

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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MICROFILMED

APR 13 1965

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Sewer laterals BIK 8 Roseville Hqts.	} 51
" BIK 44 Ocean Beach + on Pasadena Dr.	
Alley BIK 21 Teralta (Resub. Lots K+L)	52
Storm drain 43 rd - So. of Market	54
Sewer Ext. Lantana Dr. N.Y. of Dwight	} 55
Water Ser. Thomas Everts - Dawes	
Sewer Lat 4 Water Ser. Boxes BIK. 56 City Hqts	} 62-64
Sewer Lat. BIK. 56 City Hqts	
Martin St. 30 th to 31 st	65
Alley BIK. 56. City Hqts - Grades	66-
Silver St. + BIK. 10 La Jolla Park Sewer Lat - - - Grades	68
Alleys BIK. 108-111 + 116 Mission Beach Santa Barbara Place " "	67 72
Estakes Alley BIK. 7 City Hqts.	73
Sewer Alley BIK 7A Pt. Loma Hqts.	74
" prospect + Jenner - - -	75

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	N.	S.		
	Rough grade	Curbs.	Rough C.	
T.P.	7.87	88.28	2.47	80.41
1+72	<u>77.66</u> 5.22 <u>3.96</u> C 1.26	INDEXED WK MAY 16 1949	<u>76.66</u> 6.22 <u>5.71</u> C 0.51	
1+28	<u>76.69</u> 6.19 <u>4.23</u> C 1.96	74.87 6.03 80.70x S.O.D.	<u>75.69</u> 7.19 <u>7.14</u> C 0.05	
0+84	<u>75.72</u> 7.16 <u>5.08</u> C 2.08		<u>74.72</u> 8.16 <u>8.21</u> F 0.05	
Brk. 0+40	<u>74.75</u> 8.13 <u>6.22</u> C 1.91	<u>74.75</u> 5.15	<u>73.75</u> 7.10v 9.13 <u>8.47</u> C 0.64	N. water 1p top Hydt.
Ch. E.C. 0+06	<u>73.87</u> 7.01 <u>7.02</u> C 1.99	<u>73.87</u> 6.03 <u>5.43</u> C 0.60	<u>73.06</u> 7.84v 9.82 <u>9.89</u> F 0.07	<u>74.87</u> 5.03 <u>79.90</u> 0.30 <u>79.60</u> 7.84 <u>7.84</u> 89.44 X
0+00 = E.L. Cass.	<u>73.72</u> 9.16 <u>9.15</u> C 0.01	<u>73.72</u> 6.18	<u>72.94</u> 9.74 <u>9.95</u> C 0.01	B.M. E.L. S.E. (copy) + 0.01
T.P. T.H.F. Cass + Law S.W.B.P.	8.01 8.85	82.88 75.25	0.38 — 66.40	74.87

	Rough Ct.	Curbs stakes	Rough Ct.	①
4+60	<u>89.28</u> 83.05 5.23 2.85 <u>C 2.38</u>		<u>82.05</u> 6.23 <u>6.43</u> F 0.20	
4+20	<u>82.36</u> 5.72 <u>3.99</u> C 1.95		<u>81.36</u> 6.92 <u>6.78</u> C 0.14	
3+80	<u>81.67</u> 6.61 <u>4.86</u> C 1.75		<u>80.67</u> 7.61 <u>7.30</u> C 0.31	
3+40	<u>80.78</u> 7.30 <u>5.24</u> C 2.06		<u>79.78</u> 8.30 <u>8.25</u> C 0.05	
3+00	<u>80.29</u> 7.99 <u>6.59</u> C 1.40		<u>79.29</u> 8.99 <u>8.85</u> C 0.14	X 80.90
Brk 2+60	T.P. 0.30 <u>79.60</u> 8.68 <u>7.67</u> C 1.01	79.60	<u>78.60</u> 2.30v <u>7.29</u> C 0.37	78.60 7.68 7.29 C 0.37
2+16	<u>78.63</u> 9.65 <u>8.51</u> C 1.14		<u>77.63</u> 10.65 <u>9.95</u> C 0.70	
		88.28		

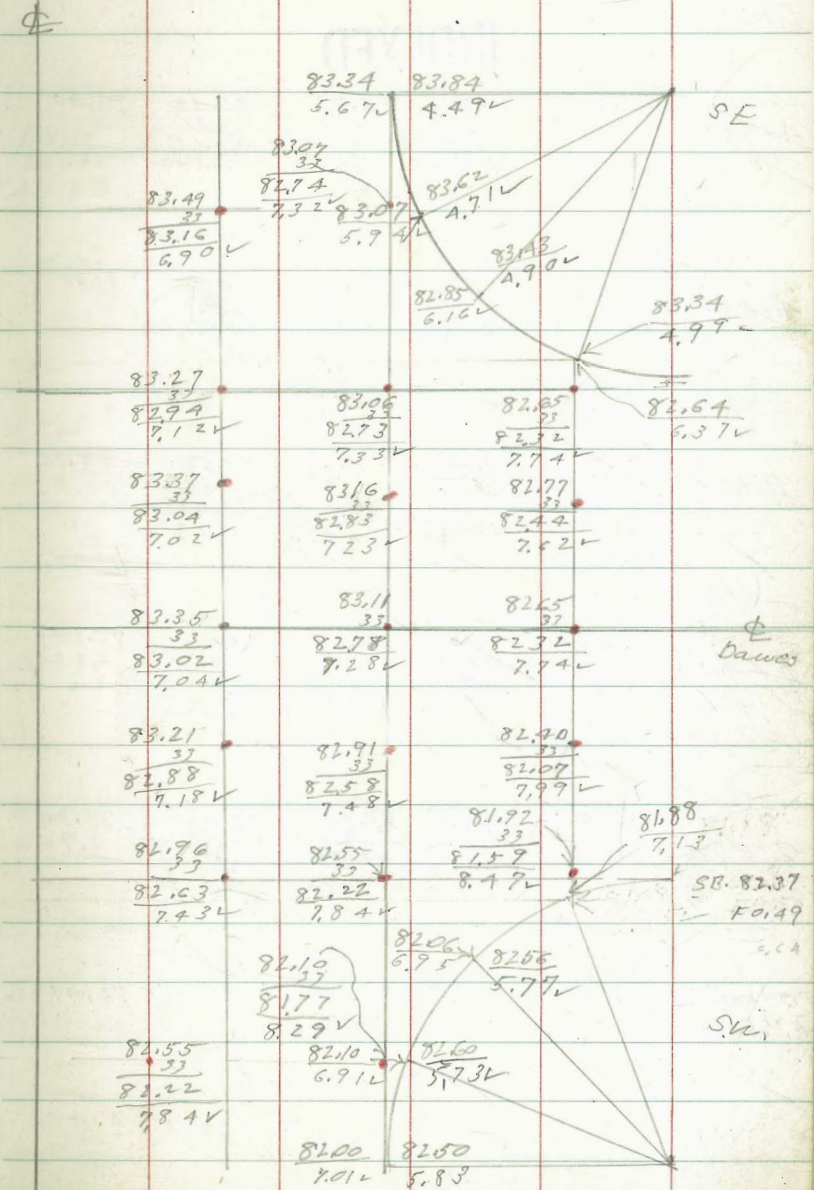
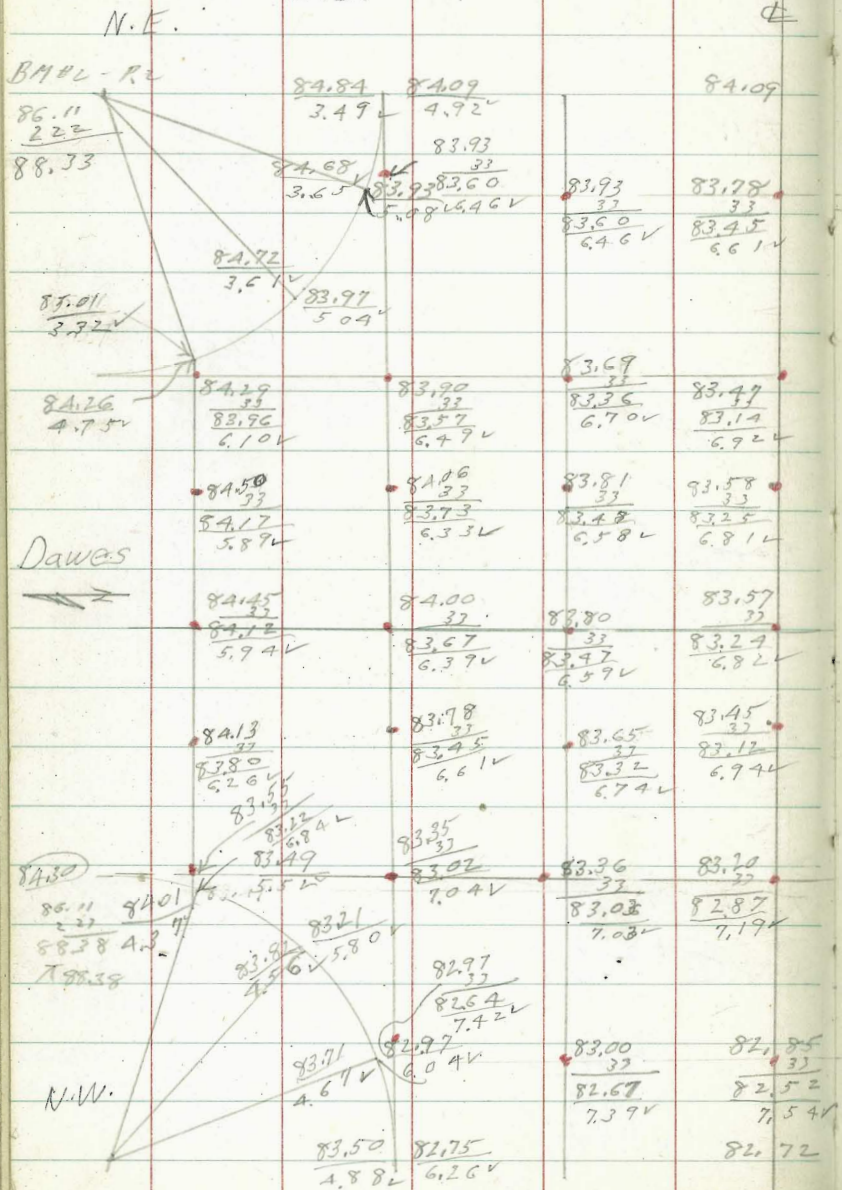
	Rough Grade	Curb stakes	Rough grade		A+13.4 Exist Pav, +curbs	96.04 3.65 3.05	Curb stakes 96.04 95.04	95.04 1.65 2.67 1.00	(2) Rough grade
		Water Meters			B-k, 3+73.4	94.83 4.86 3.51 C1.35		93.83 5.86 4.96 C0.90	
0+90	87.06 8.63 6.22 C2.41		86.06 9.63 9.75 F0.10						
0+50	85.95 9.74 7.35 C2.39		84.95 10.74 11.29 F0.65						
		889.44						4' in st 92.61 3.08 0.94 C2.14	
Ch.E.C. 0+10	84.84 70.85 7.81 C3.04	84.84 4.60	83.84 11.85 12.42 F0.57	83.84				4' in st 91.61 4.08 3.06 C1.02	
E.L.Daves 0+00	84.68 17.01 7.84 C3.17		83.62 12.07 12.62 F0.46					4' in st 91.50 4.19 2.12 C2.07	
T.P.	12.53	95.69	5.12	83.16				90.39 5.30 3.02 C2.28	89.39 6.30 4.57 C1.73
W.L.Daves A+98 ²	83.71 4.57 2.66 C2.31		82.60 5.68 5.78 F0.10					89.28 6.41 4.25 C2.16	88.28 7.41 6.23 C1.18
N.W. Radix & Daves		889.44							
U.B.C. A+98 ²	83.50 4.78 2.30 C2.48	83.50 5.94 5.49 C0.50	82.50 5.78 3.80 F0.02	82.50				88.17 7.52 5.65 C1.87	87.17 8.52 7.64 C0.88
		88.28							
							95.69		

INDEFYEN

Beryl St At Dawes.

86.11
290
89.01x

86.11 Sub.
395 Orals (3)
7006 T



Pavement Grades Beryl.

	N. Gutt.	N. 1/4	E	S 1/4	S. E. 1/4
W.L Dawas	82.97	83.00	82.85	82.55	82.19
INDEXED					
Ch. B.C. 4+88 ³	82.75	82.85 <u>33</u> 82.52 5.97 ^v	82.72 <u>33</u> 82.39 6.10 ^v	82.48 <u>33</u> 82.15 6.34 ^v	82.00
4+68 ³	82.11	82.52 <u>33</u> 82.19 6.30 ^v	82.43 <u>33</u> 82.10 6.34 ^v	82.15 <u>33</u> 81.82 6.57 ^v	81.66
← π = 88.49 →					
2+60	78.86 <u>10.15^v</u>	78.95 <u>33</u> 78.63 2.94 ^v 1.16	78.87 <u>33</u> 78.54 2.93 ^v	78.58 <u>33</u> 78.25 3.22 ^v	78.10 <u>10.91</u>
?	X 89.01			X 89.01	
0+40	74.00 <u>5.49^v</u>	74.15 <u>33</u> 73.82 7.65 ^v	74.02 <u>33</u> 73.69 7.77 ^v	73.78 <u>33</u> 73.45 8.02 ^v	73.26 <u>6.23^v</u>
0+06	73.26 <u>6.23^v</u>	73.25 <u>33</u> 72.92 8.55 ^v	73.13 <u>33</u> 72.80 7.67 ^v	72.89 <u>33</u> 72.56 8.71 ^v	72.54 <u>6.95^v</u>
0+00 E.L. Cass	73.13		72.98	72.41	
		X 81.47		81.47X 24.87 46 ^v 77.99 ^v	

	N. Gutt.	N. 1/4	E	S. 1/4	S. Gutt.
					96.04 2.20 98.24X
Exist Paved A+13 ⁴	95.37	95.37	95.45	94.98	94.47
3+73 ⁴	94.18 <u>4.06</u>	94.29 <u>3.95</u> 2.2 4.28	94.20 <u>4.04</u> 3.2 4.17	93.91 <u>4.33</u> 3.2 1.66	93.43 <u>4.81</u>
0+30	84.65 <u>5.41^v</u>	84.76 <u>33</u> 84.43 5.63	84.67 <u>33</u> 84.34 5.72	84.37 <u>33</u> 84.04 6.02	83.88 <u>6.18^v</u>
Ch. E.C. 0+10	84.09 <u>5.97^v</u>	84.19 <u>33</u> 83.86 6.20 ^v	84.09 <u>33</u> 83.76 6.30 ^v	83.81 <u>33</u> 83.48 6.58 ^v	83.34
0+00 E.L. Dawos.	83.93	83.72	83.78	83.49	83.07
					86.11 3.95 90.06X

BERYL Sidewalk Grades
 El. = curb side of walk grades

Cl. Ord. N. Walk S. Cl. Ord.

W.L. Daves
 4798²

83.82

82.71

INDEXED

86.11
 167
 87.74

BM. #2 L

B.C.
 4788²

83.50
 4.68v

83.61
 4.13v

82.61
 4.99

82.50
 5.68v

86.11
 209
 88.10x

2+60

81.99
 79.60
 2.39v

79.71
 1.96v

78.71
 8.89

78.60

4713⁴

96.04

96.15

95.15

95.04

BM. #2 PL

1.49

87.60

x-87.60

86.11

0+40

74.75
 7.24v

74.86
 6.21v

73.86
 4.25v

73.75

cl.
 0+10 E.C

84.84

84.95
 9.13

83.75
 3.65v

83.84

0+06

73.87
 8.12v

73.98
 7.09v

73.17
 4.94v

73.06

BM. #2 PL
 86.11
 5.97
 92.08x

x-87.60

E.L. Cass

73.72
 7.35v

72.94

0+00
 E.L. Daves

0+00

for
 cl.

7.12

81.99

74.87

for
 walk

6.20

81.07 = x N. walk

74.97

x for
 N. walk

BM. #1

3.24

79.11 = x S. walk

74.87

S. walk

Page 1

Sub. grade Beryl. 5/17/28

E. line Cassara	0+06	0+40	2+60	4+68.3	92.87 6.03 780.90
	73.13 33 72.80	74.92 33 73.69	78.87 33 78.54	82.43 33 82.10	
	8.10V	7.21V	2.36V	5.20V	

	4+88.3	4+98.3	W.L. Dawes		86.11 +1.19 87.30
	82.72 33 82.39	82.85 33 82.52			
	4.71V	4.78V			

E.L. Cass	0+30		76.32X		86.11
20+00	84.67		3+73.4		10.21
0+00	33		94.20		96.32X
83.78 33	84.34		93.87		
83.45 3.85V	2.96V		2.45		

	N. Line	cb.	☉	cb.	S. Line
E. Gutter Dawes	84.29	83.90	83.97	83.06	82.65

Dawes ☉	84.15	84.00	83.57	83.11	82.65
------------	-------	-------	-------	-------	-------

Dawes W. gutter	83.55	83.35	83.20	82.55	81.92
--------------------	-------	-------	-------	-------	-------

Sewer Lats. BIKs 48, +65, 0, B.

