

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

G-252

INDEXED
Completely
except page # 79

MICROFILMED

APR 13 1965

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

E. W. Alley Blk 1 - Corella Tract	57
" " Blk 2. " "	57
Morena Knoxville Nly.	58
Knoxville Sly.	58-59
Savannah (Knoxville Sly)	60
Morena Nly. + Sly. of Savannah	61+62
Naples St.	63
Weeks Knoxville to Buena	65-69
Naples ^{place} + Portions of Dorcas Cushman weeks	69-72
Cushman Naples - East	72
" Place	74

For Changes see G 246 56 to 62

F.B. 1544 + 1791

1

Locust & Evergreen	Garrison to Dickens	Finish stakes - 11	Rough Grade	2-4
Santa Barbara Pl. Sewer	+ + Alleys Blks. 109-111-116	16-17+18		
Mission Blvd.	"	4 5+6		
Cb. Stakes	Finish stakes p. 11			
Evergreen (Garrison to Fenelon)	Sewer from Nightman			7
Wabash	to 325' N.W. y.			10
Sewer laterals Blk. 116 bench	Mission			19
Sewer 1422 West of Morena Blvd.	Paul St. to Letigh.			20+21
Sewer Paul St. & Corella tract	Blk 3.			22+23
Viola St - Morena East.				23
Lillian St + (Viola - No. + So.)				25
" " Gertrud east.				27
Gertrude St. (Viola North)				26
" Dorcas "				31
Dorcas -				28+78
out Fall. (As Constructed) -				75
Pacific Hy. to Weeks + Knoxville				33
Everview Road				34
Plainview				36-40 + 46
Monitor Road				37
Hilda road - Elevation Rd				41
Brownell St.				47
Also - CROWN St.				47
Ellsworth St.				48
Savannah Street (Dorcas South)				49
Buenos + Bianca				50
Savannah Place				52
Knoxville (Weeks Nly)				54
N. + S. Alley - Corella tract				56

Rough Grade Evergreen

Garrison to Fenelon

2-8-49
W.D. 3/161

Sommermeier
McCoy
Jones

S.W.B.P. Garrison +
Locust 12.51 BM #1

2

1+00

R-2°

27.43
7.28
8.23
F 0.95

+2' BK
28.19
6.52
4.22
C 2.30

11.82
24.33
0.95
23.38
11.33
34.71
7.64

S.W.B.P. Evergreen to }
Fenelon } 25.07 BM #7

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W.K.

OCT 5 1949

0+80

0.30 BK
on wall

27.55
7.16
6.16
C 1.00

N. - 2' BK
28.33
6.38
3.71
C 2.67

Nly line
2+00 = Fenelon 25.33
9.38
7.38

26.12
8.59
8.57
0.01 BK

0+60

0.25 BK
on wall

27.50
7.21
6.21
C 1.00

0-2'
28.31
6.40
3.94
C 2.46

1+87^E

25.60

26.20

0+25 = E.C.

0.25 BK
- on wall

27.28
7.43
6.43
C 1.00

0-2'
28.15
6.56
3.77
C 2.79

1+75

0.9 BK
on wall

25.85
8.86
6.86
C 2.00

26.60
8.11
5.04
C 3.07

0+12^E

27.23

28.07

1+40

0-2°

26.72
7.99
8.46
F 0.47

27.47
7.24
4.07
C 3.17

X-1' out

0+00 = sly. line Garrison

27.18
7.53
7.53

28.10
6.61
6.61

1+20

0-2°

27.15
7.56
8.49
F 0.93

27.90
6.81
4.31
C 2.50

0-2°

Locust - Rough Grade
Garrison to Dickers

3

	Ely	Sommermeyo- Wly	Ely	Wly
2-8-49 31416 Nly Fenelon 2+00	11.07 4.27 4.21 0.06 ✓	11.82 3.52 5.57 0.01 ✓	Nly Emerson 2+00 10.35 7.10 7.12 0.02 ✓	11.10 6.35 6.39 0.04
INDEXED W.K. OCT 5 1949 1+75	0-2' 11.00 4.34 4.44 FO.10	0-2' 11.60 3.74 2.02 C 1.72	1+75 10.47 6.98 6.66 C 0.32	0-2' 10.97 6.48 4.18 C 2.30
BM#1 P2 1+25	0-2' 10.74 4.60 6.24 F.T.G. 4	0-2' 11.40 3.94 2.23 C 1.61	1+25 10.65 6.80 6.88 FO.08	X-2' 11.15 6.30 4.49 C 7.81
BM#3 S.W. 74 Prop L.T. Fenelon Locust 0+75	0-2' 10.47 9.87 5.85 FO.98	0-2' 11.20 4.14 2.45 C 1.69	0+75 10.83 6.62 7.24 FO.62	0-2' 11.33 6.12 4.50 C 1.62
S.E. Disk - BM#4 Emerson & Locust	0-2' 10.20 5.14 4.71 C 0.43	0-2' 11.00 4.34 2.68 C 1.66	0+25 11.00 6.45 6.52 FO.09	0-2' 11.50 5.95 4.19 C 1.76
Sly. Garrison 0+00	10.03 5.31 5.32 -0.01 ✓	11.10 4.24	Sly Fenelon 0+00 11.10 6.35 ✓	11.98 5.47 ✓
	X 15.34		X 17.45	

Locust
Rough grade

4

Nly Dickens
2+00

Ely

Wly

Meet Curbs.
1+00

12.77
4.68
4.70
- .02

13.32
4.12
4.07
- .02

0+62^E

+ - 1'
12.11
5.34
4.76
0.58

+ - 2'
17.66
4.79
3.10
1.69

0+25

11.45
6.00
4.80
1.20

+ - 2'
12.00
3.45
3.67
1.78

Sly Emerson
0+00

11.20
6.25
6.22
.03

11.80
5.65
5.66
.01

17.45

Santa Barbara Place
+ Mission Blvd. Sewer

2-9-49
W.O. 60267
Plan. - L-7175

INDEXED
OCT 5 1949

Sommermeier
McCoy
Jones

Santa Barbara Place (358' of Line)

0+00 = M.H.#1 @ Santa Barbara Place
and Bay Side Lane
stakes set 10' Right (North)

M.H.#1	□	□	N	N
Cross 10+00	0+00	0+80	1+20	1+60
-7.70	-7.50	-7.30	-7.10	-6.90
12.03	11.83	11.63	11.43	11.23
5.24	5.04	5.26	5.02	4.97
C 6.79	C 6.74	C 6.37	C 6.41	C 6.29
□	□	N	N	
2+00	0+00	1+80	3+20	3+58 = M.H.#2
-6.70	-6.50	-6.30	-6.10	-5.91
11.03	10.83	10.63	10.43	10.24
4.86	4.71	4.63	4.63	4.86
C 6.17	C 5.92	C 6.00	C 5.80	C 5.38

BM#1 = B.P. Seewall @ Santa Barbara

7.03	
2.45	
9.48	
7.75	
-0.27	
4.60	
4.33	
4.86	
-0.53	
5.32	
4.79 = X#2	
2.10	
2.69	
	2.69
	8.18
	8.87 = π
	-3.83
	BM 7.04 ✓

□ = stub
N = Nail in pave.
+ = cross in conc.

(Pave. 2.42)
72)

Mission Blvd. line (6' East of cb. face) 5
Cuts marked on curb.

0+00 = 103' So. of Santa Barbara
M.H.# set on Santa Barbara and 65 south of
North line of alleys (07,7175-4)

M.H.#5	+	+	+	N	M.H.#2
0+00	0+34.33	0+68.66	1+03.1401		
-5.00	-5.27	-5.54	-5.82		
7.79	10.06	10.33	10.61		
5.28	4.74	4.84	5.32		
C 4.51	C 5.32	C 5.49	C 5.29		
	C 5.17	C 5.38	C 5.56		

+	+	N	M.H.#3	
1+37.22	1+71.66	2+06.1	2+46	
-5.64	-5.46	-5.29	-5.09	-4.99
10.43	10.25	10.08	9.88	9.80
4.99	5.18	5.53	5.11	5.15
C 5.44	C 5.12	C 4.70	C 4.55	C 4.88
	C 5.32			

+	+	+	M.H.#4 N
2+86	3+26	3+66	3+98
-4.89	-4.69	-4.49	-4.33
7.68	7.48	7.28	7.12
5.23	5.25	5.38	5.22
C 4.45	C 4.23	C 3.90	C 3.77
	C 4.24	C 4.09	C 3.81

4.79 π

M.H.# R.P.s are 6' + 16' wly. of ctr. M.H.

parallel to Alley line 6' = Nail + 16' = cross

M.H.#5 =	-5.00	0+34.33
	0 4.51	-5.27
6' Nail =	-0.49	10.35
	5.57	5.02
	5.08	C 5.33
	5.41	
	-0.33	
	5.14	
	4.81	

Extra cuts
on mean of
orig. stations
of cuts.

3/7/49

Restake Santa Barbara
 (From page 5) 2/11/49

0+15	No.
<u>7.62</u>	<u>-7.62</u>
11.87	11.87
<u>5.32</u>	<u>5.24</u>
C 6.55	C 6.63

0+25
<u>7.57</u>
11.82
<u>5.10</u>
C 6.80

Stakes 6' N of sewer

6

Nail or cross 6' North of \neq

0+00	0+20	0+40	0+60	0+80
-7.70	7.60	-7.50	-7.40	-7.30
	11.87	11.73	11.65	11.55
	5.32	5.09	5.10	5.05
	C 6.53	C 6.66	C 6.55	C 6.50

1+00	1+20	1+40	1+60	1+80	2+00
<u>-7.20</u>	<u>-7.10</u>	<u>-7.00</u>	<u>-6.90</u>	<u>-6.80</u>	<u>-6.70</u>
11.45	11.35	11.25	11.15	11.05	10.95
<u>5.08</u>	<u>4.95</u>	<u>4.96</u>	<u>4.95</u>	<u>4.89</u>	<u>4.89</u>
C 6.37	C 6.40	C 6.29	C 6.20	C 6.16	C 6.06

2+20	2+40	2+60	2+80	3+00
<u>-6.60</u>	<u>-6.50</u>	<u>-6.40</u>	<u>-6.30</u>	<u>-6.20</u>
10.85	10.75	10.65	10.55	10.45
<u>4.93</u>	<u>4.85</u>	<u>4.82</u>	<u>4.65</u>	<u>5.09</u>
C 5.92	C 5.90	C 5.83	C 5.90	C 5.36

3+20	3+40	M.H.#2 3+52 6' west -5.91	0+00 stake B5 E.L. = -0.91 5.16 <u>4.257</u>
<u>-6.10</u>	<u>-6.00</u>	10.16	
10.35	10.25	4.78	
<u>4.52</u>	<u>4.32</u>		
C 5.83	C 5.93	C 5.38	

Cb. stakes Evergreen 2/16/49
 Garrison to Fenelon Sommermayer
 W.O. 31461 A1107
 Jones

BM #2-P2
 25.07
 6.07
 31.14

7

1+00

27.43
 3.71
 x

28.19
 2.95
 x

INDEXED

Nly Fenelon
 2+00

25.33
 5.81

26.12
 5.02 ✓

W.K.
 OCT 5 1949
 0+80

27.55
 3.59
 x

28.33
 2.81
 x

1+87^E

25.60
 5.54
 x

26.20
 4.94
 x

0+60

27.50
 3.64
 x

28.31
 2.83
 x

B.C.
 0+25

27.28
 3.86
 x

28.15
 2.99
 x

Cl. B.C.
 1+75

25.85
 5.29
 x

26.60
 4.54
 x

0+125

27.23
 3.91
 x

28.07
 3.07
 x

1+40

26.72
 4.42
 x

27.17
 3.67
 x

Sly Garrison
 0+00

27.18
 3.96
 3.98
 -0.02

28.07
 3.07
 x

1+20

27.15
 3.99
 x

27.90
 3.24
 x

Locust Cb. stakes
Garrison to Fenelon

2/15/49

Nly. Fenelon
2+00

$\frac{11.07}{4.57}$

1+875

INDEXED

W.K.

OCT 5 1949

$\frac{11.04}{4.50}$
X

1+75

B.M. #3 #3

11.21
3.43
15.64

Rake

$\frac{11.00}{4.64}$
X

0+25

$\frac{10.20}{5.44}$
X

0+125

$\frac{10.10}{5.54}$
X

Sly Garrison
0+00

$\frac{10.03}{5.61}$

Sommitormeyer
Allen
Jones

$\frac{11.82}{3.82}$

$\frac{11.70}{3.94}$
X

$\frac{11.60}{4.04}$
X

$\frac{11.00}{4.64}$
X

$\frac{10.95}{4.69}$
X

$\frac{11.10}{4.54}$
4.50
0.102

Locust Cb. Stakes
Fenelon to Emerson

2/15/49

8

Nly. Emerson
2+00

$\frac{10.35}{5.31}$

INDEXED

W.K.

OCT 5 1949

1+875

$\frac{10.40}{5.26}$
X

1+75

$\frac{10.47}{5.17}$
X

Rake

0+25 = EG

$\frac{11.00}{4.66}$
X

0+125

$\frac{11.05}{4.61}$
X

Sly Fenelon
0+00

$\frac{11.10}{4.56}$

$\frac{11.10}{4.56}$
4.58
0.02

B.M. #4
A.3

11.05
4.61
15.66

$\frac{11.00}{4.66}$
X

$\frac{10.97}{4.69}$
X

$\frac{11.50}{4.16}$
X

$\frac{11.75}{3.91}$
X

$\frac{11.98}{3.68}$

Locust. Gb. Stakes
Emerson to 100' Sly.

INDEXED

OCT ^{W.K.} 5 1949

BM #4, P.3.

11.05
6.39
17.44 X

Exit db.
1+00

12.77
4.67

13.32
4.12

0+02⁵

12.11
5.33
X

12.66
4.78
X

0+25 = E.C.

11.45
5.97
X

12.00
5.44
X

0+12⁵

11.32
5.12
X

11.92
5.62
X

Sly. Emerson

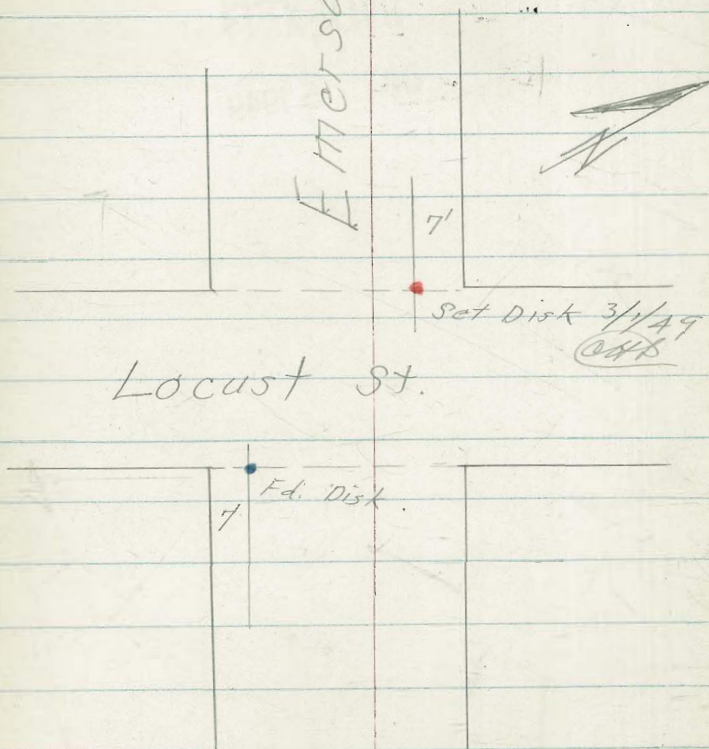
0+00

11.20
6.24

11.80
5.64
5.66
-2.02

Emerson St.

9



Stake Sewer Wabash Ave
From Wightman to 325 N. W. 14.

