

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

INDEXED

to page # 15

MICROFILMED

APR 13 1965

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.036	.041	.045	.050	.054	.059
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.887	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Index

- 43rd at National, curb grades 1
- 54th N. of University, culvert extension 2
- Opal St., Mission Blvd. to Bayard water meter grades 3
- Montezuma Road, College to 63rd, curb grades 5
- University Hts. Alley Bkls. 126 + 147 Also Polk E. of Landis, grade storm drains 12
- Highland Garden Alley bet. Dayton + Gilbert, paving grades 15
- Paving grades - La Jolla Hermosa 33
- " " Imperial - from Merlin 38
- " " N. end Brant St. 39
- " Afton Road nr. Airport 41
- Storm Drain, S. of Camino del Rio 47
- grades in 53d, S. of Redwood 48

Curb Grades East Side 43rd St
 H. National Ave

INDEXED

M.K.
 JAN 31 1950

Sept 23-49
 H.S. 5509
 Garber
 Coto
 No. 22022

1

BM	0.51	72.98	72.47	M.P. Keeler +43.50
TP	2.01	64.86	10.12	62.85
	0.10	N. National	57.41	7.45- 7.10- 69.35
	+20		57.44	7.42- 6.94- 69.78
	+40		57.51	7.35- 7.13- 69.22
	+60		57.72	7.14- 7.28- 69.14
	+80		57.97	6.89- 7.02- 69.73
	+90		58.13	6.73- 7.02- 69.49

National

Fdht

* 10 * 10 *

Horton Ave

Fdht

7

Grades Extension of Culvert 18"
 East of 54th St. North of University Ave.
 Lot 22 Loman Villa #784

Oct. 4-49
 H.S. Sison
 Garber
 Cota
 W.O. 20556
 Opening 3777B
 Plan 3776B
 Levels 1697-72

2

Stakes off Set 10' East of 1/2 Tranche

2+0	30996	5.74 3.78 c2.96	4+0	318.00	1.93 2.22 c2.27
+75	30896	7.74 4.11 c3.63	+25	316.99	5.97 5.69 c0.85
750	30795	8.75 6.37 c2.38	+50	315.99	6.94 5.13 c1.76
+25	30695	9.75 7.67 c2.38	3+14.17 EC 7'50"	314.55	8.98 6.98 c1.90
1+0	30594	10.76 8.25 c2.51	1 15'40"		
+75	30492	11.77 8.84 c2.93	3+00.49 5'52.30" R200'	314.00	8.93 6.76 c2.23
+50	30393	12.77 8.75 c4.02	T 27.52		
+25	30293	13.77 10.79 c2.98	+86.82 3°55' L54.69	313.45	9.18 6.68 c2.10
0+0.114 Exit ramp	30192	14.78 11.25 c3.53	c=11.98 for 10' F of 0.8.59.43		
BM 668 316.70	310.02	15.78 11.25 c4.53	+73.15 1°57.30"	312.90	10.03 7.53 c2.50
			+59.48 BC PI	312.35	10.58 7.10 c3.48
			TP 7.95 322.93 1.72	314.98	
			2+25	310.97	5.73 1.70 c4.01
				316.70	

INDEXED
 W.K.
 JAN 31 1950

Water Meter Grader
Opal St. Mission Blvd. to Boyard

70' Wide
12' Curb
Staked offset
3' N or S of Curb Face
Grade on Stake 3' west of Meter