Between Santa Cruz + Coronado.
Bacon to Sunset Cliffs Blvd.

5/26/48

W/O

733.00

INDEXED

WK
MAY 16 1949

#1	#2	#7	#6	#5
25.25	24.42	24.92	24.00	22.76
7.81	8.64	8.64	9.06	10.30
3.22	4.57	3.79	4.63	5.43
C 4.59	C 4.07	C 4.85	C 4.43	C 4.87

33.27X

#3 #4

22.25	21.99
11.02	11.28
5.83	5.00
C 5.19	C 6.28

#8 45.00 #9 45.00

#10 #11

30.09	31.04	33.24	37.80
14.97	14.02	11.82	7.26
10.70	7.28	7.55	2.83
C 4.27	C 4.74	C 4.27	C 4.43

Sammermeier
McCoy
W Moore
Sherman

X 33.00 N.W. Bacon
Santa Cruz

28.89	12.80
X 41.69	11.61
JR 30.08	2.98
X 33.06	5.50
27.52	5.75
X 33.27	0.52
32.75	12.31
X 45.06	11.75
33.21	3.45
36.76	8.17
28.53	4.10
32.63	4.10
28.52	

S.E. BA
Coronado
Cable. 2489

Bayside Walk

W.O

60135

7

at Balboa Ct.

7/9/48 sidewalk stakes

□ = set stake 2' west of prop. line

= 2' west of west edge walk

+75' EXIST
walk

0.32 ✓ walk is 15' on
private prop.
at this point.

EXIST

0+65E

0.30
4.164 EXIST

0+57.8

0.24
4.702

0+38

0.18
4.762

719

0.09
4.185

0+00 =

0.00
4.942 EXIST

0.00
4.94
4.94X

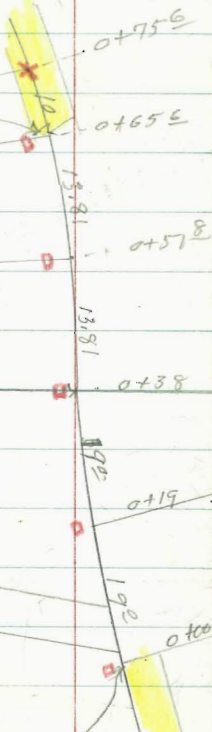
INDEXED

WK
MAY 16 1949

P.R.C.

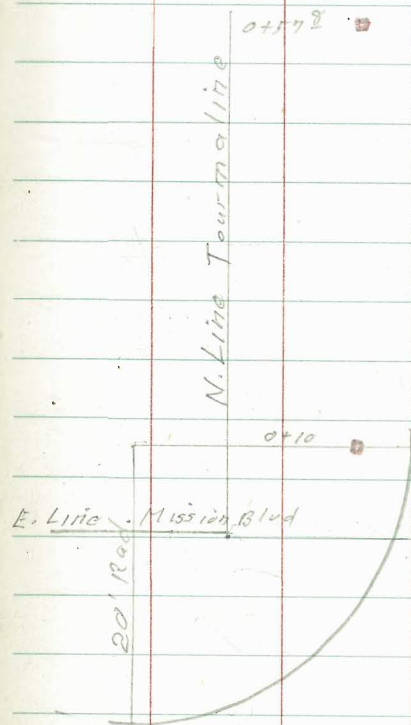
Balboa Ct.

assumed
El. = 0.00





See B-27 page 34



Keating + Lynnwood.

Summer 1948
9-2-48
Curb stakes on prop line
lots 1+2 Blk 40 Middletown Map. 1121

INDEXED
W K
MAY 16 1949

0+00	+09	+18.	+50	1+00
131.12	132.140	133.0	133.37	133.95
3.54	2.34	1.74	1.37	0.79
7.89	8.30	9.08	10.11	11.22
F4.35	F5.96	F7.24	F8.74	F10.43

T.P. 0.89 134.74 12.86 133.85
Spike pole # P1753
N.W. Keating + Lynnwood, 6.49 140.22 BM #2

T.P. 0.08 146.71 12.83 146.63

T.P. 0.44 159.46 13.05 159.02
S.E. cb End.
Pringle + Lynnwood, 4.08 167.99
Lynnwood + Pringle SS 7.75 164.32 BM #1
S.W. 13' L+T.

T.P. 1.32 172.07 13.02 170.75

T.P. 0.03 183.77 13.02 183.74
Pringle +
Only, 0.30 196.76 196.46 13' L+T.

SEE ALSO PAGE 28

9

check

Book

134.74

0.92

133.82

12.74

146.56

0.01

146.55

13.05

159.60

0.06

159.54

12.79

172.33

1.09

171.24

12.79

184.03

2.08

187.94

13.05

196.99

0.52

196.47 orig B.M.

0.01

1+82 • 134.19

Keating

1+00 • 133.95

0+50 • 133.37

0+18 • 133.0

0+09 • 132.4

0+00 • 131.2

LINWOOD

Par. San Rafael Pl.

	N	W	S	
Sommermeier		W.O. 31156		
McCoy		4-29-48		
W. Moore				
Sherman	□ 2' out.	-1.26	-1.56	□ 2' out.
0+80		4.77	4.77	
		4.85	4.85	
		Co.09	Co.29	
0+60	X in Conc. 2' out.	-1.00	-1.30	X on Bricks 2' out
		4.51	4.51	
		4.81	4.81	
		Co.30	Co.03	
0+40	□ 2' out.	-0.74	-1.04	X in Conc 2' out.
		4.25	4.25	
		4.34	4.10	
		Co.09	Co.15	
0+20	X in Conc. 0.8 out.	-0.48	-0.78	□ 2' out.
		3.99	3.99	
		3.93	3.65	
		Co.06	Co.34	
0+10	□ 0.80 Bad	-0.35	-0.57	□ 2' out.
		3.86	3.86	
		3.86	3.58	
		Co.12	Co.28	
0+00		-0.21	-0.22	
		3.72	3.73	
		3.72	3.72	
		Co.12	Co.14	
E. 32nd St. M. Blvd.				
+ San Rafael	3.79	3.51	8.07	-0.28
B. M. Seawall	0.66	7.99		7.13
at San Rafael				

INDEXED

WK
MAY 16 1949

	North	West	South	
2+09 ⁵⁰	X on walk on line	-0.70	-0.70	
W. Line		4.58	4.58	
Bayside		4.28	4.25	
Walk.		Co.30	Co.33	
2+00	□ 2' out.	-0.80	-1.10	□ 2' out
		4.68	4.68	Also Nail in
		4.81	4.81	Fence = C122
		Co.13	Co.31	
1+80	□ 2' out.	-1.00	-1.30	□ 2' out.
		4.88	4.88	Also Nail in
		4.61	4.95	Fence = C
		Co.27	Co.07	
1+60	□ 2' out.	-1.20	-1.50	□ 2' out
		5.08	5.08	Also Nail in
		4.65	5.04	Fence = C122
		Co.43	Co.04	
TIP	4.67	3.88	4.30	-0.79
1+40	X in walk 1' out	-1.40	-1.70	□ 2' out
		4.91	4.91	Also Nail in
		4.45	4.80	Fence =
		Co.46	Co.11	C 100
1+28 ⁵⁰		-1.68	-1.86	
E. L. Bay-		5.19	5.37	
side Lane				
1+12.50		-1.67	-1.88	
W. L. Bay side		5.18	5.26	
Lane				
1+00	□ 2' out	-1.52	-1.82	□ 2' out
		5.03	5.03	
		4.70	4.70	
		Co.13	Co.13	
		3.51		

Stake sewer BIK 166 La Playa

6-2-48
W.D. 80087

Rogers &
Rosecrans

Gammertmeyer
McCoy
W Moore
Sherman

L Sheet # 7198

B.M. N.E., B.P. Perry
+ Rosecrans E.L. 64.15

B.M. #1	4.70	49.78	—	45.08	49.78 16
1839					49.62
A					12.93
					62.57

Exit D.E. 0400	0+25	0+50	0+75	1+01.6	Δ 84° 14' 30"
				out lot, inlet	Rt.
36.88	37.85	38.83	39.80	40.84	41.20
12.90	71.93	10.95	9.98	8.94	8.58
7.02	5.60	4.50	3.00	3.29	3.29
05.88	06.33	06.45	06.52	05.65	5.29
				out	10.20
					19.6

62.45X	74.31X	M.H.#	2 Δ 67° 5'	2 Δ 67° 5'	62.45X
1124.8	1155.2	out	in lot	out	62.21
50.03	58.86	1481.89	1481.89	1481.89	62.21
12.42	15.45	6.61	6.61	6.61	12.07
9.44	8.29	2.01	2.01	2.01	74.51X
C 7.98	C 7.16	C 4.54			0.07
					74.24
					11.95
					86.17
					0.12
					86.06 TP

86.19X	95.49X	Δ 67° 53'	Rt.	M.H.#	1 N lot	Both ways
2+10	2+38.1	2+66.2	2+94.4	2+94.4	2+94.39	10420' 24"
72.27	76.85	81.42	86.00	86.00	86.140	70° 40' Back
13.92	9.34	14.06	9.48	9.08	9.08	Tang.
7.74	1.88	6.80	6.73	6.73	6.73	
C 6.18	C 7.46	C 7.26	C 2.75	2.35	2.35	86.06 TR
			out	IN	IN	7.43
						95.48X

INDEXED
WK
MAY 16 1949

Δ 6° 12' RT.
B.K.

TR 3000
93.87

3+19.39	3+44.39	3+69.39	3+94.39
92.37	98.35	104.32	110.30
13.46	7.48	13.71	7.73
10.40	3.51	6.95	1.71
C 3.00	C 3.97	C 6.76	C 6.42

11.96
105.83 X
44
105.39
12.64
118.03 X
17

4+19.39	4+44.39	4+69.39	End
117.95	125.60	133.25	
11.21	3.56	5.85	
7.60	0.52	1.17	
C 3.61	C 3.04	C 4.68	

117.86
11.30
129.16 X
0.47
128.69
10.41
139.10

M.H.#37	0400	Going south.
86.40	0+94	0+24
	82.25	0+44
	90.53	0+71.50
	91.86	92.30
	7.80	7.30
	12.41	9.13
	9.65	4.99
	02.76	04.74
		C 6.15
		C 7.44
		C 6.77

93.87
5.77
99.66

0+99	1+26.5	D.E. 1+54
92.86	93.36	93.84
6.80	6.30	5.82
5.50	8.93	8.48
C 1.30	F 2.63	F 2.66
C 3.80	F 0.13	F 0.16

Curb Stakes Jarvis & Scott

Lots 4-546 Blk 92 Roseville

A lso Lots 1-2-48

6-11-48

Sommermeier

W.D. 21018

McCoy

W Moore

S-15' Line Jarvis }
W.L. - 25' Scott }

L+T.

4.46 0.91 B.M. #1

S.W. L+Dist } 3.91 5.37 8.40 1.46

INCELOW

Rosecrans

6.52 9.86 - 3.34

INDEXED
WK
MAY 16 1949

272	224	176	B.C. 128	A 114	B 100
2.65v	2.13v	3.61v	4.09v	4.23v	4.37v

C 1.00	D 1.05	EC 1.80	120	130
4.37v	4.32v	4.27v	4.17v	4.07v

B.M. #1 A 125

0.91	4.82	4.00	3.57	3.27
0.86	2.75	3.77	4.20	4.50
7.77				

Fig for. stake line on 36' Rad

36'
Rad: Ch. Dets Δ

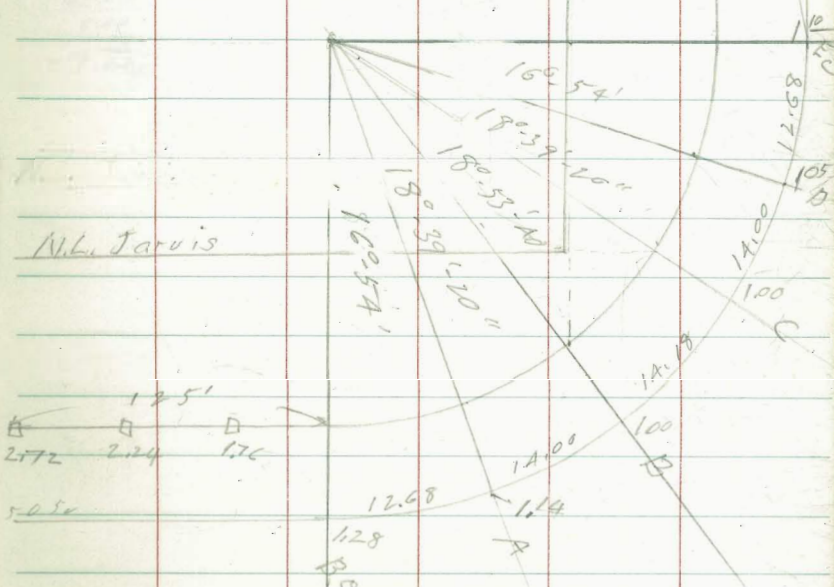
A 10.58 8°-27'

B 21.98 17°-46'-30"

C 32.94 27°-13'-30"

D 42.88 36°-33'

E.C. 50.91 45°-00'



Chalcedony St.
Mission Blvd. west to Ocean Blvd.

INDEXED
WK
MAY 16 1949

Set. B.M.
W 125' N.
5+35.

6.00

32.26

(15)
B.M. #1

2+80

42.32
9.16
8.40
C0.76

42.82
8.66
9.60
F0.94

NEB.R.
Mission Blvd
Chalcedony
48.49
2.99
51.48
12.96
38.62
4.64

5+00

30.86
7.46
7.21
C0.25

30.16
8.16
7.00
C1.10
31.36
6.96
7.17
F0.17

2+60

43.07
8.41
8.25
C0.16

43.57
7.91
7.61
C0.30

43.26
8.55
3.47
3.61
38.32

4+60

32.24
6.08
9.27
F3.19

32.74
5.58
6.19
F0.61

R.V.C.
2+40

43.48
8.00
8.15
F0.15

43.98
7.50
6.90
C0.60

E.V.C.
4+20

33.62
4.79
10.66
F5.96

38.32

34.12
4.20
4.85
F0.65

1+90

44.08
7.40
7.83
F0.14

44.58
6.90
6.52
C0.38

4+00

34.42
8.84
8.56
C0.28

34.92
8.34
9.20
F0.86

1+40

44.68
6.80
7.41
F0.61

45.18
6.30
8.90
C0.40

3+80

35.46
7.80
8.87
F1.07

35.96
7.30
7.38
F0.98

0+90

45.27
6.21
6.76
F0.55

45.77
5.71
5.15
C0.56

3+60

36.71
6.55
6.17
C0.38

37.21
6.05
6.11
F0.06

0+40

45.86
5.62
5.86
6.12
F0.26

46.36
5.12
4.12
C1.00

3+40

38.20
5.06
1.76
C3.30

38.70
4.56
8.04
F4.08

0+20

46.10
5.38
5.77
F0.39

46.60
4.88
3.89
C0.97

R.V.C.
3+20

39.80
7.68
9.12
C2.56

42.26

40.30
2.96
6.33
F3.37

W.L.M. Blvd
0+00

46.09
5.39

46.95
1.53

3+00

41.23
10.25
7.29
C2.96

54.88

41.73
9.75
12.86
F3.11

R.P. #1

← ?

Nly + Sky Alley thru BIK 117 - Resub
of Lot 42 Pacific Beach.

Missouri to Chaldeony

2470

West

East

34.75

35.28

3.57

3.04

3.61

2.64

F 0.04

C 0.40

INDEXED

WK

MAY 16 1949

2450

35.10

36.00

2.62

2.32

3.75

0.25

F 1.13

X 38.32

C 2.07

38.32

0.24

38.08

C 0.40

X 44.48

1477 E

37.60

37.75

6.98

6.73

8.28

2.99

F 1.40

C 3.74

1445

39.50

39.50

4.98

4.78

1.52

4.24

C 0.46

C 0.74

1435

39.60

39.60

X 44.48

1425

39.50

39.50

4.98

4.98

4.65

4.46

C 0.33

C 0.52

0485

38.64

38.65

5.84

5.83

5.54

5.23

C 0.30

C 0.60

0445

37.76

37.81

6.72

6.67

6.02

6.37

C 0.70

C 0.40

0400

Nly Line

36.77

36.77

36.84

Missouri

7.77

7.61

7.11

6.67

C 0.60

C 0.94

Set 1

B. Mont. M.H. (North Cross)

4.57

39.91

B.M.#2

1435 E

?

