

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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INDEXED
to page #68
except pages #1 & 57

MICROFILMED

APR 13 1965

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Walker
Johnson
Allen
6-15-48

GRADES - Proposed Sewer
on Horton (St.) AVENUE

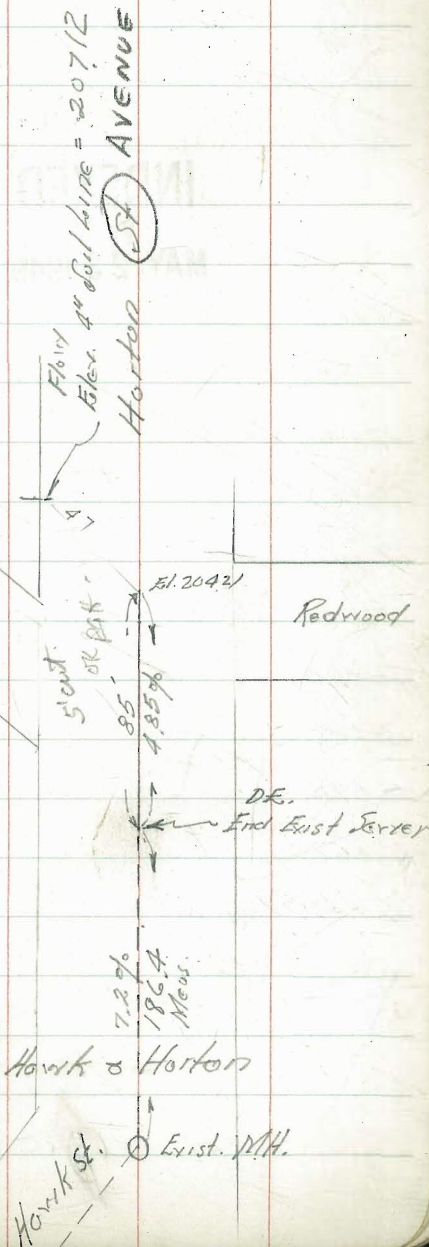
From East DE. to Redwood

110 60 275

INDEXED
WK
MAY 23 1949

			Elev.	Flow Line	Cuts.	offsets
	343		207.12			
+85 = 3.5' South of E Redwood	1.34	209.21	204.21	5.00	4' Rt.	
+60	2.09	208.46	202.76	5.70	"	
+30	3.28	207.27	201.30	5.97	"	
0+00	4.80	205.75	200.08	5.67	"	
0+00 Flow Exist. 6" Sewer	10.47	200.08	200.08			
TP	8.36	210.55	1.04	202.19		
	16.63	203.23		186.60		

B.M. Flow Line M.H. Hawk & Horton
017



Walker GRADES - El Cerrito Storm Drain
 Johnson
 Allen Vale Way, 60th St., Estelle St.
 Gregory College Way and Public Hqs. of Way.
 6-23-48 Plan 7164, 7165, 7166, 7167-1

Stations Elev. Flow line Cuts offsets

INDEXED
WIK
MAY 23 1949

18+00	4.47	417.63	410.40	7.23	
17+65	4.20	417.90	410.58	7.32	
17+30	3.87	418.23	410.76	7.47	10' 4"
17+20.25' F.C.	3.86	418.24	410.81	7.43	10' 4"
17+20.25' F.C.	3.26	418.84	410.81	8.03	6' 4"
17+10	3.15	418.95	410.86	8.09	"
17+00	3.03	419.07	410.91	8.16	"
16+90	2.96	419.14	410.96	8.18	"
16+80	3.44	418.66	411.01	7.65	"
16+70	3.35	418.75	411.06	7.69	"
16+60	3.25	418.85	411.11	7.74	"
16+42.57' B.C.	2.83	419.27	411.16	8.11	6' 4"

3.44 132.10 418.66

El Carrizo Storm Drain

Station			El. Flow Line	Cuts	
22+25		1.73	408.55	402.85	5.70
22+00		1.21	409.07	408.15	5.92
T.P.	1.09	410.28	12.91	409.19	
21+75 - Bk.		12.55	409.55	403.45	6.10
21+40		11.79	410.31	404.43	5.88
21+35 - B. Cleanout		11.76	410.34	404.57	5.77
21+05		11.14	410.96	405.40	5.56
20+88.04 } Equation					
21+17.26 } Equation		10.80	411.30	405.87	5.43
21+00		10.43	411.67	406.12	5.55
20+65		9.70	412.40	406.65	5.75
20+30		9.05	413.05	407.18	5.87
19+95		8.41	413.69	407.71	5.98
19+61.80 = F.C.		7.70	414.40	408.21	6.19
+46.20		7.37	414.73	408.45	6.28
19+31.34 - B.C.		7.12	414.98	408.67	6.31
19+00		6.44	415.66	409.14	6.52
18+62		5.75	416.35	409.71	6.64
18+24.91 $\Delta H = 12^{\circ} 21'$		4.80	417.30	410.28	7.02
18+24.91		4.76	417.34	410.28	7.06

10' H. "Rd" to Forward Turn

10' H. "Rd" " Back "

422.10

El Carrito Storm Drain

5

Stations			El. Flow line	Cuts	offsets.
28+16.68		6.48	397.12	391.73	5.39
28+00.04		6.19	397.41	392.06	5.35
27+83.41 RC.		5.86	397.74	392.31	5.43
27+50		5.19	398.41	393.05	5.36
T.P.	4.40	403.60	11.08	399.20	
27+15		11.23	399.05	393.74	5.31
26+80		10.53	399.65	394.43	5.22
26+45		9.91	400.37	395.12	5.25
26+10		9.19	401.09	395.81	5.28
25+75		8.50	401.78	396.50	5.28
25+40		7.89	402.39	397.19	5.20
25+05		7.14	403.14	397.88	5.26
24+70		6.47	403.81	398.57	5.24
24+35		5.87	404.41	399.26	5.15
24+00		5.20	405.08	399.95	5.13
23+65		4.56	405.72	400.64	5.08
23+30		3.78	406.50	401.33	5.17
22+96 = ^{pk} Cleanout #6		3.17	407.11	402.00	5.11
22+60		2.48	407.80	402.43	5.37

410.28

El Cerrito Storm Drain

			El. Flow LITE	Cuts.	Offsets.
5					
32+50		722	393.01 385.86	7.15	10' Rt.
32+15		729	393.01 386.28	6.73	"
31+20		667	393.63 386.58	7.05	"
31+80		647	393.83 386.70	7.13	"
31+45		606	394.24 387.12	7.12	✓
31+10		504	395.26 387.54	7.72	"
30+75		466	395.64 387.96	7.68	✓
30+40		417	396.13 388.38	7.75	✓
+12.5		348	396.82 388.71	8.11	✓
30+05		338	396.92 388.80	8.12	✓
29+70		309	397.21 389.22	7.99	✓
29+35		330	397.00 389.64	7.36	✓
29+04.84 = Δ		382	396.18 390.00	6.48	10' Lt.
	3.66	400.30	396.64		
			BM Nail 2816689 10' Lt.		
			0.01		
	FB 1825-P-20		397.76		
	Chk Nail 2812516	6.43	397.17		
28+66.59 = E.C.		6.76	396.64 390.76	5.88	
+4994		6.81	396.79 391.08	5.90	
28+33.3'		6.69	396.91 391.41	5.71	
				5.50	

403.60

32 + 16.7 = End of Pipe	10.50	389.80	385.06	4.74
32 + 86	9.99	390.31	385.43	4.88
32 + 55	7.32	392.98	385.80	7.18

400.30

El. Cerrito Storm Drains

Grades - Sewer laterals

Lateral No 55

El.

Flow Line

Cuts. offsets.

0+20	INDEXED	12.69	409.41	404.80	4.61	5'4"
0+15	WK	12.85	409.25	404.30	4.95	"
0+07.5	MAY 23 1949	12.88	409.22	402.30	6.92	"
0+01.5		12.86	409.24	402.10	7.14	5'4"
0+00						

02

04

Lateral No 57

20+09

El.

Flow Line

0+20 = HCB Vole Vlog		8.48	413.62	407.80	5.82	on curb
0+15		9.01	413.09	407.40	5.69	5'4"
0+07.5		8.90	413.20	406.40	6.80	"
0+01.5		8.87	413.23	406.20	7.03	"

0+00 = East Sewer

Lateral No 20

0+72						
0+62 = HCB Estelle		3.91	418.19	413.90	4.29	on curb
0+33		5.01	417.09	413.7	3.39	5'4"
0+04		4.77	417.33	413.5	3.83	5'4"
0+00						

3.44 422.10 418.66

El. Carrito Form Drain

Grades Sewer Laterals

24153 Lateral No 71

			El. Flow Line	Cuts:	Offsets.
0+20	5.81	404.47	399.80	4.67	1/2 on curb, 1/2 on Drive
0+15	6.11	404.17	399.40	4.77	
0+07.5	6.25	404.03	397.90	6.13	
0+01.5	6.33	403.95	397.70	6.25	
0+00			396.60		

23190 Lateral

0+20	4.33	405.95	400.90	5.05	
0+15	4.27	405.31	400.40	4.91	
0+07.5	5.02	405.26	399.00	6.26	
0+01.5	5.20	405.08	398.80	6.28	
0+00			398.00		

22106 Lateral No 54

0+20	1.56	408.72	404.80	3.92	
0+15	1.62	408.59	404.30	4.29	
0+07.5	1.69	408.59	402.00	6.59	
0+01.5	1.64	408.64	401.80	6.84	
0+00					

T.P. 1.09 410.28 12.91 409.19

43210

El Carrito Storm D10112
Sewer laterals

	27+54.5 27+59 - Sewer lateral #80	El. Flow line	Cuts	offsets
0+20	421 399.39	394.40	4.99	5' 11"
0+15	485 398.75	393.70	5.05	"
0+07.5	520 398.40	392.00	6.40	"
0+01.5	539 398.21	391.80	6.41	"
0+00		391.00		

T.P. 440 403.60 11.08 399.20

	13 26+75 - Sewer lateral			
0+20	833 401.95	397.00	4.95	1/2 on curb
0+15	896 401.32	396.50	4.82	5' 11"
0+07.5	918 401.10	394.70	6.40	"
0+01.5	934 400.94	394.50	6.44	"
0+00		393.70		

	25+78 Lateral #70			
0+20	705 403.23	397.80	5.43	"
0+15	760 402.68	397.40	5.28	"
0+07.5	767 402.61	396.20	6.41	"
0+01.5	785 402.43	396.0	6.43	"
0+00		395.10		

410.28

San Gabriel Carrito Storm Drain
Grades - Sewer laterals

INDEXED
WK
MAY 23 1949

			E./ Flow		Cuts	offsets	
	28+06	lateral # 79					
0+20			5.00	398.60	392.86	5.74	End cb.
0+20	Flow		10.74	392.86	392.86	0.00	5.4.
0+15			5.74	397.86	392.06	5.80	5.2.
0+07.5			6.07	397.53	390.90	6.63	"
0+01.5			6.30	397.30	390.70	6.60	"
0+00							

40360

El Cerrito Stern Drain				13	
Stations	Grades	EL. Flow Line		Cuts	Offsets
		0.02			
16+49.57-B.C.	8.15	419.27 419.29	ck.		
16+45.57	8.13	419.31	411.18	8.13	10' Lt
16+35.57-E.C.	8.03	419.41	411.37	8.04	
16+26.73	7.99	419.45	411.55	7.90	
16+17.89	7.74	419.70	411.73	7.97	
16+09.06	7.49	419.95	411.91	8.04	
16+00.23-B.C.	7.47	419.97	412.09	7.88	10' Lt.
15+75	5.51	421.93	412.59	9.34	✓
15+40	5.30	422.14	413.29	8.85	
15+05	4.79	422.63	413.99	8.64	
14+70	4.67	422.77	414.69	8.08	
14+35	4.15	423.29	415.39	7.90	
14+00	3.07	424.37	416.09	8.28	
13+65	2.36	425.08	416.79	8.29	
13+30	1.71	425.73	417.49	8.24	
12+99.34-E.C.	0.52	426.92	418.20	8.72	7' Rt.
B.M.	8.78	427.44	418.66	N.W.B.P.	60th E Estelle

El Cerrito Storm Drain
 Stations Grades Elevation
 Flow line

Cuts Offsets

Alley West of 60th St.

