

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

31.46

18A1

13.05

12.53

15.2

INDEXED
Completely

MICROFILMED

APR 13 1965

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Friday - Cont. P. 81
Grades

1

Oliver (Gresham to Farnel) 2-5
 Alley between "Oliver" + P.B. Drive 6-7 ✓
 " BIK 12 + 19 O.B. Park 8 to 13 ✓
 " " 70 Ocean Beach 9 + 14 to 18 ✓
 Storm Drain Proctor Pl. 19
 Beryl, INGRAHAM TO JEWELL Paving 20
 Dalbergia Una to Woden 24
 Landi's Laimant to Arizona to Arnold 27
 Diamond Marrell 28
 Euclid Hilltop to 51 34
 Between Cape May + Saratoga - Alley BIK. 55. O.B. Summit cliffs to Cable 35 ✓
 Drain BIK. 192 Univ. Hqts 37
 Haines - Missouri to Law } Drainage
 Jewell - Chalcedony to 125'so. }
 Kendall - Chalcedony to Law } 39 + 40
 ANNA + PACIFIC - ELY. Sewer Thru P.L. 272 49-50
 Witherby Underpass drain 51
 SCOTT ST. South of Lo well 52
 Pump houses } (Bird Rock LaJolla Hermosa Cravilla St) 54-56
 Alley BIK 59. Univ. Hqts 57-58 ✓
 Ties Redondo St. + P.L. # } 59
 Wild wood sub

See 1903 for Tie outs
42

Oliver St. Gresham to Farnel

South

7-20-49

N.O. 31472 (2)

INDEXED
MK
SEP 6 1950

So. Prop. Rough Cr.	Curb	Gutter	So. 1/4
32.47x 26.61 5.86 5.93 A-0.07	26.61 3.65 x	25.94 6.00	
x ²² mark 30.87x 26.38 4.49 4.09 C 0.40	26.38 3.88 x	25.71 6.23	
26.08 4.79 4.148 C 0.31	26.08 4.18 x	25.41 6.53	
		25.00 6.74	
25.25 5.62 4.62 C-1.00	25.25 5.01 x	24.58 7.36	
25.07 5.80 4.98 C 0.82	25.07 5.19 x	24.40 7.54	

date 7/27/49 Sommermayer
McCoy
Allen
W Moore 2

North

North Prop.	Gutter	Cl.	North Prop.
26.75 26.75 5.19 2.71 x	26.75 5.19	27.55	32.47x 27.55 4.72 4.47 C 0.45
26.52 26.19 5.75	26.52 5.42	27.32 29.4 x	30.87x 27.32 3.55 2.87 C-0.68
26.22 25.89 6.05	26.23 5.71	27.03 3.23 x	30.87 27.03 3.84 2.89 C 0.35 C 0.95
25.85 25.52 6.72	25.82 6.12		BM # 1 21.17 9.07 302.6x 3.65 2.661 4.00 30.61x
25.33 25.00 6.94	25.40 6.54	26.20 4.06 x	26.20 4.67 3.26 C-1.41
25.10 24.77 7.17	25.27 6.67	26.07 4.19 x	26.07 4.80 3.146 C-1.34

3194

B.M. # 1
N.W. B.P.
P-B Drive
Gresham
21.19
9.68
308.7x
2.87
28.00
4.47
324.7x
11.48
209.9=
G.I. B.P.
Farnel +
Oliver

Note: See
Margin # 3
for H.I.
on curb cuts
& Grade

Oliver Street

8/19/49
For Gutters
& Grades

South

North

	Prop.	Cl.	Gutter	1/4	±	1/4	Gutter	Cl.	Prop.	NW BR BM #1 PB. Drive Graham 21.19 + 9.19 30.38 - 2.72 27.66 + 4.28 31.94
2+20	26.46 6.01 5.80 C 0.21	26.46 4.15 x	25.79 6.13 ✓		26.59 .33 26.26 5.68 ✓		26.57 5.37	27.37 3.24 x C 0.35	27.37 5.10 4.75 C 0.35	
2+00	26.66 5.81 5.61 C 0.20	26.66 3.95 x	25.99 5.95 ✓		26.79 .33 26.46 5.78 ✓		26.78 5.16	27.58 3.03 x C 0.49	27.58 4.89 4.40 C 0.49	
1+80	26.79 5.68 5.57 C 0.41	26.79 3.82 x	26.12 5.82 ✓		26.93 .33 26.60 5.37 ✓		26.93 5.01	27.73 2.88 x C 0.73	27.73 4.74 4.01 C 0.73	
1+60	X in Drive 26.85 5.62 5.54 C 0.08	26.85 3.76 x	26.18 5.76 ✓		26.99 .33 26.66 5.28 ✓		26.99 4.95	27.79 2.82 x C 0.68	27.79 4.68 4.00 C 0.68	
1+40	26.84 5.63 5.67 F 0.04	26.84 3.77 x	26.17 5.77 ✓		26.98 .33 26.65 5.29 ✓		26.99 4.95	27.79 2.82 x C 0.63	27.79 4.68 4.05 C 0.63	
1+20	32.47X 26.76 5.71 5.60 C 0.11	30.61X 26.76 3.85 x	26.09 5.85 ✓		26.90 .33 26.57 5.37 ✓		26.90 5.04	30.61X 27.70 2.91 x C 0.60	27.70 4.77 4.17 C 0.60	

X 31.94

South

North

	Prop	cl.	Gutter	1/4	±	1/4	Gutter	cl.	Prop
A+50	$\frac{22.19}{10.28}$ $\frac{9.80}{C-0.48}$	$\frac{22.19}{8.42}$ x						$\frac{22.97}{7.64}$ x C-1.66	$\frac{22.97}{9.50}$ $\frac{7.84}{C-1.66}$
A+00	$\frac{23.15}{9.32}$ $\frac{8.90}{C-0.42}$	$\frac{23.15}{7.46}$ x			$\frac{23.28}{33}$ $\frac{22.95}{8.99}$			$\frac{23.95}{6.56}$ x C-1.00	$\frac{23.95}{8.52}$ $\frac{7.52}{C-1.00}$
3+50	$\frac{24.10}{8.37}$ $\frac{7.92}{C-0.45}$	$\frac{24.10}{6.51}$ x	Rake		Rake			$\frac{24.94}{5.67}$ x C-0.40	$\frac{24.94}{7.53}$ $\frac{7.13}{C-0.40}$
3+00	$\frac{25.05}{7.42}$ $\frac{7.10}{C-0.32}$	$\frac{25.05}{5.56}$ x				$\frac{25.19}{33}$ $\frac{24.86}{7.08}$		$\frac{25.93}{4.68}$ x F-0.04	$\frac{25.93}{6.54}$ $\frac{6.58}{F-0.04}$
2+60	$\frac{25.83}{6.64}$ $\frac{6.29}{C-0.35}$	$\frac{25.83}{4.78}$ x				$\frac{25.95}{33}$ $\frac{25.62}{6.32}$	$\frac{25.93}{6.01}$ x31.94	$\frac{26.73}{3.88}$ x C-0.21	$\frac{26.73}{5.74}$ $\frac{5.53}{C-0.21}$
2+40	$\frac{26.41}{26.17}$ $\frac{6.30}{5.93}$ C-0.37	$\frac{30.61x}{26.17}$ $\frac{4.44}{x}$	$\frac{25.50}{6.44}$	$\frac{26.30}{33}$ $\frac{25.97}{5.97}$		$\frac{26.28}{5.66}$ x30.61x $\frac{27.08}{3.53}$ x C-0.29	$\frac{27.08}{5.39}$ $\frac{5.10}{C-0.29}$		

Oliver St.

5

South

North

Prop.	cl.	Gutter	1/4	±	1/4	Gutter.	cl.	Prop.
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5+00 Exist dr

32.47x	30.61x	29.59	
21.24	21.24	11.35	
11.23	7.37	11.35 ✓	
11.25	7.38		
cl. -1.02	-0.01		

21.27	21.30	30.61x	32.47x
10.67	10.64	21.99	21.99
10.67 ✓	10.64	8.62	10.48
		8.61	10.50
		10.84	- .02 cl

(31.94)

4+80

32.47x	20.97	
8.5	10.97 ✓	

↑
Take

21.74	21.70
33	10.24
21.41	
10.53	

↑
Take

Alley BIK 301 Pac. Beach
(South of Oliver)

6

INDEXED

SEP 6 1950

MK

	South	±	North		South	±	North	
1+00	0-2' <u>23.85</u> 4.74 <u>4.49</u> C-0.25	23.70	N. 15° <u>24.15</u> 4.44 <u>2.95</u> C-1.49	2+60	0-2' <u>22.93</u> 6.15 <u>5.35</u> C-0.80	22.78	N.-0.75 <u>23.23</u> 5.85 <u>4.27</u> C-1.58	NW.B.P. Pac.Beach Dr. + Gresham <u>21.19</u> 7.40 <u>28.59</u> 4.88 23.91 5.17 <u>29.08</u>
0+80	0-2' <u>23.82</u> 4.77 <u>4.57</u> C-0.20	23.67	N-120 <u>24.12</u> 4.47 <u>3.21</u> C-1.26	2+40	0-2' <u>23.13</u> 5.95 <u>5.08</u> C-0.87	22.98	N.0.75 <u>23.43</u> 5.65 <u>4.24</u> C-1.41	
0+60	0-2' <u>23.69</u> 4.90 <u>4.39</u> C-0.51	23.54	0-1' <u>23.99</u> 4.60 <u>4.19</u> C-0.41	2+20	0-2' <u>23.28</u> 5.80 <u>5.01</u> C-0.79	23.13	N.-0.70 <u>23.58</u> 5.50 <u>3.94</u> C-1.56	
0+40	0-2' <u>23.46</u> 5.13 <u>4.15</u> C-0.98	23.31	X-2' <u>23.76</u> 4.83 <u>4.09</u> C-0.74	2+00	28.09X 0-2' <u>23.40</u> 5.68 <u>4.58</u> C-1.10	23.25	28.09X N.-65 <u>23.70</u> 5.38 <u>4.35</u> C-1.03	
0+20	0-2 <u>23.15</u> 5.44 <u>4.69</u> C-0.75	23.00	M.-15 <u>23.45</u> 5.14 <u>3.37</u> C-1.77	1+60 T.P.	28.59X 0-2' <u>23.60</u> 4.99 <u>4.68</u> C-0.31	23.45	28.59X N.-0.65 <u>23.90</u> 4.69 <u>3.45</u> C-1.24	
Gresham 0+00	0-2' 28.59 <u>22.75</u> 5.84 <u>4.58</u> C-1.26	22.59	0-2' <u>23.03</u> 5.56 <u>3.85</u> C-1.71	1+20	0-2 28.59X <u>23.80</u> 4.79 <u>4.45</u> C-0.34	23.65	0-2' 28.59X <u>24.10</u> 4.49 <u>4.10</u> C-0.39	

Alley. So. of Oliver

7

	South	±	North	
				726.33
4+00	0-2' <u>20.83</u> 8.25 8.45 F0.20	20.68	0-2 <u>21.17</u> 7.95 7.68 C-0.27	02 BK 21.13 5.20 4.90 C-0.30
3+80	0-2' <u>21.26</u> 7.82 7.77 C-0.05	21.11	0-2' 02 BK <u>21.56</u> 7.52 7.50 C-0.02	21.56 4.77 4.72 C-0.07
3+60	0-2' <u>21.64</u> 7.44 7.36 C-0.08	21.49	0-2' <u>21.94</u> 7.14 6.80 C-0.34	3+60 21.94 C-0.34 Elev 2228 + 40.5 726.33
3+40	0-2' <u>21.96</u> 7.12 7.14 F0.02	21.81	0-2' <u>22.26</u> 6.82 6.08 C-0.74	
3+20	0-2' <u>22.23</u> 6.85 6.65 C-0.20	22.08	0-2' <u>22.53</u> 6.55 4.86 C-1.69	
2+80	0-2' 29.087 <u>22.71</u> 6.37 5.90 C-0.47	22.56	0-2' 29.087 <u>23.01</u> 6.07 5.23 C-0.84	

	So.	No.
2+90(South) = Lat. #2	29.087 <u>17.65</u> 11.43 5.85 C-5.58	
3+15(North) = Lat. #1		29.087 <u>17.59</u> 11.49 4.73 C-6.76

	South	±	North
Fanuel 5+00	18.08 11.00 11.02 -0.02	18.05	18.42 10.66 10.56 C-0.10
4+80	0-2' <u>18.69</u> 10.39 9.92 C-0.47	18.54	0-2' 18.99 10.09 9.48 C-0.61
4+40	0-2' <u>19.81</u> 9.27 9.47 F0.20	19.66	0-2' 20.11 8.97 8.69 C-0.28
4+20	0-2' <u>20.35</u> 8.73 8.40 C-0.33	20.20	0-2' 20.65 8.43 8.20 C-0.23

Alley BIK 19. O. B. Park
Sewer Laterals

7-25-49

W.O. 31507

INDEXED

SEP 6 1950

Lat. # 7 (Sheet 7317-L)

Sommermeier
McCoy
Allen
Rohr.

24.65 X
15.02 = EL.
9.63
4.40
C-5.23

Voltaire + Cable
S.W.B.P.

17.10
7.55
24.65

FB 1825
AS

ALLEY BIK. 12, O. B. Park.
Sewer Laterals

8

(Sheet 7317-L)

0+00 = Aly. line cable St.

Nail & Back.	2+10 RT.	4+60 RT.
0+10 RT.		
#1	#2	#3
22.52 X	27.42 X	27.42
12.86	15.93	19.38
<u>9.66</u>	11.49	8.04
3.80	<u>6.28</u>	2.80
C-5.86	C-5.21	C-5.24
5+60 RT	5+35 LT	3+85 LT.
#4	#5	#6
31.60 X	31.60 X	27.42 X
20.75	20.41	18.35
<u>10.85</u>	11.19	7.07
5.82	<u>6.12</u>	4.03
C-5.03	C-5.07	C-5.04

INDEXED

SEP 6 1950

17.10
5.42
22.52 X
1.60
20.92
6.50
27.42 X
2.12
25.30
6.30
31.60 X
5.96
25.64 = SW. B.R. Voltaire
+ Sunset Cliff
25.62

See also
page 10

Block 70 O.B.

