$

5+04.6 367.00 $\frac{8.42}{3.74}$

4+58.8 364.30 $\frac{11.17}{3.79}$

TP 964 375.47 0.48 365.83

4+13 = F.V.C. 361.60 $\frac{4.91}{3.22}$

3+73 359.90 $\frac{6.41}{3.70}$

3+33.0 = P.V.C. 359.10 $\frac{7.31}{3.77}$

2+85.5 358.70 $\frac{7.61}{3.76}$

2+38 358.30 $\frac{8.61}{3.74}$

366.31

Grades 6" N of Main Estrella Ave
Trojan Ave. to El Cajon Ave

INDEXED

WK

DEC 15 1948

+50				344.85	1054 228 c3.32
TP	751	355.41	4.99	347.87	
2+0				344.46	8.10 4.29 c3.71
+50				344.07	8.79 5.36 c3.43
1+0				343.68	9.18 5.77 c3.41
+50				343.29	9.57 6.26 c3.31
0+0 = 1/2 Trojan				342.90	9.06 6.45 c3.51
BM	858	352.86		344.28	N.F.B.P. Trojan Ave. +781.51

Mail to Paving
off set E East of 2 Ditch

July 19-48

5,550.7

5,331.5

218.8

25

xlo 31211

+35 = S.L. El Cajon Ave.				346.30	9.11 5.81 c3.30
4+0				346.03	9.39 6.19 c3.20
+50				345.63	9.78 6.48 c3.30
3+0				345.24	10.17 6.77 c3.40

355.41

Paving Grader Alley Block 47 Tract # 1368
Trojan to Elkcapn Between 2pts + Estrella

W.O. 31121
Cross Sections 1737-1

July 21-48
S. 5599
Smit 6
Sector
LCC

26

2+12.5	$\frac{6.48}{5.18}$ C.O. 30 3	348.30		348.50	$\frac{6.50}{5.36}$ 3
TP	6.18	347.78	369	348.60	
1+70	$\frac{4.77}{4.33}$ C.O. 40 3	347.57		347.77	$\frac{4.52}{3.97}$ C.O. 10 Hail Fence
INDEXED WIK DEC 15 1948					
1+27.5	$\frac{5.45}{5.31}$ C.O. 14 3	346.84		347.04	$\frac{5.25}{4.86}$ C.O. 11 3 on Conc Hpro
+85	$\frac{6.18}{5.69}$ C.O. 47 3	346.11		346.31	$\frac{5.98}{4.54}$ C.O. 14 3
TP	6.30	352.29	442	345.99	
+42.5	$\frac{5.03}{4.93}$ C.O. 60 3.8 on 100'	345.38		345.58	$\frac{4.83}{3.75}$ C.O. 68 3 Hail Fence
0+0 Trojan	$\frac{5.76}{5.59}$ C.O. 37 3	344.65		344.85	$\frac{5.56}{5.36}$ C.O. 00 cb Return
TP	5.48	350.41	823	344.93	
BM	8.88	353.16		344.28	N.M.B.P. Trojan 478173

		West	\$	East	
1+04.56 = SLEFCapn 7990 on 8109	$\frac{4.53}{4.43}$ C.O. 20 3	350.25		350.29	$\frac{4.49}{4.20}$ C.O. 20 0.75 cb Return
3+80	$\frac{4.14}{4.82}$ F.O. 88 3	350.64		350.82	$\frac{3.96}{4.07}$ F.O. 11 0.7 Hail Fence
3+60	$\frac{4.08}{4.79}$ F.O. 71 3	350.70		350.90	$\frac{3.88}{3.97}$ F.O. 09 0.9 Hail Fence
3+40 - P.V.C	$\frac{4.30}{4.90}$ F.O. 60 3	350.48		350.68	$\frac{4.10}{4.27}$ F.O. 17 3
2+97.5	$\frac{5.03}{5.03}$ F.O. 02 3	349.75		349.95	$\frac{4.83}{4.59}$ C.O. 14 3
2+55	$\frac{5.76}{5.33}$ C.O. 48 3	349.03		349.22	$\frac{5.06}{4.99}$ C.O. 54 3

354.78

Paving Grades Alley Block #6 Tract 1368
Trojan to El Copon Between Estrella & 49th St.

INDEXED

WK
DEC 15 1948

	West	E	East		
2+24	6.34 4.75 c 1.59 0.30 Nail Fence	349.76	350.06	6.34 4.75 c 1.59 0.30	
1+76	6.68 4.27 c 2.41 0.25 Nail Fence	349.42	349.72	6.68 4.27 c 2.41 0.25 Nail Fence	
1+28	7.03 4.35 c 2.68 0.55 Nail Fence	349.07	349.37	6.73 4.35 c 2.38 3	
+80 = Bk. A	7.38 5.92 c 1.46 0.6	348.72	349.02	7.08 6.62 c 1.46 3 Nail Fence	
+50	7.52 7.98 F 0.46 3	348.58	348.88	7.22 7.32 F 0.10 3	
+20 = Bk. F	7.66 8.02 3	348.44	348.74	7.36 8.86 c 0.56 16 Nail Fence	
0+0 = N. L. Trojan	7.61	348.49	348.63	7.27 7.87 c 0.60 Nail Fence	
TP	7.53	356.10	4.59	348.57	N. L. B.P.
BM	8.88	353.16		344.28	Trojan + 48th

1+199 = St. El Copon	9.70 0.20 0.20 0.20 0.20 0.20	352.69	352.06	140	27
+40	5.10 5.10 0.98 0.20	352.36	352.66	4.85 4.85 c 0.75 2.75	Tack 12005 510P
+20	5.56 5.56 0.10 0.10	351.90	352.20	5.26 4.78 c 0.50 2.75	on 8.649
TP	6.86 0.149	357.46	5.50	350.60	
+10	4.61 c 1.60 0.05	351.49	351.79	4.31 6.40 c 0.3 0.3	on 8.649
+80	4.96 5.37 F 0.41 3	351.14	351.44	4.66 4.88 c 0.38 7.0	c 1.0 Nail Fence
+60	5.21 5.86 F 0.35 3	350.86	351.16	4.91 4.35 c 0.59 10	on 8.649 Nail Fence
+40	5.17 6.18 F 0.71 1.0	350.63	350.93	5.17 4.59 c 0.58 0.2	
3+20 = P.V.C.	5.44 5.29 c 0.36 0.66 Nail Fence	350.46	350.76	5.34 4.23 c 1.12	
2+72	5.99 6.12 F 0.13 3	350.11	350.41	5.69 4.06 c 0.59 0.55	Nail Fence
		356.10			

Paving Grades Filly Block 45 Tract # 1368
Troja to El Cajon Between 49th + 51st

	West	±	East	
+50	$\frac{5.27}{5.89}$ F1.57 5	358.27	358.49	$\frac{5.86}{6.18}$ F1.12 2 076 4900
3+0	$\frac{5.40}{5.78}$ F1.38 3	358.15	358.37	$\frac{5.18}{6.00}$ F0.82 3
+50	$\frac{5.53}{5.43}$ CO.10 3	358.02	358.24	$\frac{5.31}{4.66}$ CO.65 3
2+0	$\frac{5.65}{5.52}$ CO.12 3	357.90	358.12	$\frac{5.43}{5.24}$ CO.17 3
TP	5.42	362.35	4.00	358.13
+50	$\frac{4.35}{5.26}$ F0.90 3	357.78	358.00	$\frac{4.13}{4.94}$ F0.81 3
1+0	$\frac{4.48}{5.30}$ F0.82 3	357.65	357.87	$\frac{4.41}{4.23}$ CO.03 3
+50	$\frac{4.61}{4.97}$ F0.36 3	357.52	357.74	$\frac{4.39}{4.29}$ CO.10 3
TP	5.09	362.13	6.23	357.04
0+0 = H.L. Troja	5.97	357.40		357.62
BM	0.54	363.27		362.83 H.W. BP Troja + W1070

W.O. 31121
Cross Sect 1042 1737-11

July 31-48
S. 5509
Smith
Becker + Lee
28

INDEXED
WK
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	West	±	East	
				2.80 364.52 737 CO.15 07.50 364.52 1737.16
+19.52 = H.L. El Cajon			363.14	364.10 3.23 990 = Dir. 4.18
5+0	$\frac{4.94}{5.72}$ F0.80 5		362.40	362.62 4.70 5.70 07.00 1.15 on steps 8.09
+80	$\frac{6.19}{6.77}$ F0.58 5		361.20	361.42 5.90 6.15 07.85 5
+60 = P.V.C.	$\frac{7.31}{7.71}$ F0.40 5		360.01	360.23 7.09 7.96 08.13 5
+40	$\frac{8.17}{8.48}$ F0.31 3		359.15	359.37 7.25 7.72 08.23 5
TP	9.18	367.32	5.41	358.14
+20	$\frac{4.94}{6.08}$ F1.14 5		358.61	358.83 4.97 5.72 06.98 3
4+0 = P.V.C.	$\frac{5.15}{6.54}$ F1.39 5		358.40	358.62 4.93 5.00 17 on conc. wall
			362.55	

Grades Water System Santa Clara Point
 East West 4" line
 Sketch Page 13

Stakes offset 5' south
 of 4" Ditch

July 26-48
 J. J. Smith
 Specter
 L. C. E.

29

3-41-32				
2+80 = 4" x 1" Cross		-1.27	9.12 6.43 c2.73	
2+46 = Corporation Stop out				
2+45 = Lat #2	-1.55	-1.55	9.70 7.27 c2.43	
1+99		-1.92	10.07 7.64 c2.43	
1+53		-2.29	10.44 7.42 c2.96	
1+07		-2.66	10.81 8.15 c2.66	
761		-3.03	11.18 8.15 c3.03	
5-4	-3.40		11.55 8.15 c3.40	
0+15 = 4" x 1" Tee = Lat #2		-3.40		
B.M.	9.10	-0.95	4+0 2" Santa Clara W. Pipe -0.96	
B.M.	118	8.15	78 P.F.H.D. 21.6' 4' 5" 28"	

79	2.67	9.64	1.18	6.97	
6+35				+0.91	7.24 5.52 c3.80
1-42					
5+93 = 4" x 1" Cross				+1.20	6.95 5.75 c3.60
5+48.66				+0.85	7.30 5.30 c2.00
5+04.33				+0.50	7.65 5.15 c2.50
3-44.32					
4+60 = Corporation Stop				+0.16	7.98 5.82 c2.16
1-55					
4+05 = Lat #2	-0.28			-0.28	8.43 5.19 c3.24
1+04 Corp. Stop out					
3+62.66				-0.61	8.76 5.69 c3.07
3+21.32				-0.94	9.00 5.64 c3.36

8.15

stakes offset 5' West
of 15 Ditch

7+65 = 4" x 4" TCC	0.00	9.64 6.38 63.06
7+30	+0.25	9.39 5.59 63.80
2+35		
6+95 : Corp Stop	+0.49	9.15 5.45 63.95
6+65	+0.70	8.94 5.24 63.70

9.64

1+05 = 4" x 4" TCC	-0.60	10.24 8.28 63.76
0+70	-0.36	10.00 8.25 63.95
0+35	-0.12	9.70 8.64 63.93
0+0 = 5/8" Existing Line	9.54	9.54 6.10 63.75

9.64 Bix Ford
Opp Page

Paving Grades 5 line Santa Clara Point
Sketch Page 13

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1+86	5.62	4.11	$\begin{matrix} 1.00 \\ 4.37 \\ \hline 0.50 \end{matrix}$
------	------	------	---

1+46	5.01	4.73	$\begin{matrix} 1.20 \\ 4.33 \\ \hline 0.60 \end{matrix}$
------	------	------	---

1+00.30	4.00 Sub Grade 3.82 0.18 of Conc 1/4 in. Box	5.01	$\begin{matrix} 1.00 \\ 3.75 \\ \hline 0.25 \end{matrix}$
---------	---	------	---

0+70.30 = Opp Detail H		5.04	$\begin{matrix} 3.07 \\ 3.83 \\ \hline 0.77 \end{matrix}$
------------------------	--	------	---

0+0 = 60 Curb Radius		4.32	$\begin{matrix} 4.69 \\ 5.25 \\ \hline 0.56 \end{matrix}$
----------------------	--	------	---