10

4/19/49
W.O.# 60136

INDEXED
M.K.
OCT 5 1949

Sommermayor
Allen
Jones

Grades set as per 2577-B.

S.W.B.P.
Nilo + Univ.

M.H. #1 - End.

1+50

315.15
14.42
6.15
C-8.29

322.15
11.30
333.45
5.85
327.60
1.97

3+25

320.92
8.65
0.00
C-8.65

1+25

314.33
15.24
7.15
C-8.09

327.57 X

3+00

320.10
9.47
0.73
C-8.74

1+00

313.50
16.07
8.21
C-7.86

2+75

319.27
10.30
1.40
C-8.84

0+75

312.68
16.89
9.02
C-7.87

2+50

318.44
11.13
2.30
C-8.93

0+50

311.85
17.72
9.97
C-7.85

2+25

317.62
11.95
3.25
C-8.70

0+25

311.03
18.54
10.84
C-7.70

2+00

316.79
12.78
4.11
C-8.67

2 Wightman
0+00 = Exist M.H.

310.20

Exist. M.H.
310.00
19.57
19.80
0.23

1+75

315.97
13.60
5.00
C-8.60

Finish stakes Evergreen

Garrison to Fenelon

summermajor
3-1-49

INDEXED

OCT 5 1949

W.K.

1+40

Elevations shown
are finish grade

1+20

1+00

B.M. #2 page 2 = 25.07
7.02

Curb. Cut 7 = 32.09 x

0+80

0+60

0+42.5

0+25 = E.C. cl.

0+12.5

0+00 = Sly. line Garrison

East
Gutter

East
1/4

±

West
1/4

11
West
Gutter

26.22
5.87 ✓

26.66

26.94

27.03

26.97
5.12 ✓

26.65
5.44 ✓

27.09

27.37

27.46

27.40
4.69 ✓

26.93
5.16 ✓

27.37

27.65

27.75

27.69
4.90 ✓

27.05
5.04 ✓

27.59

27.78

27.88

27.83
4.26 ✓

27.00
5.09 ✓

27.46

27.75

26.86

27.81
4.28 ✓

26.89
5.20 ✓

27.36

27.60

27.78

27.73
4.36 ✓

26.78
5.31 ✓

27.25

27.56

27.70

27.65
4.44 ✓

26.73
5.36 ✓

27.20

27.49

27.62

27.57
4.52 ✓

26.58
5.51
5.53
-0.02

27.02

27.34

27.49

27.52
4.57
4.60
-0.03

Evergreen St.
Garrison to Fenelon

Finish stakes

12

East Butter	East VA	#	West VA	w. Butter
----------------	------------	---	------------	--------------

2+00 = Nly. line Fenelon

<u>24.69</u>	24.96	25.31	25.49	<u>25.60</u>
7.90 ✓				6.99 ✓

1+87⁵

<u>25.05</u>	25.25	25.69	25.77	<u>25.90</u>
7.04 ✓				6.39 ✓

1+75 = d. B.C.

<u>25.35</u>	25.79	26.07	26.19	<u>26.10</u>
6.74 ✓				5.99 ✓

175
1+57⁵

<u>25.78</u>	26.23	26.50	26.60	<u>26.53</u>
6.31 ✓				5.56 ✓

Locust St.
Finish Grade
Garrison to Dickens

INDEXED

OCT 5 1949

Elevations shown
are finish grade

East Gutter	East 1/4	±	West 1/4	West Gutter
----------------	-------------	---	-------------	----------------

2+00 = Nly. line Fenelon St.

$$\frac{10.69}{4.69 \checkmark}$$

10.95

11.13

11.27

11.35

4.103 ✓

1+87^E

B.M. #3 Page 3

$$\frac{10.54}{4.87 \checkmark}$$

10.97

11.21

11.30

11.20

4.18 ✓

12.21

3.17

Ch. cut $\pi = \rightarrow 15.38 - \pi$

1+75 = ch. B.C.

$$\frac{10.50}{4.88 \checkmark}$$

10.91

11.14

11.21

11.10

4.28 ✓

Rate /

0+25 = E.C.

$$\frac{9.70}{5.68 \checkmark}$$

10.16

10.44

10.56

10.50

4.88 ✓

0+12^E

$$\frac{19.00}{5.78 \checkmark}$$

10.08

10.37

10.50

10.45

4.93 ✓

0+00 = Sly. line Garrison

$$\frac{9.97}{5.01}$$

$$\frac{5.97}{-0.04}$$

9.73

10.25

10.45

10.49

4.89 ✓

Locust St.

Garrison to Dickens

East utter	East 1/2	2	West 1/2	West utter
---------------	-------------	--------------	-------------	---------------

2400 = Nly. line Emerson

12.21 = 017#3 - P.3
 3.15
 15.36

9.85	10.13	10.40	10.51	10.60
5.51				4.76
5.59*				Broken
0.07				

1787⁵

9.90	10.31	10.54	10.61	10.50
5.46 ^v				4.86 ^v

1775 = cl. B.C.

9.97	10.35	10.56	10.61	10.47
5.39 ^v				4.89 ^v

Rake

0+15 = cl. E.C.

* 15138
 From Page 13

10.50	10.89	11.09	11.14	11.00
4.88 ^v				4.38 ^v

0+12⁵

10.55	10.98	11.24	11.33	11.25
4.83 ^v				4.13 ^v

0+00 = Sly. Fenelon

10.66	10.96	11.20	11.37	11.47
4.72 ^v				3.91
				3.93
				0.102

Locust St
Finish Grade

	East Gutter	East 1/4	2	West 1/4	West Gutter
2+00 = My line Dickens	$\frac{14.42}{0.94}$	14.66	14.87	14.93	$\frac{14.96}{0.40}$
1+87 ^E	$\frac{14.20}{1.16V}$	14.59	14.79	14.84	$\frac{14.70}{0.76V}$
1+75 = cl. B.C.	$\frac{13.95}{1.41V}$	14.34	14.54	14.59	$\frac{14.45}{0.91V}$
Rake					
1+00 = B.K.	$\frac{12.27}{3.09V}$	12.67	12.89	12.94	$\frac{12.82}{2.54V}$
Rake					
0+25 = cl. E.C.	$\frac{10.95}{4.41V}$	11.35	11.57	11.62	$\frac{11.50}{3.86V}$
0+12 ^E	$\frac{10.82}{4.54V}$	11.14	11.32	11.39	$\frac{11.32}{4.04V}$
0+00 = Sly line Emerson	$\frac{10.70}{4.66}$ $\frac{1.62}{4.04}$	10.89	11.05	11.19	$\frac{11.30}{4.06}$ $\frac{4.05}{0.02}$

B.M. # . Page

Sewer Alley BIK 108, M. Beach.

3/31/49

G 242 for paving

16

W.O. 60267

stakes A'Lt & sewer

B.P. in Seawall
at Santa Barbara

INDEXED

W.K.
OCT 5 1949

7.03
1.77
x 8.80

1+50

-3.82
12.62
9.36
C-3.26

1+25

-4.00
12.80
9.45
C-3.35

3+15 M.H. #6

-2.60
11.40
2.75
C-8.45

1+00

-4.18
12.98
9.47
C-3.51

3+00

-2.74
11.54
3.42
C-8.12

0+75

-4.36
13.16
9.30
C-3.80

2+75

-2.92
11.72
5.07
C-6.65

0+50

-4.54
13.34
9.27
C-4.07

2+50

-3.10
11.90
6.46
C-5.44

0+25

-4.72
13.52
8.91
C-4.61

2+25

-3.28
12.08
7.25
C-4.83

0+16

3/15/49

4.66
-4.78
9.44
4.72
C-4.72
4.66
-4.90
9.56
7.57
-0.91

C.R.P. Nail P5

-5.00 = M.H. BT,
C 4.51

-0.29 = EL. G. Nail
5.15 = Rod
-4.66 = X

0+00 = M.H. #5 P.5

0+00

2+00

-3.46
12.26
8.26
C-4.00

1+75

-3.64
12.44
8.93
C-3.51

Sewer BIK. III. Mission Beach

N.O. 60267

3-17-49

Sommerneyer

INDEXED

W.K.
OCT 5 1949

M.H. cross 2' x 10' ft.

stakes 4' Lt of sewer

B.P. in seawall
& Santa Barbara Pl.

703
2.04
9.075

1+50

- 2.63
11.70
8.34
3.36

1+25

- 3.06
12.13
8.81
3.32

1+00

- 3.48
12.55
9.20
3.35

0+75

- 3.91
12.98
9.17
3.81

0+50

- 4.33
13.40
7.08
4.32

0+25

- 4.76
13.83
9.14
4.69

0+16

- 4.91
13.98
9.31
4.65

0+00 = M.H.# 3 - P.5

0.00

4.65
- 4.91
7.59
4.92
4.67
0.00
5.18
7.86
5.42
4.49

C'RIP Nail
M.H.#3 - P.5
M.H.#1: - 5.19
cut. 4.55
- 0.74 No. 11
5.14
- 4.68X

2+75 = M.H.# 7

- 0.50
9.57
3.67
5.90

2+50

- 0.93
10.00
4.26
5.74

2+25

- 1.35
10.42
5.48
4.74

2+00

- 1.78
10.85
9.79
4.06

1+75

- 2.20
11.27
7.69
3.64

Sewer Alley BIK. 116 Mission Beach.

Semmermeyer
Allen
Jones

W.O. 60267

1+00

-2.35	0.39	-2.35
8.73	6.05	+2.62
6.05	0.37	0.3 El. St. H.
<u>2.28</u>		4.19
		<u>4.51</u>

INDEXED

W.K.

OCT 5 1949

0+75

-2.81
9.19
6.64
<u>2.55</u>

2+28 ⁺ = Exist. M.H.	0.00
	6.38
	0.44
	<u>6.82</u>

0+50

-3.27
9.65
6.65
<u>3.00</u>

2+00	-0.50	El. stake = 4.90
	6.88	
	1.48	
	<u>5.40</u>	

0+25

-3.73
10.11
6.64
<u>3.47</u>

1+75	-0.96
	7.34
	3.04
	<u>4.30</u>

0+26

-3.91
10.29
6.85
<u>3.44</u>

G.R.P. Nail
M.H. #A-P.S.
El. M.H. (P.S.)
-4.83
0.37
-0.96 El. Nail
7.34
<u>+6.38</u>

1+50	-1.42
	7.80
	4.28
	<u>3.52</u>

M.H. #A = 0+00

-4.20
10.58

1+25	-1.88
	8.26
	5.23
	<u>3.03</u>

3-17-49
W.O. 31363

BIK. 116 Mission Beach.
Sewer laterals Summermeys
McCoy,
Alford
Jones
As shown on L sheet #7055L

#1	#2	#3	#4
4.51x	4.51x	7.06x	7.06x
-3.41	-2.55	-0.75	-0.27
<u>7.72</u>	<u>7.06</u>	<u>7.81</u>	<u>7.33</u>
<u>4.82</u>	<u>4.72</u>	<u>3.89</u>	<u>2.28</u>
C-3.10	C-2.34	C-3.92	C-5.05
sta. 200 stub, Page 18	4.00	4.51	6.55
	2.16	<u>7.06</u>	0.51
			4.70

Alley BIK. 111

#5	#6	#7	#8	X
-3.86	-3.38	-2.88	-3.04	9.07
<u>12.93</u>	<u>12.45</u>	<u>11.75</u>	<u>12.11</u>	From
<u>7.80</u>	<u>9.23</u>	<u>8.34</u>	<u>8.64</u>	P. 17
C-3.63	C-3.22	C-3.61	C-3.47	
#9	#10	#11		
-2.38	-2.35	-1.84		
<u>11.45</u>	<u>11.42</u>	<u>10.91</u>		
<u>8.40</u>	<u>8.06</u>	<u>7.21</u>		
C-3.05	C-3.36	C-3.70		

3/31/49 BIK. 108 Mission Beach 19
Sewer laterals.
stakes 3' Back

#12	#13	#14	#15
-4.43	-3.83	-5.61	-2.83
<u>13.23</u>	<u>12.63</u>	<u>12.41</u>	<u>11.63</u>
<u>8.77</u>	<u>9.40</u>	<u>9.40</u>	<u>6.57</u>
C-4.46	C-3.23	C-3.01	C-5.06
#16	#17	#18	
-2.67	-2.59	-2.41	
<u>11.47</u>	<u>11.39</u>	<u>11.21</u>	
<u>5.29</u>	<u>5.65</u>	<u>4.08</u>	
C-6.18	C-5.74	C-7.13	
	8.08x		X, from
			P. 16 = 8.80

Sewer 142' west of Morena
(overlook Hqts. sewer)
Paul St. to Lehigh

9+18' Lt. (North) 3.30 = X
3+83 0.53
11.H.#90 12.77
7.77
C 5.00 on nail 9' North of E

3-29-49
W.O.#31508

Sommermeier
Allen
Jones

3+75

0.50

Grades & line from sheet 1343-D

T.P.

FB 1791
50.

8.27 X
0.40
7.87
4.08
C-3.79

stakes set 4' South unless noted.

otherwise

1+50
-0.40
8.67
4.74
C-3.93

8.4
5.08
3.19

+25

0.30
7.97
4.30
C-3.67

INDEXED

W.K.
OCT 5 1949

-0.50
8.27 X
8.77
3.92
4.77
C 4.00
4.35
8.95

3+00

0.20
8.07
4.20
C 3.87

1+00

-0.60
8.87
5.02
C-3.85

13.30 X

+75

0.10
8.17
4.31
C-3.66

+75

0.40%

-0.70
8.97
5.00
C 3.97

+50

0.40%

0.00
8.27
4.39
C-3.88

+50

-0.80
9.07
4.89
C-4.18

+25

-0.10
8.37
4.50
C-3.87

0+25

-0.90
9.17
5.89
C 3.98

2+00

-0.20
8.47
4.67
C-3.80

0+00 = M.H.#89

-1.00
9.27
6.13
C 3.14

1+75

-0.30
8.57
4.75
C-3.82

8.27

(B.M.#1)

Morena - 5.08 1991
13

B.M.# = B.P. N.W. Head wall, Box Culvert Morena + Lehigh = 10.04 - & Chisox. in M.H. Paul + W. 1/2, Rm

+ 75

$$\begin{array}{r} 1.30 \\ 12.00 \\ 7.97 \\ \hline C-4.03 \end{array}$$

+ 50

$$\begin{array}{r} 1.20 \\ 12.10 \\ 8.07 \\ \hline C-4.03 \end{array}$$

+ 25

$$\begin{array}{r} 1.10 \\ 12.20 \\ 8.27 \\ \hline C-3.93 \end{array}$$

5 + 00

$$\begin{array}{r} 1.00 \\ 12.30 \\ 8.30 \\ \hline C-4.00 \end{array}$$

+ 75

0.40%

$$\begin{array}{r} 0.90 \\ 12.40 \\ 8.30 \\ \hline C-4.10 \end{array}$$

+ 50

$$\begin{array}{r} 0.80 \\ 12.50 \\ 8.43 \\ \hline C-4.07 \end{array}$$

+ 25

$$\begin{array}{r} 0.70 \\ 12.60 \\ 8.42 \\ \hline C-4.18 \end{array}$$

4 + 00

$$\begin{array}{r} 0.60 \\ 12.70 \\ 8.78 \\ \hline C-3.92 \end{array}$$
13.30

M.H. # 91

6 + 78

$$\begin{array}{r} 0-454 \\ + 50 \end{array}$$

$$\begin{array}{r} 1.60 \\ 11.70 \\ 5.52 \\ \hline C-6.18 \end{array}$$

+ 25

0.40%

6 + 00

$$\begin{array}{r} 1.40 \\ 11.90 \\ 7.35 \\ \hline C-4.55 \end{array}$$

$$\begin{array}{r} 1.71 \\ 11.59 \\ 7.86 \\ \hline C-3.73 \end{array}$$

$$\begin{array}{r} 13.30 \\ 3.27 \\ 14.03 = B.P. \\ - 0.01 \text{ solvent} \\ \hline (B-20) \\ = 10.04 \end{array}$$

$$\begin{array}{r} 1.50 \\ 11.80 \\ 8.76 \\ \hline C-3.04 \end{array}$$
13.30

Paul St. & BIK.3 Corella tract.

