

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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Completely
except pages 32 to 39
75 to 78

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TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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B.M. - M.H. -	142.41
P.O.T. Hub. - 4+12.91	166.08
Nail in pole - 55 ⁺¹	163.73
stub at 8+00	137.92
Toe stub - 14+50 - Rt.	145.30

4-5-49

2

Rough Grades for Imperial Ave
 Realig - 7389-L - w.o. 22014 - 7.0.

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W.R.

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	Lt.	±	Rt.
2+00	$\begin{array}{r} 64.7 \\ 64.2 \\ \hline cas \\ (5.6) \\ 33.5 \end{array}$	32	$\begin{array}{r} 65.6 \\ 63.9 \\ \hline F(1.7) \\ 35.5 \text{ out.} \end{array}$
32 1+50	$\begin{array}{r} 64.1 \\ 63.7 \\ \hline F(0.4) \\ 32.6 \end{array}$	33	$\begin{array}{r} 64.9 \\ 63.1 \\ \hline F(1.2) \\ 34.8 \end{array} \quad \begin{array}{r} 64.9 \\ 63.2 \\ \hline (1.7) \\ 35.5 \end{array}$
33.8 1+00	$\begin{array}{r} 63.8 \\ 62.8 \\ \hline F(1.0) \\ 35.3 \end{array}$	33	$\begin{array}{r} 63.7 \\ 63.3 \\ \hline F(0.4) \\ 33.6 \end{array}$
38.2 0+50	$\begin{array}{r} 63.1 \\ 62.6 \\ \hline F(0.5) \\ 39 \text{ out} \end{array}$	33	$\begin{array}{r} 62.6 \\ 62.5 \\ \hline C(0.1) \\ 33.1 \end{array}$
40 0+00	$\begin{array}{r} 62.4 \\ 62.1 \\ \hline F(0.3) \\ 40.5 \text{ out} \end{array}$	33	$\begin{array}{r} 62.1 \\ 61.7 \\ \hline C(0.4) \\ 33.4 \end{array}$

Figures in [] = P.P. stakes	Lt cb. Grade	Figures in () = Toe stakes	±	Rt
5+50 $\begin{bmatrix} -0.2 \\ 10 \end{bmatrix}$	$\begin{array}{r} 56.7 \\ 37.0 \\ \hline = 19.7 \end{array}$	$\begin{pmatrix} 11.7 \\ 69.5 \end{pmatrix}$ 11.7 11.2 40 20	10.1 8.3 5.7 ± 20 40	$\begin{pmatrix} 2.2 \\ 55.6 \end{pmatrix}$ 56.9 $\begin{array}{r} 46.5 \\ \hline = 10.4 \end{array}$ $\begin{bmatrix} +4.0 \\ 10 \end{bmatrix}$
			$\pi = 148.68$	
5+00 $\begin{bmatrix} -0.1 \\ 10 \end{bmatrix}$	$\begin{array}{r} 58.6 \\ 38.7 \\ \hline = 19.9 \end{array}$	$\begin{pmatrix} 17.5 \\ 69.8 \end{pmatrix}$ 17.1 15.4 40 20	13.1 10.7 6.0 ± 20 40	$\begin{pmatrix} 3.4 \\ 49.6 \end{pmatrix}$ 59.2 $\begin{array}{r} 52.8 \\ \hline = 6.4 \end{array}$ $\begin{bmatrix} +4.1 \\ 10 \end{bmatrix}$
			$\pi = 156.18$	
4+50 $\begin{bmatrix} -1.5 \\ 10 \end{bmatrix}$	$\begin{array}{r} 60.2 \\ 51.0 \\ \hline = 9.2 \end{array}$	$\begin{pmatrix} 17.8 \\ 53.8 \end{pmatrix}$ 16.2 13.4 40 20	11.7 8.9 4.7 ± 20 40	$\begin{pmatrix} 4.1 \\ 43.3 \end{pmatrix}$ 64.7 $\begin{array}{r} 61.4 \\ \hline = 3.3 \end{array}$ $\begin{bmatrix} +1.2 \\ 10 \end{bmatrix}$
4+00 $\begin{bmatrix} 0.9 \\ 10 \end{bmatrix}$	$\begin{array}{r} 64.3 = \text{El. stake} \\ 61.5 \\ \hline = 2.8 \end{array}$	$\begin{pmatrix} 4.5 \\ 42.8 \end{pmatrix}$ 4.0 3.3 40 20	2.4 2.6 2.9 3.0 5.6 5.7 ± 20 40 42 51 60	$\begin{array}{r} 62.9 \\ 62.7 \\ \hline = 0.1 = 90 \text{ out.} \end{array}$
			$\pi = 168.82$	
3+50 $\begin{bmatrix} -0.3 \\ 10 \end{bmatrix}$	$\begin{array}{r} 65.0 \\ 62.5 \\ \hline = 2.5 \end{array}$	$\begin{pmatrix} 5.3 \\ 42.5 \end{pmatrix}$ 4.6 40 20	4.3 4.2 6.6 6.8 6.80 7.06 ± 24 33 43 60 71	$\begin{array}{r} 63.7 \\ 63.0 \\ \hline = 0.7 \end{array}$ 7.3 76 = 5 back
			edge pave	
3+00 $\begin{bmatrix} -0.7 \\ 10 \end{bmatrix}$	$\begin{array}{r} 66.2 \\ 63.4 \\ \hline = 2.8 \end{array}$	$\begin{pmatrix} 4.1 \\ 38.8 \end{pmatrix}$ 4.4 40 20	5.0 5.2 6.1 6.45 6.36 ± 15 18 26 44	7.0 65.6 6.6 60.5 63.2 65.5 out $\begin{array}{r} 2.4 \\ \hline = 66.5 \end{array}$
			edge	
2+50	$\begin{array}{r} 65.1 \\ 64.0 \\ \hline = 1.1 \end{array}$	$\begin{pmatrix} 5.2 \\ 33.7 \end{pmatrix}$ 5.1 40 20	5.6 5.9 6.04 6.6 ± 11 30 45	66.1 66.0 6.6 63.4 63.7 50 out $\begin{array}{r} 2.7 \\ \hline = 49 \end{array}$
			$\pi = 170.31$	

9+00	$\begin{bmatrix} -0.4 \\ 10 \end{bmatrix}$	$\begin{array}{r} 47.0 \\ 36.3 \\ \hline F 10.7 \end{array}$	$\begin{pmatrix} 8.2 \\ 56.1 \end{pmatrix}$	$\begin{array}{cc} 8.6 & 8.6 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 7.7 & 7.1 & 7.3 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 8.8 \\ 57.0 \end{pmatrix}$	$\begin{array}{r} 47.0 \\ 35.7 \\ \hline F 11.3 \end{array}$	$\begin{bmatrix} +0.7 \\ 10 \end{bmatrix}$
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8+50	$\begin{bmatrix} +1.0 \\ 10 \end{bmatrix}$	$\begin{array}{r} 47.8 \\ 35.0 \\ \hline F 12.8 \end{array}$	$\begin{pmatrix} 9.5 \\ 59.2 \end{pmatrix}$	$\begin{array}{cc} 9.5 & 9.0 \\ 40 & 20 \end{array}$	$\begin{array}{cccc} 8.7 & 8.3 & 6.9 & 6.5 \\ \pm & 20 & 20 & 40 \end{array}$	$\begin{pmatrix} 6.3 \\ 54.4 \end{pmatrix}$	$\begin{array}{r} 47.8 \\ 38.2 \\ \hline F 9.6 \end{array}$	$\begin{bmatrix} 0.0 \\ 10 \end{bmatrix}$
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8+00	$\begin{bmatrix} -0.5 \\ 10 \end{bmatrix}$	$\begin{array}{r} 48.7 \\ 36.7 \\ \hline F 12.0 \end{array}$	$\begin{pmatrix} 7.8 \\ 58.0 \end{pmatrix}$	$\begin{array}{cc} 7.1 & 6.6 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 6.6 & 6.6 & 6.7 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 6.0 \\ 55.3 \end{pmatrix}$	$\begin{array}{r} 48.7 \\ 38.5 \\ \hline F 10.2 \end{array}$	$\begin{bmatrix} -0.1 \\ 10 \end{bmatrix}$
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7+50	$\begin{bmatrix} -1.0 \\ 10 \end{bmatrix}$	$\begin{array}{r} 49.9 \\ 37.1 \\ \hline F 12.8 \end{array}$	$\begin{pmatrix} 7.4 \\ 59.2 \end{pmatrix}$	$\begin{array}{cc} 7.1 & 6.9 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 7.3 & 6.6 & 4.8 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 4.3 \\ 54.5 \end{pmatrix}$	$\begin{array}{r} 49.9 \\ 40.2 \\ \hline F 9.7 \end{array}$	$\begin{bmatrix} +0.4 \\ 10 \end{bmatrix}$
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144.49

7+00	$\begin{bmatrix} -0.2 \\ 10 \end{bmatrix}$	$\begin{array}{r} 51.3 \\ 36.8 \\ \hline F 14.5 \end{array}$	$\begin{pmatrix} 9.5 \\ 61.7 \end{pmatrix}$	$\begin{array}{cc} 9.4 & 9.4 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 8.6 & 7.5 & 6.5 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 5.3 \\ 55.4 \end{pmatrix}$	$\begin{array}{r} 51.3 \\ 41.0 \\ \hline F 10.3 \end{array}$	$\begin{bmatrix} +0.7 \\ 10 \end{bmatrix}$
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6+50	$\begin{bmatrix} +0.5 \\ 10 \end{bmatrix}$	$\begin{array}{r} 53.0 \\ 37.8 \\ \hline F 15.2 \end{array}$	$\begin{pmatrix} 8.5 \\ 62.8 \end{pmatrix}$	$\begin{array}{cc} 8.7 & 8.7 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 7.9 & 7.6 & 6.2 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 4.2 \\ 56.4 \end{pmatrix}$	$\begin{array}{r} 53.0 \\ 42.1 \\ \hline F 10.9 \end{array}$	$\begin{bmatrix} +0.8 \\ 10 \end{bmatrix}$
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$\pi =$ 146.25

6+00	$\begin{bmatrix} -0.2 \\ 10 \end{bmatrix}$	$\begin{array}{r} 54.8 \\ 37.4 \\ \hline F 17.0 \end{array}$	$\begin{pmatrix} 10.9 \\ 65.5 \end{pmatrix}$	$\begin{array}{cc} 10.9 & 11.3 \\ 40 & 20 \end{array}$	$\begin{array}{ccc} 10.8 & 9.4 & 7.9 \\ \pm & 20 & 40 \end{array}$	$\begin{pmatrix} 5.6 \\ 57.5 \end{pmatrix}$	$\begin{array}{r} 54.8 \\ 43.1 \\ \hline F 11.7 \end{array}$	$\begin{bmatrix} +1.7 \\ 10 \end{bmatrix}$
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$\pi =$ 148.68

12+50	$\left[\frac{+0.7}{10} \right]$	$\begin{array}{r} 47.8 \\ 47.2 \\ \hline F 0.6 \end{array}$	$\begin{pmatrix} 3.5 \\ 40.9 \end{pmatrix}$	$\begin{array}{r} 3.5 \\ 40 \\ 4.2 \\ 20 \end{array}$	$\begin{array}{r} 5.2 \\ \neq \\ 6.8 \\ 20 \\ 7.0 \\ 40 \end{array}$	$\begin{pmatrix} 6.7 \\ 45.7 \end{pmatrix}$	$\begin{array}{r} 47.8 \\ 44.0 \\ \hline F 3.8 \end{array}$	$\left[\frac{+0.1}{10} \right]$
-------	----------------------------------	---	---	---	--	---	---	----------------------------------

12+00	$\left[\frac{+0.7}{10} \right]$	$\begin{array}{r} 47.0 \\ 45.9 \\ \hline F 1.1 \end{array}$	$\begin{pmatrix} 4.8 \\ 41.7 \end{pmatrix}$	$\begin{array}{r} 5.0 \\ 40 \\ 5.5 \\ 20 \end{array}$	$\begin{array}{r} 6.0 \\ \neq \\ 7.0 \\ 20 \\ 7.7 \\ 40 \end{array}$	$\begin{pmatrix} 7.7 \\ 46.0 \end{pmatrix}$	$\begin{array}{r} 47.0 \\ 43.0 \\ \hline F 4.0 \end{array}$	$\left[\frac{-0.4}{10} \right]$
-------	----------------------------------	---	---	---	--	---	---	----------------------------------

11+50	$\left[\frac{+0.7}{10} \right]$	$\begin{array}{r} 46.5 \\ 45.5 \\ \hline F 1.0 \end{array}$	$\begin{pmatrix} 5.2 \\ 41.5 \end{pmatrix}$	$\begin{array}{r} 5.5 \\ 40 \\ 6.9 \\ 20 \end{array}$	$\begin{array}{r} 7.0 \\ \neq \\ 7.1 \\ 20 \\ 8.8 \\ 40 \end{array}$	$\begin{pmatrix} 9.3 \\ 47.6 \end{pmatrix}$	$\begin{array}{r} 46.5 \\ 41.4 \\ \hline F 5.1 \end{array}$	$\left[\frac{-0.7}{10} \right]$
-------	----------------------------------	---	---	---	--	---	---	----------------------------------

11+00	$\left[\frac{+0.6}{10} \right]$	$\begin{array}{r} 46.1 \\ 43.8 \\ \hline F 2.3 \end{array}$	$\begin{pmatrix} 6.9 \\ 43.5 \end{pmatrix}$	$\begin{array}{r} 7.2 \\ 40 \\ 8.0 \\ 20 \end{array}$	$\begin{array}{r} 8.0 \\ \neq \\ 7.9 \\ 20 \\ 9.6 \\ 40 \end{array}$	$\begin{pmatrix} 10.9 \\ 49.5 \end{pmatrix}$	$\begin{array}{r} 46.1 \\ 39.8 \\ \hline F 6.3 \end{array}$	$\left[\frac{-0.6}{10} \right]$
-------	----------------------------------	---	---	---	--	--	---	----------------------------------

