

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

89.73
- 59

89.14

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APR 13 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV



Distance of slope stake from side of shoulder
stake for any width roadway slope 1 1/2 to 2
It should be possible to lay out on 1/2

IMPROVED TABLES
AND
INFORMATION

cut taper. If it does not make the right
adjustment decrease

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with radius, I, tangent length
by dividing tangent (or external) by degree I by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.053	.057	.061
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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Law
Ingraham to Haines

7-2-49

7449-L

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	Rough Gr.	Ch.	So gutter	BM #7 page 80	SO. 1/4	North 1/4	North gutter	Ch.	Rough
1+00	<u>105.22</u> 5.92 6.12 FO.20	<u>105.22</u> 6.68 x	<u>104.55</u> 5.16 x	108.65 2.49 111.14 -8.99 102.15 7.97 110.125		105.120	105.05 4.66 x	<u>105.72</u> 6.18 x	<u>105.72</u> 5.42 4.72 C-0.70
0+80	<u>105.71</u> 5.43 5.94 FO.51	<u>105.71</u> 6.19 x	<u>105.04</u> 4.67 x	BM #7 108.65 3.25 111.90		105.68	105.54 4.17 x	<u>106.21</u> 5.69 6.46 x	<u>106.21</u> 4.93 4.42 C-0.51
INDEXED WK DEC 5 1949 0+60	<u>106.27</u> 4.87 5.23 FO.36	<u>106.27</u> 5.63 x	<u>105.60</u> 4.11 x			106.25	106.10 3.61 x	<u>106.77</u> 5.13 x 5.90 x	<u>106.77</u> 4.37 4.16 C-0.21
0+40	<u>106.87</u> 4.27 4.77 FO.50	<u>106.87</u> 5.03 x	<u>106.20</u> 3.51 x	BM #7 108.65 1.06 109.71 gutter #2		106.85	106.70 3.01 x	<u>107.37</u> 4.53 5.30 x	<u>107.37</u> 3.77 4.00 FO.23
0+20 G.E.C.	<u>107.55</u> 3.59 4.20 FO.61	<u>111.90x</u> 107.55 4.35 x	<u>106.88</u> 2.83 x			107.65	107.38 2.33 x	<u>111.90</u> 108.05 3.85 x	<u>109.05</u> 3.09 2.88 C-0.21
Wly Ingraham 0+00	<u>107.82</u> 3.32 4.04 FO.72 111.14	<u>107.82</u>	<u>107.28</u>			107.90	108.05	108.52	<u>108.52</u> 2.62 2.03 C-0.59 111.14 x

Law

Ingraham to Haines

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	South			North					
	Rough Br.	cl.	gutter	1/4	±	1/4	Gutter	cl.	Rough
Ely Haines 5+00	<u>102.50</u> 7.62 <u>7.42</u> C-0.20	102.50	101.83		102.30		102.46	103.13	<u>103.13</u> 6.99 <u>4.60</u> C-2.39
A+90 ol.B.C. = ④	<u>102.54</u> 7.58 <u>7.19</u> C-0.39	^{A32} 107.28 <u>102.54</u> 4.74	101.87		102.52		102.37	^{T-P32} 107.28 <u>103.04</u> 4.24	<u>103.04</u> 7.08 <u>4.31</u> C-2.77
A+36	<u>102.76</u> 7.36 <u>7.59</u> F0.23								<u>103.26</u> 6.86 <u>4.26</u> C-2.60
3+82	<u>102.97</u> 7.15 <u>8.11</u> F0.96								<u>103.47</u> 6.65 <u>4.46</u> C-2.19
3+28	<u>103.19</u> 6.93 <u>7.99</u> F1.06	Rake	Rake		Rake		Rake	Rake	<u>103.69</u> 6.43 <u>4.13</u> C-2.30
2+74	<u>103.40</u> 6.72 <u>8.05</u> F1.33								<u>103.90</u> 6.22 <u>4.40</u> C-1.82
	110.127 P.3								110.127 P.12

Chalcedony

Lamont to Kendall 7447-L

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	Rough	cl.	gutter		1/4	±	1/4	gutter	cl.	Rough
1+00	136.357 <u>127.68</u>	127.68	127.18	B.M. #3 @ 259		127.96	127.93	128.68	128.68	136.357 <u>128.68</u>
	8.67 8.03 C-0.64	6.03 X	7.00 X	23 126.01 10.34 136.357			6.25 X	5.03 X		7.67 3.08 C-4.59
0+80	X cross <u>127.48</u>	127.48	126.98			127.76	127.73	128.48	128.48	127.48 <u>126.98</u>
	8.87 8.25 C-0.62	6.23 X	7.20 X				6.45 X	5.23 X		7.87 3.56 C-4.31
0+60	<u>127.21</u>	127.21	126.71			127.49	127.46	128.21	128.21	127.21 <u>126.71</u>
	9.14 8.55 C-0.59	6.50 X	7.47 X				6.72 X	5.50 X		8.14 3.97 C-4.17
0+40	<u>126.87</u>	126.87	126.37			127.15	127.12	127.87	127.87	126.87 <u>126.37</u>
	9.48 8.99 C-0.49	6.84 X	7.81 X				7.06 X	5.84 X		8.48 4.30 C-4.18
0+20	<u>126.47</u>	126.47	125.97			126.75	126.72	127.47	127.47	126.47 <u>125.97</u>
	9.88 9.33 C-0.55	7.24 X	8.21 X				7.46 X	6.24 X		8.88 4.68 C-4.20
P.V.C. W.L. Lamont 0+00	<u>126.00</u>	126.00	125.38	134.18X 128.10 609 134.19X		126.19	126.29	127.00	127.00	126.00 <u>125.38</u>
	10.35 V	7.71 7.66 +0.05	8.30				134.19X	6.71 6.73 -0.02		9.35

INDEXED

M.K.

DEC 5 1949

Chalcedony

Lamont-Kendall

✓
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	Rough	cl.	Gutter	1/4	♀	1/4	gutter	cl.	Rough
3+00	136.35x 128.74 7.61 6.99 C-0.62	128.74 4.97 x	128.24 5.94 x		129.02		128.99 5.19 x	129.74 3.97 x	136.35x 129.74 6.61 4.16 C-2.45
P.V.C. 2+80	128.68 7.67 7.62 C-0.05	128.68 5.03 x	128.18 6.00 x		128.96		128.93 5.25 x	129.68 4.03 x	129.68 6.67 4.15 C-2.52
2+40	128.46 7.89 7.50 C-0.39								129.46 6.89 4.09 C-2.80
x cross 2+00	128.25 8.10 7.64 C-0.46	Rate	Rate		Rate		Rate	Rate	129.25 7.10 3.89 C-3.21
1+60	128.03 8.32 7.84 C-0.48								129.03 7.32 3.56 C-3.76
B+k-EUC. 1+20	127.82 8.53 7.92 C-0.61	127.82 5.89 x	127.32 6.86 x		128.10		128.07 6.11 x	128.82 4.89 x	134.18x 128.82 7.53 2.91 C-4.62

T.P.

Chalcedony
Lamont to Kendall

131.76 X	5+40 Lt. =
3.48	124.00
128.35	7.76
P. Hyatt Kendall	<u>131.76X</u>
- B. H. #	

± Kendall
5+40

126.69 X	
134.75 X	124.00
124.00	<u>2.69</u>
10.75	X T.P.
10.32	
C 0.43	

125.00

	Rough	Cl.	gutter	1/4	±	1/4	gutter	Cl.	Rough
E.H. Kendall 5+00	125.00	131.76 X 125.00	124.50		125.27		125.25	126.00	134.75 X 126.00
	9.75 8.66 C-1.09	6.96 X						5.76 0.24 C-2.55	8.75 6.20 C-2.55

± Cl.
R.T.G. only
4+90

	125.50	126.25	X 1/4 walk	126.25
		5.51 X		8.50 5.96 C-2.54

4+50

126.25	126.25
8.50	5.51
7.32	X
C-1.18	

Rake

Rake

127.25	127.25
4.51	7.50
	5.51
	C-1.99

Chalcedony

Kendall to Jewell

7446-L

10

	Rough	cb.	gutter	1/4	1/2	1/4	gutter	cb.	Rough
P.V.C. 1+60	122.75x 118.60	126.69 118.60	122.93x 118.10				122.82x 118.85	126.69 119.60	122.75x 119.60
	4.15 5.42 F-1.27	8.09 x	10.73 x				7.78 x	7.09 x	3.15 1.53 C-1.62
	122.75x 119.70		134.75 12.91 121.84 0.91 122.75x						122.75 120.71 2.04 0.72 C-1.32
	3.05 3.72 F-0.67								
(T.P.) rock									
0+80	120.80 13.95 14.27 F-0.32								121.82 1293 11.51 C-1.42
		Rate	Rate				Rate	Rate	
0+40	121.90 12.85 12.65 C-0.20								122.93 11.82 10.16 C-1.86
		Rate	Rate				Rate	Rate	
N. cl. + G. 0+10							123.03	126.69 123.78 2.91	123.78 10.97 9.30 C-1.67
W.L. Kendall 0+00	123.00 11.75 11.38 C-0.37	Fill 126.69 123.00 3.69 x	122.50		123.27		123.25	124.00	124.00 10.75 9.04 C-1.71 95 C-0.86 to East

Chalecdony
Kendall to Jewell

	Rough	cb.	gutter	1/4	±	1/4	gutter	cb.	Rough
3+40	<u>114.95</u> 7.80 9.29 F 1.49								<u>115.95</u> 6.80 4.00 C-2.80
2+90	<u>115.86</u> 6.89 8.38 F 1.49	Rate	Rate		Rate		Rate	Rate	<u>116.86</u> 5.89 3.08 C 2.81
E.V.C. 2+40	<u>116.77</u> 5.98 7.18 F 1.20	126.69 <u>116.77</u> 9.92 X	<u>116.27</u> 12.56 X		117.05		117.02 11.91 X	117.77 8.92 X	<u>117.77</u> 4.98 2.62 C-2.36
2+20	<u>117.16</u> 5.59 6.69 F 1.10	<u>117.16</u> 9.53 X	<u>116.66</u> 12.17 X		117.44		117.41 11.42 X	<u>118.16</u> 8.53 X	<u>118.16</u> 4.59 2.67 C-1.92
2+00	<u>117.59</u> 5.16 6.00 F 0.84	<u>117.59</u> 9.10 X	<u>117.09</u> 11.74 X		117.87		117.84 10.99 X	<u>118.59</u> 8.10 X	<u>118.59</u> 4.16 2.43 C-1.73
1+80	<u>118.07</u> 4.68 5.82 F 1.14	<u>118.07</u> 8.62 X	<u>117.57</u> 11.26 X		118.35		127.82 <u>118.32</u> 10.51 X	126.69 <u>119.07</u> 7.62 X	<u>119.07</u> 3.68 2.20 C-1.48

Chaledony

Jewell to Ingraham

7445-L

	Rough	Cl.	gutter	1/4	1/2	3/4	North gutter	Cl.	Rough
1+50	108.25 7.75 7.80 -0.05		B.M. 21 6259 23 115.45 059 116.00						109.26 6.74 5.99 C.0.75
INDEXED DEC 5 1949 1+00	109.16 6.84 6.86 -0.02	Rate	115.41 0.65 116.06				Rate	Rate	110.18 5.82 5.25 C.0.57
0+50	110.07 5.93 5.94 -0.01	Rate			Rate		Rate	Rate	111.09 4.91 4.17 C.0.74
N. Cl. + O. only 0+16.99							110.95	111.70	111.70 4.30 3.44 C.0.86
O.E.C. 0+10	110.81 Drip	116.06 110.81 5.25 DRIVE	116.06 110.31 5.75 X		111.10		108.25 X 111.07	110.00 111.82 4.24	111.82 4.18 3.27 C.0.91
W.L. Jewell 0+00	111.00 5.00	111.00	110.50		111.20		111.25	112.00	112.00 4.00 Not set.
									116.00 114.44 1.56 20.4 F.0.48

Chalcedony

Jewell to Ingraham
Rough lbs

gutter

1/4

¢

1/4

gutter

lb.

Rough

4+50

102.76

6.61

6.68

-0.07

116.00
7.61
108.39
0.98
109.37

103.78
5.59
3.18
C-2.41

4+00

103.67

5.70

5.69

+0.01

L

104.70
4.67
1.95
C 2.72

3+50

104.59

4.78

4.77

0.01

L

109.37x
105.61
3.76
1.80
C-2.46

3+00

116.00

105.50

10.50

10.45

+ 0.05

Rake

Rake

Rake

Rake

Rake

T.P. 116.00x
106.52
9.48
7.61
C 1.87

2+50

106.42

9.58

9.60

-0.02

107.44
8.56
7.07
C-1.49

2+00

107.33

8.67

8.67

X

116.00x
108.35
7.65
6.68
60.97

Chalcedony
Jewell to Ingraham.