3-30-49
W.O. 31508

Sammormayo-
Allen
Jones

stakes 4⁵' Rt. unless
otherwise noted

22

Grades + line as per sheet 1345-D

M.H.# 87
1+94.80

Tied 637+1274
Rt. on Δ split.

INDEXED

OCT 5 1949

-0.06

9.73

4.86

C-4.87

B.M.#1 (R20)

5.08

4.59

9.67 X

1+50

-0.24

9.91

4.93

C-4.98

P149
4+17.52

0.83

8.84

4.02

C-4.82

1+00

-0.44

10.11

5.01

C-5.10

3+72.52

0.65

9.02

4.12

C-4.90

0+50

-0.64

10.31

4.54

C-5.77

(P. 23)
(= 0+00 TO N.E.)

M.H.# 86

3+27.52

45+95 Rt.

0.47

9.20

4.40

C-4.80

M.H.# 88

0+33.90

Tied 492+984
Rt.
on Δ split.

-0.70

10.37

4.25

C-6.12

2+90

0.32

7.35

4.68

C-4.67

EXIST. M.H.
0+00

-0.84

10.51

4.89

C-5.62

2+40

+0.12

9.55

4.64

C-4.91

967 X

BIK.3 Carella Tract. Cont.

INDEXED

OCT 6 1949

P149
1+68

1.24
8.43
4.20
C- 4.23

1+26

1.08
8.57
4.27
C- 4.32

0+84

0.91
8.96
4.18
C- 4.58

0+42 0

0.74
8.93
4.31
C- 4.62

0+00 M.H. 86
3+27.52 (P.22)

0.57
9.10
4.40
C- 4.70

Viola St. (Sheet 134AD) 23
Morona to Lillian
stakes 45 ft. of line.

459 +
Δ 22°-14' Lt. 9.18 ft.
M.H. 30
2+89 93 (Tary = .88)
Gertrude
to south.

35.51
9.53
1.50
C- 8.03

INDEXED

OCT 6 1949

2+50

10.896

W. K.

31.20
13.84
6.25
C- 7.59

2+00

X From P.24
45.04
25.80

19.24

11.29

7.95

33.36 X

M.H. 29
1+65 56 45+9' Rt.
Gertrude St
to north

22.03

11.33

2.40
C- 8.93

22.08 ↑
11.28

1+50

21.25
12.11
3.59
C- 8.52

1+00

18.75
14.61
7.22
C- 7.39

0+50

5.96

16.25
17.11
10.10
C- 7.01

M.H. 28
0+00
Morona
635 + 12 7/8 ft.

13.75
79.61
11.89
C- 7.72

33.36 From Page 24.

Viola St.

5+50

$$\begin{array}{r} 58.62 \\ 7.83 \\ 0.70 \\ \hline C-6.93 \end{array} \text{ T.P.}$$

5+00

8.20%

$$\begin{array}{r} 54.52 \\ 11.93 \\ 1.46 \\ \hline C-7.17 \end{array}$$

4+50

$$\begin{array}{r} 66.45 \times \\ 50.12 \\ 16.03 \\ 8.16 \\ \hline C-7.87 \end{array}$$

A 21'-11" Lt. (Tan = .83)
4+00 $\frac{12}{12}$ M.H. #31
4.58 + 9.16 Rt.

$$\begin{array}{r} 46.32 \\ 10.66 \text{ over-rite} \\ 2.64 \\ \hline C-8.02 \end{array} \text{ T.P.}$$

see Q146
59

3+50

$$\begin{array}{r} 41.40 \\ 15.58 \\ 7.04 \\ \hline C-8.54 \end{array}$$
2+11
3+00

9.82%

$$\begin{array}{r} 56.98 \times \\ 36.49 \\ 20.49 \\ 12.33 \\ \hline C-8.16 \end{array}$$
Sheet
Viola St. (1344-D)S.W. Mon. Dorcas
& Morena 16.19 BM#1
$$\begin{array}{r} 7.85 \\ 23.54 \\ 3.86 \\ \hline 20.38 \\ 4.66 \\ 25.04 \\ 3.67 \\ \hline 21.37 \\ 11.99 \\ 53.36 \times \\ 0.33 \\ \hline 33.03 \\ 12.01 \\ 45.04 \times \\ 0.39 \\ \hline 44.65 \\ 12.33 \\ \hline 56.98 \times \\ 2.64 \\ \hline 54.34 \\ 12.11 \\ 66.45 \times \\ 9.0 \\ \hline 65.55 \\ 3.13 \\ \hline 78.27 \times \\ C-7.14 \end{array}$$

Lillian St.

6+64 $\frac{27}{27}$ M.H. #32
6+5 + 12.90 Rt.
T=4.56

$$\begin{array}{r} 68.00 \\ 10.27 \\ 3.13 \\ \hline C-7.14 \end{array}$$

6+50

$$\begin{array}{r} 66.82 \\ 11.45 \\ 4.87 \\ \hline C-6.58 \end{array}$$

6+00

$$\begin{array}{r} 62.72 \\ 15.55 \\ 8.54 \\ \hline C-7.01 \end{array}$$

78.27

Lillian St. - Viola - North
States. 4^E Rt.

(Street 1344-D)

M.H.#19 - 1st St. - 23 - 16 - 76
11.97
7.25

INDEXED

W.K.

OCT 6 1949

1+30 = Plug.

73.40
16.68
7.97
C-8.71

1+00

90.08 X
72.20
17.88
9.16
C-8.72

0+50

4%

70.20
98.07
0.55
C-7.52

0+00 (00179)
M.H.32 (North)
E Viola
645+12⁹⁰ Rt.

68.20
10.07
3.13
C-6.94

78.27 X

Lillian St.

Viola - South (1344-D)

25

Sheet

Plug.
2+35

100.72 X
85.00
15.72
7.11
C-8.61

2+00

11.39%

94.47 X
81.04

78.27

13.43
5.52

55

77.72

12.36

1+50

X 94.47
75.39
19.08
11.79

C-7.91

90.08 X

1.16

88.92

11.80

100.72 X

1+20 M.H.#95

C-7.29 90.09 X 90.08 X
71.80 72.00
18.28 18.08
10.15 10.15

C-8.13
To, No.

C 7.93 to 50.

1+00

71.20
18.88
11.62
C-7.26

85.00

8.61

93.61

86

94.47

X

for

Restake

1+50 X

2+00

0+50

3%

69.70
8.57
2.83
C-5.74

0+00 = M.H.32
E Viola
Going south
645+12⁹⁰ Lt.

68.20
10.07
3.13
C-6.94

X 78.27

Gertrude St.
Viola North

(sheet
1349-D)

INDEXED

OCT WK
6 1949

(Tan θ = .70)
M.H.# 33
3+50
 Δ 17 $^{\circ}$ 48' RT
4.55 + 9.10 RT

44.00
11.91
1.81
C-10.10

3+00 M.H. 33
 Δ 17 $^{\circ}$ 48' RT

40.90
15.01
3.64
C-11.37

2+50

55.91 X
37.80
18.11
7.60
C-10.51

2+00 T.P.

34.70
9.15
0.37 T.P.
C-8.76

1+50

6.20%

31.60
12.25
4.02
C-8.23

1+00

28.50
15.35
7.19
C-8.16

0+50

25.40
18.45
10.37
C-8.08

0+00 = M.H. 29
 \pm Viola

22.30
21.55
12.89
C-8.66

43.85

Gertrude st. (Viola North)

26

7+13⁹³ Plug. 52.73
12.03
4.35
C-7.78

7+00

52.48
12.28
5.02
C-7.26

6+50

11.80%

51.58
13.18
5.82
C-7.36

6+00

50.68
14.08
5.64
C-8.44

Δ 97 $^{\circ}$ 02' 30"
Tied 6 $^{\circ}$ 2' 13 $^{\circ}$ RT.

5+93⁹³ M.H.# 35
 Δ 7 $^{\circ}$ 08' 30" RT.

50.57
14.19
5.62
C-8.57

5+50

11.80%

49.78
14.98
6.27
C-8.71

5+00

48.88
15.88
7.47
C-8.41

(Tan θ = 0.92)
4+78 = M.H.# 34
23 $^{\circ}$ 00' 30" RT.
459 + 918 RT.

48.48
16.28
8.05
C-8.23

4+50

64.76 X
47.50
17.26
8.37
C-8.89

4+00

3.50%

55.91 X
45.75 T.P.
10.16
0.69
C-9.47

From P. 23
X
33.36
2.00
30.96
EL. STA. 29
M.H.
29

30.96
12.89
43.85 X
0.39
43.46
12.45
55.91 X
0.69
55.22
9.54
64.76 X
9.48
60.28
24.48
64.76

Mon.
N.E. cor
Lillian's
Gertrude

Lillian St.
Gertrude - South
(Sheet 1349-D)

Plug 1430 R. 25 Left - El. stake = $\frac{82.11}{3.06}$
 $\frac{3.05}{0.101}$ ✓

2+60 M.H. #9A

$\frac{74.10}{11.07}$
 $\frac{4.10}{C-6.97}$

$\frac{64.76}{0.50}$

2+30

INDEXED

$\frac{85.17}{71.40}$
 $\frac{13.77}{6.21}$
C-7.56

$\frac{64.26}{13.19}$
 $\frac{77.45}{0.95}$

2+00

OCT

WK
6 1949

$\frac{77.45x}{68.70}$

$\frac{76.50}{8.67}$
 $\frac{85.17}{8.75}$

$\frac{0.95}{C-7.80}$ T.P.

1+50

$\frac{64.20}{13.25}$
 $\frac{5.48}{C-7.77}$

1+00

9/9

$\frac{79.15}{59.70}$
 $\frac{17.75}{10.12}$
C-7.63

0+50

$\frac{64.76x}{55.20}$
 $\frac{9.56}{2.01}$
C-7.55

0+00 = M.H. #35

£ Gertrude

$\frac{50.70}{14.06}$
 $\frac{5.62}{C-8.44}$

64.76 From P. 26

Dorcias - Morena Nly
Sheet 1347-D

Dorcias St.

28

INDEXED

B.M.#1 - P.24

2+00 3/96

OCT N.K. 12.65
6 1949 13.74
5.30
C-8.44

5+00 28.72
10.22
4.09
C-6.13

16.19
1020
26.89 X
0.15
26.14
11.05
37.19 X
11.05
26.14
12.80
38.94 X

4⁵⁰+9⁰⁰ RT.

1+85.32 M.H.#36
Savannah place

↓ 11.98 12.20 ↑
14.41 14.19
5.60 5.60
C-8.81 C-8.59

4+50 7.74/96

24.85
14.09
7.44
C-6.65

1+50

11.45
14.94
6.50
C-8.44

4+00

38.94 X
20.98
17.96
10.81
C-7.15

1+00 1.59/96

10.70
15.69
7.11
C-8.58

4⁵⁰+9⁰⁰ RT.
3+50⁴⁰ M.H.#41
Savannah St.

26.39 X
17.15
9.24
0.68
C-8.56

22.07 X (P65)

Nail
0+50

9.95
2.12
8.11 V 9.95
check 8.32
C-8.12

3+00

15.65
10.74
2.92
C-7.82

See Page
78

0+00 = M.H.#20
Morena + Dorcias
6.19 + 12.38

9.20 22.01 X
17.19 9.10
7.10 1287
C-8.09

2+50

14.15
12.24
4.30
C-7.94

X 26.39

26.39

Dorcias

Dorcias

29

7+50

50.80
12.52
5.86
C-6.66

10+00

81.00
7.71
1.28
C-6.43

38.94
15
38.77
12.73
51.52
0.24
51.28
12.04
63.32*

7+00
10%

63.32*
45.80
17.52
11.01
C-6.51

9+50
11.5%

88.71
75.25
13.46
6.65
C-6.81

63.28*
13.03
76.31
0.03
76.28
12.43
88.71*
0.17
88.58

6+50

51.52*
40.80
10.72
3.85
C-6.87

9+00

69.50
6.81
0.03
C-6.78 T.P.

T.P.
To page 30

45+90⁰⁰ Rt.
6+25⁷⁶ = M.H.# 49
Bianca Ave

38.47
13.05
6.04
C-7.01

45+90⁰⁰ Rt.
8+69⁶⁰ M.H.# 50
Hilda Ave.

62.85
13.46
3.84
C-9.62

66.00
10.31
3.84
C-6.47

D.M.H.

6+00

7.7%

51.52*
36.48
15.04
8.31
C-6.73

8+50

76.31*
60.80
15.51
6.41
C-9.10

5+50

32.61 T.P.
6.33
0.15
C-6.18

8+00

55.80
7.52
0.04
C-7.48

38.94*

63.32

Dorcias

Dorcias

30

T.P. FROM P. 29

12+50

11.7%

109.91
8.70
2.04
C-6.66

15+50

145.01
10.51
3.51
C-7.00

88.58
13.11
101.69x
0.39
101.30
7.68
108.98x
3.24

12+00

118.61
104.06
14.55
7.92
C-6.63

15+00

155.52x
139.16
16.36
10.16
C-6.20

(105.80)
1/11160
1791
76
105.74
105.80
-0.06

151+902 Rt.
11+60²⁵ M.H.#7A
Everview

99.42
9.56
3.34
C-6.22

14+50

133.31
9.90
9.47
C-5.43

105.80
105.80
12.91
118.61
0.35
118.26
12.28
130.54
0.34
130.20
13.01

11+50

108.98x
98.25
10.73
4.38
C-6.35

14+00

143.21x
127.46
15.75
10.42
C-5.33

143.21x
0.36
142.85
13.67
155.52

11+00

11.5%

72.50
9.19
2.96
C-6.23

13+50

121.61
08.93
3.03
C-5.90

10+50

101.69x
86.75
14.94
8.76
C-6.18

13+00

130.54x
115.76
14.78
8.40
C-6.38

Dorcas + Onstad.

From P. 30

$$15 + 69^{36} \cdot \frac{1791}{77} = 154.25 = 154.28 = +0.03$$

INDEXED

WIK

OCT 6 1949

N.W.B.P. (in porch) onstad +
Everview.

16 + 89³⁶ plug. set at 16 + 99³⁶
cut should be 60 + 6.84

$$\begin{array}{r} 155.52 \times \\ 1.24 \\ \hline 155.30 \\ 12.92 \\ \hline 168.22 \\ 0.98 \\ \hline 167.24 \\ 11.51 \\ \hline 178.75 \\ 1.07 \\ \hline 177.68 \quad (177.64) \end{array}$$

$$\begin{array}{r} 178.75 \times \\ 160.49 \\ \hline 18.26 \\ 10.32 \\ \hline C-7.94 \end{array}$$

16 + 50 set at 16 + 60
cut should be 60 C-7.11
→ C-8.37

$$\begin{array}{r} 156.17 \\ 12.95 \\ \hline 3.68 \\ \hline C-8.37 \end{array}$$

16 + 00 set at 16 + 10
cut should be C-6.71

$$\begin{array}{r} 168.24 \times \\ 150.67 \\ \hline 17.57 \\ 9.71 \\ \hline C-7.81 \end{array}$$

10' chaining bull
Here

Δ 68°-27' Rt.
543 + 10 26 Rt.
15 + 69³⁶ M.H.# 82
onstad

$$\begin{array}{r} 155.52 \times \\ 147.29 \\ \hline 8.23 \\ 1.37 \\ \hline C-6.86 \end{array}$$

Gertrude-

Dorcas - North.