Bacon to ocean Between Narragansett + Del Monte

Sewer laterals

N. Wly line Bacon = 0+00

Del Monte
+ Bacon
N.W.B.P.

INDEXED

SEP 6 1950

24.04
2.82
26.86 x
3.85
23.01
6.20
29.21

2+95 Lt

4
29.21 x
19.22
9.99
1.92
C-8.07

3+35 Rt

1
29.21 x
20.02
9.19
4.96
C-4.23

1+85 Rt.

3
29.21 x
18.19
11.02
6.58
C-4.44

2+85 Rt.

2
29.21 x
18.74
10.47
7.33
C-3.14

Alley Blk. 12, O.B. Park
Sunset Cliffs Blvd. to Cable
between Voltaire + Muir

7/29/49
C.H.S.

D-V Back of paving unless
otherwise noted

10

	Lt. Qty.	£	Rt. Qty. D-1'		Lt. (Qty)	£	Rt. (Qty)	Sw.B.P. Sunset Cliffs Blvd. + Voltaire
INDEXED M.K. SEP 6 1950	1+60	24.10	24.10	4+00	20.79	20.79	20.79	25.62 5.12
		6.64 6.25	6.64 6.24		5.37 5.02	5.37 5.00	5.37 5.00	30.74x 7.17
		C-0.39	C-0.40		C-0.35	C-0.37	C-0.37	23.57 2.59
	1+20	24.65	24.65	3+60	21.34	21.34	21.34	26.16x 7.17
		6.11 5.99	6.11 5.08		4.82 4.66	4.82 3.31	4.82 3.31	18.99 3.01
		C-0.12	C-1.03		C-0.16	C-1.51	C-1.51	22.00x 4.91 17.09
	0+80	25.20	25.20	3+20	21.89	21.89	21.89	sw.B.P. Cable + Voltaire
		5.54 5.51	5.54 5.63		4.27 4.08	4.27 4.00	4.27 4.00	17.01 offer 17.10 FB 1825 75
		C-0.03	F-0.09		C-0.19	C-0.27	C-0.27	
	Brk. 0+40	25.75	25.50 25.75	2+80	N.2' 22.44	22.44	22.44	
		4.99 4.99	4.99 4.80		3.72 2.77	3.72 2.77	3.72 3.58	
		X	C-0.19		C-0.93	C-0.14	C-0.14	
	0+20	25.90	25.65 25.90	2+40	26.16x 23.00	26.16x 23.00	26.16x 23.00	
		4.84 4.78	4.84 5.45		3.16 3.13	3.16 3.08	3.16 3.08	
		C-0.06	F-0.61		C-0.03	C-0.08	C-0.08	
	Sunset Cliffs Blvd. 0+00	30.74x 25.92	25.72 25.91	T.I.P. 2+00	30.74x 23.55	30.74x 23.55	30.74x 23.55	
		4.82 4.82	4.83 4.82		7.19 6.95	7.19 6.95	7.19 7.16	
		X	.01		C-0.24	C-0.03	C-0.03	

Rate

Lt. (Lst) 4 Rt (Nly)

Cablest.
6700

17.56	17.27	17.57
4.44		4.23
4.42		4.43
<u>0.002</u>		<u>X</u>

5780

18.15	17.90	18.15
3.85		3.85
3.77		3.85
<u>0.008</u>		<u>X</u>

Bik
5760

22.007		22.007
18.58	18.33	18.58
3.42		3.42
3.28		3.31
<u>0.014</u>		<u>0.011</u>

TiP.

5720

19.14		19.14
7.02		7.02
7.25		6.33
<u>0.023</u>		<u>0.069</u>

N-0.25

4780

19.69		19.69
6.47		6.47
6.30		6.21
<u>0.017</u>		<u>0.026</u>

4740

26.167		26.167
20.24		20.24
5.92		5.92
5.57		4.60
<u>0.035</u>		<u>0.132</u>

N-0.45

Alley Blk. 19. D.B. Park.

Sunset Cliffs Blvd. between Voltaire

See also

page 8

slly = Lt

±

Rt. N.Y.

Sommermeier
7-26-49

12

				Lt.	±	Rt.	S.W.B.P. Sunset Cliffs Blvd + Voltaire
1+72	24.51 4.46 4.01 C-0.45	N. 141 24.51 4.46 3.71 C-0.75		EV.C. 3+40 22.77 6.20 5.92 C-0.28	22.52	X-2' 22.77 6.20 5.72 C-0.48	25.62 4.48 30.10X 4.60 25.50 3.47 28.97X 6.52
1+28	28.97A 24.89 4.08 3.67 C-0.41	28.97A 24.89 4.08 3.47 C-0.61		3+20 23.07 5.90 5.78 C-0.12	23.82	X-2' 23.07 5.90 5.65 C-0.25	22.45 3.91 26.36X 6.58 19.78 4.19 23.97
0+84 (5x 44°)	T.P. D-0.50 25.27 4.83 4.72 C-0.11	25.27 4.83 4.45 C-0.38		3+00 23.33 5.64 5.48 C-0.19	23.08	A-1' 23.33 5.64 5.44 C-0.20	
Brk. 0+40	D-0.75 25.65 4.45 4.48 F-0.03	25.40 25.65 4.45 4.36 C-0.09		2+80 23.55 5.42 5.28 C-0.14	23.30	23.55 5.42 5.22 C-0.20	
0+20	25.70 4.40 4.50 F-0.10	25.45 25.70 4.40 4.11 C-0.29		pvc. Brk 2+60 23.75 5.22 5.15 C-0.07	23.50	23.75 5.22 4.77 C-0.45	
Sunset Blvd. 0+00	30.10X 25.40 4.70V	25.14 30.10X 25.46		2+16 24.13 4.84 4.67 C-0.17		24.13 4.84 4.20 C-0.64	
				28.97X		28.97X	

Alley BIK. 19. O.B. Parki

Cable St.	Lt	±	Rt.
6+00	18.56	18.28	18.58
	<u>5.41</u>		<u>5.39</u>
	<u>5.92</u>		<u>5.21</u>
	N-2' X		X-2' X
5+80	23.97x	18.75	23.97
	<u>19.00</u>		<u>19.00</u>
	<u>4.97</u>		<u>4.97</u>
	<u>4.44</u>		<u>4.54</u>
	C0.53		F0.43
T.P.			
5+40	19.62		X-2'
	<u>6.74</u>		<u>19.62</u>
	<u>6.81</u>		<u>6.74</u>
	F0.07		<u>6.32</u>
			C0.42
5+00	20.25		N-0.20'
	<u>6.11</u>		<u>20.25</u>
	<u>6.25</u>		<u>6.11</u>
	F0.14		<u>5.36</u>
			C0.75
4+60	20.88		20.88
	<u>5.48</u>		<u>5.48</u>
	<u>5.47</u>		<u>5.44</u>
	F0.01		C0.04
4+20	26.36x		26.36x
	<u>21.51</u>		<u>21.51</u>
	<u>4.85</u>		<u>4.85</u>
	<u>4.88</u>		<u>4.73</u>
	F0.03		C0.12
3+80	N-175		28.97x
	<u>22.14</u>		<u>22.14</u>
	<u>6.83</u>		<u>6.83</u>
	<u>5.83</u>		<u>6.85</u>
	C1.00		F0.02

See also Alley BIK, 70. O.B.
 Bacon to Ocean Between

Narragansett
 + Del Monte

W.O. #31529
 7-25-49

Sommermeier
 McCoy
 Allen
 Rohr

T.P. South
 Lt.

North
 Rt.

East + West alley (at Bacon)

3+30

25.14
 3.88
 1.56
 C-2.32

24.84
 4.18
 1.54
 F-0.36

N.W.B.P.
 Del Monte
 + Bacon

24.04
 3.44
 27.48x
 3.88
 23.60
 4.54
 28.14x
 5.19
 22.95
 6.07
 29.02x
 3.44
 25.58
 9.49
 35.07x

South
 Lt.

North
 Rt.

T.P.

1+58

23.42
 4.72
 5.19
 F-0.47

23.12
 5.02
 5.87
 F-0.85

3+10

24.55
 4.47
 1.62
 C-2.85

24.25
 4.77
 5.35
 F-0.58

1+12

23.28
 4.86
 5.02
 F-0.16

A-1'
 22.98
 5.16
 5.01
 C-0.15

2+90

24.11
 4.91
 2.47
 C-2.44

23.81
 5.21
 6.92
 F-1.71

46.5 times

0+66

X-2'
 28.14x
 23.14
 5.00
 4.21
 C-0.77

28.14x
 22.84
 5.30
 4.54
 C-0.76

2+70

23.83
 5.19
 3.92
 C-1.27

23.53
 5.49
 6.26
 F-0.77

T.P.

0+20

23.00
 4.48
 3.02
 C-1.46

22.70
 4.78
 4.05
 C-0.73

2+50

23.69
 5.33
 3.99
 C-1.34

23.39
 5.63
 6.71
 F-1.08

Wly. Bacon
 0+00

22.26
 5.22

21.97
 5.51

2+04

29.02x
 23.56
 5.46
 5.00
 C-0.46

29.02x
 23.26
 5.76
 7.05
 F-1.29

E+W. Alley

BIK. 70-0.13

15

T.P.

Cont. P. 16

To Rt.
11th N.Y.S. Alley

D.

4+86⁶⁷

0-1'

0+02⁰

6+00

2' Both ways

(P-1A) 35.07 X

33.90

33.60

39.95

39.65

1.65

1.17

1.47

5.16

5.46

33.42

1.65

0.99

1.44

6.24

11.69

F 0.48

C 0.48

C 0.72

F 0.78

45.11 X

4+88³³

3 8³³ - 3 Times

31.46

31.16

5+80

39.43

39.13

3.61

3.91

5.68

5.98

3.28

4.13

5.48

6.59

C 0.33

F 0.22

C 0.20

F 0.61

4+10

29.02

28.72

5+60

38.53

38.23

6.05

6.35

omitted
Garage
in alley

6.58

6.88

5.59

5.62

5.62

7.41

C 0.46

C 0.96

F 0.53

3+90

27.83

27.53

5+50

37.94

X-1E

37.64

7.24

7.54

7.17

7.47

6.89

7.48

5.59

7.18

C 0.85

C 0.06

C 1.58

C 0.29

37.64
C 0.29
37.93
+ 4.01
X 41.94

3+70

26.78

26.48

Line N.Y.S. Alley

5+45

37.62

0-1'

37.32

8.29

8.59

7.49

7.79

6.73

5.97

5.97

8.25

C 1.56

C 1.82

F 0.46

3+50

35.07 X

35.07 X

Line N.Y.S. Alley

5+25

0-1 Both ways

45.11 X

45.11 X

25.88

25.58

36.35

36.05

9.19

9.49

8.76

9.06

7.67

9.49

8.52

8.88

C 1.52

C 0.24

C 0.18

41.94
36.35
5.59
5.02
10.03

E. + W. Alley. BIK. 70-0.13,

BIK. 70-0.13,

North of Alley - 0.12 on Nly. 16

0.10 = 3.14 + 0.12 on Nly. Alley

0.50

0.50

0.12

	South Lt.	±	North Rt.
Errd.	D. Light N + S. Alley		45.11 X
6+20	- 2" on E + W.		39.95
	40.10		5.16
	510.1		2.55
	412.1		0.61
	00.80		

± only
6+10

39.55

Nly. & Sly. Alley BIK 70 O.B. 7/27/49

Between Del Monte & E+W. Alley

0+00 = Sly. line N+S Alley

Nly
Del Monte
1+40

East
= Lt.
35.40

±

West
= Rt.
35.02

17

	East. Lt.	±	West = Rt.		East = Lt.	±	West = Rt.	
				1+40	35.40		35.02	
					7.43		7.81	stake 5+25 Lt.
					7.42		7.81	P. 15
0+70	X-2'		Bolt - 0.25	1+30	X-2'		X-1'	Cr. = 36.35
	38.54		38.78		36.17		35.92	cs 0.24
	4.29		4.05		6.66		6.91	EL. = 36.59
	4.36		3.36		5.88		7.18	6.24
	F 0.07		C-0.69		C 0.78		F 0.27	+ 2.83 π
0+60	X-2'			1+20	X-2'		X-1'	
	38.56		38.83		36.83		36.69	
	4.27		4.00		6.00		6.14	
	3.33		3.58		5.40		6.07	
	C-0.94		C-0.42		C-0.60		F 0.53	
0+50	X-2'		N-0.40	1+10			X-1'	
	38.48		38.77		37.38		37.35	
	4.35		4.06		5.45		5.48	
	2.76		3.39		3.39		6.10	
	F 1.59		C-0.67		C-2.06		F 0.62	
0+40	X-2'			1+00	X-2'		X-1'	
	38.29		38.59		37.83		37.88	
	4.54		4.24		5.00		4.95	
	4.65		2.41		2.71		3.49	
	F 0.11		C-1.83		C-2.29		C-1.46	
0+20	N-135		H-3'	0+90			X-1'	
	37.80		38.10		38.17		38.30	
	5.03		4.73		4.66		4.53	
	4.27		3.30		4.57		1.03	
	C-0.76		C-1.43		C-0.09		C-3.50	
Alley (E+W)				0+80	X-2		N-0.20	
0+00	36.35		37.62		38.41		38.60	
	6.48		5.21		4.42		4.23	
	6.24		3.69		4.38		3.23	
	C-0.24		C-1.52		C-0.04		C-1.00	

N¹/₂ + S¹/₂ Alley BIK. 70 O.B. 7/27/49
 Between Narragansett + E+W. Alley
 0+00 = sly. line Narragansett

Pwe. = 39.36 18

	East = Lt.	♀	West = Rt.
0+80	39.30 5.81 6.96 <u>12.77</u>		X-5' 39.60 5.51 5.17 <u>10.68</u>
0+60	D-2' 38.86 6.25 6.82 <u>13.07</u>		X-5' 39.16 5.95 5.56 <u>11.51</u>
0+40	D-1' 37.77 7.34 7.37 <u>14.71</u>		D-0.5' 38.07 7.04 6.94 <u>14.00</u>
0+20	D-1' 36.01 9.10 8.59 <u>17.69</u>		D-1' 36.31 8.90 7.14 <u>16.04</u>
0+10	34.90 10.21 9.54 <u>19.75</u>		D-1 35.20 9.91 17.32 <u>27.23</u>
Narragansett 0+00	33.68 11.43 11.47 <u>22.90</u>		34.39 10.72

From A16. T 45.11

City lat. ^{45.11} 681 Rod 11.75
 6.81
 C-4.94
 92' sly. - sly. line Narragansett on
 Ely. side N. + S. Alley.
 set 6' Below Paving grade
 because of low Lot. (4' below lot.)