101.54 BM#1
5.74
107.28

~~N.E. Prop. E.C.
on Ingraham~~ } ~~109.37
102.20
7.17
3.23
C-3.84~~

South

North

	Rough	cl.	gutter	1/4	±	1/4	gutter	cl.	Rough
EL. Ingraham 5+20	109.37 101.27 8.10	101.27 6.01	100.72		101.08		101.45	102.72	102.72 6.65 5.26 C-1.39
North only prop. B.C. 5+03	—						102.07	102.82	102.82 6.55 4.07 C-2.48
CG. B.C. 5+00	109.37x 101.84 7.53 7.47 +0.106	101.84 5.44 5.36 +0.08	101.34 5.94		102.10		104.25x 102.12 6.13	101.28x 102.87 4.41	109.37x 102.87 6.50 3.98 C-2.52
So. Prop. B.C. A+95		101.98	101.48		Rate ↑				Rate
					Rate				Rate

BM#23
102.93
532
107.25

Sewer Laterals

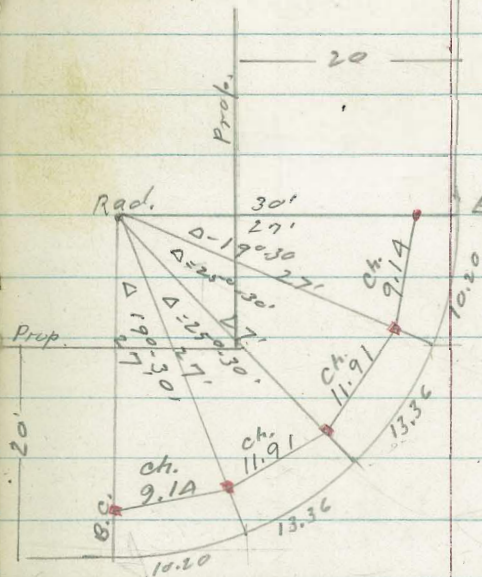
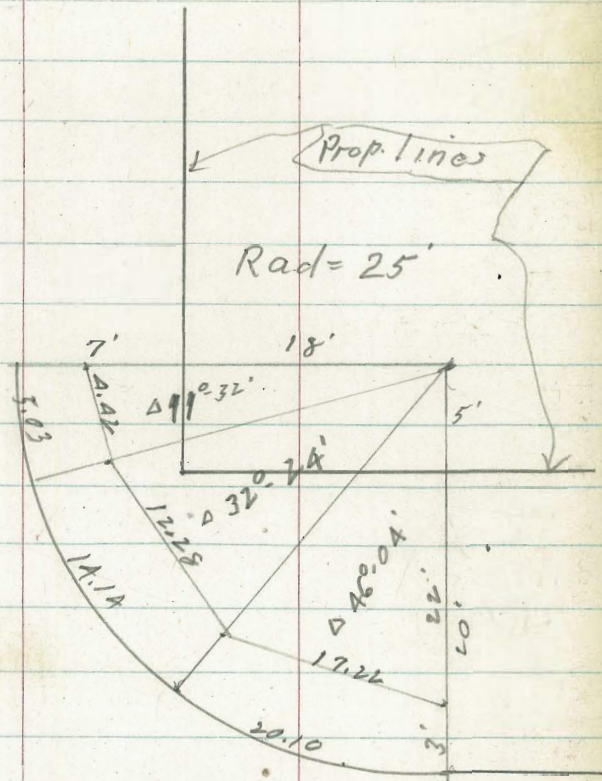
Lat. #1 (7450-L) on Law - 60' E. of Jewell

139.16 X	BM. 29 - 131.51
EL. = 128.79	7.65
10.37	139.16 X
1.31	
C-9.06	

stake
5' Back

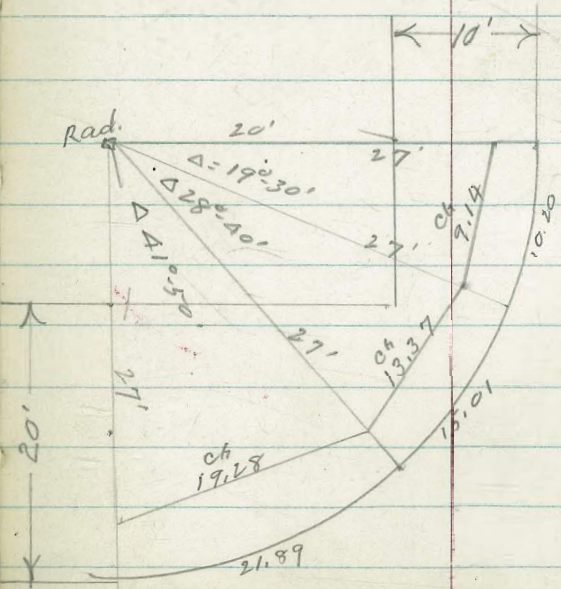
INDEXED
W.K.
DEC 5 1949

Sample Returns - 30 Rad



E.o. 20' Curbs
stakes set
3' back of ch.

22.90
12.05
35.15



10 + 20' Cbs.
Rad = 30'
stakes set
3' back cbs.

CHALCEDONY

Ingratam to Haines

120

	Rough Cr.	Cl.	Gutter	X	1/4	£	1/4	Gutter	Cl.	Rough Cr.
2+90	TIP 92.50 <u>10.50</u> 11.10 <u>F0.60</u>	92.50 Rate	Rate	X-P.19 103.00		Rate		Rate	Rate	103.00 X <u>93.50</u> 9.50 <u>8.64</u> C-0.86
6x 10 E.V.C. 2+50	92.70 <u>10.30</u> 10.92 <u>F0.67</u>	92.70 <u>9.06</u> X	92.10 10.49 X		92.98			92.95 7.74 X	101.98 X 93.70 <u>8.28</u> X	93.70 <u>9.30</u> 8.43 C-0.87
2+30	92.80 <u>10.20</u> 10.71 <u>F0.51</u>	92.80 <u>8.96</u> X	92.30 10.39 X		93.08			93.05 9.64 X	93.80 <u>8.18</u> X	93.80 <u>9.20</u> 8.03 C-1.17
2+10	92.96 <u>10.04</u> 10.50 <u>F0.46</u>	92.96 <u>8.80</u> X	92.46 10.23 X		93.24			93.21 9.48 X	93.96 <u>8.02</u> X	93.96 <u>9.04</u> 7.77 C-1.27
1+90	93.22 9.78 <u>10.58</u> F0.80	93.22 <u>8.54</u> X	92.72 9.97 X		93.50			93.47 9.22 X	94.22 <u>7.76</u> X	94.22 <u>8.78</u> 7.09 C-1.69
1+70	100.00 93.61 <u>9.39</u> 10.50 F-1.11	101.76 X 93.61 <u>8.15</u> X	102.69 X 93.11 <u>9.58</u> X		93.89			102.69 X 93.86 <u>8.83</u> X	94.61 <u>7.37</u> X	94.61 <u>8.39</u> 6.62 C-1.77

CHALCEDONY

Ingratiam to Haines

21

	Rough Gr.	Cl.	Gutter	P.20 103.00 11.10 91.90 7.03 98.93	1/4	±	1/4	Butter	Cl.	Rough Gr.
E. Line Haines 5+00	91.45 7.48 7.77 F0.29	97.33X 91.45 5.88	90.90			91.52		91.76	97.33X 92.50 4.17	92.50 6.43 4.66 C-1.77
Cl. B.C. A+90	91.55 7.38 7.72 F0.34	97.33X 91.55 5.78 X	96.77X 91.05			91.83		96.77X 91.80	97.33X 92.55 4.78 X	92.55 6.38 A.2C C-2.12
4+50	91.74 7.19 7.67 F0.48			96.41 2.36 96.77						92.74 6.19 4.27 C-1.72
4+10	91.93 7.00 7.30 F-0.30	Rate	Rate			Rate		Rate	Rate	92.93 6.00 4.88 C-1.12
3+70	92.12 6.81 6.80 C-0.01									93.12 5.81 4.77 C-1.04
3+30	92.31 6.62 6.69 F0.07									93.31 5.62 4.75 C-0.87

Chalcedony
Haines to Gresham

#7443-L

	Rough Cr.	Cl.	Gutter	From P. 22 X	1/4	¢	1/4	Gutter	Cl.	Rough Cr.
2+02	96.56 X 90.08 6.48 8.32 C-0.16			98.93 8.09 90.84 105.72 96.56						96.56 X 91.08 5.48 3.38 C-2.10
1+54	TP 90.30 8.63 8.09 C-0.54			B.M. 41 89.34 4.53 93.87 13.70 90.17 7.16 97.33 X 2.92 94.41						91.30 7.63 5.50 C-2.13
1+06	90.51 8.42 7.33 C-1.09	Rate	Rate			Rate		Rate	Rate	91.51 7.42 4.76 C-2.66
0+58	X-in Conc. 90.73 8.20 7.41 C-0.79	Rate	Rate			Rate		Rate	Rate	X-in Conc. 91.73 7.20 4.42 C-2.78
W.B.C. 0+10	90.95 7.78 7.46 C-0.52	97.30 X 90.95 6.38 X	90.45			91.22		91.20	97.33 X 91.95 5.38 X	91.95 6.98 4.98 C-2.00
W.L. Haines 0+00	98.93 X 91.00 7.93 7.23 C-0.70	97.31 91.00	90.54			91.27		91.27	92.00 6.93 5.06 C-1.87	

INDEXED
W.K.
DEC 5 1949

Chalcedony
Haines to Gresham

5400
W.L. Gresham

Rough
88.70

93871
88.70

94710
88.13

1/4

89.05

1/4

94710
89.12

Cl.
93.875
89.75
4.12
4.14
OK

123
Rough Gr.
89.75
6.81

786
790
-0.04

5.17
5.15

88.13

96.567
7.26
89.30
+0.04

A+90

88.77
7.79
7.43
C-0.36

88.77
5.10

88.27

89.05

out
89.02

89.77
4.10

89.77
6.79
4.51
C-2.28

923
X
93.87

A+42

88.99
7.57
7.43
C-0.14

88.77

88.27

X-in Conc.
89.99
6.57
5.08
C-1.49

3+94

89.21
7.35
7.79
F-0.44

90.21
6.35
5.11
C-1.24

3+46

89.42
7.14
7.30
F-0.16

Rate

Rate

Rate

Rate

90.42
6.14
4.97
C-1.17

2+98

89.64
6.92
6.99
F-0.07

Brk → 89.89
Set.

90.64
5.92
4.67
C-1.25

2+50

96.567
89.86
6.70
6.61
C-0.09

90.86
5.70
4.28
C-1.42

Law

Lament to Kendall (7451-L)

124

	Rough	cg.	gutter		1/4	±	1/4	gutter	cg.	Rough
1+00	146.82	146.82	146.15			146.80		146.65	147.32	147.32
	6.26	5.91		BM #8					5.76	5.76
	7.00	X		A.80					X	3.03
	F0.74			181.51						C-2.73
				10.71						
0+80	146.27	146.27	145.60	142.22		146.25		146.10	146.77	146.77
	6.87	6.46		3.29					5.96	6.31
	8.11	X		138.93					X	3.78
	F1.30			BM #9						C-2.53
				S.E. H. prof.						
				Kendall						
				+ Law						
0+60	145.57	145.57	144.90	138.93		145.55		145.40	146.07	146.07
	7.51	7.16		12.52					6.66	7.01
	8.43	X		151.45					X	4.70
	F0.92			4.57						C-2.31
				146.88						
				6.20						
0+40	144.73	144.73	144.06	153.08		144.71		144.56	145.23	145.23
	8.35	8.00		7.98					7.50	7.85
	9.89	X		143.10					X	5.05
	F1.54			N.W. 71						C-2.80
				L+T.						
				Lament						
				+ Law						
C.O.B.S.				153.08X						
0+20	143.77	143.77	143.10	BM #10		143.75		143.60	144.27	144.27
	9.31	8.96		143.10					8.46	8.81
	10.17	X		9.63					X	5.43
	F0.86			152.73						C-3.38
W.L. Lament										
0+00	142.63	142.63	142.02			142.53		142.47	143.13	143.13
	10.45	10.10							9.60	9.95
		10.30							9.80	
		-0.20							-0.20	

Lawn.
Larrott to Kendall

125

	Rough	Cl.	gutter	1/4	£	1/4	gutter	Cl.	Rough
2+20	152.55 147.41	147.41	146.74		147.39		147.24	147.91	152.55 147.91
	5.14 5.83 F9.69	5.32 X		153.08 6.36 146.72 5.83 152.55				4.82 X	4.64 0.93 C-3.71
2+00	TIP. 147.65	147.65	146.98		147.63		147.48	148.15	148.15
	5.43 6.36 F0.93	5.08 X						4.58 X	4.93 +2.00 C 6.93
1+80	147.76	147.76	147.09		147.74		147.59	148.26	148.26
	5.32 6.09 X F-0.97	4.97 X						4.47 X	4.82 Not set.
1+60	x-in walk 147.72	147.72	147.05		147.70		147.55	148.22	Tack on 11.00 148.22
	5.36 6.11 F 0.75	5.01 X						4.51 X	4.86 +2.87 C 7.73
1+40	147.55	147.55	146.88		147.53		147.38	148.05	148.05
	5.53 6.20 F 0.67	5.18 X						4.68 X	5.03 0.63 C 4.40
1+20	153.08 147.26	147.26	146.59		147.24		147.09	147.76	153.08 147.76
	5.82 6.47 F 0.65	5.47 X						4.97 X	5.32 1.59 C-3.73

LAW
Lamont + Kendall

	Rough	cl.	gutter		1/4	±	1/4	gutter	cl.	Rough
E.V.C. 3+40	143.24 9.31 9.77 F 0.46	143.24 6.71 X	142.57			143.22		143.07	143.74 6.21 X	143.74 8.81 6.38 C-2.43
3+20	X-in Drive 144.26 8.29 8.67 F 0.38	144.26 5.69 X	143.59			144.24		144.09	144.76 5.19 X	144.76 7.79 5.84 C-1.95
3+00	145.16 7.39 6.29 C-1.10	145.16 9.79 X	144.49			145.14		144.99	145.66 9.29 X	145.66 6.89 4.93 C-1.96
2+80	145.92 6.63 5.83 C-0.80	145.92 4.03 X	145.25			145.90		145.75	146.42 3.53 X	146.42 6.13 2.65 C-3.48
2+60	146.56 5.99 5.91 C-0.08	146.56 3.39 X	145.80			146.54		146.39	147.06 2.89 X	147.06 5.49 1.89 C-3.60
2+40	147.05 5.50 6.03 X F 0.58	147.05 2.90 X	146.38			147.03		146.88	147.55 2.40 X	147.55 5.00 1.39 C-3.61

NK 7/47
Lamont + Low
143.10
6.83
147.93 T

TR 11.03
138.92
7.03
142.95 T

LAW.
Lament to Kendall

27

136.50
7.84
3.23
C-4.61

133.65
10.69
7.80
C-2.89

152.55 X
12.95
139.60
4.74
144.34 X

E.L. Kendall
5+00

Rough Cl. gutter
134.55
9.79
7.80
C-1.99
133.88

1

1/4

1/4

gutter

Cl.