SM	2.76	9.73	6.97	Top Fire Hydrant
	2.04	9.01	6.97	

Curb Grader West Part of Detail H
Santa Clara Point

	Gutter	Sub. Grade	Curb Gr.	
1+44.50 - A	5.11	4.94	5.67	$\frac{4.35}{5.72}$ FO.87
1+25.55 - F.C.	5.15	4.98	5.71	$\frac{4.31}{4.80}$ FO.59
1+11.80 = $\frac{1}{2}$ Curve	5.17	5.00	5.73	$\frac{4.19}{4.82}$ FO.70
+98.66 - B.C. 17.5 R	5.19	5.02	5.75	$\frac{4.17}{4.72}$ FO.53
+79.56 - F.C.	5.21	5.04	5.77	$\frac{4.15}{4.94}$ FO.79
+70.34 = $\frac{1}{2}$ Curve	5.16	4.99	5.72	$\frac{4.20}{4.85}$ FO.65
+61.12 P.C.C. R 10'	5.11	4.94	5.67	$\frac{4.25}{5.65}$ FO.80
+40.74	5.09	4.92	5.65	$\frac{4.37}{5.80}$ FO.73
+20.37	5.06	4.89	5.62	$\frac{4.35}{5.27}$ FO.97
0+0 = S.W. Cor. B.C. R 60.87	5.03	4.86	5.59	$\frac{4.33}{5.22}$ FO.89
B.M.	2.95	9.92	6.97	$\frac{9.17}{}$

Curb Grader East Part of Detail H
Santa Clara Point

33

	Gutter	Sub. Grade	Curb Grade	
+27.23 = $\frac{1}{2}$ 10' R	5.13	5.01	5.74	$\frac{4.18}{4.88}$ FO.62
+17.22 = B.C.	5.21	5.04	5.77	$\frac{4.15}{4.94}$ FO.79
1+01.50 F.C.	5.19	5.02	5.75	$\frac{4.17}{5.07}$ FO.70
+87.75 = $\frac{1}{2}$	5.16	4.99	5.72	$\frac{4.30}{4.77}$ FO.57
+74.01 = B.C. 17.5	5.13	4.96	5.69	$\frac{4.23}{4.82}$ FO.59
+61.0°	5.10	4.93	5.66	$\frac{4.31}{4.86}$ FO.70
+54.06	5.08	4.91	5.64	$\frac{4.38}{4.75}$ FO.79
+32.70 Δ 60°	5.05	4.88	5.61	$\frac{4.31}{4.89}$ FO.68
+22.70 - F.C.	5.09	4.92	5.65	$\frac{4.37}{4.89}$ FO.63
+11.35 = $\frac{1}{2}$ Curve	5.12	4.95	5.68	$\frac{4.34}{4.82}$ FO.63
0+0 = P.C.C. R 60.87 + R 10'	5.16	4.99	5.73	$\frac{4.20}{4.92}$ FO.73
	$\frac{9.17}{}$			

992

Curb Grader Detail B

	Gutter	Sub Grade	Curb Grade	
Mid. point	537	3.80		
	543			
1402.44	PRC R3	3.74	3.57	4.30 5.62 6.19 FO.57
0+89.55	PA	3.77	3.60	4.33 5.39 6.26 FO.66
+76.66	PRC	3.81	3.64	4.37 5.55 6.17 FO.62
+70.19	BC R10	3.84	3.67	4.40 5.57 6.12 FO.62
+52.00	A	3.54	3.96	4.69 5.23 5.94 FO.71
+26.45	A 135°	4.18	4.01	4.74 5.18 5.88 FO.76
+13.23		4.12	3.85	4.58 5.34 6.08 FO.74
0+0	PC R	3.86	3.69	4.42 5.50 6.19 FO.67
		9.17		
BM	2.95	9.92	6.97	Top. Firm H/d.

Curb Grader Detail C+D

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Detail D

	Gutter	Sub Grade	Curb Grade	
+96.26 = 0+0			4.40	5.13 cut
			4.62	
+78.85 = A	SFCor	4.55	4.88	5.11 4.81 5.52 FO.97
	split	4.37	4.80	
+41.56 = A		5.04	4.87	5.60 4.53 5.10 FO.78
		4.37		
+20.68		4.80	4.53	5.36 4.57 5.19 FO.62
		4.60		
0+0 = SFCor		4.57	4.40	5.13 4.79 5.41 FO.62
		9.17		

Detail C				
+89.84 = 0+0			3.74	4.17 cut
			5.24	
+72.50 = PRC R15		3.93	3.76	4.49 5.43 6.13 FO.70
		5.14		
+58.88 = P		4.03	3.86	4.59 5.30 5.98 FO.65
		4.74		
+26.56 = SFCor		4.13	4.26	4.99 4.03 5.89 FO.67
		5.26		
0+0 = SFCor		3.91	3.74	4.49 5.15 5.54 FO.69
		9.17		
		9.92		

Paving Grader Superior St.
38th St. to 39th St.

INDEXED

WK
DEC 15 1948

		Subgrade			
200	1.82	112.75	112.47 1.87	112.25	1.82
+10	1.23	112.35	112.07 2.27	111.85	1.72
+20	1.82	111.75	111.47 2.82	111.25	2.33
2+0	PVC 2.53	111.05	110.77 3.52	110.55	2.03
				814	5574
				12.33	12.33
				113.57	113.57
				2 Grader	
				101.24	
				13.10	
				114.34	
0+60	8.11 7.63	105.94	105.66 8.68	105.44	8.13
0+40	8.96	104.61	104.38 9.96	104.21	9.36
0+20	10.80	102.77	102.66 11.68	102.54	11.03
0+0	13.64	100.93	100.94	100.85	12.72 Pav.

38th St.

Cross Sec. 1780-18
H.O. 31397

July 27-48
S. S. Smith &
Becker
Sec

35

		Subgrade			
39th St.					
6+00	9.22	104.35	103.97 10.37	103.75	9.82
+80	1.62	111.95	111.67 2.62	111.45	2.12
+60	1.12	112.45	112.17 2.12	111.95	1.62
+40	0.72	112.85	112.57 1.72	112.35	1.23
+20	0.52	113.05	112.77 1.52	112.55	1.03
3+0	0.41	113.15	112.87 1.47	112.65	0.93
2+80	0.52	113.05	112.57 1.52	112.55	1.03

2 Grader
July 30-48

	Gutter	Subgr.	Curb Grade		
3+14.78	4.79 aplt 4.92	4.34	4.98 5.07	1.10 1.60 F0.59	
+64.78	5.05 + 1.12	3.94	4.78 4.57	4.25 5.25 F1.01	4.50 5.00 F0.52
+39.78 = FC	5.17 4.00	3.69	4.80 4.42	4.25 5.26 F0.49	4.50 5.24 F0.67
+20.54	5.07 1.10	3.86	4.59	4.51 4.78 F0.40	
2+01.20	4.99 1.25	4.04	4.60 4.77	4.10 5.14 F0.74	4.50 5.19 F0.53
+86.30 = A	4.92 4.25	4.14	4.65 4.87	4.57 4.83 F0.33	4.75 4.75 F0.55
+64.94	4.87 4.30	4.20 4.31	4.76 5.04	4.12 5.08 F1.45	4.17 5.21 F0.81
1+44.96	4.82 4.25 aplt 4.74	4.18 4.35	4.83 5.08	4.34 5.12 F1.12	4.50 5.03 F0.94
+94.94	4.67 4.57	4.45	5.06 5.18	3.99 4.60 F0.61	
+71.34	4.99 4.68		3.89 4.32 5.28		
+44.94	4.37 4.80 aplt 4.46	4.65	5.34 5.38	3.77 4.25 F0.61	
0+0 = FC Cor	4.36 5.01	4.84	5.57	3.60 4.32 F0.72	
314	2.20 9.17		6.97	Top of H...	

	Subgr.	Curb Grade		
	2.95	3.50	3.50 Conc	
			Boat House	

3.30 3.50 Conc 3.50 Conc 3.30

Set 4" Rad curb grade as higher than walk
rest of curb same elev. as walk

Subgr. Curb Grade

Gutter 4+38.09 = 0+0 5.01 4.84 5.57 3.60

27.5 4.91 4+10.59 4.76 4.59 5.32 3.85 4.27 F0.44

27.5 4.66 3+83.09 Δ N 4.51 4.34 5.07 4.10 4.80 F0.70

aplt 4.64 3+38.49 Δ N 4.63 4.54 4.48 5.10 3.85 F0.65

Curb Grader Radius Point 60' Cb. Rad 50' at 5
of Community Hall

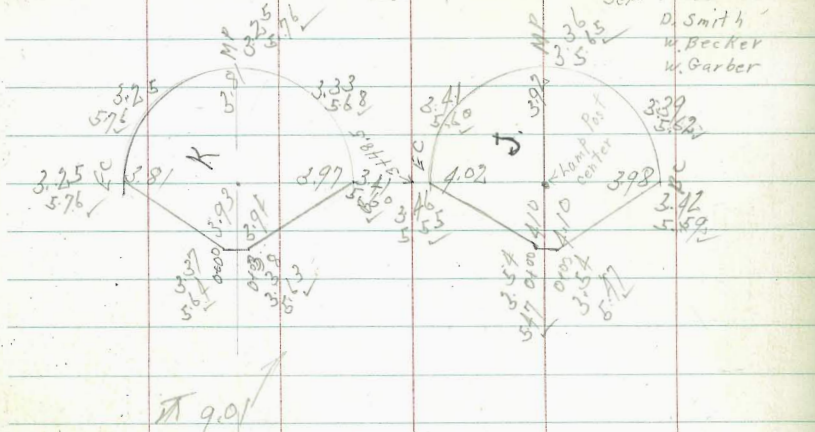
	Gutter	Sub Grade	Cb. Grade	
0+62.83 = 0+0	1.29	4.12	4.85	out
+47.13	1.41 4.72	4.24	4.97	4.25 5.90 F0.95
+31.42	4.69 4.44	4.52	5.25	4.67 5.72 F1.05
+13.71	4.61 4.52	4.44	5.17	4.75 5.88 F1.07
0+0 = Red. Line	4.29 9.13	4.85	4.85	4.85 5.07 5.96 F0.89
BM	2.95	9.92	6.97	Top Firm H/d

Curb Grader Detail E

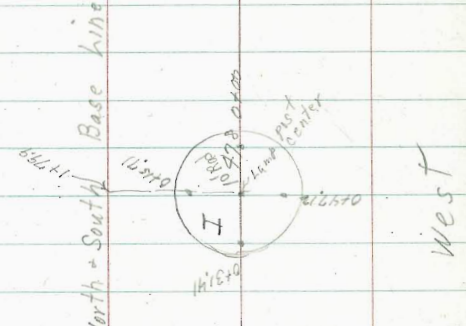
	Gutter	Sub Grade	Curb Grade	
+88.70 = 0+0		3.86		out
+75.25 = P.C.C. 15' P 393	5.34	3.76	4.49	5.23 5.88 F0.45
+57.76 = Δ	5.26	3.74	4.47	5.25 6.18 F0.70
split 91 4.16				
+32.35 = Δ	4.24	4.23	4.96	4.96 5.83 F0.87
split 196 4.21				
0+0 = S.W. Cor	5.14	3.86	4.59	5.52 5.76 F0.43
	9.17			
	9.92			

South

W.O. # 60242
 Sept 16 1948
 D. Smith
 W. Becker
 W. Garber

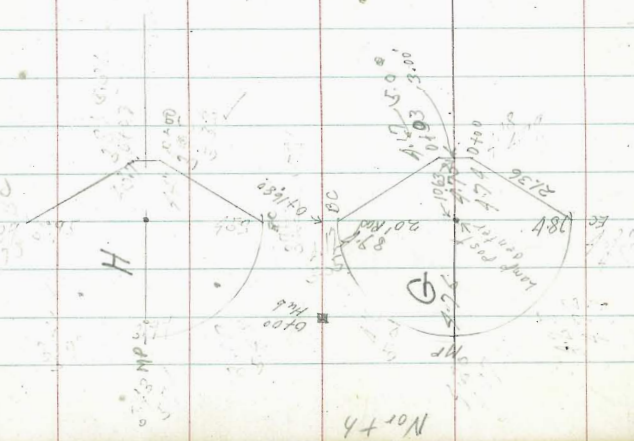


East



West

Note: All stakes set 3' inside curb face



North

Curb Grades Detail G+H. 38

	Detail H	sub grade	curb grade	
EC,	Gutter 4.32 1.69	4.52	5.25	3.92 4.59
"	4.42	4.59		F0.67
MP,	1.16	4.85	3.99	4.72 4.82
"	4.12	4.87		F0.37
BC,	4.12 4.89	3.95	4.68	4.49 5.06
				F0.57
0+03	4.54 4.77	4.37	5.10	4.07 4.72
				F0.65
0+00	4.58 4.43	4.41	5.14	4.63 4.70
				F0.67

Detail G. sub grade curb grade

EC,	Gutter 4.98 5.03	4.86	5.59	3.59 4.27
"	4.98	4.03		F0.69
M.P.,	4.93	4.08	4.76	5.49
"	4.89	4.12		3.68 4.34
BC	4.85 4.12	4.68	5.41	4.45 F0.69
0+03	4.90 4.71	4.73	5.46	3.77 4.69
				F0.97
0+00	4.91 4.71	4.74	5.47	3.70 4.35
				F0.65

B.M. 220 9.17 9.01A 6.97 Top Hyd.