10+50	$\left[\frac{+0.6}{10} \right]$	$\begin{array}{r} 46.0 \\ 42.2 \\ \hline F 3.8 \end{array}$	$\begin{pmatrix} 8.8 \\ 45.7 \end{pmatrix}$	$\begin{array}{r} 8.7 \\ 40 \\ 11.1 \\ 20 \\ 12.6 \\ \neq \\ 12.8 \\ 20 \\ 12.7 \\ 40 \end{array}$	$\begin{pmatrix} 11.2 \\ 49.8 \end{pmatrix}$	$\begin{array}{r} 46.0 \\ 39.5 \\ \hline F 6.5 \end{array}$	$\left[\frac{+0.1}{10} \right]$
-------	----------------------------------	---	---	--	--	---	----------------------------------

$$T = \underline{150.66}$$

10+00	$\left[\frac{+0.8}{10} \right]$	$\begin{array}{r} 46.1 \\ 39.3 \\ \hline F 6.8 \end{array}$	$\begin{pmatrix} 5.2 \\ 50.2 \end{pmatrix}$	$\begin{array}{r} 5.7 \\ 40 \\ 6.0 \\ 20 \end{array}$	$\begin{array}{r} 7.3 \\ \neq \\ 7.2 \\ 20 \\ 6.0 \\ 40 \end{array}$	$\begin{pmatrix} 6.8 \\ 52.6 \end{pmatrix}$	$\begin{array}{r} 46.1 \\ 37.7 \\ \hline F 8.4 \end{array}$	$\left[\frac{-0.1}{10} \right]$
-------	----------------------------------	---	---	---	--	---	---	----------------------------------

9+50		$\begin{array}{r} 46.5 \\ 34.1 \\ \hline F 12.4 \end{array}$	$\begin{pmatrix} 10.4 \\ 58.6 \end{pmatrix}$	$\begin{array}{r} 7.0 \\ 40 \\ 6.7 \\ 20 \end{array}$	$\begin{array}{r} 6.5 \\ \neq \\ 6.7 \\ 20 \\ 6.5 \\ 40 \end{array}$	$\begin{pmatrix} 6.6 \\ 52.9 \end{pmatrix}$	$\begin{array}{r} 46.5 \\ 37.9 \\ \hline F 8.6 \end{array}$	$\left[\frac{+0.2}{10} \right]$
------	--	--	--	---	--	---	---	----------------------------------

$$T = \underline{144.49}$$

16+00 $\left[\frac{+0.5}{10}\right]$ 59.1 (11.5) 10.3 12.1 14.0 14.0 13.3 11.6 10.5 5.2 5.7 5.9 7.2 6.8 2.3
 $\frac{47.0}{F 12.1}$ 43 20 15 + 4 5 19 24 45 62 79 88 95
 edge edge edge

15+50 $\left[\frac{+0.6}{10}\right]$ 57.6 (12.7) 13.3 10.5 12.0 14.2 14.2 12.6 12.4 12.1 7.0 7.3 7.6 8.4 8.1 0.8
 $\frac{45.1}{F 10.8}$ 40 27 18 14 4 5 20 40 60 73 edge 49 107 117 130
 edge edge

15+00 $\left[\frac{+0.7}{10}\right]$ 55.9 (13.4) 13.2 13.3 14.6 15.0 12.9 12.9 12.6 (12.5) 53.8 $\left[\frac{+0.4}{10}\right]$
 $\frac{45.1}{F 10.8}$ 40 20 14 4 10 20 40 (51.7) $\frac{46.0}{F 7.8}$

158.49

14+50 $\left[\frac{+0.3}{10}\right]$ 53.9 (9.6) 9.3 9.4 10.0 8.8 9.0 (8.6) 52.5 $\left[\frac{+0.3}{10}\right]$
 $\frac{44.3}{F 9.6}$ 40 20 4 20 40 (50.8) $\frac{45.3}{F 7.2}$

14+00 $\left[\frac{+0.2}{10}\right]$ 52.0 (8.8) 9.9 10.1 10.9 9.9 9.7 (10.0) 51.1 $\left[\frac{0.0}{10}\right]$
 $\frac{45.1}{F 6.9}$ 40 20 4 20 40 (50.8) $\frac{43.9}{F 7.2}$

12+60 Brk. 4.6 9.7 10.1 9.8 11.7 11.6
 40 30 20 4 20 40

13+50 $\left[\frac{+0.6}{10}\right]$ 50.2 (4.5) 4.7 5.5 6.8 8.5 11.4 (12.3) 49.8 $\left[\frac{+0.6}{10}\right]$
 $\frac{49.4}{F 0.8}$ 40 20 4 20 40 (52.5) $\frac{41.6}{F 8.2}$

13+00 $\left[\frac{+0.8}{10}\right]$ 49.4 (4.5) 4.5 6.1 7.1 9.5 10.4 (10.7) 48.7 $\left[\frac{+0.1}{10}\right]$
 $\frac{48.8}{c 0.6}$ 40 20 4 20 40 (49.3) $\frac{43.2}{F 5.5}$

$\pi = 153.86$

19+50

19+00

18+50

18+00

17+75

17+50

17+00

16+50

Lt

62.3
61.0
F 1.362.15
61.05
F 1.162.0
48.3
F 13.7New
19.861.2
48.6
F 12.6New
21.00560.2
49.4
F 10.8(5.3)
5.1(5.30)
5.0(10.2)
68.1(9.9)
64.9(9.1)
60.75.3
4.95.0
48.38.0
47.512.1
4.610.5
44.55.5
205.91
7+1.6
3212.8
3812.2
205.91
7edge
Real
have \uparrow +1.3
2011.0
2414.2
176.30
±

166.35

0.7 - Rest
Same
±12.
1014.0
8

Same

Same

0.7 - Rest
Same
±2.16
23
edge
±

67.8

65.4

63.2

63.2

0.7 - Rest
Same
±2.96
29.9
±7.8
61.55.4
60.93.2
60.20.7 - Rest
Same
±12.
1014.0
8

C 6.3

C 4.5

C 3.0

C 3.0

0.7 - Rest
Same
±- Same
±

158.49

N. Side

1:1

F.L. of
Bottom

F.L. of Bottom

8

Channel

Grade

() = Toe [] = RP.

S. Side = 1 1/2 : 1

77 Lt. of 17+01

156.00

0+00 = P.C. at E. end.

$\left[\frac{+1.3}{10} \right]$	$\frac{50.8}{46.2}$	(5.2)	7.6	
	$\frac{46.6}{46.2}$	(34.6)	30	

46.2

+50

$\left[\frac{-0.6}{10} \right]$	$\frac{49.4}{45.4}$	(6.4)	6.3	
	$\frac{44.2}{45.4}$	(34.2)	30	

45.4

1~

$\left[\frac{-1.5}{10} \right]$	$\frac{50.6}{44.6}$	(5.4)	5.1	8.0
	$\frac{46.0}{44.6}$	(36)	30	30

44.6

+50

$\left[\frac{+1.0}{10} \right]$	$\frac{46.7}{43.9}$	(9.3)	9.3	10.1
	$\frac{42.8}{43.9}$	(32.8)	30	30

43.9

RT

E

LT

N. side 1:1

S. side 1 1/2:1

9

 $\bar{\pi} = 156.00$

2~	$\left[\frac{+0.1}{10} \right]$	43.1	$\left(\frac{9.7}{33.2} \right)$	$\frac{10.1}{30}$	$\frac{10.0}{30}$	$\left(\frac{10.0}{34.4} \right)$	$\frac{46.3}{43.1}$	
+50	$\left[\frac{+0.6}{10} \right]$	$\frac{49.7}{42.3}$ 27.4	$\left(\frac{6.3}{27.4} \right)$	$\frac{9.0}{30}$	$\frac{11.8}{30}$	$\left(\frac{11.8}{32.9} \right)$	$\frac{44.2}{42.3}$	$\left[\frac{+0.2}{10} \right]$
3~	above street	41.5		$\frac{5.9}{30}$		$\left(\frac{7.2}{41.0} \right)$	$\frac{48.8}{41.5}$	$\left[\frac{-1.6}{10} \right]$
+50		40.8		$\frac{2.5}{30}$		$\left(\frac{4.7}{45.8} \right)$	$\frac{51.3}{40.8}$	$\left[\frac{-0.4}{10} \right]$
				$\bar{\pi} = 159.72$				
4~		40.0		$\frac{4.7}{30}$		$\left(\frac{6.5}{49.8} \right)$	$\frac{53.2}{40.0}$	$\left[\frac{-0.7}{10} \right]$
+50		39.2		$\frac{6.3}{30}$		$\left(\frac{7.5}{49.5} \right)$	$\frac{52.2}{39.2}$	$\left[\frac{-0.8}{10} \right]$
5~		38.4		$\frac{7.5}{30}$		$\left(\frac{8.4}{49.4} \right)$	$\frac{51.3}{38.4}$	$\left[\frac{-0.7}{10} \right]$
+50		37.7		$\frac{8.2}{30}$		$\left(\frac{9.3}{49.1} \right)$	$\frac{50.4}{37.7}$	$\left[\frac{-0.4}{10} \right]$
6~		36.9		$\frac{11.0}{30}$		$\left(\frac{11.3}{47.3} \right)$	$\frac{48.4}{36.9}$	$\left[\frac{+0.2}{10} \right]$
+50		36.1		$\frac{12.7}{30}$		$\left(\frac{13.0}{45.9} \right)$	$\frac{46.7}{36.1}$	$\left[\frac{+5.7}{10} \right]$

R+

L+

N. side - 1:1

 $\bar{\pi} = 150.23$

7+00

35.3

Above 8' cut.

+50

34.6

8 ~

 $\left[\begin{array}{c} +0.6 \\ 10 \end{array} \right]$

40.2

33.8

C 6.4

(10.0)

9.6

30

+50

 $\left[\begin{array}{c} +0.2 \\ 10 \end{array} \right]$

34.1

33.0

C 5.1

(4.3)

4.2

30

9 ~

 $\left[\begin{array}{c} +0.6 \\ 10 \end{array} \right]$

37.1

32.2

C 4.9

(5.3)

5.8

30

+50

 $\left[\begin{array}{c} +0.5 \\ 10 \end{array} \right]$

36.6

31.5

C 5.1

(5.8)

5.9

30

10 ~

 $\left[\begin{array}{c} +0.6 \\ 10 \end{array} \right]$

33.4

30.7

C 2.7

(9.0)

9.2

30

+50

Brush

29.9

+7.8 = end.

 $\left[\begin{array}{c} 0.0 \\ 10 \end{array} \right]$

36.5

29.5

C 7.0

(5.9)

6.1

30

S side - 1 1/2:1

10

4.4

30

 $\left(\begin{array}{c} 4.6 \\ 45.5 \end{array} \right)$

45.6

35.3

C 10.3

 $\left[\begin{array}{c} +0.6 \\ 10 \end{array} \right]$

5.4

30

 $\left(\begin{array}{c} 5.3 \\ 45.5 \end{array} \right)$

44.9

34.6

C 10.3

 $\left[\begin{array}{c} -0.1 \\ 10 \end{array} \right]$

8.4

30

 $\left(\begin{array}{c} 9.1 \\ 41.0 \end{array} \right)$

41.1

33.8

C 7.3

 $\left[\begin{array}{c} -0.4 \\ 10 \end{array} \right]$ $\bar{\pi} = 142.42$

7.4

30

 $\left(\begin{array}{c} 7.2 \\ 33.3 \end{array} \right)$

35.2

33.0

C 2.2

 $\left[\begin{array}{c} -0.1 \\ 10 \end{array} \right]$

8.9

30

 $\left(\begin{array}{c} 9.1 \\ 31.6 \end{array} \right)$

33.3

32.2

C 1.1

 $\left[\begin{array}{c} -1.0 \\ 10 \end{array} \right]$

10.4

30

 $\left(\begin{array}{c} 10.4 \\ 30.8 \end{array} \right)$

32.0

31.5

C 0.5

 $\left[\begin{array}{c} 0.0 \\ 10 \end{array} \right]$

11.3

30

 $\left(\begin{array}{c} 11.3 \\ 30.6 \end{array} \right)$

31.1

30.7

C 0.4

 $\left[\begin{array}{c} -0.4 \\ 10 \end{array} \right]$

29.9 = Meets channel

29.5

Ditch from Culvert to Channel

() = Toe

 $\pi = 150.23$

1:1 cut.

Lt.

Rt.

outlet of Pipe

0 + 00 =

(8.1)
(7.2)42.1
36.45
c 5.7(7.3)
(8.0)42.9
36.4
c 6.5

+ 50

(6.4)
(9.4)43.8
35.9
c 7.9(5.1)
(10.7)45.1
35.9
c 9.2

+ 100

(4.8)
(11.6)45.4
35.3
c 10.1(4.1)
(12.3)46.1
35.3
c 10.8+ 56.6 =
edge of Channel(6.2)
(10.9)44.0
34.65
c 9.4

34.6

Grades for old Imperial at E. end.

Grade

= 0+00

P.C. of curb Curve

52.4 54.3 F 1.9
52.4

+25' - d = 2° 58'

52.9 55.4 F 2.5
52.9

+50 5° 56'

52.8 56.3 F 3.5
52.8

+75' 8° 54'

53.8 57.2 F 3.4
53.8

100 11° 52'

54.8 57.3 F 2.5
54.8

+25' 14° 50'

56.7 58.6 F 1.9
56.7

+50 17° 48'

60.5 60.5 C 1.3
59.2

+75.7 = E.C.

61.9 61.9 C 2.3
59.6opp. 17+65.48
= Rt.

P.C. of 25' Rad. Cb. Return - S. side

3 N. = edge 50.7 $\frac{51.8}{50.7}$ F 1.1

opp. - 5' Back of Line 55.1 $\frac{51.1}{51.7}$ C 3.4

Cor. of Limits of fill by 25' Rad. Ret.