Rough

134.38

134.53

135.20

135.20

9.14
3.23
C-5.91

d. B.C.
4+90

135.06
9.28 X
7.69
C 1.59
135.06
7.89
X
134.39

135.00

134.87

135.54

135.54

x-walk
8.80
3.12
C-5.68

7.41
X

4+40

137.79
6.55
6.85
F0.30
137.79
5.16
X

135.00

138.27

144.34 X
138.27
6.07
2.77
C-3.30

4.68
X

3+90

152.55 X
140.52
12.03
12.95
F-0.92
142.95 X
140.52
2.43
X

Rate

Rate

Rate

142.95 X
141.00
1.95
X
152.55 X
141.00
11.55
8.15
C-3.40

LAW,
Kendall to Jewell (7450-L)

740

128

	Rough	cl.	gutter	T	1/4	±	1/4	gutter	cl.	Rough
1+34	139.96 139.62 6.34 7.58 F-1.24			144.34 12.52 131.82 8.14 139.76						139.96x 134.34 5.62 3.85 C-1.77
INDEXED WK DEC 5 1949 1+03	144.34x 133.50 10.84 12.52 F-1.68			B.M.#8 131.51 8.26 139.77x						144.34x 134.21 10.13 8.40 C-1.73
0+72	133.38 10.96 12.32 F-1.36	Rate	Rate			Rate		Rate	Rate	134.09 10.25 8.33 C-1.92
0+41	133.26 11.08 12.36 F-1.28							Rate	Rate	133.96 10.38 8.37 C-2.01
ch.B.C. 0+10	133.14 11.20 11.80 F 0.60	139.02 133.14 5.88 x	132.47		133.22		133.17	139.02 133.184 5.18 x	oo wall 133.184 10.50 2.74 C-7.76	
w.L.Kendall 0+00	144.34 133.10 11.24 11.81 F 0.57		132.45	SEE HYD. Kendall + Law 138.92 0.10 139.02 T TP. 5.88 133.20 6.57 139.77x 8.26 X 131.51 B.M.#8	133.10		133.30			144.34 133.180 10.54 2.41 C-8.13
132.70 11.64 11.81 C 0.17										135.75 8.59 2.41 C-6.18

Lavi.
Kendall to Jewell

29

	Rough	ob.	gutter	1/4	±	1/4	gutter	ob.	Rough
P.V.C. 3+20	141.60 134.33 7.27 7.87 F 0.60	139.77 134.33 5.44 X	133.66 139.96 7.62 132.34 9.26 141.60		134.44		134.41 135.08 4.69 X	139.77	141.60 135.08 6.52 2.26 C-4.26
2+89	T.P. 139.96 X-drive 134.22 5.74 7.62 F 1.88								139.96 134.96 5.00 1.20 C 3.80
2+58	134.10 5.86 7.74 F-1.88								134.84 5.12 1.42 C-3.70
2+27	133.98 5.98 7.68 F 1.70								134.71 5.25 2.66 C-2.59
1+96	133.86 6.10 7.47 F 1.37	Rake	Rake				Rake	Rake	134.59 5.37 3.02 C-2.35
1+65	139.96 133.74 6.22 7.25 F 1.03								139.96 134.46 5.50 3.03 C-2.47

LAW
Kendall to Jewell

130

	Rough,	cb.	gutter	1/4	¢	1/4	gutter	cb.	Rough,
A+40	133.10 8.50 8.09 C-0.41	133.10 [?] 6.67 X	132.57		133.25		133.12	133.79 5.98 X	133.79 7.81 3.74 C-4.07
A+20	x-in walk 133.65 7.90 7.73 C-0.17	133.65 6.12 X	132.98		133.68		133.59	134.26 5.51 X	134.26 7.24 3.75 C-3.49
A+00	133.98 7.62 7.65 F-0.03	133.98 5.79 X	133.31		134.04		133.95	134.62 5.15 X	134.62 6.98 3.79 C-3.19
3+80	134.24 7.39 6.80 C-0.59	134.21 5.56 X	133.54		134.28		134.21	134.86 1.91 X	134.86 6.74 3.40 C-3.34
3+60	134.36 7.24 6.85 C-0.39	134.36 5.41 X	133.69		134.43		134.37	135.04 1.73 X	135.04 6.56 3.00 C-3.56
3+40	x-in walk 141.65 134.41 7.19 7.36 F-0.17	Pg 28 139.77 134.41 5.36 X	133.74		134.49		134.44	139.77 135.11 1.66 X	135.11 6.49 2.67 C-3.82

LAW.
Haines to Gresham

Next page

	Rough	Obs	gutter	1/4	±	1/4	gutter	Obs	33
a. B.C. 4+90	99.18 7.78 7.62 C-0.16	104.36 99.18 5.18 X	98.68 5.43 X				99.43 4.68 X	104.36 100.18 4.18 X	100.18 6.78 5.44 C-1.34
4+42	99.46 7.50 7.01 C-0.49		6.94 98.68 5.43 104.11 78.68 6.08 105.36					105.36 100.18 5.18	100.46 6.50 4.65 C-1.85
3+94	99.73 7.23 7.46 F 0.23								100.73 6.23 4.23 C-2.00
3+46	100.01 6.95 6.76 C-0.19	Rake	Rake				Rake	Rake	101.01 5.95 3.89 C-2.00
2+98	100.28 6.68 6.56 C-0.12								101.28 5.58 3.89 C-2.19
2+50	106.76 100.56 6.40 6.17 C-0.23								101.56 5.40 3.09 C-2.31

LAW
Haines to Gresham

	Rough	cl.	gutter	1/4	¢	1/4	gutter	cl.	Rough
E.L. Gresham		104.36						104.36	
500	99.12	98.93	98.30		99.40		99.31	199.90	100.12
	7.84	5.43						4.46	6.84
		5.39						4.44	7.04
	-0.16	+0.04						+0.02	-0.20

Beryl

Lamont to Emelene 7454-L

35

	Rough	cl.	gutter	BM #10	1/4	+	1/4	gutter	cl.	Rough
+5' Bl. Driveway	162.76	162.76	162.09	143.10 13.07 156.17 0.17 156.00 12.97 168.97 6.95 162.02						163.22
	8.66 10.17 F 1.51	6.04 X	5.94 X		162.74					8.20 3.33 -4.87
INDEXED DEC 5 1949 W.L.	171.42 T			162.02						171.42 T
+40	162.55	162.55	161.88	set BM NW 7' lat Lamont + Beryl						163.08
	8.87 9.61 F 0.78	6.25 X	6.15 X		162.53					8.34 3.08 -5.26
P.V.C. on So, +20	168.97 T			168.97 T TP 5.98 162.99 + 8.43 171.42 T						168.97 T
	162.37	162.37	161.70		162.35					162.95
	6.60 6.80 F 0.20	6.43 X 5.66 V	6.33 X							6.02 0.02 -6.00
BM #17										
0+70	161.98	161.98	161.70							162.61
	162.02 6.78 168.80 X	6.99 6.64 C 0.33	6.73 = 01.70 X 6.93 = 01.45 X							6.36 0.75 -5.61
0+20	161.58	161.58	160.91		161.56					162.28
	7.39 6.83 C 0.56	7.22 X 6.45	7.12 X							6.67 0.60 -6.07
W.L. Lamont										
0+00	161.42	161.42	160.73		161.32					162.15
	168.80 7.93 161.67	7.35 7.93 -0.38	7.25 7.56 -0.31 +1.06							162.15
										7.70 7.80 -0.10
										6.65 6.95 -0.30
										6.82 7.13 -0.31

Rate

Rate

Beryl
Lament to Emeleene

36

	Rough	cl.	gutter	
2+40	163.94	163.94	163.27	163.92
	7.48	48.6	4.76	
	10.50	x		
	F. 3.02			

North only End of Return 25' cl. Rad. (on Rad. 4')

166.00
5.72
4.88
20.54

2+20	163.59	163.59	162.92	163.57
	7.83	5.21	5.11	
	10.55	x		
	F. 2.72			

North cl. B.C.
2+17²¹

168.80
4.61
163.52 164.19 164.19
4.51
x
7.23
4.88
2.35

2+00	163.27	163.27	162.60	163.25
	8.15	5.53	5.43	
	10.42	x	x	
	F. 2.21			

168.80
4.61
163.52 164.19 164.19
4.51
x
7.23
4.88
2.35

1+80	163.00	163.00	162.33	162.99
	8.42	5.80	5.70	
	10.70	x	x	
	F. 2.28			

171.42
162.68 163.35 163.35
5.35 5.45 8.07
x 9.50
4.58 3.57

Beryl

Emelene to Kendall (7454-L)

37

Rough cl. gutter 1/4 1/4 gutter cl. Rough

3+40 INDEXED

DEC 5 1949

E.C. North cl

3+03

166.02

8.73

11.80

F-3.07

X-5'

165.22

9.53

12.77

F-3.24

165.22

3.38

X

Rate

2+17.27 Rt.

164.19

+Cut. 2.35

stake= 166.54

8.21

174.75X

Rate

1/4

1/4

1/4

gutter

cl.

Rough

166.54

8.21

3.02

C-5.19

X

174.75

165.74

9.01

3.70

C-5.31

3+00 omit 10217

W.L. E. and G. North only 2+85

End of Return

25' Rad. (or Rad 1/2)

166.50

8.25

3.70

C-4.55

E.V.C. 2+80

174.75

164.73

19.02

13.43

F-3.41

164.73

4.07

X

164.06

3.97

164.71

2+60

164.82

7.10

10.53

3.93

164.82

4.48

X

163.65

4.38

X

164.30

Beryl

Emelent to Kendall

E.L. Kendall to No. 5+37

Rough Cl. gutter

1/4

1/2

1/4

gutter cl.

38

Rough

on. Rad. End. of. Ret.

172.50

Cl. B.C. to No. 5+12

174.75x
4.34
170.41
8.03

169.69

170.36

5.94
2.40
C-3.54
170.36
5.03
8.08
2.40
C-5.68

End. of cl.