	East = Lt.	♀	West = Rt.
Line E+W. Alley 1+60	39.95		40.10 5.01 4.21 <u>9.22</u>
E+W. alley ♀ only 1+50		39.55	
Line E+W. alley 1+40	2 Back Both ways 39.65 5.46 6.24 <u>11.70</u>		39.95 5.16 4.55 <u>9.71</u>
1+10	N-1 ¹ / ₂ 39.47 5.64 5.60 <u>11.24</u>		N-1 ¹ / ₂ 39.77 5.34 4.70 <u>10.04</u>

8/9/49

McCoy
Allen
Rorer

16" Storm Drain
+ Type H Curb Inlet
Proctor Place W.O. 20547.

Drawing # 3762 B

So End Proctor West Curb = 0+00	5.17	304.17	617	298.00
" " 0+50	5.71		571	298.46
" " 1+00	5.24	304.17		298.93

0+00	Flowline	295.00
		9.77
		5.88
		C-3.29

INDEXED

SEP 6 1950

0+30		294.50
		19.67
		5.96
		C-3.11

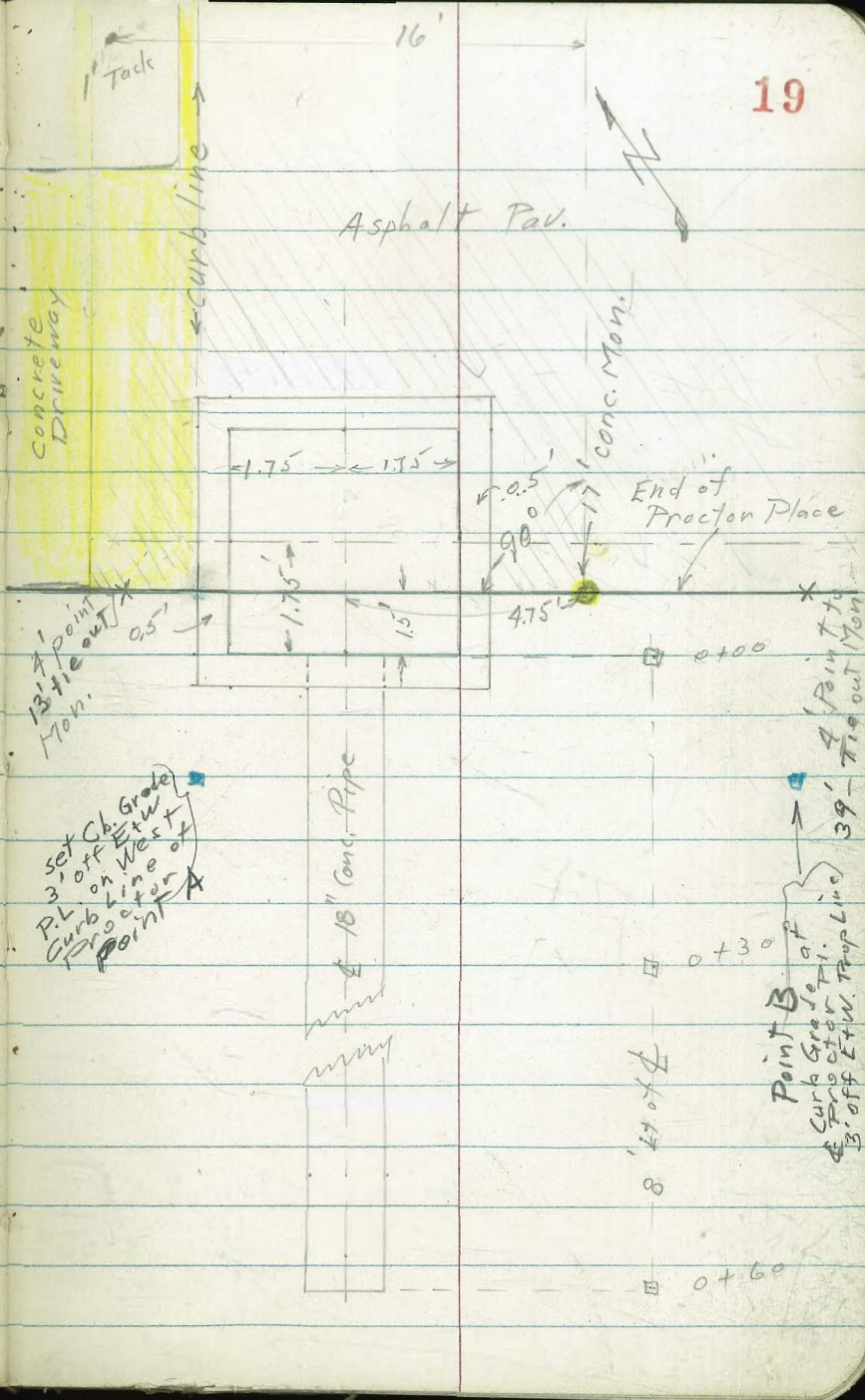
0+60	"	294.00
		10.17
		7.86
		C-2.31

Pt. A
6.17
298.00

Pt. B
5.69
298.48

Existing
So. End East
Curb.
5.22
298.95

{30417}



8/15/49

Paye Beryl Ingraham to Jewell

W.O. # 31371

20

INDEXED

7/11
SEP 6 1950

Prop. Curb Gutter 1/4 £ 1/4 Gutter Curb Prop

1+20

142.08
14.96
5.45
C 9.51

142.08

+84

131.12
25.92
11.70
C 14.22

0+48

130.16
26.88
12.30
C 14.58

TR #7 157.04

0+20

131.93
12.53
2.70
2.62
-25

0+14

129.20
15.04
3.11
C 11.94

0+00

131.93
128.70
3.23
3.32
= .09

131.93
127.70
4.23
4.44
= .21

TR #6

144.24

NW 1/4
Ingraham
to Beryl
(See Pg 23)

Prop

+ 60 153.75
 POT on 4 75.45
 2+57.50 8.16
 X W. Rim MH 7.29
 POT 5' No. PL.
 2+58.32
 + 40 152.70
 16.50
 ~~9.17~~
 C- 7.33

+ 20 151.44
 17.76
 ~~9.97~~
 7.79

2+ 00 149.98
 out

2+ 00
 + 80 148.31
 20.89
 11.90
 TP#8. C- 8.99
 ~~169.20~~

+ 60 146.43
 10.51
 2.02
 C- 8.49

+ 40 144.36
 12.68
 3.70
 C- 8.98

T 15704

Prop

Prop

5+19.±

Prep
 159.00
 10.20
 2.62
 C-7.58

5+10

158.84
 10.36
 2.88
 C-7.48

4+6.25

158.04
 11.16
 4.85
 C-6.31

4+15

157.25
 11.95
 5.98
 C-5.97

~~163.25~~
~~15.75~~
~~5.98~~

3+6.75

156.46
 12.74
 7.15
 C-5.59

+20

155.67
 13.53
 7.08
 C-6.45

153.67
 6.3

3+00

155.24
 73.96
 7.37
 C-6.59

2+80

154.59
 14.61
 7.70
 C-6.91

7169.20

Prup

22

158.23 Existing
 10.97
 11.03
 -.06

Check Benches on Paving Job
 W.O. 31371 - From N.W. B.P. Diamond
 + Gresham.

23

N.W. B.P. Diamond + Gresham	1121	81.51		70.30
TP#1	6.79	86.32	1.78	79.53
TP#2	5.78	89.57	2.23	83.79
TP#3	11.70	99.73	1.54	88.03
TP#4	12.58	110.85	1.46	98.27
Set B.M. SE 7/4 T Chalcedony + Ingraham			9.31	101.54
SE 2/4 T (7) Law + Ingraham	1303	121.68	2.20	108.65 (108.68)
TP#5	10.64	131.93	0.39	121.29
SW 7/4 T. Beryl + Ingraham			6.99	125.08 124.94 +.14
TP#6	12.63	144.24	0.3	131.61
TP#7	13.10	157.04	0.30	143.94
TP#8	12.49	169.20	0.33	156.71
TP#9 Curb BC SW Beryl + Jewell			11.03	158.17
TP#9 Curb BC SW Beryl + Jewell	0.79	158.96		158.17
TP#10	+ 0.32	147.04	- 12.24	146.72
TP#11	0.65	135.10	12.59	134.45
Set B.M. Fire Hyd SW Cor Law + Jewell			3.59	131.51
TP#12	0.88	123.36	12.62	122.48

check on fire Hyd at SE 011 Chalcedony + Jewell					B.M.#1	123.36 - 7.95	115.41 (115.41)
TP#13						110.47 - 12.91	110.45
TP#14 SE 1/4 T Chalcedony + Ingraham				0.27		101.83 - 8.91	101.56 (101.84)
TP#15						97.05 - 8.12	93.71
TP#16						95.12 - 45.9	92.46
TP#17 NW 1/4 T Chalcedony + Gresham				0.22		89.55 - 5.79	89.33 (89.34)
TP#18 NW 1/4 T NW Cor Gresham + MANSOURI				+ 1.36		80.14 - 10.77	78.78
TP#19 - NW 8P Diamond + Gresham see preceding pt						- 9.84	70.30 (70.30)

check $\frac{1807}{29}$ for 12508 Elev. SW 7/4 T Beryl
 + Ingraham

B.M.#1 Above.

115.41
6.95
122.36
50
171.86
12.43
134.29
5.94
128.35 = F.P. Fire Hyd.
134.29
4.92
129.37
6.98
136.35
10.34
126.01 = SW 7/4 T - Lamont + Chalcedony

B.M.#2

B.M.#3

Pave. grades.

Dalbergia. Una to Wodeg

B.M.#1 = N.E. 7' 24 T. Dalbergia + Una. (Sheet 7050L)

$$\begin{array}{r}
 19.11 \text{ B.M.#1} \\
 \underline{3.51} \\
 22.62 \checkmark \\
 \underline{5.19} \\
 17.43 \\
 \underline{4.123} \\
 21.65 \checkmark \\
 \underline{5.39} \\
 16.27 = \text{s.wly. 2' 24 T.} = \text{B.M.#2.} \\
 \text{Dalbergia + Vesta.}
 \end{array}$$

24

INDEXED

SEP 6 1950

$$\begin{array}{r}
 21.47 \\
 \underline{6.09} \\
 15.39
 \end{array}$$

$\frac{2}{5.77 \text{ - ct.}}$

$$\begin{array}{r}
 16.27 \\
 \underline{5.20} \\
 214.77
 \end{array}$$

$$\begin{array}{r}
 21.47 \\
 \underline{6.11} \\
 15.36
 \end{array}$$

Wly Vesta
6+00

$$\begin{array}{r}
 22.75 \\
 \underline{4.49} \\
 18.26
 \end{array}$$

$$\begin{array}{r}
 19.11 \text{ B.M.#2} \\
 \underline{3.64} \\
 22.75 \checkmark
 \end{array}$$

$$\begin{array}{r}
 22.75 \checkmark \\
 \underline{5.45} \\
 17.30
 \end{array}$$

Nly.

$$\begin{array}{r}
 15.33 \\
 \underline{6.33 \checkmark}
 \end{array}$$

VA

$$\begin{array}{r}
 15.74 \\
 \underline{5.73} \\
 33 \\
 \underline{6.06} \\
 \times
 \end{array}$$

E

$$\begin{array}{r}
 15.91 \\
 \underline{5.75} \\
 + 33 \\
 \underline{6.08}
 \end{array}$$

VA

$$\begin{array}{r}
 15.74 \\
 \underline{5.73} \\
 33 \\
 \underline{6.06} \\
 \times
 \end{array}$$

Sly

$$\begin{array}{r}
 15.83 \\
 \underline{6.33 \checkmark}
 \end{array}$$

5+85±

15.39

$$\begin{array}{r}
 15.91 \\
 \underline{5.56} \\
 33 \\
 \underline{5.89} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 16.07 \\
 \underline{5.59} \\
 + 33 \\
 \underline{5.92}
 \end{array}$$

$$\begin{array}{r}
 15.89 \\
 \underline{5.58} \\
 33 \\
 \underline{5.91} \\
 \times
 \end{array}$$

15.36

Rake

0+15

18.26

$$\begin{array}{r}
 22.75 \\
 \underline{18.52} \\
 + 4.23 \\
 + 0.83 \\
 \underline{4.56} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 18.45 \\
 \underline{4.17} \\
 + 33 \\
 \underline{4.50 \checkmark} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 22.75 \checkmark \\
 \underline{18.04} \\
 4.71 \\
 + 0.83 \\
 \underline{5.04} \\
 \times
 \end{array}$$

17.30

Ely. Una.
0+00

$$\begin{array}{r}
 18.33 \\
 \underline{4.29 \checkmark}
 \end{array}$$

$$\begin{array}{r}
 18.52 \\
 \underline{4.23} \\
 + 33 \\
 \underline{4.56} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 18.41 \\
 \underline{4.21} \\
 + 33 \\
 \underline{4.54 \checkmark} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 22.75 \\
 \underline{18.02} \\
 4.73 \\
 + 33 \\
 \underline{5.06} \\
 \times
 \end{array}$$

$$\begin{array}{r}
 17.33 \\
 \underline{5.29 \checkmark}
 \end{array}$$

B.M. #2 P.24 16.27

B.M. #2 - P.24	16.27
	<u>4.127</u>
	20.597
	<u>5.185</u>
	14.69
	<u>4.14</u>
	18.83

6+00²

Mo
12.83
5.49
18.32

curb. cut. (on. So.)