15 + 00 - on Rt.
5.
Cor. by Imp. = both ways
4.8 out 52.0 - F 3.2

Cor. on New Row. 11' out to N. to Cor.
10.5 out to E. 53.8 - F 7.3

Curb Grades

INDEXED

W.K

AUG 17 1949

N. Side

S. side

Ground Return

2 + 25' end	64.09	64.09	64.11 ₀₉	F 0.02	S. end.	62.87	62.87	63.47 _{2.87}	F 0.60
+ 50	63.47	63.48	63.97 ₄₈	F 0.49		62.71	62.72	63.45 _{2.72}	F 0.73
+ 75	63.45	63.45	63.74 ₄₅	F 0.29		62.47	62.48	63.32 _{2.48}	F 0.84
3 + 00	63.17	63.18	63.39 ₁₈	F 0.21		62.40	62.41	63.08 _{2.41}	F 0.67
+ 25'	62.83	62.84	62.97 ₈₄	F 0.13	PC. = 4 + 14.99	61.43	61.43	62.74 _{1.43}	F 1.31
+ 50	62.50	62.51	62.54 ₅₁	F 0.03					
+ 75	62.05	62.06	62.04 ₀₆	C 0.02					
4 + 00	61.58	61.59	61.51 ₅₉	C 0.08					
+ 25'	61.02	61.02	60.89 ₀₂	C 0.13		61.56	62.36 _{1.56}		F 0.80
+ 50	60.12	60.12	60.19 ₁₂	F 0.07	T.P. 60.93	60.93	61.36 _{0.93}		F 0.43
+ 75	59.32	59.32	59.42 ₃₂	F 0.10		60.09	60.39 ₀₉		F 0.21
5 ~	58.47	58.56	58.56 ₄₇	F 0.09		59.29	59.17 ₂₉		C 0.12
+ 25'	57.69	57.63	57.63 ₆₉	C 0.06		58.18	58.02 ₁₈		C 0.16
+ 50	56.72	56.71	56.71 ₇₂	C 0.01		57.19	56.92 ₁₉		C 0.27
+ 75	55.90	55.76	55.76 ₉₀	C 0.14		56.23	55.85 ₂₃		C 0.38
6 ~	55.00	54.80	54.80 ₀₀	C 0.20		55.26	54.83 ₂₆		C 0.43
+ 25'	54.08	53.86	53.86 ₀₈	C 0.22		54.36	53.86 ₃₆		C 0.50
+ 50	53.17	52.97	52.97 ₁₇	C 0.20		53.55	52.97 ₅₅		C 0.58

N Side

S side

6+75	52.33	52.13 ³³	CO.20		52.78	52.13 ²⁷⁸	CO.65
7~	51.48	51.34 ⁴⁸	CO.14		52.04	51.34 ²⁰⁴	CO.70
+25	50.70	50.62 ⁷⁰	CO.08		51.27	50.62 ¹²⁷	CO.65
+50	50.30	49.93 ³⁰	CO.37	✓ T.P.	✓ 50.43	49.93 ⁴³	CO.50
+75	49.86	49.32 ⁸⁶	CO.54		✓ 49.76	49.32 ⁷⁶	CO.44
8~	49.22	48.76 ²²	CO.46		✓ 49.24	48.76 ²⁴	CO.48
+25	48.64	48.24 ⁶⁴	CO.40		✓ 48.72	48.24 ⁷²	CO.48
+50	48.18	47.76 ¹⁸	CO.42		✓ 48.25	47.76 ²⁵	CO.49
+75	47.62	47.37 ⁶²	CO.25		✓ 47.85	47.37 ⁸⁵	CO.48
9~	47.30	47.01 ³⁰	CO.29		✓ 47.44	47.01 ⁴⁴	CO.43
+25	46.76	46.72 ⁷⁶	CO.04		✓ 46.95	46.72 ⁹⁵	CO.23
+50	46.11	46.48 ¹¹	F 0.37		✓ 46.69	46.48 ⁶⁹	CO.21
+75	45.62	46.29 ⁶²	F 0.67	+6.69 75	✓ 46.54	46.29 ⁵⁴	CO.25
10~	45.53	46.14 ⁵³	F 0.61		46.38	46.14 ³⁸	CO.24
+25	45.29	46.07 ²⁹	F 0.78		46.17	46.07 ¹⁷	CO.10
+50		46.04	F 0.84	new	45.34	46.04 ³⁴	F 0.85
+75	45.68	46.06 ⁶⁸	F 0.38		45.01	46.06 ⁰¹	F 1.05
11~	45.86	46.14 ⁸⁶	F 0.28		45.64	46.14 ⁶⁴	F 0.50
+25	46.22	46.27 ²²	F 0.05		46.01	46.27 ⁰¹	F 0.26

N. Side

S. Side

16

11 +50	46.58	46. ⁵⁸ 47	C 0.11	46.39	46.47	F 0.08	
+75	46.23	46. ²³ 71	F 0.48	46.72	46. ⁷² 71	C 0.01	
12 ~	46.92	47. ⁹² 00	F 0.08	46.89	47. ⁸⁹ 00	F 0.11	
+25	47.44	47. ⁴⁴ 35	C 0.09	47.55	47. ⁵⁵ 35	C 0.20	
+50	47.71	47. ⁷¹ 75	F 0.04	48.08	47. ⁰⁸ 75	C 0.33	
+75	48.30	48. ³⁰ 33	C 0.07	48.54	48. ⁵⁴ 20	C 0.34	
13 ~	48.62	48. ⁶² 79	F 0.17	48.94	48. ⁹⁴ 70	C 0.24	
+25	49.29	49. ²⁹ 44	F 0.15	49.38	49. ³⁸ 23	C 0.15	
+50	50.06	50. ⁰⁶ 20	F 0.14	49.79	49. ⁷⁹ 81	F 0.02	
+75	50.52	50. ⁵² 05	F 0.53	50.37	50. ³⁷ 44	F 0.07	
14 ~	52.01	51. ⁰¹ 97	C 0.04	51.07	51. ⁰⁷ 09	F 0.02	
+25	52.99	52. ⁹⁹ 95	C 0.04	51.75	51. ⁷⁵ 78	F 0.03	
T.P. +50	53.78	53. ⁷⁸ 93	F 0.15	52.40	52. ⁴⁰ 45	F 0.05	
+75	54.64	54. ⁶⁴ 90	F 0.26	52.89	52. ⁸⁹ 14	F 0.25	
15 ~	55.63	55. ⁶³ 84	F 0.21	53.51	53. ⁵¹ 84	F 0.33	
+25 - 0° 04' 30"	56.63	56. ⁶³ 74	F 0.11	53.66	54. ⁶⁶ 02	F 0.36	
+50 31' 30"	57.55	57. ⁵⁵ 60	F 0.05	# 1	53. ³⁵ 95	F 0.60	
+75 58' 15"	58.30	58. ³⁰ 37	F 0.07	# 2	53.11	53. ¹¹ 46	F 0.35
				# 3	52.92	52. ⁹² 73	C 0.19
				# 4 = E.C. on Imperial	50.32	51. ³² 84	F 1.52

Ret.

.15 + 09.35 = P.C. 25' Rad.

N. Side

S. Side 17

16+00	-1° 25'	59.03	59.05	F 0.02	along old Row.			
+25	1° 52'	59.66	59.67	F 0.01	6.74-s	450.05	51.44	F 1.39
+50	2° 19'	60.17	60.17	Grade	10.36 s	49.96	50.90	F 0.94
+75	2° 46'	60.69	60.74	F 0.05	10 s = end.	50.00	50.49	F 0.49
17 ~	3° - 13'	61.15	61.21	F 0.06				
+25	3° 40'	61.47	61.65	F 0.18				
+50	4° 07'	61.70	62.01	F 0.31				
+75	4° 34'	61.90	62.20	F 0.30				
18 ~	5° 01'	61.94	62.24	F 0.30				
+25	5° 28'	61.38	62.09	F 0.71				
+50	5° 54.15"	61.39	61.85	F 0.46				
			1.39					
= Meet cb.		60.99	61.10					

Pave Grades - Imperial

1/4 = sub. Grade

18

N. side

Around Ret.

S. side

2 +25 63.44

S. end.

62.80

+50 63.30

INDEXED

62.78

+75 63.07

W, K
AUG 17 1949

62.65

3 ~ 62.72

62.41

+25 62.30

P.C.

62.07

+50 61.87

+75 61.37

1/4 = sub. grade

1/4 = sub grade

4 ~ 60.44

* +25 60.22

61.69

+50 59.52

59.77

60.13

60.35

60.69

+75 58.75

58.97

59.30

59.41

59.63

5 ~ 57.89

57.99

58.37

58.29

58.50

+25 56.96

57.15

57.39

57.35

57.35

+50 56.04

56.22

56.42

56.32

56.25

+75 55.09

55.26

55.44

55.31

55.18

6 ~ 54.13

54.29

54.47

54.32

54.16

+25 53.19

53.36

53.52

53.36

53.19

+50 52.30

52.47

52.63

52.47

52.30

+75 51.46

51.63

51.79

51.63

51.46

	N.	1/4 = sub.	1/2 = sub.	1/4 = sub.	519
7+00	50.67	50.84	51.00	50.84	50.67
+25'	49.95	50.12	50.29	50.12	49.95
+50	49.26	49.43	49.59	49.43	49.26
+75	48.65	48.82	48.98	48.82	48.65
8~	48.0	48.25	48.41	48.25	48.08
+25'	47.5	47.74	47.90	47.74	47.57
+50	47.11	47.28	47.44	47.28	47.11
+75'	46.70	46.87	47.03	46.87	46.70
9~	46.34	46.51	46.67	46.51	46.34
+25'	46.05	46.22	46.38	46.22	46.05
+50	45.81	45.98	46.14	45.98	45.81
+75'	45.62	45.79	45.95	45.79	45.62
10~	45.47	45.64	45.80	45.64	45.47
+25'	45.40	45.57	45.73	45.57	45.40
+50	45.37	45.54	45.70	45.54	45.37
+75'	45.39	45.56	45.72	45.56	45.39
11~	45.47	45.64	45.80	45.64	45.47
+25'	45.60	45.77	45.93	45.77	45.60
+50	45.80	45.97	46.13	45.97	45.80
+75'	46.04	46.21	46.37	46.21	46.04

	N.	1/4 = sub.	E = sub.	1/4 = sub.	20 S.
12~	46.33 ¹⁷	46.50	46.66	46.50	46.33
+25	46.68 ¹⁷	46.85	47.01	46.85	46.68
+50	47.08 ¹⁷	47.25	47.41	47.25	47.08
+75	47.56	47.72	47.87	47.70	47.53 ¹⁷
13~	48.12	48.27	48.38	48.22	48.03
+25	48.77	48.89	48.94	48.78	48.56
+50	49.53	49.54	49.57	49.34	49.14
+75	50.38	50.27	50.25	49.96	49.77
14~	51.30	51.08	50.97	50.64	50.42
+25	52.28	51.93	51.73	51.35	51.11
+50	53.26	52.80	52.50	52.06	51.79
+75	54.23	53.63	53.24	52.75	52.47
15~	55.19				53.17
+25	56.07				
+50	56.93				
+75	57.70				
16~	58.38				
+25	59.00				
+50	59.50				
+75	60.07				

Grades - Alley - Blk. 93 - E.W. Morse - Sub.
 30th + B 19.5' wide
 Plan - 7213-L
 Book 1840-PT W.O. 31240 - ②

7-13-49

7.0.

N.

S.

0+00 = E.L. 30th

INDEXED

N.Y.K.

AUG 17 1949

208.52

07.25

+10 - Cut - 17' B. 09.43 ^{9.43} 08.58 C 0.85 2' B. 08.40 08.04⁴⁰ C 0.36

+20 Cut - 18' B. 09.42 ^{9.82} 08.80 C 1.02 2' B. 08.84 08.50⁸⁸ C 0.38

+70 Cross - 25' B. 10.97 ^{10.97} 10.34 C 0.63 2' B. 10.06 10.04⁶ C 0.02

1+20 Nail - 0.30 B. 11.85 ^{11.88} ₈₅ F 0.03 Nail - 11' B. 11.76 11.58⁷⁶ C 0.18

+40 - Cross - 1' B. 12.70 ⁷⁰ 12.58 C 0.12 N. - 0.70 B. 13.05 12.28^{3.05} C 0.77

+60 - 2' B. 13.62 ⁶² 13.43 C 0.19 F.L. Sewer ① 13.62 08.43 C 5.19 S. - 0.5 B. 14.29 13.13^{4.29} C 1.16

+80 - 2' B. 14.86 ⁸⁶ 14.33 C 0.53 S. - 0.5 B. 14.58 14.03⁵⁸ C 0.55

2+00 - 2' B. 15.52 ⁵² 15.09 C 0.43 S. - 1' B. 15.74 14.79⁷⁴ F 0.05

N

S

2+20-2'B.

15.91 15.50⁹¹ C 0.41

Nail - 1.07 B.

16.24 15.20⁶²⁴ C 1.04

+40-2'B.

15.77 15.57⁷⁷ C 0.18F.L. Sewer ②
15.77 2'B.
10.59 C 5.1815.61 15.29⁶¹ C 0.32

+60-2'B.

16.22 15.37⁶²² C 0.85

2'B.

15.46 15.07⁴⁶ C 0.39

+80-2'B.

15.88 14.80⁵⁸⁸ C 1.08

3'B - Cross

15.08 14.50⁵⁰⁸ C 0.58

3+00-2'B.

15.51 13.91⁵⁵¹ C 1.60

S-1'B.

14.44 13.61⁴⁴⁴ C 0.83

+20 - Nail 0.98 B.

15.42 12.70⁵⁴² C 2.72

S-1'B.

14.12 12.40⁴¹² C 1.72

+40-3'B.

13.95 11.14³⁹⁵ C 2.81

Nail - 1.26 B.

11.74 10.84¹⁷⁴ C 0.90

+80 - Cross - 2'B.

08.08 07.72⁸⁰⁸ C 0.36

Nail - 33 B.

08.36 07.42⁸³⁶ C 0.94

4+00-2'B.

06.60 06.12⁶⁶⁰ C 0.48

N. 0.6 B.

07.16 05.82⁷¹⁶ C 1.34

+20 - Cross - 3 B.