167.80

E.L. Kendall to No. 5+00

106.4
12.79
F 2.15

169.50

168.83

169.48

169.33

170.00

170.00

5.39
5.29

8.44

+ 0.10

B.C. to No. 50

4+90

169.28

169.28

168.61

169.26

169.78

9.16
12.79
F 3.63

8.66
2.73

C-5.93

4+60

168.62

9.82
14.82
F 5.00

Rate

Rate

169.14

9.30
2.84

C-6.46

4+20

178.44x
167.76
10.68
14.51
F 3.83

Rate

Rate

178.44

168.28

10.16
3.50

C-6.66

3+80

174.75x
166.89
7.86
11.10
F-3.24

Rate

174.75x

167.41

7.34
4.8

C-6.86

BERYL
Kendall to Jewell (7453-L)

✓
39

	Rough	Cl.	gutter	1/4	±	1/4	gutter	Cl.	Rough
P.V.C. 1+20	165.83	171.02x 165.83	165.16		165.81		165.66	173.86 166.33	173.20x 166.33
INDEXED N.K. DEC 5 1949 0+80	-0.23 6.08 F 6.31	5.17 x						7.53 x C 4.05	6.87 2.82 C 4.05
	167.16							178.44x 167.66	178.44x 167.66
	-1.53 3.63 F 5.10							1078 3.33 C-7.45	1078 3.33 C-7.45
	check 169.49	178.44x 168.49						168.99	168.99
2.86 1.47 F 4.33	9.95 14.28 F 4.33	Rate	Rate		Rate	Rate	Rate	9.45 174 C-7.71	
Cl. E.C. - No. 0+18					169.23		169.06	169.73 4.15 171.02x 169.73 9.29 C-7.42	169.73 8.71 129 C-7.42
Cl. E.C. - No. 0+10	178.44 169.50 8.94 12.53 F 3.59	169.50 1.52 x	168.83		169.50			178.86 - P.62 10.10	
W.L. Kendall 0+00	167.45 10.99 12.53 F 1.54	← End of cl. ←					End of cl. →	170.9 172.50 5.94 129 C-4.65	

BERYL

Kendall to Jewell

✓
40

	Rough	cl.	gutter	1/4	≠	1/4	gutter	cl.	Rough
2+40	165.63 162.64 <u>2.99</u> 11.17 F 8.18	171.02x 162.64 <u>8.38</u> X	161.97		162.62		162.47	173.86 163.14 <u>10.72</u> X	173.20x 163.14 <u>10.06</u> 7.74 C-2.32
2+20	163.07 <u>2.56</u> 9.91 F 7.35	163.07 <u>7.95</u> X	162.40		163.05		162.90	163.57 <u>10.29</u> X	163.57 <u>10.63</u> 7.56 C-2.07
2+00	163.52 <u>2.11</u> 8.66 F 6.55	163.52 <u>7.50</u> X	162.85		163.50		163.35	164.02 <u>9.84</u> X	164.02 <u>9.18</u> 7.82 C-7.36
1+80	164.04 <u>1.59</u> 7.94 F 6.35	164.04 <u>6.98</u> X	163.37		164.02		163.87	164.54 <u>9.32</u> X	164.54 <u>8.66</u> 6.05 C-2.61 Replaced C-1.8
1+60	164.59 <u>1.04</u> 7.45 F 6.41	164.59 <u>6.43</u> X	163.92		164.57		164.42	165.09 <u>8.77</u> X	165.09 <u>8.11</u> 5.80 C-2.81
1+40	165.19 <u>0.44</u> 6.91 F 6.47	165.19 <u>5.83</u> X	164.52		165.17		165.02	173.86 165.69 <u>8.17</u> X	165.69 <u>7.51</u> 3.70 C-3.81

BERYL
Kendall to Jewell

173.20 X
 $\frac{11.02}{162.18}$
 162.19
 B.M. 1/4 ↗ - .01 ↘
 $\frac{162.19}{3.44}$
 165.63 X

	Rough	cl.	gutter	1/4	±	1/4	gutter	cl.	Rough
E.L. Jewell 5+00	159.50				159.42				160.00
								End of cl. → 162.00	
								$\frac{11.20}{4.86}$ C-6.34	
Cl. B.C. 4+90	$\frac{165.63 X}{159.61}$ 6.02 11.57 F 5.45	159.61	158.94		159.59		159.44	160.11	$\frac{13.09}{4.86}$ C-8.23
4+47 5	$\frac{160.06}{5.57}$ 10.14 F 4.57								$\frac{173.20 X}{160.56}$ 12.64 4.75 C-7.89
		Rate	Rate		Rate		Rate	Rate	

BERYL
Jewell to Ingraham

L44

	Cl.	gutter	1/4	±	1/4	gutter	Cl.	Rough
3+00	160.11 150.94	150.27		150.92		150.77	151.44 8.09	151.44
	9.17 9.36 F0.19							
2+80	160.11 152.20	151.53		152.18		152.03	152.70 6.83	152.70
	7.91 8.11 F0.20							
2+60	160.11 153.25	152.58		153.23		153.08	153.75 5.78	153.75
	6.86 7.08 F0.22							
2+40	160.11 154.09	153.42		154.07		153.92	59.53 154.59 4.94	154.59
	6.02 6.18 F0.16							
2+20	154.74 154.74	154.07		154.72		154.57	59.53 155.24 4.29	155.24
		6.04 6.23 F0.19						
P.V.C. 2+00	160.11 155.17	154.50		155.15		155.00	59.53 155.67 3.86	155.67
	9.94 5.07 F0.13	5.61						

BERYL
Jewell to Ingraham

44

		Cl.	gutter	1/4	±	1/4	gutter	Cl.	Rough
3+00		160.11	150.27		150.92		150.77	151.44	151.44
		<u>150.94</u>						8.09	
		9.17							
		9.35							
		10.19							
2+80		160.11	151.53		152.18		152.03	152.70	152.70
		<u>152.20</u>						6.83	
		7.91							
		8.11							
		10.20							
2+60		160.11	152.58		153.23		153.08	153.75	153.75
		<u>153.25</u>						5.78	
		6.86							
		7.08							
		10.22							
2+40		160.11	153.42		154.07		153.92	154.59	154.59
		<u>154.09</u>						59.53	
		6.02						4.94	
		6.18							
		10.16							
2+20	154.74	160.11	154.07		154.72		154.57	155.24	155.24
		<u>154.09</u>						59.53	
		6.04						4.29	
		6.23							
		10.19							
P.V.C. 2+00	155.14	160.11	154.50		155.15		155.00	155.67	155.67
		<u>155.17</u>						59.53	
		9.94						3.86	
		5.07							
		10.13							

BERYL
Jewel II to Ingraham

✓45

	lb	quitter		1/4	2	1/4	quitter	lb	Rough
			X 146.54 13.04 ----- 133.50 2.02 ----- 135.48 0.05 ----- 135.47 13.00 ----- 148.47 52						
E.V.C. 4700	146.54 141.58	140.91			141.56		141.41	142.08 4.46 x	142.08
	A.96 DT100 ----- F 0.19	5.63 5.82 ----- F 0.19							
3780	143.86 2.68 2.91 ----- F 0.23	143.19	147.95 12.16 ----- 160.11		143.84		143.69	46.54 144.36 2.18 x	144.36
3760	145.93 0.61 DT100 ----- F 0.19	145.26 1.28 1.47 ----- F 0.19			145.91		145.76	TR. 146.43 13.10 x	146.43
3740	149.47 147.81 0.66 8.8 ----- F 0.22	147.14			147.79		147.64	148.31 11.22 x	148.31
3720	160.11 149.58	160.11 148.91	11.20 11.46 ----- F 0.26		149.46		149.31	149.98 9.55 x	149.98

BERYL

Jewell to Ingraham

✓46

Cl. Ingraham

cl. gutter

1/4

±

1/4

gutter

cl.

Rough

Cl. Ingraham

5+20±

127.70 127.25

128.06

127.96

128.70

6.82

5+08

128.70 128.03
6.82

128.68

128.53

129.20

129.20

6.52

So. Cl. + O.

5+03

129.30

Cl. B.C. on So.

5+01

129.53

Rate

4+54

Rate

Rate

Rate

135.04

135.64

JEWELL

El. of E.C. Alley

147

Chalcedony to L.A.W. 7455-L

	Rough	el.	gutter		1/4	±	1/4	gutter	el.	Rough
S. Line Alley 1+25	12220 122.00	122.63* 122.00	121.33	R.M.#5				121.83	122.50	122.50
	2.57 3.92	122.04 0.59 0.91		115.41 9.16					4.33	2.67 1.00
End Alley Cl. →	F1.35 122.00	F0.32 on 4' Rad.		124.57 1.19					Ext'd el. 0.20 High	C-1.01
Alley of B.C. 1+21	0.43 1.43 F1.00	stake 122.63 121.72	131.75 121.05	123.38 12.00 135.38				131.75 121.55 10.20		
		0.91	10.70	115.41 7.22 122.63						

INDEXED

WK

DEC 5 1949

0+86

119.31
5.26
4.93
C-0.33

3x383

0+483

116.63
7.94
8.76
F0.82

Rate

Rate

Rate

Rate

Rate

A-2'17.
119.81
4.76
4.05
C0.71

4'-0
117.13
7.44
6.02
C-1.42

ob. E.C.
0+10

124.57
113.95
10.62
11.18
F0.56

122.63
113.95
8.68
X

113.28

113.93

113.78

126.83
114.45
12.38
124.57
114.45
10.12
7.38
C-2.74

N.L. Chalcedony
0+00

#8
131.51
0.24
131.75

R.M.#5
115.41
11.42
126.83

Jewel
Chalcedony to Law

✓
48

	Rough	cl.	gutter-	1/4	1/2	1/4	gutter	cl.	Rough
2+30	128.58	128.58 6.80 6.98 -0.18	131.75x 127.91 3.84 x	126.83x 119 125.64 9.34 1349.8x	128.50		131.75x 128.41 3.34 x	129.08 5.90 x	129.08 6.70 3.63 C 2.67
2+10	127.61	127.61 7.77 7.92 -0.15	131.75x 126.94 4.81 x	127.59			131.75x 127.44 4.31 x	128.11 6.87 x	128.11 7.27 4.25 C 3.02
1+90	126.46	126.46 8.92 9.03 -0.11	131.75x 125.79 5.96 x	126.44			131.75x 126.29 5.46 x	134.98x 126.96 8.02 x	N. 0.5 in 126.96 8.42 5.83 C 2.59
1+70	125.15	125.15 10.23 10.35 -0.12	131.75x 124.48 7.27 x	125.13			131.75x 124.98 6.77 x	126.83x 125.65 1.18 x	N. 0.5 in St. 125.65 9.73 7.37 C 2.36
Alley of Ec. 1+49	123.60	123.60	131.75x 123.01 8.74 x				131.75x 123.51 8.24 x	124.18	
No. Line Alley 1+45	135.38x 123.40 11.98	123.40 1.17 1.20 -0.03	122.73				123.23	123.90 2.93 x	N. 0.5 in 4.5" up. 123.90 1.148 8.94 C 2.54 End Ch. 0.120 Higher

Rake

Jewel
Chalcedony to Law

	Rough	cl.	gutter	1/4	£	1/4	gutter	cl.	Rough
S. Line Law. 2+70	129.55		129.05		129.80				
cl. B.C. 2+60	129.32	$\begin{array}{r} 135.38x \\ 129.32 \\ \hline 6.06 \\ 5.96 \\ \hline C-0.10 \end{array}$	$\begin{array}{r} 131.75x \\ 128.87 \\ \hline 2.88 \end{array}$				$\begin{array}{r} 131.75x \\ 129.52 \\ \hline 2.23 \end{array}$	$\begin{array}{r} 130.20 \\ 4.78 \\ \hline 11.40 \\ 9.04 \\ \hline C-2.36 \end{array}$	x From P 31
2+50	129.10	$\begin{array}{r} 129.10 \\ 6.28 \\ 6.28 \\ \hline x \end{array}$	$\begin{array}{r} 131.75x \\ 128.70 \\ \hline 3.05 \\ x \end{array}$		$\begin{array}{r} 134.75x \\ 129.36 \\ \hline 5.42 \\ x \end{array}$		$\begin{array}{r} 131.75x \\ 129.22 \\ \hline 2.53 \end{array}$	$\begin{array}{r} 134.99 \\ 129.89 \\ \hline 5.09 \\ x \end{array}$	$\begin{array}{r} 129.89 \\ 5.49 \\ 3.10 \\ \hline C-2.39 \end{array}$

JEWELL

150

Law to Beryl

7455-L

1/4 ♀ 1/4 gutter cl. Rough

1+15

139.36 139.36 138.69

139.34

139.19

149.00x
139.86

139.86

INDEXED

4.03 4.03

135.39
3.89

9.14

3.53

WIK

DEC 5 1949

131.50

2.51

C1.02

11.89

143.39

0+95

137.78 137.78 137.11

137.76

137.61

149.00x
138.28

138.28

5.61
5.61
3.59
+0.04

10.72

5.11

3x 2

3.39

C1.73

C1.73

P.V.C.

0+75

136.39 136.39 135.72

136.37

136.22

149.00x
136.89

136.89

7.00
7.07
-0.07

12.11

6.50

3x 7

3.27

C1.73

C1.73

S.

0+42

x 325

134.27 134.27 133.56

134.30

134.10

149.00x
134.77

134.77

9.12
9.25
-0.13

14.23

8.62

5x 4

5.84

C-2.78

C-2.78

Cl. E.C.