12.33
6.00
18.33

12.83
6.00

13.08
5.25
+0.33
5.58
x

13.16
5.67
+0.33
6.00

12.83
5.50
+ .33
5.83

12.33
6.50

5+85²

Rake

12.90

13.28
5.05
+0.33
5.38
x

13.32
5.51
+ .33
5.84

13.02
5.31
+0.33
5.64
x

12.38

0+15

B.M. #2

16.27
3.75
20.02

0+15
Curb
20.02
5.28
14.74

14.74

20.02
15.27
4.75
+0.33
5.08

15.45
5.49
+ .33
5.42

15.27
4.75
+0.33
5.08

14.74

0+00-

Ely Vesta

14.83
5.71

20.02
15.27
4.75
+0.33
5.08

15.41
5.13
+ .33
5.46

15.27
4.75
+0.33
5.08

14.83
5.71

Intersection

Vesta & Dalbergia

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SEP 6 1950

B.M. #2-P2A

16.27
 4.87
 21.14 = \bar{A}
 0.33
 21.47 = sub. gr.
 X

Add. to \bar{A} . for
 sub grade.

check
 16.00
 14.91
 6.64
 - 3.2
 6.31 ✓

N. Gutter	N. 1/4	±	S 1/4	S Gutter
--------------	--------	---	-------	-------------

Ely gutter Vesta.

14.91	15.35	15.49	15.35	14.91
<u>6.56</u>	<u>6.12</u>	<u>5.98</u>	<u>6.12</u>	<u>6.56</u>
X	X	X	X	X

Ely 1/4

± Vesta

15.08	15.52	15.67	15.52	15.08
<u>6.39</u>	<u>5.95</u>	<u>5.80</u>	<u>5.95</u>	<u>6.39</u>
X	X	X	X	X

wly 1/4

wly gutter line Vesta.

15.25	15.69	15.83	15.69	15.25
<u>6.22</u>	<u>5.78</u>	<u>5.64</u>	<u>5.78</u>	<u>6.22</u>
X	X	X	X	X

LANDIS

Arizona to Arnold.

W.O.# 31679

Sommermeier

9-1-49

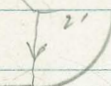
INDEXED
MK.
SEP 6 1950

28

B.P. S.E. Landis
+ ARIZONA

cl.	North G.	North VA	±	South VA	G	cl.
291.50 2.94 x OK						291.00 2.94 2.92 +0.02
276 ²⁵ Arnold	291.14 2.80 x OK		291.28		290.54 3.40 x OK	
2156 ²⁵	290.40 3.54 x		290.57		289.93 4.01 x	
0+20	285.26 8.68 x		285.65		285.23 8.71 x	
0+00 Arizona	284.84 9.10 x OK		285.47		284.93 9.01 x OK	cl. 285.50 8.44 8.53 -0.09

288.85
5.06



289.08
4.86
x
Set

288.79
5.15
5.23
-0.08

East

288.48
5.46
5.42
+0.04

N. + S. Alley

288.77
5.17
5.23
Set

287.90
6.04
6.00
+0.04

288.70
5.24
x
Set

288.46
5.48
5.50
-0.02

West

287.96
5.98
5.96
.02

288.39
5.55
Set

Landis St.

~~285.31~~
~~5.74~~
291.35

285.31
8.63
293.94 x

288.56
5.35



288.51
5.43
5.23
x

288.77
5.17
5.23
Set

Diamond & Morrell 9/14/49

10/7/49 31
Cb. stakes 4' Back of cl.

Outlet $\Sigma = 103.62$

97.00 cl.

96.50 cl.

96.00 cl.

96.30
7.32

96.05
7.57

95.93
7.69

95.80
7.82

95.68
7.94

95.55
8.07

95.30
8.32

96.54
7.08
7.09
0.01

96.23
7.39
7.41
0.02

96.10
7.52

95.97
7.65

95.85
7.77

95.74
7.88

95.44
8.18
8.21

96.96
3.31
100.27

Existing Pavement

96.56
7.06

96.18
7.44
4.09

96.04
7.58
4.27

95.90
7.72 4.37
7.73
0.01

95.77
4.50

95.77
7.85

95.64
7.98

95.64
4.63

95.38
8.24

100.27
95.38
4.89

Restaked 11/15/49

96.27
7.35
106.71
96.77
9.94
6.85
7.75
+0.10

96.00
7.62
96.50
3.88
10.11
96.23
4.05

95.80
4.47

95.80
7.82

95.83
7.79

95.83
4.44

95.76
7.86

95.76
4.51

95.58
4.69

95.58
8.04

95.33
8.29

95.33
4.94

95.12
9.00

95.12
5.16

103.62

95.18
8.74

95.18
5.10

100.27
p 28.

7.70

95.92
4.36

95.22
8.10

95.28
8.34

95.24
8.38

95.04
8.58

94.45
9.17

94.95
5.33

S.L. Diamond

5.23

8.67
8.67

INDEXED
M.K.
SEP 6 1950

T.P.

4+50	<u>382.15</u>	382.58	<u>382.15</u>	382.58
	6.02		6.02	
	<u>5.140</u>		<u>5.110</u>	
	C-0.62	382.77	C-0.92	383.07

1+50	<u>383.19</u>	383.48	<u>383.19</u>	383.48
	4.98	4.69	4.98	4.69
	<u>5.22</u>	<u>5.12</u>	<u>5.33</u>	<u>5.33</u>
	F0.24	F0.53	F0.35	F0.64
		382.94		382.84

4+00	<u>382.30</u>	382.75	<u>382.30</u>	382.75
	5.87	5.44	5.87	5.44
	<u>5.45</u>		<u>5.70</u>	
	C-0.42	382.72	C-0.117	382.47

1+00	<u>383.48</u>	383.63	<u>383.48</u>	383.63
	4.69	4.54	4.69	4.54
	<u>4.54</u>	X	<u>4.54</u>	X
	C-0.15	383.63	C-0.15	383.63

3+50	<u>382.45</u>	382.88	<u>382.45</u>	382.88
	5.72	5.29	5.72	5.29
	<u>5.93</u>		<u>5.44</u>	
	F0.21	382.24	C-0.28	382.72

E.V.C.	<u>388.17x</u>			
0+50	<u>383.78</u>		<u>383.78</u>	
	4.37		4.37	
	<u>3.79</u>		X	
T.P	C-0.60	384.38		

3+00	<u>382.60</u>	383.03	<u>382.60</u>	383.03
	5.57	5.14	5.57	5.14
	<u>5.76</u>		<u>5.81</u>	
	F0.37	382.21	F0.24	382.26

0+30	<u>383.57</u>		<u>383.59</u>	
	3.47		3.47	
	<u>2.89</u>		<u>3.12</u>	
	C-0.60	383.28	C-0.35	385.05

2+50	<u>382.75</u>	383.18	<u>382.75</u>	383.18
	5.42	4.99	5.42	4.99
	<u>5.88</u>		<u>5.79</u>	
	F0.46	382.21	F0.37	382.39

P.V.C.	<u>382.50</u>		<u>382.60</u>	
0+10	4.56		4.46	
	<u>3.67</u>		<u>3.96</u>	
	C-0.89	384.50	C-0.50	384.21

2+00	<u>382.90</u>	383.33	<u>382.90</u>	383.33
	5.27	4.84	5.27	4.84
	<u>5.59</u>	<u>5.59</u>	<u>5.44</u>	<u>5.44</u>
	F0.32	F0.75	F0.60	F0.17
	382.58		382.73	

S.L. Madison	<u>381.80</u>		<u>381.90</u>	
0+00	5.26		5.16	
	out.			

K.V.C.
6+ALE 379.40

6+30 380.00

6+10 381.02

5+90 381.45

P.V.C.
5+70 381.79 ~~382.22~~ 381.79 ~~382.22~~

T.P.

5+50 • 381.85 ~~382.28~~ 381.85 ~~382.28~~
 $\frac{5.84}{4.95}$ $\frac{5.84}{4.93}$
 C-0.89 382.74 C-0.91 382.76

5+00 387.69x
382.00 ~~382.43~~ 382.00 ~~382.43~~
 $\frac{5.69}{4.92}$ $\frac{5.69}{4.91}$
 C-0.87 382.87 C-0.78 382.78

S.E.B.P. Madison + Bancroft. 381.01 $\frac{18.11}{47}$
 $\frac{6.05}{47}$

387.06x

2.88

384.18 Rock

3.99

388.17x

5.50

382.67

5.02

387.69x

Rough Grade Hilltop Dr.
Euclid to 51st.

INDEXED

Sommermeier
McCoy
Allen
Rorer

11/14/49

V.O.#

SEP 6 1950

F.B. $\frac{1612}{16} + \frac{1617}{29}$

Profile # 3117

North

South

North

South

0+60

158.24
6.71
0.92
C-3.79

157.74
7.21
8.41
F 1.20

T.P.
↓
W.L. 51st
1+50

164.95X
145.50
19.45
12.57
C-6.88

144.95
9.74
11.80
F 2.06

0+48

159.30
5.65
0.58
C-5.07

158.80
6.15
6.64
F 0.49

1+42⁵

146.45
18.50
7.41
C-9.09

154.69X
146.13
8.56
8.25
C-0.31

0+40

160.00
4.95
0.79
C-4.16

159.30
5.65
5.84
F 0.19

1+00

153.05
11.90
3.73
C-8.17

164.95X
152.60
12.35
11.36
C 0.99

164.95X
12.57
152.38
2.31
154.69

0+30

160.86
4.09
0.73
C-3.36

159.50
5.45
3.60
C-1.85

0+80

155.90
9.05
1.48
C-7.57

155.41
9.54
9.54
C 0.00

0+60 = E. Line Euclid
To South.

164.95X
159.50
5.45
5.97
F 0.52

B.M. = 6+1 Hilltop 4.88 - 164.95
+ E. 10' line Euclid

160.07 $\frac{FB 1614}{20}$

Alley Bk. 55 Ocean Beach
 Sunset Cliffs Blvd. to Cable
 Between Cape May + Saratoga

35

11-25-49

Sommermeyer
 McCoy
 Allen
 Rover.

W.O.# 31625

INDEXED
 MAX
 SEP 6 1950

	sly.	Nly.				N.W.B.P. Cape May + Sunset Cliffs Blvd
			3+70	B-2'	N. Lina	24.04
				18.45	18.45	5.16
				7.74	7.74	29.20x
				7.40	7.03	7.46
				C0.34	C0.71	21.74
						4.45
1+40	B-2'	B-2'	3+20	B-1'	N-0.29	26.19x
	21.32	21.32		19.05	19.05	8.66
	4.87	4.87		7.14	7.14	17.53
	4.65	4.08		7.10	6.04	3.76
	C0.22	C0.79		C0.04	C 1.10	21.29x
1+20 P.V.C.	B-2'	B-2'	2+70	N-1.37	N-0.45	
	26.19x	26.19x		19.65	19.65	
	21.70	21.70		6.54	6.54	
	4.49	4.49		5.13	5.06	
	3.76	4.27		C-1.41	C-1.48	
	C0.53	C0.22				
1+00	B-1'	B-2'	2+20	B-2'	N-0.20	
	22.15	22.15		20.25	20.25	
	7.05	7.05		5.94	5.94	
	6.48	X		5.26	5.43	
	C0.57			C0.68	C0.51	
0+50	B-2'	N-0.15	1+80 E.V.C.	B-2'	N-0.55	
	23.35	23.35		20.72	20.72	
	5.85	5.85		5.47	5.47	
	5.73	5.00		4.90	4.70	
	C0.12	C0.85		C0.57	C0.77	
0+00 = Fly. Sunset Cliffs Blvd	29.20x	29.20x	1+60	X-2'	N-0.50	
	24.54	24.34		20.99	20.99	
	4.66	4.66		5.20	5.20	
	4.70			4.64	4.41	
	-0.03			C0.56	C0.79	

1.193 notes

Ely. line Cable
6+00 E.V.C.14.49
680
✓14.51
6.78
✓

14.51

Sewer Lat. #1 - 15' Rt. 4+70

5+80

0-2'
15.21
6.08
5.33
C-0.75X-2'
15.23
6.06
5.96
C-0.10

15.23

0-5'

21.29 π
El. = 12.26
9.03
3.65
C-5.38

5+60

0-2'
15.86
5.43
5.05
C-0.38X-2'
15.87
5.42
5.75
F-0.33

15.87

5+40

0-2'
16.34
4.95
4.44
C-0.51X-2'
16.34
4.95
4.30
C-0.65

16.34

PVC
5+20Nail in edge of flooring
at door.-2.48
16.66
4.63
2.26
C-2.37X-2'
16.66
4.63
4.27
C-0.36

16.66

4+70

0-2'
21.29 π
17.26
4.03
3.80
C-0.230-2'
21.29 π
17.26
4.03
3.67
C-0.3621.29 π

4+20

X-2' π
26.19 π
17.86
8.33
8.20
C-0.130-2'
26.19 π
17.86
8.33
8.38
F-0.0526.19 π

Drain BIK. 192 Univ. Hqts.
Blaine Ave - East of Centre

stakes set 9' Lt. To 1+51.45
" " 5' RT 1+51.45 to 2+12.91 **37**
stakes set 9' Lt. of $\frac{1}{2}$ gate

Sommermeier
McCoy
Allen
Rorer

W.O. # 20586
12/6/49

See sheet 780A-L
FB. 1816
70

INDEXED
MK
SEP 6 1950

1+92.09

293.71
8.84
6.70
C-2.14

0+91.45 ⁹⁰
302.55x
294.72

1+73.27

293.90
8.65
5.30
C 3.35

7.83
3.82
C-4.01

B.M. = N.W. B.P.
Univ. + Centre

B.K.
0+71.45

294.92
11.91
6.41
C-5.50

303.88
2.95
306.83x
6.41
300.42
2.13

B.C. Lt.
1+54.45

294.09
8.46
4.31
C-4.15

E.C.
0+42.13

296.05
10.78
4.61
C-6.17

302.55x
3.34
299.21
7.08
296.29
2.41
303.88x
B.M.

Δ
PORT.

Ctr. Box inlet
1+51.45
Set at 1+53.45

294.12
8.43
4.42
C-4.01

Top of box

298.12
4.43
4.42
C-0.01

B.C. RT ⁹⁰
0+26.77

296.63
10.20
5.04
C-5.16

4' RT. on wall
296.63
10.20
4.65
C-5.55

1+31.45

294.32
8.23
4.54
C-3.69

Exist pipe
0+00

306.83x
297.65
9.18

1+11.45

294.52
8.03
4.26
C-3.77

Haines St

Missouri to Chalcedony

Sommermeier
McCoy
Allen
Rorer

Rough grade, 11/7/49
(Drainage)

Chalcedony St.