05.02 04.76⁵⁰² C 0.26

N. 0.46 B.

06.09 04.46⁶⁰⁹ C 1.63

S.

N

4+60 - Nail - 226 B 03.740 ^{3.74} 2.28 C 1.46 2' B. 02.78 ^{2.78} 01.98 C 0.80

5+01.5 = end. - 2' B. 200.84 ^{00.84} 99.71 C 1.13 2' B. 97.91 ^{99.41} 7.91 F 1.50

Grades - Alley in Block 73 - Univ. Hts.

Plan 7267-L - 7-29-49 - 70.

20 Alley - 0.25' exception - both sides

B.M. = S.E. B.P. - Meade + Louisiana 332.70

INDEXED

W.

E.

0+00 = N.L. Meade

W.K.

333.61

332.57

AUG 17 1949

+20 - Nail - 0.41' B.	^{6.42} 34.23	^{6.42} 36.42	^{2.19} 2.33	2' B.	^{5.02} 34.12	35.02	^{5.02} 33.98	^{0.90} 1.07
+40 - N. - 0.12' B.	^{5.70} 34.71	^{5.70} 35.70	^{0.99} 1.11	2' B = Cross	^{5.26} 34.55	35.26	^{5.26} 34.26	^{0.71} 1.00
+60 - 2' B.	^{5.30} 35.05	^{5.30} 35.30	^{0.25} 0.51	cut. 0.51' B.	^{5.59} 34.66	35.59	^{5.59} 34.51	^{0.93} 1.08
+80 - cross - 2' B.	^{5.51} 35.24	^{5.51} 35.51	^{0.27} 0.51	cross - 2' B.	^{5.45} 35.04	35.45	^{5.45} 34.70	^{0.41} 0.75
+120 - 5' B.	^{6.30} 35.48	^{6.30} 36.30	^{0.82} 0.98	Nail - 0.34' B.	^{6.25} 35.28	36.25	^{6.25} 35.02	^{0.97} 1.23
+60 - 1' B.	^{6.04} 35.72	^{6.04} 36.04	^{0.32} 0.40	2' B.	^{5.73} 35.52	35.73	^{5.73} 35.34	^{0.21} 0.39
+200 - 2' B.	^{6.25} 36.25	^{6.25} 35.96	^{0.29} 0.29	2' B.	^{5.82} 35.76	35.82	^{5.82} 35.66	^{0.06} 0.16
+40 - 2' B.	^{6.41} 36.41	^{6.41} 36.20	^{0.21} 0.21	2' B.	^{6.42} 36.20	36.42	^{6.42} 35.90	^{0.22} 0.52

	W.			E.				
2+80 - in Grav.	36.62		3' B. - Cross.	$\begin{matrix} 7.03 \\ 36.62 \end{matrix}$	37.03	$\begin{matrix} 7.03 \\ 36.32 \end{matrix}$	$\begin{matrix} C 0.41 \\ \cancel{E 0.71} \end{matrix}$	
3+20 - 2' B.	37.37	$\begin{matrix} 37 \\ 37.05 \end{matrix}$	C 0.32	2' B.	$\begin{matrix} 37.05 \\ 6.94 \end{matrix}$	36.98	$\begin{matrix} .98 \\ 36.75 \end{matrix}$	$\begin{matrix} F 0.07 \\ \cancel{C 0.23} \end{matrix}$
+60 - 2' B.	37.62	$\begin{matrix} 62 \\ 37.47 \end{matrix}$	C 0.15	2' B.	$\begin{matrix} 37.47 \\ 7.45 \end{matrix}$	37.45	$\begin{matrix} 45 \\ 37.17 \end{matrix}$	$\begin{matrix} F 0.02 \\ \cancel{E 0.28} \end{matrix}$
4+00 - 3' B.	38.40	$\begin{matrix} 8.40 \\ 37.90 \end{matrix}$	C 0.50	2' B.	$\begin{matrix} 8.05 \\ 37.90 \end{matrix}$	38.05	$\begin{matrix} 8.05 \\ 37.60 \end{matrix}$	$\begin{matrix} C 0.15 \\ \cancel{E 0.45} \end{matrix}$
+40 - 1' B.	38.59	$\begin{matrix} .59 \\ 38.32 \end{matrix}$	C 0.27	N. 0.20' B.	$\begin{matrix} 38.58 \\ 38.32 \end{matrix}$	38.58	$\begin{matrix} .58 \\ 38.02 \end{matrix}$	$\begin{matrix} C 0.26 \\ \cancel{E 0.56} \end{matrix}$
+80 - N. - 10' B.	40.19	$\begin{matrix} 40.19 \\ 38.75 \end{matrix}$	C 1.44	2' B.	$\begin{matrix} 38.70 \\ 8.67 \end{matrix}$	38.67	$\begin{matrix} 8.67 \\ 38.45 \end{matrix}$	$\begin{matrix} F 0.03 \\ \cancel{C 0.22} \end{matrix}$
5+20 - 1' B = N.	40.53	$\begin{matrix} 0.53 \\ 39.17 \end{matrix}$	C 1.36	2' B.	$\begin{matrix} 39.17 \\ 6 \end{matrix}$	39.16	$\begin{matrix} 9.16 \\ 38.87 \end{matrix}$	$\begin{matrix} F 0.01 \\ \cancel{E 0.29} \end{matrix}$
+40 - N. - 027' B.	40.75	$\begin{matrix} 0.75 \\ 39.24 \end{matrix}$	C 1.51	2' B.	$\begin{matrix} 39.25 \\ 7.03 \end{matrix}$	39.03	$\begin{matrix} 9.03 \\ 38.96 \end{matrix}$	$\begin{matrix} F 0.22 \\ \cancel{C 0.07} \end{matrix}$
+60 - N. - 031' B.	40.52	$\begin{matrix} 40.52 \\ 39.00 \end{matrix}$	C 1.52	2' B.	$\begin{matrix} 39.05 \\ 8.89 \end{matrix}$	38.89	$\begin{matrix} .89 \\ 38.82 \end{matrix}$	$\begin{matrix} F 0.46 \\ \cancel{C 0.07} \end{matrix}$
5+80 - 2' B.	39.36	$\begin{matrix} 9.36 \\ 38.47 \end{matrix}$	C 0.89	2' B.	$\begin{matrix} 86 \\ 38.57 \end{matrix}$	38.86	$\begin{matrix} .86 \\ 38.44 \end{matrix}$	$\begin{matrix} C 0.29 \\ \cancel{C 0.12} \end{matrix}$
6+0019 = S.L. Monroe	37.73	37.64				37.86	37.82	

Grades on Dwight St Alley - 99 + 77 = (Blk)
 Plan 7064L to 7072L - 8-1-49 - 7.0.
 Block
 City Height

Alley - N. side = Blk. 77			
E' 2" Rad.	35.92	35.97	F 0.05
E' 2' B at NL.	36.27	36.07 ²⁷	C 0.20
W. 2' Rad.	35.92	35.82 ⁸²	C 0.07
W. 2' B. at NL.	37.27	35.96 ⁷²⁷	C 1.31
Alley - S. Side = Blk. 99			
E. 2' Rad.	35.70	35.49 ⁷⁰	C 0.21
E - 2' B. at S.L.	36.15	35.69 ⁶¹⁵	C 0.46
W. 2' Rad.	35.54	35.39 ⁵⁴	C 0.15
W, 2' B. at S.L.	35.98	35.54 ⁹⁸	C 0.44

INDEXED
 W.K.
 AUG 17 1949

Alley 76 + 100			
Alley - N. side. Blk. 76			City Heights
E - 2' Rad.	38.78	38.67	C 0.11
E. 2' B. at NL.	39.46	39.32	C 0.14
W. 2' B. at NL.	39.51	39.25 ⁵¹	C 0.26
W. 2' Rad.	38.87	38.53 ⁸⁷	C 0.34
Alley. Blk 100 = S. side			
E. 2' Rad.	38.19	38.27 ¹⁹	F 0.08
E - 2' B. - S.L.	38.96	38.42 ⁹⁶	C 0.54
W. 2' B. - S.L.	38.41	38.28 ⁴¹	C 0.13
W - 2' Rad.	37.68	38.13 ^{7.68}	F 0.45

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 W.K.
 AUG 17 1949

Alley Blk

75 = N.

City Heights

E. Side

2' B. at N.L.

40.12

40.34

F 0.22

INDEXED

W.K.

2' Rad on E

AUG 17 1949

40.13

40.19

F 0.06

30' E = 3' B.

} rake

F 0.39

60 E = 3' B.

F 0.45

93.38 E = Meet

Myrtle St. Grades.

INDEXED

W.K.
AUG 17 1949

N. side Myrtle - W. of Marlborough

W.L. = 0+00 = end Ret. 09.88 209.90

+35 11.04 11.22₀₄ F 0.18

+70 ✓ 11.87 12.54_{11.97} F 0.67

+105 13.82 13.86₃₂ F 0.04

+40 = 2' Rad. E.L. Alley 14.69 15.18_{4.69} F 0.49

2' B. on E. side at N.L. 16.35 15.33 C 1.02

310105 = N.W. Marl. + Myrtle

29

N. Side Myrtle - E. of Marlborough

0+00 = E.L. = Ret 09.98 09.90

+35 11.19 11.28₁₉ F 0.09

+70 12.18 12.66₁₈ F 0.48

+105 13.66 14.04_{3.66} F 0.38

+40 = 2' Rad. 14.73 15.41_{4.73} F 0.68

2' B. at N.L. 15.22 15.56₂₂ F 0.34

S. Side Myrtle - Marl. - E.

0+00 = E.L. = Ret 09.50 09.50

+10 = Brk. 09.76 09.76₇₆ C 0.05

S. side Myrt. Cont.

30

0+20	10.12	10.05 ¹²	C 0.07	2+65	19.10	19.29	F 0.19
+35	10.65	10.65	C 0.03	= Ret. 2+00 = W.L. 42 nd		20.60	
+70	11.91	11.94 ₉₁	F 0.03	Alley 99 = N. side - Bet. 42 nd & Van Dyke			
				2' Rad - W.	23.87	23.70 ⁸⁷	C 0.17
1+05	12.94	13.26 ₂₉₄	F 0.32				
				2' B. at N.L.	26.07	23.85 ^{6.07}	C 2.22
+40 = 2' Rad.	14.72	14.58 ⁷²	C 0.14				
= W.				2' B. at N.L. = E.	27.37	24.15 ^{7.37}	C 3.22
2' B. at S.L.	15.22	14.73 ^{5.22}	C 0.49				
= E.				2' Rad - E.	24.10	24.00 ¹⁰	C 0.10
2' B. at S.L.	17.13	15.48 ^{7.13}	C 1.65	Alley 105 - S. side			
				2' Rad. W.	22.84	22.93 ⁸⁴	F 0.09
= E. 1+60 = 2' Rad. = Top Hyd.	17.63	15.33 ^{7.63}	C 2.30				
				2' B. at S.L.	23.84	23.08 ⁸⁴	C 0.76
+95	16.45	16.65 ₄₅	F 0.20				
				2' B. at S.L. = E.	24.26	23.41 ^{4.26}	C 0.85
2+30	17.95	17.97 ₉₅	F 0.02				
				2' Rad. - E.	23.07	23.26 ₀₇	F 0.19

PC - N.	19.84	19.40 ⁸⁴	C 0.44
N.W. Ret Myrtle + 43 rd			
Meet on Both sides	± Ret. 19.96	19.40 ⁹⁶	C 0.56
W.L. 43 rd	19.85	19.80 ⁸⁵	C 0.05
S. side Myrtle - 43 rd to E.			
S. end of Ret. - S.L.	18.90	18.60 ⁹⁰	C 0.30
PC.			
± Ret.	19.39	18.80 ³⁹	C 0.59
PC.			
E.L. 43 rd	19.77	19.00 ⁷⁷	C 0.77
+ 40	20.91	20.72 ⁹¹	C 0.19
+ 80	22.29	23.45 ²⁹	F 1.16
= 2' Rad.			
1 + 24.48 = W. Side of Alley	24.28	24.37 ²⁸	F 0.09

2' B. at S.L. on W.	24.54	24.52 ⁵⁴	C 0.02
Alley. 101 on N.			
Middle stake -			
2' Rad. on W.	25.04	25.20 ⁰⁴	F 0.16
2' B. at N.L.	24.53	25.35 ⁵³	F 0.82
Nail in Conc.			
2' B. at N.L. on E.	24.65	26.28 ⁶⁵	F 1.63
2' Rad. on E	25.92	26.13 ⁹²	F 0.21

Sewer Grades - La Jolla Shores

1381-1384-D - Book 1857

5-10-49 - 7.0.

W.O. 31339

Camino Del Oro

INDEXED

W. K.

AUG 17 1949

$\pi = 8.10$

± Vallejos

M.H. 6 = 0+00

- 7.63

2+75' 5.55 2.09 - 6.33 8.42

3~ 5.42 2.22 6.25 8.47

+25' - 12' Lt. 7.55 +25' 5.52 2.12 6.18 8.30

+50 5.57 2.53 7.47 10.00 +50 5.56 2.08 6.10 8.18

+75 5.70 2.40 7.40 9.80 +75 5.63 2.01 6.03 8.04

1~ 5.63 2.47 7.32 9.79 4~ 5.74 1.90 5.95 7.85

+25' 5.44 2.66 7.25 9.91 - M.H. 8 +32.18 = To S. 5.68 1.96 5.86 7.82

± Calle Frescota

0+00? To N. 5.70 7.66

+50 = M.H. 7 - To U.

5.37 2.73 7.16 9.89

0+00

To E.