Cont on P. 20

Stations	Grades	Elevation Flow line	Cuts	Offsets
2+50 ^{BK} TP 7.57	432.57	0.28 425.00	413.68	5.32 6' LT
2+15		1.25 424.03	418.63	5.40 "
1+80		2.27 423.01	417.58	5.43 "
1+42.87		3.91 421.37	416.47	4.90 "
1+25 ^{BK}		4.69 420.59	415.93	4.66 6' LT
0+85.57		4.90 420.18	413.86	6.32 "
0+69.57 = E.C.		5.09 420.29	413.02	7.22 "
0+60.76		5.08 420.20	412.56	7.64 "
0+51.93		5.36 419.92	412.16	7.76 "
0+43.10		5.53 419.75	411.64	8.11 "
0+34.27 = B.C.		5.89 419.44	411.18	8.22 6' LT

B.M. 6.62 425.28 418.66

N.W.B.P. 60th & Estelle

Stations	El. Cerrito Storm Drain	Grades	Elevations Flow Line	Cuts	Offsets
4+35		3.60	449.08 442.25	6.83	10' RT.
4+00		0.41	452.27 444.70	7.57	5' RT.
T.P.	1.26	452.68	10.34 451.42		
3+62.50 Bk.		7.95	453.81 446.95	6.86	1.94 RT.
3+25 Bk.		6.28	455.48 448.64	6.84	10' RT.
2+87.50 Bk.		5.13	456.63 449.95	6.68	10' RT.
2+45.01		3.48	458.28 450.98	7.30	8' RT.
T.P.	2.89	461.76	9.31 458.87		
2+02.52 #1	Curb inlet		9.31 458.87 452.00	6.87	10' RT.
1+69.74		8.48	459.70 452.33	7.37	"
1+37.5 Bk.		8.68	459.50 452.65	6.85	"
1+12.5 Bk.		8.26	459.92 453.28	6.64	"
0+87.5 Bk.		8.46	459.72 454.40	5.32	"
0+62.5 Bk.		8.55	459.63 456.03	3.60	"
0+36.3	End of inlet Pipe		4.73 463.45 458.28	5.17	10' RT.
B.M.	2.91	468.18	465.27	N.W.B.P.	College & El Cajon

Stations	El. Cervito Grades	Stems	Drain	Elevation Flow line	Cuts	Offsets
7+21.6 ✓		7.79	436.69	429.65	7.04	
7+09.86		7.38	437.10	429.89	7.21	
7+05.5		7.10	437.38	429.98	7.40	
6+98.08		6.68	437.80	430.13	7.67	
6+86.30		5.96	438.52	430.37	8.15	
6+74.52		5.48	439.00	430.60	8.40	
6+62.74-8C.		5.05	439.43	430.84	8.59	
4.2.8	444.48		440.20		on Hub	
			.01 ck. 440.20			
check on Hub 6+62.74 = B.C. ckt 2		5.02	440.21	440.20		
6+61 BKK.		5.80	439.43	430.87	8.56	10' RT
6+24.25		6.70	438.53	431.97	6.56	10' RT
5+87.50		6.61	438.62	433.07	5.55	10' RT
T.P.	5.81	445.23	13.26	439.42		
5+50 BKK.		13.26	439.42	434.57	4.85	10' RT ✓
5+12.5 BKK.		9.54	443.14	436.82	6.32	10' RT
4+91.25		7.40	445.28	438.51	6.97 6.37	10' RT
4+70		5.82	446.86	439.80	7.06	10' RT
	452.68					

Station

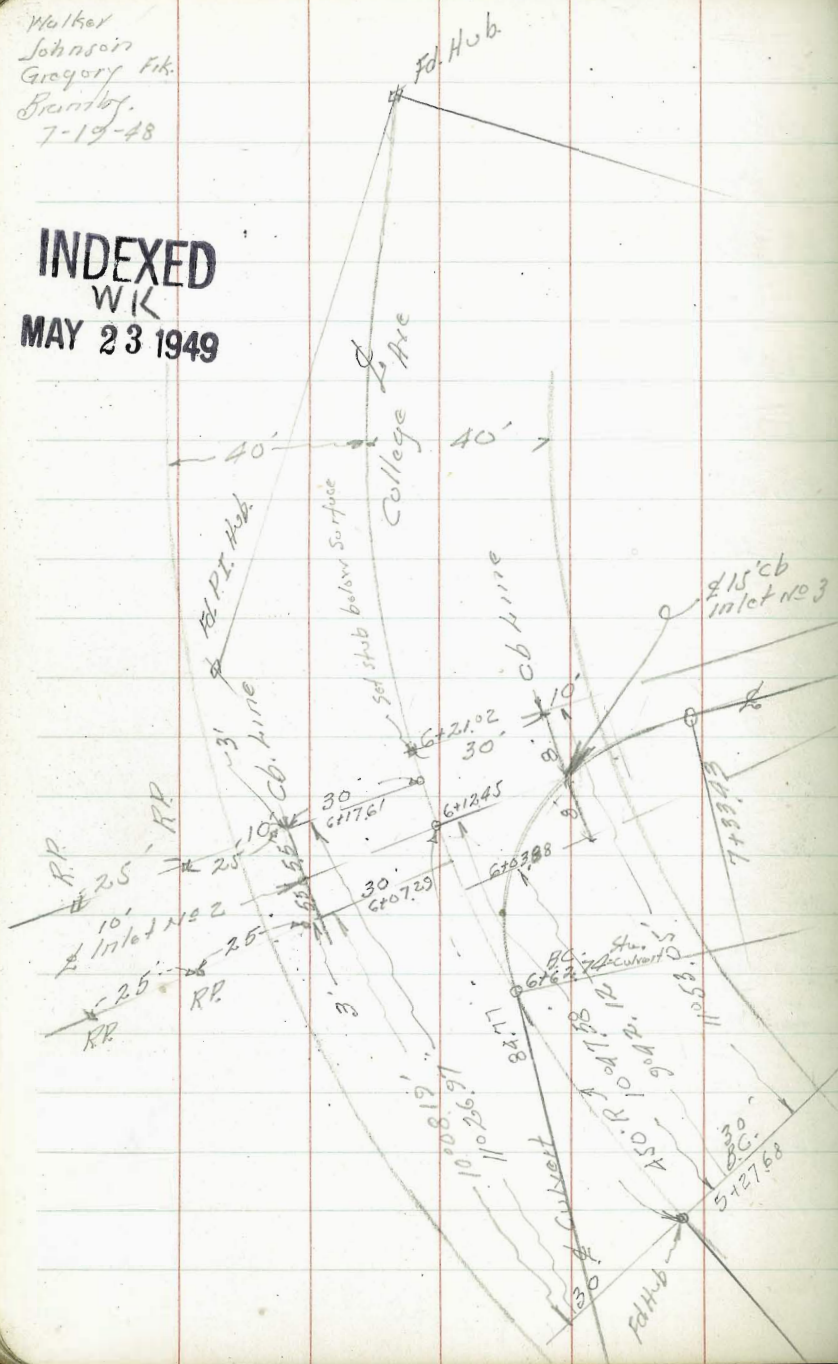
			El. Floor Line	Cuts	offsets
11+00		6.04	428.62	422.09	6.53
10+65		5.05	429.61	422.79	6.82
T.P.	4.86	434.66	1319	422.80	
10+30		13.19	422.80	423.49	6.31
9+95		11.36	431.60	424.19	7.41
9+60		9.66	433.33	424.89	8.44
9+30		8.05	434.24	425.49	9.45
9+08.73 = E.C.		6.91	436.08	425.92	10.16
8+96.26		6.14	436.85	426.15	10.70
8+85.19		6.46	436.53	426.39	10.14
8+73.41		5.99	437.00	426.63	10.37
8+61.65		5.79	437.20	426.86	10.34
8+49.87		6.01	436.98	427.10	9.88
8+38.10 = B.C.		6.73	436.26	427.33	8.93
8+00		6.76	436.23	428.09	8.14
T.P.	6.73	442.99	8.22	436.26	
7+65		7.69	436.79	428.79	8.00
7+33.43 E.C.		8.00	436.48	429.42	7.06

Cont. from P.

44448

Walker
Johnson
Gregory Fk.
Bramby.
7-19-48

INDEXED
WIK
MAY 23 1949



El Cerrito Storm Drains 18
Ties to Cb inlets No 2 and No 3

Stations

Elev.
Flowline

Cuts

offsets

			428.38		
FB. 1825-11 Chk. E. Hub 12+29.64	6.23	428.43			
12+24.34	7.68	426.98	418.20	872-4.13 8.78	
12+82.56	7.31	427.35	418.44	8.91	
12+70.78	6.85	427.81	418.67	7.14	
12+58.95	6.23	428.43	418.95	9.48 ✓	
12+46.30	5.91	428.75	419.14	9.61 ✓	
12+35.33	5.95	428.71	419.38	9.33 ✓	
12+23.64 BC 45K	5.73	428.93	419.61	9.32	
11+92.64	6.03	428.63	420.23	8.40	
11+61.65 = 2 Cleanout	5.92	428.74	420.85	7.89	
11+30	6.10	428.47	421.49	6.98	

434.66

El Cerrito Storm Drain
in Alley West of 60th

Station

El.
Flow line

Cuts. Offsets

Station	El.	Flow line	Cuts.	Offsets
		0.01		
Chk. Hub 5+34.80 FB. 1825-P-29	7.50	425.06 425.07		
4+81.57	8.69	423.88	422.00	1.88 6'lt.
4+60	8.65	423.92	421.78	2.14 "
4+25	7.20	425.37	421.43	3.94 "
3+90	6.12	426.45	421.08	5.37 "
3+55	5.89	426.68	420.73	5.95 "
3+20	5.87	426.70	420.38	6.32 "
2+85	6.62	425.95	420.03	5.92 "
2+50 = Bk	432.57	419.68		
	Cont. from P. 14			

El. Carrito Storm Drain
 Slope Stakes For Ditch
 from End Pipe 32116.7

2

21

1+00

384.50
 12.5

12.5
 10.1
 C 24

10.1
 9.0
 +1.1
 30

0+50

384.75
 12.3

12.30
 8.1
 C 4.2

RP.
 8.1
 7.1
 +1.0
 30

0+00

12.08 384.97 384.97

1.38 397.05

395.67

8-18-48
Hendricks
Roberts
Greer
Rorer

Stake Cb Inlets #11 & 12 & 10
El Cerrito Storm Drain
(Drawing # 71664)

(27)

INDEXED

WK
MAY 23 1949

Grade Next Page

VOID

Set Hub

Cb R. = 113.3
 $\Delta = 58^{\circ} 21' 45''$

30.1475
Cb Inlet
#10 15' Inlet
29.9975

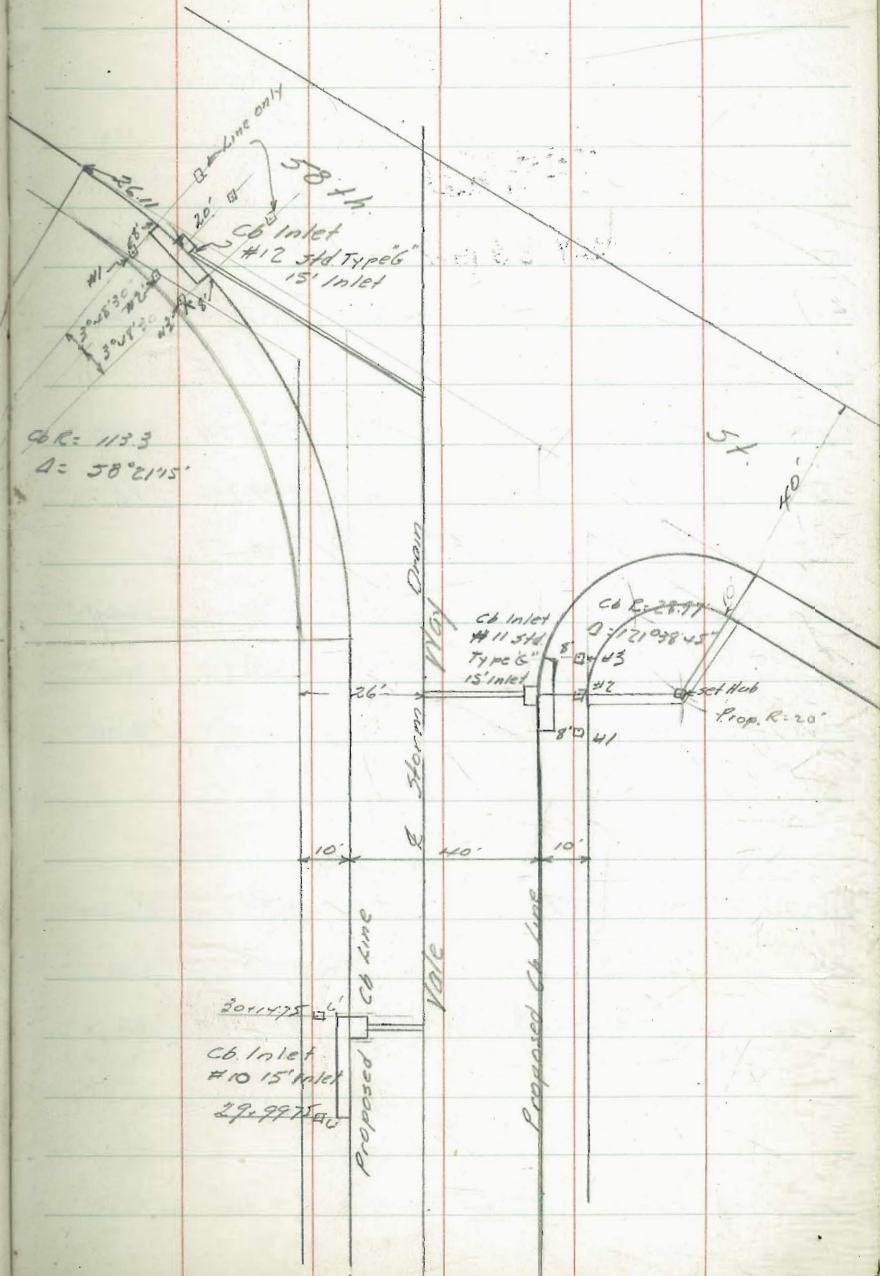
Proposed Cb Line
Storm Drain
Vale
Proposed Cb Line

Cb Inlet
#11 std
Type 6"
15' Inlet

Cb R. = 28.77
0.7219945
8.0443

Set Hub
Prop. R. = 20

10' 10' 10'

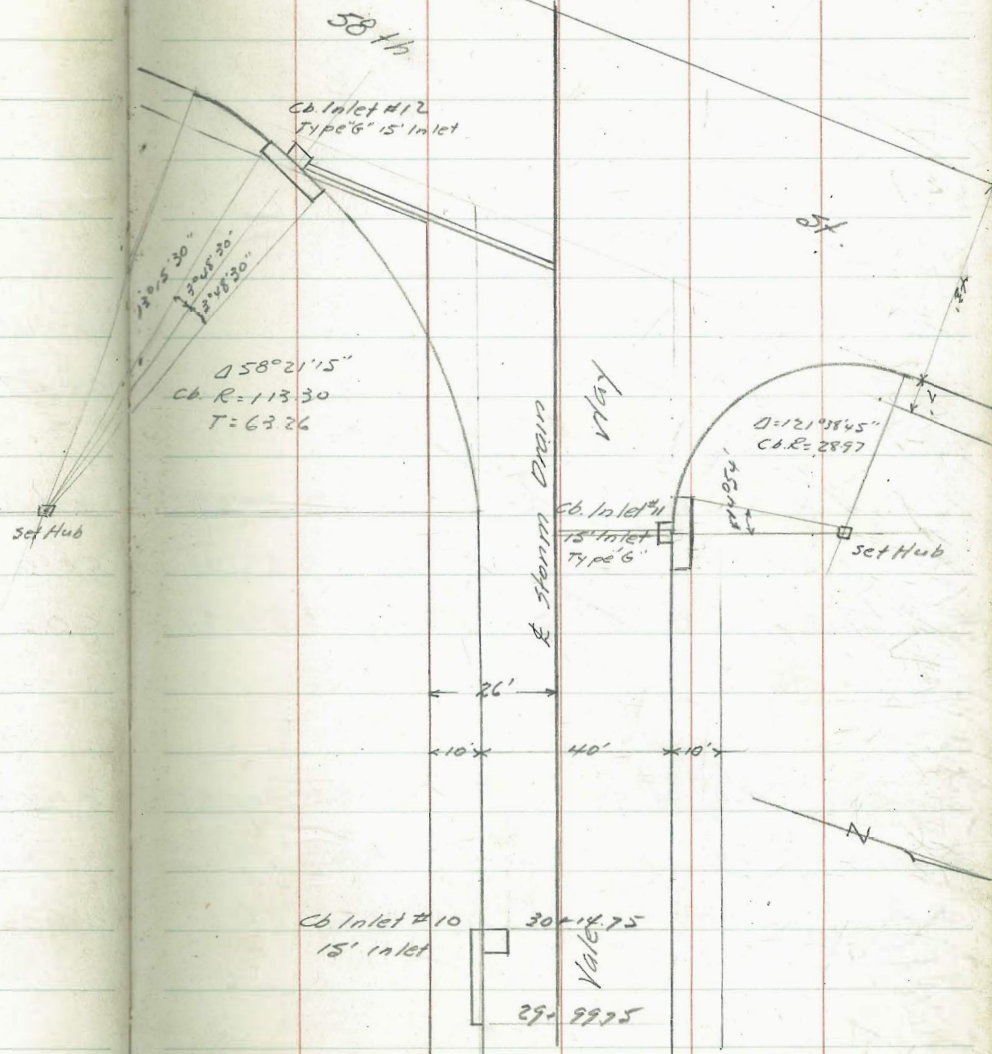


Grades of Inlets No 11 & 12 & 10
El Cerrito Hills.