Dec. 21-49
F. Simon
Rorer
Bunch
No 60 020
C6 Grade

3

6+49.5 North Side Curb Grade 3.20
93.93 Co. 99

5+94.5 92.73 ^{4.50}
~~6.50~~
Co. 92

5+50.5 91.77 ^{5.46}
~~4.31~~
Co. 15

INDEXED
W.K.
JAN 31 1950

5+01 90.69 ^{6.54}
~~5.43~~
Co. 77

4+44.5 89.46 ^{7.77}
~~7.18~~
Co. 57

TP 858 9722 130 88.65

3+84.5 88.15 ^{1.80}
~~1.30~~
Co. 80

3+33.5 87.04 ^{2.91}
~~2.00~~
Co. 91

2+91 86.12 ^{3.83}
~~2.82~~
Co. 91
2' N of 8' W

TP 1232 89.95 014 77.63 ^{S.W. 1/4}
~~S.W. 1/4~~
Mission
Opal

+10 = Brk

0+0 = EL Mission Blvd

B.M. 556 72.21 ^{H.W. RP}
~~60.1.21~~
Mission

TP 945 77.77 027 68.32

B.M. 784 68.59 60.75 ^{H.W. RP}
~~Boyd~~ Mission

South Side

6+46 93.36 ^{3.87}
~~2.54~~

6+40 93.23 ^{4.00}
~~3.87~~
Co. 91

6+07 92.47 ^{4.78}
~~3.70~~
Co. 06

5+21 90.53 ^{6.70}
~~5.25~~
Co. 75

4+82 89.65 ^{7.58}
~~6.50~~
Co. 79

3+26.5 86.27 ^{3.58}
~~2.50~~
Co. 04

2+84.5 85.20 ^{4.75}
~~4.00~~
Co. 75

2+34 84.06 ^{5.80}
~~4.81~~
Co. 28

1+25 81.82 ^{8.13}
~~5.87~~
Co. 26
2' North of
S. Side of
Curb

8993.7

Water Meter Grader
Opal St. Bayard East

North Side Curb Grade

South Side
Curb Grade

BM 1.40 100.94 ^{SE 74+1} opalt
cast 100.92

2+16

98.25 ^{7.09}
^{5.22}
^{0.97}
2.11

1+75.6 97.04 ^{8.36}
^{7.86} 0.57

1+26

96.62 ^{8.72}
^{8.01}
^{0.91}
2.14

+61.5 96.00 ^{9.92}
^{7.27} 0.67

TP 8.78 105.34 0.67 96.56 ^{0.5746}
^{0.714} 0.7343

0+70

95.60 ^{9.74}
^{8.25}
^{0.147}
2.1465

+34.3 95.48 ^{1.75}
^{0.24} 0.1.68

105.34

+15 - Brk

+15 - Brk

0+0 - FL Bayard

0+0 - FL Bayard

97.23

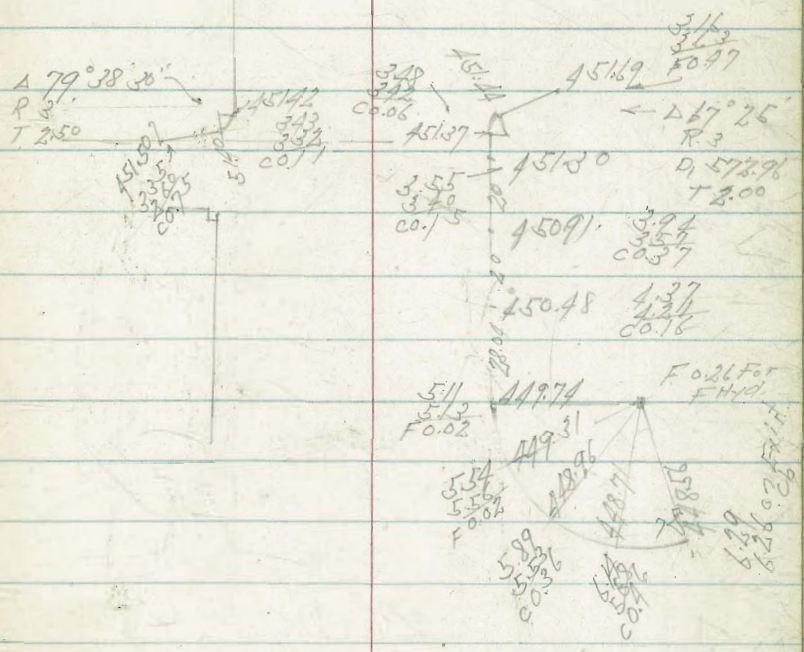
Montezuma Road Curb Grader
College Ave to 63rd St

Jan 13 1950
F. Sisson
D. Smith
Rorer
Chavez
M.O. 22 007

5

Notes For Line
Used L.R.T. 1808-44

INDEXED
W.K.
JAN 31 1950



B.M. 502 454.85 449.83
NE SP
College Ave
+ 7/10/1950
134-64

College Ave

Montezuma Road

Hort's Curb
Grad.