0+10

132.15 132.15 131.39

132.23

131.98

149.00x
141.60
132.65

132.65

11.24
11.34
-0.10

8.95

4.97

C-3.98

N.L. Law

0+00

131.50

JEWELL

Law to Beryl

	Rough	Ch.	gutter		1/4	±	1/4	gutter	Ch.	Rough
1+55	143.07	143.07	142.40			143.05		142.90	149.05 143.57	155.62X 143.57
		0.31 0.38 -0.07		143.39X 0.35 143.04 12.58 155.62X					5.43 x	1205 9.44 C-2.51
Alley of E.C. 1+49	142.48	142.48	141.81		132.33 11.57 143.90X 37 144.23 Sub. Ch. T			142.31	142.98	
N.L. Alley 1+45	142.09	142.09	141.42		135.65 Ch. M. 11.57 147.22X 0.3 147.55 Sub. Ch. T			141.92	149.00X 142.59	142.59 1303 10.00 C-3.03
E Alley 1+35 (prop 140.75)			140.45			141.10		140.95		(146.31 Prop)
S.L. Alley 1+25	140.24	140.24	139.57					140.07	147.00X 140.74	143.59X 140.74
		3.15 3.26 -0.11							3.26 3.26	2.65 2.26 C-0.39
Alley of B.C. 1+21	140.24	139.89	139.22					139.72	140.39	

JEWELL
Law to Beryl

	Rough	cl.	quitter		1/4	±	1/4	quitter	cl.	Rough
S.L. Beryl. 2+70	156.50		155.83	$\begin{array}{r} 155.62 \\ 0.43 \\ \hline 155.19 \\ 10.60 \\ \hline 165.79 \\ 360 \\ \hline 162.19 \\ = B.M. \\ \text{Top Hyd.} \\ \text{Beryl} \\ \text{+ Jewell} \end{array}$		156.65		156.33		157.00
cl. B.C. 2+60	155.30	155.30	154.63		155.28		155.113	$\begin{array}{r} 160.13 \\ 155.80 \\ 4.33 \\ \hline \end{array}$	$\begin{array}{r} 155.62 \\ 155.80 \\ -0.18 \\ 2.92 \\ \hline F 3.10 \end{array}$	
2+27E	151.40	151.40	150.99				$\begin{array}{r} 160.13 \\ 151.90 \\ 8.23 \\ \hline \end{array}$	$\begin{array}{r} 151.90 \\ 3.72 \\ 5.32 \\ \hline F 1.60 \end{array}$		
1+95 ^{ENC}	147.50	147.50	146.83		147.48		147.33	$\begin{array}{r} 160.13 \\ 148.00 \\ 12.13 \\ \hline \end{array}$	$\begin{array}{r} 148.00 \\ 7.62 \\ 6.89 \\ \hline C 0.73 \end{array}$	
1+75	145.19	$\begin{array}{r} 155.62 \\ 145.19 \\ 10.43 \\ 10.50 \\ \hline -0.07 \end{array}$	144.52	$\begin{array}{r} 218 \\ 157.87 \\ 226 \\ \hline 160.13 \\ 12.13 \\ \hline 148.00 \\ 1.00 \\ \hline 149.00 \end{array}$	145.17		145.02	$\begin{array}{r} 149.00 \\ 145.69 \\ 3.31 \\ \hline \end{array}$	$\begin{array}{r} 155.62 \\ 145.69 \\ 9.93 \\ 9.47 \\ \hline C 0.46 \end{array}$	

INDEXED

WK

DEC 5 1940

CHALCEDONY

Kendall

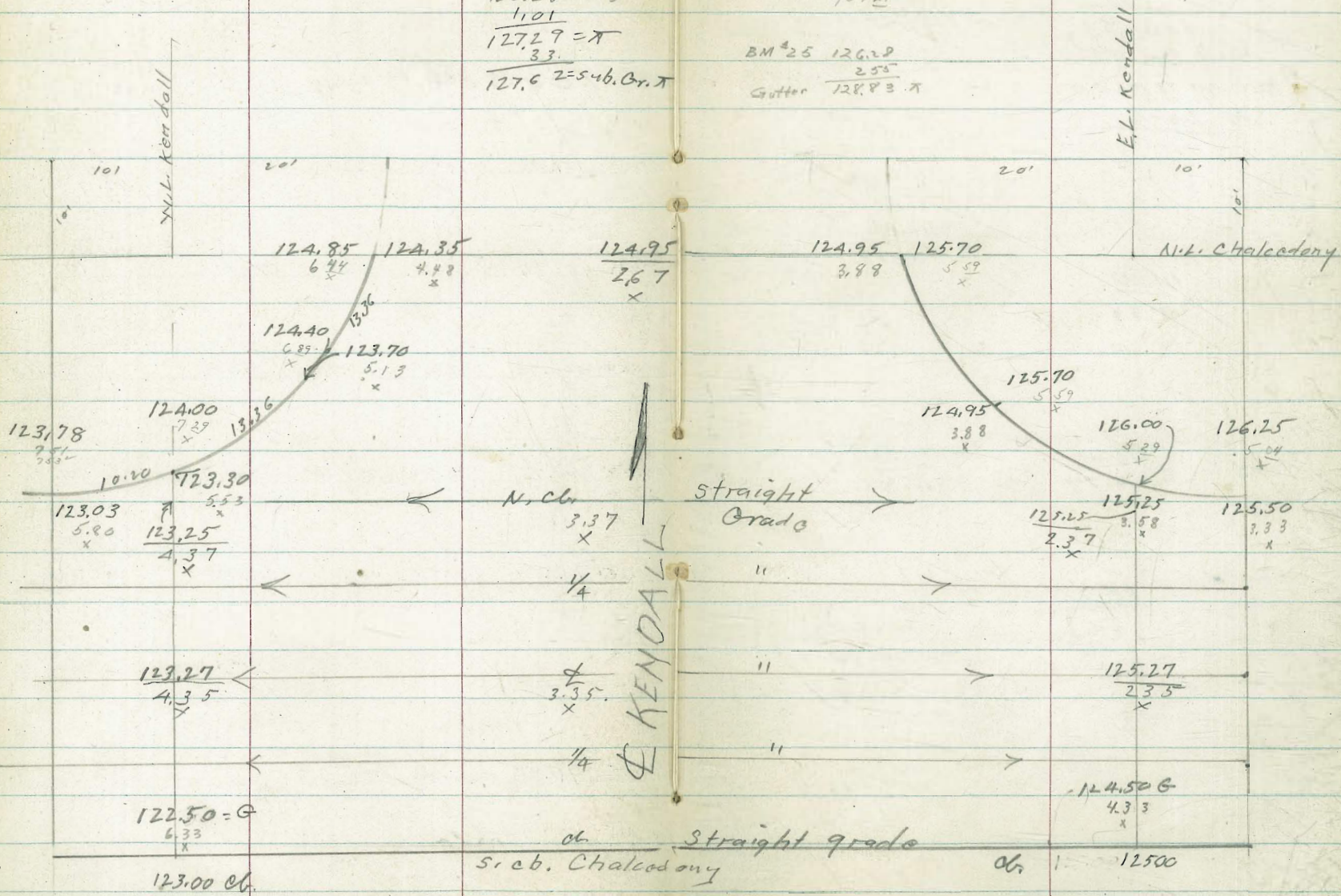
7447-L

155

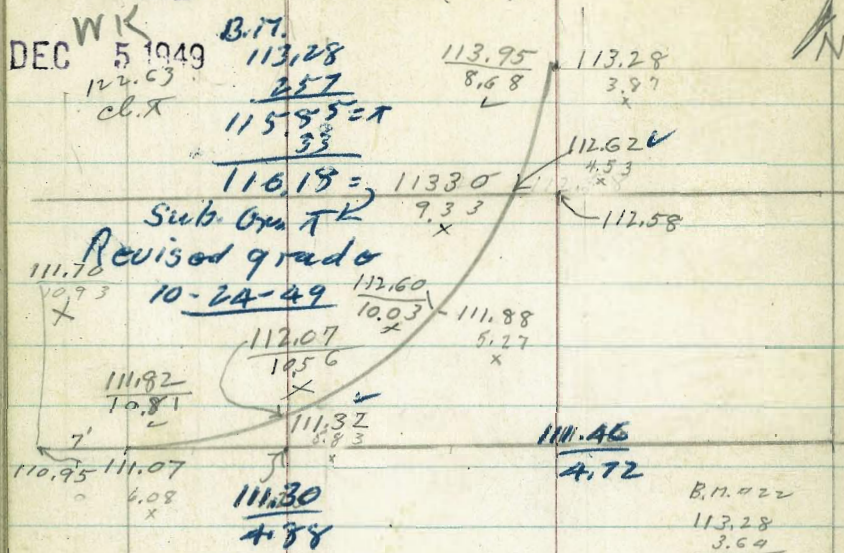
126.29 BM #5
 $\frac{1.01}{127.29} = X$
 $\frac{33}{127.62} = 546.0r.T$

BM #K 128.24
 $\frac{2.27}{131.29}$
 Curb - HI

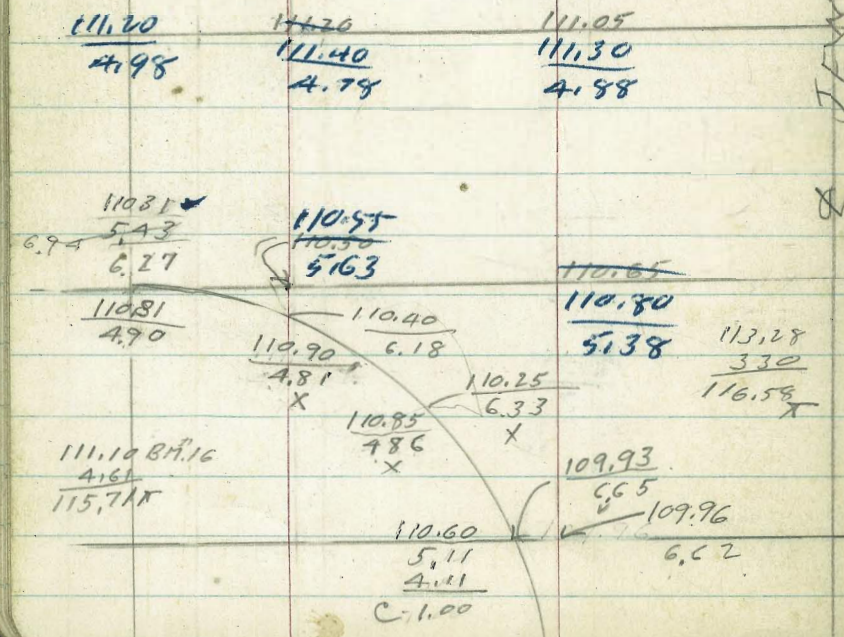
BM #25 126.29
 $\frac{2.55}{128.83} = X$
 Gutter