Sta.		H. I.	-	Elev. Stakes	Cb. Grade	Cut or Fill	Offset
Ck B.M.			4.55	395.75	395.75		Starting B.M.
West End Inlet #10			3.56	396.74	396.60	C0.14	6' Lt
East End Inlet #10			3.16	397.14	396.73	C0.41	6' Lt.
TP	3.73	400.30	0.98	396.57			
West End Inlet #11 (23)			3.15	394.40	394.35	C0.05	6' Rt
W Inlet #11 (22)			3.21	394.34	394.23	C0.11	6' Rt
East End Inlet #11 (21)			2.91	394.64	394.34	C0.30	6' Rt
Void #11 & 12							
No Line Inlet #12 (23)			4.32	393.23	392.60	C0.63	8' Lt.
W Inlet #12 (22)			4.84	392.71	392.53	C0.18	8' "
So End Inlet #12 (21)			4.89	392.66	392.60	C0.06	8' "
B.M.	1.80	397.55		395.75			B.M. P.O.I.C # 178269 on 58th St. to Linc Valet Way (FR 1825 - P. 31)

8-19-48
Hendricks
Roberts
Greer
Rorer

State Curb Inlets - #110212
El Cerrito Storm Drain
(Dwg # 7/66 L)



Grades Inlets #11 & 12

Sta.	+	H.I.	-	Elev. Stakes	Ch. Grade	Cut or Fill	Offsets
West End Inlet #11		3.81		394.32	394.35	6" R+	F0.03
Q Inlet #11		3.55		394.58	394.23	"	C0.35
East End Inlet #11		3.52		394.61	394.34	"	C0.27
So Line Inlet #12		4.89		392.24	392.60	10" L	C0.64
Q Inlet #12		4.88		392.25	392.53	"	C0.72
No Line Inlet #12		5.28		392.85	392.60	"	C0.25
B.M.	2.38	398.13			395.75	Point # 178268	F131825 P.31

8-20-48 State Curb Inlets # 4 & 5
 Hendricks El Cerrito Storm Drain
 Roberts DWG # 71642
 Greer
 Korol

(26)

Estelle

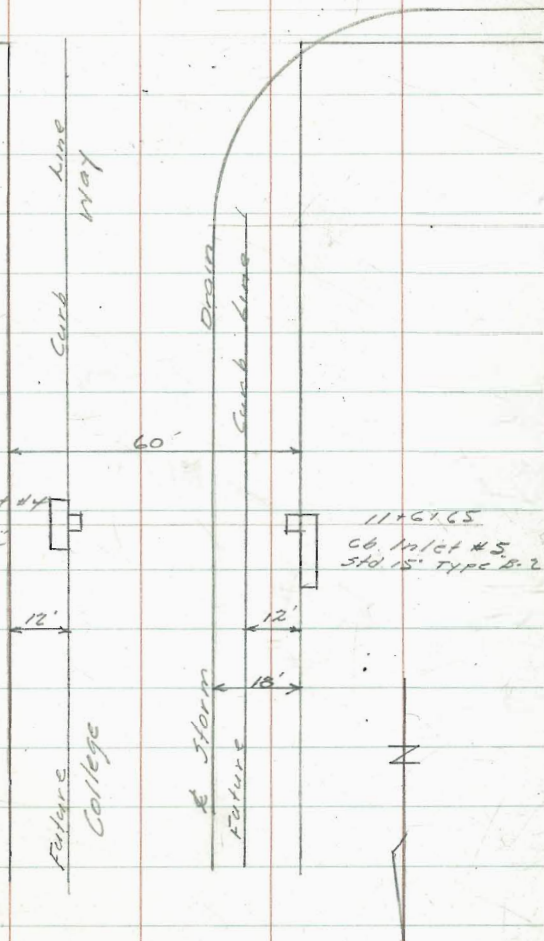
St.

Sta. + N1 - Elev Station Cb. Elev Cor F offsets

INDEXED

WK
 MAY 23 1949

CK 51K 7 RT 11+67.65 P 19	4.35	428.66	428.74		
No End Inlet # 4	4.37	428.64	429.58	F 0.94	10' LT
So End Inlet # 4	4.28	428.73	429.44	F 0.71	"
No End Inlet # 5	3.97	429.04	429.09	F 0.05	6' RT
So End Inlet # 5	4.02	428.99	428.88	C 0.10	"
T.P.	6.15	433.01	0.01	426.86	
B.M.	8.21	426.87		418.66	NV 13 P 60th & Estelle



8 20-28 Stake Curb Inlets # 2 & 3
 Hendricks El Cerrito Storm Drain
 Roberts (Dwg # 7164 L)
 Greer
 Korner

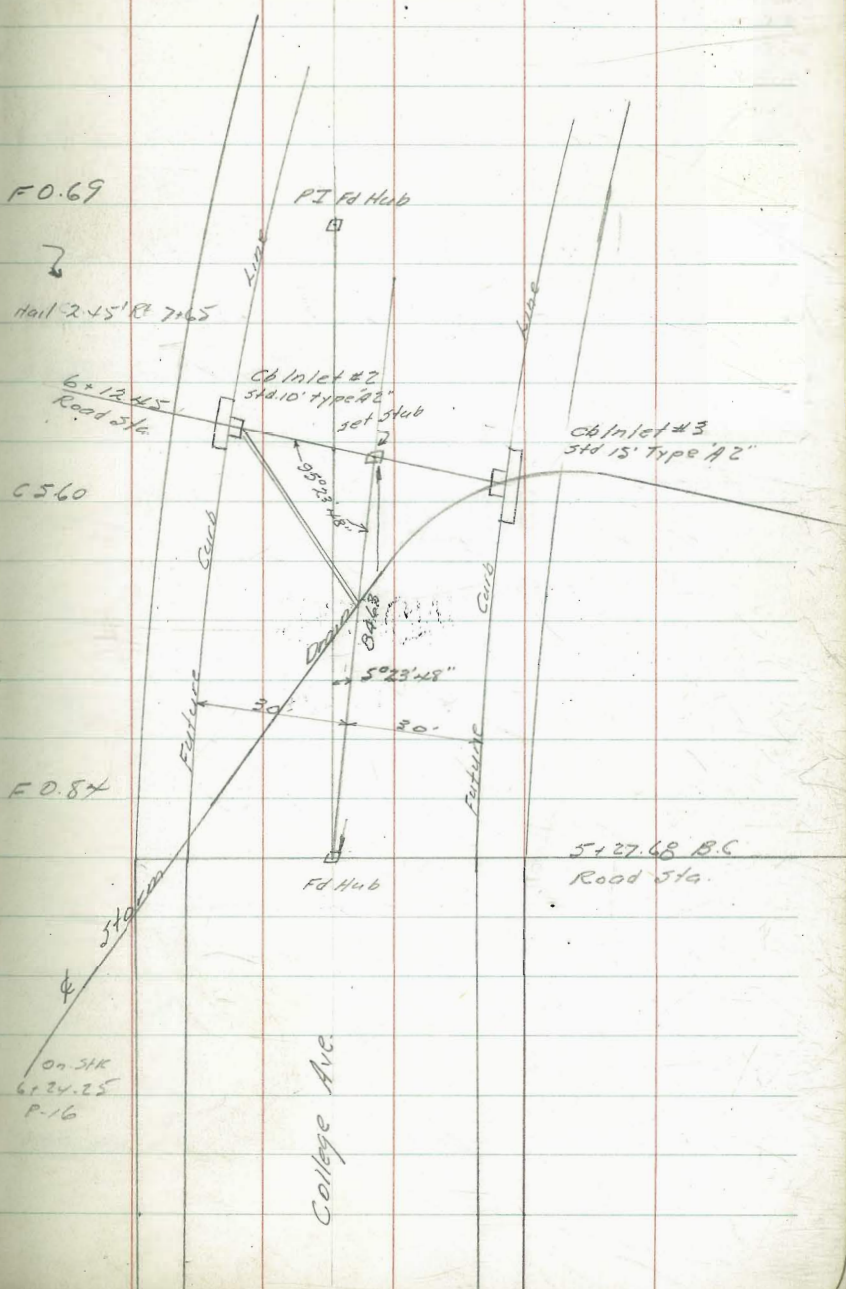
Reset Cb Inlet No. 3					
CK	El Inlet # 2	1.35	444.35	444.36	
	El Cb Inlet # 3	8.63	437.07	437.76	F 0.69
BM	8 91	445.70		436.79	
CK		10.08	436.78	436.79	Dist 245' @ 7165

No End Inlet # 2					
El Inlet # 2	2.50	444.36	438.76	65.60	
So. End Inlet # 2					

INDEXED
 WK
 MAY 23 1949

No End Inlet # 3					
El Inlet # 3	9.94	436.90	437.76	F 0.84	
So. End Inlet # 3					

BM	8 33	446.86		438.53	
----	------	--------	--	--------	--

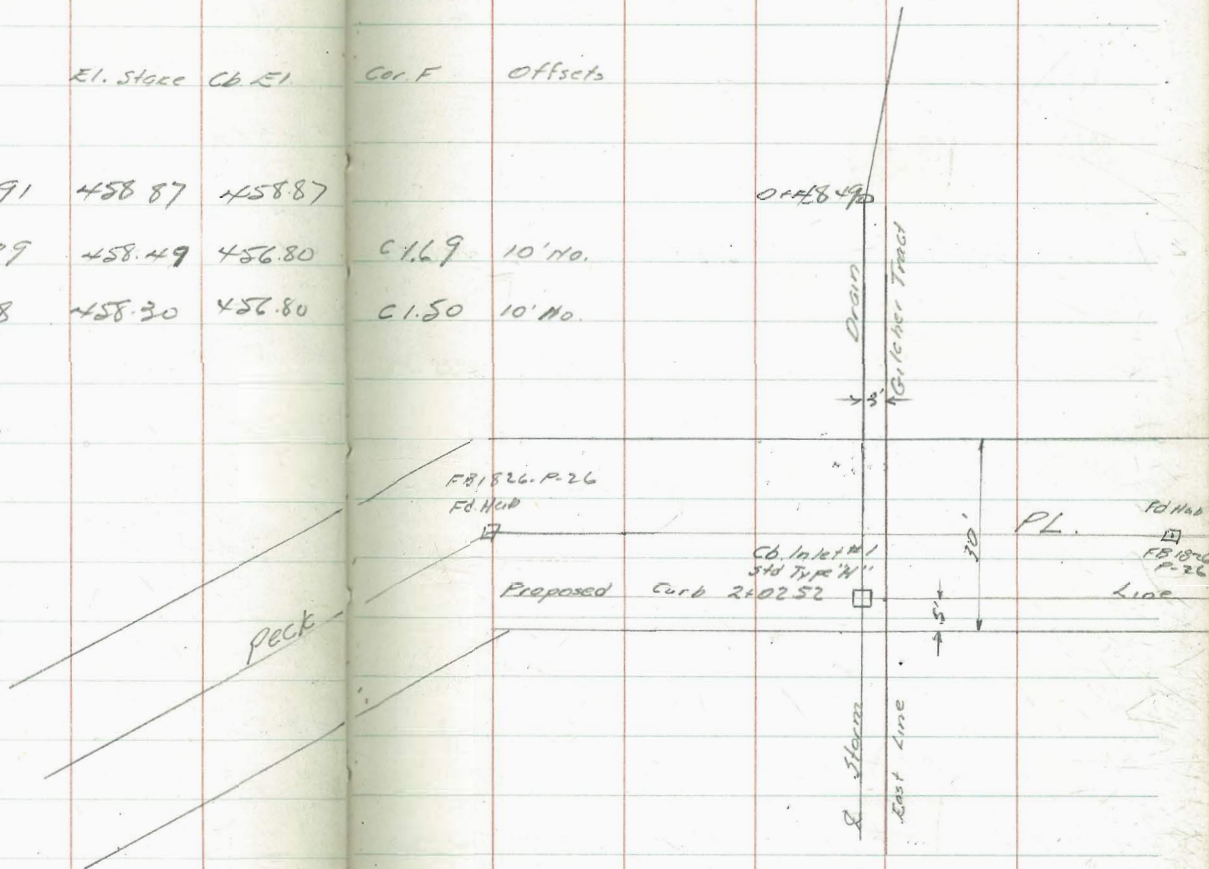


8-23-48
 Hendricks
 Roberts
 Greer
 Korer

State Curb Inlet #1
 El Cerrito Storm Drain

Sta.		H.I.	-	El. Stake Cb. El.	Cor. F	Offsets
CK Hub (210252 P.15)		5.91		458.87	458.87	
W. End Inlet #1		6.29		458.49	456.80	C1.69 10' No.
E " " #1		6.48		458.30	456.80	C1.50 10' No.