Detail J

sub
gradeCurb
grade

EC,	3,29	4,02	5.15 5.80 F0.65
-----	------	------	-----------------------

M.P.	3.19	3,92	5.25 5.84 F0.59
------	------	------	-----------------------

B.C.	3,25	3,98	5.19 5.83 F0.64
------	------	------	-----------------------

0+03	3,37	4,10	5.07 5.75 F0.68
------	------	------	-----------------------

0+00	3,37	4,10	5.07 5.74 F0.67
------	------	------	-----------------------

Detail F

subgrade

Curb
grade

0+47.2	4.30 4.71	4,13	4.31 5.01 F0.70
--------	--------------	------	-----------------------

0+31.41	4.30 4.71	4,13	4.31 4.94 F0.66
---------	--------------	------	-----------------------

0+15.71	4.32 4.79	4,05	4.39 5.06 F0.67
---------	--------------	------	-----------------------

0+00	4.22 4.79 4.90	4,05	4.39 5.10 F0.71
------	----------------------	------	-----------------------

9.12

Detail K

sub
gradeCurb
grade

EC,	3,08	3,81	5.36 5.93 F0.57
-----	------	------	-----------------------

M.P.	3,08	3,81	5.36 6.11 F0.75
------	------	------	-----------------------

B.C.	3,24	3,97	5.20 5.82 F0.62
------	------	------	-----------------------

0+03	3,21	3,94	5.23 5.85 F0.62
------	------	------	-----------------------

0+00	3,30	3,93	5.24 5.85 F0.61
------	------	------	-----------------------

9.12

Sewer Laterals Alley Block 47

Ocean Beach

Cross Section 1814 x/o 31431

offset 5' back PL

BM 9.45 45.64
 ① North
 90' W of W.L. Sunset Cliff 31.76
 HW BP
 Sunset Cliff
 13.88
 8.65
 c 5.25
 5' N of PL

③ South
 90' W of W.L. Sunset Cliff 31.73
 13.91
 8.96
 c 4.95
 5' N of PL

INDEXED

WK
 DEC 15 1948

① North
 262.5' W of W.L. Sunset Cliff 28.20
 17.41
 11.92
 c 5.52
 5' N of PL

Sewer Laterals Alley Block 58

Ocean Beach

Cross Section 1768 x/o 31398

Aug. 30. 48
 5' 59.2
 5' 17.6
 Brother
 Ranger

40

BM 6.58 19.13 1305
 HW BP
 Cable +
 Cap. 11.17

① North
 10' W of W.L. Cable St 9.30
 9.83
 4.17
 c 5.65
 5' N of PL

INDEXED

WK
 DEC 15 1948

② South
 115' W of W.L. Cable St 9.03
 10.10
 5.39
 c 4.82
 5' N of PL

Paving Grader Hilley Block 21 University Hill
University to Lincoln between 3rd + Bancroft.

	West	East
+60	3.85 2.41 c1.44 5	344.79 344.49 4.15 4.67 F0.57 3
TP	4.07	348.64 9.01 344.57
+120	7.30 5.27 c2.03 5	346.08 345.78 7.80 6.79 c1.01 1.7 rail
INDEXED WIK DEC 15 1948		
+80	6.21 4.89 c1.32 3	347.37 347.07 6.57 6.85 F0.28 4 x on 4 R pro
+40	4.92 4.17 c0.85 5	P.V.C. 348.66 348.36 5.27 5.41 c0.14 4
+20	1.46 3.85 c2.39 5	349.18 348.87 4.76 4.90 F0.19 4
0+0 = N4U4N.	349.45 4.13 4.18 on Pav	349.12 4.45
BM	4.73	352.58 348.85 7' Cop. Rad 1694-69

Oct 27-48
S. S. Roy
Smith
Becker
Bancroft
Clark

W.O. 31236

Cross Sections
#1694

41

	West	East
+10	4.53 4.96 F0.43 2	339.81 339.51 4.83 4.49 c0.34 5
+20	4.33 3.99 c0.34 7	340.01 339.71 4.63 4.38 c0.25 4
TP	5.14	344.34 9.44 339.20
3+0	8.26 7.98 c0.28 2	340.38 340.08 8.56 9.23 F0.67 3
+80	7.70 8.82 c1.12 1 rail 1 rail	P.V.C. 340.94 340.64 8.00 9.12 F1.12 5
+40	6.42 4.75 c1.67 29 rail	342.22 341.92 6.73 6.83 F0.13 2
2+0	5.14 2.94 c2.20 3	343.50 343.20 5.44 5.76 F0.32 4

348.64

	588	N	Z	E	595
+97.31	SL Linc 5.58 4.82 1	343.46 342.95	343.25	343.39 342.88	
+80	5.54 4.82 1	343.57 342.29	343.26	343.41 343.12	5.71 3.84 1.58 1.87 1
+60	5.43 4.82 1	343.53 342.40	343.14	343.29 342.76	5.67 4.08 1.59 1.46 1
+40	5.53 5.31 1	343.33 342.80	342.90	343.05 342.61	5.82 5.29 1.53 1.46 1
542.0	5.86 5.99 1	342.97	342.52	342.67	1.16 5.54 1.5 1
TP	5.53	348.83	10.5	343.29	
+80	2.25 2.00 1	342.09		341.79	2.55 2.20 1.35 1
+40	3.10 1.90 1	341.20		340.90	3.24 3.46 1.02 1
+40	4.02 4.37 1	340.32		340.02	4.33 4.32 0.10 1
+80	4.37 5.28 1	339.97		339.67	4.67 4.94 1.07 1
3460	4.54 5.17 1	339.80		339.50	4.84 5.48 1.64 1
		344.34			

INDEXED
WK
DEC 15 1948

Flankwise

1442.97

337.34

11.30
9.45
1.85
1

1457.22

336.90

11.24
9.24
2.00
1

+71.48

336.46

12.18
7.81
4.37
1

+35.74

336.02

12.62
8.39
4.23
1

040 - 7/5 Exist clear cut

335.58

13.06
5.39
7.67
1

348.64 T

Paving Grades Boundary St.
University Ave to Lincoln Ave

INDEXED
WK
DEC 15 1948

TP 6.35 343.32 1.95 336.97

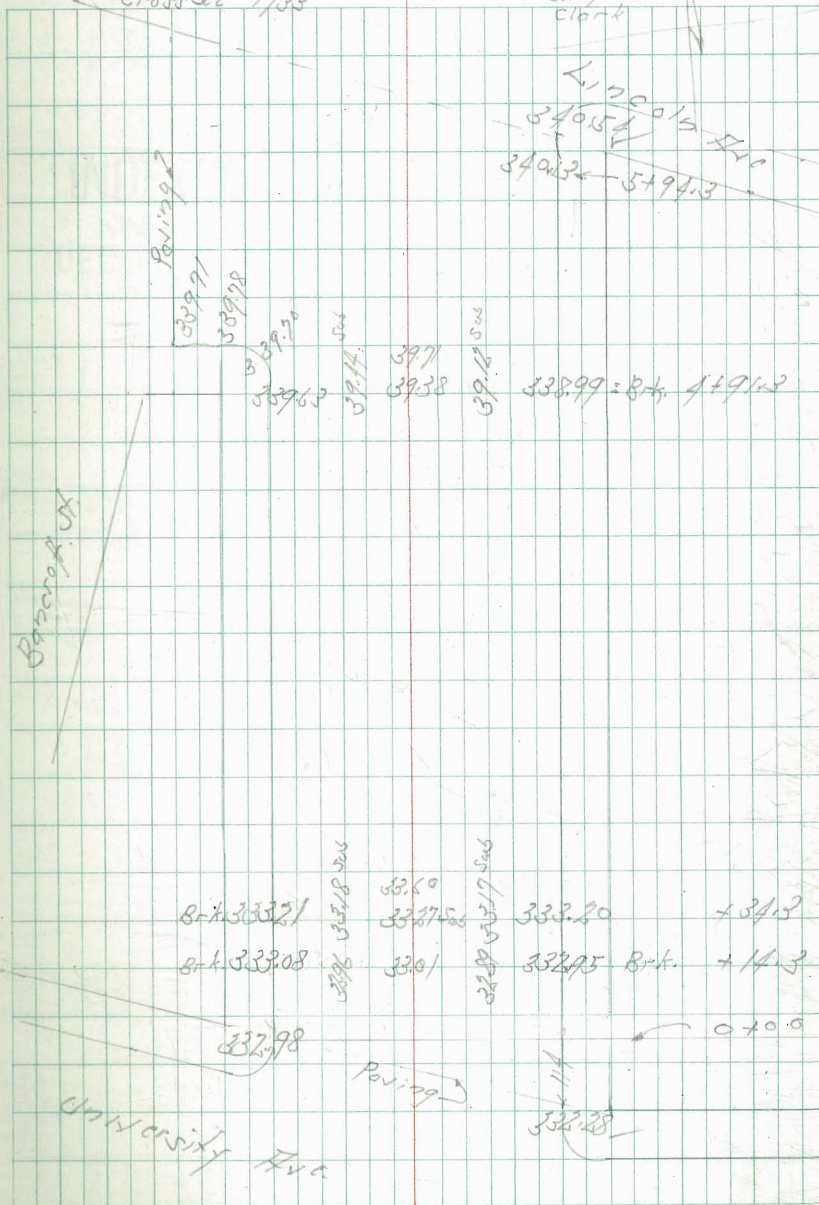
BM 5.98 338.92 333.44

N.W. B.P.
University
+ Boundary

Oct 27-48
Swooz
Smith
Becker
Borgas
Clark

X.O. 31206

Cross Sec #1733



B.M. 333.21 33.60 332.75 333.20 + 34.3
B.M. 333.08 33.01 332.88 332.95 B.M. + 14.3

332.98

0+00

University Ave

Grader Shuffboard Courts
Highland & Landis Community Center

See Sketch Page 2

BM 668 360.19 355.51 HMBP
Landis &
Highland

Court #1

H 355.73 4.47 Poured
4.46
4.47
F0.26 ✓

L 355.73 4.46
5.54
F0.58

S 355.73 4.46
5.55
F1.09

Court #2

H 355.71 4.48
4.49 Poured
4.47
F0.19 ✓

S 355.71 4.48
5.54
F1.06

Court #3

H 355.69 4.51 Poured
4.50
4.53
F0.03 ✓

S 355.69 4.50
5.48
F0.98

Court #4

H 355.67 4.52
4.53
F0.10 ✓

S 355.67 4.52
5.70
F1.18

Court #5

H 355.65 4.54
4.67
F0.13 ✓

S 355.65 4.54
5.72
F0.98

Restake
Nov. 23-48
Smith
Bocker
Barger

NO. 60283

Nov. 1, 48
Smith
Bocker
Clark

44

INDEXED
WIK
DEC 15 1948

Curb Grades N Side Diamond Betseyan
 Ingram & Jewell
 Lot 31-34 Block 145 Pacific Beach

B.M. 669 90.28 82.59 ^{L+T} Diamond
 E.L. Ingram

INDEXED
 WK
 DEC 15 1948

LOT 31-34 BLK. 145 ADD. Pacific Beach
 OWNER C. W. Spafford
 CONTR. Pacific Cement Co.
 PERMIT NO. 3462

Dec. 2-48
 J. S. Smith
 S. M. Barker
 S. M. Barker

45

Jewell 94.00
 FDL+T

NO. 21018

Lot 21
 stakes set 3' back
 of face of curb

250

10/19/33
 88.33 + 11 = 88.33

89.20 ^{1.00} ^{1.50} 88.52 ^{1.10}
 FO. 51
 88.46 ^{1.82} ^{1.77}
 CO. 68
 87.72 ^{2.51} ^{2.20}
 CO. 06
 86.98 ^{3.30} ^{2.97}
 61.13

Diamond

Lot 40

155

81.00/30 x 30 FDL+T

Ingram

Curb Grader Garrison St
 Willow St to Plum St

3+15.86 013.13 27' 13.4
 BM 1.97 85.68

3+01.68 S Ely Plum 17' 46.6
 17.96
 C 4.57

+87.68 8° 27'
 R 10 C 11.83
 R 36 C 10.58

+75 = C6 BC

+60 0 75.85

+375

+10 @ Rt 17.63 70.02
 12.05 87.65 0.25 75.60

2+0 = Bck on Lt

+62.5

+60 = 64.32

1+25 = Bk Lt = 809 New Curb

1+10 = 58.77

TP 12.7 75.95 0.27 63.34

+60 = Series Lateral @ 53.22

0+0 = Hwy Willow

BM 12.26 63.71

SE Top of Hyd.
 Plum x
 Garrison
 85.69 1756-48

INDEXED
 WK
DEC 15 1948

BM 51.45
 12.72
 64.22
 0.60
 63.62
 12.88
 76.50
 70.43
 76.07
 12.97
 89.04
 89 Ford