31

5/4/49

See G-146

58

2 + 50

$$\begin{array}{r} 27.00 \\ 10.19 \\ \hline 3.28 \\ C-6.91 \end{array}$$

2 + 00

$$\begin{array}{r} 25.50 \\ 11.69 \\ 4.87 \\ \hline C-6.82 \end{array}$$

456 + 912 Rt.
1 + 49⁹⁰ M.H.# 48
Δ 180°-16' Lt.

$$\begin{array}{r} 24.00 \\ 13.19 \\ 6.14 \\ \hline C-7.05 \end{array}$$

1 + 00

$$\begin{array}{r} 21.80 \\ 15.39 \\ 8.35 \\ \hline C-7.04 \end{array}$$

0 + 50

$$\begin{array}{r} 19.60 \\ 17.59 \\ 9.91 \\ \hline C-7.68 \end{array}$$

Spike 4.66 Rt.
0 + 00 = M.H. 41
Savannah St.
+ Dorcas. + Gertrude
Δ 29°-52' Lt.

$$\begin{array}{r} 17.40 \\ 7.79 \\ 11.48 \\ \hline C-8.31 \end{array}$$

37.19 From P. 28

Gertrude
Doreas Nly.

32

$$\begin{array}{r} 37.19 \\ \underline{0.40} \\ 36.79 \\ \underline{6.49} \\ 43.28 \text{ X} \end{array}$$

4+49²⁰ plug

$$\begin{array}{r} 33.00 \\ \underline{10.28} \\ 1.44 \\ \text{C-} 8.84 \end{array}$$

4+00³⁰

$$\begin{array}{r} 31.50 \\ \underline{11.78} \\ 3.77 \\ \text{C-} 8.01 \end{array}$$

3+49²⁰ M.H.#100

$$\begin{array}{r} 43.28 \text{ X} \\ \underline{30.00} \\ 13.28 \\ \underline{5.81} \\ \text{C-} 7.47 \end{array}$$

3+00

3

390

$$\begin{array}{r} 37.19 \text{ X} \\ \underline{28.50} \\ 8.69 \\ \underline{1.43} \\ \text{C-} 7.26 \end{array}$$

37.19

Outfall From Pacific Hy
to Weeks + Knoxville
4-11-49 (Sheet B-3428 + D-1341)

See page 75

stakes set 10' RT

1024 + 2045 At. on split

2+2A²⁹ - M.H.#1
Site = 2.16

INDEXED

W.K.

OCT 6 1949

2+00

-4.04

7.354

13.54

1+75

-4.17

9.46

13.47

C-4.09

8.22

C-5.25

1+50

-4.19

1+25

-4.27

13.69

13.62

9.22

7.92

C-4.47

C-5.70

1+00

-4.34

0.39

13.84

0+75

-4.42

8.73

13.77

C-5.11

8.39

C-5.38

0+50

-4.49

0+25

-4.57 out.

13.99

8.60

C-5.39

Ely Cross in M.H. Rim
0+00 = EXIST M.H.
#16. (D-1341)

9.504

-4.64

14.14

7.80

C-6.34

9.35 - check

-4.64

13.99

7.64

C-6.35 ✓

2+50

-3.80

0.2690

8.69

4.80

C-4.39

2+50

9.50 +

-3.93

13.43

8.62

C-4.81

B.P. Tecolote Creek bridge

for stations + 155

7.85

1.65

9.50 +

8.62

0.88

4.01

4.89 +

3.60

1.29 B.M.#1

spike

B.M. in power pole

s.w. weeks + Knoxville EL. =

For 7.85

+ 1.50

+ 75 9.35

3.45

TIP 0.90

4.11

5.01 +

3.71

1.30

11.29

1.01

5.01 +

3+25 - 3.72

8.73

4.53

C-4.20

5.01

2+75 - 3.87

8.88

4.85

C-4.03

9.50 +

TIP

11.29

5.01

Everview
 Dorcas to Plainview Rd.
 (1350-D)
 (1351-D)

See C246
 60

INDEXED

OCT 6 1949

453+900 ft
 1+70 M.H.#75
 1800

148.16

132.00
 16.16
 10.84
 C-5.32

4+00

146.83

13.39
 7.87
 C-5.52

12+00 (P.30)

104.06
 C-6.63
 1196.9 stake
 12.78

1+50

127.88
 8.01
 1.47
 C-6.54

3+50

141.48
 18.74
 11.83
 C-6.91

123.42
 0.21

123.21
 12.68
 135.89 x
 0.29

1+00

20.60 %

135.89 x

117.58
 18.31
 11.39
 C-6.92

Tang = 1.50
 Sec. = 4.74 TIP
 3+35.72 M.H.#76
 Δ 36° 52' 30" Lt.

160.22

139.95
 8.21
 0.81
 C-7.40

135.60
 12.56
 148.16
 0.81

T.P.

0+70

111.40
 12.02
 5.58
 C-6.44

3+00

138.24
 9.92
 2.20
 C-7.72

147.35
 12.87
 160.22
 5.62

0+40 = Brk.

105.22
 18.20
 11.40
 C-6.80

2+50

4.8 %

135.84
 12.72
 4.21
 C-8.11

M.H.#74 (Dorcas)
 P.30 = 0+00

99.42
 24.00
 17.94
 C-6.06

2+00

133.44
 14.72
 7.42
 C-7.30

123.42

148.16

4⁵+9⁰⁰ Rt.
6+19.76 M.H.#78
onstad.

170.34
14.37
7.33
C-7.04

8+50

173.69
11.02
1.62
C-9.40

160.22
0.45
159.77
12.66
172.43
1.5
172.18
12.53
184.71
7.04
177.67
N.W. B.P.
onstad (P31)
184.71

6+00

168.23
16.48
8.67
C-7.81

Tang 0.77
Sec. 4.57
8+40.69 M.H.#79
 $\Delta 19^{\circ} 27' \text{ Rt.}$

173.65
11.06
1.70
C-9.36

184.71
T.R.

5+50

10.77

162.88
9.55
1.16
C-8.39

8+00

173.05
11.66
1.93
C-9.73

5+00

157.53
14.90
C-8.8
C-8.02

7+50

1.5090

172.30
12.41
2.97
C-9.44

172.43
T.R.

4+50

152.18
8.04
1.50
C-6.54

7+00

171.55
13.16
4.96
C-8.20

Tang. 1.30
Sec. 4.68
4+43.48 M.H.#77
 $\Delta 32^{\circ} 07' - 15'' \text{ Lt.}$

151.48
8.74
2.50
C-6.24

6+50

170.80
13.91
6.35
C-9.56

160.22

184.71

Everview

Plainview Road
Everview S.Ely.

36

Tang. 1.87
Sec. A. 87
11+46² M.H. #80
Δ 45°-04' RT.

↓ 174.87 179.67 ↑
 16.90 12.10
 5.85 5.85
C-11.05 C-6.25

11+00

174.69
 17.08
 8.96
C-8.12

INDEXED

10+50
OCT 6 1949
W.K.

174.49
 17.28
 11.06
C-5.22

10+00 90
0.4

174.29
 17.48
 12.39
C-5.09
191.77
T.P.

9+50

174.09
 10.62
 4.91
C-5.71

9+00

173.89
 10.82
 2.79
C-8.03

184.71

INDEXED
OCT 6 1949
W.K.

184.71
 5.48
179.23
 12.54
191.77
 0.68
191.09
 9.15
200.24
 2.82

± Herb. Monitor
± Plainview

197.42

197.17
 17.91
 11

End-plug

12+99 14

187.55
 12.69
 5.35
C-7.34

42.5

12+56 64

186.25
 13.99
 7.13
C-6.86

42.5

200.24

Tang. 1.86 T.P.

Sec. A. 87
12+14 13 M.H. #81
Δ 44°-57'-30" RT.

184.95
 6.82
 0.68
C-6.14

11+80 90
7.70

182.31
 9.46
 3.55
C-5.91

191.77

Monitor Rd.
Hilda N.E.W.

(1351-D)

37

Tang 1.09
Sec. 4.60

INDEXED

2+01³² M.H. #68
Δ 27°-18' Lt.

OCT 6 1949
W.K.

117.49
14.46
7.13
C-7.33

4+50

10.390

146.25
10.69
- 3.46
C-7.23

X from P. 41

95.01
22
97.79
12.34
107.13
0.69
106.44
12.84
119.28
0.06

131.95X
T.P.

Tang 1.04
Sec. 4.62
4+22⁶⁸ M.H. #69
Δ 26°-01' Lt.

143.41

13.53
- 6.69
C-6.84

119.22
14.73
131.95
1.8
131.77
12.98
144.75
0.37
144.38
12.56
156.94
0.38
156.56
E.L.T.P.

sec. A.60
1+35=M.H. 67
22°-35' Rt.

107.21
12.07
6.15
C-5.92

4+00

141.10
15.84
9.08
C-6.76

1+00

15.59%

101.78
17.50
11.95
C-5.55

3+50

10.30%

156.94X
T.P.

135.95
8.80
1.55
C-7.25

119.28X
T.P.

0+50

94.03
13.10
7.70
C-5.40

3+00

130.80
13.95
6.38
C-7.57

Sec. 6.42
M.H. #51. Hilda
Monitor = 0+00
Δ 89°-56' Lt

T.P.

X 107.18
T.P.
86.28
8.73
1.96
C-6.77

2+61³² Brk.

126.79
17.96
10.88
C-7.08

X 144.75
T.P.

2+31³²

122.14
9.81
2.34
C-7.77
131.95

95.01

Monitor Rd

6+81 Brk		$\begin{array}{r} 168.00 \\ 14.24 \\ 4.00 \\ \hline C-10.18 \end{array}$		$\begin{array}{r} \text{Elev from pp 37} \\ \text{T.P.} + 156.56 \\ \hline 12.73 \\ 169.29 \text{ T} \\ 0.05 \\ \hline 169.24 \\ 13.00 \\ \hline 182.24 \\ 6.11 \\ \hline 176.13 \\ 13.05 \\ \hline 189.18 \end{array}$
6+61 Brk	167.04		9+50	$\begin{array}{r} 172.26 \\ 16.92 \\ 12.58 \\ \hline C-4.34 \end{array}$
6+41 Brk	$\begin{array}{r} 15.20 \\ 5.36 \\ \hline C-9.84 \end{array}$	$\begin{array}{r} 165.64 \\ 16.60 \\ 7.02 \\ \hline C-9.58 \end{array}$	189.18 T.P.	
6+21 Brk	163.80		9+00	$\begin{array}{r} 171.51 \\ 10.73 \\ 6.12 \\ \hline C-4.61 \end{array}$
Tang 0.99	18.44			
Sec. 4.61	9.33			
6+10 ⁶⁶ M.H.# 70	C-9.11		8+50	$\begin{array}{r} 170.76 \\ 11.48 \\ 6.39 \\ \hline C-3.09 \end{array}$
Δ 2A°-45' Lt.		$\begin{array}{r} 162.77 \\ 19.47 \\ 10.75 \\ \hline C-8.72 \end{array}$	1.50/10	
6+00	161.70		8+00	$\begin{array}{r} 170.01 \\ 12.23 \\ 5.02 \\ \hline C-7.21 \end{array}$
	$\begin{array}{r} 20.54 \\ 12.08 \\ \hline C-8.46 \end{array}$			
	*182.24 T.P.		Tang. -0.76	
5+50		$\begin{array}{r} 156.55 \\ 12.74 \\ 5.28 \\ \hline C-7.46 \end{array}$	Sec. 4.56	
10.3%			7+81.19 M.H.# 71	$\begin{array}{r} 169.73 \\ 12.51 \\ 4.32 \\ \hline C-8.19 \end{array}$
			Δ 19°-08' Lt.	
			7+41.17	$\begin{array}{r} 169.12 \\ 13.12 \\ 3.33 \\ \hline C-9.77 \end{array}$
5+00	151.40		7+01 Brk	$\begin{array}{r} 168.52 \\ 13.72 \\ 3.22 \\ \hline C-10.50 \end{array}$
	$\begin{array}{r} 17.89 \\ -10.76 \\ \hline C-7.13 \end{array}$			
169.29 T.P.				182.24

12+00

183.32
 $\frac{16.75}{8.48}$
 C-8.27

590

200.07
 T.P.

11+50

180.82
 $\frac{836}{0.67}$
 C-7.69

Tan 9.076
 Sec. 4.56

11+33 ⁶⁶ Drop.
⁶⁶ M.H.# 72
 Δ 190-13'-30 Rt.

↓ 175.02 180.00 ↑
 $\frac{14.16}{1.84}$ $\frac{99.18}{1.84}$
 C-12.32 C-7.34

11+00

174.51
 $\frac{14.67}{3.50}$
 C-11.17

10+50

173.76
 $\frac{15.42}{6.98}$
 C-8.44

10+00

173.01
 $\frac{16.17}{10.18}$
 C-5.79

189.18

204.34

Tan 9.450
 Sec. 6.36

14+63 ⁴⁴ M.H.# 73
 Δ 89'-58 Rt.

190.90 191.00
 $\frac{9.17}{2.44}$ $\frac{9.07}{2.44}$
 C-6.73 C-6.63

14+50

190.70
 $\frac{9.37}{2.57}$
 C-6.80

14+00

1.590

189.95
 $\frac{10.12}{3.85}$
 C-6.27

189.18 X
 9.67
 188.51
 11.56
 200.07
 2.44
 197.63
 6.71
204.34

13+50

189.20
 $\frac{10.87}{3.90}$
 C-6.97

13+03 ⁶⁶ Brk

188.50
 $\frac{11.57}{4.15}$
 C-7.42

12+50

185.82
 $\frac{14.25}{6.00}$
 C-8.25

200.07

Plainview
Monitor Rd S. Ely,

40

204.34
6.99
197.35

Hub. Monitor
Plainview 1791 →
197.37
6.99
204.36
6.95
197.41 = L & T. & Monitor Rd
N Ely ch.
Plainview

15498⁴⁴ Plug

193.70
10.64
4.30
C-6.34

15450

270
270

192.73
11.61
5.27
C-6.34

15400

191.73
12.61
6.38
C-6.23

20434

Hilda

(sheet 1352-D)

41

1+50 Brk

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$$\begin{array}{r} 72.92 \\ 10.00 \\ 4.54 \\ \hline C-5.46 \end{array}$$

1+30 Brk

$$\begin{array}{r} 70.81 \\ 12.11 \\ 6.70 \\ \hline C-5.41 \end{array}$$

1+10 Brk

$$\begin{array}{r} 69.10 \\ 13.82 \\ 8.44 \\ \hline C-5.38 \end{array}$$

0+70 Brk

$$\begin{array}{r} 67.80 \\ 15.12 \\ 9.75 \\ \hline C-5.37 \end{array}$$

0+45

$$\begin{array}{r} 65.32 \\ 17.60 \\ 10.49 \\ \hline C-7.11 \end{array}$$

on Diagonal
0+00 = D.M.H. #50
Hilda + Dorcas (P29)

$$\begin{array}{r} 62.85 \\ 20.07 \\ 10.96 \\ \hline C-9.11 \end{array}$$

82.92

3+29 71

$$\begin{array}{r} 94.04 \\ 10.98 \\ 3.95 \\ \hline C 7.03 \end{array}$$

3+09.71

$$\begin{array}{r} 92.28 \\ 12.74 \\ 5.82 \\ \hline C-6.92 \end{array}$$

2+79.71

$$\begin{array}{r} 89.28 \\ 15.74 \\ 8.92 \\ \hline C-6.82 \end{array}$$

Also 6.42 Nail
Tang. - 0.24

Sec. 4.50
2+49.71 M.H. #51
Monitor Rd.
Δ 6" - 04' RT.