INDEXED
 WK
 MAY 23 1949



BM 158 464.78 463.20 Nail in Pole #7070 FB-1826-P.11

State Pavement Grade for
Cleanout # 28151 Cerrito Storm Drain

Elev. Pavement
Stake Grade

(29)

INDEXED

WK

MAY 23 1949

Cleanout #1

CK Stake Inlet #3 683 436.93 436.92 P.27

Cleanout #1 384 439.92 438.42 C.150

BM 5.23 443.76 438.53 on Stake 6+24.25 P.16

Cleanout #2

CE 9+60 778 433.34 433.33 P.17

Cleanout #2 -613 434.99 436.74 F175

BM 5.04 441.12 436.08 on Hub 9+08.73 P.17

Walker
F. Gregory
Bohler
9-20-98

Grades - Culvert Extension

Block is Paradise Hills

Drawing 7234-L

30

INDEXED
WK
MAY 23 1949

0243091

			Elev. Flow line	Cuts
			0.01	
FR 1796-66		166.63		
chk Grating 3141.5	3.27	166.64		
4+21.8 = End Work	8.18	161.73	158.8	2.93
3+96.22 = B.C. H.	6.82	163.09	160.62	2.47
3+57.75 = B.C.	3.03	166.88	163.33	3.55
3+42.8 = Beginning Work		163.90		
3+40.85 = B.C. H.				

3.25 169.91

167.66

S.M. Top of Inlet 3141.5 FB 1796-P-66

Walker Grades - North Mine Alley
 Allen Block 1 - North Highland Park
 F. Gregory
 Branby
 9-30-46

INDEXED
 WIK
 MAY 23 1949

Station	Top	0	001	Elev. Grade	NL. Alley
check 9" Conc. Wall	+1.80	377.56	374.55		
4+50 = PVC			368.32		
4+46.7 Bk	2.46	370.29	368.29		
4+30 "	2.60	370.15	368.15		
4+10 "	2.71	370.04	368.04		
3+90 "	2.77	369.98	367.98		
3+72 = Beg. 9" Conc. Wall	2.15	370.00	368.00		
3+70 Bk = PVC of 120' VC.			368.01		
3+50.8 Bk	2.67	370.08	368.08		
3+30 = PVC					
0+00 = Wh. line 33rd St					
TP	2.73	372.75	7.28	370.02	
	3.05	377.30		374.25	

Cuts

C 2.00

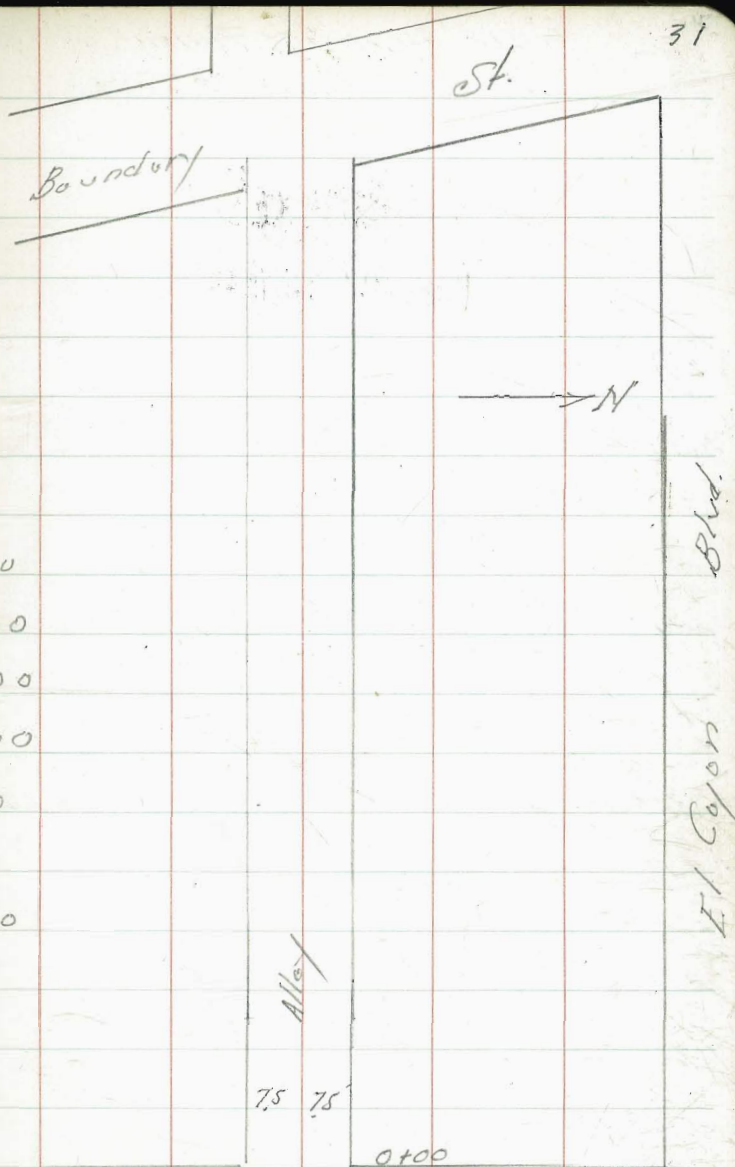
C 2.00

C 2.00

C 2.00

C 2.00

C 2.00



33rd

St.

B.M. B.P. SW El Cajon & 33rd St.

Gibbs Airport - Finish Grades

Wly End Runway "B"

75'

50

25'

£

25

ft.

50

75'

37

INDEXED

WK

MAY 23 1949

10+00 = Beg. Paving

404.53

404.78 405.03 405.28 405.03 404.78 404.53

2+50

404.28

404.53 404.78 405.03 404.78 404.53 404.28

9+00

404.03

404.28 404.53 404.78 404.53 404.28 404.03

8+50

8+00

Gibbs Airport - Finish Grades

Runway "C" ELY. END

P. 33

				Lt.			Rt.		
		75'		50	25'	±	25'	50'	75'
46+00		412.05		412.30	412.55	412.80	412.55	412.30	412.05
		5.31		5.06	4.81	4.56	4.81	5.06	5.31
45+75		412.15		412.40	412.65	412.90	412.65	412.40	412.15
		5.21		4.96	4.71	4.46	4.71	4.96	5.21
45+50		412.22		412.47	412.72	412.97	412.70	412.44	412.18
		5.14		4.89	4.64	4.39	4.66	4.92	5.18
± 456 47+00									
T.P.	461	417.36	458	412.75					
45+00		412.27		412.52	412.77	413.02	412.67	412.33	412.00
		5.06		4.81	4.56	4.31	4.66	5.06	5.33
44+50		412.32		412.57	412.82	413.07	412.78	412.49	412.20
		5.01		4.76	4.51	4.26	4.55	4.84	5.13
44+00 = End Paving		412.38		412.63	412.88	413.13	412.88	412.63	412.38
	6.43	417.33	410.90	B.M. ±	Runway "C"				

MAY end Runway "A" - Finish Grades

Gibbs Airport 75'

Walker
Johnson
Pope
Riley
1-17-49

INDEXED
WK

MAY 23 1949

110+00 Beg. Paving.

406.45

406.70 406.95 407.20 406.95 406.70 406.45

109+50

406.35

406.60 406.85 407.10 406.85 406.60 406.35

5.39

5.14 4.89 4.64 4.89 5.14 5.39

109+00

406.25

406.50 406.75 407.00 406.75 406.50 406.25

5.49

5.24 4.99 4.74 4.99 5.24 5.49

108+50

404.87

405.20 405.53 405.86 405.64 405.42 405.20

6.87

6.54 6.21 5.88 6.10 6.32 6.54

108+00

403.82

103.98 104.14 104.30 104.40 104.50 104.60

7.92
8M 5106
Mod

840 411.74

403.34 108+00

7.76 7.60 7.44 7.34 7.24 7.14

Lt

50

25'

2

Rt

25'

50'

75'

P-34

Gibbs Airport

Walker
Johnson
Pope
Riley
1-19-48

FINISH GRADES FLY END RUNWAY "A"

75'

Lt

Rt

50 25 25 50 75

146+00

415.20 415.30 415.90 415.50 415.34 415.17 415.00
6.59 6.49 6.39 6.29 6.45 6.62 6.79

145+50

415.50 415.75 416.00 415.25 416.00 415.75 415.50
6.29 6.04 5.79 5.54 5.79 6.04 6.29

145+00

416.45 416.70 416.95 417.20 416.95 416.70 416.45
5.34 5.09 4.84 4.59 4.84 5.09 5.34

144+50

416.29 416.54 416.79 417.04 416.79 416.54 416.29
5.50 5.25 5.00 4.75 5.00 5.25 5.50

6.46 421.79

415.33 126100

BIM Cont.
11.00

144+00

416.13 416.38 416.63 416.88 416.63 416.38 416.13

Walker
Johnson
Pope
Riley
2-7-49

PACIFIC RIVIERA VILLAS

Culvert Grades in Blk 3, & 4.
From La Jolla Blvd. to Ocean

Plan
Drawing 7375-L
Profile 7385-L

NO. 90083

LA JOLLA BLVD. P. 36

Proposed Curbline

0+00

Cont P 37

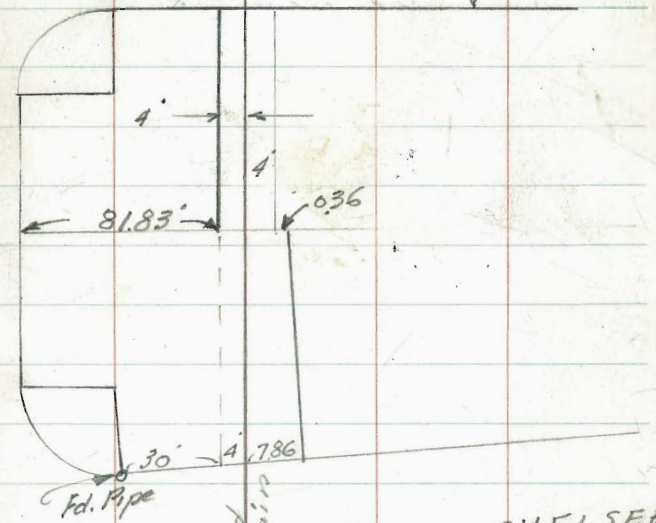
INDEXED

WK
MAY 23 1949

				El. Flow	Cuts
				2172	
2+55.5=Blk	4.68	52.69	41.68	1101	
3+35.5=Blk	3.16	54.21	43.65	10.56	
3+10	1.27	56.10	45.24	10.86	
2+80	1.37	56.00	47.10	8.90	
2+40	0.80	56.57	49.57	7.00	
TR ¹³	0.21	57.37	57.16		
2+100	10.50	59.34	52.06	7.28	
1+60	8.92	60.92	54.54	6.38	
1+23=Blk	7.26	62.58	56.83	5.75	
0+80	5.49	64.35	58.00	6.35	
0+40	3.89	65.95	59.09	6.86	
0+10	0.68	69.16	59.91	9.25	
0+00=					
Chk Existing Flow 24" Pipe	9.66	60.18	60.18	60.18	First-Flu line to North cuthead 1101
0+0					60.27=Flu
TR ¹⁴	0.29	69.84	4.24	69.55	
TR ¹¹	4.22	73.79	8.96	69.57	
	0.55	78.53		77.98	

BIMBER
LA JOLLA
COLUMBIA
DRAWING
7385-L

ARCHER



Restaked
see P 52

Fd. Pipe

Proposed
4\"/>

CHELSEA ST.

Fd. Pipe

3+60.17
B.C.
 $\Delta = 22^\circ$
 $R = 45'$

B.C.
3+77.67

4+26.92 = End Pipe

SEE ALSO PAGE NO 52

Grades - Culvert No 2
 Riviera Villas Unit No 1
 Cont. from P. 36

P. 37

4+26.9 18.0 24.5

4+08 8.4 36.1

0.00 42.47 42.47

Slk Starting BM 140 77.98
 77.99

TP 11.20 79.39 0.69 68.19

TP 11.87 68.88 2.24 57.01

TP 12.53 59.25 0.18 46.72

4+26.92 = End 42" Pipe 11.29 35.61 24.50 11.11
 28.80 6.81

3+95.5 = Slk 4.43 42.47 33.78 8.69
 34.78 7.69

TP 2.12 46.90 12.59 44.78

3+77.67 = E.C. 9.71 47.66 37.85 9.81
 38.35 9.31

3+60.17 = P.C. Lt 5.12 52.25 40.82 11.43
 41.09 14.18

57.37

Grade changed as shown
 to meet existing ground
 at end of pipe

Per. E. F. Gabrielson

2-9-48

Stake Portion Culvert No 1

P-8

Walker
Johnson
Pope

Rivera Villas

Unit No 1

Kilo
2-8-49

0+63	3.48	71.21	61.53	7.68
0+124	4.71	69.78	61.12	8.66
0+144 = Int. Gas Line	5.29	69.40	60.56	8.84

0+100 = 2' East Proposed abutment 60.27 Using Phelps Datum.

507 74.69 69.62 Elev. Stake
C 9.35 = Cut on Stake
60.27 To Floor

TP #2 P-36
 507 74.62 69.55

GRADES - CULVERT = 24" Conc. Pipe

Walker on Imperial Ave
Johnson
Pope from 14th Street to Switzer
Crossford
2-17-49 Storm Drain West of 15th St.

Drawing 7436-L- NO. 60342

Cont. P. 40		El.	Flow Line	Cuts	Offsets
3+60	INDEXED	5.46	7.15	-1.82	8.97 6'R ✓
3+25	INDEXED	5.36	7.25	-1.60	8.85 ✓ ✓
2+90	WK MAY 23 1949	5.33	7.28	-1.37	8.65 ✓ ✓
2+55		5.15	7.46	-1.15	8.61 ✓ ✓
2+20		5.03	7.58	-0.92	8.50 ✓ ✓
1+85		4.95	7.66	-0.70	8.36 ✓ ✓
1+50		4.82	7.79	-0.47	8.26 ✓ ✓
1+15		4.84	7.77	-0.25	8.02 ✓ ✓
0+81.00 = E.G.		4.68	7.93	-0.02	7.95 ✓ ✓
0+61.11		4.71	7.90	0.10	7.80 ✓ ✓
0+41.22		4.65	7.96	0.23	7.73 ✓ ✓
0+21.33		4.68	7.93	0.36	7.57 ✓ ✓
0+01.44 = B.C. H.		4.75	7.86	0.49	7.37 ✓ ✓
0+00 = Inside Inlet Well				0.50	

4.64 12.61

7.97

P.M. 547' fact Imp. Ave & 15th St.