+60
3.96
3.90
0.06 457.07

+40
3.87
3.76
0.11 457.16

+20
3.84
3.87
0.03 457.19

+0
3.89
3.96
0.07 457.14

+80
4.00
3.96
0.04 457.09

+60
4.18
4.20
0.02 457.85

0+40
4.42
4.17
0.25 457.61
0.23

TP 4.17 456.03 2.99 457.86
454.85

17

TP 345 451.30 8.18 447.85

540 P.V.C. $\begin{array}{r} 837 \\ 818 \\ \hline 19 \end{array}$ 447.66

+50 $\begin{array}{r} 769 \\ 749 \\ \hline 20 \end{array}$ 448.34

140 $\begin{array}{r} 703 \\ 673 \\ \hline 30 \end{array}$ 449.01

+50 $\begin{array}{r} 634 \\ 617 \\ \hline 17 \end{array}$ 449.69

240 $\begin{array}{r} 537 \\ 516 \\ \hline 21 \end{array}$ 450.36

475 $\begin{array}{r} 533 \\ 523 \\ \hline 10 \end{array}$ 450.70

+16.53 $\begin{array}{r} 495 \\ 471 \\ \hline 24 \end{array}$ 451.08

240 - F.V.C. $\begin{array}{r} 435 \\ 426 \\ \hline 09 \end{array}$ 451.68

1480 $\begin{array}{r} 412 \\ 407 \\ \hline 05 \end{array}$ 451.91

456.03

Montezuma Road

+60
 $\begin{array}{r} 4.07 \\ 3.96 \\ \hline 8.03 \end{array}$ 447.23

8+20
 $\begin{array}{r} 4.45 \\ 4.36 \\ \hline 8.81 \end{array}$ 446.85

+80
 $\begin{array}{r} 4.63 \\ 4.49 \\ \hline 9.12 \end{array}$ 446.57

+40
 $\begin{array}{r} 4.90 \\ 4.87 \\ \hline 9.77 \end{array}$ 446.40

7+0
 $\begin{array}{r} 4.96 \\ 4.85 \\ \hline 9.81 \end{array}$ 446.34
 of Comp
 64.58
 17.167

+60
 $\begin{array}{r} 4.91 \\ 4.62 \\ \hline 9.53 \end{array}$ 446.39

6+20
 $\begin{array}{r} 4.76 \\ 4.18 \\ \hline 8.94 \end{array}$ 446.54

+80
 $\begin{array}{r} 4.20 \\ 4.26 \\ \hline 8.46 \end{array}$ 446.81

5+40
 $\begin{array}{r} 4.13 \\ 4.07 \\ \hline 8.20 \end{array}$ 447.17

451.30

1104
10.63
11 + 24.53 3° 23.81' 0.071450.68

1138
10.92
+ 99.37 2° 52.98' 0.076150.34

11.72
11.25
+ 74.21 2° 24.15' 0.078449.99

13.08
12.84
+ 49.06 1° 55.32' 0.024449.64

13.42
12.16
10 + 23.90 1° 26.49' 0.026449.30

12.77
12.52
+ 98.74 0° 57.66' 0.018418.95

stake line C 25.76

13.12
12.85
9 + 73.58 0° 28.83' 0.017448.60

10.25.16 out
BM 793 461.72 153.79
+ 48.42
+ 27.777 B.G.R. 3.04
2.85
0.25 448.26

5.56
3.52
9 + 0 0.007447.74

451.30

451.30

2.87

448.43

456.36

2.83

453.53

072.91pc
50.818
8c
072.91pc
B.C. 072.91pc

Montezuma Road

+80

$\frac{810}{813}$
Fo.03 453.62

+50

$\frac{834}{816}$
Co.78 453.38

72+20

$\frac{861}{843}$
Co.78 453.11

+90

$\frac{896}{878}$
Co.78 452.81

+67.82 = FC

$\frac{915}{900}$
Co.75 452.57

C 29.96

8° 43.32'

+30

$\frac{961}{981}$
Fo.20 452.11

C 21.72

0° 34.38'

12+00

$\frac{1000}{1007}$
Fo.07 451.72

+74.85

$\frac{1035}{1035}$
Co.05 451.37

11+49.69

$\frac{1069}{1039}$
Co.35 451.03

461.72

B.M.