3+29

2+09.95

$$\begin{array}{r} 80.86 \\ 14.15 \\ 8.28 \\ \hline C-5.87 \end{array}$$

3+29

1+70 Brk

$$\begin{array}{r} 75.44 \\ 7.48 \\ 2.00 \\ \hline C-5.88 \end{array}$$

82.92

M.H. #50-P29

E.L. invert =

$$\begin{array}{r} 66.00 \\ \text{Cut } 6.47 \\ \hline \text{E.L. Stake } 72.47 \\ 10.25 \\ \hline 82.92 \times \\ 0.20 \\ \hline 82.72 \\ 12.27 \\ \hline 95.01 \times \\ \text{to page 37} \end{array}$$

X 105.02 X

$$\begin{array}{r} 86.28 \\ 8.73 \\ 2.60 \\ \hline C-6.13 \end{array}$$

$$\begin{array}{r} 86.28 \\ C 6.13 \\ \hline 92.41 \text{ E.L. of Stake} \\ 12.61 \\ \hline 105.02 \times \end{array}$$
95.01 X
T.P.

5+00

$$\begin{array}{r} 96.88 \\ 17.18 \\ 5.87 \\ \hline C-11.31 \end{array}$$

4+50

0.470

$$\begin{array}{r} 96.68 \\ 17.38 \\ 6.13 \\ \hline C-11.25 \end{array}$$

Tang 1.08
Sec. 4.63
A+35th = M.H.#52
Δ 27°05' Rt.

$$\begin{array}{r} 114.00 \\ 96.62 \\ 17.44 \\ 6.46 \\ \hline C-10.98 \end{array}$$

.4520

3+89th

$$\begin{array}{r} 96.44 \\ 17.62 \\ 8.67 \\ \hline C-8.95 \end{array}$$

T.P. 114.06 A/

3+69th

$$\begin{array}{r} 96.12 \\ 8.90 \\ 8.7 \\ \hline C-8.03 \end{array}$$
 T.P.
3+49th

$$\begin{array}{r} 95.32 \\ 9.70 \\ 2.24 \\ \hline C-7.46 \end{array}$$

10502

Tang. 1.81
Sec. 4.827+09th M.H.#54
Δ 43°-46' Lt.
$$\begin{array}{r} 97.72 \\ 16.34 \\ 6.77 \\ \hline C-9.35 \end{array}$$

$$\begin{array}{r} 105.02 \\ 87 \\ \hline 104.15 \\ 9.91 \\ \hline 114.06 \\ 3.43 \\ \hline 110.63 \\ 12.20 \\ \hline 122.83 \end{array}$$
7+00th cb.
$$\begin{array}{r} 97.67 \\ 16.39 \\ 7.32 \\ \hline C-9.07 \end{array}$$

6+50

0.490

$$\begin{array}{r} 97.47 \\ 16.59 \\ 8.59 \\ \hline C-8.00 \end{array}$$

6+00

$$\begin{array}{r} 97.27 \\ 16.77 \\ 8.05 \\ \hline C-8.74 \end{array}$$
Tang 0.145
Sec. 4.52
5+78.67 M.H.#53
Δ 110°-26' Rt.
$$\begin{array}{r} 97.19 \\ 16.87 \\ 7.81 \\ \hline C-9.06 \end{array}$$

5+50

$$\begin{array}{r} 97.08 \\ 16.98 \\ 7.39 \\ \hline C-9.59 \end{array}$$

114.06

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OCT 6 1949Tang. 1.70
Sec. 4.81
9+21⁸ M.H. # 56
Δ 41° 24' Lt.
$$\begin{array}{r} 118.27 \\ 16.99 \\ 6.46 \\ \hline C-10.53 \end{array}$$

9+00

$$\begin{array}{r} 116.17 \\ 19.11 \\ 8.43 \\ \hline C-10.68 \end{array}$$

T.P.

135128A

8+50

$$\begin{array}{r} 111.32 \\ 11.51 \\ 2.01 \\ \hline C-9.50 \end{array}$$
Tang. 1.98
Sec. 4.928+13.8⁸ M.H. # 55
Δ 47° 35' Lt.
$$\begin{array}{r} 107.82 \\ 15.01 \\ 6.50 \\ \hline C-8.51 \end{array}$$

8+00

$$\begin{array}{r} 106.47 \\ 16.36 \\ 7.90 \\ \hline C-8.46 \end{array}$$

7+50

$$\begin{array}{r} 101.62 \\ 21.21 \\ 12.23 \\ \hline C-8.58 \end{array}$$

122.83

T.P.

12+00

$$\begin{array}{r} 141.42 \\ 10.90 \\ 2.78 \\ \hline C-8.12 \end{array}$$

$$\begin{array}{r} 122.83 \times \\ 0.37 \\ \hline 122.46 \\ 12.82 \\ \hline 135.28 \\ 0.21 \\ \hline 135.07 \\ 11.22 \\ \hline 146.29 \\ 6.66 \end{array}$$

11+50

$$\begin{array}{r} 138.79 \\ 13.55 \\ 5.86 \\ \hline C-7.69 \end{array}$$
139.63 BM #
spike in pole
499910' rt. of
15 + 15'

11+00

$$\begin{array}{r} 136.12 \\ 16.20 \\ 8.94 \\ \hline C-7.26 \end{array}$$
139.63 J
12.69
152.32 X
0.28
152.04
12.10
164.14

10+50

$$\begin{array}{r} 152.32 \times \\ 133.47 \\ 18.85 \\ 12.23 \\ \hline C-6.62 \end{array}$$
152.32
XTied 45+90 RT
10+12⁸ M.H. # 57
$$\begin{array}{r} 126.30 \\ 19.99 \\ 8.78 \\ \hline C-11.21 \end{array}$$
131.50 ↑
14.79
8.78
C 6.01

45'

T.P. 146.49

9+67³¹

$$\begin{array}{r} 122.30 \\ 12.98 \\ 1.41 \\ \hline C-11.51 \end{array}$$

45'

8.89

135.48

Elevation Road

1A+50
5.390
122.441

154.67
9.47
2.62
C-6.85

1A+00
122.441

Tang. 1.06
Sec. 4.62

13+60 ⁴⁷ M.H. #60
Δ 26° 30' Lt.
149.93
14.21
7.24
C-6.97

13+50
149.37
14.77
7.49
C-7.28

13+00
5.390

146.72
17.42
9.38
C-8.04

12+50
144.07
20.07
11.72
C-8.35

164.14

Tang. 0.46
Sec. 4.52

16+96 ⁴³ M.H. #62
Δ 11° 37' Lt.
172.22
17.21
8.50
C-8.65

16+50
189.43
T.P.

16+00
176.05x
165.09
11.56
3.90
C-7.86

15+50
7.490
213.52

15+00
157.69
18.96
12.05
C 6.91

Tang. 1.03
Sec. 4.62

14+82 ²¹ M.H. #61
Δ 25° 45' Rt.
156.42 = T.P.
7.72
0.49
C-7.28

164.14

T.P. (Below)

163.70
12.95
176.65
0.11
176.54
12.89
189.43

168.79
20.64
12.12
C-8.52

176.65
T.P.

176.65
T.P.

164.14
44
163.70 = EL. Nail

20+00

$$\begin{array}{r} 185.74 \\ 15.98 \\ 7.97 \\ \hline C-8.01 \end{array}$$

19+50

$$\begin{array}{r} 183.99 \\ 17.73 \\ 9.94 \\ \hline C-7.79 \end{array}$$

19+00

$$\begin{array}{r} 182.24 \\ 19.48 \\ 11.20 \\ \hline C-8.28 \end{array}$$

18+50

$$\begin{array}{r} 180.49 \\ 21.23 \\ 12.45 \\ \hline C-8.78 \end{array}$$

Tang. 0.40
Sec. 4.52
18+40.95 M.H.#63
 $\Delta 10^{\circ}-10' Lt.$

$$\begin{array}{r} 201.72 \\ \hline T.P. \rightarrow 180.17 \\ 9.26 \\ 0.58 \\ \hline C-8.68 \end{array}$$

18+00

$$\begin{array}{r} 177.92 \\ 11.51 \\ 2.08 \\ \hline C-7.43 \end{array}$$

17+50

$$\begin{array}{r} 175.17 \\ 14.26 \\ 4.79 \\ \hline C-9.47 \end{array}$$
189.43

22+50

22+00

Tang. 0.160
Sec. 4.54
21+52⁵² M.H.#65
 $\Delta 15^{\circ}-06' Rt.$
Brown ell st.

21+00

20+50

Tang. 0.21
Sec. 4.50
20+15.30 M.H.#64
50-28' Rt.
onstad st.

$$\begin{array}{r} 195.38 \\ 16.74 \\ 8.24 \\ \hline C-8.50 \end{array}$$
212.12

$$\begin{array}{r} 192.45 \\ 9.27 \\ 0.76 \\ \hline C-8.51 \end{array}$$

$$\begin{array}{r} 187.83 \\ 13.89 \\ 5.78 \\ \hline C-8.11 \end{array}$$

$$\begin{array}{r} 193.88 \\ 18.24 \\ 7.75 \\ \hline C-8.49 \end{array}$$

T.P.#2

$$\begin{array}{r} 190.08 \\ 11.64 \\ 3.29 \\ \hline C-8.35 \end{array}$$

$$\begin{array}{r} 186.27 \\ 15.45 \\ 7.27 \\ \hline C-9.18 \end{array}$$
201.72

$$\begin{array}{r} 189.43 \\ 0.58 \\ \hline 188.85 \\ 12.87 \\ \hline 201.72 \\ 7.6 \\ \hline T.P.#2 = 200.96 \\ 11.16 \\ \hline 212.12 \end{array}$$

$$\begin{array}{r} 195.38 \\ 16.74 \\ 8.24 \\ \hline C-8.50 \end{array}$$

$$\begin{array}{r} 193.88 \\ 18.24 \\ 7.75 \\ \hline C-8.49 \end{array}$$

$$\begin{array}{r} 192.45 \\ 9.27 \\ 0.76 \\ \hline C-8.51 \end{array}$$

$$\begin{array}{r} 190.08 \\ 11.64 \\ 3.29 \\ \hline C-8.35 \end{array}$$

$$\begin{array}{r} 186.27 \\ 15.45 \\ 7.27 \\ \hline C-9.18 \end{array}$$

Plainview Road

25+50

204.61
 $\frac{12.65}{5.07}$
 C-7.58

217.26

25+00 180'
 3%

203.11 = T.P.
 $\frac{9.01}{1.70}$
 C-7.31

24+50

201.61
 $\frac{10.54}{3.25}$
 C-7.26

Tang. 4.53
 Sec. 6A9

24+02 ⁸⁵ M.H.#66
 Δ 90-25'-30" RT.
 Plain View + Elevation
 Rd.

↓ 199.96 200.20 ↑
 $\frac{12.16}{4.79}$ $\frac{11.92}{4.79}$
 C-7.37 C-7.13

23+50

198.38
 $\frac{13.74}{5.70}$
 C-8.04

23+00 3%

196.88
 $\frac{15.24}{6.92}$
 C-8.32

212.12

212.12
 $\frac{1.70}{}$
 210.42
 $\frac{6.84}{}$
 217.26

For check
 15+98.04 P. 10
 Invert 193.70
 $\frac{C-6.34}{}$
 200.04 = stub.
 $\frac{12.08 \text{ Ord. rod to stub.}}{12.06}$
 $\frac{0.02}{}$ - OK

25+50
 On = 204.61
 $\frac{C-9.99}{}$
 EL Nail: 212.19
 $\frac{4.84}{}$
 217.037

26+82 ⁸⁵ Plug

206.30
 $\frac{10.96}{4.49}$
 C-6.47

26+32 ⁸⁵

0.790
 160'

205.95
 $\frac{11.31}{3.59}$
 C-7.72

50'

Tie 45+98 RT.
 25+82 ⁸⁵ M.H.#98

217.03
 205.60
 $\frac{11.43}{3.81}$
 C-7.62 ✓

↓ Moved 3' NE. Cr. = 217.037

205.60
 $\frac{11.66}{4.05}$
 C-7.61

217.26

Brownell St.
Elevation Rd. to Cushman
(1348-D)

stakes
4571.0 ft

2+50 M.H.#97

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T.P.#2
P. 45
 $\frac{200.96}{7.78}$
 $\frac{196.20}{12.54}$
 $\frac{5.22}{c 7.32}$
208.74

2+00

$\frac{195.45}{13.29}$
 $\frac{6.43}{c 6.86}$

750

$\frac{194.70}{14.04}$
 $\frac{7.66}{c 6.38}$

1+00

$\frac{193.95}{14.79}$
 $\frac{8.64}{c 6.15}$

0+50

$\frac{193.20}{15.54}$
 $\frac{8.33}{c 7.21}$

M.H.#65 = 0+00
Elevation Road
(P.45)
C 36 on split

$\frac{192.45}{16.29}$
 $\frac{8.40}{c 7.89}$

208.74

CROWN ST (1345-D)

47

Elevation Road to Monitor

2+60 plug

$\frac{157.80}{14.46}$
 $\frac{6.36}{c 8.10}$

2+20
370

$\frac{156.60}{15.66}$
 $\frac{7.35}{c 8.31}$

X from
P 44

164.14
0.87

$\frac{163.27}{8.97}$
172.26

Tang. 0.27
Sec. 4.51

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1+80 M.H.#96

$\Delta 70 \pm$
60.08 ft.

OCT 6 1949

$\frac{155.40}{16.86}$
 $\frac{8.39}{c 8.47}$

172.26

T.P.

For check

1+35

$\frac{154.05}{10.09}$
 $\frac{1.59}{c 8.55}$

5+50 - P. 38
INVERT 156.55
 $\frac{c 7.46}{164.01}$

Grade Rod 8.25
 $\frac{8.25}{-0.01}$

0+90

370

$\frac{152.70}{11.44}$
 $\frac{3.09}{c 8.35}$

OK

0+45

$\frac{151.35}{12.79}$
 $\frac{5.00}{c 7.79}$

See G-246
62

M.H.#60 Elevation Rd
= 0+00 (P.44)

$\frac{150.00}{14.14}$
 $\frac{7.24}{c 6.90}$

164.14

Ellsworth St.
Elevation road to Monitor
(Sheet - 1345-D)

2+19⁵⁰ Chimney

2+00

128.40

17.89

5.03

C 12.86

Tang. 0.52
Sec. 4.53 #
1+69⁵⁰ M.H. 58
 $\Delta 100-48-30^\circ$ Lt.
13°-10' Lt.

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128.10

18.19

5.44

C 12.75

1+50

127.90

18.39

5.61

C 12.78

1+00

see 6-24C
C1

127.40

18.89

6.10

C 12.79

0+50

126.90

19.39

6.54

C 12.85

Tang. 1.90
Sec. 4.88
0+00 = M.H. #57
Elevation Road
+ Ellsworth
 $\Delta 47-52'$ Lt.

126.40

19.89

8.48

C 11.41

146.29

pl 49
4+76⁶⁶

131.16

15.55

4.88

C 10.67

48

4+50

130.90

15.81

4.96

C 10.85

4+12⁶⁶ Chimney

B.M. #1 - P 43

139.63

6.66

146.29 - X

4.55

141.74

4.97

146.71 X

4+00

130.40

16.31

4.66

C 11.65

3+50

129.90

16.81

4.43

C 12.38

Tang. 0.44
Sec. 4.53
3+26⁶⁶ M.H. #59
 $\Delta 13-47'$ Lt.

129.66

17.05

4.43

C 12.62

3+14⁶⁶ chimney

3+00

129.40

17.31

4.63

C 12.68

T.P. $\pi = 146.71$

2+50

128.90

17.39

4.55

C 12.84

146.29

Savannah Street,
Dorcas to Cushman.
(Sheet 1348-B)

49

B.M. #1-P.24

2+25⁵⁰ M.H.#42
No A
19.00
14.92
6.58
C-8.34

4+50

20.93
16.36
10.03
C-6.33

16.19
8.82
25.01
1.25
24.76
9.16
33.92 X
7.13

2+00

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18.81
15.11
6.66
C-8.45

4+38⁴² M.H.#43
No A

37.29 X
20.60
16.69
10.02
C-6.67

37.29 X
20.70
16.59
10.02
C-6.57

26.79
10.50
37.29 X
7.84
27.45

T.R. & Hub
Savannah &
Buones.

i+50

18.43
15.49
6.79
C-8.70

4+00 (T.P.)