East + West Alley

BIK 117 - Lot 42 Pac. Beach.

South

North

INDEXED

WK

MAY 16 1949

Restake

12-1-48

0-2'

40.39

44.90

44.90

0-2'

NE.B.P.

Miss. Blvd

Chaldeony

48.49

0.00

48.49

2+10

8.10

4.51

4.21

7.80

8.36

4.77

3.83

7.40

F 0.26

F 0.28

C 0.38

C 0.40

0-2'

40.52

40.52

40.82

40.82

1+90

7.97

4.38

4.08

7.67

8.25

4.67

3.88

7.46

F 0.28

F 0.27

C 0.20

C 0.21

0-2'

40.69

40.69

40.99

40.99

1+70

7.80

4.21

3.91

7.50

7.64

4.06

3.72

6.95

C 0.16

C 0.15

C 0.13

C 0.55

0-2'

40.90

44.90

44.90

0-2'

04.51

1+50

7.59

4.00

3.70

7.29

7.07

3.54

3.19

7.06

C 0.52

C 0.46

F 0.09

C 0.23

Restake

12-1-48

0-2'

41.16

48.58

48.58

0-2'

48.49

1+30

7.33

4.16

4.46

4.46

7.16

7.41

7.12

7.03

C 0.17

C 0.14

C 0.24

C 0.33

48.58

7.27

41.31

3.59

0-2'

41.68

41.68

41.98

41.98

0+93.4

6.81

6.90

6.60

6.51

6.62

6.72

6.52

6.21

C 0.19

C 0.18

C 0.08

C 0.30

0-2'

42.17

48.58

48.58

0-2'

12.49

0+56.7

6.30

6.39

6.09

6.00

6.32

6.50

6.03

5.95

F 0.03

F 0.21

C 0.06

C 0.05

0-2'

42.70

42.70

43.00

43.00

0+20

5.79

5.88

5.58

5.49

5.72

6.11

5.94

5.79

C 0.07

F 0.23

F 0.36

F 0.30

0+00 =

42.98

42.98

43.41

43.41

Wil. Mission

3.51

5.60

5.14

5.08

Blvd

18.58

X

X 48.49

X 48.49

E+W. Alley Cont.

Nail in post.

3+75	39.50 6.01 3.50 C0.47	39.50 5.40 X	39.50 5.40 4.72 C0.68	39.50 6.01 6.10 F0.09	
D-2 3+50	39.63 5.88 5.62 C0.21	39.63 5.27 5.15 C0.12	39.93 4.77 4.71 C0.26	39.93 5.58 5.52 C0.06	D-2
N-0.25 IN ALLEY 3+15	39.82 5.69 5.58 C0.11	39.82 5.08 4.29 C0.80	40.12 4.78 4.56 C0.22	40.12 6.39 5.00 C0.39	D-2
D-2 2+80	40.01 5.50 5.14 C0.36 45.51X	40.01 4.89 4.64 C0.25	40.31 4.59 4.27 C0.32	40.31 5.20 4.89 C0.53 45.51X	D-2
N-0.05 2+45	40.20 8.29 8.29 X	40.20 4.70 4.45 C0.25	40.50 4.40 4.00 C0.40	40.50 7.99 7.55 C0.44	D-2
	48.49X	44.90 X			

Chamounie Thorn & Dwight
Sewer Grades.

7-17-28
W.O. 60276 (Lot # 7268) Sommermayer
McCoy X
W. Moore
E. Melton.

Stakes or spikes 6' west &.

Cuts marked on west curb. 0.1026%

Lateral stakes 5' E. of East end, n.w. B.P., Chamounie
Myrtle

INDEXED

WK

MAY 16 1949

5+00 318.48 19.46 3.78 C15.68	5+50 318.51 19.43 3.80 C15.63	5+50 318.53 19.41 3.77 C15.64	5+75 318.56 19.38 3.75 C15.63	6+00 318.59 19.35 3.66 C15.69	337.94 335.89 2.05 337.94 X 3.75 334.19 5.39 339.58 X 7.79 331.79 1.17 332.96 X 4.18 331.78 7.76 339.54 3.65 335.89 0.79 B.M.
3+75 318.35 19.59 4.34 C15.25	4+00 318.38 19.56 4.22 C15.34	4+25 318.41 19.53 4.09 C15.44	4+50 318.43 19.51 4.10 C15.41	4+75 318.46 19.48 4.01 C15.47	337.54 3.65 335.89 0.79 B.M.
2+50 318.23 19.71 4.83 C14.88	2+75 318.25 19.69 4.75 C14.94	3+00 318.28 19.66 4.70 C14.96	3+25 318.30 19.64 4.48 C15.16	3+50 318.33 19.61 4.41 C15.20	
1+25 318.10 19.84 5.15 C14.69	1+50 318.13 19.81 5.16 C14.65	1+75 318.15 19.79 5.12 C14.67	2+00 318.18 19.76 5.03 C14.73	2+25 318.20 19.74 5.07 C14.69	
M.H.#2 0+00 317.97 19.97 5.55 C14.42 West	0+25 318.00 19.94 5.29 C14.65	0+50 318.02 19.92 5.33 C14.59	0+75 318.05 19.89 5.22 C14.67	1+00 318.07 19.87 5.15 C14.72	
19.97 5.84 C14.43 East		337.94 7			

Lat #1 319.85 13.71 7.71 C5.40 ←	#2 320.00 12.96 7.00 C5.76 ←	Lat #3 322.00 10.76 4.93 C6.03 ↑	#4 328.00 11.58 5.70 C5.88 ←	Lat #5 329.40 11.18 5.44 C5.74 ↑	#6 328.60 10.98 4.51 C6.47 ↑	18.
13+75 319.31 13.65 out.	M.H.#3 13+65 319.33 13.63 9.85 C3.78 6' west on top	13.63 10.07 C3.56	6' East Nail			
12+00 319.18 13.78 5.24 C8.54	12+25 319.20 13.76 6.16 C7.60	12+50 319.23 13.73 7.06 C6.67	12+75 319.25 13.71 8.00 C5.71	13+00 319.27 13.67 8.90 C4.79	13+25 319.29 13.67 9.80 C3.87	
10+50 319.04 20.56 7.06 C13.50	10+75 319.05 20.53 7.63 C12.90	11+00 319.07 20.89 1.70 C12.19	11+25 319.10 20.86 2.55 C11.31	11+50 319.12 20.84 3.56 C10.28	11+75 319.15 20.81 4.48 C9.33	
9+00 318.89 20.71 5.38 C15.33	9+25 318.89 20.69 5.53 C15.16	9+50 318.92 20.56 5.76 C14.96	9+75 318.94 20.64 5.79 C14.85	10+00 318.97 20.61 5.93 C14.68	10+25 319.00 20.58 6.40 C14.18	
7+50 318.71 20.87 4.54 C16.33	7+75 318.74 20.84 4.64 C16.20	8+00 318.76 20.82 4.82 C16.00	8+25 318.79 20.79 4.98 C15.81	8+50 318.82 20.76 5.17 C15.59	8+75 318.84 20.74 5.22 C15.52	
6+25 318.61 20.97 5.41 C15.56	6+50 318.63 20.95 5.75 C15.20	6+75 318.64 20.94 5.28 C15.66	M.H.#1 6+85 318.65 20.93 5.00 C15.93 on west.	7+00 318.66 20.92 4.62 C16.30	7+25 318.69 20.89 4.31 C16.58	
			20.93 5.11 C15.82 on east			
		339.58 7				

Catalina + Talbot.

Curb grades.

7-22-48

INDEXED
WK
MAY 16 1949

Schmittmayer
McCoy.
Melton.

N.W.B.P. Santa Barbara

+ Catalina

260.68

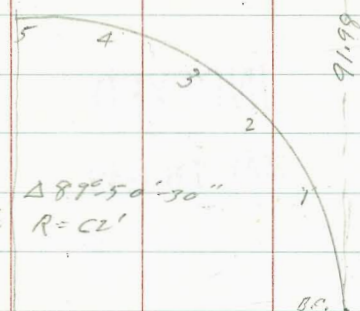
2.00

262.68

Def #1 80° 59' Chord = 18.43
 ✓ #2 17° 58' for stake line
 #3 26° 57' (59' Rad) = 5' back
 ✓ #4 35° 36' face of ch.
 ✓ E.C. = 45 44° 55'

Talbot

104
talbot 19



Δ 87° 50' 30"
 cl. R = CL'

B.C. 256.06
 6.62
 24.68
 C 1.94

#1	2	3	4
256.00	255.94	255.88	255.82
6.69	6.74	6.80	6.86
482	3.62	3.46	3.40
C 2.46	C 3.12	C 3.34	C 3.46

256.19
 6.49
 5.24
 C 1.15

#5
 255.76
 6.92
 3.74
 C 3.18

256.32
 6.36
 5.12
 C 0.84

256.45
 6.23
 5.62
 C 0.61

256.58
 6.10
 5.68
 C 0.42

256.71
 5.97
 5.65
 C 0.32

300' N.
 Talbot.

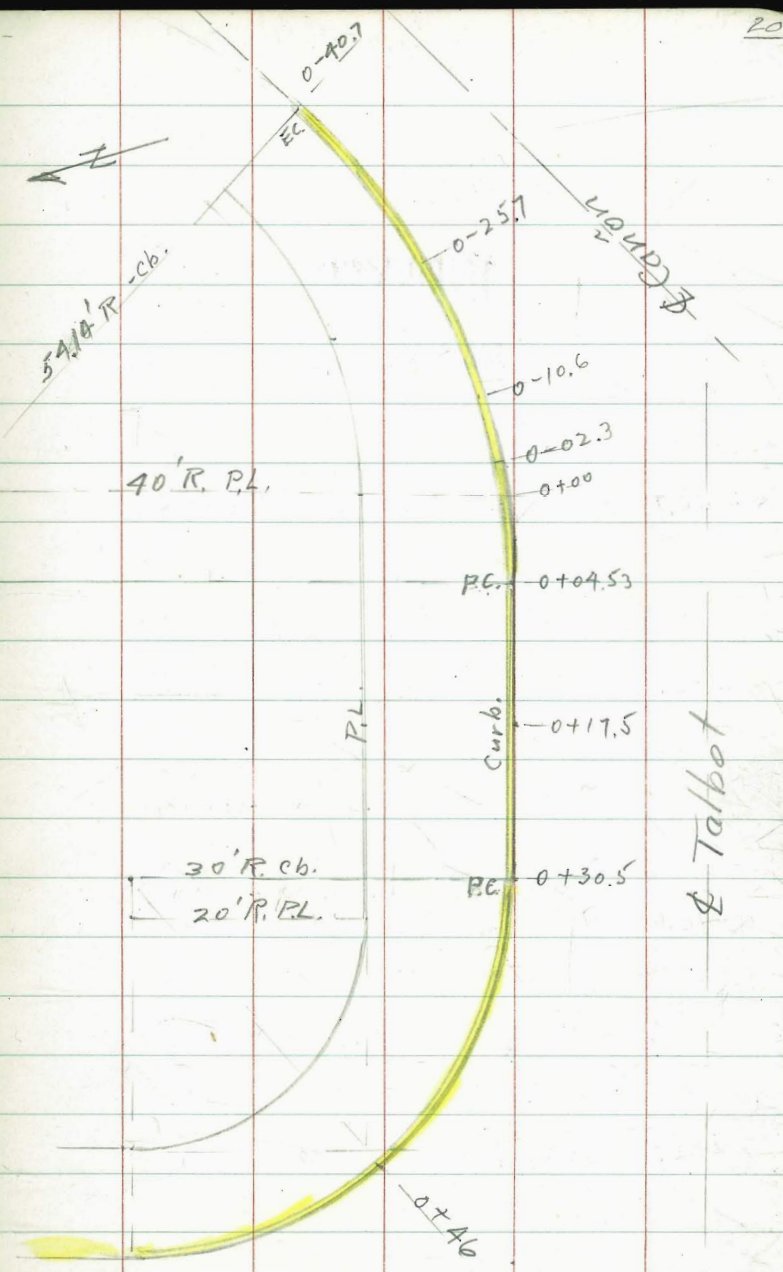
Catalina

8/2/48
McCoy
W. Moore

Carh Checkat Cañon Dr.
+ Talbot NW. Ch. Return

INDEXED
WK
MAY 16 1949

0+00	Prop Line	5.66	233.94	
0+04.53	Clb. PC.	5.30	234.30	
0+17.5		4.30	235.30	
0+30.5		3.28	236.32	
0+46		2.13	237.47	
TP. Clb. EC	0.90	<u>239.60</u>	10.76	238.70
	0.39	249.46	13.81	249.12
Mon. Talbot E N. Line Catalina	0.38	261.93	13.81	261.55



Ch. Change N.W. Ch. Return
Canon Dr. + Talbot

LT.

Card

HT.

21

INDEXED
WKS
MAY 16 1949

Half Section Radially

231.52	229.92	230.81	231.75
8.08	9.68	8.79	7.85
	20	32	44

0-40.7 End Ch. 8.08 231.52

0-25.7 7.30 232.30

0-10.6 6.40 233.20

0-02.3 Exp. Joint 5.84 233.76

7 239.60

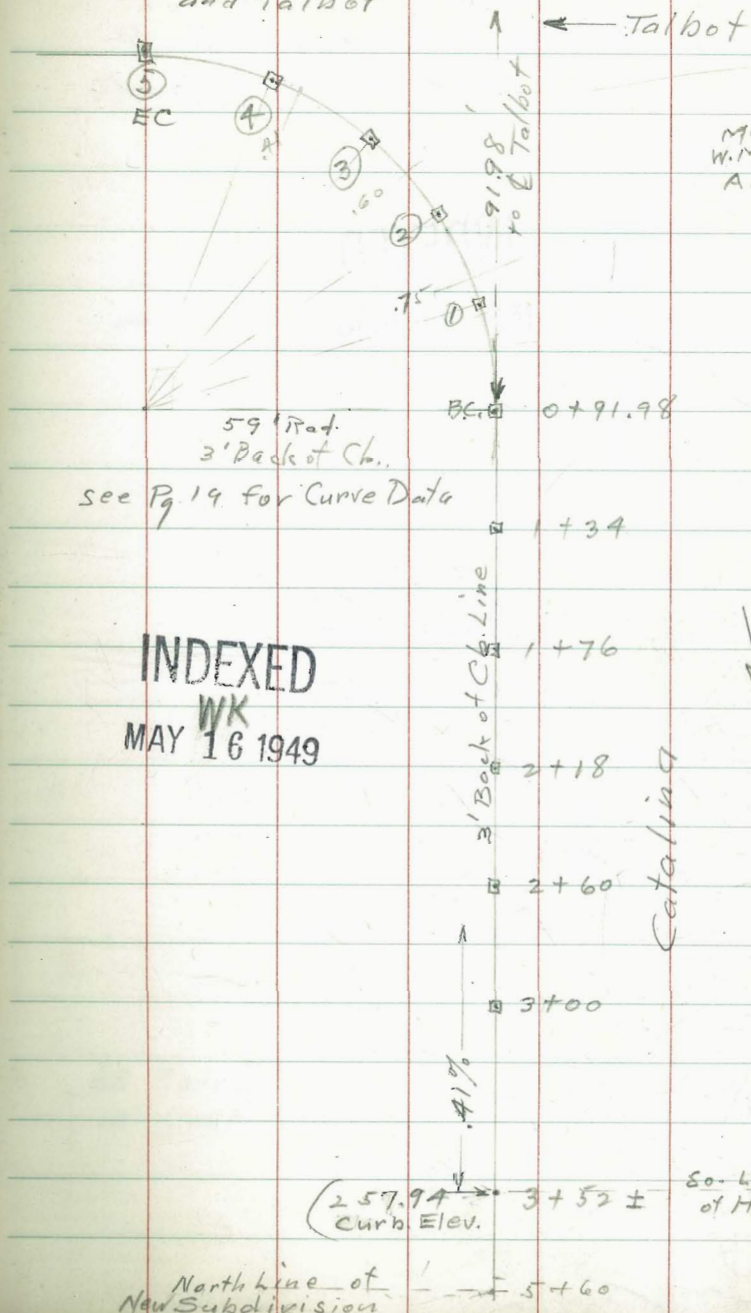
5		256.25
		5.67
		-3.00
		C = 2.67
4		256.39
		5.55
		-2.65
		C = 2.90
3		256.53
		6.53
		-3.84
		C = 2.68
2		256.66
		6.40
		-3.98
		C = 2.42
1		256.79
		6.27
		-4.59
		C = 1.68
0+91.98 RC.		256.88
		6.78
		-5.04
		C = 1.73
1+34		257.05
		6.01
		-5.62
		C = 0.37
1+76		257.22
		5.84
		-5.91
		F = 0.07
2+18		257.90
		5.66
		-6.01
		F = 0.35
2+60		257.57
		5.49
		-5.07
		F = 0.58
3+00		257.73
		5.33
		-6.03
		F = 0.70

π 261.94
 \times 263.06
 $-$ 3.85
 \hline 259.21
 $+ 2.73$
 \hline π 261.94

NW. BP.
Catalina
& Santa Barbara

263.06

260.68



INDEXED
WK
MAY 16 1949

8/4/48
McCoy
W. Moore
Allen

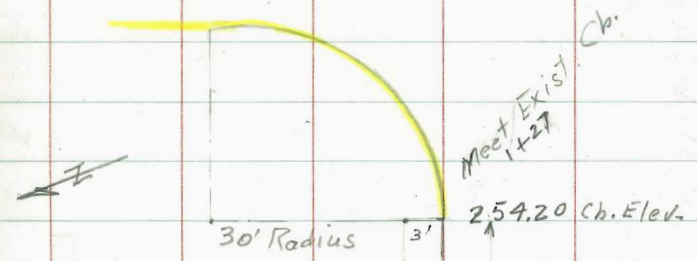
8/5/48

McCoy
W Moore
Allen

Curb Grades on tangent
Between Catalina + Point St.
North Side Talbot.