Six RP
 Willow x
 Garrison

Dec. 648
 S 15307
 Smith
 Garber

Y.P. 21323
 Cross Sec. #1756-89
 Lt C6 Grader
 Seal A6

85.85

84.66

83.29

74.33

65.68

#1 8901 7 Back of Curb Face
 #2 " " " " " " **46**

3.39 R C6 Grader
 1.26 120.00
 Fo. 86 85.85
 1.34 2.95
 2.95 84.70
 Fo. 11 7

5.20 3.90
 5.28 83.75
 Fo. 10 7

6.44 5.05
 6.75 53.7
 Fo. 29 7

10.81 9.47
 11.13 78.23
 Fo. 32 7

87.65

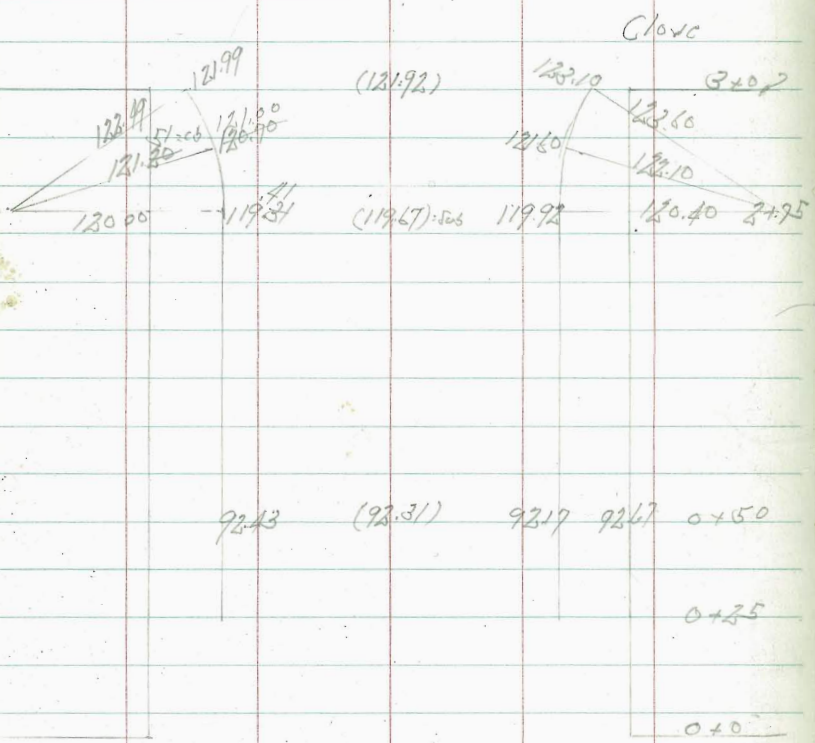
2.65 7.00
 3.11 84.3
 Fo. 46 7

89.04
 85.69
 85.69

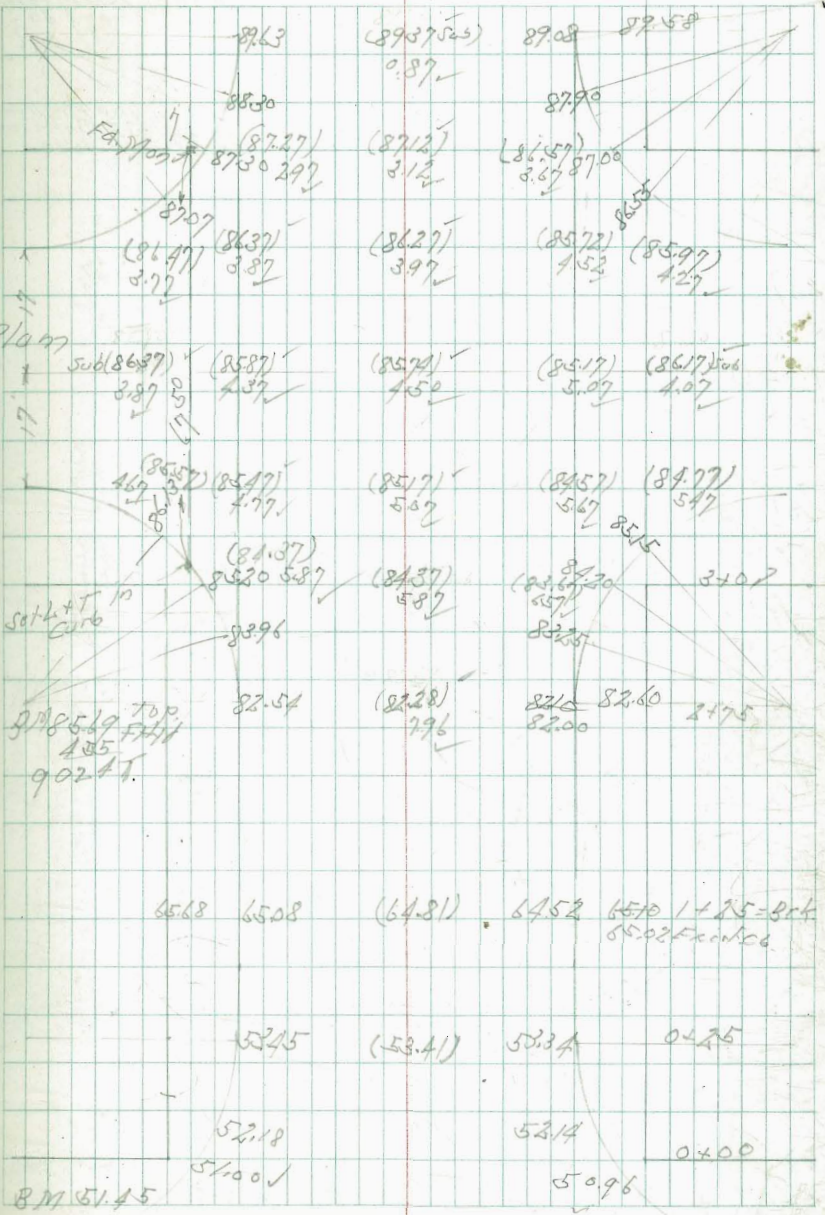
7.02 6.37
 6.89 8.01
 Co. 13 7

11.40 10.75
 11.49 10.70
 Fo. 109 Co 60.05
 7 Back Face of Curb

75.85



Plan



Willow

BM			3.99		125.42	NE BP Clove + Garrigton 128.90 1756-11
3 + 01.68 = EL Clove						
+ 8768						
TP	7.14	129.41		1.60	122.27	Top Fire Hrd SF Garrison + Clove
+ 75 = Cb BC						
+ 30						
2 + 10	(11)	107.35	1.52 1.87 0.55 2	(11)	107.41	16.44 9.25 170.2 2
TP	13.19	123.87		0.00	110.68	
+ 85						
+ 60						9.33 2.85 66.48 2
14 + 10				(11)	101.35	
1 + 10	(12) L	95.35	15.33 8.32 0.57 2	(12)	95.35	15.83 0.55 65.83 2
TP	12.66	110.68		0.72	98.02	
+ 95						
+ 60						9.35 3.37 65.98 2
0 + 50 = Brk					(10) 89.35	
0 + 25 = Cb F.C.						
0 + 12.32						
0 + 10 = (12) L		83.62	15.17 8.17 0.00 10.00 Co 7 C Block No 11		(11) 83.30	15.44 8.50 65.94 2 Back of
0 - 1.68						
0 - 15.86						
BM	22.05	98.74			85.69	SETop FH Plum + Garrigton

Souls						
						2.18 3.27 10.03
						123.30
						5.83 2.85 0.84
						3.68 3.27 129.10 Fo 09
						7.31 6.14 01.17 7
						5.38 5.22 00.10
						120.10
						5.27 2.04 2.18 7
						109.1 10.85 00.95
						114.87
						9.08 7.85 01.35
						5.14 5.27 Fo 13
						109.32
						1.06 0.81 07.05 7
						16.69 10.83 00.06
						103.77
						6.96 5.96 00.95 7
						110.68
						3.25 3.21 Fo 06
						98.22
						0.52 0.09 00.43 7
						8.80 7.00 Fo 20
						92.67
						6.07 2.13 Fo 06 7
						11.89 11.90 Fo 01
						89.58
						9.16 9.97 01.19 7
						0.64 0.41 00.23
						88.40
						10.32 9.16 07.18 7
						1.51 1.20 00.14
						87.50
						11.69 10.53 01.17 7
						1.99 2.05 Fo 06 3
						87.05
						98.78

89.44
6.14
88.93
12.54
10.47
0.29
10.18
16.28
14.46
11.46
17.67
12.11
125.78
3.54
122.24

Top FH +
F.C. Clove +
SF Garrison

Grades Storm Drain Lots 35 to 38
Block 7 Parker Add. South of Westminster St.
Between Louisiana St + Texas St.

5+ 42.84

INDEXED

WK
DEC 15 1948

258.70

9.97
4.25
c 5.47
10

5+ 17.34

259.21

9.41
4.30
c 4.71
10

4+ 90.84 Catch Basin
77c 10' South + 45c For Pipe

259.72

8.90
4.80
c 4.10
15

4+ 60.00

260.31

4+ 29.16

260.91

3+ 98.33 = Δ 5" Lt.
Existing Conc. Box

261.51

6.99 on Flow
L. 158

Dec 14 48

49

Stakes off set
10' South 60° of B.O. L. 49

Sirvo
Smith
Becker
Gardner

NO. 80133

B.M.

1114

268.62

257.48

Flow
L. 170
Existing Pipe
Cut

6+ 05.99 = Fly Conc. Pipe Cut

257.48

6+ 02.84 = FC.

out 257.57

Δ 20° 41' 30"

R 90'

5+ 86.59 = 1/2 Curve

T 16.43
L 32.50
E 1.49

257.88

10.74
4.00
c 6.65
10

5+ 70.34 = B.C. Lt.

258.19

10.43
4.50
c 5.90
10

INDEXED
WK
JUL 28 1949

Jan. 18. 49
Sisson
Smith
Garber

W.O. 90066

Location 7853

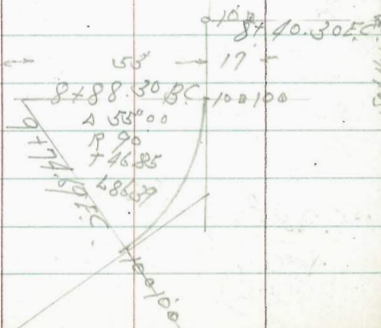
B.M. 19.81
3.23
23.27

Curblet #2

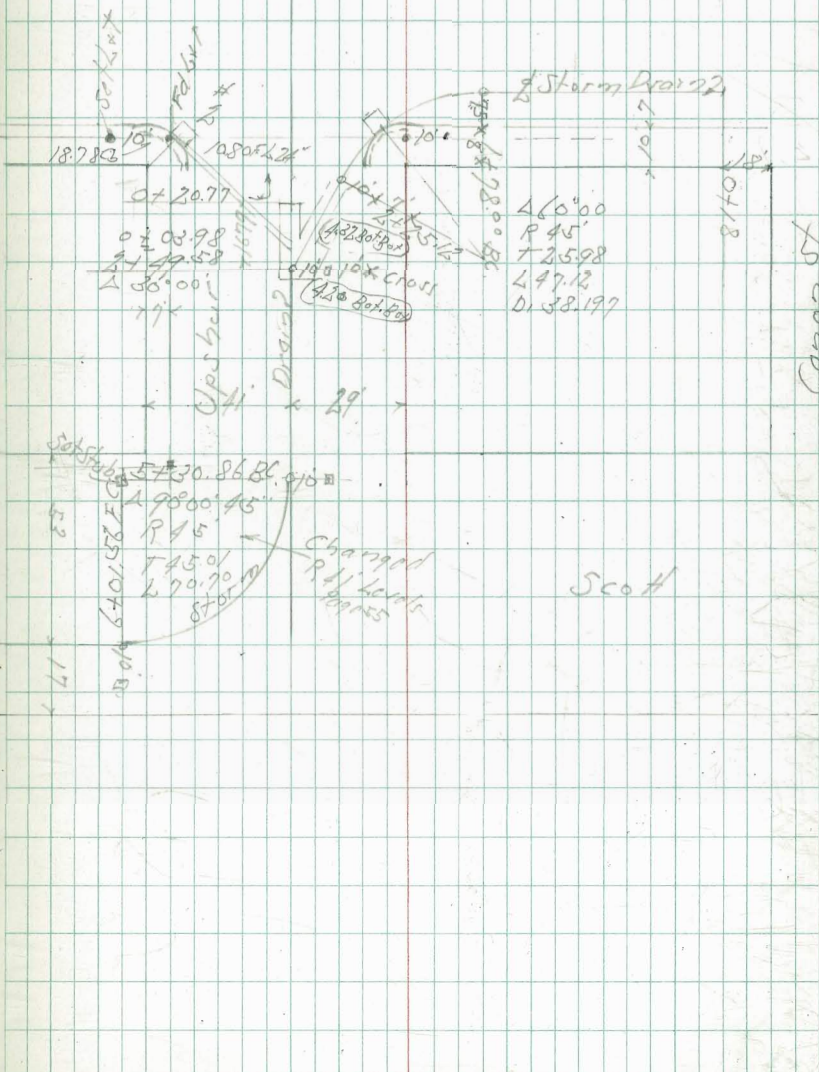
18.78
4.46
4.80 on ch
10.80
13.44
2.76
1.98
c 7.1