NEBP Chalcedony + Haines	Exist Pave	
92.58 077 <u>93.35</u> X	3.21 2+70 Pave. → 90.14 9008	3.21
88.87	2+16	88.95 4.40 4.08 <u>C 0.32</u>
4.48 3.63 <u>C 0.85</u>		
87.66	1+62	87.75 5.60 5.51 <u>C 0.09</u>
5.69 5.127 <u>C 0.42</u>		
86.45	1+08	86.55 6.80 6.86 <u>X</u>
6.90 6.60 <u>C 0.30</u>		
85.25	0+54	85.35 8.00 8.85 <u>X</u>
8.10 7.75 <u>C 0.35</u>		
Ord. on cl. line = 84.05	0+00	84.15 = Ord on cl. line
9.30 8.80 <u>C 0.50</u>		9.20 8.85 <u>C 0.35</u>

Dirt street

INDEXED
MK

SEP 7 1950

stakes 3' back of cl. line

stakes 3' back of cl. line

Haines St. - Chalcedony to Law.
Rough grades
(Drainage)

39

INDEXED

SEP 7 1950
MK

Law + Haines	Exist. Pave.	Law. St.
NE.B.P. 163.10 100 <u>104.10</u> X	3.45 EL: 100.85 2+70	2.75 101.35 = EL.
99.03 5.07 3.36 <u>C - 1.71</u>	2+16	99.51 4.59 3.25 <u>C 1.34</u>
97.20 6.90 4.95 <u>C 1.95</u>	1+62	97.68 6.42 4.95 <u>C - 1.47</u>
95.38 8.72 6.57 <u>C - 2.15</u>	1+08	95.85 8.25 6.68 <u>C - 1.57</u>
93.55 10.55 8.37 <u>C - 2.18</u>	0+54	94.02 10.08 8.37 <u>C - 1.71</u>
12.37 91.73 EL.	0+00	11.91 92.19 = EL.
	Exist. Pave. Chalcedony	

Jewell St. { 125' So. of Chalcedony
To Chalcedony
Rough grades for drainage 12/7/49

Kendall St. Law to Chalcedony
Rough grades for drainage. 40

Chalcedony Exist. Pave.	110.51 EL. Pave.
109.97 = Exist. Pave.	1+25
INDEXED SEP 7 1950	
108.72 5.24 3.60 C 1.64	0+75
107.44 6.52 5.60 C 0.92	0+25
106.80 7.16 6.97 C 0.19	0+00
Not graded so as to save oiled road.	145' 20' wide oiled road.
	N. line Missouri

stakes 3' back of ch. line.

Exist. Pave. Law St.	132.07 = El. Pave.	132.97 = El. Pave.
NEBP Law & Kendall	2+70	
135.65 1.29 136.93 X	1131.00 5.93 4.25 C 1.68	
	2+26	
	1+82	
	1+38	
	0+94	
	0+50	
124.40 = El. Pave.		125.01 = El. Pave.
	Exist. Pave. Chalcedony	

stakes 3' back of ch. line

INDEXED
SEP 7 1950

131.81
5.12
2.83
C 2.29

130.65
6.28
3.83
C 2.45

129.49
7.44
5.00
C 2.44

128.33
8.60
6.66
C 1.94

127.17
9.76
8.10
C 1.66

Hortensia No. of La Jolla

185' Sewer

12/12/49

Sommermeier
McCoy
Allen
Burch

INDEXED
MK
SEP 7 1950

0+00 = M.H. ctr. Hortensia +
La Jolla.

Set. Nail in pole #

Hortensia + La Jolla.

EL. 65.82

1+50

9.24 Ritt Exst M.H.

59.65
5.70
65.35

1+00

5.60

14.84 = Red 74.49 X

14.84

59.65 I.E. M.H.

61.65
12.84
6.40
C 6.44

~~285 @ 2.5% Cr~~

~~8.12~~
66.77

rise 2%

0+50

73.00

66.77

6.23

285 @ 2%

73.00 Crd

65.35

7.65 Crd

74.49 X
60.65
13.84
7.55
C 6.29

La Jolla Blvd.

0+00 I.E. 59.65

41

B.M. - SE. Ampudia + La Jolla = 43.75

D.E. = 2+85

65.35

12.85

56.60

Ord EL = 73.0

9.14

0.59

1.40

C - 7.74

56.01

11.07

2+50

64.65

67.08

9.84

1.26

2.47

65.82

C - 7.37

8.67

74.49

2+00

63.65

10.84

3.95

C - 6.89

INDEXED
MK

62.65

SEP 7 1950

11.84

5.60

C 6.20

39th St. Ocean View to Imperial

S. y. Franklin
2+79²

99.95
12.03
x

111.80x
100.55
11.25

100.35
11.63
x

BM #4

N.W. B.P. Ocean View

+ 39.15 = EL. 110.29

1.67

111.98x

11.63

100.35 =

S.W. 7' L + 1

Franklin

+ 39.15

= BM #5

1+99² Bk

102.77
9.21

INDEXED
MK

N. L. Alley
1+49²

SEP 7 1950

104.63

7.35

6.67

Top. Cl.

9.0.68

104.57

7.41

6.78

9.0.68

S. L. Alley to West

1+32²

105.13

6.85

6.19

S. L. Alley to East

1+27²

Top. Cl.

9.0.66

105.12

6.85

6.19

9.0.67

0+20

108.82

3.16

x

109.42

2.38

108.82

3.16

x

N. y. Ocean View

0+00

109.48

2.50

2.50

+ 0.04

111.80x

110.02

1.72

109.49

2.49

2.51

-0.02

Alleys Bk 1 + 2 (Superba Suburba) Hqts

42

BK 1

INDEXED

MK

N. line SEP 6 1950

Cl. 2' Ret. E.C. - 8' Prop.

104.57

104.71

7.27

x

105.25

6.73

x

±

104.85

—

105.12

S. Line

105.12

105.16

6.82

x

105.50

6.48

x

Alley Bk 2 (Superba) Hqts.
Superba

N. line Prop ← 8' Ret. E.C. 2' → Cl. line

N. line

105.30

6.68

x

104.77

7.21

x

104.63

INDEXED

MK
SEP 6 1950

±

105.16

—

104.88

S. line

105.52

6.46

x

105.21

6.77

x

105.13

39th Franklin to Superior

INDEXED

SEP 7 1950

BM#5
P.42

100.35
7.47
107.82
3.90
103.92
103.94
- 0.02
87.83
P.46

sly. Superior
2+70t

103.30
4.52
X

111.457
103.98
7.47

103.86
3.96
X

Nlx. line Alloy
1+45t

101.82
6.00
5.35
Top. ob.
0.65

sly. Line Alloy
130.t

101.61
6.21
5.59
Top. ob.
0.62

N.L. Franklin
0+00

99.70
8.12
X

106.291
100.45
5.84
33
6.17
L

100.40
7.42
X

Alley Bk.3 Suberba Hgts.

44

INDEXED

SEP 6 1950

Drop - 8' - EC. - 2 - ob.

BM#5 P.42

N. Line 102.40
5.42
X

101.94
5.88

101.82

100.35
5.74

106.29X

108.94
7.18

111.12

+ 33

111.45X

102.00

101.71

S. line

102.20
5.62
X

101.73
6.09
X

101.61

39th + Superior Int.

INDEXED
mk
SEP 7 1950

Noturnis
107.94 - 8.113-2-246
8.07
110.01

104.42
5.77
6.16 = 5.77

104.84
5.67

104.58
6.31

104.46
6.43

104.55
6.34

104.43
6.46

104.32
6.57

104.22
6.67

104.00
6.01

103.95
6.94

5.76

104.10
5.91

10'

15'

BA #5
103.94
6.62
110.56
+ 83
110.89 Sub. Dist.

39th

Superior

104.20
5.81

104.29
6.60

104.26
6.63

104.06
6.83

103.85
7.04

104.15

15'



103.99
6.02

104.12
6.77

104.09
6.80

103.88
7.01

103.50
7.39

103.57
6.46

8.12

10'

103.86
6.15

104.02
6.87

103.98
6.91

103.77
7.12

103.80
6.71

INDEXED
 mx.
 SEP 7 1950

P. 48
 B.M. #2

114.01
 1.25
115.277
 11.83
103.94

= S.W. 7'
 L+T.
 Superior.
 + 39 =
 BM #3

Prop. - 8' - B.C. - 2' - cl. 1190

Sly Suberba
 2+65t

113.20
 2.07

113.20
 5.11

112.40
 2.87

N.L.

109.16
 6.11
 x

108.94
 6.33
 x

108.59

Nly 1190 Alley
 1+40

108.89
 Nail 6.38
 6.53
 F 0.15

±

108.74

108.60

Sly Line Alley
 1+25

108.30
 Nail 6.97
 7.14
 F 0.17

S. 1190

108.81
 6.46
 x

108.40
 6.87

108.30

O+20 BIK

104.69
 10.58
 x

110.897
 105.25
 5.64
 x

105.02
 10.23
 x

Nly Superior
 O+00

109.00
 11.27
 x

104.55

109.42
 10.85
 x

39th + Suberba Int.

Superba

INDEXED
MK
SEP 7 1950

114.91
2.165

BM#2-PLA8

±39

BM#2-PLA8
114.01
4.194
118.817
119.305460.7

112.98

5.56
X

113.27

6.03
X

113.55

3.75
X

113.67

5.58
X

113.47

3.17
X

112.99
5.65
X

113.20

6.10
X

113.49

5.81
X

113.56

5.74
X

113.42

5.88
X

113.58

5.06
X

112.90

6.40
X

112.78

6.52
X

113.35

5.95
X

113.65

5.05
X

113.46

5.84
X

113.96

5.94
X

113.07

6.23
X

112.60

6.70
X

112.76

5.88
X

113.50

5.14
X

113.26

6.04
X

113.86

5.94
X

113.27

6.03
X

112.96

6.34
X

112.50

6.14
X

112.52

6.12
X

113.20

5.44
X

113.30

6.00
X

113.20

6.40
X

112.90

6.40
X

112.40

6.40
X

10'

10'

10'

10'

10'

10'

15'

15'

INDEXED

SEP 7 1950

Alley BIK. I

48

				B.M. #1		
sly. Imperial 2+47E	117.67 1.62 1.63 x	118.97X 117.95 1.02	117.83 1.46 1.49 0.03	B.P.S.E. 39+Imp. 118.40 0.89 119.29 5.28	Prop.	c.b. line
2+27.2 Brk	117.31 1.98 x	119.30X 117.47 1.83 x	117.43 1.86 x	114.01 = N.W. 7' Lot. Suberba = B.M. #2	N. line 116.11 3.18	115.74 3.54 - .07 3.48 - 2' back of c.b. line x
Nly. line Alley 1+40	115.74 3.55 3.84 Nail F.O. 29				± 115.76	115.60
sly. line Alley 1+25	Nail 115.47 3.82 4.11 F.O. 29				sly. line 115.91 3.38	115.47 3.82 - .9 3.73 Rod 2' back of c.b. line x
0+20 Brk	113.79 5.50 x	119.30X 113.92 5.38 x	113.25 6.04 x			
Nly. Suberba. 0+00	113.47 5.82 x	113.11 113.55 .42	0+10 112.98 6.31 x 113.38 2.44			

Senior grades
ANNA + PACIFIC Hy. Ely. Thru. P.L. 272

Sommermeier
McCoy
Allen
Buech

INDEXED
SEP 7 1950

N.O. 20468
3-9-50

B.M. = 1 + 10⁵⁶ $\frac{1875}{70}$

1 + 57.56
- 5.76
15.82
4.51
C 11.31

~~- 5.76~~
~~16.14~~
~~4.89~~
C - 11.45

4.92
11.38
16.30 X
11.38
4.92
5.46
10.38 X

2 + 75

10.38 X
- 5.59
15.97
0.75
C - 15.22

1 + 37⁵⁵
- 5.79
15.85
4.97
C 10.88

~~- 5.79~~
~~16.17~~
~~5.24~~
C - 10.93

2 + 75.
E. = 15.22
Gr. = - 5.59
1 9.63 = El. stab.
0.43

2 + 40

- 5.61
15.99
0.90
C - 15.09

1 + 17⁵⁶
- 5.82
15.88
5.25
C 10.63

~~10.38 X~~
~~- 5.82~~
~~16.20~~
~~5.50~~
C - 10.70

10.06 = X
2.39
7.67 = B.M. #1
R.R. spike in pole
N.E. Anna + Pacific

2 + 20

- 5.67
16.05
6.07
C - 7.98

0 + 94² = P.O.T. on E

See Page 53

0 + 36² = P.O.T. on E

2 + 00 - 5.70
15.76
4.149
C - 11.27

~~- 5.70~~
~~16.08~~
~~4.80~~
C - 11.28

Exist M.H. Pacific
0 + 00 Anna

1 + 37⁵⁵
- 5.79
15.85
- 0.4
15.81
12.00
C - 3.81
to nail

15.84
12.09
C - 3.73
to nail

- 6.00
1 + 17⁵⁵
10.06 X
- 5.82
15.88
- 0.4
No 15.84
12.16
C - 3.68
to nail in bulkhead

- 7.81 = Trunk
24.11
24.09
100% OK

15.84 south
12.19
C - 3.65

1 + 80 - 5.73
15.79
4.34
C - 11.45

~~- 5.73~~
~~16.11~~
~~4.53~~
C - 11.58

7.67 = B.M. #1

1.97
9.64 49

Restake

7 4 - 3 - 50
2.02 1/2 off
1 + 17.56
2.64
- 5.82
15.46
0.4
15.42
12.24
C - 3.18

2.14 1/2 off
- 5.82
- 5.82
15.46
- 0.4
15.42
12.24
C - 3.18

Nail in
No. stringer
1 + 37⁵⁵
9.64 X
- 5.79
15.43
- 0.4
15.39
12.29
C - 3.10
2.05 1/2 off.