554

456.18

07. RP 404
155. 27 1/2
154.09.46
456.19
9247+38.43 FC 55° 0' 15" ⁷⁴³
5.57 454.29
01.86+25.61 36° 41' 14" ⁷⁴⁴
5.22 454.28
01.970+1381 18° 20' 35" ⁷⁴⁵
7.33 454.27
00.130+0
+11.53 = C6 BC 1/4 ⁷⁴⁶
7.29 454.26
F0.031540 ⁷⁴⁹
7.36 454.23
F0.21+70 ⁷⁶⁰
7.78 454.12
F0.18+40 ⁷⁷³
7.82 453.99
F0.0914+10 ⁷⁹¹
7.93 453.81
F0.06

461.72

Grades Storm Drains N45W110W
 Block 126 University Hts & Block 147
 1750 Polk Ave. East of Louisiana St.

M.O. 20593

Jan 19-50
 F. S. Simon,
 D. Smith,
 Rorer,
 Chavez. **12**

12+30.36 EC		297.98	16.86 4.54 1.57 1.55	+75	200.00	15.95 3.71 1.22
+49.44	INDEXED N.K. JAN 31 1950	297.74	17.10 5.90 1.62	11+0	299.67	16.28 3.80 1.26 1.50 1.50 1.50
+68.53		297.49	17.35 7.13 1.02	+25	299.35	16.60 5.99 1.26
12+87.67		297.24	17.60 8.84 9.36	+50	299.02	16.93 5.90 1.26 5
13+06.70		296.99	17.85 9.52 1.23	+75	298.70	17.25 5.69 1.26 5.20
+25.79		296.74	18.10 10.87 9.23	TP	2157 215.95 2.46 312.38	Nail Polk E side Hill 50.00
+44.88		296.50	18.31 12.07 6.62	11+95.80 B.C. P22	298.11	16.40 5.85 1.26 5.1
13+63.97		296.25	18.59 13.19 5.70	12+07.32	298.28	16.56 5.85 1.26
13+87.87 = 1/2 First Clean out		296.00	18.84 13.15 5.70	12+18.84	298.13	16.76 5.98 1.26
+83.06 P40		314.84	13.09			
B.M.	1.18	326.13	324.95			

31484

+50	302.93	13.02 1.77 c 8.55 5
+75	302.60	13.35 3.91 c 9.47 5
9+0	302.28	13.67 3.15 c 10.52 5.51 No 1 Fence
+25	301.95	14.09 3.86 c 10.61 5.63 No 1 Fence
+50	301.62	14.33 4.86 c 9.47 5
+75	301.30	14.65 4.87 c 9.84
10+0	300.97	14.98 4.88 c 10.68
+25	300.65	15.30 5.19 c 10.19
10+50	300.32	15.63 4.91 c 10.73 5 East

315.95

6+0		
+25		
+50		
+75		
TP	7.53	321.71
7+0		17.7
+25		
+50		
+75		
8+0		
8+25		

315.95

306.18	15.53 2.37 c 11.19 5.45 No 1 Fence
305.85	15.86 2.63 c 11.23 5.86
305.53	16.18 2.95 c 11.25 4.70 No 1 Fence
305.20	16.51 3.25 c 10.76 4.63 No 1 Fence
304.88	14.07 3.31 c 9.76 4.81 No 1 Fence
304.55	11.40 2.15 c 9.25 4.63 No 1 Fence
304.23	11.72 2.63 c 9.27 2.5
303.90	12.05 2.98 c 9.27
303.58	12.37 2.06 c 8.31
303.25	12.70 2.47 c 8.5 5 East