INDEXED
W K
MAY 16 1949

Point Street



1+02 E0.60

0+77 C-1.00

0+52 C-1.78

0+27 C-2.17

Flaked in
& Talbot

62' Radius
10' Curb

0+00 C-2.62

2156.25 Elev. Ch. E.C.

$\frac{1}{3}$ Back

← catalina →

Grades Lower Way at Manor

	2.79	26347		26666
T.P.	0.92	25142	1297	25050
T.P.	0.10	23871	1281	23861
T.P.	0.88	22879	1080	22791
6 lines = 0.100				22230
				6.49
				33
				6.82

INDEXED
WK
MAY 16 1949

0 + 564			22262	
			6.17	
			33	
			6.50	

1 + 1564			22342	
			5.37	
			33	
			5.70	

1 + 2564			22440	
			4.39	
			33	
			4.72	

1 + 3564			22550	
			3.29	
			33	
			3.62	

1 + 4385			22646	
			2.33	
			33	
			2.66	

Grade of houses			22150	
			7.29	
			33	
			7.62	

T.P.		288	225.91	
------	--	-----	--------	--

Cut stakes Catalina Blvd.
Whittier North. SEE ALSO PAGE 45

Set water grades (invert) 4'
Below east curb grade.

8-30-49
W.O. 31137

D-6' East Sommermayer
Water line
Invert.

66.78 X

57.24
9.54
8.6A
C 0.90

52.5A
6.27
2.48
C 3.79

56.5A
10.24
1.93
C 8.49

62.10
0.60
62.70
12.83
49.87
6.09

2+35
57.09
9.69
7.26
C 2.43

52.39
6.42
2.02
C 4.12

56.39
10.39
10.74
F 0.35

INDEXED
MAY 16 1949

1+00

55.88 T.P.
00.08
0.48
F 0.40

51.42
7.39
3.70
C 3.69

55.18
11.60
1.25
C 10.14

55.96
7.99
45.97
47.40
N.7' W. 11' 15"

2+20
57.91
8.87
6.31
C 2.56

53.21
5.60
1.50
C 4.1

57.21
9.57
10.60
F 1.03

0+80

54.12
1.84
4.28
F 2.44

49.42
9.39
5.25
C 4.13

53.22
13.30
2.70
C 10.66

55.96 X
0.48
55.48 T.P.
11.30
66.78 X
8.49

2+00
58.59
8.19
6.05
C 2.14

53.99
2.82
1.15
C 3.67

57.89
8.89
9.81
F 0.92

55.96 X

0+40

2100 50.17
5.77
10.06
F 4.27

45.87
12.99
9.00
C 3.9

66.78 X
49.47
17.31
10.70
C 6.61

45.99
12.84
58.81 X
6.10

1+80
58.87
7.91
5.76
C 2.21

54.17
4.64
1.0A
C 3.6

58.17
8.61
8.21
C 0.40

0+20

55.96 X
48.20
7.76
11.88
F 4.12

43.87
14.94
11.04
C 3.9

55.96
27.87
8.19
2.60
C 3.49

52.71
2.57
53.28 X
12.51
40.77
2.03
45.20 X

1+60
58.73
8.05
5.35
C 2.70

54.03
4.78
0.98
C 3.80

58.03
78.75
3.50
C 5.25

0+00

55.96 X
47.00
N.Ely. Whittier 8.96

58.81 X
43.0A
15.77
Meet Frist Curbs 8.92

55.96
47.0A
8.92

1+40
66.78 X
58.19
8.59
5.60
C 2.99

53.49
5.32
1.53
3.79

66.78 X
57.49
9.29
2.00
C 7.19

B.M. = S E L + T. $\frac{FB 1721}{41} = 62.10$

West

East

From P. 26

West

East

Water
line
invert
Grade

Water
line

59.597
46.40
A+20=Eb
13.19
Ec. 8.85
C 4.34

41.70
11.58
7.57
C 3.99

46.877
45.70
1.17
1.25
Ea. 0.8

58.29
1.30
59.597
13.10
46.49
0.38
46.877
12.47
34.40
4.55
38.95
7.49
31.46 =
31.47
B. M. H. H.

Sheet 6997 L
* 46.87
To west To south

A+10
47.70
11.87
Back 5' Both
ways on East 8.36
C 3.53
Back 5' west
only on west

43.00
10.28
6.84
C 3.44

47.00
- 0.13
0.92
F 1.05

48.40
- 1.53
92
F 2.45

Banning St.

Back 5' 1 way
on west

5 Back Both
ways 49.70
3+50 on West 9.89
4.95
C 4.94

45.00
8.28
3.96
C 4.42

59.597
To West To North
49.00
10.59
11.47
Ea. 0.88

Cl. B.C.
3+40 50.35
9.24
4.81
C 4.43

53.28
45.65
7.63
3.43
C 4.20

49.65
9.94
11.30
F 1.36

2+95 59.597
53.26
6.33
2.8
C 3.53

58.81
48.56
10.25
6.10
C 4.15

59.597
52.56
7.03
3.20
C 3.83

End. job.
5+10 38.957
34.70
4.25
6.05
F 1.80

38.957
A 3.20
30.00
13.20
8.78
C 4.42
38.957
34.00
4.95
8.76
F 3.81

A+65 46.877
40.55
6.32
5.28
C 1.04

53.28
46.877
35.85
17.43
13.28
C 4.15
46.877
39.85
7.02
8.77
F 1.75

water
levels.
check
x 43.20
39.85
335
5.11
F-1.76
OK

Profile
& traveled road.

Sommermeier
M^o Coy
W. Moore

on Keating from W line Lynwood

to 100' E. of E. line Lynwood.

9-2-48

SEE ALSO PAGE 8

INDEXED
WIK
MAY 16 1949

1+00

7.4

+50

7.7

+18

7.5

409

7.2

0+00

133.8

6.9

0-30

6.3

0-60

134.6

6.2

BM # 2

P. 7

0145

140.57

140.22

Restake Portion Alley Bk. A5
Track 1368

El Cajon (Bet. 494 Winona) to South.

E. W.

Station from El Cajon

INDEXED

WK
MAY 16 1949

Station	Old Station	Old Station	Old Station
0+80	A+80	359.85 5.08 2.34 C-2.74	359.60 5.33 5.12 F0.77
0+60	A+60	360.70 4.23 3.28 C0.95	360.45 4.18 5.14 F0.86
0+40	A+80	362.10 2.83 1.66 C-1.17	361.85 3.08 4.16 F1.28
0+20	S+00	363.30 1.63 1.31 C0.32	363.05 1.88 3.33 F1.45
S.L. El Cajon 0+00	S+20	364.10 0.83	363.14 1.79
Old. Cut at 20' Lt. Gr. 362.62 C 1.00 Stake 363.62	131.	364.93 *	363.62

Station	Old Station	Old Station	Old Station
Moot old grade. 1+40	S+80	358.50 6.43 6.68 F0.25	358.25 6.68 8.34 F1.66
1+20	A+00	358.82 6.11 6.82 F0.21	358.57 6.36 7.73 F1.57
1+00	A+20	359.25 5.68 5.17 C0.51	359.00 5.93 7.99 F7.86

Alley Bk. 47 - O.B.

Paver

30

7-10-48
W.O. 31431INDEXED
WK
MAY 16 1949Sommermeier
Mc. Coy
W. Moore

		No.			No.		No.	X (P. 32)
1+00	36.38 5.64 5.64 x	36.39 5.63 5.51 C 0.32		2+80	32.90 4.75 4.57 C 0.18		32.90 4.75 4.35 C 0.40	42.02 7.51 34.51 3.14 37.65X
0+80	37.07 4.95 5.39 F 0.44	37.13 4.89 5.07 F 0.18		2+60	33.24 4.41 4.67 F 0.26		33.24 4.41 4.29 C 0.13	
0+60	37.99	38.12		2+25	37.65X 33.90 3.75 4.13 F 0.38		37.65X 33.90 3.75 3.02 C 0.73	
0+50	42.02X 38.56 3.46 5.00 F 1.54	3.90 4.17 F 0.27	42.02X 38.73 3.29 2.40 C 0.85					
0+40	45.87X 39.12 6.75 6.75 x	39.35 6.52 3.10 C 3.42		1+90	42.02X 34.56 7.46 7.18 C 0.28		42.02X 34.56 7.46 7.05 C 0.41	
0+20	45.87X 40.47 5.40 6.40 F 1.00	40.81 5.06 2.81 C 2.25		1+55	35.22 6.80 6.90 F 0.10		35.22 6.80 6.57 C 0.23	
0+00 = w. line Sunset Cliffs Blvd	42.03 3.84 v	42.53		1+20	35.89 6.13 6.03 C 0.10		35.89 6.13 5.84 C 0.59	

45.87
From Page 32

INDEXED

WK

MAY 16 1949

Alley BIK. 47.08

30.

NO

4+60³

36.94 X

36.94 X

31.5431.54

5.40

5.40

5.675.72

F0.27

F0.32

4+20²

31.78

31.78

5.165.165.195.50

F0.03

F0.34

37.65 X

5.25

32.20

4.74

36.94 X

5.64

31.30

5.15

36.45

3+80^v

36.94 X

36.94 X

32.0232.02

4.92

4.92

3.924.04

C.1.00 mil

C0.88

6+00

30.77

5.68

7.23

F0.05

30.59

5.86

5.90

F0.04

3+40

37.65 X

37.65 X

32.2632.26

5.39

5.39

5.335.29

C0.06

C0.10

5+80⁶30.82

5.63

4.38

C1.25

30.82

5.63

5.00

C0.63

3+20

32.41

32.41

5.245.245.244.57

x

C0.67

5+40⁵

31.06

5.39

4.82

C0.97

31.06

5.39

5.04

C0.35

3+00

37.65 X

37.65 X

32.6332.63

5.02

5.02

5.044.73

F0.02

C0.29

5+00⁴

36.45 X

31.30

5.15

4.80

C0.35

31.30

5.15

5.21

F0.06

Cont. P. 32
por. walls

31

Alley BIK. A7-Ocean Beach

South wall (Sheet 7086-L)

Top.

Base to East

Base to West

South face of walls on prop. line
0.15 Jog in paving.

0+50 $\frac{39.06}{2.96}$
 $\frac{5.00}{F 2.04}$

$\frac{36.00}{6.02}$
 $\frac{5.00}{C 1.02}$

INDEXED
WK
MAY 16 1949

0+40 $\frac{39.62}{6.25}$
 $\frac{6.75}{F 0.50}$

$\frac{36.50}{9.37}$
 $\frac{6.75}{C 2.62}$ $\frac{36.00}{9.87}$
 $\frac{2.44}{39.58}$
 $\frac{6.29}{42.02}$

0+20 $\frac{40.97}{4.70}$
 $\frac{6.00}{F 1.50}$

$\frac{36.50}{9.37}$ EFW.
 $\frac{6.00}{C 2.97}$

0+18 $\frac{41.09}{4.78}$
 $\frac{6.29}{F 2.00}$

$\frac{36.50}{9.37}$ EFW
 $\frac{6.29}{C 2.59}$

0+10 $\frac{41.56}{4.31}$
 $\frac{7.51}{F 3.20}$

$\frac{38.00}{7.87}$
 $\frac{7.51}{C 0.36}$ $\frac{36.50}{9.37}$
 $\frac{7.51}{C 1.86}$

0+04 $\frac{41.91}{3.96}$
 $\frac{5.32}{F 1.36}$

$\frac{38.50}{7.37}$
 $\frac{5.32}{C 2.05}$ $\frac{38.00}{7.87}$
 $\frac{5.32}{C 2.55}$

0+00 $\frac{42.15}{3.72}$
 $\frac{4.04}{F 0.32}$

38.50

N.W. & P.
Sunset Cliff
& Del Mar

9.68 45.87 - 36.19

Alley BIK. A7-Ocean Beach 32

North wall (7086-L)

End,
0+50

top.

$\frac{39.73}{6.14}$ = T.P. El. 39.58
 $\frac{6.29}{F 0.15}$

Stub

Base

0+46

Knocked out
 $\frac{42.97}{2.90}$
 $\frac{3.94}{F 1.04}$ Restake
47.10
 $\frac{42.97}{4.13}$
 $\frac{6.15}{F 2.12}$

0+40

$\frac{42.97}{2.90}$ - stub grade = 42.77
 $\frac{3.10}{F 0.20}$ $\frac{4.32}{42.10}$

0+34^E

0+31^E

0+20

$\frac{42.97}{2.90}$
 $\frac{2.91}{C 0.09}$

0+00

$\frac{42.97}{2.90}$
 $\frac{2.58}{C 0.32}$

INDEXED
WK
MAY 16 1949

Pavement stakes

Alley Blk. 58- Ocean Beach

9-21-48 (Sheet: L-7085)

Sommermeier
McCoy
W Moore
C Hatch
Mo.

W.O. 31398

So.

1+20	19.01 X 13.60 <u>5.44</u> 5.74 F0.33	19.01 X 13.45 <u>5.56</u> 5.38 C0.18	13.05 <u>5.96</u> 19.01 X <u>6.56</u> 12.45 3.32 15.77 X <u>6.02</u> 9.75 <u>5.01</u> 14.74 X <u>5.01</u> 9.75 <u>4.59</u> 14.34 X
------	--	--	--

INDEXED

WIK

MAY 16 1949

0+80	14.18 <u>4.83</u> 5.01 F0.18	14.03 <u>4.98</u> 5.09 F0.11	14.74 X <u>5.01</u> 9.75 <u>4.59</u> 14.34 X
0+60	14.36 Cross <u>4.65</u> 4.06 C0.59	14.24 <u>4.77</u> 4.27 C0.50	14.34 X

0+40	14.40 Prec. <u>4.61</u> 4.10 C0.51	14.30 <u>4.71</u> 4.01 C0.70	
------	---	---------------------------------------	--

0+20	14.29 <u>4.72</u> 4.11 C0.61	14.24 <u>4.77</u> 4.51 C0.26	
------	---------------------------------------	---------------------------------------	--

w/y. cable 0+00	19.01 X <u>13.95</u> 5.06 V	19.01 X <u>13.98</u> 5.03 L	
--------------------	-----------------------------------	-----------------------------------	--

S.W.P. Cable
+ Cape May

— 13.05

South

North

3+40	15.77 X <u>10.47</u> 5.30 <u>5.08</u> C0.28	15.77 X <u>10.32</u> 5.45 <u>5.47</u> F0.02
------	---	---

3+20 Nail.	10.73 <u>5.04</u> 4.10 C0.94	10.58 <u>5.17</u> 1.62 C0.57
------------	---------------------------------------	---------------------------------------

2+80	11.30 <u>4.47</u> 4.72 F0.25	11.15 <u>4.62</u> 4.98 F0.36
------	---------------------------------------	---------------------------------------

2+40	11.88 <u>3.89</u> 3.99 F0.10	11.73 <u>4.04</u> 4.07 F0.03
------	---------------------------------------	---------------------------------------

2+00	15.77 X <u>12.45</u> 3.32 <u>3.32</u> x	15.77 X <u>12.30</u> 3.47 <u>1.82</u> C7.65
------	---	---

1+60	19.01 X <u>13.03</u> 5.98 <u>5.72</u> C0.26	19.01 X <u>12.88</u> 6.15 <u>5.76</u> C0.37
------	---	---

	South	North
5+20	$\begin{array}{r} 14.34T \\ 9.67 \\ \hline 4.67 \\ 4.49 \\ \hline C 0.18 \end{array}$	$\begin{array}{r} 14.74T \\ 9.52 \\ \hline 5.22 \\ 4.08 \\ \hline C 1.14 \end{array}$
4+80	$\begin{array}{r} 14.34T \\ 9.79 \\ \hline 4.55 \\ 4.76 \\ \hline F 0.21 \end{array}$	$\begin{array}{r} 14.74T \\ 9.64 \\ \hline 5.10 \\ 4.96 \\ \hline C 0.14 \end{array}$
4+40	$\begin{array}{r} 15.77T \\ 9.91 \\ \hline 5.86 \\ 5.84 \\ \hline C 0.02 \end{array}$	$\begin{array}{r} 15.77T \\ 9.76 \\ \hline 6.01 \\ 5.64 \\ \hline C 0.37 \end{array}$
4+00	$\begin{array}{r} 10.03 \\ 5.74 \\ \hline 5.50 \\ \hline C 0.24 \end{array}$	$\begin{array}{r} 9.88 \\ 5.89 \\ \hline 5.78 \\ \hline C 0.11 \end{array}$
3+80	$\begin{array}{r} 10.12 \\ 5.65 \\ \hline 5.50 \\ \hline C 0.15 \end{array}$	$\begin{array}{r} 9.97 \\ 5.80 \\ \hline 5.83 \\ \hline F 0.03 \end{array}$
3+60	$\begin{array}{r} 15.77T \\ 10.27 \\ \hline 5.50 \\ 5.33 \\ \hline C 0.17 \end{array}$	$\begin{array}{r} 15.77T \\ 10.12 \\ \hline 5.65 \\ 5.82 \\ \hline F 0.17 \end{array}$

Alley Blk. 58. O.B.