6.75 9.48 +25' 5.15 2.49 5.52 8.01

+25 5.47 2.63 7.08 9.71 +50 5.38 2.26 5.34 7.60

+50 5.63 2.47 7.00 9.47 +75 5.72 1.92 5.17 7.09

+75 5.67 2.43 6.93 9.36 1~ 5.75 1.89 4.99 6.88

1~ 5.66 2.44 6.85 9.29 +25 5.68 1.96 4.82 6.78

+25 5.76 2.34 6.78 9.12 +50 5.79 1.85 4.64 6.49

+50 5.76 2.34 6.70 9.04 +85 = D.E. 5.86 1.78 - 4.40 6.18

+75 5.77 2.33 6.63 8.96

$\pi = 7.64$

2~ 5.46 2.18 6.55 8.73

+25 5.53 2.11 6.48 8.59

+50 5.66 1.98 - 6.40 8.38

In Alley - E. of MH. 7

INDEXED

W.K.

AUG 17 1949

8.10

F.L.

cut

0+00 = MH. 7-

+25 - 10' Lt.

+50

+75

1~

+25

+53.14 = MH. 41

0+00

+25

+50

+75

1~

+25

+50

+75

2~ - D.E.

4.58 3.52 6.25 9.77

3.58 4.55 5.75 10.30

4.63 3.47 5.25 8.72

4.64 3.46 4.75 8.21

4.66 3.44 4.25 7.69

4.72 3.39 3.69 7.07

4.70 3.40 3.51 6.91

4.39 3.71 3.34 7.05

4.66 3.44 3.16 6.60

4.56 3.54 2.99 6.53

4.16 3.94 2.81 6.75

4.08 4.02 2.64 6.66

3.37 4.73 2.46 7.19

2.86 5.24 2.29 7.53

Vallecitos - Camino Del Oro - W. to Comfort Sta.

INDEXED

W.K.

AUG 17 1949

41

To N.

7.63

C 10.51

0+00 = M.H. 6

+20 - 12 Lt.

+45

+70

+95

1+20

+45

+70

+95

2+20

+45 = D.E.

- 7.20 10.08

6.82 9.54

6.45 8.64

6.07 8.22

5.70 7.87

5.32 7.45

4.95 7.00

4.57 6.52

4.20 6.27

3.82 6.08

3.52 5.78

M.H. 5 on De La Playa To M.H. 53 in
La Jolla Shores Hotel.

42

		F.L.	cut			
M.H. 5 - 12' + 14' Lt	To E.	1.35	- 9.09	10.44		
0 + 00 =	To W.	1.35	- 8.25	9.60	0 + 75	1.46 - 5.70 7.16
+ 25' - 12' Lt		1.30	8.01	9.31	1 ~	1.45 5.60 7.05
+ 50		1.42	7.76	9.18	+ 25	1.38 5.50 6.88
+ 75' - 14' N. = fence		1.10	7.51	8.61	+ 50	1.40 5.40 6.80
M.H. 42 12' + 24' Rt	To E.	0.83	- 7.20	8.03	+ 75	1.37 5.30 6.67
1 + 05.09 =	To S.	0.83	6.97	7.80	2 ~	1.30 5.20 6.50
+ 25' - 12' Lt		1.07	6.87	7.94	+ 25'	1.27 5.10 6.37
+ 50		1.03	6.77	7.80	M.H. 53 - 12' Lt.	
+ 75'		1.11	6.67	7.78	+ 50 =	1.23 - 5.00 6.23
1 ~		1.30	6.57	7.87		
+ 25'		1.30	6.47	7.77		
+ 50		1.36	6.37	7.73		
+ 75'		1.60	6.27	7.87		
2 ~		1.79	6.17	7.96		
+ 25'		1.77	6.07	7.84		
M.H. 52 + 42 =		1.63	- 6.00	7.63		
0 + 00						
+ 25		1.56	5.90	7.46		
+ 50		1.50	- 5.80	7.30		

INDEXED
W.K.
AUG 17 1949

De La Playa - M.H. 4 to 5

INDEXED

WK

AUG 17 1949 F.L.

cut

M.H. 4 12+24			
0+00 = 6.5' N. = fence	2.89	-9.97	12.86
+25' - 12' lt.	2.76	-9.90	12.66
+50' = 9' N. = fence	2.51	-9.82	12.33
+75'	2.36	9.75	12.11
1 ~ - 9.8' N. = fence	2.54	9.67	12.21
+25'	2.62	9.60	12.22
+50'	1.84	9.52	11.36
+75'	1.85	9.45	11.30
2 ~ - 10.7' N. = fence	1.87	9.37	11.24
+25'	2.06	9.30	11.36
+45'	1.68	9.23	10.91
+70' ^{10.5' N. of stob} = chain fence	1.57	9.16	10.73
94.25'			
+93' 75' =	1.35	9.09	10.44
M.H. 5			

Calle Frescota - M.H. 8 to 9

INDEXED

WK

AUG 17 1949

43

M.H. 8			
0+00 =	1.96	-5.70	
+25' = Cross	2.81	-5.62	8.43
+50' "	2.94	5.54	8.48
+75' - stob.	2.15	5.47	7.62
1 ~ "	2.26	5.39	7.65
+25' "	2.37	5.32	7.69
+50' "	2.49	5.24	7.73
+75' "	2.59	5.17	7.76
2 ~ "	2.50	5.09	7.59
+25' Cross	3.47	5.02	8.49
+50' "	3.77	4.94	8.71
+75' - Tack	3.40	4.87	8.27
12 + 25' - on line			
+95' 25' = To W.	4.07	-4.81	8.88
M.H. 9			
To N. + S.		-4.60	8.67

Paseo Grande - North from M.H. 9
at Calle Frescota

S. from M.H. 9

S.E.F.H. 7.44

44

INDEXED

F.L. cut

F.L. cut

		INDEXED		F.L.	cut			F.L.	cut	
0+00 = M.H. 9		4.07	4.60	8.67		0+00 = M.H. 9		4.07	4.60	8.67
+25 - 12' Rt.		4.12	4.52	8.64		+25 - 12' Lt.		4.30	4.50	8.80
+50		4.19	4.45	8.64		+50		4.39	4.40	8.79
+75		4.16	4.27	8.53		+75		4.64	4.30	8.94
1 ~		4.04	4.30	8.34		1 ~		4.82	4.20	9.02
+25		3.64	4.22	7.86		+25		4.90	4.10	9.00
+50		3.32	4.15	7.47		+50		5.09	4.00	9.09
+75		3.17	4.07	7.24		+75		5.23	3.90	9.13
2 ~		3.08	4.00	7.08		2 ~		5.54	3.80	9.34
+25 12' Rt.		3.15	3.92	7.07		+25		5.75	3.70	9.45
+50 12' Lt.		3.05	3.85 2.11	5.96		+50		6.07	3.60	9.67
+75		2.82	3.77 2.23	6.00		+75		6.32	3.50	9.82
3 ~		2.67	3.70 2.15	5.85		^{12' + 25' = cross} 2+07.80 =		6.47	3.37	9.84
+25		2.60	3.62 2.00	5.62		M.H. 10 = 0+00				
+50 = M.H. 26		2.51	3.55 2.02	5.57		+25		6.62	3.27	9.89
						+50		6.78	3.17	9.95
						+75		6.87	3.07	9.94
						1 ~		6.81	2.97	9.78
						+25		6.70	2.87	9.57

1+50	6.57-2.77	9.34	M.H. 26 = 0+00	2.02 - 3.58	-	5.57
+75	6.53 2.67	9.20				
2~	6.47 2.57	9.04	+25 - 12' Rt	2.36	3.47 2.05	5.52
+25	6.41 2.47	8.88	+50 12' Lt	2.27	3.39 2.18	5.57
+50	6.41 2.37	8.78	+75	2.35	3.32 2.21	5.53
+75	6.12 2.27	8.39	1~	2.31	3.24 2.11	5.35
3+00 = To N.	6.11 2.17	8.28	+25	2.29	3.17 2.04	5.21
M.H. 11 To E.	1.95	8.06				
0+00 = to S.	2.00	8.11	+50	2.10	3.09 1.88	4.97
+25	6.21 1.82	8.03	+75	2.03	3.02 2.00	5.02
+50	6.13 1.64	7.77	2~	1.77	2.94 2.25	5.19
+75	6.00 1.47	7.47	+25	2.00	2.87 1.91	4.78
1~	5.97 1.29	7.26	+50	2.10	2.79 2.09	4.88
+25	5.92 1.12	7.04	+75	1.92	2.72 2.02	4.74
+50	5.92 0.94	6.86	3~	1.96	2.64 1.94	4.58
+75	5.75 0.77	6.52	+25	2.12	2.57 1.89	4.46
2~	5.80 0.59	6.39	+45.70 = N+S	2.19	2.51 1.90	4.41
+25	5.68 0.42	6.10	M.H. 27 = 0+00 To E		2.40	4.30
+50	5.61 0.24	5.85	+25	2.26	2.43 1.96	4.39
+65 =	5.55 0.14	5.69	+50	2.34	2.36 1.84	4.20
M.H. 39 = end.			+75	2.28	2.28 1.85	4.13

Top F.H. opp 1+00 = 5.51

28 R.P. to MH. 28 =

7.93

INDEXED

W/K

AUG 17 1949

1 +00	2.52	2.21	1.95	4.16
+25	2.66	2.13	1.99	4.12
+50	2.73	2.06	2.10	4.16
+75	2.99	1.98	2.31	4.29
2 ~	3.23	1.91	2.57	4.48
+25	3.46	1.83	2.76	4.59
+50	3.63	1.76	3.30	5.06
+75	3.92	1.68	3.30	4.98
3 ~	4.27	1.61	3.50	5.11
+25	4.74	1.53	3.93	5.46
+50	5.31	1.46	4.49	5.95
+75	5.92	1.38	5.05	6.43
4 ~	6.75	1.31	6.02	7.33
+17.03 = To S.	7.24	1.26	6.47	7.73
M.H. 28 = 0+00 To N.		1.00		7.47

MH. 5 to 6 in Del Oro

46

INDEXED

W/K

AUG 17 1949

of Del Oro

Note = Moved 2.64 S. along +

0+00 = MH. 5 = nail	1.35	8.90	10.25
+25 - 12' Rt.	1.30	8.83	10.13
+50	1.14	8.75	9.89
+75	1.12	8.68	9.80
1 ~	1.18	8.60	9.78
+25	1.22	8.53	9.75
+50	1.46	8.45	9.91
+75	1.48	8.38	9.86
2 ~	1.47	8.30	9.77
+25	1.67	8.23	9.90
+50	1.79	8.15	9.94
+75	1.97	8.08	10.05
3 ~	2.19	8.00	10.19
+25	2.26	7.93	10.19
+50	2.22	7.85	10.07
+75	2.25	7.78	10.03
4 ~	2.27	7.70	9.97
+24.88 =	2.85	7.63	10.48

M.H. 6

Paseo Grande - M.H. 28 to End.

47

				+75' - 12' Lt.	22.40	10.23	12.17
0+00 = M.H. 28		- 1.00		2 ~	23.22	10.36	12.86
+25' - 12' Lt.	7.52	- 0.08	7.60	+25'	24.13	10.48	13.65
+50	8.47	+ 0.86	7.62	+50	24.94	10.61	14.33
+75'	9.31	1.77	7.54	+75'	25.79	10.74	15.05
1 ~	10.08	2.70	7.38	2 + 91.07 = M.H. 30	26.21	10.82	15.39
+25'	10.99	3.62	7.37	⁰⁺⁰⁰ 12.08' + 24' RP. Lt.			
+50	11.84	4.55	7.29	+25'	26.81	10.94	15.87
+75'	12.69	5.47	7.22	+50	27.33	11.07	16.26
2 ~	13.58	6.40	7.18	+75'	27.99	11.19	16.80
+25'	14.46	7.32	7.14	1 ~	28.56	11.32	17.24
+50	15.31	8.25	7.06	+25'	29.12	11.44	17.68
+80 = M.H. 29	16.36	9.36	7.00	+50	29.65	11.57	18.08
⁰⁺⁰⁰ - 12' Lt.				12' Lt. = Back Tang. To S.			
				+61.96 = M.H. 31	29.96	11.63	18.33
				⁰⁺⁰⁰ 12' Lt. ahead.			
+25'	17.22	9.48	7.74	on Colorado To E.	30.47	22.80	7.67
+50	18.07	9.61	8.46	+25'	31.40	23.80	7.60
+75'	18.99	9.73	9.26	+50	32.16	24.80	7.36
1 ~	19.79	9.86	9.93	+75'	33.10	25.80	7.30
+25'	20.66	9.98	10.68	1 ~	34.08	26.80	7.28
+50	21.59	10.11	11.48	+25'	35.02	27.80	7.22

1+50	35.91	28.80	7.11	3+00	11.86	3.60	8.26
+75	36.90	29.80	7.10	+17.75 = M.H. 32	-12.93	3.96	9.97
2~	37.93	30.80	7.13	= 12' W. = 12' E.	12' W. → 12.25		8.29
+20 = D.E.	38.64	31.60	7.04	N. on Ocaso - from M.H. 32			
				12' W = 12.25			8.05
Camino Del Oro - M.H. 27 to 32				0+00 = M.H. 32 = 12' E. → 12.93	4.20		8.73
				= 12' W.			
				+25 - 12' Lt. = Nad	12.54	4.77	7.77
0+00 = M.H. 27	- 2.40			+50	12.99	5.35	7.64
+25	2.35	1.90	4.25	+75	13.38	5.92	7.46
+50	2.53	1.40	3.93	1~	13.66	6.50	7.16
+75	2.66	0.90	3.56	+25	14.26	7.09	7.17
1~	3.11	0.40	3.51	+50	14.65	7.65	7.00
+25	3.04	0.10	2.94	+75	14.92	8.22	6.70
+50	4.07	0.60	3.47	2~	15.50	8.80	6.90
+75	5.18	1.10	4.08	+25	15.91	9.37	6.54
2~	6.41	1.60	4.81	+50	16.36	9.95	6.41
+25	7.90	2.10	5.80	+75	16.87	10.52	6.25
+50	9.19	2.60	6.59	3+00	17.54	11.10	6.44
+75	10.45	3.10	7.35	+21 = M.H. 33	18.09	11.58	6.51

INDEXED

W.K.