Storm Drain
Cont. from P-39

Cont. P-51

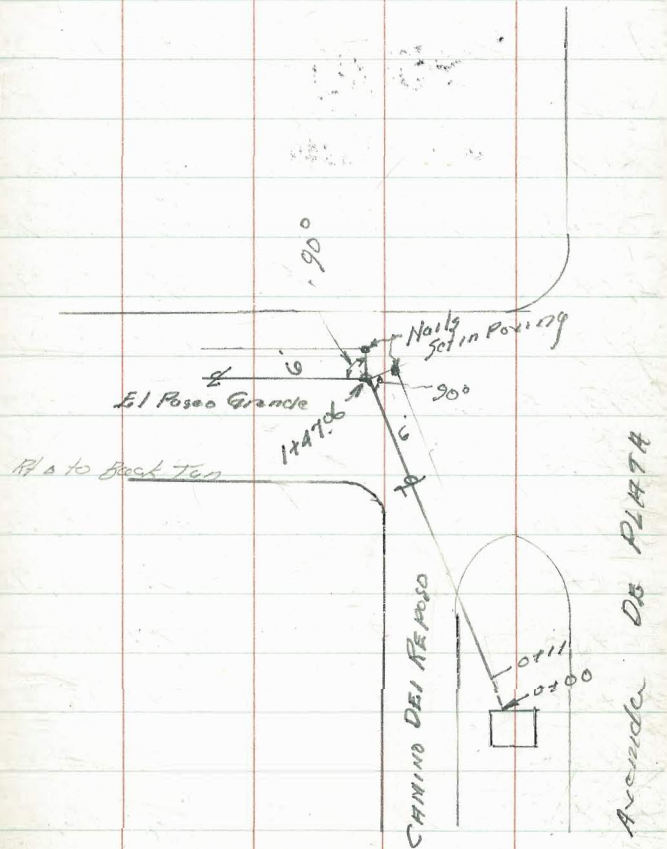
			El. Flowline	Cuts	Offsets
5+75	6.37	6.24	-3.20	9.44	6' RT ✓
5+35	5.79	6.82	-2.95	9.77	✓ ✓
5+00	5.71	6.90	-2.72	9.62	✓ ✓
4+65	5.72	6.89	-2.50	9.39	✓ ✓
4+30	5.62	6.99	-2.27	9.26	✓ ✓
3+95	5.51	7.10	-2.05	9.15	✓ ✓

12.61
3

CONST. GRADES - TRUNK SEWER (121)

Walker From La Jolla Shores Pumping
 Johnson Station to Prospect Place
 Pope
 Crawford
 2-28-49 Drawing 1369-D to 1371-D
 3-1-49

					Elev.	
T.P.	8.10	19.32	0.77	11.22	Flowline	Cuts
4150	INDEXED		0.77	11.22	5.66	5.56
4100	WIK		1.53	10.46	5.28	5.18
3150	MAY 23 1949		3.35	9.64	4.89	4.75
3100			3.06	8.93	4.51	4.42
2150			2.83	8.16	4.12	4.04
2100			4.55	7.44	3.74	3.70
1470.6	} 24.62° 04' 15" Turned		5.26	6.73	3.33	3.40
1470.6			5.17	6.82	3.33	3.49
1700			4.64	7.35	2.97	4.38
0150			4.02	7.97	2.58	5.39
011" Bq. Project			2.97	9.02	2.28	6.74
0100						
FB 1857-21					6.38	
Check Rim M.H. 0110 094			5.63		6.36	
			3.42	11.99	8.57	



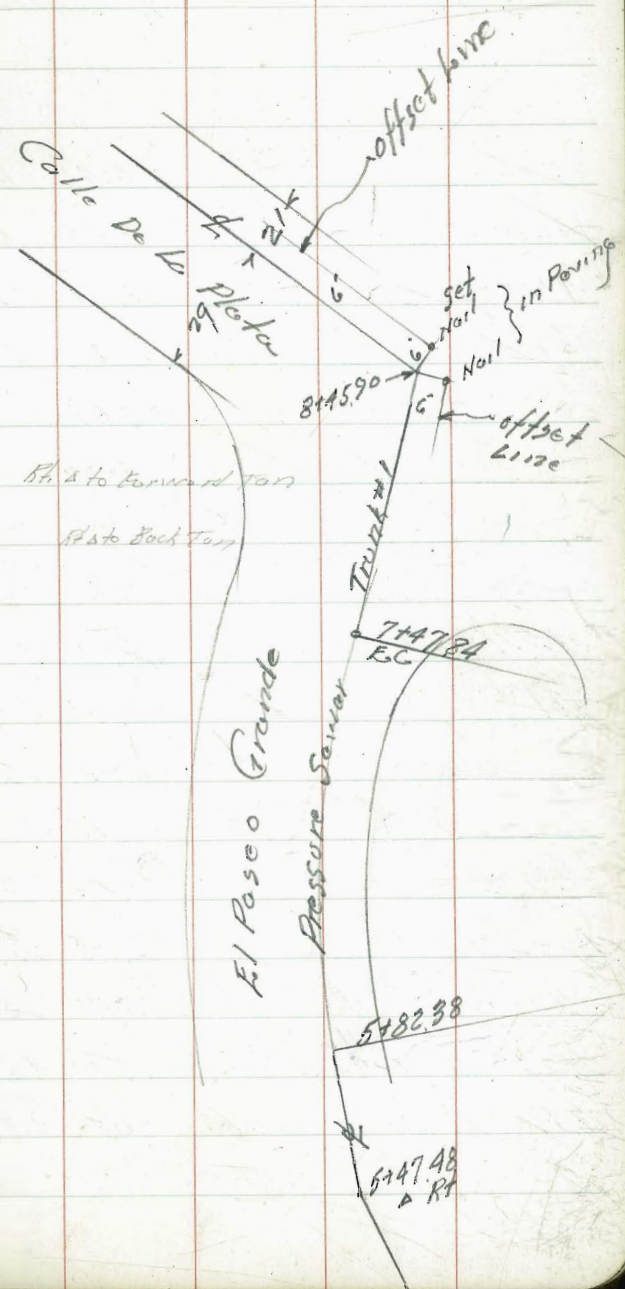
B.M. on Spike 0100 FB 1857-6

Trunk Sewer Cont.
from P-41

1						
11+00		0.05	28.04	24.20	3.84	
10+50		3.14	24.95	20.50	4.45	
10+00		7.39	20.70	16.80	3.90	
9+50		11.10	16.99	13.70	3.89	
T.P.	12.54	28.02	3.77	15.55		
8+96-Bk.		5.47	13.85	9.10	4.75	
		6.95	12.37		3.66	
8+45.90		6.39	12.92	8.71	4.22	
8+45.90 = Δ L 49°49'17"		6.99	12.33	8.71	3.62	
8+00		7.22	12.10	8.35	3.75	
7+47.84 = E.C.		6.65	12.67	7.95	4.72	
7+25		5.29	13.03	7.77	5.26	
7+00		5.80	13.52	7.58	5.94	
6+75		5.56	13.76	7.39	6.37	
6+50		5.77	13.55	7.20	6.35	
6+25		5.98	13.34	7.01	6.33	
6+00		6.23	13.09	6.82	6.27	
5+82.38 = B.C. RT		6.43	12.89	6.68	6.21	
5+47.48 = Δ 6°33'36" RT		6.85	12.47	6.41	6.06	
5+00		7.82	11.50	6.05	5.45	

Cont. from
P-41

19.32



Plota to forward turn
Plota Back Turn

5+47.48
RT

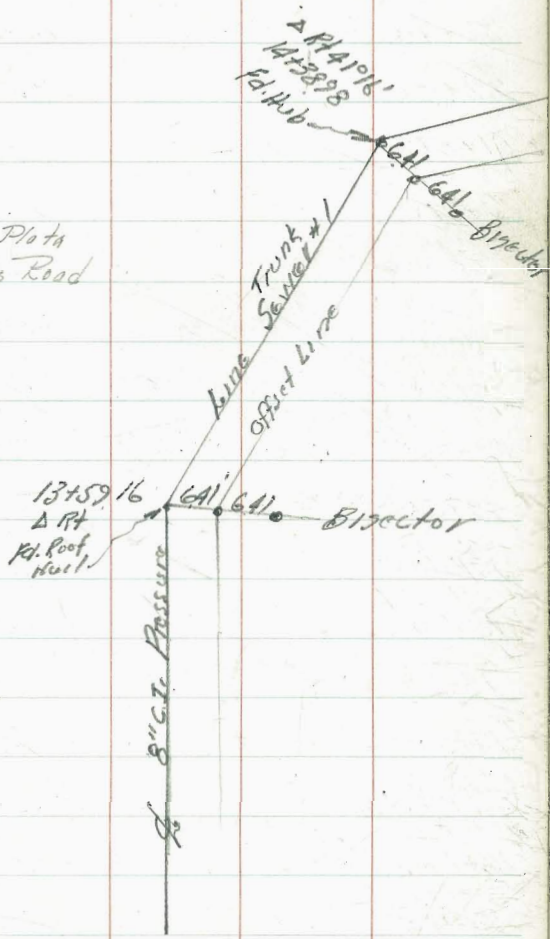
LA DOLLA TRUNK SEWER NO. 1
 from Pumping Plant
 to Prospect Pl. Cont. from P-42

			El.	Flow	Cuts
15+00		6.44	61.20	57.42	3.78'
14+70		7.59	60.05	56.55	3.50'
14+38 ⁹⁸	ART 4 1/2'	8.52	59.12	55.65	3.47'
14+00		11.04	56.60	51.54	5.06'
	12.95	67.69		54.69	

N.E.B.P. - Calle De La Plata
 B.M. Torrey Pines Road

			0.03			
	Calle DE LA PLATA Torrey Pines Rd	362	54.69	47.20		
	Check N.E.B.P.		54.72			
13+59	1/2" ART 4 1/2'	261	53.72	47.20	6.52'	
T.P.	10/12	67.34	0.27	53.22		
13+00		7.69	45.80	40.91	4.89'	
T.P.	12.23	53.49	0.45	40.56		
12+50		1.04	39.97	35.62	4.35'	
12+40	B.M.	1.95	39.06	34.56	4.50'	
12+00		5.47	35.54	31.60	3.94'	
11+50		9.80	31.21	27.90	3.31'	
T.P.	12.27	41.01	0.05	28.04		
			2.809			

Cont. from
 P-42



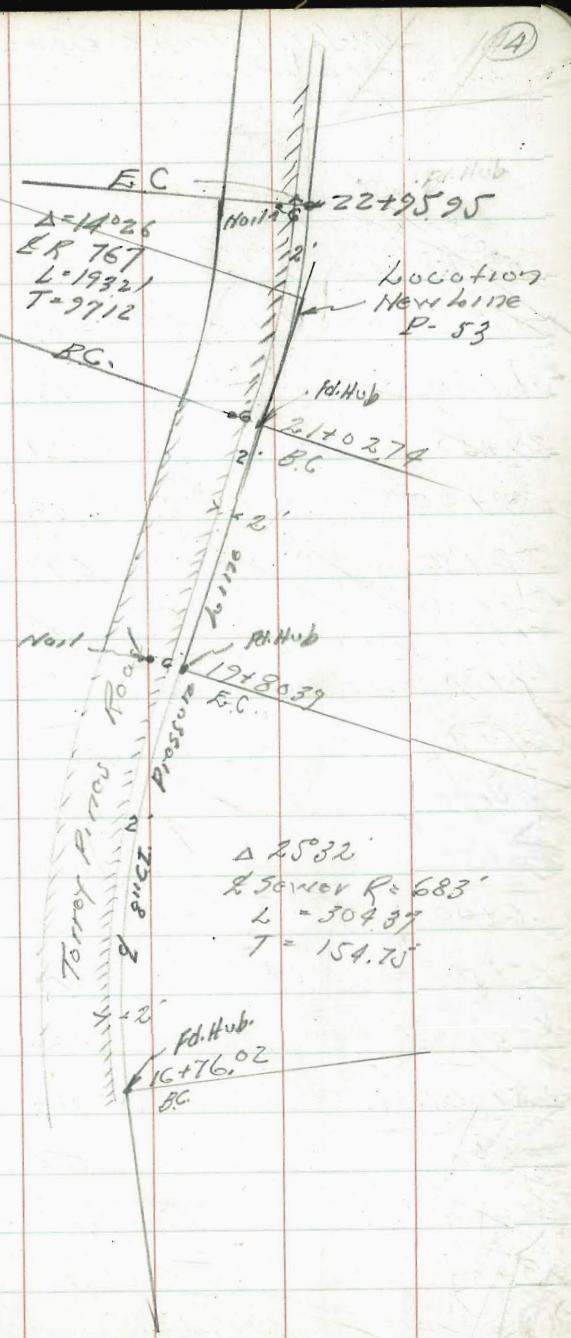
La Jolla Trunk Sewer No. 1
 from Pumping Plant
 to Prospect Pl. (Cont. from P-43)

				Elev	Fl. line
22+95.95 = E.C.		4.59	86.15	80.51	
22+50	This Portion of line changed See P-53 for New Location	5.57	85.17	79.18	
22+00		6.80	83.94	77.73	
21+50		8.23	82.51	76.28	
21+02.74 = B.C.		9.60	81.14	74.91	
20+60		11.05	79.69	73.67	
T.P.	12.84	90.74	0.94	77.90	
20+20		2.01	76.83	72.51	
19+80.39 = E.C.		4.22	74.62	71.36	
19+50		4.61	74.23	70.47	
19+00		7.28	71.56	69.02	
18+50		7.84	71.00	67.57	
18+00		8.81	70.03	66.12	
17+50		10.10	68.74	64.67	
17+00		10.76	68.08	63.22	
16+76.02 = B.C.	11.22	78.84	0.02	67.62	62.52
16+40		1.50	66.14	61.48	
16+00		4.16	63.98	60.32	
15+50		4.35	63.29	58.87	