33.92 X
20.31
13.61
7.13
C-6.48

1+00

0.75%

18.06
15.86
7.28
C-8.58

3+50

19.93
13.99
6.90
C-7.09

0+50

17.68
16.24
7.93
C-8.31

3+00

0.75%

19.56
14.36
6.78
C-7.58

0+00 = M.H.#41
Dorcas + Savannah
Tied 6.36 + 12.72

17.31

2+50

19.18
14.74
6.63
C-8.11

33.92 X

33.92

Savannah Street

50

7+38⁴² M.H.# AA
No. A
$$\begin{array}{r} 27.30 \\ 9.99 \\ 2.68 \\ \hline C-7.31 \end{array}$$

7+00

$$\begin{array}{r} 26.43 \\ 10.86 \\ 3.90 \\ \hline C-6.96 \end{array}$$

6+50

$$\begin{array}{r} 25.33 \\ 11.96 \\ 5.95 \\ \hline C-6.01 \end{array}$$

6+00

2.70
70
$$\begin{array}{r} 24.23 \\ 13.06 \\ 7.71 \\ \hline C-5.35 \end{array}$$
8+28⁴² Plyg.
$$\begin{array}{r} 29.28 \\ 8.01 \\ 1.17 \\ \hline C-6.84 \end{array}$$

5+50

$$\begin{array}{r} 23.13 \\ 14.16 \\ 9.21 \\ \hline C-4.95 \end{array}$$
7+83⁴²

$$\begin{array}{r} 28.29 \\ 9.00 \\ 1.58 \\ \hline C-7.4.2 \end{array}$$

5+00

$$\begin{array}{r} 22.03 \\ 15.26 \\ 10.02 \\ \hline C-5.24 \end{array}$$
4.57
2.20%

37.29

Buenos Ave.
Also Bianca Ave.
(1348-D)

2+00
2.60%

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33.22
18.30
7.79
C-10.51

Tang 1.65
Sec. 4.79
1+87.58 = M.H. #46
Δ 40° 22' LT

51.52 X
32.90
18.62
8.83
C-9.79

1+50

(T.P.)

39.68 X
30.50
9.18
0.12
C-9.06

1+00
6.40%

27.30
12.38
4.77
C-7.61

0+50

24.10
15.58
9.19
C-6.39

0+00 = M.H. #43
Savannah St. +
Buenas

20.90
18.78
12.25
C-6.53

39.68

End
5+42.40 M.H. #99

BIANCA ST.

51

39.02
13.77
4.30
C-9.47

T.P. from P. 49

5+00

38.47
14.32
4.25
C-9.87

27.45
12.23
39.68 X
12

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39.56
11.96
51.52 X
2.75
48.77
41.02
52.79

4+50

37.82
14.97
4.75
C-10.22

4+00

0.70%

52.79
37.17
15.62
4.48
C-11.14

3+50

1.30%

T.P. 1/2

51.52 X
← 36.52
15.00
2.75
C-12.25

Tang 2.08
Sec. 4.96
3+02 40 M.H. #47
Δ 49° 33'

35.90
15.62
2.75
C-12.87

2+50

51.52 X
34.52
17.00
4.83
C-12.17

Savannah Place 7/7/49
 Dorcas to Cushman
 (Sheet 13A7-D)

2+26-M.H.#37
 No 4
 T.P. 14.33
 11.16
4.22
 C-6.94

2+00 INDEXED
 W.K.
 OCT 6 1949

14.10
 11.39
 4.59
C-6.80

1+50
 13.65
 11.84
 4.84
C-7.00

1+00 0.9%

13.20
 12.29
 5.03
C-7.26

0+50
 12.75
 12.74
 4.77
C-7.97

0+00 = M.H.#36
 Savannah Place
 Dorcas

12.30

25.49

Savannah Place 52

4+50 16.35
 12.52
 4.80
C-7.72

4+38.82 M.H.#38
 No 4
 16.25
 12.62
 4.53
C-8.07

4+00 15.90
 12.97
 5.34
C-7.63

3+50 15.45
 13.42
 5.76
C-7.66

3+00 0.9%
 15.00
 13.87
 6.68
C-7.19

2+50 14.55
 14.32
 7.16
C-7.16

28.87

BM#1. P.24
 16.19
 9.30
 25.49 X
 4.22
 21.27
 7.60
28.87 X

Savannah Place.

(143.75)
to here

53

7+38 ⁸² M.H.39
No A

18.95
12.80
5.03
C-7.77

7+00

18.60
13.15
5.68
C-7.47

6+50

0.99%

18.15
13.50
6.42
C-7.18

6+00

T 31.95

17.70
14.05
6.97
C-7.08

plug
8+28 ⁸²

19.75
12.00
3.44
C-8.56

228.87
458
2429
7.46
3175
9.33

5+50

TIP

17.25
11.62
4.58
C-7.04

45-

22.42
488
27.50
3.94
21.36
3.02
24.38
8.09
16.29

5+00

16.80
12.07
4.61
C-7.46

7+83 ⁸²

0.99%

19.35
12.40
4.04
C-8.36

45-

28.87

Knoxville

Weeks N.Ely.

INDEXED

M.K.

OCT 6 1949

(1341-D)

54

2+50

B.M.#1 P.33

1.29

5.50

6.79

4.73

2.06

S.W. Mon
Knoxville + Naples

B.M.#2

6.79

3.63

3.16

6.10

9.26

6.54

2.62

B.M.#A
S.L. Knoxville +
W.H. Savannah

0.32

1+00

0+50

0+00 = M.H.#2
Weeks + Knoxville

- 2.86

9.65

4.37

C-5.28

9.80

4.52

C-5.29

- 3.01

9.80

4.52

C-5.29

- 3.16

9.95

4.79

C-5.16

- 3.31

10.10

4.65

C-5.45

- 3.46

10.25

5.07

C-5.118

- 3.61

10.40

6.79

- 2.86

9.65

- 2.93 + 25

9.72

4.04

C-5.68

- 3.08 + 75

9.87

4.66

C-5.21

- 3.16

9.95

- 3.23 + 25

10.02

4.62

C-5.40

- 3.31

10.10

- 3.38 + 75

10.17

4.72

C-5.45

- 3.46

10.25

+ 25 - 3.53

10.32

5.71

C-4.61

- 3.61

10.40

6.79

5+00

4+50

4+00

3+50

3+00

Tang. 0.32
Sec. 8.00

2+62 AL M.H.#6

Δ 40-25' Lt.

- 2.11

11.37

5.87

C-5.50

- 2.26

11.52

5.51

C-5.71

- 2.41

11.67

6.13

C-5.54

- 2.56

9.35

3.59

C-5.76

- 2.71

9.50

4.29

C-5.21

- 2.83

7.62

4.42

C-5.20

+ 25

- 2.03

11.29

5.49

C-5.80

+ 75

- 2.18

11.44

5.65

C-5.79

- 2.26

11.59

5.95

C-5.64

+ 75

- 2.48 = T.P.

9.27

3.63

C-5.64

- 2.56

9.42

4.00

C-5.42

- 2.71

9.57

4.42

C-5.15

6.79

10 + 23 - 0.53
 13.59
 3.74
 C-9.65
 B.M.#3
 (Below)
 8.84
 1.22
 13.06X

7+50

-1.36
 10.62
 4.69
 C-5.93
 +25 - 1.43
 10.69
 5.10
 C-5.59

9+980

-0.61
 13.67
 4.15
 C-9.52
 +73 - 0.68
 13.74
 4.09
 C-9.65

7+00

-1.57
 10.77
 5.02
 C-5.75
 +75 - 1.58
 10.84
 5.12
 C-5.72

9+48

-0.76
 13.82
 4.26
 C-9.56
 +23 - 0.83
 13.89
 4.32
 C-9.57

6+50

-1.66
 10.92
 5.33
 C-5.59
 +25 - 1.73
 10.99
 5.22
 C-5.77

9+08 -0.88
 Tarr = 39
 New Δ = 5' 2"
 8+96 57
 New sta. M.H. 15

-0.71
 13.94
 4.10
 C-9.79
 8+80+ 13.09X
 0-97
 14.03
 4.22
 C-9.81

6+00

-1.81
 11.07
 5.14
 C-5.93
 -1.81

8+88⁵⁹ M.H.#25
 Knoxville + Morena
 12.77X
 -1.02
 13.79
 5.74
 C-8.05

-0.95
 10.21
 0.42
 C-9.79
 = B.M.#3 → 8.84 = EL. Nail
 +75 - 0.98
 10.24
 0.89
 C-9.56
 11.31 R.P.
 2' 45"
 in N.W.
 Quad.

5+72¹¹ M.H.#21
 No A

-1.90
 11.16
 4.95
 C-6.21

8+50

-1.06
 10.32
 3.26
 C-7.06
 +25 - 1.13
 10.39
 3.77
 C-6.62
 8.84
 3.93
 12.77X

5+50

-1.96
 11.22
 5.10
 C-6.12
 -1.96

8+00

-1.21
 10.47
 4.31
 C-6.16
 +75 - 1.28
 10.54
 4.42
 C-6.12

9.26

9.26

Blks. 1+2 Corella tract.
(Nly + Sly Alley) (1345-D)

stakes 7' Mt.

13+00

INDEXED

W.K.

OCT 6 1949

0.28 = T.P. EL. = 5.88 = B.M. #5
 $\begin{array}{r} 12.91 \\ 7.31 \\ \hline 12.99 \\ 5.32 \\ \hline C-7.67 \end{array}$ +75
 B.M. #3 P55
 $\begin{array}{r} 8.84 \\ 4.35 \\ 13.19 \times \\ 7.31 \end{array}$

12+50

+0.13
 $\begin{array}{r} 13.06 \\ 5.30 \\ \hline C-7.76 \end{array}$ +125
 +0.06
 $\begin{array}{r} 13.13 \\ 5.70 \\ \hline C-7.43 \end{array}$ 1215
 5.88 B.M. #4
 6.07
 11.95x

Tang. 4.50
Tied 6.36

12+00⁰⁵ M.H. 84

(000 page 57)
Δ 90° (L.T.)

-0.02
 $\begin{array}{r} 13.21 \\ 5.33 \\ \hline C-7.88 \end{array}$ EL. = 7.96 = B.M. #4
 +75 -0.09
 $\begin{array}{r} 13.28 \\ 5.16 \\ \hline C-8.12 \end{array}$

11+50

-0.16
 $\begin{array}{r} 13.35 \\ 5.16 \\ \hline C-8.19 \end{array}$ -0.16
 +25 -0.24
 $\begin{array}{r} 13.43 \\ 5.01 \\ \hline C-8.42 \end{array}$

11+00

-0.31
 $\begin{array}{r} 13.50 \\ 4.76 \\ \hline C-8.74 \end{array}$ +75 -0.39
 $\begin{array}{r} 13.58 \\ 4.00 \\ \hline C-9.58 \end{array}$

10+50

10+50²⁶ M.H. 83

Δ 84° 43' Lt.

M.H. 83

7' Mt. at 90°

-0.46
 $\begin{array}{r} 13.65 \\ 3.98 \\ \hline C-9.67 \end{array}$ -0.46
 $\begin{array}{r} 13.06 \\ -0.46 \\ \hline 13.52 \end{array}$
 13.19

Alley Blk 1+2 Corella

56

(Nly + Sly Alley) (1345-D)

stakes 7' Mt.

P149
15+80

1.48
 $\begin{array}{r} 10.47 \\ 5.60 \\ \hline C-4.87 \end{array}$ 15+50 - 1.27
 $\begin{array}{r} 10.68 \\ 5.50 \\ \hline C-5.18 \end{array}$

15+20

1.06
 $\begin{array}{r} 10.89 \\ 5.29 \\ \hline C-5.60 \end{array}$

Tang. 4.50
Tied 6.36

1A+89⁹⁹ M.H. # 85

(0+00 page 57 Δ 90°)
Rt.

0.85
 $\begin{array}{r} 11.10 \\ 5.15 \\ \hline C-5.95 \end{array}$ +75 = 0.80
 $\begin{array}{r} 11.15 \\ 5.05 \\ \hline C-6.10 \end{array}$

1A+50

0.73
 $\begin{array}{r} 11.22 \\ 4.69 \\ \hline C-6.53 \end{array}$ +25 = 0.65
 $\begin{array}{r} 11.30 \\ 4.77 \\ \hline C-6.53 \end{array}$

1A+00

0.58
 $\begin{array}{r} 11.37 \\ 4.48 \\ \hline C-6.89 \end{array}$ +75 = 0.50
 $\begin{array}{r} 11.45 \\ 4.40 \\ \hline C-7.05 \end{array}$

13+50

0.43
 $\begin{array}{r} 11.52 \\ 4.40 \\ \hline C-7.12 \end{array}$ +25 = 0.35
 $\begin{array}{r} 11.60 \\ 1.90 \\ \hline C-9.70 \end{array}$
 11.95

Ely & Wly Alley stakes 7' RT
 BIK. 1 Corella track
 (1345-D)

Ely & Wly Alley 57
 BIK. 2 Corella Tract,
 (1345-D)

stakes 7' RT
plug

plug
 3+68⁸ $\frac{1.67}{13.93}$
 $\frac{6.68}{C-7.25}$

3+34⁴ $\frac{1.53}{14.07}$
 $\frac{6.67}{C-7.38}$

M.H. #92
 3+00 $\frac{1.40}{14.20}$
 No A $\frac{6.92}{C-7.28}$

2+50 $\frac{1.20}{14.40}$
 $\frac{7.22}{C-7.18}$

2+00 $\frac{1.10}{14.60}$
 $\frac{8.96}{C-5.64}$

1+50 $\frac{0.80}{14.80}$
 $\frac{6.22}{8.58}$

1+00 $\frac{0.60}{15.00}$
 $\frac{7.23}{C-7.77}$

0+50 $\frac{0.40}{15.20}$
 $\frac{7.63}{C-7.57}$

0+00
 M.H. 84 $\frac{0.20}{15.40}$
 (P. 56) $\frac{7.74}{7.66}$
 Lt.

15.60

3+68⁸ $\frac{2.42}{8.76}$
 $\frac{4.50}{C-4.26}$

3+34⁴ $\frac{2.28}{8.90}$ (P. 56)
 $\frac{5.04}{4.62}$ 11.95
 $\frac{6.51}{C-4.28}$ 4.67

M.H. 93 $\frac{2.15}{9.03}$ 11.18
 3+00 $\frac{4.92}{C-4.11}$ 3.40
 No A 7.78

2+50 $\frac{1.95}{9.23}$ 7.82
 $\frac{4.66}{C-4.57}$ 15.60
 7.74

2+00 $\frac{1.75}{10.20}$ 7.86
 $\frac{5.04}{C-4.76}$ - B.M. #4
 7.86

1+50 $\frac{1.55}{10.40}$ 13.04
 $\frac{5.25}{C-5.15}$ 4.20
 8.84

1+00 $\frac{1.35}{10.60}$ orig B.M.
 $\frac{4.91}{C-5.69}$ P. 56.
 OK.