Set Box

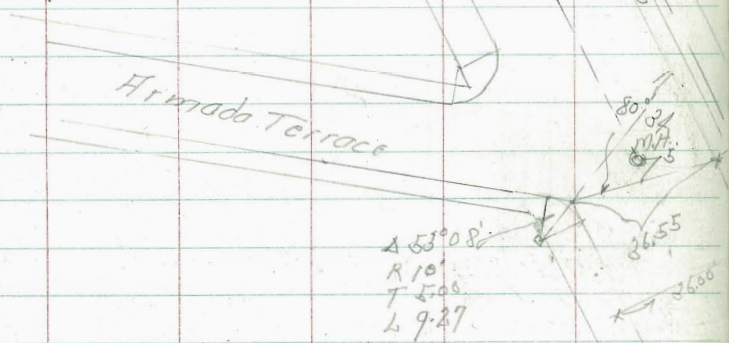
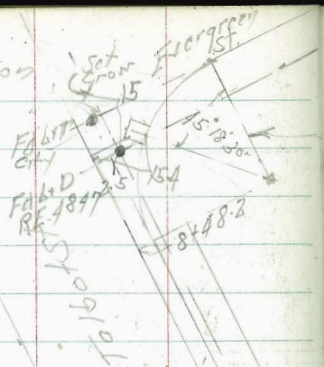
Fast End 420.80 19.04 5.01 5.03 c 13.03 5	W.F. d 432.80 18.95 12.87 c 12.51	Set Box 432.80 18.95 12.87 c 12.51	W.F. d 432.80 18.95 12.87 c 12.51	W.F. d 432.80 18.95 12.87 c 12.51	W.F. d 432.80 18.95 12.87 c 12.51
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Resection set



Alignment Canon St.
Storm Drain To Holst St. Connection



$\Delta 53^{\circ} 08'$
R 10'
T 5.00
 $\Delta 9^{\circ} 27'$

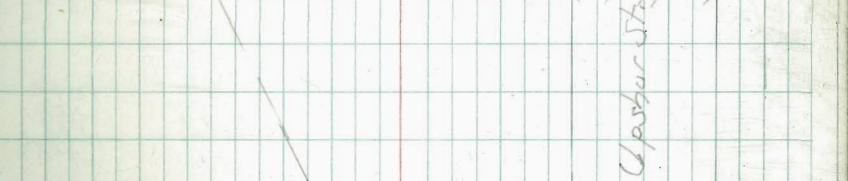
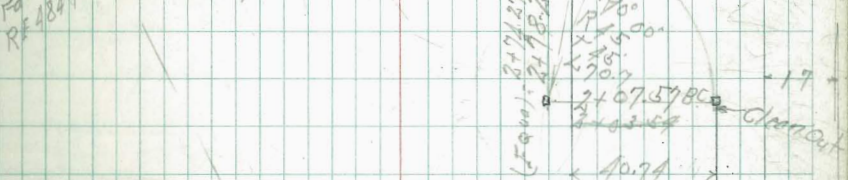
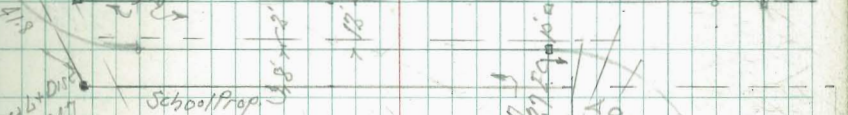
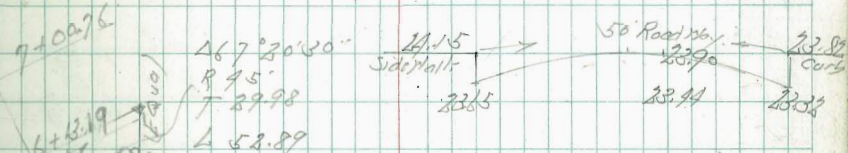
$\Delta 90^{\circ} 37'$
R 35'
T 35.88
L 55.35

BM 621 26.07

5' 1/2 Lvt
Persepolis
+ Curber

Top clean out

23.70
2.17
2.46
Eo. 29



Rosecrans St.

Grades Canon St. Storm Drain

Alignment Page 50

2+25.12 EC	30° 00'	5.01	18.10 4.39 13.71 10' pt on SW
C1580	10.06.6		
2+09.24	19° 53.4'	5.20	17.91 4.31 13.60 7' pt 7.5 SW
C1554	9° 56.9'		
+9562	7+7 9° 56.9'	5.39	17.72 4.30 13.42 7' pt on SW
C1554			
1+78	= BCLT	5.58	17.52 4.28 13.24 7.5 pt on SW
1+46		5.96	17.15 4.07 13.08 7.5 pt on SW
1+14		6.35	16.76 3.94 12.82 7.5 pt on SW
0+82		6.73	16.38 3.78 12.60 7.5 pt on SW
0+50		7.12	15.99 3.56 12.43 7.5 pt on SW
0+18		7.50	15.61 3.34 12.27 7.5 pt on SW

B.M.

19.81

S.M. 7.2 HT
R.J. 5.0
4P. 5.0

17.377

B.M.							
+10				2.50		14.87 3.30 11.57	
+75				2.79		14.80 2.26 12.54	
+50				3.07		14.30 2.08 12.22	
+25				3.36		14.01 1.88 12.13	
3+0				3.64		13.73 1.70 12.03	
TP	7.03	23.11	1.29	16.08		0.00 sub 10 ft 3.40	
+75				3.92		13.18 1.55 11.63	
+49.58 = 1030°				4.22		12.89 1.30 11.59	
2+41.13				4.52		12.39 1.02 11.37	
				4.82		11.87 0.75 11.12	

Canon St. Storm Drain

17.37x

+83.88	A 67° 36' 38"	0.40	16.92 4.55 c12.68
+66.21	A 45° 00' 22"	0.60	16.77 5.34 c11.73
+48.53	A 22° 30' 11"	0.80	16.57 5.01 c11.57
+34.86 B.C.R.41'			
+20.86 = B.C.R.45		1.01	16.36 4.84 c11.52
540		1.26	16.01 4.08 c11.73
+75		1.64	15.73 4.22 c11.37
+50		1.93	15.44 3.66 c11.78
+25		2.21	15.16 3.00 c11.76

+19.63 = B.C.H.									
BM 1	1.80	12.15							
" 2	7.22	17.37							
+50						18.89 2.16 c11.73	-1.52		13.89 2.80 c11.89 10.24
+25									18.40 2.11 c11.29
740									18.07 8.26 c11.35
+75									18.04 7.04 c10.97
+50									17.72 6.22 c11.29
+25									17.36 6.36 c11.75
+0.56 = F.C. 90° 00' 45"									17.19 5.33 c11.84

Canon St. Storm Drain

+53.10	20°32'5"	-3.84	$\frac{15.99}{7.21}$ c878
+31.50	13°45'	-3.59	$\frac{15.76}{8.95}$ c895
c 21.55			
9+09.90	6°52.5'	-3.34	$\frac{15.49}{5.70}$ c9.79
+88.30 = B.C.P.		-3.10	$\frac{15.25}{7.75}$ c10.5
+64.30		-2.82	$\frac{14.97}{3.86}$ c11.77
8+40.30 F.C.	A 89°59'	-2.55	$\frac{14.70}{3.65}$ c11.25
+22.69	A 67°29'15"	-2.35	$\frac{14.50}{2.89}$ c12.41
8+04.97	A 44°59'30"	-2.14	$\frac{14.37}{2.41}$ c11.88
7+87.30	A 22°29'45"	-1.94	$\frac{14.09}{2.59}$ c11.55

12.15

9.14 54

+42.69 = #4		-6.00	$\frac{9.14}{7.12}$ c2.00
+34.69 = #3		-5.91	$\frac{9.05}{2.00}$ c3.05
+26.69 = #2		-5.82	$\frac{8.96}{3.12}$ c3.87
+18.69 = Pier #1		-5.73	$\frac{8.88}{3.26}$ c3.88
14+0		-5.52	$\frac{8.66}{3.22}$ c5.72
TP	2.03 3.14 11.04	1.11	$\frac{17.39}{11.54}$ c6.84
+75		-5.23	
+50		-4.95	$\frac{17.10}{10.13}$ c6.97
+25		-4.66	$\frac{16.81}{7.50}$ c9.31
10+0		-4.37	$\frac{16.52}{7.29}$ c9.23
9+74.69 F.C.	27°30'	-4.08	$\frac{16.23}{8.22}$ c7.97

12.15

Canon St. Storm Drain Line Change

6+03.27 = 6+01.51 old

+99.27 = FC	90°	0.23	17.48 5.26 c11.82
+92.06 ✓	80°	0.31	17.41 1.20 c12.71
+84.91 ✓	70°	0.39	17.32 2.53 c12.7
+77.76 ✓	60°	0.47	17.21 6.36 c10.94
+70.61 ✓	50°	0.55	17.16 6.53 c11.07
+63.46 ✓	40°	0.64	17.07 5.58 c11.47
+56.31 ✓	30°	0.72	16.99 5.82 c11.67
+49.16 ✓	20°	0.80	16.91 5.56 c11.5
+42.01 ✓	10°	0.88	16.83 5.28 c11.55
5+34.86 BC 4/R		0.96	16.75 5.05 c11.70
BM 5.18	17.71	12.53	07 Feb 19 5+30.81 old BC

Gradat Canon St Storm Drain
Talbot St. Connection

March 19
Sissy?
Smith?
See for
80194

55

+23.58		17.69	17.08 0.87 c11.01
+14.42	100°	17.46	13.31 0.20 c12.71
9-7.855		17.22	13.55 0.22 c12.71
+07.57 = B.C.		17.16	13.61 0.25 c12.71
2+05.57 = 7 Clean out		15.68	15.09 0.56 c11.07
+75		14.47	16.30 0.53 c11.23
+50		13.86	17.51 1.06 c11.67
+25		12.05	18.72 11.08 c11.67
1+0 = B+C		10.47	20.30 11.97 c11.67
+70.57		9.25	21.43 11.81 9.81 70 ft
+55		7.30	
0+20.77	out	19.81	SM 9407 Reservoir 10 Apr 64
BM 10.96	30.77		

Grader Canal St. Storm Drain
Tail of St. Connection

4+0		22.72	8.05 18.7 c 6.97 10' RI
+75	20768	22.16	8.61 21.7 c 6.97
+50	814	21.61	9.71 21.8 c 6.97
+25		20.85	9.92 22.6 c 6.97
3+0	7573	20.10	10.67 20.7 c 6.97
+74.87 +78.27	-FC.	19.32	11.45 21.6 c 6.97
+70.41		19.09	11.68 21.8 c 6.97
+62.55		18.86	11.96 22.1 c 6.97
+54.70	727	18.63	12.14 22.3 c 6.97
+46.84		18.40	12.37 22.5 c 6.97
+38.99		18.16	12.61 22.8 c 6.97
2+31.13		17.92	12.85 23.1 c 6.97 10' RI

3077

+ 11.19 - 2 Clean out		27.35	11.71 4.78 c 6.97 10' RI
6+ 07.43		27.26	11.80 4.80 c 6.97 10' RI
+ 99.575		27.09	11.87 4.82 c 6.97
+ 94.72		26.92	11.94 4.84 c 6.97
+ 82.865	50.80	26.74	12.02 4.86 c 6.97
+ 76.01		26.57	12.09 4.88 c 6.97
+ 68.155		26.39	12.17 4.90 c 6.97
+ 60.30 + 57.64 - B.C. RA		26.22	12.24 4.92 c 6.97
+ 25		25.50	12.31 4.94 c 6.97
5+0		24.94	12.38 4.96 c 6.97
+ 25		24.38	12.45 4.98 c 6.97
TP 792	20769	30.54	12.52 5.00 c 6.97
+ 50		23.89	12.59 5.02 c 6.97
4+25		23.27	12.66 5.04 c 6.97 10' RI

3077

Grades	Canon St	Storm Drain	Talbot St	Connection
83.5 + 8.2 = End			40.88 40.66	9.45 0.45 c 8.96
75.5 + 7.0 = 1/2 of C.O. "3" out			40.34	9.95 out
+ 5.0			38.64	11.65 2.33 9.30 on Paving
+ 2.5			36.98	13.31 3.31 c 10.00 5.7996
84.0			35.32	14.95 2.85 c 10.12
+ 7.5			33.66	16.63 2.43 c 10.20
+ 5.0 = Bk			32.00	18.29 2.26 c 10.03
72.5 34.31			30.82	19.47 2.51 c 9.97
71.0076 = 1/2 Std. Lug			29.67	20.62 1.10 c 9.58
13.26				
+ 87.50 = Bk			29.04	21.25 11.82 c 9.43
TP • 12.94	50.29	1.11	27.35	9.97
+ 62.73			28.49	9.66 c 8.84
+ 37.96			27.95	10.51 3.12 c 7.39
+ 34.77				
(+ 13.19 = FC			27.40	11.06 2.76 6.30 5.7996

38.46

Curb Inlet #1		Talbot St	At-grade	Test
	50.29			
Top Curb		40.11	10.18	10.18
Bottom Box		31.85	18.41	10.49 c 8.25
TP	5.51	55.35	6.45	49.84
Curb Inlet #2				
Top Curb		50.00	5.35	5.35 5.01 c 5.01
Bottom Box		44.00	11.25	5.01 c 6.21
B.M.	3.34	52.01	N.W.B.P. Emergency + Talbot 51.99	

Water Main Grade Alley Block 8
 Mountain View. From Landis to High Street
 between Chamoune & 6th St.