67.64

Cuts Offsets

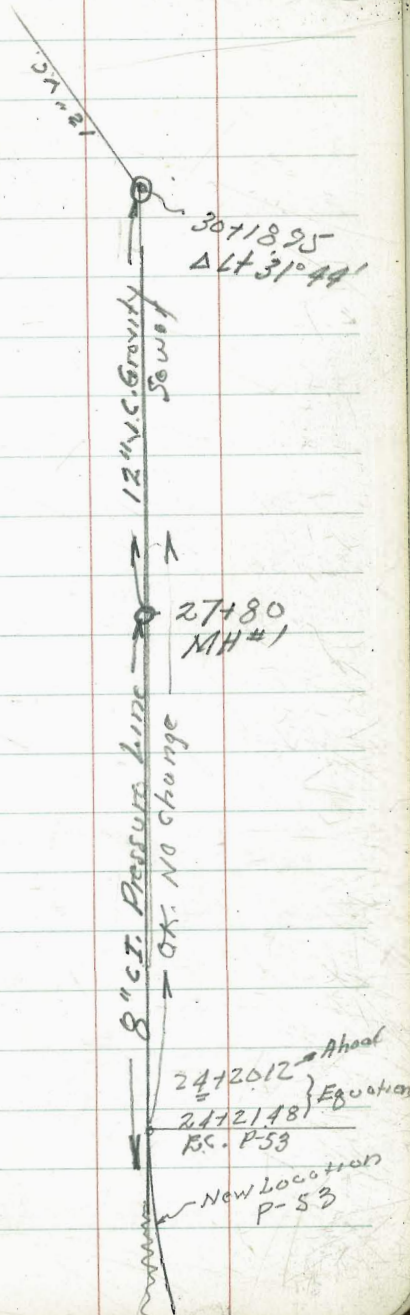
5.64	6'8"
5.99	"
6.21	"
6.23	"
6.23	"
6.02	"
4.32	"
3.26	"
3.76	"
2.54	"
3.43	"
3.91	"
4.07	"
4.86	"
5.10	"
4.66	"
3.16	"
4.42	"



La Jolla Trunk Sewer #1
 from Pumping Station
 to Prospect Pl. Cont from P. 44

			003		
NW 1/8 P. Viking Way to Torrey Pipes Rd chk FB 1847-31	8.06	96.32	by Moore		
TP	7.57	104.35	0.19	96.78	
30+00		0.19	96.78	86.56	10.22
29+50		1.27	95.70	87.01	8.69
29+00		3.53	93.44	87.46	5.98
28+50		5.78	91.19	87.91	3.28
28+00		6.51	90.46	88.36	2.10
MH #1 27+80 End Pressure Line	6.16	90.81	88.54	2.27	
27+50		7.07	89.90	88.31	1.59
27+00		8.49	88.48	87.93	0.55
26+50		8.79	88.18	87.55	0.63
26+00		6.90	90.07	87.18	2.89
25+50		5.83	91.14	86.80	4.34
TP	9.47	96.97	0.24	90.50	
25+00 - Bk.		0.24	90.50	86.42	4.08
24+50		1.44	89.30	84.97	4.33
24+00	Line Changed see P-53	3.67	88.07	83.51	4.56
23+50		3.48	87.26	82.07	5.19

90.74



24+2012 } Ahead
 24+2148 } Equation
 K.C. P-53
 New Location
 P-53

La Jolla Trunk Sewer #1
 from Pumping Station to
 Prospect Pl. Cont. from P. 45

35+36.30	MH #3	7.96	84.97	81.73	3.24
35+05		7.78	85.15	82.02	3.13
+70		7.02	85.91	82.33	3.58
+35		5.47	87.46 86.46	82.65	4.81
34+00		3.46	89.47	82.96	6.51
+65		1.78	91.15	83.28	7.87
T.P.	1.36	92.93	10.82	91.57	
33+30		9.64	92.75	83.59	9.16
+95		7.69	94.70	83.91	10.79
+60		5.86	96.53	84.22	12.31
32+25		4.60	97.79	84.54	13.25
+90		3.61	98.78	84.85	13.93
+55		3.38	99.01	85.17	13.84
31+20		3.43	98.96	85.48	13.48
30+85		3.67	98.72	85.80	12.92
30+50		3.74	98.65	86.11	12.54
30+18.95	FD. Tong	4.66	97.73	86.39	11.34 OK
30+18.95	BK. Tong				
30+18.95	MH #2	4.80	97.59	86.39	11.20 OK
6.07	102.39		96.38		

Void
 See New Grades
 And Location, 61, 62

12" V.G. Gravity Line
 offset line

MH #2
 30+18.95
 ΔLT 31+44

N.W.B.P. Viking Way & Torrey Pines Rd. FB. 1847-31

La Jolla Trunk Sewer #1
 from Pumping Plant
 to Prospect Pl. Cont. from P. 96

Station	807	92.72		84.65		
below						
				0.05		
Station → FB. 1847-38				84.65		
CK. B. M. 12135		3.31		84.60		
39+83.42		9.50	78.41	76.86	1.55	
Fd. Tan						
39+51.42		2.27	84.94	78.00	6.94	
Bc. Tan. Δ Lt 87°49'						
39+51.42 MH 49		3.43	84.48	78.00	6.48	
39+20		5.04	82.87	78.27	4.60	
+85		5.04	82.87	78.58	4.29	
+50		4.72	83.19	78.90	4.29	
38+15		4.63	83.28	79.21	4.07	
T.P.	4.53	87.91	9.55	83.38		
+80			9.55	83.38	79.53	3.85
+45			9.45	83. ⁴⁸ 58	79.84	3.64
37+10			9.02	83.91	79.16	4.75
+75			8.79	84.14	79.47	4.67
+40			8.67	84.26	80.79	3.47
36+05			8.88	84.05	81.10	2.95
35+70			8.55	84.38	81.42	2.96

Void
 For New Grades See P. 68

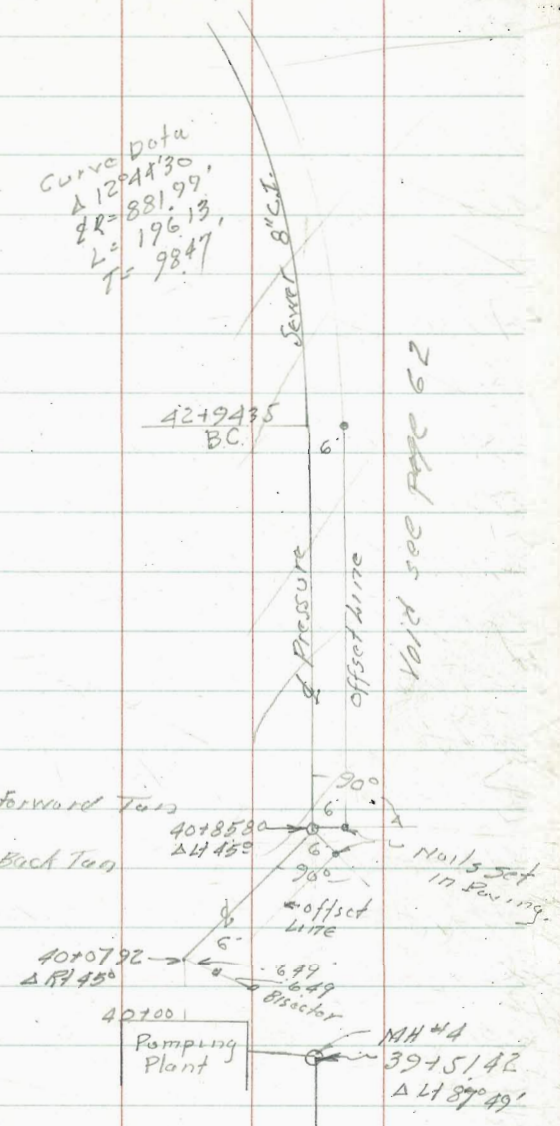
92.93

LA JOLLA TRUNK SEWER #1
GRADES

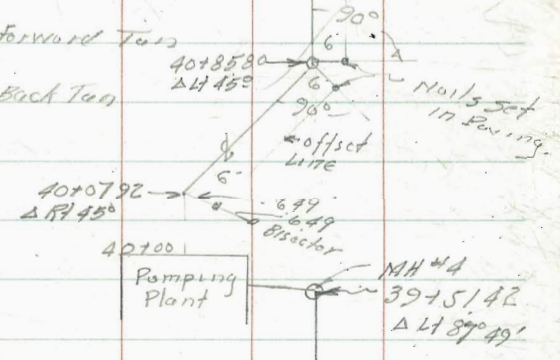
			El.	Flow Line	Cuts	
T.P.	12.71	117.70	028	104.99		
43+60 Bk			028	104.99	100.80	4.19
43+40			1.46	103.81	99.41	4.40
43+20			2.70	102.57	98.03	4.54
43+94.35 B.C. H.			4.41	100.86	96.26	4.60
+50			7.68	97.59	93.21	4.38
42+00			11.18	94.09	89.76	4.33
T.P.	12.70	105.37	0.15	93.57		
41+60 Bk			1.41	91.31	87.00	4.31
41+20			3.80	88.92	85.03	3.89
40+85.8 } $\Delta L 45^\circ$			5.25	87.47	83.38	4.09
40+85.8			5.33	87.39	83.38	4.01
40+45			6.08	86.64	81.46	5.18
40+07.92 $\Delta R 45^\circ$			10.78	81.94	79.67	2.27
40+00			12.77	79.95		

92.72
}

Curve Data
 $\Delta 12^\circ 44' 30''$
 $R = 881.99'$
 $L = 196.13'$
 $T = 98.47'$



Valid see page 62



La Jolla Trunk Sewer #1

Grades

Cont. P. 50				Elev. Flowline	Cuts.	
48+25			8.56	121.78	116.36	5.42
48+00-Bk.			9.80	120.54	114.70	5.84
47+75			10.78	119.56	113.90	5.66
47+50			11.70	118.64	113.11	5.53
47+25			12.50	117.84	112.32	5.52
T.P.	12.82	130.34	0.18	117.52		
47+00			0.73	116.97	111.53	5.44
46+75			1.63	116.07	110.74	5.33
46+49.75-B.C. 11			2.59	115.11	109.94	5.17
46+00			4.51	113.19	108.37	4.82
45+50			6.53	111.17	106.79	4.38
45+23.19-217 25+41			7.21	110.49	105.94	4.55
44+90.48-50			8.16	109.54	104.92	4.62
44+75			8.36	109.34	104.43	4.91
44+50			9.02	108.68	103.64	5.04
44+25			9.80	107.90	102.85	5.05
44+00			10.33	106.87	102.06	4.81
43+80			11.73	105.97	101.43	4.54

117.70

Cont. from
P-48

Walker
Johnson
Pope
Clowford
3-3-49

La Solla Trunk Sewer #1
Grades

Fl.
Flowline Cnts

(Completed 3-3-49)

Station	Grade	Flowline	Cnts
Grade Book 253-8	150.58	150.58	
Chk. 354+20.68	5.16	150.54	
52+51.73	5.16	150.54	144.58
52+50	5.39	150.31	144.47
52+00	6.53	149.17	141.20
51+50	9.89	145.81	137.91
T.P.	12.91	155.70	0.10
51+00	1.05	141.84	134.60
50+50	5.00	137.89	131.28
50+00	8.25	133.94	127.96
49+87.72	9.98	132.91	127.14
49+87.72	10.08	132.81	127.14
T.P.	12.63	142.89	0.08
49+50	0.37	129.97	124.64
49+00	4.03	126.31	121.33
48+70	6.01	124.33	119.34
48+43.64 = E.C.	7.49	122.85	117.60

7043'15" Ht.
Turned

6' H. & to Forward Turn
6' H. & to Back Turn

130.34

Drains - Imperial Ave
 to 15th Cont. from P. 39-40

Plan 74362

GRADES NE Returns

			E.I.	Curb
0+31.42 = E.C.	3.70	8.43	8.43	
0+23.20 = 1/2" Inside Edge Inlet	3.83	8.30	8.30	
0+15.71 = 1/2" Inlet = 1/2" Return	3.93	8.20	8.20	
0+08.20 = Bag. Inside edge Inlet	3.90	8.23	8.23	
0+00 = B.C. 20' CbR.	3.72	8.41	8.41	

Grades S.E. Returns

0+31.42	5.39	6.74	7.80
0+23.20 = 5/8" Inside Inlet.	4.29	7.84	7.84
0+15.71 = 1/2" Inlet = 1/2" Return	4.23	7.90	7.90
0+08.20 = Bag. Inlet = Inside edge	4.17	7.96	7.96
0+00 = B.C. 20' CbR.	4.03	8.10	8.10

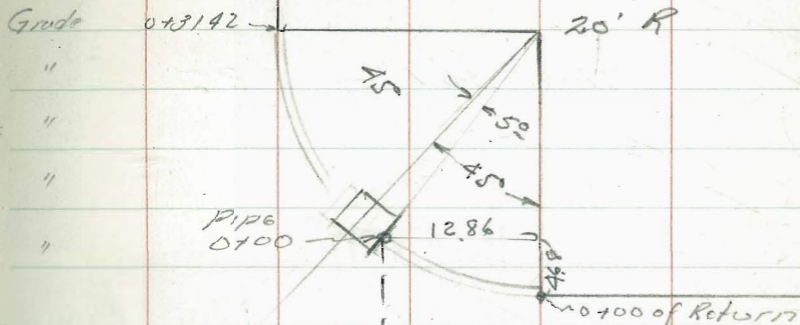
Grades 18" Conc. Pipe

			E.I.	Flow Line	Cuts
0+61.36 = End Pipe	4.15	7.98	1.50 = Flow to West		
0+30	3.83	8.30	1.00 = Flow to North		
0+00	3.78	8.35			
420	12.13				793

INDEXED

WK
MAY 23 1919

Cuts



F1.06

Grade

"

"

"

Cuts

0.50 = Flow to West

6.98

6.64 0+31.42

6.05

BM 017 No 1

0+21.33 P. 39

Pipe
0+100

18" Conc. Pipe

1/2" Imp. Ave

0+00 of Return

0+61.36

0+31.42

BM 017 No 1

0+21.33 P. 39

Walker
Johnson
Pope
Crowford
3-7-49

Pacific Riviera Villas.
Culvert Grades Blk 3, 4
Re stake Portion
on account stakes being lost.