INDEXED CHALCEDONY + Jewell

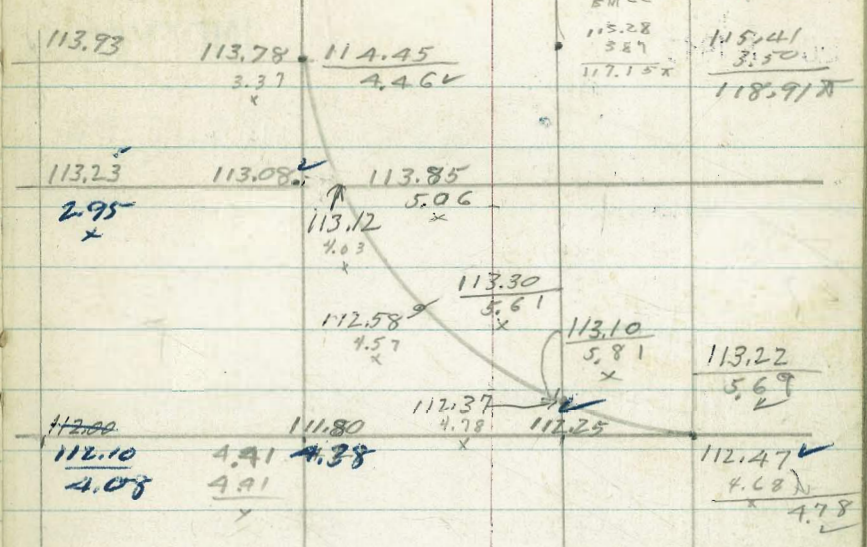


B.M. 422
 113.28
 3.64
 116.92
 33
 117.25
 Sub. Ort X

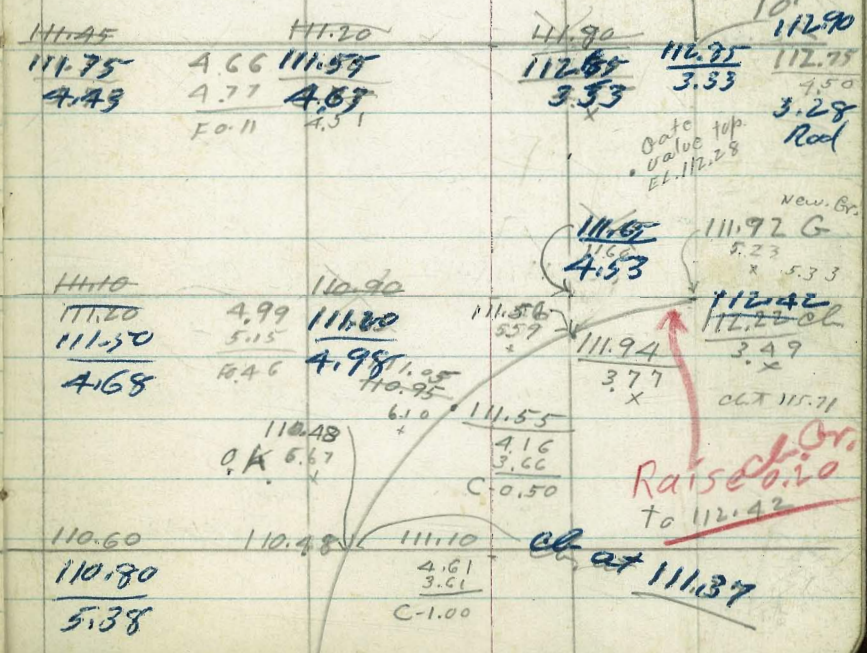


JEWELL

7446-L



56
 F.M. 22
 115.28
 3.87
 117.15 X
 115.41
 3.50
 118.91 X



date value top
 EL. 112.28

Raised Br.
 to 112.42
 cl. at 111.37

LAW + HAINES

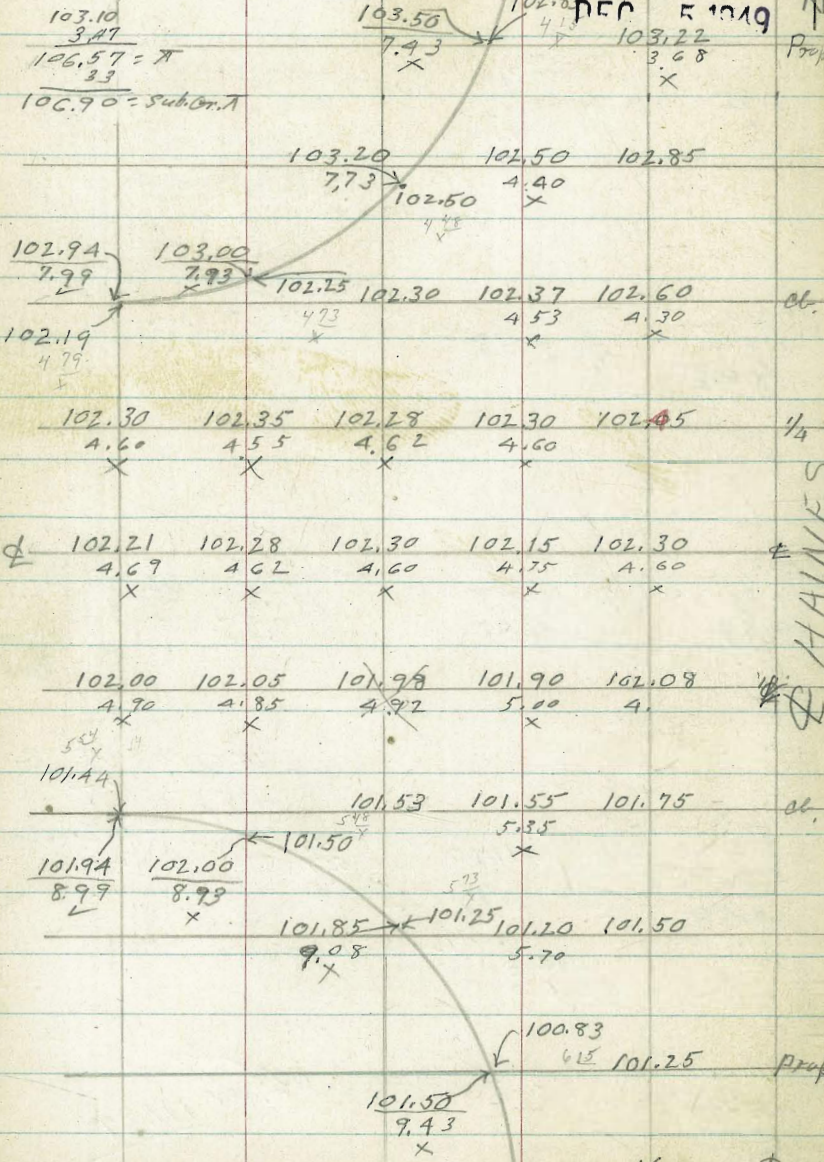
Rad. Prop.

cb. $\pi = 110.93$

INDEXED

DEC 5 1949

Prop.



Rad. Prop.

cb.

1/4

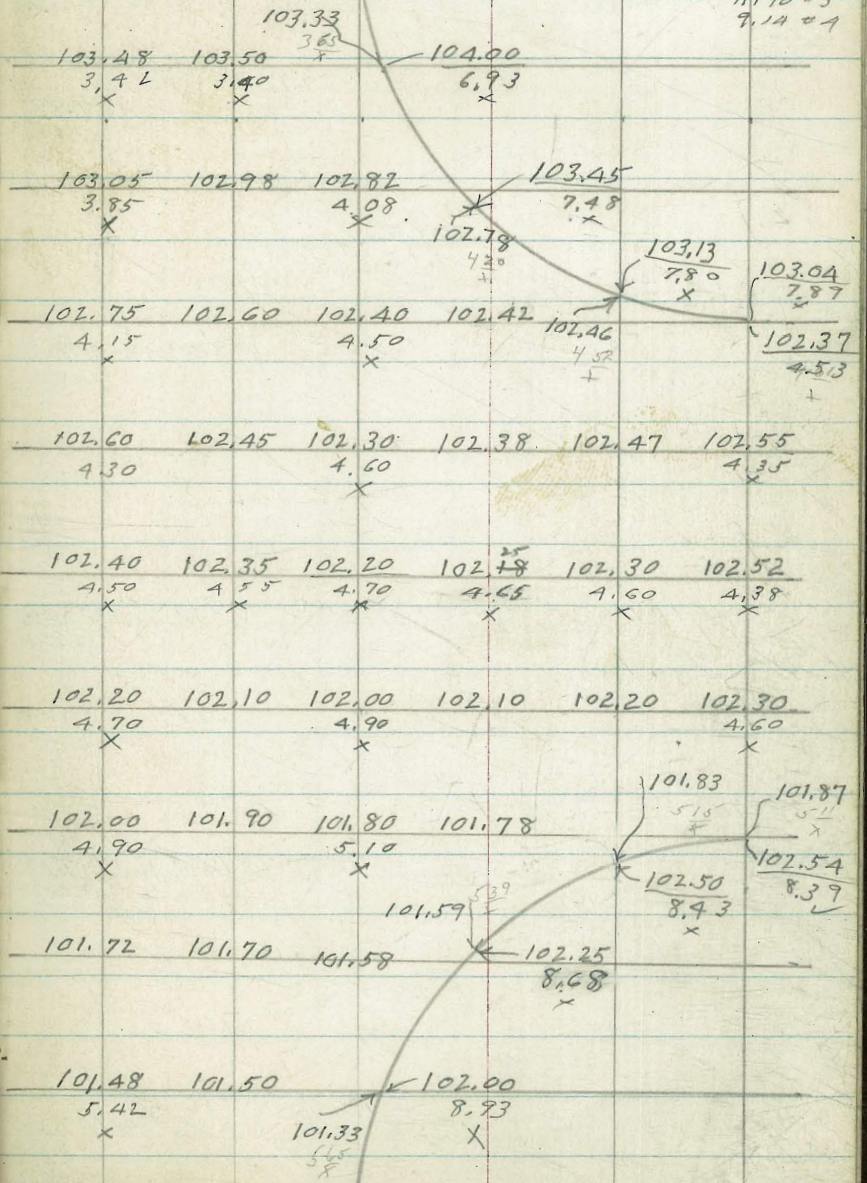
Prop.

BM # 12 105.29
106.90 1/4
106.90 1/4

7449-L Prop.

157 Rad.

Chords - 27' Rad. = 9.14 #1
11.70 #2
11.70 #3
9.14 #4



Prop.

1/4

cb.

Prop.

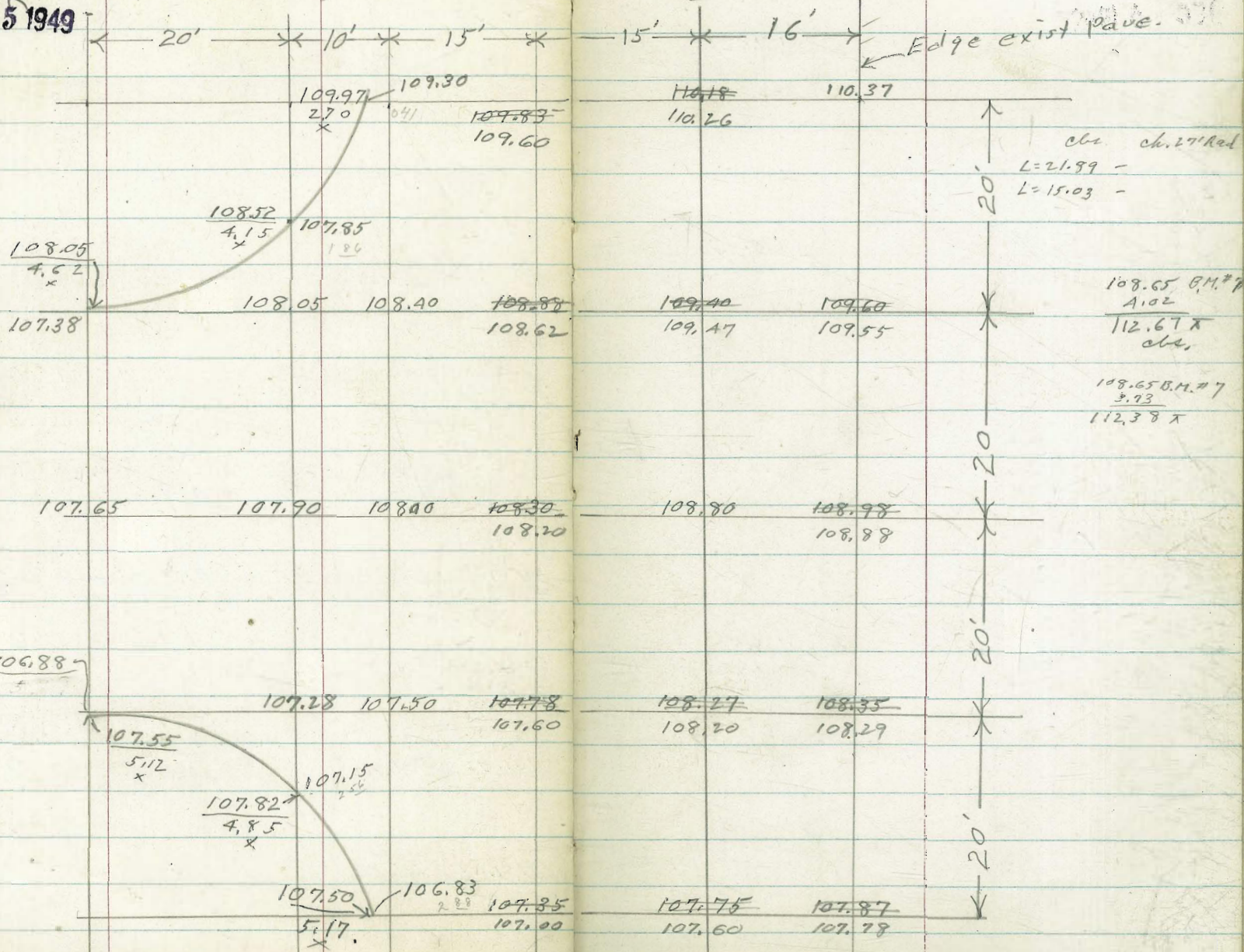
Rad.

INDEXED

DEC 5 1949

LAW + Ingraham
(7449-L)

13358



INDEXED

LAW & JEWELL

DEC WK
1919

BM #27

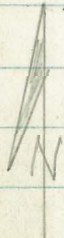
132.33

2.12

134.45 - 7

33

134.78 = sub. On. T.



LAW ST.

132.33 B.M. #27

6.77

139.10

4.10

134.90

3.63

138.03

131.39

131.02

3.43 Paul

130.43

4.02 Paul

129.98

4.47 Paul

129.55

4.90 Paul

129.05

5.40 Paul

Jewell

132.23

2.55

X

131.80

2.98

X

131.20

3.58

X

130.70

4.08

X

130.25

4.53

X

129.80

4.98

X

131.98

3.84

X

131.45

4.37

4.30

X

131.48

131.00

3.78

X

130.65

4.13

X

130.30

4.48

X

129.80

6.01

X

129.53

6.29

X

132.65

5.91

X

132.12

6.34

X

131.15

4.67

X

131.30

4.52

X

130.72

3.25

X

130.80

7.66

X

130.45

8.01

X

130.20

8.26

X

L 7455

#8

131.51

6.95

cb = 138.46

59

cut to 135.82

131.82

6.64

X

132.00

6.46

X

132.29

6.17

X

131.33

4.20

X

131.62

4.20

X

10'

132.04

2.78

X

130.57

3.25

X

131.00

4.82

X

131.12

7.34

X

131.50

6.96

X

130.20

5.62

X

130.80

7.66

X

Butler
138.03 From P. 59

LAW & KENDALL

INDEXED
WK
DEC 5 1949

21.28 135.65
122
136.87
33
137.20
60
Prop. B.C. Sub. Ch. T.

B.C. Prop. 135.75 135.08 1/4 135.50
395 2.75 1.70
X X X

134.70 134.05 134.50
5.00 3.15 2.70
X X X

134.02 134.03
5.68 4.00
X X

133.84 133.20 133.30 133.70
5.55 4.00 3.90 3.50
X X X X

133.17 133.35
4.86 4.68
X X

133.17 133.15 133.10 133.05 133.40
4.03 4.05 4.10 4.15 3.80
X X X X X

133.22 133.10 133.00 132.95 133.25
3.98 4.10 4.20 4.25 3.95
X X X X X

132.90 132.76 132.63 132.65 133.00
4.30 4.44 4.57 4.55 4.20
X X X X X

132.47 132.35 132.30 132.80 133.10
5.56 4.85 4.90 4.40 4.10
X X X X X

133.14 133.05 132.23
5.32 5.65 5.80
X X X

B.M. #9 132.18 132.60 132.90
138.93 5.02 4.60 4.30
+ 0.47 5.56
138.45 X X X

Prop. 132.90 132.03 132.40 132.80
5.76 6.00 4.80 4.40
X X X X

Kendall

1/4 135.83 136.50
2.20 3.20
135.80 1.40
X X

135.36 134.85 134.90 134.80
1.84 2.35 2.30 2.40
X X X X

135.60 134.93
4.10 3.10
X X

135.20 135.54
4.50 2.16
X 2.49

134.15 134.15 134.15
3.05 3.50
X X

134.87
3.10
2.33

133.75 133.72 133.60 134.10 134.75 135.00
3.45 3.48 3.60 3.10 2.45 2.20
X X X X X X

133.50 133.50 133.30 133.75 134.38 135.00
3.70 3.70 3.70 3.45 2.82 2.20
2.58 X X X X X

133.25 133.10 133.15 133.52 134.05 134.80
3.95 4.10 4.05 3.68 3.15 2.40
X X X X X X

133.05 133.00 133.37 133.33 134.00
4.15 4.20 3.83 4.70 4.46
X X X X X

132.90 132.98 134.55 135.06
4.30 4.22 4.15 3.91 3.40
X X X X X

132.70 133.65
4.50 4.81
X X

132.98
5.05
3.4

B.M. 419

170.72
276
173.48X

BERYL + KENDALL INDEXED

DEC 5 1949

172.50 171.85
0.98 354
2.48 1.98
F 1.50

172.30
1.33

170.95 170.90
2.53 2.73
170.20 3.19
170.10 169.40

171.45
2.18

173.86
169.73
4.23
169.06
6.23
X

170.00 170.23
3.43 3.40
X X

170.75
2.88
X

169.20
4.43
X

169.90 170.07
3.73 3.56
X X

170.50
3.13

< 8' X 10' X 7' X 18' X 15' X

169.23 169.50 169.95 170.10
4.40 4.13 3.78 3.53
X X X X

170.40
3.23
X

X 10' X 20' X X X

169.25 169.58
4.38 4.05
X X

170.05 170.15
3.58 3.48
X X

168.83
6.59
169.50
3.98

168.80 169.40
6.59 4.08
X X
5.99

169.45
4.18
X

168.70 168.15
4.78 7.24
6.59 X

167.45 166.95
6.03 8.44
7.94 X

20'

Kendall to So.