34

	South	North	Top of Wall
	INDEXED WIK MAY 16 1949		stakes 5' N. of property.
E4. Bacon 5+992	$\begin{array}{r} 7.41 \\ 6.93 \\ 6.94 \\ \hline F 0.01 \end{array}$		$\begin{array}{r} 9.54 \\ 6.80 \\ 6.80 \\ \hline \end{array}$
5+97	End of wall	Cross on Line	$\begin{array}{r} 11.16 \\ 3.18 \\ 6.37 \\ \hline F 3.19 \end{array}$
5+80	$\begin{array}{r} 8.35 \\ 5.99 \\ 5.26 \\ \hline C 0.73 \end{array}$	Nail: 4.7 out from	$\begin{array}{r} 11.50 \\ 2.84 \\ 2.85 \\ \hline F 0.01 \end{array}$
5+60	$\begin{array}{r} 9.04 \\ 5.30 \\ 4.81 \\ \hline C 0.49 \end{array}$		$\begin{array}{r} 8.96 \\ 5.38 \\ 2.11 \\ \hline C 3.27 \end{array}$
5+40	$\begin{array}{r} 9.48 \\ 4.86 \\ 4.74 \\ \hline C 0.12 \end{array}$		$\begin{array}{r} 11.90 \\ 2.44 \\ 3.11 \\ \hline C 0.33 \end{array}$
5+25	start of wall	Nail	$\begin{array}{r} 12.30 \\ 2.04 \\ 1.77 \\ \hline C 0.27 \end{array}$
			$\begin{array}{r} 14.34T \\ 9.39 \\ \hline 4.95 \\ 1.91 \\ \hline C 3.04 \end{array}$
			$\begin{array}{r} 14.34 \\ 12.60 \\ \hline 1.74 \\ 1.91 \\ \hline F 0.17 \end{array}$

9/2-1/48
Drawing
6823-L

East West Alley
Univ. Heights

BIK 105
(W.O. 31323)

McCoy
W. Moore
C. Hatch

R. Livo Arizona
2799.69
Exist. Pav.

340.04
8.34
8.33
C 0.01 ✓

340.11
8.27
8.28
F 0.01

35

2' Back Pav.

South

North

2' Back Pav.

2' Back Pav.

2' Back Pav.

1 + 39.85
E. Alley Line
to North

360.21
11.61
9.37
C - 2.24

360.21
11.61
9.80
C - 1.81

2' East
+ 2' North
Corner of
Pav.

2 + 89.69

341.37
7.01
5.89
C - 1.12

341.37
7.01
5.71
C - 1.20

+ 20

362.72
9.10
7.77
C 1.38

362.72
9.10
8.27
C 0.83

+ 64

348.38
344.63
3.75
2.99
C 0.76

348.38
344.63
3.75
3.63
C 0.12

INDEXED

WIK
MAY 16 1949

1 + 00

364.95
6.87
6.29
C 0.28

364.95
6.87
6.46
C 0.41

+ 38

Nail in
Fence
0.43 Back

360.59
347.90
12.69
10.69
C - 2.00

360.59
347.90
12.69
12.96
F 0.27

+ 80

366.63
5.19
5.51
F 0.36

366.63
5.19
4.19
C 1.00
+ Mark on
Garage
0.31 Back

2 + 12

Nail in Fence
0.38 Back

351.16
9.43
8.43
C 1.00

351.16
9.43
8.92
C 0.51

+ 60

367.66
4.16
4.10
F 0.09

367.66
4.16
4.10
C 0.06

1 + 86

360.59
354.43
6.16
5.84
C - 0.32

360.59
354.43
2.16
6.10
C 0.06

+ 40

368.15
3.67
4.02
F 0.35

368.15
3.67
3.66
C 0.01

1 + 59.85
E. Alley Line
to North

371.82
357.69
14.18
12.22
C - 1.91

357.69

368.35
3.47
371.82
12.12
359.70
7.89
360.59
12.96
371.63
0.75
348.38

0 + 20

368.07
3.75
3.13
C 0.62
367.51
4.31
2.29
2.22

368.07
3.75
3.09
C 0.66
367.20
4.18
1.24
E. 0.06
Patch

1 + 49.85
E. N. S. Alley

B.M. #1-8' At 1 + 20

8 + 00
Exist. Pav.

N.E.P.
Hamilton + E. Galen

347
371.82

368.35

Staking North + South Alley
Block 105 - Univ. Heights

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WK
MAY 16 1949

West East
or x-2' Back (1175 from 4) unless Noted

Begin Embankment

	West	Restake	East	Restake
#5333 Wall	358.82 5.68 6.01 F0.33	358.52 4.85 4.87 F0.02	359.12 5.38 0.77 C4.61	358.82 4.55 4.37 C4.92
+20 N. End Wall	358.65 5.85 7.13 F1.46	358.35 5.02 6.17 F1.15	358.95 5.55 3.42 C2.13	358.65 4.72 2.27 C2.45
#10 5' out	358.44 6.06 6.29 F0.23	358.14 5.24 5.14 C0.09	359.22 5.28 2.83 C2.45	358.97 4.94 2.21 C2.70
0+05 2' of Wall	362.147 358.06 4.08 4.15 F0.33	Top Wall 358.39		
0+00 5' west face of wall 2' of wall 5' N. of prop.	357.69 6.81 6.68 C0.13	362.14 357.69 4.45	360.31 4.27 2.48 C1.81	363.36 Both ways 360.01 3.35 1.37 C2.02
0-0.50 W. End Wall	Restake 362.14 357.13 5.21 4.25 C0.56	Top Wall 357.46	360.21 359.70 2.44 362.14	359.70 2.44 362.14
B.M. #1 P.35	4.80	364.30	359.70	

1 X 56
Begin

Begin Embankment

End

Restake West Restake East

Center stakes set from
west header as shown on plans
10-8-48

2+00	366.55 359.76 6.59 8.70 F2.11	360.21 7.06 7.44 F2.38	366.55 360.38 6.17 3.85 C2.22	360.51 6.76 4.57 C2.17
+80	363.36X 359.45 3.91 5.30 R1.41	367.27X 359.75 7.52 7.27 F1.70	363.36X 359.80 3.56 3.70 F0.14	359.70 4.80 364.50X 5.68 358.82 8.45 367.27X 4.20 362.07 3.64 365.71X
366.55 + 60	359.12 4.24 5.22 F0.98	364.50X 359.42 5.08 6.37 F1.29	359.42 3.94 3.79 C0.15	367.27X 359.72 7.55 7.70 F0.15
1+40	358.95 4.41 5.48 F1.07	359.25 5.25 6.64 F1.39	359.35 4.01 2.08 1.55	359.55 4.95 3.58 C1.37
1+20	358.85 4.51 5.42 F0.91	359.15 5.35 6.56 F1.21	359.15 4.21 2.90 C1.31	359.45 5.05 4.05 C1.00
0+86.66	363.36 358.68 4.68 5.50 F0.82	358.98 358.98 5.52 6.65 F1.13	363.36 358.99 4.38 1.93 C2.65	359.28 5.22 2.88 C2.34

1497
Begin

1476
End Emb.

2x36
End Emb.

2x78
2x66
2x60
2x50
Begin Emb - to Meade.
End Emb
Begin - End 2x25
End Emb 2x77

		West	East	
+45	0-2'	363.71* 361.36 4.35 5.92 F1.57	361.66 4.05 2.95 C1.10	□ 1' Back
+20	x 0.30 Back	367.27* 361.61 5.66 4.66 C1.00	363.71* 361.91 3.80 0.52 C3.28	□ 2'
3+00	x 0.35 Back	361.81 5.46 4.46 C1.00	362.11 5.16 9.30 C4.82	□ 0.90 Back
+80	0-1' Back	361.90 5.37 6.72 F1.35	362.20 5.07 1.29 C3.78	□ 1.5' Back
+60		361.76 5.51 5.73 F0.22	362.06 5.21 1.10 C4.07	
	Restake		Restake	
+40		366.55* 361.31 5.24 4.84 C0.40	361.71 5.56 2.25 C3.31	
2+20		366.05* 360.60 5.95 6.86 F0.91	361.03 6.24 2.86 C3.38	
		367.27*		

		West	East	
+50	End Wall	359.13 6.58 6.58	360.61 5.10 5.07 0.03	Top Wall 359.46 T.P. #4
+30	0-2'	360.22 5.49 3.97 F0.48	360.81 4.90 2.74 C-2.16	□ 2'
+25	Begin Wall	360.34	360.67	Top Wall
+10	0-2.5' B	360.71 5.00 4.48 C0.52	361.01 4.70 3.79 C-1.21	□ 1' Back
+90	0-2'	360.91 4.80 6.49 F1.69	361.21 4.50 2.89 C1.61	□ 1.25' B
3+70	0-2'	361.11 4.60 6.03 F1.43	361.41 4.30 2.98 C1.32	□ 1.45' B
		361.71		

Alley BIK to Univ. Hqts.

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Levels for
Nall on P. 40WK
MAY 16 1949stakes 2' Back
of 95 except
where noted.

1+20	N. 120 B 361.25 4.28 4.02 F 0.16	360.97 4.147V	361.55 3.98 2.53 C 1.45 Nail in pole # P.A. 442V 4.50	359.13 64 365.53 3.57 361.96 1.50	3+60	372.30 363.10 7.20 7.54 F 0.34	362.62 7.83V	372.30 363.10 8.90 6.75 C 1.75
0+80	X. 2' 360.97 4.56 C. 0.4 F 1.48	360.49 4.75L	361.27 4.26 1.21 C 3.05	366.46 136 365.10 Nail pole # P.A. 445V Sta. 4700	3+20	362.65 3.81 4.80 F 0.99	362.17 8.28V	N. 0.35 B 362.95 3.51 1.49 C 2.03
0+60	X. 2' 360.83 4.70 5.21 F 0.51	360.37 4.87L	361.20 4.33 1.24 C 3.09	365.10 7.00 372.30X F 0.4 T.P. 0.4	2+80	62.37 189 362.37 4.09 4.95 F 0.86	365.24X 361.89 3.35X Not set	N. 0.25 B 362.67 3.79 2.46 C 1.33
0+40	65.24 60.62 46.2 4.97 F 0.29	X. 2' 360.62 4.71 5.19 F 0.28	360.29 4.95L 361.29 4.24 2.08 C 2.16	0 2' P. 37 357.13 6.11 365.24X 2.77 362.47 7.98	2+40	N. 2.77 B 362.09 4.37 4.12 C 0.25	361.61 3.63V	0 2' 362.39 4.07 2.95 C 1.12
0+20	X. 1' 360.26 5.27 5.40 F 0.13	360.24 5.00V	361.51 4.02 2.13 C 1.89	0 2' 370.45 X	2+00	N. 0.75 B 361.91 4.65 5.33 F 0.68	361.33 3.71L	N. 0.75 B 366.46X 362.11 4.35 3.13 C 1.22
N. 1100 Meade 0+00	565.24 359.82 5.92	X. 2' 360.23 5.01	365.24X 360.23 361.89 3.64		1+60	0 3' B 366.46X 361.53 4.93 6.67 F 1.74	361.05 4.19V	0 2' 365.51X 361.83 3.70 2.77 C 0.93
10' Lt. A150 Alloy B/R 101	6.40	365.53	359.13					

Blk. 70 Univ. Hqts.

A+80	<u>366.41</u> 5.89 <u>6.12</u> F0.23	<u>365.93</u> 4.52v	<u>366.71</u> 5.59 <u>3.74</u> C1.85
------	---	------------------------	---

A+60	<u>365.65</u> 6.65 <u>6.70</u> F0.05	<u>365.17</u> 5.28v	<u>365.95</u> 6.35 <u>2.18</u> C2.07
------	---	------------------------	---

A+40	<u>364.98</u> 7.32 <u>7.16</u> C0.16	<u>364.50</u> 5.95v	<u>365.28</u> 7.02 <u>5.17</u> C1.85
------	---	------------------------	---

A+20	<u>364.38</u> 7.72 <u>8.00</u> F0.08	<u>363.90</u> 6.55v	<u>364.68</u> 7.62 <u>6.08</u> C1.54
------	---	------------------------	---

A+00	<u>363.87</u> 8.43 <u>8.07</u> C0.36	<u>363.39</u> 7.06v	<u>364.17</u> 8.13 <u>7.28</u> C0.85
------	---	------------------------	---

3+80	<u>363.44</u> 8.86 <u>9.06</u> F0.14	<u>362.96</u> 7.47v	<u>363.74</u> 8.56 <u>7.12</u> C1.44
------	---	------------------------	---

372.30

check

Ob. End.

<u>370.45x</u> 368.93	<u>368.93</u>	<u>370.05</u>
1.52	5.65	4.53
<u>1.55</u>	<u>5.67</u>	
-0.07	-0.02	

S. line
Horroo
6+00

<u>368.80</u> 5.78 <u>5.67</u> C0.11	<u>368.62</u> 1.83v	<u>369.70</u> 4.88 <u>2.16</u> C0.22
---	------------------------	---

5+80

<u>369.05</u> 5.53 <u>5.27</u> C0.24	<u>368.67</u> 1.78v	<u>369.69</u> 4.89 <u>3.77</u> C0.96
---	------------------------	---

5+60

<u>374.54x</u> 369.01	<u>368.57</u> 1.88v	<u>374.58x</u> 369.46	
5.59		5.12	372.30
<u>6.51</u>		<u>3.90</u>	3.27
F0.94		C1.22	369.07
			5.51
			37458

5+40

<u>372.30x</u> 368.66	<u>368.20</u> 2.25v	<u>372.30x</u> 369.00	
3.64		3.30	
<u>3.47</u>		<u>1.63</u>	
C0.15		C1.67	

5+20

<u>368.01</u> 4.29 <u>4.72</u> F0.43	<u>367.53</u> 2.92v	<u>368.31</u> 3.99 <u>2.45</u> C1.54
---	------------------------	---

Curb. Ret. Wall Bk. 70
Univ Hqts. (6823-4)

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WK
MAY 16 1949

0+52

360.88

1.65

5.08

F 0.43

0+48

360.96

1.57

5.13

F 0.56

0+40

360.87

4.66

5.19

F 0.53

0+20

360.61

1.92

5.40

F 0.48

0+04

360.16

5.37

5.59

F 0.22

0+00

359.94

5.89

5.70

F 0.11

365.53 from page 38

Paving Grades Monroe
Oregon to Louisiana

S. Gutter Sub. Grade N. Gutter

S 1/4 ♀ N 1/4

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WK
MAY 16 1949

East Line
Hamilton
3+00

374.92	375.06	375.25	375.17	375.15
6.77				6.54
6.75				6.59
0.02		38126		10.07

2+80	375.02	375.18	375.39	375.32	375.30
	6.67	6.08	5.87	5.94	6.29

2+50	375.25	375.39	375.60	375.55	375.56
	6.44	5.87	5.66	5.71	6.13

Rake

Rake

Brk 0+20	377.42	377.49	377.63	377.51	377.46
	4.27	3.77	3.63	3.75	4.23

0+00	377.62				
W.L. Oregon	4.07		377.94		377.62
	4.03				4.07
	0.04				

S.E. B.P.
Monroe &
Hamilton

6.39	381.69		375.30	
------	--------	--	--------	--

sub. Grade

S. Gutter Finish Gr. S 1/4 ♀ N 1/4 N. Gutter Finish Gr.

Brk 2+00	376.90x				376.90x
	366.30	366.56	366.89	366.96	367.10
	10.60	10.10	9.77	9.70	9.80
	X				X