Orig. Staking P-36

INDEXED
W/K
MAY 23 1949

Fl.
Flow Line

Cuts offsets

CHK		⁰⁰¹				
3+10 P-36	12.05	56.10	56.11	45.24	10.87	6' 4"
2+80	12.21	55.95	55.95	47.10	8.85	"
2+40	11.82	56.34	56.34	49.57	6.77	"
2+00	8.81	59.35	59.35	52.06	7.29	"
1+60	7.25	60.91	60.91	54.54	6.37	"
1+24 = Blk	6.64	61.52	61.52	56.77	4.75	"
1+23 = orig. Blk Now inaccessible				56.83		
0+80	3.65	64.51	64.51	58.00	6.51	"
0+40	2.21	68.16	68.16	65.95	59.09	B.M. on stake 0+40 P-36

LA JOLLA TRUNK SEWER #1

New Alignment from Station

21+02.74 to 24+20.10

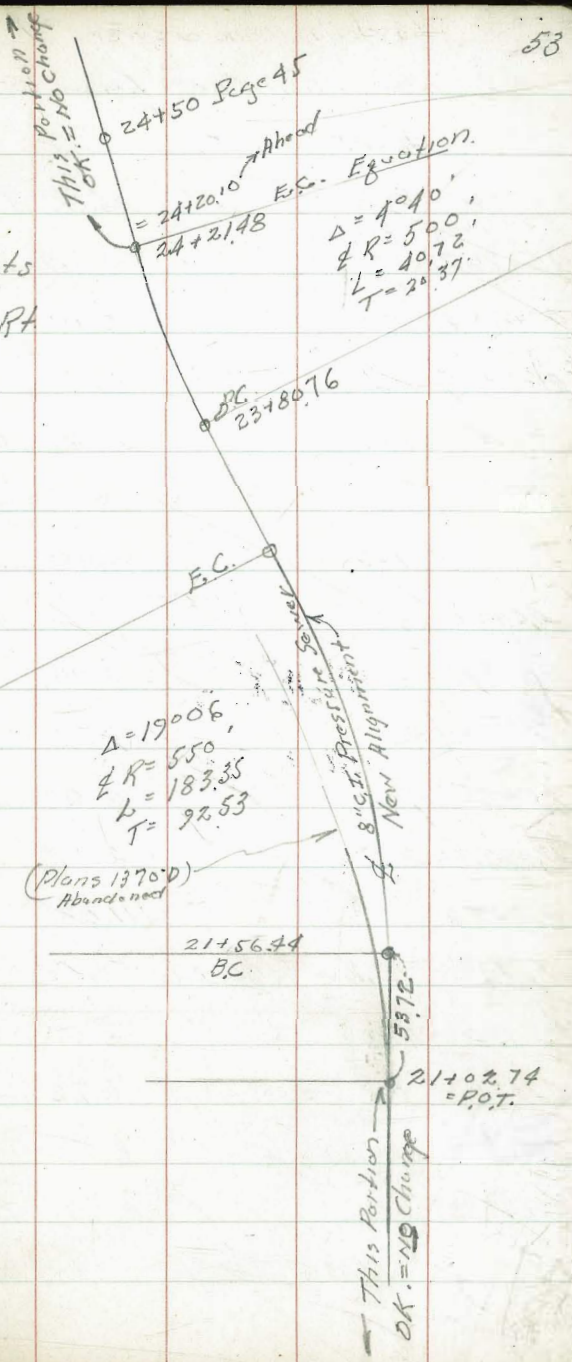
Reason for change to this location:
To clear 6" High Pressure Gas Main
at station 22+25 order Gabrielson
3-9-49 El. Flow

Station	Equation = E.C.	Cuts	Offsets
24+20.10 Ahead			
24+21.48		2.79	88.49 84.12
24+01.12		3.19	88.09 83.52
23+80.76 = B.C. RT		4.23	87.05 82.92
23+39.79 = E.C.		4.47	86.81 81.74
23+13.58		4.85	86.43 80.98
22+87.39		5.19	86.09 80.23
22+61.20		5.74	85.54 79.48
22+35.01		6.34	84.94 78.73
22+08.82		6.96	84.32 77.98
21+82.63		7.65	83.63 77.23
21+56.44 = B.C. LH		8.51	82.77 76.47

INDEXED
WK
MAY 23 1949

10.14 91.28 81.14 PM
21+02.74 = Plan B.C. = P.O.T. New Alignment 74.91

Cuts	Offsets
4.37	6' RT
4.57	"
4.13	"
5.07	"
5.45	"
5.86	"
6.06	"
6.21	"
6.34	"
6.40	"
6.30	"



La Jolla Trunk Sewer #1 - GRADES

New Alignment from Station

			Stations	4' offset	Cuts
40+85.80	to		79		
			Elev. - Elev.		
45+60 = EVC		4.87	110.67	107.35	3.44
52° Diag Bk					
45+26.22 = L.P. RT		5.62	109.94	106.22	3.72
P.V.C					
44+89.43 = E.C.		6.01	109.55	105.25	4.30
44+75 = EVC		6.37	109.19	104.95	4.24
+50 Bk		6.88	108.68	104.15	4.53
T.P.	7.35 115.56	0.18	108.21		
+25 Bk		0.99	107.85	103.40	4.45
44+00 Bk		1.69	106.70	102.35	4.35
+75 Bk		2.77	105.57	100.90	4.67
+50 Bk		4.48	103.86	99.80	4.06
43+25 = P.V.C		6.07	102.27	98.19	4.08
42+98.77 = B.C.		7.57	100.77	96.44	4.33
42+50		11.03	97.31	93.18	4.13
T.P.	12.26 108.34	0.93	96.08		
42+00 EVC		2.67	93.84	89.84	4.00
41+50 Bk		6.22	90.29	86.50	3.79
Fwd. Tan					
41+03.22 = 4' RT	} P.V.C	8.59	87.92	84.25	3.67
Bk. Tan					
41+03.22 = 6' RT		8.79	87.72	84.25	3.47
	11.86 96.51		84.65		

R. Nail. F.B. 1897-38 Sta-12+35

La Jolla Trunk Sewer #1 - Grades
New Alignment from Station

40+85.80 to 52+63.45 4' offset
El. Flow

Cuts

50+40		4.46	136.26	132.56	3.70
50+15		6.74	133.98	130.78	3.20
49+91.30 = B.C.		8.66	132.06	129.09	2.97
49+50		11.32	129.40	126.14	3.26
T.P.	12.27	140.72	0.07	128.45	
49+00	Exc.	2.90	126.12	122.58	3.54
	Brk.				
48+49.86 = E.C.		5.61	122.91	119.40	3.51
+75	Brk.	6.86	121.66	118.20	3.46
48+00	PVC	8.12	120.40	117.00	3.40
+75		9.03	119.49	115.99	3.50
+50		9.69	118.83	114.98	3.85
+25		10.48	118.04	113.97	4.07
47+00		11.31	117.21	112.97	4.24
+75		12.31	116.21	111.95	4.26
T.P.	13.05	128.52	0.09	115.47	
+50.67 = B.C.		0.33	115.23	110.97	4.26
+19.17 = E.C.		2.10	113.46	109.69	3.77
46+03.82		2.84	112.72	109.09	3.63
+88.48 = B.C.		3.44	112.12	108.49	3.63

115.56

LaSolla Trunk Sewer #1 - Grades
 New Alignment from Station

40+85.80 to 52+63.45 4' offset

Check			0.01			
354+00 = S'RT Grade Book 257		3.45	149.80 149.79	G-253	P-8	
354+02.09 = S'RT MH, 12" line " Reg. Gravity		3.35	149.89	142.95		6.94
52+63.45 - Plug End		3.58	149.66	143.15		6.51
+33 Bk.		4.00	149.24	142.40		6.84
52+00 Bk		5.64	147.60	141.35		6.25
+50 Bk		8.48	144.76	139.10		5.66
51+00 Bk		12.25	140.99	136.40		4.59
T.P. 12.58 Bk	153.24	0.06	140.66			
50+60.09 = E.C.		7.84	137.88	134.00		3.88

140.72

Walker Lg Solla Trunk Sewer #1
 Johnson & Notes & Profile Levels
 Pope
 Crawford
 3.10.49
 New Alignment from Station

58

	40+85.80	to 52+63.45	& stations
45+88.48 = B.C.		3.19	112.37
+60		4.56	111.00
45+26.22 A Pt. Rt.		6.14	109.42
44+89.43 = F.C.		6.38	109.18
+75		6.72	108.84
+50		7.24	108.32
T.P.	7.35	115.56	0.13 108.21
+25		0.81	107.53
44+00		1.90	106.94
+75		3.10	105.24
+50		4.57	103.77
43+25		6.07	102.27
42+98.77 = B.C.		7.69	100.65
42+50		11.24	97.10
T.P.	12.26	108.34	0.43 96.08
42+00		2.98	93.53
41+50		6.46	90.05
41+03.22 = A Pt. Lt.	45°	8.90	87.61
	11.86	96.51	84.65

& Nail F.B. 1847-38 Sta. 12+35

Walker & Profile Levels
 Johnson La Jolla Trunk Sewer #1
 Pope New Alignment from Stations
 Clifton
 2-10-49 40+85.80 to 52+63.45 & Stations

50+60.09 = E.C.	3.10	137.62	
+40	4.73	135.99	
50+15	6.75	133.97	
49+91.30 = B.C.	8.56	132.16	
49+50	11.59	129.13	
T.P.	12.27	140.72	0.07
49+00	2.78	125.74	
48+49.86 = E.C.	5.89	122.63	
+25	7.13	121.39	
48+00	8.40	120.12	
+75	9.26	119.26	
+50	10.05	118.47	
+25	10.86	117.66	
47+00	11.64	116.88	
+75	12.46	116.06	
T.P.	13.05	123.52	0.09
46+50.67 = B.C.	0.52	115.04	
46+19.17 = E.C.	1.92	113.64	
46+03.82	2.60	112.96	

115.52

Walker La Sotta Trunk Sewer #1
 New Alignment from Station
 40+85.80 to 52+63.45 2 Stations
 Profile Levels

			0.01	
			149.80	
354+00	5' RT	3.45	149.79	G-253 P-8
52+63.45	Plug End	3.38	149.86	
+33		4.32	148.92	
52+00		5.68	147.56	
+50		8.53	144.71	
51+00		12.47	140.77	
T.P.	12.58	153.24	0.06	140.66
			140.72	

Lafolla Trunk Sewer #1
 New location of Alignment
 in Torrey Pipes Road

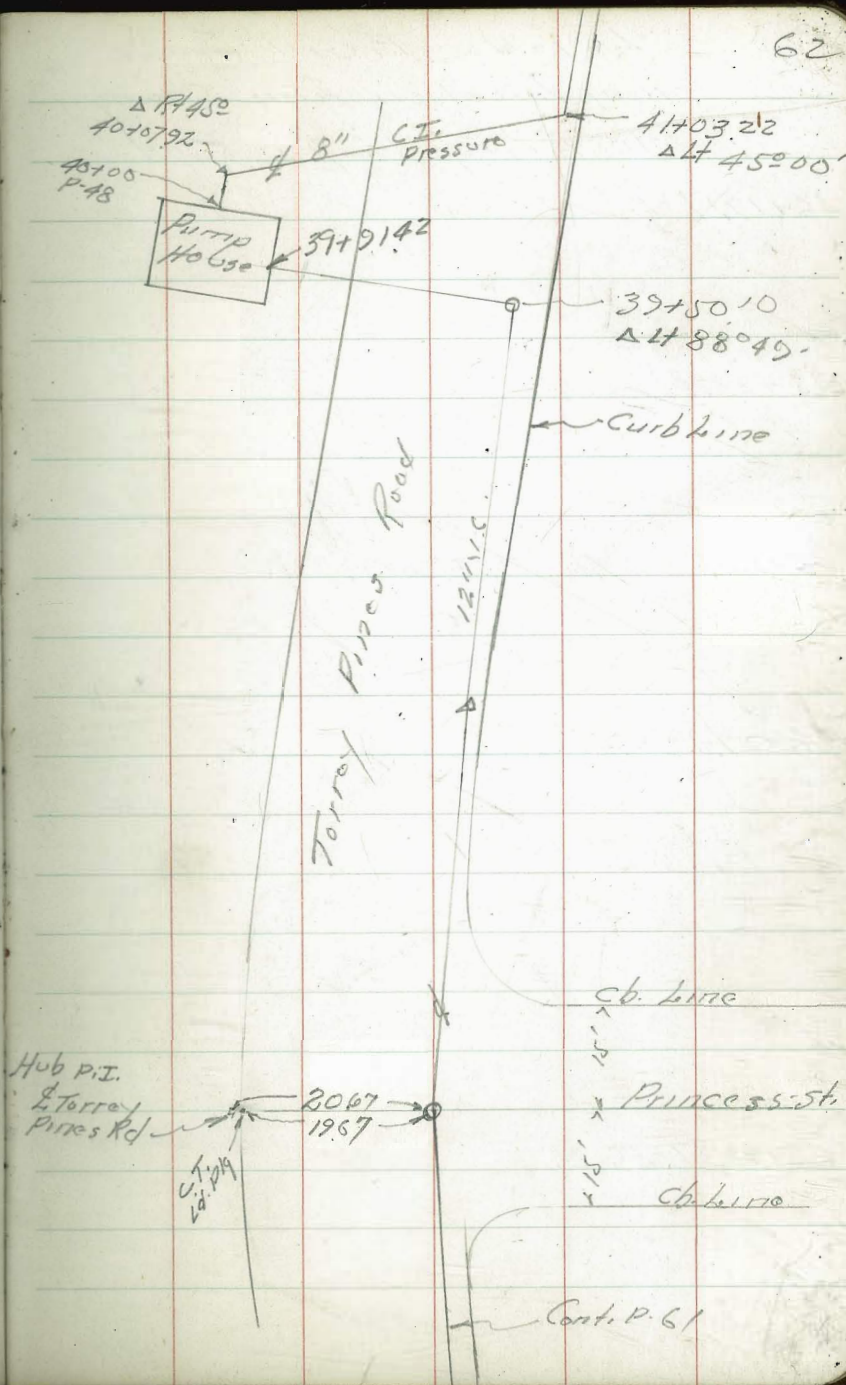
39+91.42 = Pump House

39+50.10

36+70 = Rt 1051'

35+32.23 = MH #3 Δ Rt 15° 31' 30"

62



Lapolla Trunk Sewer #1
New Location Line Change
in Turrey Pines Road

46+19.17 = E.C.