+40			342.60	$\frac{13.2}{2.3}$ c59
	INDEXED			
	W.K.			
	JUL 28 1949			
TP	8.64	355.76	1.27	347.12
2.400				341.78 $\frac{1.6}{2.0}$ c4.6
+60			341.16	$\frac{7.2}{3.3}$ c4.6
1720	=P.V.C.		340.75	$\frac{7.6}{5.6}$ c4.0
780			340.45	$\frac{7.9}{3.6}$ c4.3
+40			340.15	$\frac{8.7}{3.8}$ c4.4
0700	=H.L. Landis		339.85	$\frac{8.5}{1.1}$ c4.4
B.M.	7.39	348.39	341.00	$\frac{11.0}{1.0}$ c4.0

Cross Sec. 1815. 34
 Stakes off 1/4"
 East of Ditch No. 31459

Jan. 21-49

58

+86.94	=5 L. High Street			
Tap Curb East		9.24	346.52	
+46			345.61	$\frac{10.1}{5.6}$ c4.8
5406	=P.V.C.		346.71	$\frac{9.0}{5.0}$ c4.0
+60	=E.V.C.		346.88	$\frac{8.9}{2.5}$ c4.0
4120			346.82	$\frac{8.9}{4.2}$ c4.2
+80			346.31	$\frac{8.5}{6.7}$ c4.4
+40	=P.V.C.		345.38	$\frac{10.4}{5.9}$ c5.1
3410			344.51	$\frac{11.3}{6.2}$ c5.2
3480	=E.V.C.		343.65	$\frac{12.1}{7.1}$ c5.0

355.76

Sewer Grades Venice St. Newport Rd to Miller
South of Niagara Area

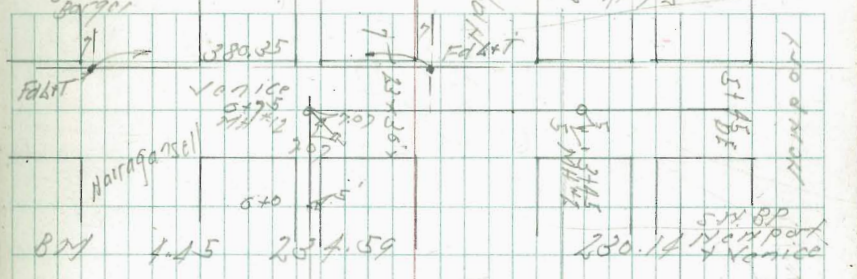
Jan. 24-49
S. 509
S. 510
S. 511
S. 512
S. 513

No. 80139
36528
Stakes of set
of 2 Bites 59

3+0		22229		213.45	9.54 3.25 C6.09
B.M.			5.59	217.90	5.87 Niagara Venice 27.72
+55				211.56	11.73 5.98 C5.75
2+10				209.67	13.62 2.30 C5.72
+65				207.78	15.51 10.85 C4.66
TP	363	213.89	13.03	210.26	
1+20				205.89	8.00 4.03 C3.97
+75	MH #1 = 190° of Venice			204.00	9.89 5.98
				203.71	4.11 10.19 5.78 C4.48
+39.5				202.34	10.55 6.68 C3.87
0+0 = Exist Sewer				202.96	16.93 6.37 C4.66

INDEXED
W.K.
JUL 28 1949

				380.35	
B.M.	1.45			204.59	2.07 2.07 2.07
+15 D.E.				224.94	9.65 8.54 C6.77
5+05				223.02	11.57 1.99 C6.58
+65				221.10	13.42 6.89 C6.53
4+25				219.18	15.46 9.08 C6.73
+85				217.26	17.33 10.82 C6.76
3+95 = MH #2				215.34	19.45 12.85 C6.70
TP	1.55	22329	12.85	221.74	



Grader Curb Inlets + Culverts

Contour Blvd. + 52nd St

Sketch Page 62

+77.4

INDEXED

N.K.
JUL 28 1949

Flow line

374.92

0.09
2.60
c 6.42

+46

1.5' 5" of 12" Contour
Clear cut 1.09

Curb Top
382.87

377.91
378.80

6.03
2.92
c 3.54 North
c 2.65 South

+27

279.08
Top of water main

383.94

379.22

8.09
5.22
c 2.87

TP

2.51

5.58

381.43

379.36
378.92
7.11
c 2.43

1+20.5

+95

1/2 Curb Inlet
3.59
3.04
c 0.05
10

Curb Top
383.42

379.92

7.09
4.22
c 2.87
7.11

+77

cb BC

380.10

6.91
4.00
c 2.91
7 South

+50

380.37

6.66
4.65
c 4.97
7 South

+25

380.62

6.39
4.92
c 1.47
7.50

0+0

1/4 of 12" Contour

380.87

6.14
4.92
c 1.22
7 South

BM Jet

3.42

384.59

SE RP
Contour v 52nd
c 7.22
6.7 South

BM

1.27

387.01

385.74

6+77.45
1601-25

Feb 1-49

5.5.30

5 miles

Section

Burgor

60

Stake offset 7' South
Also 7' West of 2 Curb

150.81200

3+22.5

RP 7' 1/2 x 7 1/2

Top of Wall
362.80

360.30

7.18
10.61

+97.5

362.90

4.58
5.42
F 0.87

TP

1.89

367.48

12.78

365.59

TP

3.78

378.37

9.25

374.59

+71.5 - End Contour

365.50

18.44
14.98
c 3.46

+40.2

368.64

1.25
2.25
c 5.95

2+18.8

371.78

12.16
6.87
c 5.29
7.11

383.94

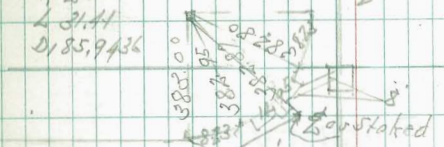
Contour Blvd. Sewer Lateral

140936	End = Lot 31 & 32	381.76	7.31 7.31 F 2.00 5.11
+84		381.59	7.48 8.17 F 0.69 5.11
+56		381.39	7.98 8.25 F 1.51 5.11
+28		381.20	7.87 8.81 F 1.66 5.11
#6	0+0 = Exist BM	380.94	8.13 FL 8.07 5.44 F 3.63 5.11
BM	4.48	389.07	384.59
	#3		383.96
BM	6.66	391.25	384.59
Lateral #2			386.55
Sewer Lateral #1			385.86
BM	4.16		392.08

INDEXED
W.K.
AUG 11949

B.M. 384.59 S.F.P.P. Contour #52nd
2.82
387.92

			382.81	382.84	382.91
			3.25 1.88 F 1.13	5.70 5.25 F 1.33	3.64 3.64 F 1.53
			382.88	382.87	382.90
			1.64 5.78 F 1.12	4.59 8.06 F 1.44	1.56 8.05 F 1.49
			383.43	383.42	383.44
			1.03 4.03 3.00	1.98 3.98 C 0.96 1.0	1.03 4.24 F 0.22 1.0
					385.23
					384.21
					387.79
					389.07



Sewer Lat #1

Sewer Lateral #5

TP

Dawson Ave Grader El Cajon Blvd to
Castour Blvd

Markers East Carb.

391.38

+28.20

385.65

386.41

+85.05

2/11/49

385.44

386.23

INDEXED

WK

AUG 1 1949

+17.55

385.25

386.07

+10.05

2/11/49

385.05

385.92

+65.02

384.83

385.73

+20 = 0.4

384.60

385.55

+10.4

2/11/49

384.60

0 + 0

N.L. El Cajon
2/11/49

5.66 385.72 385.65

7.41 383.97 384.10

18.17

60.11 383.88

63

5.1
5.5
CO 1
5' off

5.9
4.2
C13
5' off

6.1
5.1
CO 9
5' off

6.3
5.1
C13
5' off

6.5
6.3
CO 4
5' off

6.8
7.4
FO 5
5' off

5.0
3.0
CO 2
5' off

5.3
2.5
CO 22
5' off

5.3
1.2
CO 9
1' off

5.5
1.2
CA 3
1' off

5.7
1.7
CA 2
1' off

5.8
1.7
CA 1
1' off

CB. NEPL. El Cajon & Dawson

CB. NW PL. El Cajon "

SW PL 538 El Cajon

	WestCurb	EastCurb
0.27	391.28	391.11 from P. 65.
+9.505	SL Morning 387°0	387°50
+87°05	CBBC 386.96	387.47
+4391	386.74	387.29
4400.77	386.52	387.12
+57.63	386.31	386.94
3714.99	386.09	386.76
271.34	385.87	386.58

44
35
C10 /
5' off.

44
42
C04 /
5' off.

49
45
C05 /
5' off.

55
48
C03 /
5' off.

53
50
C02 /
5' off.

55
50
C05 /
5' off.

39
12
C22 /
5' off.

45
12
C23 /
5' off.

43
28
C15 /
5' off.

44
32
C12 /
5' off.

46
32
C14 /
5' off.

48
32
C16 /
5' off.

		West Carb		East Carb
BM7	6.03	390.62		384.59
+20 - BCht		387.96		
T.P.	5.63	394.90	1.25	389.27
+80		388.20		
+40		388.40		
+1316	BC out			389.00
+10	PVC	388.40		388.88
+55		388.00		388.49
+10	Prop F.C. out			388.10
+08	Cb E.C. W	387.57		
0+0	ALL W. Area	387.50		
TP			3.79	391.11

SCBP 52nd E Contour

2Z
13
C1A
5' off.

67 Rod
56
C11
5' off

65 Rod
54
C11
5' off

59
52
C11
5'

65
57
C08
5' off.

60
55
C11
5' off

69
62
C07
5' off.