Brk. 1+90	366.90	367.17	367.50	367.58	367.72
	10.00	9.49	9.16	9.08	9.18
					X

Brk 1+60	368.25	368.54	368.89	368.98	369.14
	8.65	8.12	7.77	7.68	7.76
	3.3				3.3
	8.98				8.09

Brk 1+40	369.15	369.41	369.74	369.81	369.95
	7.75	7.25	6.92	6.85	6.95
	3.3				3.3
	8.08				7.28

Rake

Brk. 0+20	373.25	373.43	373.69	373.69	373.75
	3.65	3.23	2.97	2.97	3.15

X = 376.66

0+00	376.90x			376.90
W.L. Hamilton	373.97		374.40	374.47
375.30				2.43
1.60				2.42
376.90				0.01
12.24				
264.12				
1.97				
366.09x				

Monroe

	S. Butter Finish Cr.	Sub. grade			N. Butter Finish grade
		S 1/4	±	N. 1/4	
E. line ARIZONA					
3+00	366.097 353.41 12.68		354.58		366.097 354.81 12.28
Brk 2+80	356.30 9.79 x	356.65 7.77	357.11 7.31	357.32 7.10	357.63 8.46 x
Brk 2+50	360.12 5.33 x	361.04 3.38	361.37 3.03	361.48 2.94	361.64 1.15 x
Brk 2+40	362.14 3.75 x	362.41 7.01	362.73 1.67	362.80 1.62	362.93 3.16 x
		± 364.42			
Brk 2+30	366.097 363.30 2.79 x	363.55 13.11	363.88 12.78	363.94 12.72	366.097 364.07 2.02 x
Brk 2+10	376.90x 365.40 11.50 x	365.65 11.01	365.98 10.68	366.04 10.62	376.90x 366.18 10.72 x
		± 376.66			

Monroe

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	S. Butter Finish Cr.	Sub. Grade			N. Butter Finish Cr.
		S 1/4	±	N. 1/4	
Brk. 0+90	343.79 10.54 x	344.11 8.01	344.50 7.62	344.62 7.50	344.82 9.51 x
Brk 0+80	344.34 9.99 x	344.66 7.46	345.05 7.07	345.18 6.94	345.38 8.95 x
Brk 0+70	345.15 9.18 x	345.47 6.65	345.87 6.25	346.00 6.12	346.20 8.13 x
0+45	347.52 8.81 x	47.85 4.27	48.26 3.86	48.39 3.73	348.61 5.72 x
Brk 0+20	349.90 4.43 x	50.24 1.88	350.65 1.47	50.80 1.32	351.02 3.21 x
		± 52.12			
0+00 W. line ARIZONA	354.33x 351.60		352.50		354.33x 352.99
S. 1/4 Monroe Texas 338196	2.73 2.78				1.34 1.34
Red 1236 Dist 3.01	2.07				
	354.33 x				

Monroe

	S.G.	S 1/4	&	N 1/4	N. G.
	Finish	Sub. Grade.			Finish
	Gr.				Gr.
Ex 1170 Louisiana	3700	337.40		337.16	337.31

	2780	337.07		337.43	337.41
--	------	--------	--	--------	--------

Void

	0740			338.34	
--	------	--	--	--------	--

N. 1700 Texas		337.85		338.44	338.75
------------------	--	--------	--	--------	--------

Catalina -

Whittier - North.

SEE ALSO PAGE
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WK

MAY 16 1949

1+20

$$\begin{array}{r} 57.24 \\ 0.94 \\ 1.45 \\ \hline F0.51 \end{array}$$

$$\begin{array}{r} 56.57 \\ 1.59 \\ 1.26 \\ \hline C0.33 \end{array}$$

$$\begin{array}{r} 56.54 \\ 2.62 \\ 2.90 \\ \hline F0.28 \end{array}$$

$$\begin{array}{r} 45.97 \\ 12.21 \\ 58.18x \\ 0.83 \\ \hline 57.35 \end{array}$$

2+50

56.82

56.17

55.47

3.69

3.07

C0.62

2+40

$$\begin{array}{r} 2.34 \\ 2.28 \\ \hline C0.06 \end{array}$$

$$\begin{array}{r} 2.99 \\ 1.94 \\ \hline C1.05 \end{array}$$

56.39

2.77

2.53

C0.24

1+00

$$\begin{array}{r} 55.88 \\ 2.30 \\ 2.73 \\ \hline F0.43 \end{array}$$

$$\begin{array}{r} 55.23 \\ 2.96 \\ 2.42 \\ \hline C0.54 \end{array}$$

$$\begin{array}{r} 55.18 \\ 3.98 \\ 4.23 \\ \hline F0.25 \end{array}$$

$$\begin{array}{r} 59.16 \\ 12.42 \\ 46.74 \\ 0.08 \\ \hline 46.82x \end{array}$$

2+20

$$\begin{array}{r} 57.91 \\ 1.25 \\ 1.62 \\ \hline F0.39 \end{array}$$

$$\begin{array}{r} 57.26 \\ 1.90 \\ 1.28 \\ \hline C0.62 \end{array}$$

57.21

1.95

1.02

F0.07

0+80

$$\begin{array}{r} 54.12 \\ 4.06 \\ 4.67 \\ \hline F0.61 \end{array}$$

$$\begin{array}{r} 53.47 \\ 4.71 \\ 3.98 \\ \hline C0.73 \end{array}$$

$$\begin{array}{r} 53.42 \\ 5.74 \\ 5.86 \\ \hline F0.12 \end{array}$$

2+00

$$\begin{array}{r} 58.59 \\ 0.57 \\ 0.85 \\ \hline F0.28 \end{array}$$

$$\begin{array}{r} 58.94 \\ 0.22 \\ 0.85 \\ \hline F0.63 \end{array}$$

57.89

1.27

1.45

F0.18

0+40

$$\begin{array}{r} 50.17 \\ 8.01 \\ 7.11 \\ \hline F1.10 \end{array}$$

$$\begin{array}{r} 49.52 \\ 8.66 \\ 8.12 \\ \hline C0.54 \end{array}$$

$$\begin{array}{r} 49.47 \\ 9.69 \\ 9.40 \\ \hline C0.29 \end{array}$$

1+80

$$\begin{array}{r} 58.87 \\ 0.29 \\ 0.86 \\ \hline F0.59 \end{array}$$

$$\begin{array}{r} 58.22 \\ 0.94 \\ 0.65 \\ \hline C0.29 \end{array}$$

58.17

.99

1.29

F0.28

0+20

$$\begin{array}{r} 58.18x \\ 48.20 \\ 9.98 \\ 10.80 \\ \hline F0.82 \end{array}$$

$$\begin{array}{r} 58.18x \\ 47.74 \\ 10.44 \\ 10.32 \\ \hline C0.11 \end{array}$$

$$\begin{array}{r} 59.16x \\ 47.87 \\ 11.29 \\ 10.19 \\ \hline C1.10 \end{array}$$

1+60

$$\begin{array}{r} 59.16x \\ 58.73 \\ 0.43 \\ 1.14 \\ \hline F0.71 \end{array}$$

$$\begin{array}{r} 59.16x \\ 58.08 \\ 1.08 \\ 0.71 \\ \hline C0.37 \end{array}$$

58.03

1.13

1.23

F0.10

0+00

$$\begin{array}{r} 49.00 \\ 11.83 \\ \hline \end{array}$$

$$\begin{array}{r} 46.35 \\ 11.83 \\ \hline \end{array}$$

49.04

1+40

$$\begin{array}{r} x 58.18x \\ 58.17 \\ - 0.01 \\ .82 \\ \hline F0.84 \end{array}$$

$$\begin{array}{r} 58.18x \\ 57.54 \\ 0.64 \\ 0.24 \\ \hline C0.40 \end{array}$$

59.16x

57.49

1.67

1.73

F0.06

11

Catalina

A+10 $\begin{array}{r} 59.16X \\ 47.70 \\ 11.46 \\ 12.79 \\ \hline F 1.33 \end{array}$ $\begin{array}{r} 59.16X \\ 47.05 \\ 12.11 \\ 12.00 \\ \hline C 0.11 \end{array}$

N.E. Ret. 4 parts 48.40

3+80 $\begin{array}{r} 48.170 \\ 10.46 \\ 11.24 \\ \hline F 0.78 \end{array}$ $\begin{array}{r} 48.05 \\ 11.11 \\ 10.63 \\ \hline C 0.48 \end{array}$

SiE Ret. 4 parts

3+50 $\begin{array}{r} 49.70 \\ 9.46 \\ 9.56 \\ \hline F 0.70 \end{array}$ $\begin{array}{r} 49.05 \\ 10.11 \\ 9.26 \\ \hline C 0.85 \end{array}$

061 B.C 3+40 $\begin{array}{r} 59.16X \\ 50.35 \\ 8.81 \\ 8.96 \\ \hline F 0.15 \end{array}$ $\begin{array}{r} 49.70 \\ 9.46 \\ 8.75 \\ \hline C 0.71 \end{array}$ $\begin{array}{r} 49.65 \\ 9.51 \\ 9.30 \\ \hline C 0.21 \end{array}$

2+95 $\begin{array}{r} 53.58 \\ 5.58 \\ 5.63 \\ \hline F 0.05 \end{array}$ $\begin{array}{r} 52.93 \\ 6.23 \\ 5.31 \\ \hline C 0.92 \end{array}$ $\begin{array}{r} 52.56 \\ 6.60 \\ 6.42 \\ \hline C 0.18 \end{array}$

46.94X
4+65 Lt. 40.55
cutstake 6.27
5.22
C 1.05 OK Page 27 = C.104
46.82 X

Banning +10.47 +20.94 Catalina
N.E. Ret. 48.40 47.60 46.75 45.70 - A120
-1.58 -0.78 0.07
0.01 0.08 0.36
F 1.59 F 0.86 F 0.29

*59.16
Catalina +10.47 +20.94 Banning
SiE Ret. 49.65 49.00 48.72 49.00
9.51 10.16 10.44 10.16
9.66 10.27 10.26
C 0.50 C 0.19 F 0.10

End Job
5+10 $\begin{array}{r} 34.70 \\ 12.12 \\ 12.73 \\ \hline F 0.61 \end{array}$ $\begin{array}{r} 34.05 \\ 12.77 \\ 12.05 \\ \hline C 0.72 \end{array}$ $\begin{array}{r} 34.00 \\ 12.82 \\ 12.53 \\ \hline C 0.19 \end{array}$

A+65 39.90 39.85
A+60 41.20 6.92 6.97
5.62 5.12 6.85
C 0.05 C 0.12

4+20 45.75 45.70
1.07 1.12
0.40 1.137
C 0.67 F 0.25

Winchester Rough Grade
Sea Breeze to Roanoke

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10-25-48
W.O. 80102

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WK
MAY 16 1949

Sommermeier
McCoy
Allen
Jones

No. Prop.

So. Prop.

Property cut stubs - set to curb grade		No. Prop.	So. Prop.				
2+36	250.63		250.98				
	11.93		11.58				
	10.92		11.51				
	C 1.01		C 0.07				
1+16	245.65	246.14					
	4.99	4.50					
	3.17	2.70		2+16	249.48	249.87	
	C 1.82	C 1.80			13.08	12.69	
					11.74	12.18	
					C 1.34	C 0.51	
0+96	245.26	245.75		T.P.	6.80	262.56	0.88
	3.39	4.89				249.76	
	3.74	1.74		1+96	248.47	248.88	
	F 0.35	C 3.13			2.17	1.76	
					0.88	1.27	
					C 1.29	C 0.49	
0+76	245.01	245.50					
	3.63	5.14		1+76	247.58	248.02	
	6.30	1.38			3.06	2.62	
	F 0.67	C 3.76			1.94	1.58	
					C 1.22	C 1.04	
Prop. E.C.							
0+25	244.50	245.00		1+56	246.81	247.27	
	6.14	5.64			3.83	3.37	
	6.81	2.67			2.79	2.05	
	F 0.67	C 2.97			C 1.04	C 1.32	
E.L. Sea Breeze							
0+00	242.36	245.80		1+36	246.17	246.65	
	8.28	4.84			4.47	3.99	
	8.10	1.02			3.30	2.24	
	C 0.18	C 2.82			C 1.17	C 1.75	
Edgewater + Sea Breeze	5.46	251.64	—	245.18	S.W.B.P.		

Winchester

S. End.
S.W. Ret.
N. End
N.W. Ret.

N.W. Ret Gaviota

4741-
Ctr. Carb
Return

262.11
9.44
8.48
C 0.96

S.W. Ret.

262.19
7.66
5.79
C 3.87

T.P.
Ctr. Carb
Returns

No. Prop.
N.W. Ret.
268.00
3.85
1.62
C 2.23

Calle Serena

So. Prop.
S.W. Ret.
267.11
4.74
6.84
F 2.10

Calle
Serena
Prop. B.C.
2435.04

267.25
4.60
3.17
C 1.43

266.75
3.10
7.62
F 2.52

Prop. B.C
4715.92
261.50
10.35
9.95
C 0.40

So. Prop.
261.50
10.35
7.21
C 3.14

1782.53
266.32
5.53
3.57
C 1.96

265.93
5.92
7.69
C 3.77

3771
258.79
13.06
11.36
C 1.70

258.87
12.78
8.49
C 4.29

1730.02
265.38
6.47
3.23
C 3.24

265.12
6.73
7.25
F 2.52

T.P. 1209 271.85 2.80 259.76
3726 2560.7
6.49
4.60
C 1.89

T.P.
256.74
6.32
2.80
C 3.52

077751 264.44
7.41
2.37
C 5.04

264.31
7.54
8.86
F 1.32

2781 253.35
7.21
8.15
C 1.06

253.61
8.95
6.32
C 2.63

Prop. EC
0725 263.50
8.35
3.10
C 5.25

263.50
8.35
7.62
C 0.73

Ctr. Carb
Returns
Gaviota
N.E. Ret.
263.21
8.64
3.80
C 4.84

S.E. Ret.
262.96
8.89
7.48
C 1.41

262.50

Winchester

N. Prop.

Rate per Ft. = 4.0926'

Def
10°-14'
1+50

284.83
7.10
6.34
C 2.76

Def
6°-49' 11"
1+00

280.22
13.71
10.85
C 2.86

Def.
3°-24'-40"

12.17 293.93 1.03 281.76

0+30

275.61

0+00

7.18

R.C.C. =

4.01

C 3.17

Also = P.C.D.

Prop. E.C.

= 0+00

0+25 =

271.00

Back.

11.79

8.62

C 3.17

N.E. Ret.

Con. dl.

Returns

Colle Sarona

270.12

12.67

9.52

C 3.15

12.50

282.79

1.62

290.23

S. Prop.

284.33

7.60

8.17

C - 1.41

279.72

14.21

12.17

C - 2.04

275.11

7.68

5.63

C 2.05

270.150

12.29

10.15

C - 2.14

S.E. Ret.

268.58

14.21

11.34

C - 2.87

Winchester

N. Prop.

Def. 21°-00'
E.C. 1.88
3+07

295.45

5.99

0.89

C 5.10

Def. 19°-06'

2+80 294.65

6.79

3.51

C 3.28

Def. 17°-44'

2+60 293.75

7.69

4.42

C 3.27

7.86

301.44

0.35

293.58

16°-21'-11"

2+40 292.59

8.85

6.17

C 2.68

15°-00'-20"

2+20 291.14

1.79

87

C 0.92

13°-38'-30"

2+00 289.44

4.49

2.62

C 1.87

49
S. prop.

294.95

6.49

4.74

C 1.75

294.15

7.29

5.16

C 1.93

293.25

8.19

2.60

C 1.59

292.09

1.84

0.35

C 1.49

290.64

3.29

2.09

C 1.20

288.94

4.99

3.85

C 1.14

Winchester
N. Prop.

S. Prop.

Winchester
No Prop.

50
S. Prop.

1/2 Muh.
T.P.A. F.B. 1700-A24

6.54 283.09 283.08

Oct. 10⁰-A1'

4+20 293.35
8.09
5.77
C 2.32

292.85
8.59
8.38
C 0.21

Sly. 1170
Tres Lomes

5+62⁶⁵ 283.92

5.71
5.45
C 0.26

283.00

6.63
6.47
C 0.16

Oct. 7⁰-A8¹-30⁰

4+00 294.36
7.08
4.08
C 3.00

293.86
7.58
7.39
C 0.19

N.E. Ret.

ctr. ab.
Ret.

285.40 Roanoke

4.23
3.37
C 0.86

Oct. 4⁰-56'

3+80 295.08
6.36
2.48
C 3.90

294.58
6.86
6.34
C 0.52

T.P.

Oct.

E.C. 2A⁰-00'

5+12⁶⁸ 287.00

263
221
C 0.42

T.P.