Nail in
stringer
15.43
- 0.04
15.39
12.29
3.10
2.13 1/2 off

3+80¹²

$$\begin{array}{r} 9.61 \times \\ -5.43 \\ \hline 15.04 \\ 8.54 \\ \hline C-6.50 \end{array}$$

$$\begin{array}{r} 10.38 \times \\ 2.80 \\ \hline 7.58 \\ 3.66 \\ \hline \end{array}$$

End of Job.

5+00

$$\begin{array}{r} -5.25 \\ 14.86 \\ 4.89 \\ \hline C-9.97 \end{array}$$
3+60¹²

$$\begin{array}{r} 11.24 \times \\ -5.46 \\ \hline 16.70 \\ 10.25 \\ \hline C-6.45 \end{array}$$

$$\begin{array}{r} 11.24 \times \\ 10.25 \\ \hline 0.99 \\ 8.62 \\ \hline 9.61 \\ 0.06 \\ \hline 9.55 \\ 0.69 \\ \hline \end{array}$$

A+75

$$\begin{array}{r} -5.29 \\ 14.90 \\ 5.06 \\ \hline C-9.84 \end{array}$$
3+40¹² ± special
Joint
$$\begin{array}{r} -5.49 \\ 16.73 \\ 3.66 \\ \hline C-8.01 \end{array}$$

$$\begin{array}{r} 10.24 \\ 5.32 \\ \hline 14.92 \checkmark \\ \text{only B.M.} \end{array}$$

A+50

$$\begin{array}{r} -5.33 \\ 14.94 \\ 5.00 \\ \hline C-9.94 \end{array}$$

3+25

$$\begin{array}{r} -5.51 \\ 16.75 \\ 7.10 \\ \hline C-9.65 \end{array}$$

A+25

$$\begin{array}{r} -5.36 \\ 14.97 \\ 4.66 \\ \hline C-10.31 \end{array}$$

3+05

$$\begin{array}{r} -5.54 \\ 16.78 \\ 3.62 \\ \hline C-13.16 \end{array}$$

A+00

$$\begin{array}{r} -5.40 \\ 15.01 \\ 6.99 \\ \hline C-8.02 \end{array}$$

2+90

$$\begin{array}{r} 11.24 \times \\ -5.57 \\ \hline 16.81 \\ 3.66 \\ \hline C-13.15 \end{array}$$
± special
3+9A¹² = Joint
$$\begin{array}{r} -5.41 \\ 15.02 \\ 7.71 \\ \hline C-7.31 \end{array}$$

Witterby Underpass Drain

Sommer

3-15-50

W.O.# 20453

Rate on 7603-L = 3.23%

ii set to miss exist drain = 3.66%

S.W.B.P. Witterby + Moor

INDEXED
SYST.
SEP 7 1950

27.73

0.80

28.53

11.93

16.60

1.01

17.61

6.72

10.89

2.48

13.379

4.50

8.87

3.60

C-5.27

3.32

10.95

3.33

C-6.72

+1.49

11.88

3.19

C-8.69

-0.34

13.71

5.59

C-8.12

-2.17

15.54

6.68

C-8.86

-3.75

17.12

7.10

C-10.02

+9.50

9.87

3.60

C-6.27

+2.46

10.91

3.83

C-7.58

+9.84

12.53

3.19

C-9.34

-0.77

14.4

5.59

C-8.55

-2.39

15.76

6.68

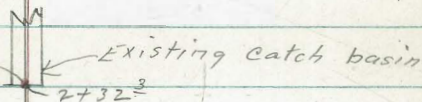
C-9.08

-3.77

18.14

7.10

C-10.04

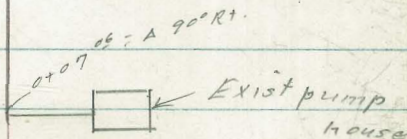


2+00

1+50

1+00

0+50



Scott - South of Lowell

4/3/50

N.O. 22004

52

0+00 = 100' Sly. from Sly. line Lowell.

Ed. Nail in Bldg. 0+00 Lt.

Sommermeier
McCoy
Allen

West.
Butter

±

East
gutter

Berm Cr. 1.27

Cut = 2.30

El. Nail 3.57

3.82

7.39 X

0+80

1.95

2.12

1.58

INDEXED

MK

SEP 7 1950

3 0+60

1.40

1.60

1.07

5.99

5.79

6.76

6.77

F 0.77

F 0.98

0.75 over old pavement - required
clearance.

0+40

0.99

1.19

0.68

6.40

6.20

6.75

6.84

F 0.25

F 0.64

0+20

0.75

0.93

0.42

6.69

6.46

6.75

6.86

F 0.11

F 0.40

0+00

7.39 X

0.60

0.60

0.30

6.79

6.79

6.74

6.82

C 0.05

F 0.03

No paving
on this
line

Anna St + Pacific Hy Sewer

From P. 49

4/10/50

(Nail 10' Rt. - Line only)

Stub 10' Lt.

O+1A

-5.98

23.50

7.25

C-16.25

BM#1 P.49

7.67

7.85

17.52 X

Stub 10' Lt

O+03

0.510

-6.00

23.52

8.62

C-14.90

O+00 =

-6.00

23.52

8.60

C-14.92

on Rly R/W, M.H.

Pump House
La Jolla Hermosa

54

Sommermeier

Allen
Sherman

Nly + Ely lot lines located
as shown on sheet 1530 D.

INDEXED
mk.

SEP 7 1950

Sot. B.M. 7' tack. at E.C. ^{179A}
5A

5.79 24.56

Check Expt M.H. #5
FB1429-1

0.23 30.13 (30.13) ^{ok}

M.H. #6 819 30.35

— 22.16

FB1429
/

Pump House
Bird Rock

±
Bird Rock

55

INDEXED
MS
SEP 7 1950

X = cross in Conc

□ = stub

Grade from M.H. (I.E. = 19.00 at 1532D) to
Exist M.H. ± Bird Rock & Dolphin Pl.

0+25	0+00	0+10	0+20	0+30	0+40
M.H. to	19.65	19.91	20.17	20.42	20.66
bc Const.	10.81	11.55	11.29	11.04	10.80
	5.33	5.03	4.76	4.53	4.18
19.00	C-6.48	C-6.52	C-6.53	C-6.51	C-6.62
0+50	0+53 = Exist M.H.		B.M.		
	20.92	20.96	26.07		
	10.54	10.50	5.44		
	3.88	3.82	31.46X		
	C-6.66	C-6.68			

cb. (End of
Bird rock
roadway)

Pump House

4'

Located as shown
on sheet 1532D.

Set B.M. chiselad □ in
So. Cl. Bird rock
(See opposite page)
20' from end of Cl.

A.41 26.02

S.E. 10' ±
Dolphin
Bird Rock.

2.80 30.43

— 27.63

FB 1646
39

41

Pump House
Gravilla St.

Sommermeier
Allen
Sherman

4/27/50

sheet 1528-D ✓

x = cut cross in conc.

. = nail

INDEXED

SEP 7 1950

x - on steps,
(opposite page)

N.E.B.P.

Gravilla

Vista Del Mar

10.79 18.02

0.49 28.81 — 28.32

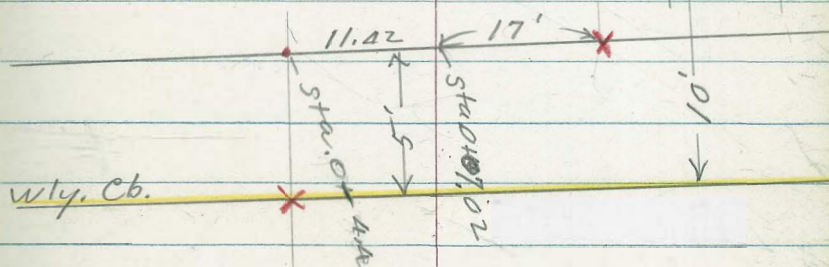
Gravilla

Nly line
Pump house

4' EXIST 56
conc steps.

set B.M.

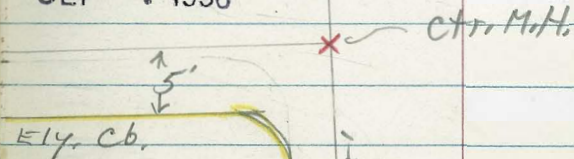
EL. = 18.02



Neptune place.

INDEXED

SEP 7 1950



Alloy BIK 59 Univ. Hgts.

5/17/50

Sommermayer
Begg
Alloy
Shannon

W.O. 31707

57

	West	East	West	East
			3+32	
			U-1'	
			384.68	384.88
			5.68	5.48
			5.14	5.39
			C-0.54	C-0.09
1+28	383.36	383.56		
	5.41	5.21		
	5.07	4.53		
	C-0.34	C-0.68		
			3+01	
			W-12	
			384.36	384.56
			6.00	5.80
			5.46	4.57
			C-0.54	C-1.23
			2+70	
			384.05	384.25
			6.31	6.11
			6.07	5.29
			C-0.24	C-0.82
0+60	383.08	388.77X 383.28		
	5.69	5.49		
	5.34	5.04		
	C-0.55	C-0.45		
			2+50	
			383.88	390.36X 384.08
			6.48	6.28
			6.11	5.24
			C-0.37	C-1.04
0+40	382.92	386.50X 383.13		
	3.58	3.37		
	2.20	2.70		
	C-1.38	C-0.67		
			2+30	
			X-2'	
			383.77	388.77X 383.97
			5.00	4.80
			4.66	3.70
			C-0.34	C-1.10
0+20	382.61	382.82		
	3.89	3.68		
	4.04	2.71		
	C-0.15	C-0.97		
			1+96	
			383.64	383.84
			5.13	4.93
			4.68	4.57
			C-0.45	C-0.36
0+00	382.23	382.44		
	4.27	4.06		
	✓	✓		
			1+62	
			383.50	383.70
			5.27	5.07
			5.24	4.22
			C-0.03	C-0.85

INDEXED

MK

SEP 6 1950

0+94

X-2'

383.22

5.55

4.76

C-0.79

383.42

5.35

4.77

C-0.58

0+60

383.08

5.69

5.34

C-0.55

388.77X

383.28

5.49

5.04

C-0.45

0+40

N-0.40

382.92

3.58

2.20

C-1.38

386.50X

383.13

3.37

2.70

C-0.67

0+20

D-1'

382.61

3.89

4.04

C-0.15

382.82

3.68

2.71

C-0.97

0+00

382.23

4.27

✓

382.44

4.06

✓

	West	East
5+18	386.57 5.36 4.97 C 0.39	386.77 5.16 4.29 C 0.87
A+87	386.25 5.68 5.49 C 0.20	X-2 386.45 5.48 4.45 C 1.03
A+56	385.94 5.99 5.90 C 0.09	386.14 5.79 5.45 C 0.34
A+25	385.62 6.31 5.62 C 0.69	391.93X 385.82 6.11 5.48 C 0.63
3+94	385.31 5.05 5.36 C - 0.31	390.86X 385.51 4.85 4.91 F 0.06
3+63	Oh. 0.10 384.99 5.37 4.92 C 0.45	390.36X N. 0.10 385.19 5.17 4.97 C 0.70

2+65-15' Lt = 9. Lat. #1 EL = 379.01
 11.35
 6.43
 C - 4.93

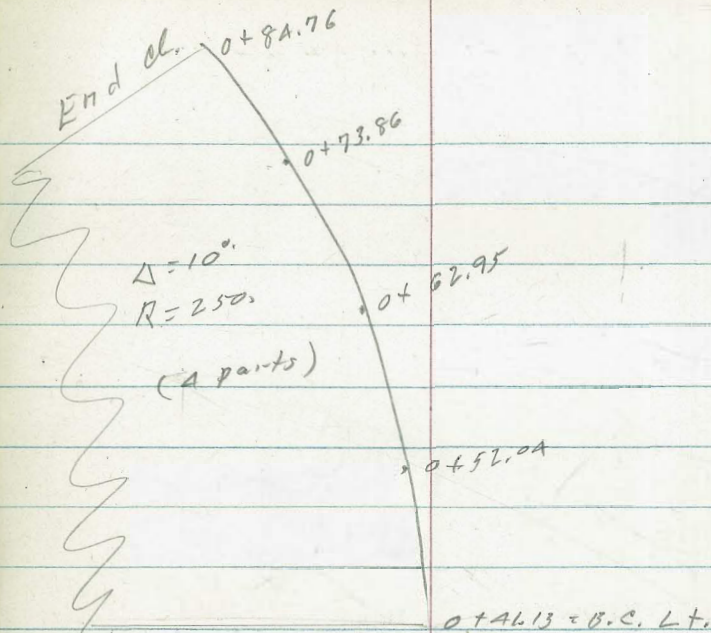
	West	East
6+00	387.38 4.56 4.55 X	387.48 4.46
5+80	387.22 4.74 4.92 F 0.18	U-2 391.94X 387.40 4.54 3.99 C 0.53
5+49	386.88 5.05 4.87 C 0.18	391.93X 387.08 4.85 4.32 C 0.53

Ch. N. Ely. Midway + Frontier

INDEXED
 MK
 SEP 7 1950

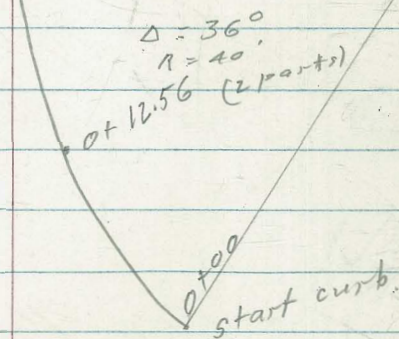
Start ch.		E.C.	B.C. Lt.
0+00	0+12.56	0+25.13	0+41.13
<u>4.42</u>	<u>4.38</u>	<u>4.34</u>	<u>4.17</u>
4.14	4.18	4.22	4.39
<u>5.88</u>	<u>5.35</u>	<u>5.44</u>	<u>5.132</u>
F 1.74	F 1.17	F 1.22	F 0.93

			End ch.
0+52.04	0+62.95	0+73.86	0+84.76
<u>4.12</u>	<u>4.08</u>	<u>4.04</u>	<u>4.00</u>
4.44	4.48	4.52	4.56
<u>5.12</u>	<u>5.02</u>	<u>5.13</u>	<u>4.48</u>
F 0.68	F 0.54	F 0.61	C 0.09



7830' ✓
 = 5+19 $\frac{1}{2}$ feet. Set.
 40' el. Rad.