64
57
C13
5' off

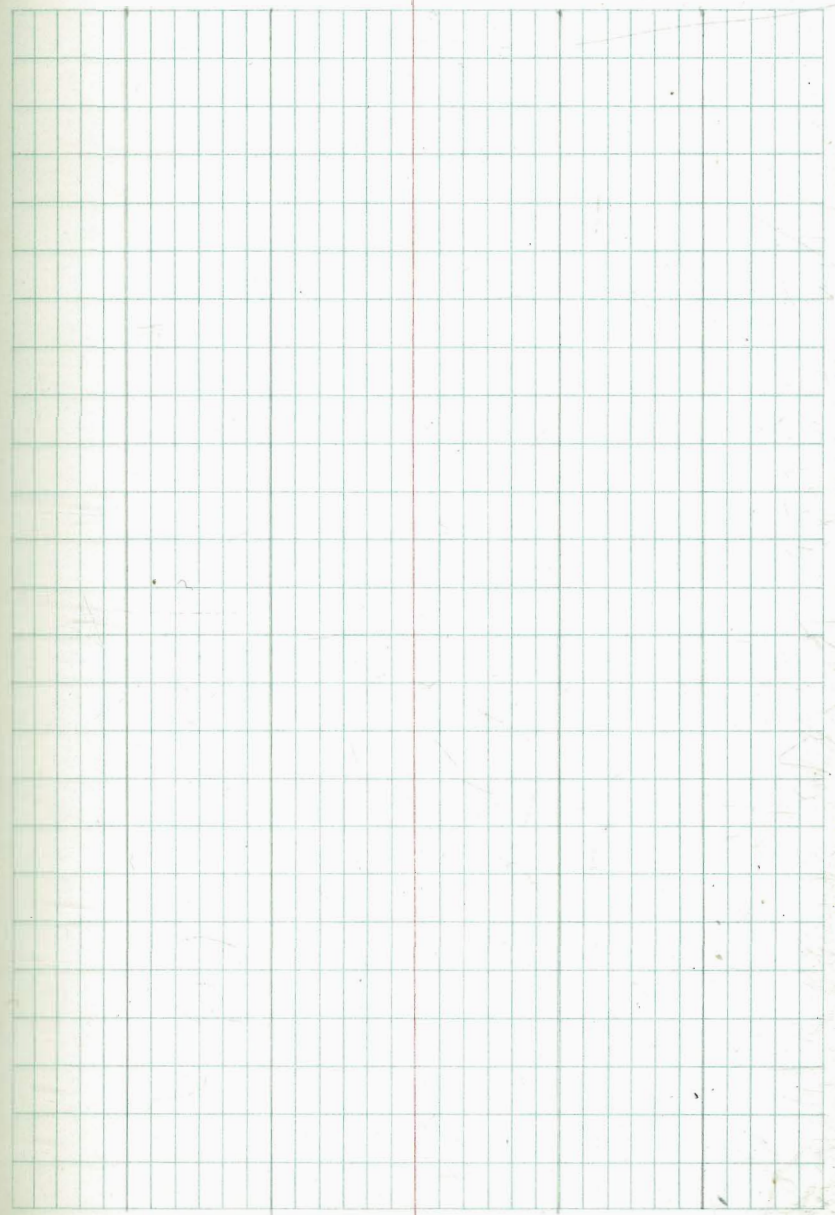
68
56
C12
5' off

73
60
C13
5' off.

SE Top F Hydt.

Contour Blvd. Grader

	West Curb	East Curb
+96.48		388.09
+50.92	CB C. 02X	388.57
1+07.41	389.57	389.03
	20	
+63.91	390.03	389.49
+20.41	CB EC. 02X	389.95
0+0	Prop RI out	
0-23.20	CB EC. RT	390.41
0-31.20	N. L. Monroe 07 East	390.50



Contour Blvd.	West Carb	East Carb
+69.01	385.58	387.83
5+52.86	385.99	385.10
5-86.15		
+9.71 - B.C.H.	386.30	385.38
4+47.02	386.60	385.79
+97.33	386.90	386.19
3+47.64	387.20	386.60
+97.95 E.C. 00M	387.50	387.00
+57.52 - F.L. Davis 07 East		387.44
2+42.04		387.60

Contour Blvd.

West Curb

East Curb

+75.33 CBFC

383.54

383.00

7+67.33 = 14.58nd

383.50

382.95

+

7+07.33 = FL 5th 0.21

0

383.80

+99.33 = CBBC 0.21

383.85

6+77.45 EC

384.50

384.00

+41.31

384.86

384.28

6+05.16

385.22

384.53

Contour Blvd

10+72.66	23° 31'	FC. 07E	386.77	386.00
31.85		25.94 07E		
+40.81	17° 54'			385.70
35.73		29.14 07E		
10+05.08	11° 36'			385.10
32.90				
+72.18	5° 48'			384.60
38.90		26.82 07E		
9+37.28		BC. 07E	384.60	384.10
+99.28			384.20	383.70
+81.28			384.10	383.60
+45.27			383.92	383.40
8+10.46			383.73	383.20

INDEXED

W.K.

AUG 1 1949

	West Curb		East Curb	
TP 537	393.32	3.30	387.95	(2)
+85.44	387.93		387.48	
	$\frac{5.5}{5}$		$\frac{5.6}{5}$	
(D) +74	$\frac{5.5}{5}$		$\frac{5.6}{5}$	387.43
				$\frac{3.82}{5}$
+142.1	387.79		387.30	387.78
	$\frac{5.5}{5}$		$\frac{5.7}{5}$	
(D) +70	$\frac{5.5}{5}$		$\frac{5.7}{5}$	387.28
TP 550	393.40	3.78	387.90	$\frac{3.97}{5}$
2+03.04	387.65		387.11	$\frac{3.88}{5}$
	$\frac{4.8}{5}$		$\frac{4.8}{5}$	
(D) +84	$\frac{4.8}{5}$		$\frac{4.8}{5}$	387.09
				$\frac{4.22}{5}$
+61.84	387.51		386.93	$\frac{4.15}{5}$
	$\frac{4.2}{5}$		$\frac{4.2}{5}$	
(D) +76	$\frac{4.2}{5}$		$\frac{4.2}{5}$	386.85
				$\frac{4.10}{5}$
+20.64 = Bk	387.87		386.74	$\frac{4.89}{5}$
	$\frac{4.3}{5}$		$\frac{4.2}{5}$	
(D) 0+99	$\frac{4.3}{5}$		$\frac{4.2}{5}$	386.61
				$\frac{4.66}{5}$
+80.42	387.17		386.49	$\frac{4.65}{5}$
	$\frac{4.5}{5}$		$\frac{4.5}{5}$	
(D) +52	$\frac{4.5}{5}$		$\frac{4.5}{5}$	386.32
				$\frac{4.22}{5}$
+40.21	386.97		386.25	$\frac{4.20}{5}$
	$\frac{4.7}{5}$		$\frac{4.9}{5}$	$\frac{0.03}{5}$
3-103	$\frac{4.6}{5}$		$\frac{4.9}{5}$	780.46
				$\frac{0.03}{5}$
0+0 = 10+72.66 E.C.	386.77		386.00	$\frac{5.7}{5}$
	$\frac{4.9}{5}$		$\frac{4.9}{5}$	$\frac{0.8}{5}$
0-123	386.70			
	$\frac{5.8}{5}$			
BM 7.09	391.68		384.39	J.F.P.P.
(D) BM 6.66	391.25		384.59	Contour

	West Curb	460	East Curb	388.80	388.80
B.M.					388.80
+32.15	B.C. 0774	388.98			388.83
		1.4			
		3.3			
		01.3			
		on Rod.			
+12.04	B.C. 02 F	out	388.76		
			4.6 out		
4+0		388.89	388.71		
		1.5	4.7		
		3.4	4.5		
		01.4	0.5		
		5		388.60	
M +71				4.72	
				4.81	
				00.41	
+50		388.74	388.52		
		4.2	4.8		
		3.2	00.5		
		01.3			
		5		388.39	
M +17				4.93	
				4.78	
				00.75	
5+0		388.58	388.32		
		1.8	5.6		
		3.7	4.9		
		01.1	00.3		
		5	03 Nail	388.78	
⊕ +87				5.04	
				4.82	
				00.32	
+50		388.44	388.14		
		5.0	5.3		
		3.5	5.9		
		01.4	00.5		
		5		388.10	
M +40				5.22	
				5.13	
				00.10	
4+0		388.29	387.95		
		5.2	5.4		
		3.8	5.6		
		01.7	00.5		
		5		387.91	
⊕ +93				5.10	
				5.32	
				00.08	
+50		388.14	387.76		
		3.5	5.6		
		4.3	5.8		
		00.9	00.5		
⊕ +33				387.69	
				5.63	
				5.61	
				00.02	
3+26.64 = Bck		388.07	387.67		
		5.3	5.7		
		5.4	5.6		
		00.1	00.5		
		5.12 street			
		39340			

Monroe H. Co. Grades 52nd St. to Contour Blvd.

H.C.C.

S.C.C.

+70 - H.L. Davis 387.50

387.00

+68 - C.B.C. 387.43

386.94

+63 387.09

386.66

INDEXED

N. K.

AUG 1 1949

+84 386.76

386.37

+45 - F.L.H. Hoy 386.43

386.08

+25 - H.L.H. Hoy 386.26

385.93

+86 385.93

385.64

+47 385.60

385.35

39

+08 - C.B.C. 385.27

385.06

0+0 = Fairline 52nd St. 385.20

385.00

Empty grid on the right page of the notebook.

Monroe H.C. Gradar
South Carb Line Stationing
N.C.B.

Sa.Cb

73

243.38 = E.L. Carbon 390.50

+82.38 = Cb EC So. 390.90

+71.51 = Cb BC So. 391.00

+50 390.70

+35 = ~~71~~ 390.51

1+10 390.20

+90.44 = Cb BC N. 389.90 389.75

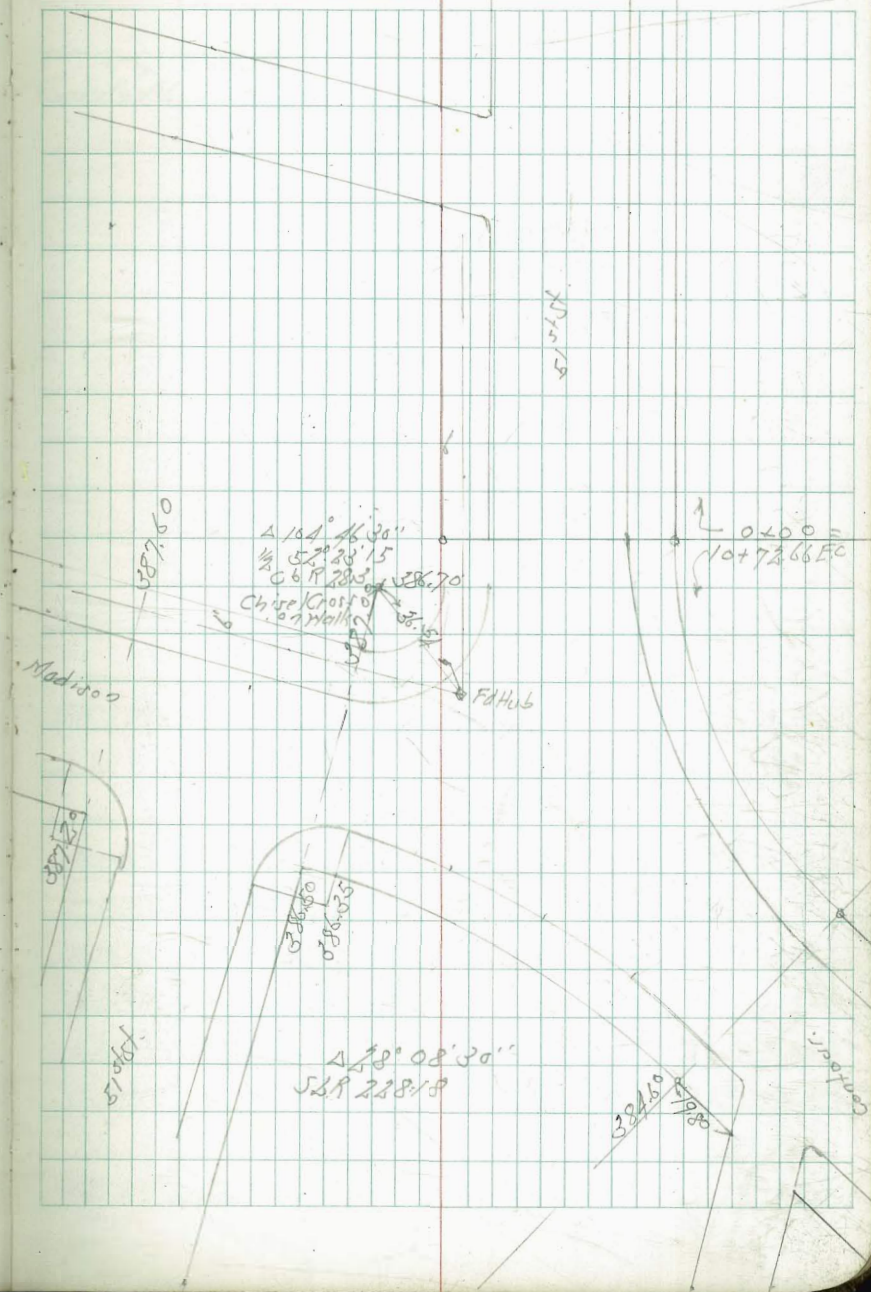
+63.62 389.48 389.14

+36.81 389.06 388.53

+10 = Cb EC N. 388.65 387.92

+08 = Cb EC So. out 387.88

0+0 = F.L. Damm 388.40 387.70



4-5-49 State Rough Grades Contour Blvd.
 Hendrick
 Greer
 Korol
 Woz

INDEXED
 W.K.
 AUG 1 1949

- Lt CB EL. EL Stake Lt Cor F Lt

- Rt. CB EL. EL Stake Rt. Cor F Rt.