1.11 289.63 12.92 288.52

Oct. 2⁰-0A'

3+60 295.53
5.91
1.86
C 4.05

295.03
6.41
5.71
C 0.70

Oct. 18⁰-A6'-40"

Rate = 8.62' per ft.
B.C.

3+45.65 295.70
5.74
1.17
C 4.57

295.20
6.24
5.57
C 0.67

4+76³⁴ 289.54

11.90
10.48
C -1.42

289.04

12.40
11.93
C -0.67

Oct. 13⁰-33'-20"

3+20 295.65
5.79
0.96
C 4.83

295.15
6.29
4.74
C 1.55

4+40 292.09

9.35
7.34
C 2.01

291.59

9.85
7.60
C 0.25

301.44

Sewer Laterals
Roseville Hqts. BIK 8.

4.69

W.O. 31297
11-23-48

INDEXED
WK
MAY 16 1949

Sommermeier
McCoy
Allen
Jones

M.H. Rinn & Banger = ~~216.34~~

For X check

set from curbs ~~226.11~~

216.65
9.37
~~226.02~~
19
225.83
13.29

0-01
8' So. ch. 216.65
9.37
226.02 X
8' No. ch. 226.02
217.03
6.99 ✓
8.97
41

~~1720~~
50
Check. Area
3105 18' H. 233.59
232.01
-0.02

2+10
Lat #2

219.17
229.50
9.62
4.69
C 4.93

FL. at
prop. 13' Lt. of E Alley

0+10
Lat. #1

13' Rt. of E Alley

226.02
214.28
11.74
9.38
C 7.36

FL. at
prop.

0+00 = Ely line Banger.

Sewer Laterals
BIK AA Ocean Beach.

(57)

11-23-48 (L sheet # 7046)
W.O. 31332

Sommermeier

INDEXED
WK
MAY 16 1949

Lat #2

27.83 X
19.87
7.96
3.36
C 4.60

Lat #1

33.97
24.80
9.17
3.87
C 5.30

1/2 50' W. of Reso. Dr.
on E + W. Alley

3.53 30.44

T.P.

Pole # PH4220

7.08 33.97 0.74 26.89

N.W. B. P.
Bermuda
+ Sunset
Cliff Rd.

6.64 27.83 — 21.19

Alley BIK 21 (Resub BIKs. K+L)

Ter alta.

Orange to El Cajon, between ^{43rd +} El Cajon
 11-30-49
 W.O. 31345

INDEXED

WK
 MAY 16 1949

Summer days
 1900-7
 Alley
 Jones.

		West	East	
			358.49 5.01	
		West	East	
			363.50 2.23	
			359.17 5.89	
BIK 0+60	N.-0.35	360.42 4.63 3.40 C 1.23	360.22 4.83 5.02 F 0.19	365.05X 6.89 358.16 3.06 361.22
0+40	N.-0.30	360.61 4.44 3.42 C 1.02	360.43 4.62 4.54 C 0.08	D-2'
0+30	N.-0.25	360.56 4.47 2.78 C 1.71	360.40 4.65 4.10 C 0.55	D-3'
0+20	N. 0.22	360.40 4.65 2.76 C 1.89	360.28 4.77 4.01 C 0.46	Mark on 1/4 -30
0+0 N.L. Orange		359.80 5.25 5.34 - .05	359.77 5.28 5.32 - .04	
N.W. B.P. 440 + Orange El Cajon Fairmount S.W. B.P.			358.49	
			352.03 out.	

52

		West	East	
3+00	D-2'	355.84 5.38 5.20 C 0.18	361.22 355.64 5.58 4.23 C 1.35	N. 1.18
BIK 2+80	D-2'	356.18 5.04 4.64 C 0.40	355.98 3.24 3.58 C 1.66	N. 1.38
2+36	D-2'	361.22X 357.03 4.19 3.48 C 0.71	356.83 4.39 3.39 C 1.00	N. 1.45
1+92	D-2'	365.05X 357.88 4.17 2.09 C 0.68	357.68 7.37 5.25 C 1.92	N. -0.43
1+48	N. 0.05	358.73 C 3.2 4.96 C 1.36	358.53 6.42 6.13 C 0.39	D-2'
1+04	Cross 5'-	365.05X 359.58 5.47 5.21 C 0.26	359.38 5.67 4.72 C 0.95	Mark on line

Storm Drain South of Market
West of A3rd
Morrison
Blk 13 - Mair-scene Park

W.O. 80131
12/6/49

INDEXED
WK
MAY 17 1949

Sommermeier
McCoy
Jones

Rate of fall = $2 \frac{76}{10}$

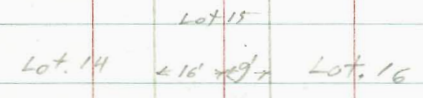
El. 0100 = 122.03 = W. line A3rd

Exist 24"

0100	+10	+10	+60	0180
122.03	121.48	120.93	120.38	119.83
9.92	10.47	11.02	11.57	12.12
7.92	6.95	8.30	8.81	9.72
	C3.52	C2.72	C2.76	C2.40

check, o.k.

S.E. B.P. A3rd + Market
127.54
04.41
13 1.95X



otod = Exist 24"

+ A3rd



Sewer Ext. Lantana Dr.,
Nly. of Dwight.

12-10-48
W.D. 60330

Sommermeier
McCoy
Jones

B Sheet # 3576

Stakes set 6' west
Rate of grade = 3.7%

EL. Exist M.H. =

322.05

But to rim 9.88
Road to 8.56

INDEXED

18.44
340.47

Total Red. = 18.44

WK
MAY 17 1949

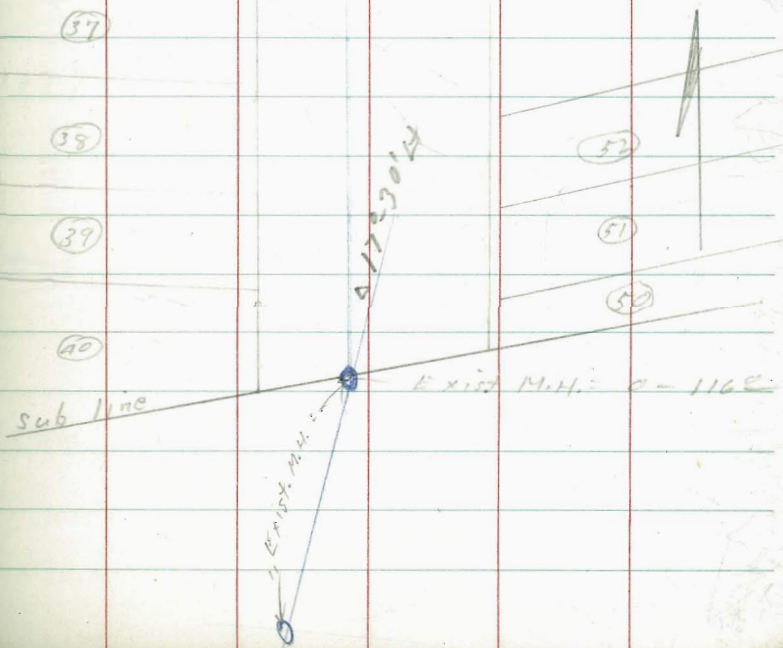
			D.E.
0-116	0400	0427 ^E	0+55
322.05	326.34	327.36	328.38
18.44	14.55	13.53	12.51
	3.97	3.04	2.49
	C 10.58	C 10.49	C 10.07

53

LOT 1
LANTANA DR.

0+55 = Dead End EL. 328.38

EL. 326.34
0400 - Make Conn. to
EXIST D.E. = 0400



Water Services - Thomas Ave.

Events to Dawes.

	South	North
12-16-48		
W.O.#3107A		Sommermeier McCoy Jones
0+82	21.25 ⁺	—
	<u>6.20</u> 6.20	B.M.#1-PG1 26.04 <u>1.41</u> 27.45

INDEXED

WK

MAY 17 1949

0+42	—	22.70 ⁺
		<u>1.75</u> 1.82 C292
0+38	—	22.79 ⁺
		<u>1.66</u> 1.66 C31.00
0+29	22.51 ⁺	—
	<u>4.94</u> 4.76 C0108	
0+25	22.60 ⁺	—
	<u>4.85</u> 4.75 X	

10237

	South	North
1+32	20.05	—
	<u>7.40</u> 6.88 C0.52	
1+28	20.16	—
	<u>7.29</u> 6.70 C0.59	
1+20	—	20.84 ^x
		<u>6.61</u> 5.21 C1.40
1+16	—	20.99 ^x
		<u>6.52</u> 5.07 C1.45
0+97	—	21.39 ^x
		<u>6.06</u> 3.95 C2.11
0+93	—	21.28 [?]
		<u>5.97</u> 3.75 C2.22
0+86	21.16 ⁺	—
	<u>6.29</u> 6.29 X	

27.45
X

0+00 = W. Time Events

Daws to Events

		South		North				
2+30 ^E		—		18.26 ^x		3+14	—	17.18 ^x
				<u>3.90</u>				<u>4.98</u>
				4.16				<u>4.98</u>
				F0.26				x
2+26 ^E		—		18.36 ^x		3+10	—	17.21 ^x
				<u>3.80</u>				<u>4.95</u>
				3.92				<u>4.95</u>
				F0.12				x
2+26		17.86 ^x		—		2+76	17.05 ^x	—
		<u>4.30</u>					<u>5.11</u>	
		4.03					4.86	
		C0.27					C0.25	
2+22		17.94 ^x		—		2+72 cent.	17.16 ^x	—
		<u>4.22</u>					<u>5.04</u>	
		4.00					4.73	
		C0.22					C0.23	
1+90	ork							
1+72		19.11 ^x		22.16		2+72	—	17.59 ^x
		<u>3.05</u>		19.87 ^x				<u>4.57</u>
		2.67		<u>3.29</u>				<u>4.60</u>
		C0.36		2.06				F0.03
				C0.23				
1+68		19.20 ^x		—		2+68	—	17.62 ^x
		<u>2.76</u>		22.16 ^x				<u>4.54</u>
		2.54		19.96				<u>4.47</u>
		C0.42		2.20				C0.07
				1.87				
				C0.31				
T.P.	1.57	<u>22.16</u>	6.88	20.57			<u>22.16</u>	
		27.45					x	

Dawes to Everts S.E. 1/4 Mon. Dawes + Thomas

7.33

+ 0.01
14.93

(14.84)

South

North

4+90 Brk

3+74

16.30
5.86
5.78
C 0.08

—

4+75

15.62
6.54
6.46
C 0.08

—

3+70

16.32
5.84
5.87
x

—

4+71

15.65
6.51
6.51
x

—

3+65

—

16.84
5.32
5.35
F 0.03

4+25

15.95
6.21
6.06
C 0.15

—

3+61
1900'

—

16.87
5.29
5.44
F 0.15

4+22

—

16.47
5.69
5.87
F 0.18

3+26

16.60
5.56
5.41
C 0.15

—

4+21

15.98
6.18
6.02
C 0.16

—

3+22

16.62
5.54
5.87
C 0.15

—

4+18

—

16.50
5.66
5.58
C 0.08

3+20 Brk

22.16

22.16
x

Fanuel to Everts

S.E. Top Hydt. Fanuel + Thomas $\frac{1769}{25} = - 32.18$
 $\frac{32.88}{0.70}$
 $\frac{32.88}{32.88}$

N.W. 1/4 Lt T. Fanuel + Thomas $\frac{29.88}{29.88}$

1705 $\frac{27.95}{4.93}$
 $\frac{4.93}{1.93}$
 X

1701 $\frac{27.99}{4.87}$
 $\frac{4.87}{4.60}$
 $\frac{4.60}{20.29}$

0755 $\frac{28.45}{4.43}$
 $\frac{4.43}{3.75}$
 $\frac{3.75}{20.68}$

0757 $\frac{28.49}{4.39}$
 $\frac{4.39}{3.68}$
 $\frac{3.68}{20.71}$

0710 $\frac{28.90}{3.78}$
 $\frac{3.78}{3.71}$
 $\frac{3.71}{20.27}$

$\frac{29.41}{3.47}$
 $\frac{3.47}{2.90}$
 $\frac{2.90}{20.57}$

INDEXED
 WK
 MAY 17 1949

1781 $\frac{27.19}{5.69}$
 $\frac{5.69}{5.76}$
 $\frac{5.76}{20.07}$

1777 $\frac{27.23}{5.65}$
 $\frac{5.65}{5.67}$
 $\frac{5.67}{20.02}$

1759 $\frac{27.91}{4.97}$
 $\frac{4.97}{5.20}$
 $\frac{5.20}{20.23}$

1755 $\frac{27.95}{4.93}$
 $\frac{4.93}{5.71}$
 $\frac{5.71}{20.78}$

1734 $\frac{28.17}{4.71}$
 $\frac{4.71}{5.35}$
 $\frac{5.35}{20.44}$

1730 $\frac{28.21}{4.67}$
 $\frac{4.67}{5.09}$
 $\frac{5.09}{20.42}$

32.88

Faniel to Events

2+63	$\begin{array}{r} 26.57 \\ 6.51 \\ 6.53 \\ \hline F0.02 \end{array}$	—				
2+59	$\begin{array}{r} 26.41 \\ 6.47 \\ 6.69 \\ \hline F0.22 \end{array}$	$\begin{array}{r} 26.91 \\ 5.97 \\ 6.05 \\ \hline F0.08 \end{array}$	3+82	—	$\begin{array}{r} 25.68 \\ 4.69 \\ 2.37 \\ \hline C2.35 \end{array}$	$\begin{array}{r} 32.88 \\ 6.53 \\ 26.35 \\ 4.02 \\ \hline 30.37x \end{array}$
2+55	—	$\begin{array}{r} 26.95 \\ 5.93 \\ 5.93 \\ \hline \end{array}$	3+78	—	$\begin{array}{r} 25.72 \\ 4.65 \\ 2.41 \\ \hline C2.24 \end{array}$	
2+26	$\begin{array}{r} 26.74 \\ 6.14 \\ 6.41 \\ \hline F0.24 \end{array}$	—	3+47	—	$\begin{array}{r} 26.03 \\ 4.34 \\ 3.06 \\ \hline C1.28 \end{array}$	
2+22 2+00 = 81K	$\begin{array}{r} 26.78 \\ 6.10 \\ 6.42 \\ \hline F0.32 \end{array}$	—	3+44	$\begin{array}{r} 25.56 \\ 4.81 \\ 4.73 \\ \hline C0.08 \end{array}$	—	
1+97	—	$\begin{array}{r} 27.53 \\ 5.35 \\ 5.41 \\ \hline F0.06 \end{array}$	3+43	—	$\begin{array}{r} 26.07 \\ 4.30 \\ 3.07 \\ \hline C1.23 \end{array}$	
1+93	—	$\begin{array}{r} 27.57 \\ 5.31 \\ 5.35 \\ \hline F0.04 \end{array}$	3+40	$\begin{array}{r} 30.37x \\ 25.60 \\ 4.77 \\ 4.64 \\ \hline C0.13 \end{array}$	—	

32.88

Fannual to Everts,

A+68

24.32
6.05
4.79
C 11.26

A+65

24.85
5.52
2.75
C 2.77

A+36

25.14
5.23
2.65
C 2.57

A+32

25.18
5.19
2.45
C 2.74

3+97

25.03
5.34
4.47
C 0.87

3+93

25.07
5.30
5.06
C 0.24

30.37

Fannual to Everts
Water Services

61

12/16/48

SE. 7' Mem
Everts + Thomas

A.33 26.04

B.M.#1

A+72

24.28
6.09
4.85
C 1.24

A+69

24.81
5.56
2.56
C 2.70

30.37

Water Meter grades
Alley Bk. 56 City Hgts

SEE ALSO
PAGE 66

62

Wrightman to El Cajon. Between 37+38

1-17-49
N.W. 31527
Lsheet 7273

INDEXED
W.K.

Samuel Meyer
McCoy
Jones.

LT MAY 17 1949 RT.

So. No So. No

0+55

329.77

6.53

0+51

329.71

6.42

6.59

6.43

6.16

6.11

0+42

329.59

6.71

6.24

0+39

329.54

6.76

6.43

6.33

6.27

0+22

329.01

7.29

6.35

0+18

328.94

7.36

6.20

6.16

6.94

NEW
Service

0+87

330.06

0+84

329.99

6.24

6.79

6.31

7.03

6.55

6.72

336.30

LT.

RT.

So.

No

So.

No

stakes set 9' Lt. or RT of 2 Alley

1+41

332.08

4.22

3.37

1+37

331.93

4.37

3.63

6.74

6.85

1+05

330.53

5.77

1+01

330.40

5.31

5.90

6.46

5.27

6.63

1+03

330.75

5.55

0+99

330.65

5.72

5.65

6.17

5.72

6.07

T.A. Rail in
Pole R3749
N.W.B.P.
37+Wrightman

6.46

33 6.30

9.86

329.84

0.88

339.70

338.82

BK 56 City Hqts
Water Meter Box 83
Lt. RT.