AUG 17 1949

0100 = MH. 33

18.09 11.58 6.51

+25 18.75 12.15 6.60

+50 19.42 12.73 6.69

+75 19.94 13.30 6.64

1~ 20.60 13.88 6.72

+25 21.31 14.45 6.86

+50 21.98 15.03 6.95

+75 22.63 15.60 7.03

2~ 23.28 16.18 7.10

+25 23.90 16.75 7.15

+50 24.55 17.33 7.22

+75 24.99 17.90 7.09

3~ 25.55 18.48 7.07

12.4

+21.29 = MH. 34 25.89 18.97 6.92

0100

+25 26.12 19.34 6.78

+50 28.97 19.72 6.25

+85 = Plug. 28.95 20.25 5.70

S. on Ocaso - from MH. 32 = Del-Ovo

INDEXED

W.K.

AUG 17 1949

0100 = MH. 32 - 12' E 4.20

+25 12.78 4.35 8.73

+50 12.96 4.50 8.46

+75 13.06 4.65 8.41

1~ 13.12 4.80 8.32

+25 13.27 4.95 8.32

+50 13.36 5.10 8.26

+75 13.45 5.25 8.20

2~ 13.54 5.40 8.14

+25 13.63 5.55 8.08

+50 13.72 5.70 8.02

+75 13.81 5.85 7.96

3~ 13.90 6.00 7.90

+35 = MH. 35 14.02 6.21 7.81

0100

+25 14.16 6.36 7.80

+50 14.25 6.51 7.74

+75 14.38 6.66 7.72

1~ 14.45 6.81 7.64

+25 14.52 6.96 7.60

49

1+50	14.62	7.11	7.51
+75	14.76	7.26	7.50
2-	14.82	7.41	7.41
+25	14.96	7.56	7.40
+50	15.02	7.71	7.31
+75	15.14	7.86	7.28
3+10 = MH. 26	15.52	8.07	7.45

N. on La Jolla Shores Dr. from M.H. 13

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INDEXED
W.K.
AUG 17 1949

0+00 = M.H. 13 - 10' Lt.	11.25	3.00	8.25	1+50	18.70	12.34	6.36
+25 10' Lt.	11.27	3.50	7.77	+75'	19.53	12.84	6.69
+50	11.56	4.00	7.56	2~	19.99	13.34	6.65
+75'	11.76	4.50	7.26	+25'	20.47	13.84	6.63
1~	12.04	5.00	7.04	+50	21.02	14.34	6.68
+25'	12.25	5.50	6.75	+75'	21.47	14.84	6.63
+50	12.30	6.00	6.30	3~	22.14	15.34	6.80
+75'	12.52	6.50	6.02	+17 = M.H. 21	22.94	15.68	6.26 7.26
2~	12.96	7.00	5.96	-0+00			
+25'	13.42	7.50	5.92	+25' 10' Lt.	23.01	15.84	7.17
+50	13.80	8.00	5.80	+50	23.13	16.00	7.13
+75'	14.27	8.50	5.77	+75'	23.33	16.16	7.17
3~	14.77	9.00	5.77	1~	23.51	16.33	7.18
+17.13 = M.H. 20	15.03	9.34	5.69	+25'	23.77	16.49	7.28
-0+00				+50	24.23	16.65	7.58
+25'	15.75	9.84	5.91	+75'	24.36	16.81	7.55
+50	16.25	10.34	5.91	2~	24.62	16.98	7.64
+75'	16.94	10.84	6.10	+25'	24.70	17.14	7.56
1~	17.69	11.34	6.35	+50	24.91	17.30	7.61
+25'	18.23	11.84	6.39	+75'	25.12	17.46	7.66

3+00	25.41	17.63	7.78	+75	26.74	20.53	6.21
+25	25.57	17.79	7.78	1~	27.08	20.70	6.38
+41.06 = M.H. 22 = 0+00	25.68	17.90	7.78	+25	26.92	20.86	6.06
				+50	27.67	21.02	6.65
+25	25.79	18.06	7.73	+75	27.97	21.18	6.79
+50	26.08	18.22	7.86	2~	28.27	21.35	6.92
+75	26.27	18.38	7.89	+25	28.62	21.51	7.11
1~	26.48	18.55	7.93	+50	28.72	21.67	7.05
+25	26.64	18.71	7.93	+75	29.34	21.84	7.50
+50	26.74	18.87	7.87	+90 = M.H. 24 To S	29.58	21.94	7.64
+75	26.94	19.03	7.91	+0+00 To N.		22.10	7.48
2~	26.97	19.20	7.77	+25	30.01	22.80	7.21
+25	26.97	19.36	7.61	+50	30.40	23.50	6.90
+50	27.07	19.52	7.55	+75	31.08	24.20	6.88
+75	27.08	19.68	7.40	1~	31.90	24.90	7.00
2~	27.00	19.85	7.15	+25	32.52	25.60	6.92
10' S. of E Del Oro +30 = M.H. 23 = 0+00	27.13	20.05	7.08	+50	33.18	26.30	6.88
				+75	34.17	27.00	7.17
+25	26.87	20.21	6.66	2~	34.89	27.70	7.19
+50	26.51	20.37	6.14	+25	35.77	28.40	7.37

2+50	36.94	29.10	7.84	0+00 = M.H. 12 = n' S.F.	9.05	0.70	8.35
+75	37.60	29.80	7.80	+25' - 12' Lt.	9.12	1.12	8.00
3~	38.41	30.50	7.91	+50	9.50	1.55	7.95
+25	39.06	31.20	7.86	+75	9.81	1.97	7.84
+52 = M.H. 25	39.90	31.96	7.94	1~	10.25	2.40	7.85
+25	40.51	32.21	8.30	+25'	10.62	2.82	7.80
+50	40.98	32.46	8.52	+50	10.93	3.25	7.68
+75	41.30	32.71	8.59	+75'	11.30	3.67	7.63
1~	41.53	32.96	8.57	2~	11.73	4.10	7.63
+25 = Plug.	41.73	33.21	8.52	+25'	12.06	4.52	7.54
				+50	12.43	4.95	7.48
				+75	12.85	5.37	7.48
				3~	13.21	5.80	7.41
				+25'	13.55	6.22	7.33
				+50	13.81	6.65	7.16
				+75	14.03	7.07	6.96
				4~ = M.H. 37	14.22	7.50	6.72
				+25	14.41	7.67	6.74
				+50	14.52	7.85	6.67
				+75' 12' Lt.	14.73	8.02	6.71

1~	12' Lt.	14.86	8.20	6.66				
+25'		14.95	8.37	6.58	0+25'	10.24	3.30	6.94
+50'		15.11	8.55	6.56	+50'	10.31	3.50	6.81
+75'		15.28	8.72	6.56	+75'	10.36	3.70	6.66
2+00 = Plug. = 12' Lt.		15.33	8.90	6.43	1+10 = Plug. = 12' Lt.	10.51	3.98	6.53

S. on Ocaso - from M.H. 12

0+00 = M.H. 12 = 12' Lt. ^{on Diag. = SE.} +20' RP	9.05	0.70	8.35
+25' - 12' Lt.	8.90	0.90	8.00
+50'	9.08	1.10	7.98
+75'	9.16	1.30	7.86
1~	9.21	1.50	7.71
+25'	9.41	1.70	7.71
+50'	9.47	1.90	7.57
+75'	9.61	2.10	7.51
2~	9.69	2.30	7.39
+25'	9.40	1.50	7.30
+50'	9.96	2.70	7.26
+75'	10.08	2.90	7.18
3+00 = M.H. 38 12' Lt.	10.13	3.10	7.03

Vallecitos - M.H. 11 to 13

0+00 = M.H. 11	6.29	-1.95	8.24
+25' - 10' Lt.	6.19	-1.75	7.94
+50'	6.29	1.55	7.84
+75'	7.50	1.35	8.85
1~	7.50	1.15	8.71
+25'	7.85	0.95	8.80
+50'	8.12	0.75	8.87
+75'	8.36	0.55	8.91
2~	8.65	-0.35	9.00
+25'	8.77	-0.15	8.92
+50'	8.23	+0.05	8.18
+75'	8.48	+0.25	8.23

Paseo Del Ocaso - S. of La Playa.

INDEXED

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W.K.

AUG 17 1949

= 12' S.E. on Diag.				Exist.		
2+01.52 = M.H. 12 = 0+00	9.05	0.46	8.59	0+00 = M.H. in La Playa	11.72	7.20 4.52
+25' - 12' Lt	9.19	0.66	8.53	+25' - 10' Lt.	11.51	7.32 4.19
+50	9.30	0.86	8.44	+50	12.24	7.45 4.79
+75'	9.54	1.06	8.48	+75'	12.71	7.57 5.14
1 ~	9.70	1.26	8.44	1 ~	13.31	7.70 5.61
+25'	9.90	1.46	8.44	+25'	13.75	7.82 5.93
+50	10.12	1.66	8.46	+50	14.22	7.95 6.27
+75'	10.27	1.86	8.41	+75'	14.71	8.07 6.64
2 ~	10.39	2.06	8.33	2+10 = M.H. 48 = To N. = 0+00	15.45	8.25 7.20
+25'	11.37	2.26	9.11	To S.	15.45	8.45 7.00
+50	11.74	2.46	9.28	+25' - 10' Lt.	15.98	8.90 7.08
+75' - 1'	11.15	2.66	9.49	+50	16.60	9.35 7.25
+88 = M.H. 13 = To W. 12' Lt.	11.69	2.77	8.92	+75'	17.14	9.80 7.34
N. + S.	11.69	3.00	8.69	1 ~	17.72	10.25 7.47
				+25'	18.28	10.70 7.58
				+50	18.84	11.15 7.69
				+75'	19.44	11.60 7.84
				2 ~	19.87	12.05 7.82
				+25'	20.45	12.50 7.95

2+50	20.90	12.95	7.95			
- 10+20 E						
+74.31 = M.H. 49	21.69	13.39	8.30	+25' - 10' Lt.	26.25	18.17 8.08
+ 0+00 E Dorado				+50	26.55	18.42 8.13
+25' - 10' Lt.	21.45	13.69	7.76	+75'	26.86	18.67 8.19
+50	22.13	13.99	8.14	1+00	27.12	18.92 8.20
+75'	22.47	14.29	8.18	+25'	27.43	19.17 8.26
1~	22.75	14.59	8.16	+50	27.56	19.42 8.14
+25'	22.98	14.89	8.09	+75'	27.85	19.67 8.18
+50	23.26	15.19	8.07	10+20 +90 = Plug.	28.02	19.82 8.20
+75'	23.45	15.49	7.96			
10+20						
+87.64 = M.H. 50	23.51	15.64	7.87			
+ 0+00 B.M. on 20 Cross.	24.37					
+25' - 10' Lt.	23.95	15.94	8.01			
+50	24.30	16.24	8.06			
+75'	24.61	16.54	8.07			
1~	24.95	16.84	8.11			
+25'	25.20	17.14	8.06			
+50	25.44	17.44	8.00			
+75'	25.66	17.74	7.92			
- 10+20 E						
+89.90 = M.H. 51	25.82	17.92	7.90			
+ 0+00						

La Jolla Shores Dr. S. of La Playa

Nail in Pole By MH. 17

33.44

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INDEXED

W. K. 699
AUG 17 1929

To N								
0+00 = MH. 15' To S.	16.99	9.64	7.35	+25	28.20	19.24	8.96	
+25'	17.42	10.27	7.15	+50	29.14	19.77	9.37	
+50'	17.73	10.80	6.93	+75'	29.77	20.29	9.48	
+75'	18.00	11.32	6.68	2~	30.18	20.82	9.36	
1~	18.36	11.85	6.51	+25	30.58	21.34	9.24	
+25'	19.13	12.37	6.76	+50	30.81	21.87	8.94	
+50'	19.78	12.90	6.88	+75'	30.97	22.39	8.58	
+75'	20.38	13.42	6.96	3~	31.34	22.92	8.42	
2~	20.93	13.95	6.98	0+16.5' Lt.				
+25'	21.53	14.47	7.06	+27~ MH. 17	32.08	23.48	8.60	
+50'	22.46	15.00	7.46	0+00				
+75'	23.07	15.52	7.55	+25'	32.47	23.80	8.67	
3~	23.86	16.05	7.81	+50	33.02	24.13	8.89	
+27 = MH. 16	24.55	16.62	7.93	+75'	33.58	24.45	9.13	
0+00				1~	34.02	24.78	9.24	
				10+20' RP.				
				+33.67 = Aug.	34.60	25.22	9.38	
				0+00				
+75'	25.33	17.14	8.19	+25'	34.94	25.54	9.40	
+50'	25.95	17.67	8.28	+50	35.15	25.87	9.28	
+75'	26.65	18.19	8.46	+75'	35.37	26.19	9.18	
1~	27.23	18.72	8.51	1~	35.63	26.52	9.11	

10 + 33 RP. = To N.			
1 + 29.40 = M.H. 18 = 0+00	36.29	26.90	9.39
To S	36.29	27.00	9.29
+25'	36.75	27.60	9.15
+50	37.16	28.20	8.96
+75'	37.84	28.80	9.04
1 ~	38.46	29.40	9.06
+25'	39.04	30.00	9.04
+50	39.70	30.60	9.10
+75'	40.53	31.20	9.33
2 ~	41.31	31.80	9.51
10 + 37 RP. + 17.59 = M.H. 19 = 0+00	42.02	32.22	9.80
+25'	42.64	32.97	9.67
+50	43.25	33.72	9.53
+75'	43.76	34.47	9.29
1 ~	44.47	35.22	9.25
+25'	44.95	35.97	8.98
+50	45.65	36.72	8.93
+75'	46.37	37.47	8.90
2 ~	47.41	38.22	9.19
10 + 41 RP. + 32 = Plug	48.66	39.18	9.48

M.H. 10 Lt. 0+00 = Exist.	6.40	1.90	4.50
+25'	5.96	2.00	3.96
+50	6.28	2.10	4.18
+75'	6.60	2.20	4.40
1 ~	6.91	2.30	4.61
+25'	7.19	2.40	4.79
+50	7.51	2.50	5.01
+75'	7.86	2.60	5.26
2 ~	8.21	2.70	5.51
15 + 30 RP. To N. + 13.26 = M.H. 46 = 0+00	8.58	2.75	5.83
To S	8.58	2.85	5.73
+25'	8.81	3.10	5.71
+50	9.22	3.35	5.87
+75'	9.63	3.60	6.03
1 ~	10.00	3.85	6.15
+25'	10.32	4.10	6.22
+50	10.63	4.35	6.28
+75'	11.01	4.60	6.41

2 ~ 11.38 4.85 6.53

+25' 11.78 5.10 6.68

+50 12.04 5.35 6.69

+75' 12.00 5.60 7.40

3 ~ 12.96 5.85 7.11

+25 13.12 6.10 7.02

+51.74 = M.H. 47 ^{10+20 RP.} 13.23 6.37 6.86

+25 13.69 6.62 7.07

+50 13.93 6.87 7.06

+75 14.17 7.12 7.05

1 ~ 14.12 7.37 6.75

+25 13.70 7.62 6.08

+47 = Plug 13.32 7.84 5.48

0+00 = M.H. 46 8.58 2.85 5.73

+25 = 11' Lt. 8.99 3.60 5.39

+50 = 10' Lt. 9.62 4.35 5.27

+75 11.53 5.10 6.43

1 ~ 12.90 5.85 7.05

+25 13.47 6.60 6.87

+50 13.87 7.35 6.22

+85 = Plug. 14.33 8.40 5.93

De la Playa - Pump Sta to W.