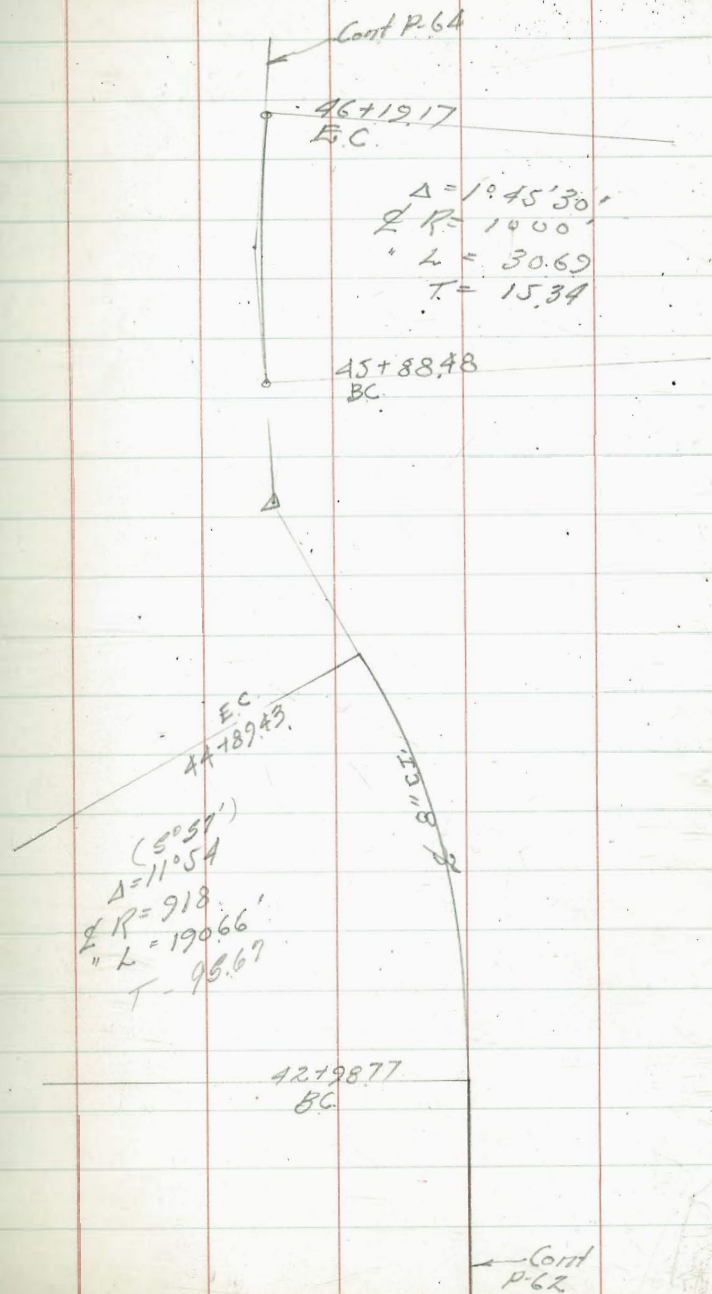
45+88.48 = B.C. RA

45+26.22 = Δ RA 23°28'30"

44+89.43 = E.C.

42+98.77 = B.C. LA

63



La Bolla Trunk Sewer #1
New location of Alignment
in Torrey Pines Road

52+65.45 = S. MH.

52+63.45 = Plg. end stub to MH

65

Cont - 66

52+65.45

52+63.45

52+62.09
60.20
54.45
60.20
54.45

Prospect Pl.
d Sewer Grade Book
253

165° 22' 30"

← Curb to 1170

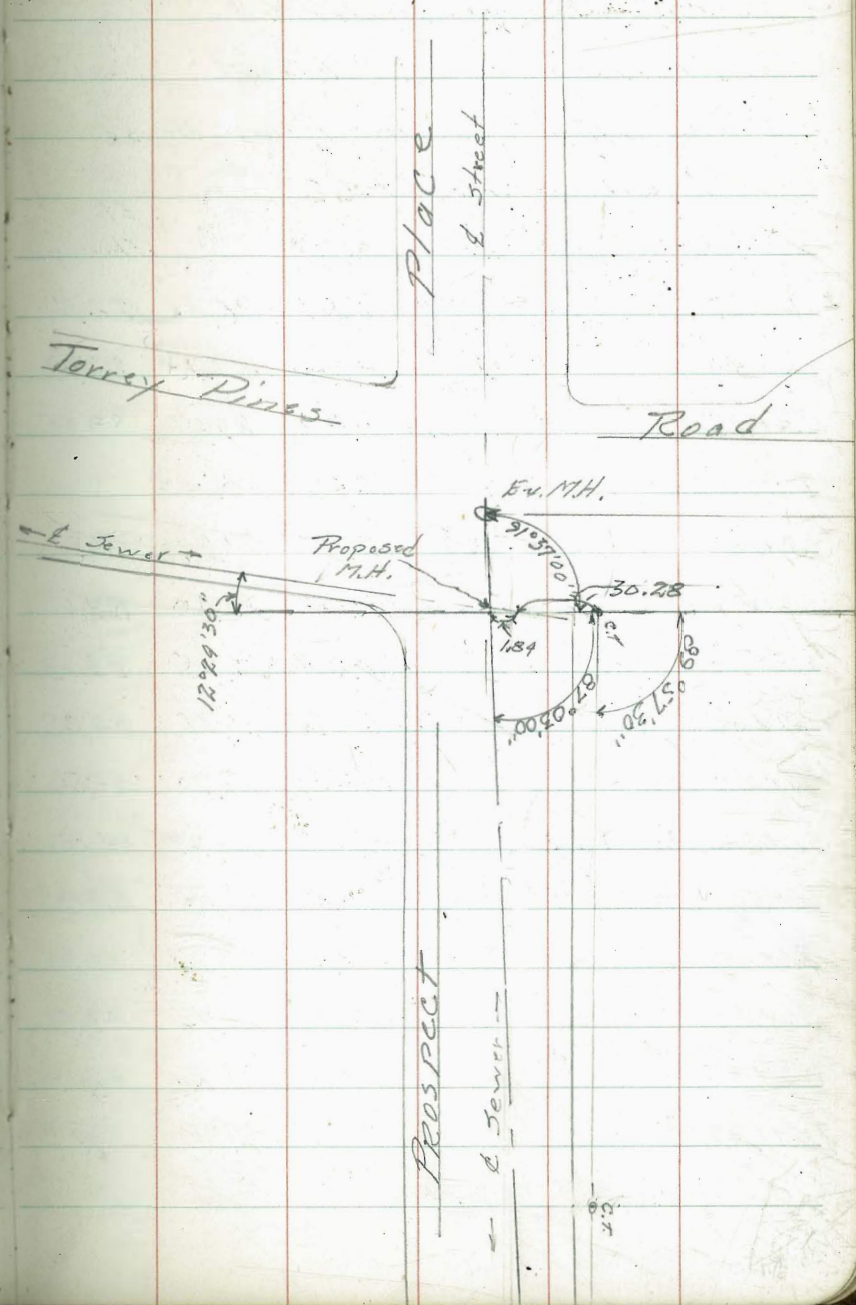
← 1.30

50+60.09
E.C.

> ← 13'

Cont. P. 64

3-14-49
 Intersection Prospect Place &
 Torrey Pines Road Ties to
 Johnson & Jewer in Both Directions
 Pope
 Crawford



GRADES

Lafolla Trunk Sewer #1
117 Torrey Pines Road
from MH #2 to Pump House
Location P-61-62

Profile
Elev.
= Top of Sewer
For Plotting

Cont. P&B			El.	Flow line	Cuts	
34+65	1	561	86.46	82.37	409	86.16
34+30		434	87.73	82.69	509	87.31
33+95		240	89.67	83.00	667	89.37
TP	162	9207	1269	90.45		
33+60		1145	91.69	83.31	838	91.36
33+25		964	93.50	83.61	989	93.17
32+90		789	95.25	83.93	1132	95.16
32+55		629	96.85	84.25	1260	96.93
32+20		524	97.90	84.56	1334	98.03
31+85	9060	421	98.93	84.87	1406	98.76
31+50		408	99.06	85.19	1387	98.84
31+15		418	98.96	85.50	1346	98.76
30+80		440	98.74	85.82	1292	98.44
30+45		457	98.57	86.13	1244	98.12
30+18.95			97.73 ^{4.16}	86.39	1134	
	682	103,14	96.32			

BM NW 1/4 P. Viking Way & Torrey Pines Rd.

La Jolla Trunk Sewer #1

Grades

				El. Flowline	Cuts.	Top Paving Profile Elev. For Plotting.
39+91.42 = End - at Pump House		P-47	78.47	76.86	1.55	
39+58		3.77	84.46	77.79	6.67	
39+50.10	MH #4 Alt 88°49'	3.49	84.74	78.01	6.73	8439
39+50.10		4.14	84.09	78.01	6.08	
39+15		6.11	82.12	78.32	3.80	8262
38+80		5.39	82.84	78.64	4.20	8292
38+45		4.83	83.40	78.95	4.45	8316
38+10		4.85	83.38	79.27	4.11	8329
37+75		4.51	83.72	79.58	4.14	8342
37+40	442 88.23	8.26	83.81	79.90	3.91	8355
37+05		8.08	83.99	80.21	3.78	8371
36+70 = ARH 1°51'		7.86	84.21	80.53	3.68	8394
36+35		7.77	84.30	80.84	3.46	8404
36+00		7.66	84.41	81.16	3.25	8424
35+65		7.98	84.09	81.47	2.62	8456
35+32.23 = ARH 15°31'30"	MH #3	7.31	84.76	81.77	2.99	8509
35+00		7.09	84.98	82.06	2.92	8535

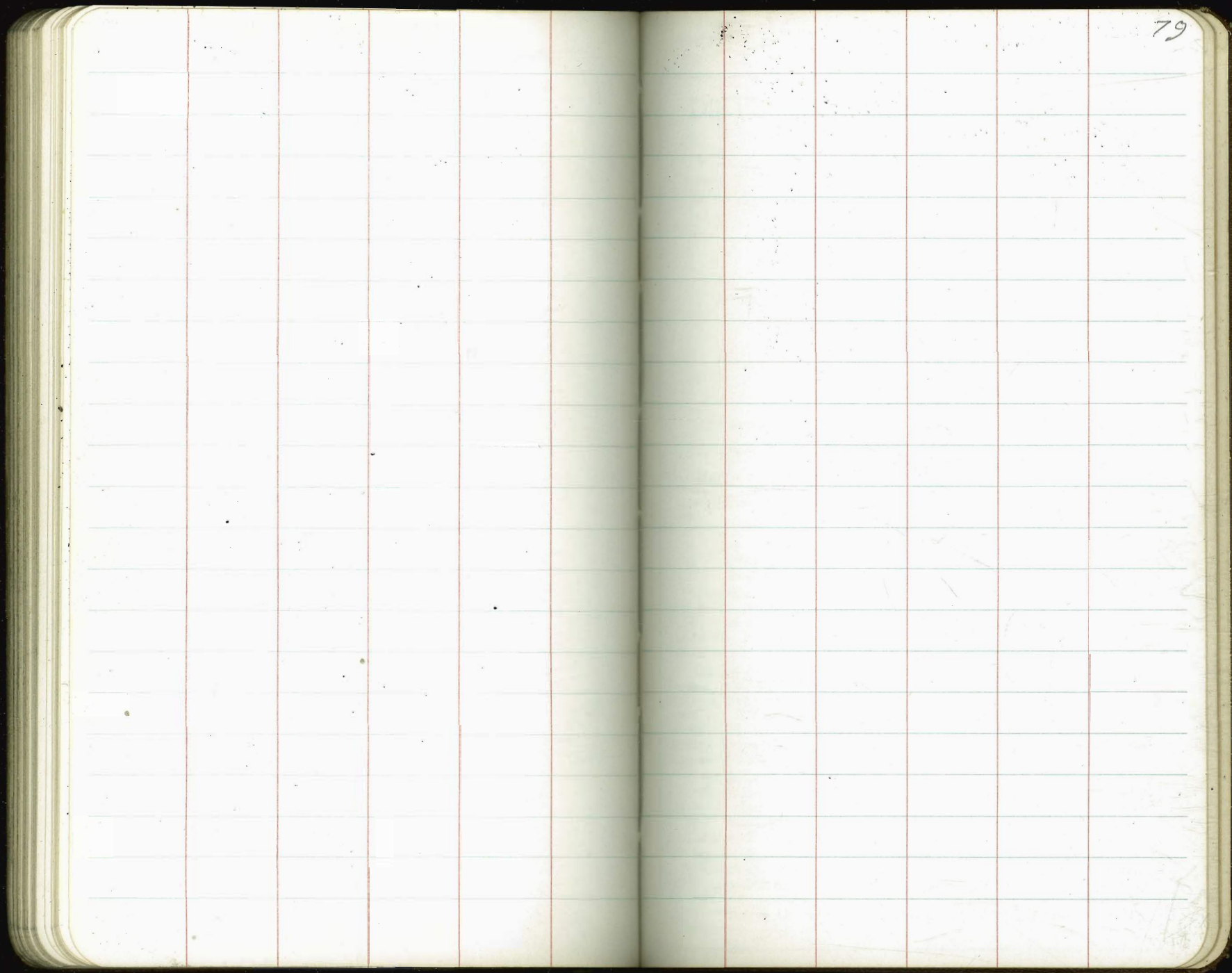
2.77%
0.900%

92.07

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both sides of each page. The notebook is bound in the center, and the pages have rounded corners. The number '70' is handwritten in the top right corner of the right page. The notebook is set against a dark, possibly black, background.

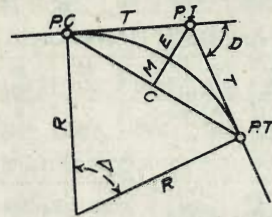


The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both sides of each page. The notebook is bound in the center, and the pages appear slightly aged with some minor smudges and discoloration. The right page has the number '75' handwritten in the top right corner. The entire notebook is set against a dark, solid background.



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos \frac{\Delta}{2}\right) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

35410209

3.16

1037
1074

179 59 60
12 24 30
167 35 30

8/8318
1662
27 8344
9976

445.70
43876
694

43301
432
2569

0+511
15.9
66.6

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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