CK - 2.40 386.75 386.77

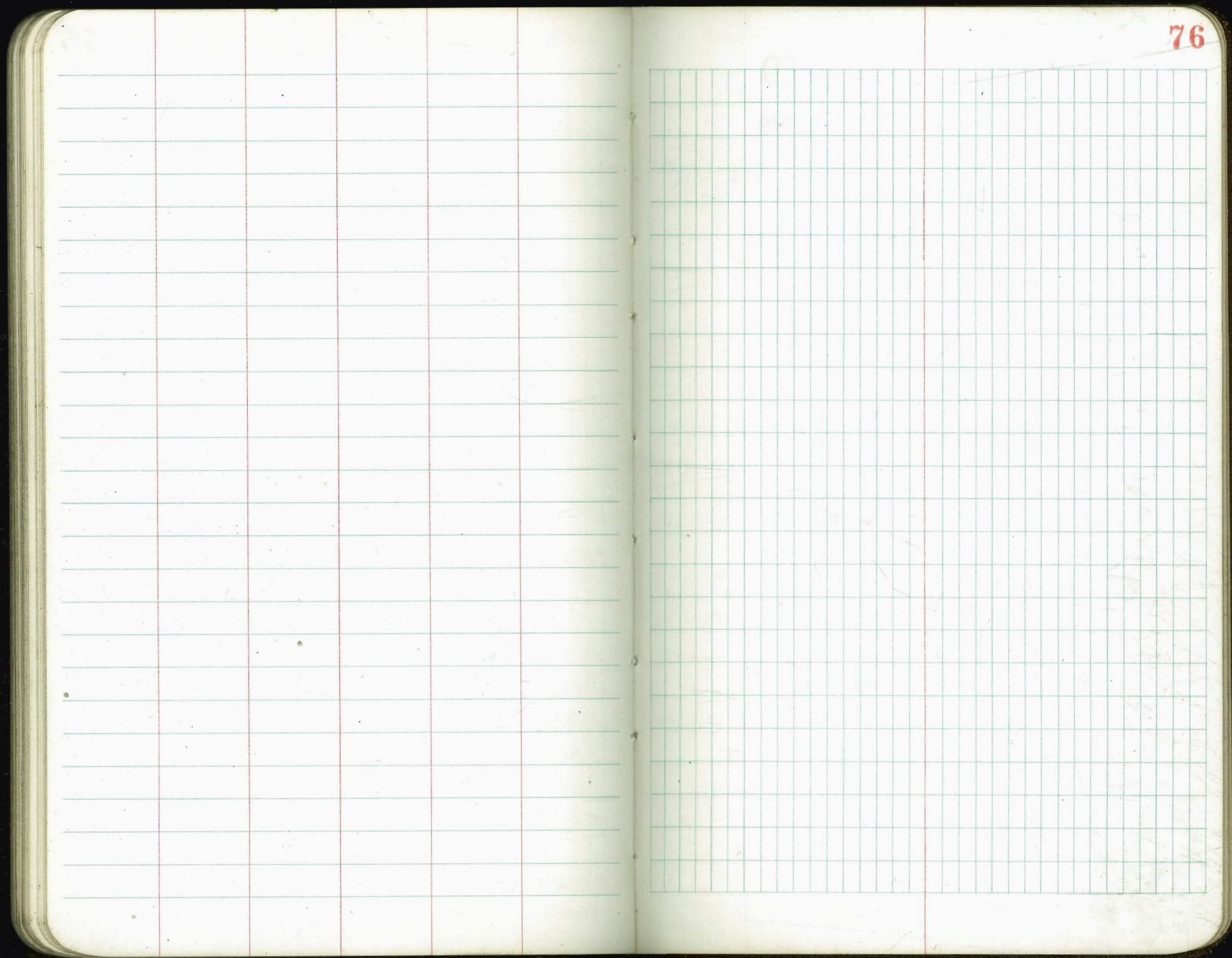
CK BC 0:00 on East 51st St.

7+75.06 CB EL Lt. 7.3 383.00 381.9
 8+10.46 7.1 383.20 382.1
 8+45.87 6.4 383.40 382.8
 8+81.28 5.0 383.60 384.2
 8+99.28 5.0 383.70 384.2
 9+39.28 BC 5.0 384.10 384.2

F1¹ 6.5 383.52 382.7 F0⁸
 F1¹ 7.0 383.72 382.2 F1⁵
 F0⁶ 7.0 383.91 382.2 F1²
 C0⁶ 6.3 384.10 382.9 F1²
 C0⁵ 6.3 384.20 382.9 F1³
 C0¹ 3.9 384.60 385.3 C0⁷

B17 4.56 389.15 384.59

389.15
 3KBP Contour @ 52nd



Paving Grades J St.
30th St to Bancroft

INDEXED

N.K.

AUG 1 1949

31st St

4-25-49	76.50	75.80 4.63	75.37 5.66	76.00	7+99
Paving Station	77.01	75.64 4.72	75.37 3.93	76.00	7+50
	782.51				
	79.51	74.17	73.48	73.48	4+0
BM 77.01	77.01	73.78	73.09	73.09	3+15
BM 76.72	76.72	72.50	72.66	72.66	2+20
77.01	77.01	73.41	73.00	73.00	2+0
80.28	76.65	73.55	72.70	72.70	1+80
		75.95	74.30	74.30	0+20
77.00	76.26		74.58	75.00	0+02

30th St

BM

77.01 SWR
JST 430

Parent Item (75.32) = Sub Grade

Feb 2-49
Sims
Sucker
Barger

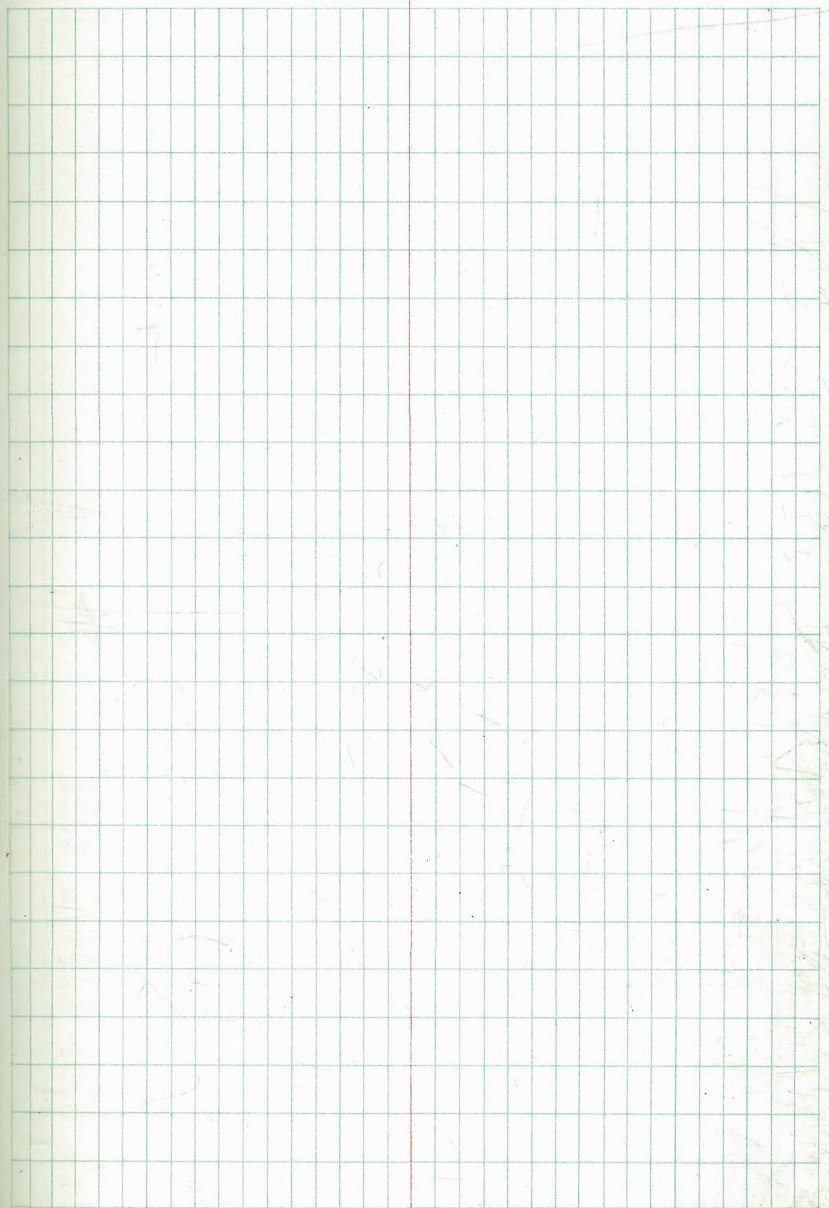
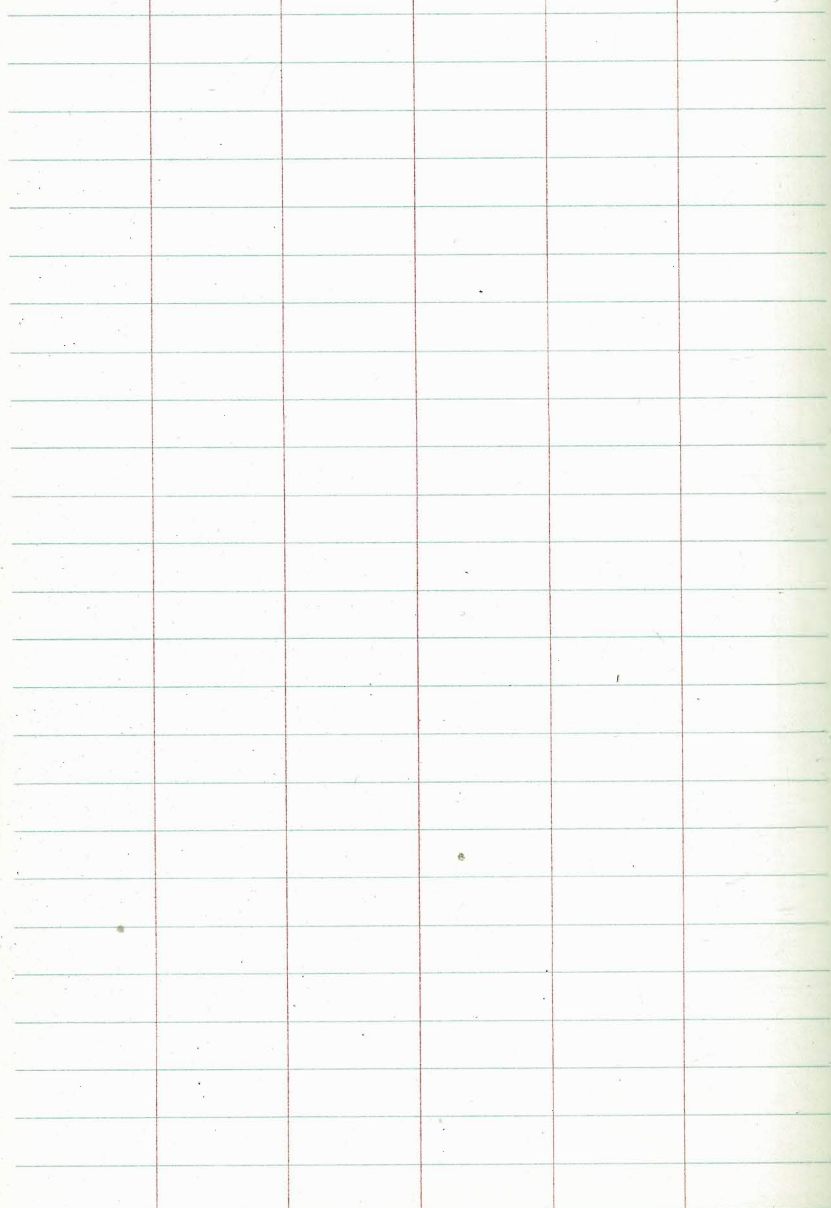
77

N.O. 31209

32nd St

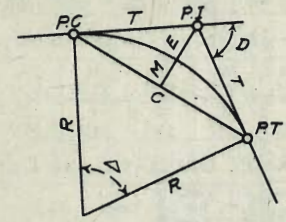
81.00	80.35			80.39	81.50	6+00.8
81.19	80.19			80.62	2.92	5+80.8
79.00	78.33			77.83	78.50	3+0
76.65	76.83			76.23	7.27	0+50
77.00	76.50			76.09	76.50	0+02

31st St



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $\div 8\frac{1}{8}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.=Sta. P.I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.=Sta. P. C.+ $L=164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve=.3 $\times 54.5 \times 8\frac{1}{8}=136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2=6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20'=960.6 \div 8\frac{1}{8}=115.27$ and from Table V correction=.10 or $E=115.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42=5.5$ or $D=5^\circ 30'$.

53
26.5

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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