						9.45 7	
						539.416	-10.59 14.75
30' S. Plug.	9.30	-13.34	22.64	+34.16 = M.H. 3	539.400	-10.49	14.55
To S.	8.57	-12.00	20.57	Exist. 8"		-0.38	
0+00 M.H. 1 To W. -10' RT.	8.57	-11.80	20.37				
+25'	8.03	11.72	19.75	0+00 = ^D M.H. 3 10' RT.		-10.49	✓
+50'	7.39	11.64	19.03	0+25	554.391	-10.41	14.32
+75'	6.80	11.57	18.37	0+50	569.376	-10.34	14.10
1~	5.91	11.49	17.40	0+75	581.364	-10.26	13.90
+25'	5.58	11.42	17.00	1+00	597.348	-10.19	13.67
+50'	5.40	11.34	16.74	1+25	6.08.337	-10.11	13.48
+75'	5.23	11.27	16.50	1+50	6.37.308	-10.04	13.12
10+20' R.P. 2+02.50 = M.H. 2	4.84	11.19	16.03	1+72.65 = ^D M.H. 4	663.282	-9.97	12.79
817	5.45	9.45	4.00	ONE No. 1	4440.98	Calle De la Playa (F81857 P-6)	
+25'	4.10	5.35	-11.11				
+50'	4.42	5.03	-11.04				
+75'	4.69	4.76	-10.96				
1~	5.33	4.12	-10.89				
+25'	5.28	4.17	-10.81				
+50'	5.24	4.21	-10.74				
+75'	5.19	4.26	-10.66				

2-10-50 Stake Jewer Alleys Blocks
 Hendricks 179, 180, 181 Mission Beach
 Johnson
 Greer
 Cats
 WO #2039

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INDEXED

MAY 22 1950

					Cats
2+96.58	4.69	0.08	-5.36		5.44
2+71.86	4.69	-0.42	-5.46		5.04
2+47.15	4.48	-0.21	-5.56		5.35
2+22.43	4.44	-0.17	-5.66		5.49
1+97.72	4.40	-0.13	-5.76		5.63
1+73	4.47	-0.20	-5.86		5.66
1+64 (13)	4.85	-0.58	-5.20		4.62
1+48.29	4.43	-0.16	-5.96		5.80
1+23.57	4.41	-0.14	-6.06		5.92
1+12 (12)	4.75	-0.48	-3.12		2.74
0+98.86	4.67	-0.40	-6.16		5.76
0+89 (11)	4.44	-0.17	-5.46		5.29
0+74.14	4.38	-0.11	-6.26		6.15
0+49.43	4.74	-0.47	-6.36		5.89
0+24.71	4.93	-0.66	-6.46		5.80
0+00 Ex MH Bayside Lane	5.66	-1.39	-6.56		5.17

BM 5.02 4.27

-0.75

L&D S.W.-E Line Mission Blvd
 Alley Block 176 M. Beach GB 261 P. 24

2-21-50 State Alleys Block 1758179

Hendricks

Mission Beach

Johnson

Greer

Cora

Dwg 6782-A

	H.1	-H.	Elev. State	Elev. Grade	Corr F	offset	-Rt.	Elev. State	Elev. Grade	Corr F	Dist.
no. 31330 BM			4.20	7.21	7.19						
015333 End			5.78	5.63	5.66	FO.03	1' BK	5.44	5.97	5.69	CO.28 7E
014733			4.87	6.54	5.72	CO.82	line	5.54	5.87	5.82	CO.05 2'
014133			3.84	7.57	5.98	C1.59	0.17 in alley	5.27	6.14	6.04	CO.10 1' BK
0120			3.52	7.89	6.80	C1.09	0.28 BK	4.59	6.82	6.83	FO.01 0.4'
0110			4.00	7.41	7.07	CO.34	1' BK	4.07	7.34	7.08	CO.26 0.4'
0100 N. Line Strandway			4.29	7.12	7.09	Ex. Pav.				7.09	
1480.72 E. Line Strandway			4.45	6.96	6.95	Ex. Pav.				6.96	
1173.85			4.58	6.83	6.48	CO.35	1' BK	4.42	6.99	6.48	CO.51 1'
1453.85			6.26	5.15	5.01	CO.14	1' BK	6.47	4.94	5.01	FO.07 0.5'
TP. 6.88 18.41			0.57	4.53							
1433.85			1.25	3.85	3.54	CO.31	1' BK	1.15	3.95	3.54	CO.41 2'
1113.85			2.33	2.77	2.24	CO.53	1' BK	2.56	2.54	2.24	CO.30 1'
0193.85			4.17	0.93	1.26	FO.33	2'	3.70	1.40	1.26	CO.14 2'
0173.85			4.35	0.75	0.63	CO.12	1'	4.29	0.81	0.63	CO.18 2'
0153.85			5.05	0.05	0.32	FO.27	2'	4.41	0.69	0.32	CO.37 0.95' in alley
0133.85			5.00	0.10	0.18	FO.08	2'	4.47	0.63	0.18	CO.45 0.2' alley
0113.85			5.25	-0.15	0.05	FO.20	2'	5.06	0.04	0.05	FO.01 0.13' in
0100 N. Line Mission Blvd			4.90	0.20	-0.04	CO.24	2'	4.77	0.33	-0.05	CO.38 1' BK

BM 5.85 5.10

-0.75

LB Disc. 5' West E. Line Mission Blvd. Alley B/C 176
Mission Beach (GB 261 P. 20)

3-1-50
Hendricks
Greer
Cota
WO# 31306

Stake Cbs Kalmia St.
Montclair to Vancouver
Dwg. 7723-L

Note
* - Restake

27855
963
193

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Sta.	+ H1	- Lt.	Elev.	Grade	Elev.	Stake	Grade	Cut & Fill	Sta.	- Rt.	Elev.	Stake	Grade	Cut & Fill
3+20.35	H Line Vancouver	* 4.73	267.20	267.20	267.20	FO.38	267.20	FO.38	3+20.46 PL	* 13.30	267.26	267.26	266.80	CO.46
3+15.29	BC	* 4.75	267.45	267.45	267.45	FO.42	267.45	FO.42	3+00	10.45	267.51	267.51	267.80	FO.29
3+10		* 4.44	267.75	267.75	267.75	FO.48	267.75	FO.48	3+80	9.52	268.44	268.44	268.92	FO.48
2+80		* 8.55	269.42	269.42	269.42	FO.48	269.42	FO.48	2+6361.8	8.66	269.30	269.30	269.84	FO.54
2+50		* 7.30	271.10	271.10	270.66	FO.44	270.66	FO.44	2+50	7.90	270.06	270.06	270.60	FO.54
2+30		* 6.87	272.11	272.11	271.66	FO.44	271.66	FO.44	2+30	7.30	270.66	270.66	271.61	FO.95
2+10		5.52	272.89	272.89	272.44	FO.45	272.44	FO.45	2+22 EC	6.51	271.45	271.45	271.94	FO.49
1+90		5.02	273.46	273.46	272.94	FO.52	272.94	FO.52	2+22 at PL	4.66	273.30	273.30	272.15	CI.15
1+72	EC Alley Rd	4.75	273.76	273.76	273.21	FO.55	273.21	FO.55	1+98 at PL	4.18	273.78	273.78	272.84	CO.94
1+72	at Prop Line	3.04	273.94	273.94	274.92	CO.98	274.92	CO.98	1+98 BC Alley	5.87	272.09	272.09	272.75	FO.66
1+48	at Prop Line	3.28	274.05	274.05	274.68	CO.63	274.68	CO.63	1+90	5.50	272.46	272.46	272.96	FO.50
1+48	BC Alley Rd	4.75	273.89	273.89	273.21	FO.68	273.21	FO.68	1+72	5.19	272.77	272.77	273.26	FO.49
1+30		4.76	273.79	273.79	273.20	FO.59	273.20	FO.59	1+48	5.17	272.79	272.79	273.38	FO.59
1+10		5.01	273.46	273.46	272.95	FO.51	272.95	FO.51	1+30	5.21	272.75	272.75	273.29	FO.54
0+90		5.79	272.89	272.89	272.19	FO.70	272.19	FO.70	1+10	5.50	272.46	272.46	272.90	FO.44
0+70		6.34	272.11	272.11	271.62	FO.49	271.62	FO.49	0+90	5.96	272.00	272.00	272.39	FO.39
0+50		7.04	271.40	271.40	270.92	FO.18	270.92	FO.18	0+70	6.67	271.29	271.29	271.61	FO.32
0+20		8.53	269.51	269.51	269.43	FO.08	269.43	FO.08	0+50 Sewer	5.41	272.52	272.52	265.20	CI.32
0+10		8.92	269.20	269.20	269.04	FO.16	269.04	FO.16	0+50	7.61	270.35	270.35	270.60	FO.23
0+00		8.87	269.00	269.00	269.09	EX CB	269.09	EX CB	0+20	* 8.08	* 270.47	* 270.47	270.60	FO.23
BM.	8.43	277.96		269.53		HERP	269.53	HERP	0+10	9.88	268.08	268.08	268.20	FO.12
BM.	9.02	* 278.55		* 269.53			* 269.53		0+00	10.16	267.80	267.80	267.80	EX CB

INDEXED
MAY 22 1950

277.96
Kalmia & Montclair

Johnson
Greer
Bunch
3-27-50
W.O. 31669

Stake Alley BIK 78 Pawun
29th to 30th Btwn
Imperial Ave. 5' 2" 54
Bank 5 Reed's Central Ad. *left*

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Right

INDEXED
MAY 22 1950

	T	HI.		Stake Elev	Grade Elev	Cut or Fill	Offset Left	Offset Rt.		Stake Elev	Grade Elev	Cut or Fill
3+00			5.18	73.09	72.74	CO ³⁵	2' BK	14 in	4.67	73.60	72.71	CO ²¹
2+80			3.96	74.31	72.88	CO ⁴³	2' BK	2' BK	5.39	72.88	72.84	CO ⁰⁴
2+60			5.24	73.03	73.02	CO ⁰¹	2' BK	2' BK	5.32	72.95	72.97	FO ⁰²
2+40			4.78	73.49	73.16	CO ³³	2' BK	2' BK	4.76	73.51	73.10	CO ⁴¹
2+20			4.46	73.81	73.30	CO ⁵¹	4' BK	2' BK	4.65	73.62	73.23	CO ³⁹
2+00			4.30	73.97	73.44	CO ⁵⁸	2' BK	4' BK	4.61	73.66	73.36	CO ³⁰
1+80			4.84	73.43	73.58	FO ¹⁵	5' BK	2' BK	3.76	74.57	73.49	CO ⁰⁸
1+60			4.42	73.85	73.57	CO ¹³	2' BK	2' BK	4.53	73.79	73.62	CO ¹²
TP	4.30	78.27	5.53	73.97								
1+40			5.49	74.01	73.86	CO ¹⁵	2' BK	Line	5.49	74.01	73.75	CO ²⁶
1+20			5.46	74.10	74.00	CO ¹⁰	2' BK	3' BK	4.87	74.63	73.88	CO ²⁵
1+00			5.16	74.34	74.14	CO ²⁰	2' BK	2' BK	5.18	74.32	74.01	CO ³¹
0+80			4.83	74.67	74.28	CO ³⁹	2' BK	2' BK	5.10	74.40	74.14	CO ²⁶
0+60			4.38	75.12	74.42	CO ⁷⁰	2' BK	2' BK	4.88	74.62	74.27	CO ³⁵
0+40			4.16	75.34	74.56	CO ⁷⁸	2' BK	6' BK	4.59	74.91	74.40	CO ⁵¹
0+20			4.06	75.44	74.70	CO ⁷⁴	2' BK	2' BK	4.67	74.83	74.53	CO ³⁰
0+00					74.84						74.66	
B.M.	7.95	79.50		72.05		S.W. Cor. 29th & Imperial Ave						