7454-L

174.69X
3.05
171.64
TOP of pit

171.64 218
5.14
174.78 62 B.C.
171.64 419
173.86 Bpt.

172.00 172.62X
3.39 172.52
X 0.12

171.237
2.40

171.35 1.27
171.35
3.43 1.93
170.60
4.79 2.15
out

170.65
2.98
X

170.00 170.68
4.10 X

170.36 170.00
4.33 170.10
169.69 169.33
5.70 6.06
3.97

169.95
169.74
5.65 0.6
169.07
4.56
Raised 0.17

170.30
3.33
X

169.68 169.50 169.17
3.95 4.13 4.46
X X 4.28
1/4 Raised

3' X 17" X 8' X 12' X 10'

170.30 169.90 169.75 169.48 169.26
3.55 3.73 3.88 4.15 4.37
X X X 4.08 4.27
X 4.007 24 - Raised
0.10

X 20' X 20' X 10' X

170.00
3.63
X

169.60
4.03
X

169.20
4.43
X

169.05
4.58
1/4

169.53
4.10
X

169.35
4.28
X

168.70
6.69
X

168.61
6.78 0.6
169.29

169.25 169.30
3.14 4.18
X X
168.82
4.66
X

5.10
4.19
6.10

167.55
6.08

167.25
8.14
X

167.80
5.68
X
7.59

170.34 B.M.
29c
173.30 = X P.
33
173.63 = sub. Bpt

20'

B.C.

INDEXED

WK

DEC 5 1949

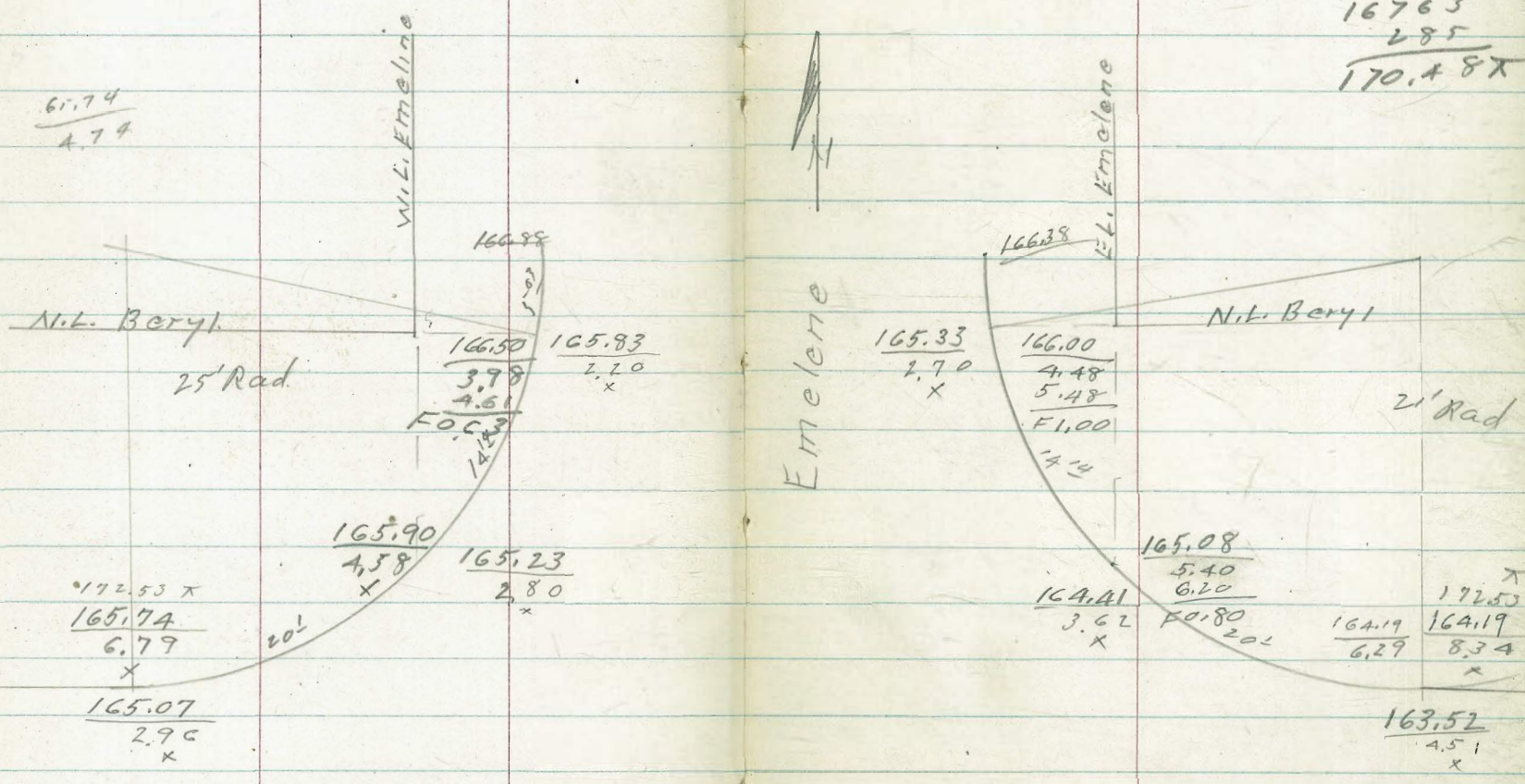
BERYL + EMELENE

7454L

63

$\begin{array}{r} 174.69 \\ \times P.62 \\ 4.33 \\ \hline 17036 \\ 217 \\ \hline 17253 \end{array}$

$\begin{array}{r} \times P.62 \ 174.78 \\ 7.15 \\ \hline 16763 \\ 285 \\ \hline 170.48 \times \end{array}$



Beryl St.

Ingraham & Chalcedony
 10' 10' 10'

Grade change 10/21/49 64

See p. 5A for ch. returns

102.93 BM#23
 2.34
 105.27 X
 33
 105.60 = Sub. Cr. X

10065	10106	10166
495	454	394
395	354	294
	3.65	3.11
	F0.11	F0.27

102.05	102.09	101.98
3.55	5.36	5.47
285	5.50	5.72
	F0.14	F0.35

101.70-50+
 102.93 = B.M. #23
 3.90
 106.63 = X
 23
 106.96 = Sub. Cr. X

102.93
 4.52
 107.45 = Fin. HZ

INDEXED

DEC 5 1949

99.23	99.98	99.90	100.34	101.00
6.37	5.62	5.70	5.26	4.60
5.37	4.62	4.70	4.26	3.60
	4.83	4.73	4.30	3.69
	F0.21	F0.03	F0.04	F0.09
99.37	99.80	99.70	100.13	100.75
6.23	5.80	5.90	5.47	4.85
5.23	4.80	4.90	4.47	3.85
5.31	4.98	4.97	4.52	3.95
F0.08	F0.18	F0.07	F0.05	F0.10
99.26	99.60	99.50	99.90	100.52
6.34	6.00	6.10	5.70	5.08
5.34	5.00	5.10	4.70	4.08
5.42	5.17	5.17	4.76	4.22
F0.08	F0.17	F0.07	F0.06	F0.14
98.92	99.40	99.30	99.62	100.26
6.68	6.20	6.30	5.98	5.34
5.68	5.20	5.30	4.98	4.24
5.72	5.47	5.34	5.02	4.49
F0.04	F0.27	F0.04	F0.04	F0.15
98.48	99.20	99.10	99.45	100.00
7.12	6.40	6.50	6.15	5.60
	5.40	5.50	5.15	5.60
	5.64	5.53	5.21	5.73
102.93 = BM 23	F0.24	F0.03	F0.06	F0.13
167				
104.60 = X				

1mk = Finish Cr.

101.55	101.63	101.50	101.30	101.45	102.12
4.05	5.33	5.46	5.66	5.51	5.33
3.67	5.87	5.95	6.25	6.00	
3.05	6.06	6.10	6.26	6.00	
3.01	F0.24	F0.15	F0.11	Grade	
3.04					
1.28	101.35	101.25	101.00	101.40	102.30
1.32	5.61	5.71	5.96	5.56	
1.90	6.10	X	6.45	6.05	F0.10
1.42	6.27	6.35	6.48	6.16	
1.32	F0.17	F0.15	F0.08	F0.11	
1.09					
1.04	101.12	101.00	100.80	101.08	102.10
4.56	5.84	5.96	6.16	5.88	
4.13	6.33	X	X	6.37	
0.43	6.51	6.58	6.71	6.37	
3.96	F0.18	F0.13	F0.06	Grade	
3.47					
3.09					
6.78	100.88	100.75	100.60	100.92	101.80
4.82	6.08	6.21	6.36	6.04	
4.38	X	X	X	6.53	
4.44	6.57	6.70	6.85	6.64	
4.82	6.75	6.83	6.98	6.64	
3.25	F0.18	F0.13	F0.13	F0.11	
6.10					
100.53	100.64	100.50	100.40	100.70	101.34
5.07	6.32	6.46	6.56	6.22	
4.64	X	X	X	6.75	
4.43	6.81	6.95	7.05	6.88	
4.07	7.00	7.07	7.10	6.88	
3.98	F0.19	F0.12	F0.05	F0.13	
20.09					

98.96	99.02	99.57
6.64	6.58	6.03
	5.58	5.03

100.05	100.15	100.04	100.25
5.55	7.30	7.41	
4.55			

Law + Kendall

INDEXED

DEC^{WK} 5 1949

Ch. E.C. →

④ 136.10

⑧ 135.66

⑭

Ch. E.C.

Prop.

135.66
3.96
x

Prop.

①
133.20
6.42

⑤ 133.00
6.62
x

⑩ 133.70
5.92
x

⑮
134.25
5.37
x

⑲
135.00
4.62

② 133.10
133.25
6.57
x
6.52
x

⑥ 132.80
6.82
x

⑪ 133.20
6.42
5.00
11.42

⑯
133.80
5.92
x

⑳
135.20
4.42
x

③ 132.50
7.10

⑦ 132.35
7.27
x

⑫ 132.70
6.92
x

⑰
133.70
5.92
x

㉑
134.60
5.02

Emp.

132.03
7.59
x

132.80
6.82

132.98
6.64

Prop.

13

131.80

13 132.20

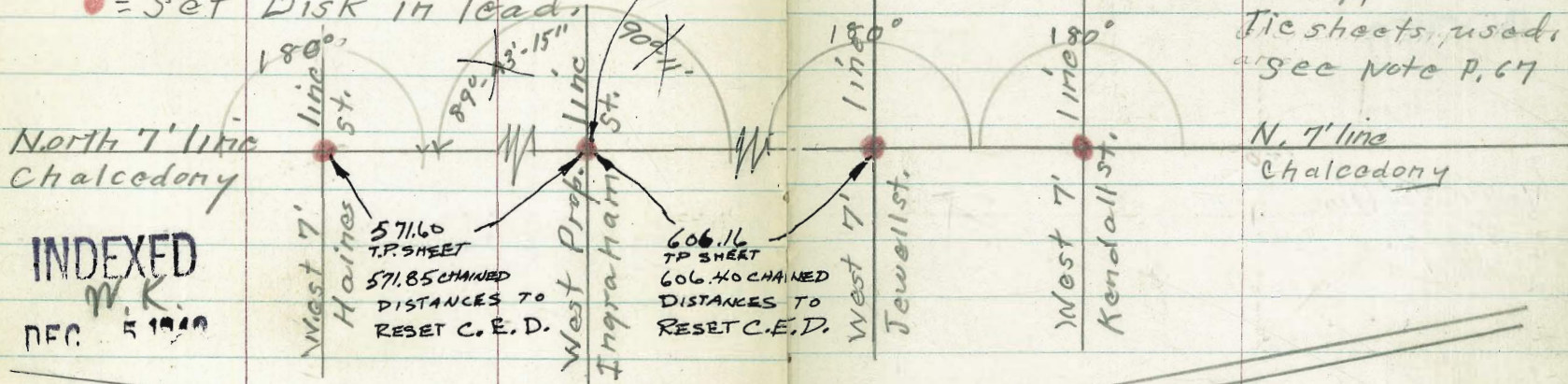
Tie Points set on
Chalcedony - Law

(FD)

11/22/49
Sommermeier

• = set Disk in lead.