B.M. on Culvert
 Head wall
 2.90
5.66
 8.56



Pave. N.E. Midway + W. Pt. Loma

Stations from 7829-L.

5+19 $\frac{3.84}{6.34}$

B.M.
2.90
7.28
10.18 X
4.00
6.12
4.15
10.27 X

E.C. 0+50
=0+00 $\frac{4.32}{5.95}$
C.16
F0.21

1+00 $\frac{4.09}{6.18}$
6.45
F0.27

1+62 $\frac{3.79}{6.48}$
6.48

Prop. E.C.
A+70⁵⁰ $\frac{4.77}{5.81}$
6.46
F0.65

INDEXED
7/7
SEP 7 1950

10.27 X

A+33⁶⁰ $\frac{4.78}{5.40}$
5.62
F0.22

0+50
6.02
4.25
4.28
F0.03

1+00
5.52
4.75
4.36
C0.19

1+50
5.02
5.25
5.16
C0.09

E.C. 1+70.13
4.55
5.72
5.95
F0.23

Pav. E.C.
3+95⁶³ $\frac{5.18}{5.00}$
5.36
F0.36

1+25
6.32
3.86
3.94
F0.08

P.R.C. 1+43.38 = 0+00
6.49
3.69
3.99
F0.30

0+10
6.42
3.76
4.06
F0.30

10.18 X

0+25
5.41
4.77

0+50
5.64
4.54
4.90
F0.36

0+75
5.87
4.31
4.59
F0.28

1+00
6.10
4.08
X

0+00 paving E.C. = 3+95⁶³ opposite page.

Sewer Laterals
 Lowell St Rosecrans to Harbor Dr
 Sheet 7AAL-L

62

Sommermejer

6/9/50

INDEXED
 MK
 SEP 7 1950

B.M. sly ab. F.C. scott + Lowell E.L.: 2.69
 (7AAL-L)

2.69
 4.71
 7.40 X
 4.91
 2.49
 3.96
 6.45 X
 3.76
 2.69 only B.M.

Lat #1	Lat #2	Lat #3
7.10 X	6.45 X	6.45
-2.45	-2.50	-2.55
9.85	8.95	9.00
5.10	4.30	4.69
C-4.75	C-4.65	4.31

Lat #4	Lat #5	Lat #6
		6.25
-2.90	-2.90	-2.90
9.35	9.35	9.35
5.00	4.67	4.50
C-4.35	4.68	C-4.85

INDEXED

Alley Bk 62 Ocean Beach

MK
SEP 6 1950

Paving Grades

63

Sommermeyer

5-12-50

Be99
Allen

Sheet 7565-1

3+00

South

±

North

South

±

North

S.E.B.P.

Cable

Niagara

1+20

0-2'

19.83

5.94

5.56

C-0.38 ✓

X-3'

19.63

6.14

5.72

C-0.42 ✓

19.94

5.83

25.77 X

6.54

19.23

4.45

23.68 X

2+60

N-0.82

18.97

4.71

3.35

C-7.36 ✓

0-2'

18.77

4.91

4.79

C-0.12 ✓

1+00

0-2'

20.04

5.73

5.38

C-0.35 ✓

X-3'

19.84

5.93

5.69

C-0.24 ✓

2+20

N-0.08

19.18

4.50

3.96

C-0.34 ✓

0-1'

18.98

4.70

4.52

C-0.18 ✓

0+60

0-2'

20.48

5.29

4.60

C-0.69 ✓

X-3'

20.28

5.49

4.96

C-0.53 ✓

1+80

25.77 X

0-2'

19.39

6.38

6.11

C-0.27 ✓

0-1'

25.77 X

19.19

6.58

6.58

X ✓

0+20

0-2'

20.93

4.84

3.55

C-1.29 ✓

0-2'

20.73

5.04

3.60

C-1.44 ✓

1+60

19.51

6.26

6.08

C-0.18 ✓

0-2'

19.31

6.76

6.25

C-0.21 ✓

cable

Wly line

0+00

25.77 X

20.97

4.80

L

25.77 X

20.95

1+40

0-2

19.66

6.11

5.77

C-0.34 ✓

0-2'

19.46

6.31

5.80

C-0.51 ✓

	South	±	North
5+20	X-2' 17.55		17.37
	5.12		5.30
	4.37		4.89
	C-0.73 ✓		C-0.41 ✓

	0-2'		0-2'
5+00	17.71		17.51
	4.96		5.16
	4.46		4.59
	C-0.50 ✓		C-0.57 ✓

	X-2'		0-15'
4+60	17.92		17.72
	4.75		4.95
	4.35		4.89
	C-0.40 ✓		C-0.06 ✓

	0-2'		N-1.17
4+20	18.13		17.93
	4.54		4.74
	4.31		3.35
	C-0.23 ✓		C-1.39 ✓

	X-0.20		0-15'
3+80	22.67X		22.67X
	18.34		18.14
	4.33		4.53
	3.92		4.34
	C-0.41 ✓		C-0.19 ✓

	23.68X		0-1'
3+40	0-0.25		23.68X
	18.55		18.35
	5.13		5.33
	5.13		5.11
	X		C-0.22 ✓

Sewer Laterals

#1	#2	#3
0+15-south	0+65-south	3+20-North
25.77X	25.77X	23.68X
15.94	15.43	13.46
9.83	10.34	10.22
3.40	5.03	5.08
C-6.43 ✓	C-5.31 ✓	C-5.14 ✓

	South	±	North
--	-------	---	-------

Ely Bacon, 6+00	22.67X 16.08		22.67X 15.93
	6.59		6.74
	06.00		

	0-2'		0-2'
5+80	16.55		16.39
	6.12		6.28
	4.19		4.59
	C-1.93 ✓		C-1.69 ✓

	0-2'		0-2'
5+60	16.98		16.80
	5.69		5.87
	3.96		4.70
	C-1.73		C-1.17 ✓

	N-0.40		0-2'
5+40	17.32		17.13
	5.35		5.54
	3.77 ✓		4.82 ✓
	C-1.58		C-0.72

Evergreen St.
Lowell to Keats

7/18/21

Obs. ^{Sub. E.} _{rough} _{Admitted}

X 32.86
7.48
25.38 = S.E.B.P. Evergreen Lowell

65

B.M. #2

Sommermeier

FB 1853

32

Sheet # 7776-L

→ 26.17
4.02
X 30.19

From $\frac{1853}{33}$ B.M. #1

S.E. Mon Lowell + Evergreen

EL: 261.7

26.17
6.69

East
Rough Curb

East
Gutter

West
Gutter

West
Ch.

Rough Gr.

1 + 25

32.86 X
T.P. 9.75

24.23

24.33
5.86
1.11
24.23
5.44
5.71
FO 27

24.61
5.92

25.00
5.19
5.61

25.00

1400

23.11
4.128
27.39

8.53
7.56
C 0.97

4.42
4.69
5.12
FO 43

25.50
4.69
5.12

7.86
4.120

C-3.46

INDEXED
MKI
SEP 7 1950

0 + 75

25.16
7.70
6.83

25.16
5.03
5.32
FO 19

25.33
5.00

26.00
4.12
4.70
FO 51

26.00

0 + 50

C-0.87

25.38
4.61
5.04
FO 45

26.44
4.01

26.00
3.69
4.29
FO 60

C 3.54

Ch. E.C.

0 + 25

26.00
6.86
5.52
C 1.34

26.00
4.12
4.68
FO 49

26.44
4.01

27.00
3.19
3.90
FO 11

27.00

5.86
2.50
C 3.36

0 + 12.5 8° 53' 15"

^{40' Rad}
2' BK C = 12.36

26.10
6.76
5.90
C 0.86

26.10
4.09
4.48
FO 39

27.03
3.16
3.69
FO 53

27.03

5.83
2.50
C-3.33

S.L. Lowell

0 + 00 Defl. = 17° 46' 30"

2

26.08
6.78
6.77
.01

26.08
4.11
4.10

26.33
3.64
3.98

27.08
3.11
3.10

27.08

5.78

Evergreen

66

Lowell to Keats

	East		East		West		
	Rough Br	Curb	Gutter	±	Gutter	Curb	Rough Br.
N. Line Keats 2+00 L=17°46'30"	22.87 9.77 9.77 .02	22.87 7.32 7.29		23.26 6.93		24.46 5.73 5.72	24.46 8.40 8.38 C-0.02
1+875 L=8°53'15"	23.20 9.66 9.43 C-0.23	23.20 6.99 7.24 FO ²⁵				24.10 6.09 6.32 FO ²³	24.10 8.76 5.25 C-3.51
Ch. B.C. 1+75	23.50 9.36 8.55 C-0.81	23.50 6.69 7.08 FO ³⁷		23.69 6.84		24.00 6.19 6.40 FO ²¹	24.00 8.86 4.86 C-1.00
1+50		23.92 6.27 6.52 FO ²⁵				24.50 5.69 6.10 FO ⁴¹	

Evergreen
Keats to Jarvis.

T = 30 12

67

East

East
Gutter

West

Gutter

Curb

Rough Cr.

Rough Cr.

Curb

±
22 22
824

22 20
742

22.70

796

4.69

F042

2.50

22 85

C-2.19

754

776

F041

23 00

23.00

719

4.39

758

1.54

F039

C-2.85

23 15

704

750

F046

22 64
789

22 98
754

23 30

23.30

689

4.09

730

1.79

F041

C-2.30

23 50

23.50

669

3.89

703

1.56

F034

C-2.33

23 03
716

23 82

27.39*

637

23.82

632

3.57

3.55

.02

1+25

X-4'

22 00

819

22.00

5.39

802

7.77

F043

F 2.58

22 20

792

823

F024

1+00

INDEXED
SEP 7 1950

0+75

0-7'

22 40

779

22.40

4.99

819

7.93

F040

F 2.94

22 60

759

807

F048

0+50

Cl. E.C.

0+25

0-2'

22.80

22 80

4.59

739

6.87

782

F 2.28

F043

0+125 X=8'53" K"

22.73

22 73

4.66

746

6.87

771

F 2.21

F026

K from P. 65

S.L. Keats

0+00 K=17°46'30"

27.39

22 66

22.66

4.73

753

4.72

757

C

Evergreen

68

Keats to Jarvis

East

West

	Rough Cr.	Curb	Gutter	±	Gutter	Curb	Rough Cr.
N.L. Jarvis 2+00±17°46'30"	21.23 6.16 6.14 1.02	21.23 8.96 8.93		21.70 8.49		22.53 7.66 7.63	22.53 4.86 8.84 1.02
1+87.5 128°53'15"	a-4 21.45 5.94 7.41 F-1.47	21.45 8.74 9.06 F0.32				22.44 7.75 7.98 F0.23	22.44 4.95 2.13 C-2.82
Ch. B.C. 1+75	27.39 21.60 5.79 7.75 F-1.96	21.60 8.59 8.76 F0.37		21.94 8.59		22.40 7.79 8.03 F0.24	27.39 22.40 4.99 2.20 C-2.79
1+50		21.80 8.39 8.07 F0.30				22.53 7.64 8.07 F0.43	

Stake Meter Boxes

Upsthur St 7/20/50

Sommermeier
Begg
Aentra

W.O.

stakes set 3' back of curb face
2' Each side of Box.

21.97X
Ch. 18.25
3.62
3.63
-0.01 X

SW. 7' Lt. Rosecrans &
Upsthur.

19.55
2.42

21.97X

Lt. & Rt.

1+73 Rt

14.48
7.49
6.96
C-0.63

INDEXED

SEP 7 1950

1+32 Rt

15.56
6.41
6.03
C-0.38

Lt. Rt.

3+00 1/2 Wly. line south

2+69 Rt.

11.96
10.01
8.52
C-1.49

1+02 Lt.

16.85
5.12
5.60
F0.48

2+52 Lt

12.90
9.07
8.25
C 0.82

0+72 Rt.

17.14
4.83
4.10
C-0.63

2+32 Rt

12.93
9.04
7.94
C-1.10

0+00 = Ely line Rosecrans

Stack Water Meter Boxes
Evergreen
Fenelon to Carlton

70

Sommermeier

7-21-50

Begg
Acuna

W.O. 60020

0+40 RT

INDEXED
MK
SEP 7 1950

26.51 X
21.12
5.39
3.86
C-1.73

B.M. = Sly, 7' Dick Emerson & Evergreen

0+00 = Sly, line Dickens

El. = 18.50
5.35

23.85 X

3.47

20.38

6.13

26.51 X

W. End of Ret.

N.W. Cor. Evergreen

+ Dickens

26.51 X
23.50
3.01
2.28
C-0.73

1+56 RT

21.45

24.0

2.81

C-1.59

1+03 RT

23.85 X
19.74
4.11
2.42
C-1.69

1+20 RT

23.85 X

22.30

1.55

0.25

C-1.30

0+57 RT

19.46
4.39
2.75
C-1.64

0+00 = Sly line Fenelon

0

0+00 = Sly line Emerson

Auburn Dr. at Ontario
stake Culvert.

W.O. 20008

7-25-50

Sommermeier

Begg

Allen

Acuña

INDEXED

SEP 7 1950

Ref.

F.B. 2077

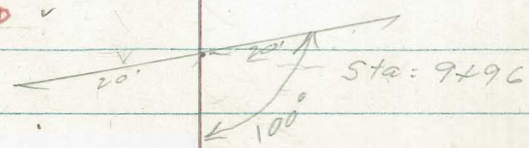
10

sheet 3993-B

stakes set 10' North of \pm
staked 40' of twin barrel 48" pipe
20' each side of \pm Auburn Dr.