5+99		348.13		
		<u>3.75</u>		
5+95	348.13	3.94		
		<u>3.90</u>		
		3.91		
	F0.90	352.03	2.47	341.13
T.P.				
4+59		<u>339.31</u>		
		4.29		
4+55	339.29	4.39		
		<u>4.31</u>		
		4.44		
	F0.13	F0.05		

INDEXED

WK
MAY 17 1949

4+54

338.99 82 RT of

4.61

4.66

F0.05

4+50

338.97

4.63

5.02

F0.39

4+30

338.88

4.72

4.88

F0.16

4+26

338.86

4.74

4.81

F0.07

3+99

339.04

4.56

3.77

C0.59

3+94

339.02

4.58

3.81

C0.74

343.60

Sewer Lats.
Alley BK 56 City Hqts.

64

Sheet - L 7273

INDEXED

WK

MAY 17 1949

4"
Lat. #1

5+50
15' RT of 2

339.41

12.62

5.51

C 7.11

Pava. 10' RT 2.

4.06

348.97

348.98

352.03

1942

20

Martin St. 31st to 30th

Curb.

INDEXED
WIK
MAY 17 1949

INDEXED
MAY 17 1949

4+18³³ Meats Cl. 59.50

Rake

Brk. 3+19.83 set. d, 12 above 347.83 52.62 Rod 4.78

317.83 52.50 Rod. 4.20 Meats Cl.

Brk. 1+09⁸³ 49.92 48.13 49.82 47.83 Meats.
1.69
1.62
C 0.07
1.99
1.97
0.02

Brk. 0+99⁸³ 48.00 47.59 Meats.
1.82 - set at
1.74 - grade
C 0.08
2.27 - set at
2.15 - grade
C 0.08

Brk. 0+89⁸³ 49.82 47.08 Meats Cl.
2.28
2.21 - Meats
C 0.03
2.74
2.83
-0.09

42.23 = 0.00 Rt. 42.23 = 0.00 Lt.
7.57 7.57
49.82 Lt. 7.57 Vok.

w. Line 31st
0+00

Alloy Bk. 56 City Hgts.

		West	East	
Sly. Univ.				342.42 X 320 339.22 10.65 349.87
6+00		348.13 1.74 1.67 High 0.07	347.98 1.87 2.05 F 0.16	avg. ok. 0-2'
5+90	x-0.10 in	348.11 1.76 0.76 C 1.00	347.90 1.97 2.20 F 0.23	0-2'
5+80	x-0.10 in	347.42 2.45 1.45 C 1.00	347.12 2.75 2.53 C 0.22	0-2'
5+30	x-0.55	342.47 7.40 6.40 C 1.00	342.17 7.70 4.51 C 3.19	0-2'
5+15	x-0.19 in	341.16 8.71 7.71 C 1.00	340.86 9.01 6.46 C 2.55	0-2'
5+00	x-0.58	340.21 9.66 8.66 C 1.00	339.91 9.96 9.19 C 0.78	0-2'
4+85	x-1'	349.87 339.61 10.26 10.14 C 0.12	349.87 339.31 10.56 10.65 F 0.09	0-2'
T.P. Rock				
4+70	0-2'	339.36 3.06 2.95 C 0.11	339.06 3.36 3.98 F 0.62	X-0.4
4+26 ⁶⁵	x-1'	339.16 3.26 2.39 C 0.87	338.86 3.56 3.64 F 0.08	N. -1.85
		342.42 X	342.42	

Sewer Laterals

Silver St. to BIK. 10 - La Jolla Park.

3/27/49
wa. 31334

Sheet 70 82-L

Sommermeier
Allen
McCoy

INDEXED
W.K.
MAY 17 1949

60' East 2' Back 84.16 X
Draper Lat #1 74.68
9.48
1.54
C-4.94

so. side

60' No. 5' Back 90.32
Silver Lat #2 78.14
12.18
6.99
C-5.19

East side

260' so 2' Back 90.32
Pearl. Lat #3 82.74
7.58
1.20
C 6.38

west side

T.P. 7.69 90.32 1.53 82.63

B.M. SW,
Silver
Eads

1.16 84.16 — 83.00

Alley BIK. 116 Mission Beach

4-5-49
W.O. 31363

G252
5-18 For sewers.

Sommermeier
Allen
Jones

Moss & Keating

INDEXED
WIK
MAY 17 1949

	North	±	South
0+90	x-2 1.68	1.43	0-2' 1.68
	5.77		5.77
	5.62		5.66
	C-0.15		C0.11

0+70	x-2' 2.56	2.31	x-2' 2.56
	4.89		4.89
	4.95		4.98
	F0.06		F0.09

0+40	x-2' 4.02	3.77	0-2' 4.02
	3.43		3.43
	3.30		3.57
	C-0.13		F-0.14 out
			F0.65

0+20	Mark -0.06	4.68	0-2' 4.93
	4.93		4.93
	2.52		2.23
	1.29		2.95
	C-1.23		F-0.13 out.
			F0.72

strand way
E Line
0+00

	5.72	5.35	5.76
	1.73-		1.69✓

7.45

B.P. Santa Barbara Pl. + Sea Wall

Sly. cross N.H. Rim
12x10-12

w. line
Mission
Blud.
2+035

	North	±	South
			7.03
			2.43
			9.46
			4.02
			5.44
			2.01
			7.45X

			7.03
			3.59
			10.62
			5.12
			5.50
			1.66
			7.16X

1+80	0-2' -0.10	-0.35	0-2' -0.10
	7.55		7.55
	7.88		7.65
	F0.33		F0.10

1+50	7.16 0.20	0-2' 0.20	0-2' 0.20
	6.96		7.25
	7.71		7.25
	F0.75	F0.45 out.	F0.45

1+30	0-2' 0.50	0.25	0-2' 0.50
	6.95		6.95
	7.50		7.21
	F0.55		F0.26
			F0.28

1+10	0-2' 0.99	0.74	X0.90 0.99
	6.46		6.46
	6.86		6.43
	F0.40		C0.03

7.45

Alley BIK. III Mission Beach,
Pavement.

M.B

70

INDEXED

WK
MAY 17 1949

B.P.
Santa Barb.
+
sea wall

7.03

2.76

9.79

	No.	±	So.
1+20	0.44	0.19	0.44
	<u>9.35</u>		<u>7.35</u>
	<u>9.01</u>		<u>9.24</u>
	C 0.34		C 0.11

No.	±	So.
-----	---	-----

	No.	±	So.
1+00	1.04	0.79	1.04
	<u>8.75</u>		<u>8.75</u>
	<u>8.47</u>		<u>8.32</u>
	C 0.28		C 0.43

Wily. Mission Blvd

250 39 So.

246 9A No

X-in ob.		X-in ob.
-0.40	-0.65	-0.40
<u>10.19</u>		<u>10.19</u>
<u>10.12</u>		<u>10.05</u>
C 0.07		C 0.14

	No.	±	So.
0+80	1.87	1.62	1.87
	<u>7.92</u>		<u>7.92</u>
	<u>7.88</u>		<u>7.65</u>
	C 0.04		C 0.27

2+20

No.	±	So.
0.31	-0.56	0.31
<u>10.10</u>		<u>10.10</u>
<u>9.80</u>		<u>9.85</u>
C 0.30		C 0.23

	No.	±	So.
0+50	3.27	3.02	3.27
	<u>6.52</u>		<u>6.52</u>
	<u>6.10</u>		<u>6.23</u>
	C 0.42		C 0.29

1+90

No.	±	So.
0.21	-0.46	0.21
<u>10.00</u>		<u>10.00</u>
<u>9.78</u>		<u>9.90</u>
C 0.22		C 0.10

	No.	±	So.
0+20	4.67	4.42	4.67
	<u>5.12</u>		<u>5.12</u>
	<u>3.86</u>		<u>4.67</u>
	C 1.26		C 0.45

1+60

No.	±	So.
0.12	-0.37	0.12
<u>9.91</u>		<u>9.91</u>
<u>9.80</u>		<u>9.57</u>
C 0.11		C 0.34

E. Line strand way

	No.	±	So.
0+00	5.75	5.35	5.75
	<u>4.04</u>		<u>4.04</u>

1+40

No.	±	So.
0.05	-0.20	0.05
<u>9.74</u>		<u>9.74</u>
<u>9.39</u>		<u>8.94</u>
C 0.35		C 0.80

Alley BIK 108 Mission Beach
 B.P.
 Santa Barb.
 + Sea wall

INDEXED

WK
MAY 17 1949

	North	±	South	
1+20	x-2' 0.120 8.47 8.59 F 0.12	x-2' 0.04 8.63 8.59 C 0.04	x-2' 0.04 8.63 8.59 C 0.59	703 164 8.67x 0.120 8.47 8.04 C 0.43
1+00	x-2' 0.62 8.05 7.92 C 0.13	x-2' 0.50 8.17 7.92 C 0.25	x-2' 0.50 8.17 7.92 C 0.38	0.62 8.05 7.92 C 0.26
0+80	x-1 1.31 7.36 6.82 C 0.54	x-1 1.22 7.45 6.82 C 0.63	D-3' 1.22 7.45 6.82 C 1.01	1.31 7.36 6.82 C 0.72
0+60	N. -0.91 2.25 6.42 5.46 C 0.96	D-2' 2.21 6.46 5.46 C 1.00	D-2' 2.21 6.46 6.00 C 0.46	2.25 6.42 6.00 C 0.42
0+40	D-2 3.46 5.21 4.81 C 0.40	3.26 3.46 5.21 4.50 C 0.71	D-2' 3.46 5.21 4.50 C 0.71	
0+20	D-2' 4.82 3.93 C 0.89	4.59 4.59 3.69 C 1.15	D-2' 4.84 3.69 C 1.15	
Ely Strand Way 0+00	6.19 2.48	5.81	6.23 2.44 ✓	

867

66. line -0.50
 9.17

4/20/49
 2nd change

05171
 9.18

	North	±	South	
190 ±	x-2' -0.23 8.90 8.52 C 0.38	x-2' -0.71 9.38 8.52	x-2' -0.48 9.47 8.62	Vol. by Mission Blvd x-on db. -0.23 8.90 8.52 C 0.38
2+60	D-2' -0.22 8.89 9.11 F 0.22	D-2' -0.63 9.30 9.11 C 0.19	D-2' -0.63 9.30 9.11 C 0.19	-0.22 8.89 9.11 F 0.22
2+30	D-2' -0.16 8.83 9.10 F 0.27	D-2' -0.51 9.18 9.00 C 0.08	x-1' -0.51 8.18 9.04 C 0.14	-0.16 8.83 9.10 F 0.27
2+00	D-2' -0.10 8.77 9.19 F 0.42	D-2' -0.39 9.06 9.19 F 0.13	D-2' -0.39 9.06 9.30 F 0.24	-0.10 8.77 9.19 F 0.42
1+70	D-2' -0.04 8.71 9.39 F 0.68	D-2' -0.27 8.94 9.39 F 0.45	D-2' -0.27 8.94 9.15 F 0.21	-0.04 8.71 9.39 F 0.68
1+40	x-2' +0.02 8.65 8.83 F 0.18	x-2' -0.15 8.92 8.53 F 0.01	D-2' -0.18 8.92 9.01 F 0.19	+0.02 8.65 8.83 F 0.18

867

Santa Barbara Place - Pave.

INDEXED

WK
MAY 17 1949

	North	±	South
1+20	0-2' 0.51 <u>7.39</u> 7.82 F0.43	0.27	N.-0.12 0.51 <u>7.39</u> 6.88 C0.51
1+00	0-2' 0.98 <u>6.92</u> 6.93 F0.01	0.74	M.-0.10 0.98 <u>6.92</u> 6.52 C-0.40
0+80	0-2' 1.72 <u>6.18</u> 5.83 C0.35	1.48	0-2' 1.72 <u>6.18</u> 5.73 C-0.45
0+60	X-1' 2.73 <u>5.17</u> 4.76 C-0.41	2.49	0-2' 2.73 <u>5.17</u> 4.65 C-0.52
0+30	0-2 4.35 <u>3.55</u> 3.27 C 0.28	4.06	0-2 4.37 <u>3.53</u> 3.34 C- 0.19
Ely. Strand Way 0+00	5.97 <u>1.73</u>	5.63	6.02 <u>1.88</u> 1.71 -0.03
	7.90X		

	North	±	South	72
Wly. Mission Blvd. 2+65 ⁵⁸ ±	-0.17 <u>8.07</u>	-0.39	-0.13 <u>8.03</u> 8.05 -0.02	B.M. 7.03 0.07 <u>7.90X</u>
2+50	N.-1.75 -0.01 <u>7.91</u> 7.53 G0.38	-0.25	0-2' -0.01 <u>7.91</u> 8.35 F0.44	
2+28	N.-1.73 0.07 <u>7.83</u> 7.67 C-0.16	-0.17	0-2' 0.07 <u>7.83</u> 8.28 F0.45	
2+06	0-2' 0.13 <u>7.77</u> 8.37 F0.60	-0.11	0-2' 0.13 <u>7.77</u> 8.47 F0.70	
1+84	0-2' 0.19 <u>7.71</u> 8.23 F0.52	-0.05	0-2' 0.19 <u>7.71</u> 8.34 F0.63	
1+62	0-2' 0.26 <u>7.64</u> 8.14 F0.50	0.02	0-2' 0.26 <u>7.64</u> 8.40 F0.76	
1+40	0-2' 0.32 <u>7.58</u> 8.24 F0.66	0.08	N.-0.22 0.32 <u>7.58</u> 7.55 C-0.03	

± Grades. Alley BIK 7

City Hqts.

N.O. 3109A

7002-L

Sammermeyer

A-1A-A9

± Stakes set to

subgrade

INDEXED

WK

MAY 17 1949

4+90

299.50

2.77 ✓

4+70

299.2A

3.05 ✓

Reko

301.96
3)
302.29
Sub. Dist

0+80

293.31

3.56 ✓

0+50

292.72

4.15 ✓

0+20

291.85

5.02 ✓

0+00

296.87 = X Sub. Dist

33
296.54

Meat

291.17

5.37

6+20

(Meat)

295.57

6.72

32

6.39 ✓

73

6+05

296.29

6.00 ✓

S.E. B.P. Maple 4

Boundary = 295.12

1.42

296.54

3.56

5+95

297.71

4.58 ✓

296.54

+ .33

292.98

8.78

296.87

301.96

X for

subgrade

5+80

298.74

3.55 ✓

5+65

299.39

2.70 ✓

5+50

299.65

2.64 ✓

5+30

299.70

2.59 ✓

5+10

299.65

2.64 ✓

Sewer Extension Blk. 74 point

Loma Hgts

Between Del Mar + Orchard

0+00 = 40' Ely from Ely line Santa Barbara

5/2/49

W.D. 60138

INDEXED

W.K.
MAY 17 1949

Sommermejer
McCoy
Allort
Jeros

True elevations as set,

use opposite page for

0+70 = Santa Barbara

245.54	245.56
12.05	12.05
4.68	4.70
C-7.37	C-7.35

0+46^E

245.37
12.24
4.90
C-7.34

0+23^E

0.87

245.18
12.43
5.45
C-6.98

0+00 = Existing Sewer

244.97	G 169
12.62	7
12.1	

257.61

INDEXED

244.79 Exist pipe (Assumed correct)

12.62
257.61
7.44

250.17 = S.W.B.P. orchard & Santa Barbara (E.L. = 250.36)

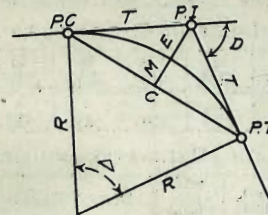
250.36
7.44
257.80 = true K

Santa Barbara

0+00	+23.3	+46 ^E	0+70
245.18	245.37	245.56	245.75
12.62	12.43	12.24	12.05
Exist	5.45	4.90	4.70
	C-6.98	C-7.34	C-7.35

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers } \frac{\Delta}{2}$ (5) (6)
- External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (7) (8) $= R \text{exsec } \frac{\Delta}{2}$ (9)
- Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction=.36 or $T = 414.85$ ft. P. C.=Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.=Sta. P. C.+ $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= $158 - \text{Sta. P. C.} = 54.50$, hence offset= $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve=.3 $\times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction=.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

spatz

354

48165
30799
3777

8750
8384
246

Alleys: B/k ^S 52-^{N.} 71-^{N.} 72

Shirley ^S 277 Place (B/k 51)

1634 1673 1671
967 798 936
2602 2512 2867

1634
967
2611

349.13 ^S 347.77 Rt. B/k 50 ditto 49
1902

67
10.40
3.50
71.90
14.57
5743

9400
274
9130

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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