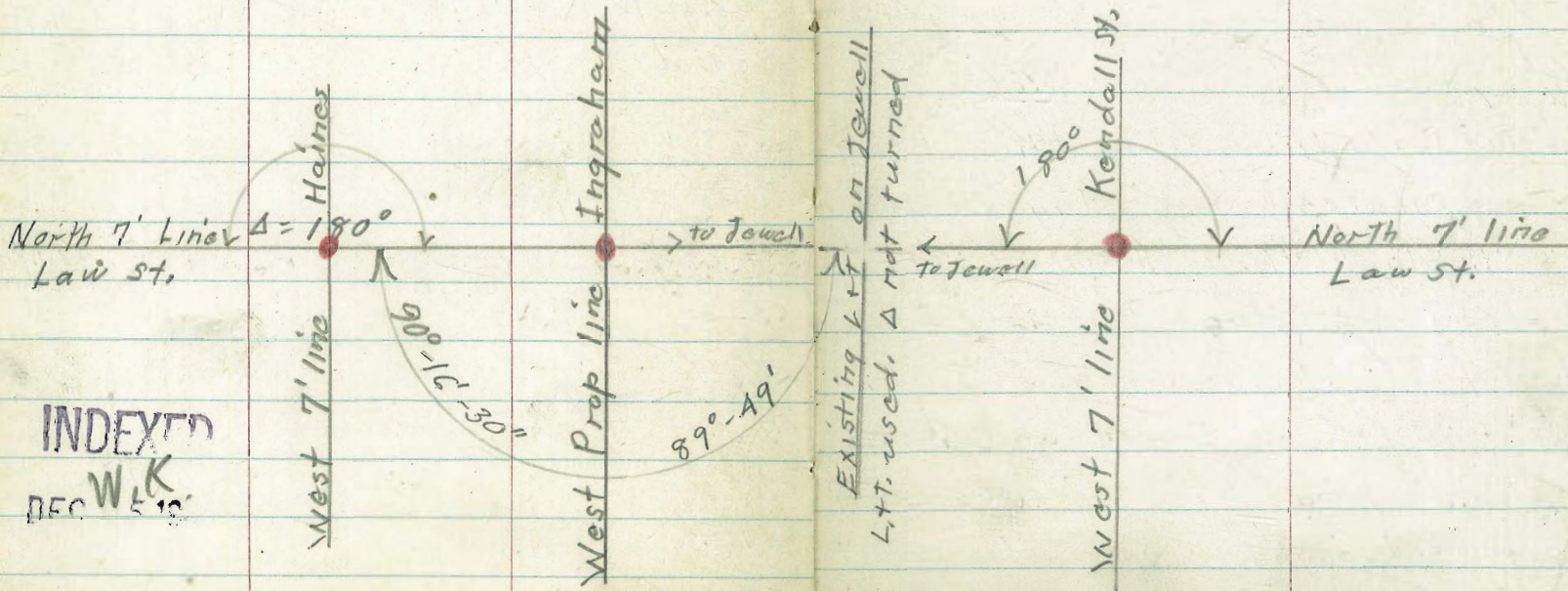
IN ERROR BY 1.00'
WAS MOVED TO FIT DESCRIPTION.
5-4-73 BJR



Existing points on
Tie sheets, used
see Note P. 67

N. 7' line
Chalcedony

INDEXED
W.K.
DEC 5 1949



INDEXED
W.K.
DEC 5 1949

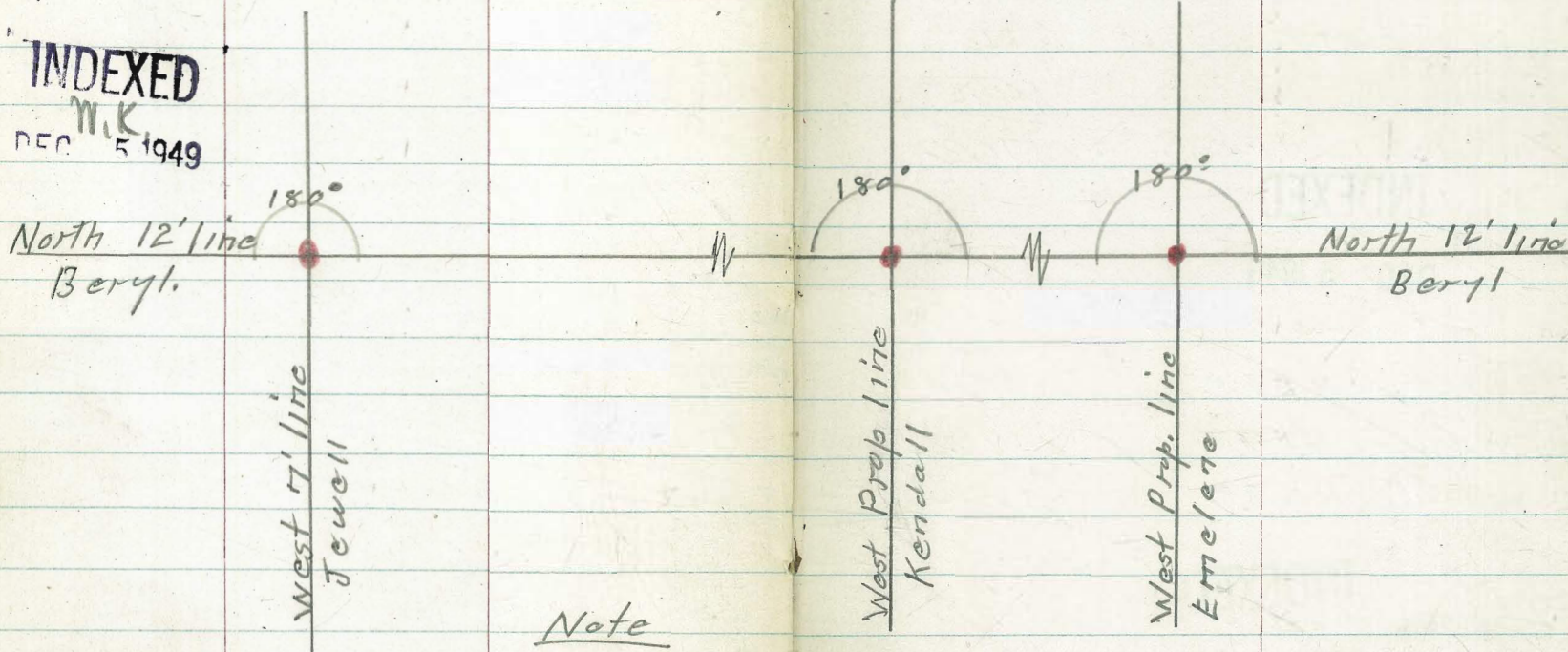
Tie points set on
Beryl St.

(FR)

11/24/49 67
Sommermeyer

INDEXED

M.K.
DEC 5 1949



Note

North & South lines plug thru from Beryl to Chalcedony.
 Law & Chalcedony plug thru Gresham to Ingraham. Δ at Ingraham.
 " St. plugs thru Jewell St. to Lamont.
 Chalcedony plugs thru - Ingraham to Lamont.
 Beryl St. plugs thru - Ingraham to Lamont.
 Existing Lt^s on Jewell and Beryl are o.k. as shown.
 Used existing Lt^s on Gresham at Law & at Chalcedony
 Used existing Lt^s on Lamont at Law - Chalcedony & Beryl.
 used existing Lt^s on Law St. at Jewell

Benches Set, ~~ORIF~~
 These benches run from Diamond + Gresham
 (These benches also shown on pages 78 to 80)

Beryl St.		EL.:
Jewell -	N.E. B.P.	160.15
Kendall	N.E. B.P.	170.34

INDEXED

 WK
 DEC 5 1949

Law St.

Haines	N.E. B.P.	103.10
Jewell	N.E. B.P.	132.33
Kendall	N.E. B.P.	135.65

INDEXED

 WK
 DEC 5 1949
 Chalcedony

Gresham	N.E. B.P.	89.82
Haines	N.E. B.P.	92.58
Ingraham	N.E. B.P.	102.93
Jewell	N.E. B.P.	113.28
Kendall	N.E. B.P.	126.28

INDEXED

 WK
 DEC 5 1949

INDEXED

W.K.

DEC 5 1949

Transfer B.M.s To Bench Plugs.

78

BM#12 to NEBP Law + Haines

$$\begin{array}{r} 105.22 \text{ BM\#12} \\ 1.67 \\ \hline 106.98 \text{ H} \\ 5.68 \\ \hline 103.10 \text{ Elv} \\ = \text{B.M. \#21} \end{array}$$

Set N.E.B.P.

Chalcedony + Jewell

3.50

113.28 = B.M.#22

5.68 116.78

111.0 B.M.#16-P80

Set NEBP

Chalcedony + Ingraham

6.50

102.93 = BM#23

0.72 109.43

108.65 = #7

Set N.E.B.P.

Chalcedony + Haines

4.19

92.58 = BM#24

2.36 96.77

94.41 #13

Set NE.B.P.

Chalcedony + Kendall

2.55

126.28 = BM#25

0.48 128.83

128.35 #19

N.E.B.P.

Gresham + Chalcedony

3.72

89.82 = B.M.#26

4.20 93.54

89.34 B.M.#1

Set N.E.B.P.

Gresham + Law

0.94

100.26

BM.#26

11.38

101.20

89.82

Set. ~~B.P.~~ Beryl

N.E.B.P. + Jewell

3.63

160.15

= B.M.#30

5.91 163.78

157.87

B.M.#18A

N.E.B.P. Beryl

+ Kendall

5.05

= B.M.#29

170.34

B.M.#19

4.67

175.39

170.72

Set N.E.B.P.

Law + Kendall = B.M.#28

2.38

135.65

X from P.59

138.03

Set N.E.B.P.

Law + Jewell = B.M.#27

3.49

132.33

B.M.#8

P.80

4.31

135.82

131.51

INDEXED
W.K.
DEC 5 1949

Set B.M. s.w. Beryl & Jewell
7x14⁵ Cross in 26. 4.78 157.87 = B.M. #18A

0.46 162.65 162.49 B.M. #14

Back walk. N.E. by B.C.
set. 15' Radi. Ref. 190 170.72 = B.M. #19

B.M. #18 0.98 172.62 — 171.64

Benchmarks Beryl St. 79

Beryl.

Jewell Top, S.E. Fire Hydr. (P.52) ~~B.M. #1A~~
162.19

Lamont N.W. L & T. (P.35) 162.02 #17

Kendall Top, S.E. Hydr. (P.62) taken out #18
11/2/49 171.64 #1

INDEXED

W.K.
DEC 5 1949

Benches Set
Levels in G259-P23

INDEXED
W.L.
DEC 5 1949

set 7x1	Chalcedony		
	At Grestham	N.W. 7' L+T.	89.34 = #1
	Fanuel	N.E. "	85.26 = #2
sc	Everts	N.E. "	179.11 = #3
	Ingraham	S.E. "	101.54 = #4
	Jewell	S.E. Fire Hydt	115.41 = #5
	Haines	Top. Fire Hydt.	94.41 = #13
	Kendall	" " (P. 9)	128.35 #15
	Jewell	(L+T. on S. 7') S.W. 3' Tie Back	111.10 #16
		Law. St	
	at Ingraham	S.E. 7' L+T.	108.65 = #7
	Jewell	Top S.W. Fire Hydt.	131.51 = #8
	Kendall (P. 24)	Top S.E. " "	138.93 #9
	Lamont. (P. 24)	N.W. 7' L+T.	143.10 #10
	Grestham (opposite page)	S.E. 7' L+T.	98.68 = #11
	Haines	Top Hydt.	105.29 #12
	Law. (P. 25)	N.W. 7' L+T.	
	Beryl.		
	P. 79		

80

89.34 = B.M. #1
 $\begin{array}{r} 12.00 \\ 101.34 \\ \underline{2.66} \\ 98.68 = \text{set. B.M. #11} \end{array}$

41-50
 $\begin{array}{r} 28.40 \\ \underline{70.30} \end{array}$

115.41 = B.M. #5
 $\begin{array}{r} 0.33 \\ 115.74 \pi \\ \underline{4.64} \\ 111.10 \\ 115.74 \pi \end{array}$

126.01 S.W. L 47 - Lamont &
Chalcedony

Set
7x1



101120
9868
25.2

90.64
75
89.89

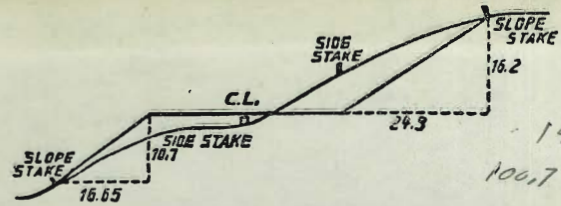
12
3
15.1
36

11.5

74
47
27

92.5
69.7
2.8
99.50
100.90
200.30
100.10

99.80
100.80
204.30
100.15
99
199.90
99.95



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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