0+50 $\frac{1.15}{10.80}$
 $\frac{4.83}{C-5.97}$

0+00 = M.H. 85 $\frac{0.95}{11.00}$
 (P. 56 Rt.) $\frac{5.15}{C-5.85}$

Δ from P. 56 = 11.95

Morena (Knoxville - Nly)

(1343-D)

6/19/49

See C-246
 57

B.M.#3 - P.55
 EL. = 884
 507
 13.917

Plug.
 1 + 85

INDEXED

M.K.
OCT 6 1949

0.55
13.36
 4.30
 C-9.06

75 = +0.47
13.44
 4.35
 C-9.09

1 + 50

+0.30
13.61
 4.45
 C-9.16

+25 = +0.13
13.78
 4.50
 C-9.28

1 + 00

-0.05
13.96
 4.59
 C-9.37

+75 = -0.22
14.13
 4.57
 C-9.46

0 + 50

-0.40
14.31
 4.82
 C-9.49

+25 = -0.57
14.48
 4.91
 C-9.57

0 + 00 = M.H. 25
 (P.55)

-0.75
14.66
 5.12
 C-9.54

Morena (Knoxville South).
 (1344-D)

58

2 + 60 M.H. #26 ↓ 0.55
12.55
 3.66
 C-8.89

+0.75 ↑
12.35
 3.66
 C-8.69

B.M.#3
 P.55

8.84
 4.26
 13.107

2 + 50

0.50
12.60
 3.87
 C-8.73

125 = 0.38
12.72
 4.25
 C-8.47

2 + 00

0.25
12.85
 4.47
 C-8.38

1 + 75 = +0.13
12.97
 4.60
 C-8.39

1 + 50

0.00
13.10
 4.62
 C-8.48

+25 = -0.13
13.23
 4.55
 C-8.68

1 + 00

-0.25
13.35
 4.51
 C-8.84

+75 = -0.38
13.48
 4.39
 C-9.09

0 + 50

-0.150
13.60
 4.28
 C-9.32

+25 = -0.63
13.73
 4.21
 C-9.52

0 + 00 = M.H. #25
 (P.55)

-0.75
13.85
 4.31
 7.34

13.10

Morena (1344-D)

Line change see P. 76 1/7/49

59

8+04 ⁸² M.H.#28
Viola St. 13.56

5+50

9.45

8+00

13.50

5+00

7.95

7+50

13.00

See P. 76

see G245
57

4+50

6.45

7+00

12.50

4+00

4.95

6+50

12.00

3+50

3.45

Tang: 1.73
Sec: 4.82
6+28 ⁵⁴ M.H.#27
Δ-42° Rt.

11.80

3+00

1.95

6+00

10.95

Savannah (Knoxville-Sly)
(1343-D)

60

B.M.#2
P.54
2.06

2+50
-0.80
8.98
5.125
C-3.73

+15 -0.90
9.08
5.21
C-3.87

2+00
-1.00
9.18
5.129
C-3.89

+75 -1.10
9.28
5.127
C-4.01

1+50
-1.20
9.38
5.114
C-4.24

+25 -1.30
9.48
5.112
C-4.36

1+00
-1.40
9.58
5.112
C-4.46

+75 -1.50
9.68
4.96
C-4.72

0+50
-1.60
9.78
4.82
C-4.76

+25 -1.70
9.88
4.19
C-5.69

0+00 = M.H.#21
Knoxville St
P.55
-1.80
9.98
3.87
C-6.11

8.18

5+50
17.21
2.85
14.36
6.71
C-7.65

5+00
1.90
15.31
9.17
C-6.14

+75 = 1.42
15.79
10.56
C-5.23

4+50
0.95
16.26
11.46
C-4.80

4+00 M.H.22
No. Δ

-0.20
8.38
3.93
C-4.45

3+50
-0.40
8.58
4.90
C-3.68

3+00
-0.60
8.78
5.28
C-3.50

8.18

17.21
12.23
4.98
3.20
8.18

+25 2.37
14.84
7.84
C-7.00

17.21 x
+25 = +0.147 T.P.
16.74 EL=4.98
12.23
C-4.51

0.00
8.18
3.93
C-4.25

+75
-0.30
8.48
4.64
C-3.84

+25 -0.50
8.68
5.14
C-3.54

+75 -0.70
8.88
5.32
C-3.56

Savannah.

8' stub
M.H.#23
EL: 14.18
8.32
22.50X
2.75
19.75
4.85
7.60
7.62460

8+00

7.60
14.90
5.14
C 9.76

7+50

6.65
15.85
6.30
C 9.55

7+00

1.990

5.70
16.80
7.36
C 9.44

6+50

22.50X
4.75
17.75
8.19
C 9.56

6+39⁵⁵
No Δ
Vega st.

8' x 16' LH
M.H.#23

17.21X
4.55
12.66
3.03
C 9.63

T.R.#2
P.64
15.52
16.9
+25 4.27
12.94
3.96
C 9.48

6+00

3.80
13.41
4.34
C 9.07

17.21
115 = 3.82
13.89
5.53
C 8.36

Morena - South of Savannah 61

10+50

11.59
13.01
5.24
C 7.79

10+00

0.790

24.60X
11.24
13.36
5.12
C 8.24

Tan 9, 1.73
SEC 1.82

9+99.03 9+69.55
M.H.#2A
Morena Δ 42° RT.
9+66.33 Back = L

South
Ahead

9+75.77 to North

24
H 100 ↓ ↑ H 110
24.60X
22.50X
10.76
2.75
C 8.01
11.04
13.56
4.56
C 9.00

should be

1.735
C 9.01

To South

9+50

10.45
12.05
3.39
C 8.66

9+00

9.50
13.00
3.56
C 9.44

8+50

8.55
13.95
4.28
C 9.67

Morena
Savannah - Sly.

(1343-D)

M.H.#
12+23⁰³

12.81
11.79
6.14
C-5.65

12+00

12.64
11.96
5.87
C-6.09

11+50

12.29
12.31
5.73
C-6.58

11+00

11.94
12.66
5.49
C-7.17

Morena
Savannah - Nly.

62

(1343-D)

plug.
2+05

14.18
10.42
3.56
C-6.86

2+00

14.10
10.50
3.58
C-6.92

See G-246
56

1+50

13.35
11.25
3.86
C-7.39

1+00

12.60
12.00
4.07
C-7.93

0+50

11.85
12.75
4.37
C-8.38

= 0+09⁴⁴ Ahead
0+00 M.H.# 24

P. 55.

Line Charge

7/15/49

24.60x
11.10 +.14
11.24
13.36
4.56
C-8.80 To north.

Naples
Knoxville to Dorcas.

INDEXED

W.K.

OCT 6 1949

2+50

-1.73 ^{101 Lt.}
8.90
5.64
C-3.26

+25 = -1.83
9.00
5.77
C-3.23

2+00

-1.93
9.10
5.70
C-3.20

+75 = -2.03
9.20
5.77
C-3.43

1+50

0.40%

-2.13
9.30
5.51
C-3.79

+75 = -2.23
9.40
5.59
C-3.81

1+00

-2.33
9.50
5.102
C-4.48

+75 = -2.43
9.60
4.98
C-4.62

0+50

-2.53
9.70
5.107
C-4.63

+25 = -2.63
9.80
5.01
C-4.79

0+00 = M.H.#16
Knoxville P.54

-2.73
9.90
4.86
C-5.10

7.17

8' Lt
(1342-D)

Naples

63

5+00

2.97
14.23
5.88
C-8.35

B.M.#2
P.54
2.06
5.11
7.17x
0.89
6.28
10.92
17.20

4+50

1.77
15.43
7.62
C-7.81

+25 1.17
16.03
8.59
C-7.44

4+00

2.40%

+ 17.20x
0.57
16.63
9.63
C-7.100

+75 = 7.17x T.P.
-0.03
7.20
0.89
C-6.31

3+50

-0.63
7.80
2.17
C-5.63

3+20 M.H.#17

6.27
1.27
8.72
2.97
C-4.75

-1.45 ↓ ↑ -1.35
8.62
3.84
C-4.78

8.52
3.84
C-4.68

3+00

-1.53
8.70
4.50
C-4.20

+75 = -1.63
8.80
4.82
C-3.98

7.17

use this
-7.77
-7.44
-7.10
-6.31
-5.63
-4.75
-4.20
-3.98

Maples

T.P. From A.77

15.57
7.71
 23.28
5.34
 17.94
4.13
 22.07

7+50

6.77
16.51
6.41
 C-10.10

10+00

0.40%

22.07
7.77
14.30
4.23
 C-10.07

7+00

0.40%

6.57
16.71
7.05
 C-9.66

9+69⁹⁹ T.P.
 M.H.#19
 No. Δ

7.65
15.63
5.34
 C-10.29

6+50

23.28
6.37
16.91
7.50
 C-9.41

9+50

7.57
15.71
5.22
 C-10.49

6+39⁹⁹ M.H.#18 T.P.
 Vega - No Δ

6.33
10.87
1.68
 C-7.19

#2
 T.P. E1 = 15.52
 +25-5.97
11.23
2.14
 C-9.09

9+00

7.37
15.91
4.98
 C-10.73

6+00

2.40% use this

Restate 7/10/49

9.77

5.37
17.83
2.79
 C-8.84

+75-4.77
12.43
3.79
 C-8.64

8+50

0.40%

7.17
16.11
5.05
 C-11.06

5+50

17.10
1.69
 15.52 T.P.

4.17
13.03
4.50
 C-8.53

+25-3.57
13.63
5.20
 C-8.43

8+00

6.97
16.31
5.81
 C-10.50
23.18

17.20

Naples St.

Weeks.
Knoxville to Buena
stakes 8' Lt. of # 1346-D.

65

12+95⁸⁹ M.H.#20
Morena

8.95
13.12
4.97
C-8.13

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OCT 6 1949

12+50

8.77
13.30
4.88
C-8.42

21.85
8.87
12.98
4.64
8.34

12+00

8.57
13.50
5.06
C-8.44

11+50

0.40 90

8.37
13.70
4.93
C-8.77

11+00

8.17
13.90
4.28
C-7.42

10+50

7.97
14.10
4.19
C-9.91

2207

INDEXED

W.K. -2.71

OCT 6 1949

2+00

7.97
4.74
C-3.03

+75
-2.81
8.07
4.77
C-3.28

1+50

0.40 90

-2.91
8.17
4.76
C-3.41

+25
-3.01
8.27
5.50
C-2.77

Tang 2.62

Sec. 8.45

1+09 M.H.#3

-3.07
8.33
5.30
C-3.03

Δ 36° 17' Rt.

B.M.#1 P.33

0+72.8

-3.22
8.48
4.92
C-3.56

1.29
3.77
5.26 X
5.15
0.11
10.51
10.62 X
4.11
6.51
11.94
18.45
8.12
10.33 =

0+36.4

-3.37
8.63
4.56
C-4.07

spike in P pole
2102
Vega + Weeks
= B.M.#2

364-3 times

0+00 M.H.#2.
Knoxville + weeks.

5.26
-3.51
8.77
4.33
C-4.44

5+00

0.40%

-1.51
12.13
10.94
C-1.19

+75 -1.61
12.23
10.56
C-1.67

4+50

-1.71
12.33
10.98
C-1.35

-1.71
10.62 X
+25 -1.81
12.43
10.78
C-1.65

EL=0.11=T.P

3+96⁸⁶ M.H.# 4

No A

-1.92
7.18
5.15
C-2.03

+75 -2.01
7.27
5.08
C-2.19

3+50

0.40%

-2.11
7.37
5.05
C-2.32

-2.11
+25 -2.21
7.47
4.95
C-2.52

3+00

-2.31
7.57
4.97
C-2.60

+75 -2.41
7.67
5.01
C-2.66

2+50

+25

-2.51
7.77
4.78
C-2.79

-2.51
+25 2.61
7.87
5.08
C-2.79

5.26 X

7+50

0.70%

2.45
14.03
3.62
C-10.41

7+00

16'R.P.M.H.
17.32 - 14.56
3.63 3.67
C-13.69 C-10.93
North South

16.48 X
2.10
14.38
4.59
C-9.79

16.54 X
-0.78 +1.98
17.32 14.56
5.20 5.20
C-12.12 C-9.36
8'R.P.

6+81⁸⁶ DMH# 5

Vaga.st
No A

-0.78 +1.98
19.23 16.47
8.02 6.82
C-14.21 C-10.45
+75 -0.81

EL.T.P=6.51

6+50

Pier,
6+01.86

-0.91
11.53
4.11
C-7.42

18.45 X
19.26 Restake
8.19 B.M.#2-95
C-11.07 10.33
+25 -1.01 6.21
11.63 16.54
8.11
C-3.52

6+00

5+85.86
5+69.86
5+53.86
PIERS

-1.11
11.73
10.43
C-1.30

+75 -1.21
11.83
10.99
C-0.84

5+50

-1.31
11.73
11.09
C-0.84

-1.31
+25 -1.41
12.03
11.05
C-0.98

Weeks

B.M.#2-P65

$$\begin{array}{r} 10.33 \\ 6.15 \\ \hline 16.48X \\ 5.16 \\ 11.32 \\ 10.93 \\ \hline 22.25X \end{array}$$

10+50

0.70%

4.57

$$\begin{array}{r} 11.91 \\ 8.31 \\ \hline \end{array}$$

C-3.60

³²
13+28 M.H.#7
NO A Dorcas

6.50 ↓

↑ 6.70

15.75

15.55

7.10

7.10

C-8.65

C-8.43

10+01 ⁸⁶ M.H.#6

NO A

4.22

$$\begin{array}{r} 12.26 \\ 3.43 \\ \hline \end{array}$$

C-6.83

13+00

6.30

15.95

8.05

C-7.90

9+50

3.85

$$\begin{array}{r} 12.63 \\ 4.70 \\ \hline \end{array}$$

C-7.93

12+50

5.95

16.30

9.30

C7.00

9+00

0.70%

3.50

$$\begin{array}{r} 12.78 \\ 4.27 \\ \hline \end{array}$$

C-8.71

12+00

0.70%

22.25X

5.62

16.63

10.33

C 6.30

8+50

3.15

$$\begin{array}{r} 13.33 \\ 3.05 \\ \hline \end{array}$$

C-10.28

11+50

5.27

11.21

5.16

C-6.05

8+00

16.48X

2.80

13.68

3.08

C 10.60

11+00

4.92

11.56

7.64

C-3.92

Weeks

15+68³² M.H.#8
NO A
$$\begin{array}{r} 15.10 \\ 13.46 \\ \underline{5.88} \\ C-7.58 \end{array}$$

15+50

$$\begin{array}{r} 14.16 \\ 14.10 \\ \underline{5.85} \\ C-8.25 \end{array}$$

15+00

$$\begin{array}{r} 28.56X \\ 12.71 \\ \underline{15.85} \\ 6.02 \\ \underline{C-9.83} \end{array}$$

14+50

3.50%

$$\begin{array}{r} 22.25X \\ 10.96 \\ 11.29 \\ \underline{1.33} \\ C-9.96 \end{array}$$

14+00

$$\begin{array}{r} 9.21 \\ 13.04 \\ \underline{4.41} \\ C-8.63 \end{array}$$

13+50

$$\begin{array}{r} 22.25 \\ 7.16 \\ 11.79 \\ \underline{6.90} \\ C-7.89 \end{array}$$

Weeks

plyg
17+08³²

$$\begin{array}{r} 19.02 \\ 9.54 \\ \underline{4.22} \\ C-5.32 \end{array}$$

17+00

$$\begin{array}{r} 18.76 \\ 9.80 \\ \underline{4.60} \\ C-5.10 \end{array}$$

16+50

2.80%

$$\begin{array}{r} 17.36 \\ 11.20 \\ \underline{5.70} \\ C-5.50 \end{array}$$

16+00

$$\begin{array}{r} 15.96 \\ 12.60 \\ \underline{5.97} \\ C-6.63 \end{array}$$

X 22.25

133

2092

7.64

28.56X

1.70

26.86

Nail & Weeks

+ Buonas

= B.M.#3

Maples Place

Also Dorcas -ushman & weeks 1342-D
1346-D

24.09x
chock
8.70
15.79
7.59
8.20
C-8.19

8.35
13.22
5.31
C-7.91

S.W. Morr.
Morera + Dorcas
16.19
5.38
21.57x

+ 12.72 }
6.36 on split
1+64⁹⁰ M.H.9

1+50

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OCT 6 1949

8.20
13.37
5.06
C8.31

1+00
1⁹⁰

7.70
13.87
4.53
C-9.34

0+50.