Left

Right 66

	T.	H.I.	-	Stake Elev.	Grade Elev.	Cut or Fill Co ⁶¹	offset Lt.	offset Rt.	-	Stake Elev.	Grade Elev.	Cut or Fill Co ⁶²
6+99.58			5.14	74.04	72.77	C1 ²⁷	.60 in	2' bK	5.78	73.40	72.77	Co ⁶³
T.P	6+23	79.18	4.99	72.95		Co ⁵⁸						Co ⁶²
6+24.58			3.84	73.60	72.43	C1 ¹⁷	.60 in	2' bK	4.56	72.88	72.43	Co ⁴⁵
						Co ³³						
6+04.58			4.15	73.29	72.13	C1 ¹⁶	.58 in	2' bK	4.91	72.53	72.13	Co ⁴⁰
5+89.58			4.75	72.69	71.88	Co ⁸¹	2' bK	2' bK	5.11	72.33	71.88	Co ⁴⁴
5+60.58			4.01	73.43	71.72	C1 ⁷¹	line	2' bK	4.67	72.77	71.72	C1 ⁰⁵
5+44.58			5.45	71.99	71.63	Co ³⁶	2' bK	5' bK	5.13	72.34	71.63	Co ⁷¹
						Co ⁴⁸						Co ²⁷
5+24.58			4.20	73.24	71.62	C1 ⁶²	0.20 bK	1' bK	4.90	72.54	71.62	Co ³²
5+04.58			5.56	71.88	71.66	Co ²²	2' bK	2' bK	4.76	72.68	71.66	C1 ²²
4+89.58			5.59	71.85	71.79	Co ¹¹	2' bK	2' bK	5.26	72.18	71.79	Co ⁴⁴
												Co ³⁴
4+69.58			5.71	71.73	71.83	FO ¹⁰	2' bK	2' bK	5.12	72.32	71.83	Co ²⁹
												Co ³²
4+44.58			4.42	73.02	71.92	C1 ¹⁰	.40 bK	1.7 in	4.66	72.78	71.92	Co ³⁶
												Co ⁴⁷
4+24.58			4.05	73.39	72.01	C1 ³⁸	.50 bK	1.6 in	2.31	75.13	72.01	Co ¹²
						FO ²⁶						
4+04.58			4.09	73.35	72.10	C1 ²⁵	.60 bK	2' bK	5.00	72.44	72.10	Co ³⁴
T.P	4.77	77.44	5.60	72.67								Co ²⁶
3+84.58			5.41	72.86	72.19	Co ⁶⁷	1' bK	1.35 in	5.82	72.45	72.19	Co ²⁶
												FO ⁴³
3+64.58 (Brk)			5.95	72.32	72.28	Co ⁰⁴	1' bK	1.7 in	4.92	73.35	72.28	C1 ²⁷
						Co ²⁶						
3+40			5.03	73.24	72.46	Co ⁷⁸	line	2' bK	5.73	72.54	72.45	Co ²⁹
3+20			5.27	73.00	72.60	Co ⁴⁰	2' bK	1' bK	5.30	72.83	72.58	Co ²⁵

78.27

78.27

Johnson
Greer
Bunch
3-27-50
W.O. 31669

Grades for 18" Drain
Alley BIK 78 &
Sewer Laterals

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INDEXED

MAY 22 1950

6+64, 58 = #2 Sewer Lateral to Lt.
T.P.

+	HI	-	Offset	Stake Elev	Grade Elev	Cut or Fill
		5.54	5'6L	73.64	68.16	C5.48
6.23	79.18	4.49		72.95		
	^					

5+64, 58 = #1 Sewer Lateral to Rt.

+	HI	-	Offset	Stake Elev	Grade Elev	Cut or Fill
		4.81	5'6L	72.63	68.56	C4.07
	77.44					

2+10, 30

2+00

1+60

1+20

T.P.

0+80

0+40

0+00 = Catch Basin = 5+26, 58 on E Alley

+	HI	-	Offset	Stake Elev	Grade Elev	Cut or Fill
		5.32	6'RT	73.86	64.01	C9.85
		4.99	6'RT	74.24	64.10	C10.14
		4.82	5.5'RT	74.36	64.52	C9.84
		5.82	8'RT	73.36	64.99	C8.42
6.23	79.18	4.49		72.95		
		4.77	8'RT	72.70	65.36	C7.34
		4.65	8'RT	72.79	65.78	C7.01
		4.77	7'RT	72.67	66.20	C6.47
		4.77		72.67	71.20	C1.47
					F.L. TOP Basin	
				77.44	See P. 66	
				^		

Johnson
Greer
Bunch
3-31-50

Grades for Storm Drain
Tompkins Street

W.O. 20620 -
F.B. 1763/74
Drawing 3919-B

Between Francis & 35th

INDEXED
MAY 22 1950

All stakes 10' offset to left

Check Flow line of existing drain
716 41.04
41.05

- Rods Elev Stake Elev Grade Cutz or Fill

1404 = End of proposed drain

12.06 36.15 35.60 C 0.55

0+78

4.98 43.23 36.96 C 6.27

0+52

4.03 44.18 38.32 C 5.86

0+26

1.00 47.21 39.68 C 7.53

0+00 = End of existing 30" pipe

7.16 41.05 41.09 0.00

48.21

T.P. 8.61 48.21 2.59 39.60

B.M. 13.62 42.19 2.19 29.57

= B.P. on rail of Bridge
Near 34th & Imperial

4-19-50 Stake Alleys Blocks 178, 179 & 180
 Hendricks
 Johnson
 Greer
 W# 31330

71

Sta	+	N-1	- Lt	Elev. State Lt	Elev. Grade Lt	Corf Lt	Offset	- Rt	Elev. State Lt	Elev. Grade Lt	Corf Rt	Offset	
0+82				4.95	-0.36	-0.24	FO ¹³	1°	4.74	-0.15	-0.24	CO ⁰⁹	2°
0+62				4.67	-0.08	-0.26	CO ¹⁸	1°	4.44	0.15	-0.26	CO ⁴¹	6°
0+36				4.53	0.06	-0.32	CO ³⁸	0°	4.69	-0.10	-0.32	CO ²²	0°
0+10				4.54	0.05	-0.39	CO ⁴⁴	Line	4.82	-0.23	-0.39	CO ¹⁶	0°
0+00	E Line Mission			5.46	-0.87	-0.56	(FO ³¹ Ex)		5.55	-0.96	-0.56	FO ⁴⁰	
T.P.	5.13	4.59	9.26	-0.54									
1+85+	West Line Mission			8.58	0.14	0.13	Ex Paving				0.14		
1+67				8.66	0.06	0.23	FO ¹⁷	0°	8.30	0.42	0.23	CO ¹⁹	0°
1+47				8.92	-0.20	0.34	FO ⁵⁴	2°	8.38	0.34	0.34	CO ⁰⁹	1°
1+27				7.93	0.79	0.45	CO ³⁴	0°	8.37	0.35	0.45	FO ¹⁰	2°
1+07				7.83	0.89	0.60	CO ²⁹	1°	7.82	0.90	0.60	CO ³⁰	1°
0+87				7.27	1.45	1.30	CO ¹⁵	1°	7.09	1.63	1.30	CO ³³	1°
0+67				5.65	3.07	2.50	CO ⁵⁷	1°	6.06	2.66	2.50	CO ¹⁶	2°
0+47				4.45	4.27	3.90	CO ³⁷	1°	4.40	4.32	3.90	CO ⁴²	1°
0+20				2.06	6.66	6.13	CO ⁵³	2°	2.77	5.95	6.13	FO ¹⁸	6°
0+00	E Line Strandway					7.80			0.98	7.74	7.80	Ex Pav.	
T.P.	1.21	8.72	4.63	7.51									
BM	4.95	12.14				7.19							

Brass Plug Sea Wall & Santa Clara St.

(Cont'd. from P-71)

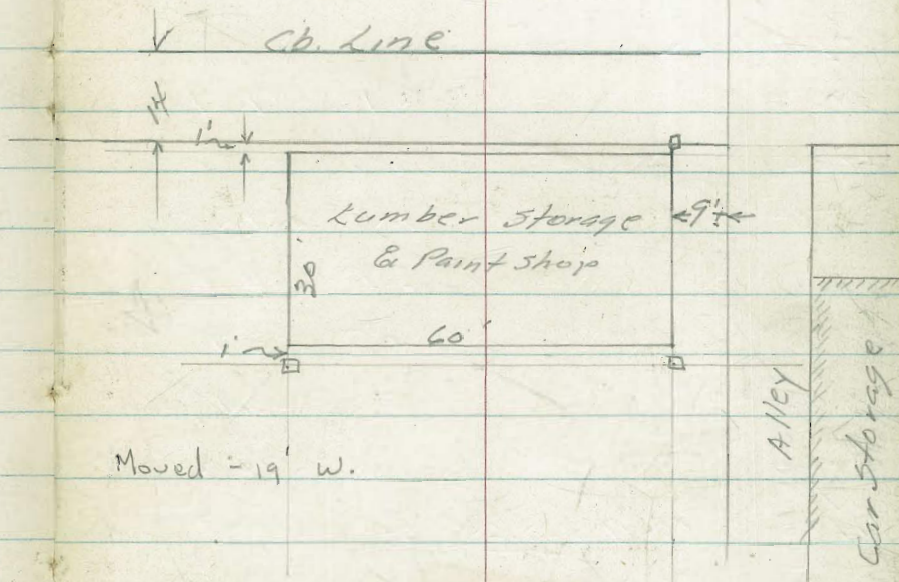
72

Sta.	+	H.I.	- Lt.	Elev. Stake Lt.	Elev. Grade Lt.	Corr Lt.	offset	- Rt.	Elev. Stake Rt.	Elev. Grade Rt.	Corr Rt.	offset
0+61.33	End		4.76	-0.17	-0.60	CO ⁴³	2°	5.21	-0.62	-0.60	FO ⁰²	2°
0+44.65			4.89	-0.30	-0.75	CO ⁴⁵	1°	5.03	-0.44	-0.75	CO ³¹	1°
0+27.98			5.19	-0.60	-0.91	CO ³¹	1°	5.32	-0.73	-0.91	CO ¹⁸	1°
0+07.98			5.28	-0.69	-1.10	CO ⁴¹	0 ²⁰	5.13	-0.54	-1.10	CO ⁵⁶	0 ³⁰
0+00	E. line	Pay side	5.85	-1.26	-1.22	Ex. Pay		5.85	-1.26	-1.26	Ex. Pay.	
2+42.7	W. line	Pay side	5.84	-1.25	-1.23	Ex. Pay		5.77	-1.18	-1.19	Ex. Pay.	
2+20			5.02	-0.43	-0.92	CO ⁴⁹	1°	5.27	-0.68	-0.91	CO ²³	3°
2+00			5.03	-0.44	-0.76	CO ³²	0 ¹⁰	4.92	-0.33	-0.76	CO ⁴²	2°
1+75.5			4.71	-0.12	-0.57	CO ⁴⁵	2°	4.60	-0.01	-0.57	CO ⁵⁶	2°
1+51			4.97	-0.38	-0.37	FO ⁰¹	2°	4.91	-0.32	-0.37	CO ⁰⁵	2°
1+26.5			4.11	0.48	-0.26	CO ⁷⁴	2°	4.59	0.00	-0.26	CO ²⁵	0 ⁵⁰
1+02			4.90	-0.31	-0.30	FO ⁰¹	1°	4.78	-0.19	-0.30	CO ⁴	2°
			4.59					4.59				

5850 Stake Lumber Storage
 Hendricks & Paint Shop
 McCoy (20th & B Sts)
 Bunch
 Crawford
 WO# 20543

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INDEXED
 MK
 MAY 29 1950



SVI Cor. 5.14 66.36

SE Cor. 5.38 66.12

TP 6.39 71.50 1.52 65.11

BM 0.15 66.67 66.52

4365 BM
 20 & B

Carpenter Shop

Grades on South H Line
of Loring St Lamont to PL

74

Sta. + H.I. - Elev. Stake Elev. Grade Cor f.

INDEXED

MAY 29 1950

Sta.	+ H.I.	- Elev. Stake	Elev. Grade	Cor f.
		7.65	220.99	220.99 Top Cement Skirway 8.5' H 4+98.87 FB1553 P. 50
4+98.87	PL		223.00	
4+50		8.9	219.7	222.75 F3 ⁰
4+00		8.3	220.3	222.50 F2 ³
3+50		7.4	221.2	222.25 F1 ¹
3+00		3.9	224.7	222.00 C2 ⁷
2+80		4.7	223.9	221.90 C2 ⁰
2+40		5.2	223.4	221.50 C1 [?]
2+00		9.4	220.2	220.00 C0 [?]
1+60	10.17	228.64	1.26	218.47 C1 ⁻
1+20		7.2	212.5	214.12 F1 ⁵
0+80		11.4	208.3	211.60 F2 ³
0+40		10.8	208.9	210.05 F1 ³
0+00	E. line Lamont	11.7	208.0	208.70 F0 [?]
BM	12.99	219.73	206.85	187 3' 50 Loring on E 7' Lamont. (FB1553 P. 47)

Grades on Steps to Pump Sta. at Loring
Plan = 12-52-D

B.P. = 46.00

B.M. = 22.65 = Top cb. - s.w. Cor.

W.O. 20194

8-2-49 **79** 7.0

INDEXED

Lt. = S.

Rt. = N.

0+00 = face of cb. at Φ ^{W.K.}
AUG 17 1949 47.00

+12.12 = Back of Top 47.75 47.00⁷⁵

C 0.75 = To Bottom 48.37 47.00^{8.37} C 1.37

+24.50 = Back of 1st Landing 44.20 39.41^{44.20}

C 4.79 47.89 39.41^{47.89} C 8.48

+40.75 = " 2nd " 33.74 30.66^{3.74}

C 3.08 41.08 30.66^{41.08} C 10.42

+57.00 = " 3rd " 24.53 22.16^{4.53}

C 2.37 26.36 22.16^{6.36} C 4.20

+73.00 = edge at Φ

50.43
 11.43
 61.86 = T
 0.93

61.86
 6.86
 55.00

6400 - N

60.93 4+50

50.43
 9.98
 60.41
 5.42
 54.99

7.17
 68.10

4.38
 63.72 = Nail in Pole

68.10
 4.01
 64.09

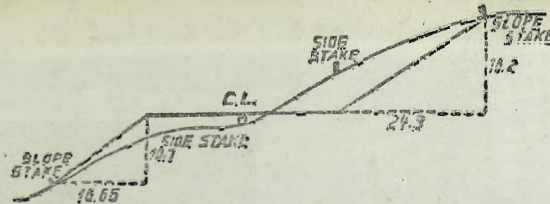
945
 657
 288
 997
 1285

2.10
 1.05
 525

NL = 19.53

15' N = 20.23

65' N = 22.52



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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