256.60

247.77	247.87	247.97
8.83	8.73	8.63
5.75	7.49	7.04
C 3.08	C 1.24	E 1.59 ✓
D ✓	D ✓	



B.M. = top of cb. 14" Lt. Sta 10+16.7 FB 2077
19

251.42 = B.M.
5.18
256.60 ✓

Alley BIK 18 La Jolla Park
 BIK 22
 Stake for Const. 7-26-80
 W.O. 62182

Sommermeier
 Bogg
 Allen
 Bunch

FB 1853-37
 sheet 80A1-L

Left = West ±
 Right = East

INDEXED
 MK
 SEP 6 1950

	Left = West ±	Right = East	
5+70	91.26 ✓	91.56	SE, B.P. Pearl & Girard
	7.06	6.76	
	6.92	6.70	
	C-0.14	C-0.06	115.17
			0.04
5+50 ✓	91.71	92.01	115.21
	6.61	6.31	11.75
	6.58	6.07	103.46
	C-0.03	C-0.24	2.46
		C-0.45	105.92
		tack - 2'	10.40
			95.52
5+00	92.75	93.00	2.80
	92.96	93.26	78.37
	5.36	5.06	
	5.70	5.30	
	F-0.34	F-0.24	
	F-0.13	C-0.02	
		x-1'	
4+50	93.60	93.70	94.51
	74.21	94.51	3.81
	4.11	5.10	5.10
	4.80	F-1.27	F-1.27
	F-0.29	F-0.27	F-0.27
	F-0.08	F-0.48	F-0.48
		N. 0.517	
4+00	94.80	95.00	95.77
	95.47	95.77	2.55
	2.85	2.55	0.64
	2.80	0.64	
	C-0.05	C-1.91	
	67	77	
	C-0.72	C-2.68	

EXTENSION

4+365 92²⁴ 72
 Check grate 1856

5' Lt. + 5' Rt.
 6+23²⁴ = 4
 Catch Basin
 Cut from 0-5' Lt.
 8630 = 1 E.
 12.02
 6.70
 C-5.32

92.98 41
 5.34
 5.75
 .01 ✓
 Changed by E.G. + O.S.
 0.00 = changed grades + cuts
 To fit Imp.
 Use Circled Figures
 Note.

Left = West ±
 Right = East

	Left = West ±	Right = East
6+28.08 Lt.	90.56	
	7.76	
	6.67	
	C-1.09	
6+23.35 Rt.		90.89
		7.43
		5.80
		C-1.63
6+10	90.68	90.98
	7.64	7.34
	6.85	6.28
	C-0.79	C-1.06
5+90	90.92	91.22
	7.40	7.10
	7.21	6.27
	C-0.19	C-0.83

Stake
TYRIAN ST.

7-31-50
W.O. 31347

73

Sommermeier
B 999
Allen
Bunch

Sheet # 7711-L
7712L
FB- 1826-P58

West Curb	West Gutter	East Gutter	East Curb
-----------	-------------	-------------	-----------

1000 = Back (North) side of wall.
0+99 = Retaining wall

Prop.	72.73		
	69.45	69.40	69.60
		3.33	
		4.83	
		<u>F1.50</u>	
			69.80
			2.93
			4.29
			<u>F1.36</u>

INDEXED

0+9933
1000 = End Pav

SEP 7 1950

Rough	Rough	East Gutter	East Curb	Rough	Grade
0-5' South	72.73				0-2'
0-5' West	69.40	68.90	69.10	69.30	69.80
	4.03	3.33			3.63
	5.88	4.83			4.77
	<u>F1.85</u>	<u>F1.50</u>			<u>F1.36</u>

SW 7' 1/2 +
Marine + La Jolla
FB 1826-P59

0+96

0-5'	72.73				72.73	0-5'
	68.88	69.39	69.39	68.89	69.29	69.29
	4.55	4.04	3.34			2.94
	73.43 X	5.88	4.77			4.24
		<u>F1.84</u>	<u>F1.43</u>			<u>F1.30</u>

0+48

BA
68.88
3.85
72.73

0-2'	72.73				72.73	0-1'
	69.24	69.24	68.74	69.14	69.14	69.64
		3.49				3.79
		4.19	4.24			3.24
		4.95	F0.75			2.98
		<u>F0.76</u>				<u>C0.11</u>

0+00 Nly. Marine

0-1'	73.43	72.73				73.43
	69.10	69.10	68.60	69.00	69.00	69.50
		4.33	3.63			3.93
		4.68	3.99			3.91
		<u>F0.35</u>	<u>F0.36</u>			<u>0.02</u>

0+05 = Ch. E.C. 11/1/50

	72.73				72.73	
	69.05	68.55	68.90	68.99	69.41	
					3.32	

Alley. Blk 2 LaJolla Park

Sommerville
Boggs

8-1-50
Sheet 7712-L
W.O. 31347

Pauc. at 0+00

Allen
Bunch

0.40 dip to E

B.M. shown on plans is gone.
Used pavement for Elev. See Page 98

	Lt. East	±	Rt. West		Lt. East	±	Rt. West		Pauc. at 0+00 on ±
	66.74 X		65.10 X	2+80	66.74 X	62.80	63.35	X-0.25	56.77
	59.66	59.11	59.36		63.35		63.05	4.86	61.63 X
	7.08		5.74		3.39		3.69		3.38
	6.03		5.37		3.11		3.52		58.25
	C-1.05		C-0.37		C-0.28		C-0.17		6.85
									65.10 X
0+80	66.74 X		65.10 X	2+60	X-2'	62.35	62.60	N-0.20	3.76
SEP 6 1950	59.66	59.11	59.36		62.90		62.60		61.34
	7.08		5.74		3.84		4.14		5.40
	6.03		5.37		3.52		2.83		66.74 X
	C-1.05		C-0.37		C-0.32		C-1.31		3.47
									63.27
0+60	65.10 X		65.10 X	2+20	0-3'		61.89	N-0.18	6.93
	59.17	58.62	58.87		62.19		61.89		70.20 X
	5.93		6.23		4.55		4.85		
	4.81		5.43		4.61		3.79		
	C-1.12		C-0.80		F-0.06		C-1.06		
					66.74 X		65.10 X		
0+40	65.10 X		65.10 X	1+80	66.74 X		61.18	N-0.22	
	58.59	58.04	58.29		61.48		61.18		
	6.51		6.81		5.26		3.92		
	4.96		6.02		5.01		2.17		
	C-1.55		C-0.79		C-0.25		C-1.75		
0+20	61.63 X		61.63 X	1+40	60.77		60.47	X-0.1	N-0.25
	57.93	57.38	57.63		4.33		4.63		60.47
	3.70		4.00		3.83		4.50		4.63
	0.51		3.38		C-0.50		C-0.13		3.46
	C-3.19		C-0.62						C-1.17
Soiling Pearl 0+00	61.63 X	61.63	61.63 X	1+00	65.10 X	59.51	65.10 X		
	57.35	56.77	57.00		60.06		59.76		
	4.28	4.86	4.63		5.04		5.34		
	4.36	4.86	4.62		4.41		5.65		
	+0.08	X	-0.01		C-0.63		F-0.31		

Alley BIK 2 - La Jolla Park

	Lt= East D-1'	±	Rt= West N-Line
4+00	65.94 4.26 3.86 C-0.40	65.79	65.64 4.56 4.44 C-0.12
3+90	□-2' 65.50 4.70 4.22 C-0.48	65.30	X-2 65.20 5.00 5.25 F-0.25
3+80	N-0.26 65.23 4.97 3.08 C-1.87	64.68	X-2 64.93 5.27 5.25 C-0.02
3+60	X-2 64.99 5.21 4.92 C-0.29	64.44	X-2 64.69 5.51 5.55 F-0.04
3+40	X-2' 64.65 5.55 5.54 C-0.01	64.10	X-2 64.35 5.85 5.68 C-0.17
3+20	X-2' 64.22 5.98 5.74 C-0.24	63.67	□-4' 63.92 6.28 6.30 F-0.02
3+00	X-2' 70.20 63.73 6.47 6.17 C-0.30	63.18	70.20 63.43 6.77 7.23 F-0.46

0+10 Rt Lat #1	0+60 Rt Lat #2	1+10 Rt Lat #3
52.09	53.09	54.09

Alley BIK. 3. La Jolla Park

76

8-2-50

W.O.#31347

INDEXED

Sheet 7711 L.

Sommertmeyer

Begg
Allen
Bunch

SEP 6 1950

0.30 dip to E

stubs v' back unless noted.

	Lt = East	±	Rt = West		Lt = East	±	Rt = West	
				3+00	81.73X Lt = East		81.73X Rt = West	SE. R.P. Pearl + Cuvier
					N-.91		N.0.06	
					77.86	72.41	77.56	
					3.87		4.17	81.06
					2.38		2.58	1.97
					C-1.49		C 1.59	83.03
								9.66
				2+80	N-.91		0-1'	73.37
					77.51	77.06	77.21	5.53
					4.22		4.52	78.90X
					2.65		4.35	3.17
					C 1.57		C 0.17	75.73
0+80	0-1'							6.00
	74.04		73.7A					81.73X
	4.86		5.16					3.29
	3.95	Rate	4.12	2+40	76.81		76.51	78.44
	C-0.91		C 1.04		4.92		5.22	5.64
					4.22		5.29	
					C-0.70		F 0.07	84.08X
0+40	N-0.04							
	73.35	72.90	73.05		X-2		N-.25	
	5.55		5.85	2+00	76.12		75.82	
	3.44		5.77		5.61		5.91	
	C 2.11		C-0.08		4.90		4.96	
					C 0.71		C 0.95	
0+20	N-2'							
	73.00	72.55	72.70		81.73X		81.73X	
	5.90		6.20	1+60	75.42		75.12	
	5.13		5.98		6.31		6.61	
	C-0.77		C-0.22		5.42		6.19	
					C 0.87		C 0.42	
					78.90X		78.90X	
S. line Pearl	78.90X		78.90X		0-1'		74.43	
0+00	72.93	72.44	72.38	1+20	74.73		4.47	
	5.97		6.52		4.17		4.25	
			6.53		3.48			
			0.01		C-0.69		C 0.22	

	Lt= East	±	Rt= West
3+99 ⁹⁸	N-1.08 80.00 <u>4.08</u> 2.57 C-1.49	79.55	79.70 <u>4.38</u> 4.28 C-0.10
3+80	79.55 <u>4.53</u> 4.01 C-0.52	79.10	N-2.66 79.25 <u>4.83</u> 2.35 C-2.48
3+60	79.10 <u>4.98</u> 4.24 C-0.74	78.65	78.80 <u>5.28</u> 4.95 C-0.33
3+40	78.66 <u>5.42</u> 4.57 C-0.85 N-.68	78.21	78.36 <u>5.72</u> 4.96 C-0.76
3+20	84.08X <u>78.25</u> 5.83 4.71 C-1.12	77.80	84.08X <u>77.95</u> 6.13 6.00 C-0.13

Sewer La Jolla Shores Dr.
North of Camino Del Oro.

5/31/50

79

INDEXED

SEP 7 1950

B. sheet #3989

0+00	0+25	0+50	0+75
35.60X			
22.10	22.45	22.70	22.95
13.40	13.15	12.90	12.65
5.83	4.66	4.51	3.67
C-7.57	C-8.49	C-8.39	C-8.98

1+00	1+25 ⁴⁶ stub end
23.20	23.43
12.40	12.17
1.93	0.66
C-10.47	C-11.51

$$B.M. = I.E. \text{ @ } \text{Exist} + M.H.$$

$$= 21.94$$

$$\frac{13.66}{35.60X}$$

Villy Ch. La Jolla Shores Dr.

EXIST 8" SEWER

cut cross in d.

59.80

cut cross in pave

Ed. LS #2341

71.32

15'08"

1+25⁴⁶

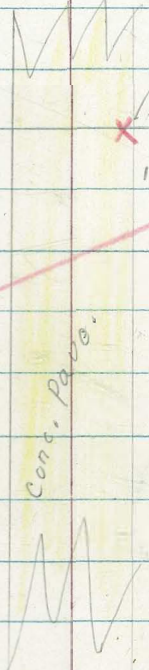
74°52'

0+00

conc. pave.



N



Rosecrans

Sewer Extension North of Rogers

80

Sommermayor
Begg
Allet
Sherman

5/31/50

1+00 30.20
7.06
4.06
C 8.00

INDEXED
M.K.
SEP 7 1950

sheet # 5590-L

N.E.B.P. Perry &
Rosecrans

0+00 = M.H. #4 - (5590-L)

6415
218
6633
12.86
53.47
1.26
54.73
12.73
42.00
0.13
42.13
10.09
32.09
5.17
37.26 X

0+50

29.70
7.56
5.15
C-2.41

0+00 = A 22°-47' Rt.

3726 X
9.36
27.90 EL. EXIST M.H.

0+00 =
M.H. #4

29.20
8.06
5.34
C-2.72

EXIST M.H. #
(5590-L)

M.H. #2

1+00 33.15 sep. Pa. va. 0+27 31.57 0+00 34.93

EXIST M.H. #5

	Sewer Ext. Rosecrans N. of Rogers	80
50 Be A Sh.	" " La Jolla Shores Dr. ^{North of} Camino Del Oro	79
	Sewer Lat. Lowell St.	- 62
	(cable to Bacon - so. of Niagara)	
	Alley BIK 62 Ocean Beach	63+64
	(Pave, etc.)	
	Evergreen Lowell to Keats	65-68
	" Fenelon to Carlton	
	stake water meters	70
	stake water meters	
	Upshur - Rosecrans to Scott	69
	Auburn & Ontario - Culvert	71 ^{stake}
	Alley BIK 8 + BIK 22 La Jolla Park	72 ^{stake.}
	stake Tyrion St.	73
	" Alley BIK 2 La Jolla Park	74-75
	" " BIK 3 " " "	76-77
	Sewer La Jolla Shores	79-
	Drive N. of Camino Del Rio	
14 33	Rosecrans Sewer extension	80
	N. of Rogers	

1.58
7.84
9.42

476
460
936

5.78
15.33
21.11

748
8.4
66.4

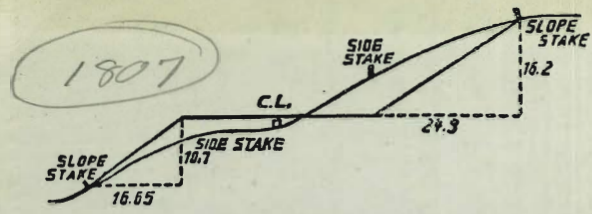
285
3
8.55
59.65
68.20

16.27
490
21.17

285
2
57.0

285
2 1/2
1.42
57.0
71.2

285
5.70



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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