7.20
14.37
4.66
C-7.77

0+00=M.H.7.
Dorcas + weeks

6.70
14.87

© = chimney

69

4+84²

4+50

0.490

©

10.81
18.77
3.36

4+34⁹

4+00

3+94²

29.58x
10.61
18.97
4.70
C-14.27

©

C-15.41

Morr.

16.19
8.30
24.49x
0.53
23.96
5.62
29.58x

3+84⁹⁰ M.H. #10

10.81 T.P.
13.94
0.53

C-13.41²

3+50

10.20
14.29
3.10
C-11.19

© 3+34²

1⁹⁰

©

3+00

9.70
14.79
5.30
C-9.49

2+50

9.20
15.29
6.86
C-8.43

Maples Place

7+4+2

Ⓢ

7+00

6+94?

0.4%

11.81
17.08
5.63
C-11.45

Ⓢ

6+50

6+44?

11.61
17.28
5.50
C-11.78

Ⓢ

6+1A⁶⁵ M.H.#11
No A Buena

11.47
17.42
5.14
C-12.28

Ⓢ

6+00

0.4%

28.89x
11.41
17.48
4.96
C-12.52

For check
29.58x
11.41
18.17
5.63
C-12.54 ✓

8+50

0.4%

25.99x
12.41
13.58
4.54
C-9.04

8+00

T.P.

28.57x
12.21
16.68
5.48

C-11.20

5+34?

Ⓢ

5+00

11.01
18.57
4.12
C-14.45

7+94?

Ⓢ

7+50

12.01
16.88
5.02
C-11.86

B.M.#3-P.68

12.81
13.18
5.06
C-8.12

26.86
2.03
28.89x
5.48
23.41
2.58
25.97x

12.47
13.52
4.74
C-8.78

Naples place + Cushman
1346-D

INDEXED

W.K.
OCT 6 1949

12+00

0.57%

14.00
11.14
4.00
C-7.14

11+50

13.75
11.39
3.60
C-7.79

Tied c²⁵ 12¹² on split
11+09 ⁷² M.H.# 13
Cushman St.
Δ 90° RT.

For check
28997
~~18.25~~ 13.45 ↓ ↑ 25.14
13.55
12.54 11.69 11.59
5.47 4.56 4.56
~~7.7~~ C-7.13 C-7.03

11+00

13.41
12.58
5.48
C-7.10

10+50

0.4%

13.21
12.78
4.90
C-7.88

10+00

25.99
13.01
12.98
5.38
C-7.60

Cushman + Weeks

71

B.M. = Mon.
Naples + Dorcas.

14+50

25.14
16.76
8.38
3.80
C-4.58

14+00

16.11
9.03
4.48
C-4.53

13+50

15.46
9.68
1.46
C-5.22

13+00

14.81
10.33
4.73
C-5.60

12+7A ⁶⁴ M.H.# 14
Δ weeks

14.37 ↓ ↑ 14.48
10.77 10.66
4.95 4.95
C-5.82 C-5.71

12+50

14.25
10.89
4.96
C-5.93

16.19
10.81
2700
3.74
23.26
2.90
26.16
5.58
20.58 =
6²⁵ R.P.M.H.
#5
Morana +
Cushman.
= B.M.#5
20.58
4.56
25.14
3.81
21.33
10.47
31.80
4.89
26.91
- B.M.#3
R.68
26.86

Weeks
No. of Cushman

1346-D

Cushman
Naples place Ky.

72

Pl49
16+99⁶⁴

20.00
11.80
3.11
C-8.69

2+50

17.90
11.14
4.11
C-7.03

M.H.#13 (P71)

invent = 19.55
cut. = 7.03
El. stake = 20.58
8.46
29.047

16+50
1.3%

19.36
12.44
4.48
C-7.96

2+00

17.05
11.99
5.30
C-6.69

16+00

18.71
13.09
5.186
C-7.23

1+50

1.70%

16.20
12.84
C.44
C-6.40

15+74⁶⁴ M.H.#15
No A

18.38
13.42
6.50
C-6.92

1+00

15.35
13.69
7.48
C-6.21

15+50
1.3%

18.06
13.74
7.14
C-6.60

0+50

14.50
14.54
8.28
C-6.26

15+00

31.80 x
17.41
14.39
8.87
C-5.52

0+00 = M.H.#13
Morgan (P71)

29.04 x
13.65
15.39
8.58
C-6.81

Cushman

1347-D

1348-D

73

5+09⁷⁵ M.H.#45

↓ 30.20
10.49
3.40
C-7.09

30.50 ↑
10.19
3.40
C-6.79

5+00

29.47
11.22
3.86
C-7.36

4+50
7.59%

25.72
14.97
6.55
C-8.42

P149
6+69⁷⁵

42.50
10.74
0.92
C-9.82

4+00

275
21.97
18.72
7.47
C-9.25

6+50

41.00
12.24
3.58
C-8.66

3+76³⁷ M.H.#40

↓ 20.05
20.64
11.03
C-9.61

20.20 ↑
20.49
11.03
C-9.46 T.P.
19.60

6+00
7.59%

53.24
37.25
15.99
9.52
C-6.47

3+50

29.04
18.75
10.29
2.67
C-7.62

9.44
0.40
C-9.04

5+50

T.P.
33.50
7.19
0.50
C-6.69

3+00

29.04 T
0.00
28.64 - 10.00
12.05
40.69 T
0.50
40.19
13.05
53.24 T

Cushman Place.

1347-D

74

INDEXED
W.K.
OCT 6 1949

T.P. 3450 - P. 73

2450

24.00
10.14
4.23
C-5.91

28.64
5.50
34.14 X

2400

23.25
10.89
6.39
C-4.50

1450

1.590

22.50
11.64
6.77
C-4.87

1400

21.75
12.39
6.07
C-6.32

3405 M.H. #102

24.83
9.31
2.75
C-6.56

0450

21.00
13.14
4.82
C-8.32

3400

24.75
9.39
2.86
C-6.53

0400 = M.H. #40
(P. 73)

34.14 X
20.25
13.89
4.48
C-9.41

40.69 X
20.44
11.03
C-9.41

Outfall Sewer

Pacific Hy. to Weeks and Knoxville str.

As constructed

5-10-49

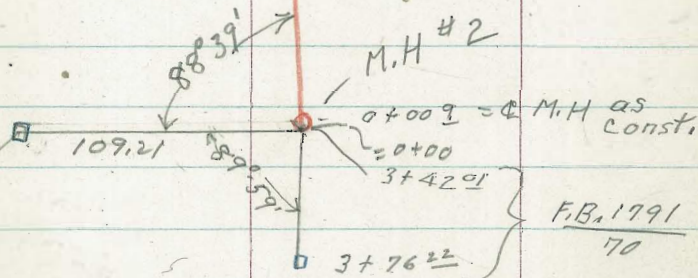
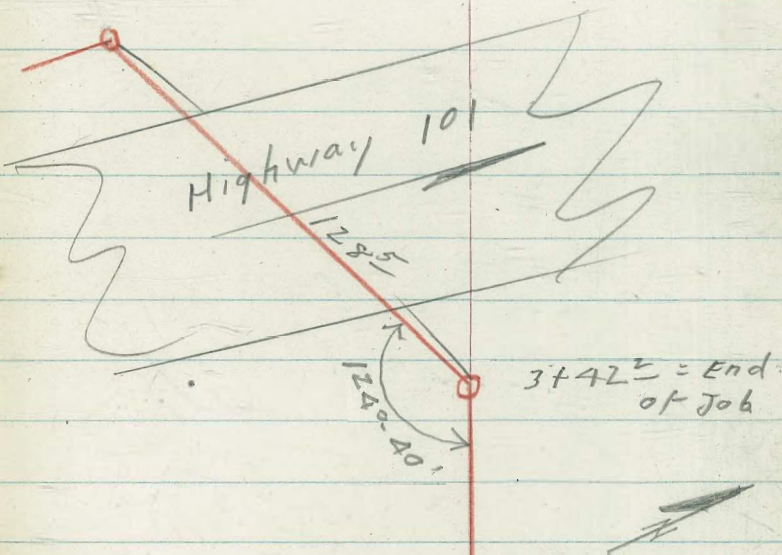
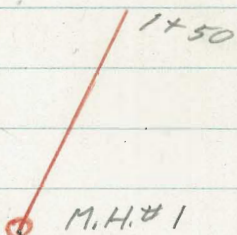
Sommermejer
McCoy
Alley

See page 33 for original
stakes.

INDEXED
WK
OCT 6 1949

Also
F.B. 1791
G 246

1+10.9
Δ 29° 11' RT.



1+50

Morena M.H. #26 to Viola St.
(Line Change 7-7-49)

Tang. 0.83
Sec. 457

M.H. 27A

Sec G 246

76

57

4+50
6.45
20.18
10.96
C-9.22 26.63x
5.70
20.93
11.86
C-9.07

← T.P.

4+25

4+00
4.95
9.32
0.41
C-8.91

3+75
4.20
10.07
1.27
C-8.80

3+50
3.45
10.82
2.27
C-8.59

3+25^{dp.}
2.70
11.57
3.17
C-8.44

3+00
1.95
12.32
3.81
C-8.51

2+75
1.20
13.07
4.49
C-8.58

Sec.: 457
Tang.: 0.83
2+60 = M.H. #26
From P. 58
Δ 21° N.

0.75

14.27

6+63⁷¹
Δ 21° N.

6+29¹²

M.H. #27
5+94⁵³

5+75

5+50

5+25

5+00

4+75

12.14
14.49
4.70
C-9.79

11.44
15.19
5.42
C-9.77

10.74
15.89
5.92
C-9.97

10.20
16.43
6.44
C-9.99

9.45
17.18
7.17
C-10.01

8.70
17.93
8.09
C-9.84

7.75
18.68
9.03
C-9.65

7.20
19.43
10.01
C-9.42

26.67

B.M. #3-P55

8.84
5.43
14.27x
.21

13.86
12.77
26.63x

Restake Naples (Also R63)

M.H. 17 to 18

79/13/49

77

Cont. p. 63,
6+00

5.37

B.M. #2 - P.54

2.06
4.21
6.27
1.29
4.98
12.45
17.43
1.86
15.57
T.P. To page 63

Viola St.
M.H. # 28
8+05.2

13.56
13.07
5.03
C-8.04

8+00

13.50
13.13
4.98
C-8.15

7+75

13.25
13.38
4.78
C-8.60

7+50

13.00
13.63
4.63
C-9.00

7+25

12.75
13.88
4.53
C-9.35

7+00

12.50
14.13
4.53
C-9.60

6+75

12.25
14.38
4.66
C-9.72

26.63

+50

4.17

5+00

2.97
14.46

4+50

1.77
15.66
1.69

4+00

10.57
16.86
9.85
C-7.01

T.P.

+50

17.43
-0.63
18.06
18.45
C-5.61

M.H. 17 T.P.
3+00

5.27
-1.35
7.62

Darcas + Moreno

198
45
973

Morena
S.W. Mon. Darcas +

16.19
5.66
21.85

From P. 28

0 + 50

ok
C-8.12 9.95
11.90

0 + 40

9.80
12.05
3.42
C-8.63

0 + 30

9.65
12.20
3.12
C-9.08

0 + 20

9.50
12.35
3.05
C-9.30

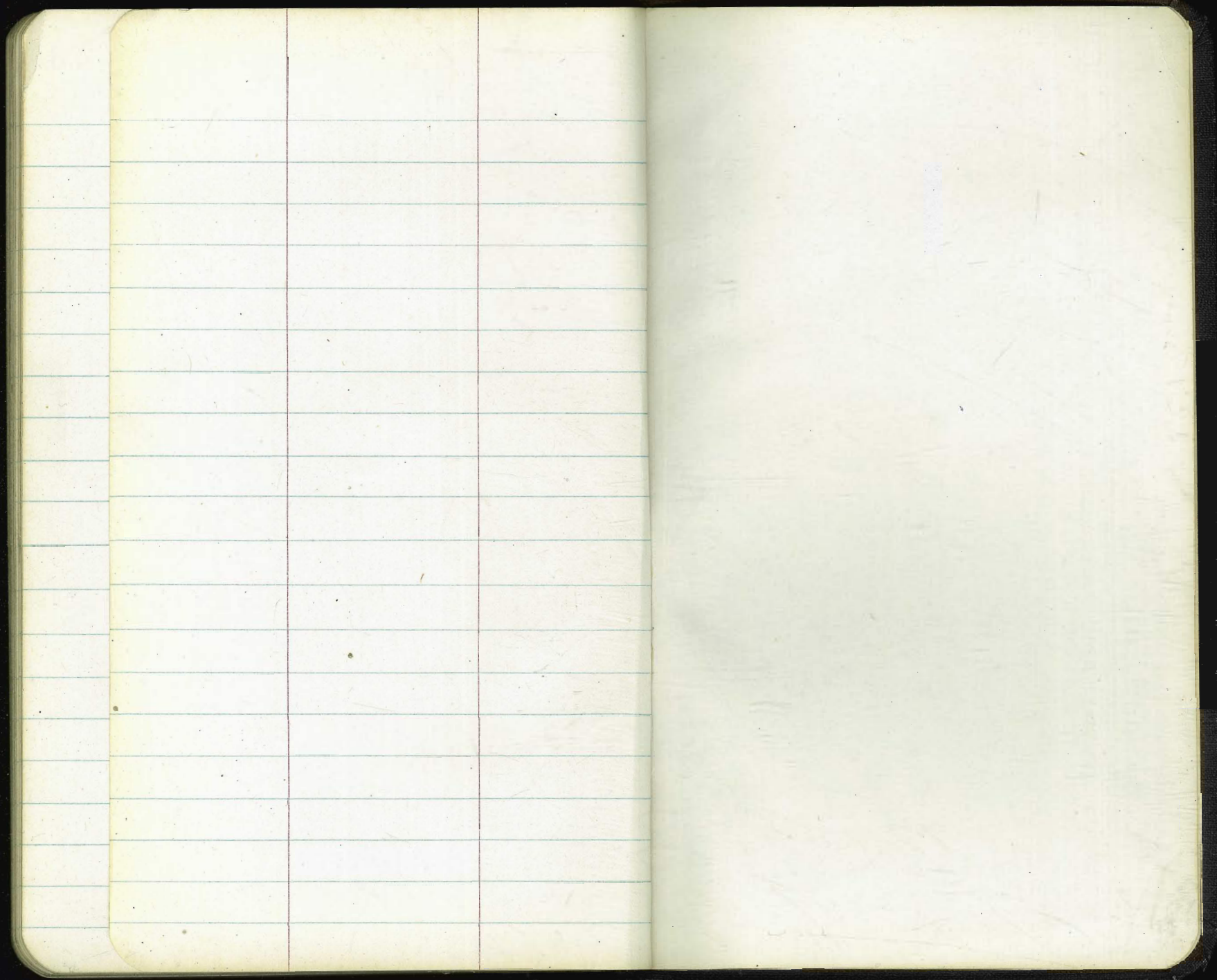
0 + 10

9.35
12.50
3.60
C-8.90

M.H. #20
0 + 00 =

8.75
7.70
9.75
C-8.13

9.20
12.65
4.77
7.88



137.62

56.07
52

69.97

1.2142
9

11.3136

11406.21
187

4434

36.4
25

33.8

36.68

1732
1416

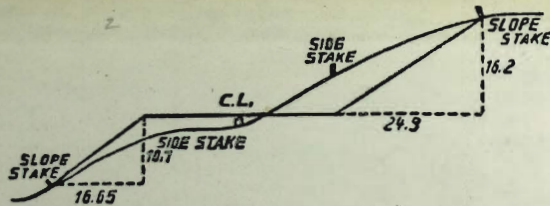
276

26-30
1.16

142.30

943.6
828.6

115



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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