+75

311.90 ^{9.86}
^{4.18}
c 5.6
5.2 x oncb

+40

311.12 ^{10.59}
^{4.81}
c 6.08
5.2 x oncb

+25

310.34 ^{11.37}
^{4.85}
c 6.32
5.2 x oncb

+50

309.58 ^{12.15}
^{5.03}
c 7.12
5.2 x oncb

+75

308.78 ^{12.93}
^{5.30}
c 7.63
5.2 x oncb

540

308.00 ^{13.76}
^{5.68}
c 8.03
5.2 x oncb

+285 - Clear out

307.11 ^{14.59}
^{6.29}
c 8.29
+07 Cub

B.M. Pac 318.04

378 317.93 ^{5.28 P}
^{4.70}
Howard
47 tax or +23.48

+53.50 Howard St

306.78 ^{14.92}
^{5.46}
c 9.47
5 nail Pav. 2+50

5+78.50 - Clear out

306.46 ^{15.25}
^{5.25}
c 10.00
7 x oncb

321.71

321.71

313.50 ^{8.31}
^{3.20}
c 5.51
10.14
312.68 ^{9.03}
^{3.97}
c 5.17
5.2 x oncb

Garber 7/10/50
 Chavez W.O. 62183
 Rorer See BK. 1807 P-58 Paving Grades

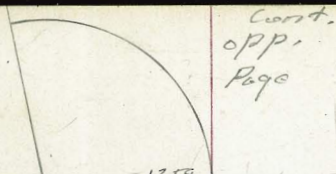
Alley in Highland Gardens btw. Dayton & Gilbert adj.
 to Lot 31

Lt.

Rt.

INDEXED
 MKK
 JUL 14 1950

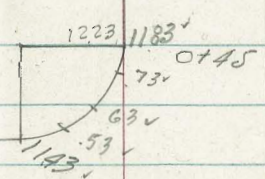
	Lt.	Rt.		
+ 20.41	421.16 Hub 4.87 2.0 BK 3.80 C-1.07	421.26 Hub 2.0 BK 4.77 4.77 0.00		
+ 00.41	421.83 4.20 Hub 3.17 2.0 BK C-1.03	421.78 4.25 x on Conc 3.03 2.0 BK C-1.22		
+ 80.41	422.16 3.87 3.41 Hub C-0.46 2.0 BK	422.03 4.00 x on Bldg 3.00 2.15 BK C-1.00		
+ 77.63 Sewer Lateral	426.03 Hub 4.13.00 11.03 5.0 BK 3.32 C-7.71			
+ 60.41	422.15 Hub 3.88 2.0 BK 3.48 C-0.40	422.00 x on Bldg 4.03 1.5 BK 3.03 C-1.06		
+ 40.41	421.80 Hub 4.23 2.0 BK 3.40 C-0.83	421.70 x on Bldg 4.33 1.2 BK 3.33 C-1.00	+ 52.63	418.55 Existing 7.48 pave 7.49
0+00	420.80 5.23 Existing 5.43 Existing pave.	420.80 5.23 Existing 5.38 pave		
	6.72 426.03 H.I.	NEBP 419.31 El Cajon & Dayton	+ 40.41	420.15 Hub 5.88 2.0 BK 4.60 C-1.28
				419.81 6.22 Hub 5.46 C-0.76 2.0 BK



Const.
opp.
Page

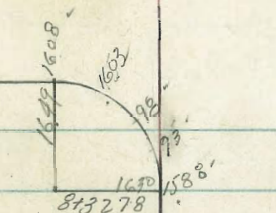
2198.22	1359	1319
2175		1307
2150		1294
2125		1280
2100	1306	1267

1175		1253
1150	1240	
1145	1237	
1125	1226	
1105		1215
1100		
0180		1202
0175		
0165		1194

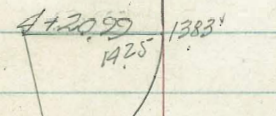


Tanapah

Littlefield
p-18



Knoxville st.	7175	1588.62
Paving Gutter Elev.	7150	1545.51
	7132	1543
	7125	1533.59
Brk	7100	1515.28
	6175	1508.13
	6150	1498.99
	6125	1483.84
Brk	6100	1470
	5175	1458
	5150	1445
	5125	1433
	5100	1420
	4197	1418
	4175	1408
	4150	1396



Nashville p-19

Knoxville

1+60.5
K 1730 1688

1+50 1683

1+25 1671

1+00 1658

0+75 1645

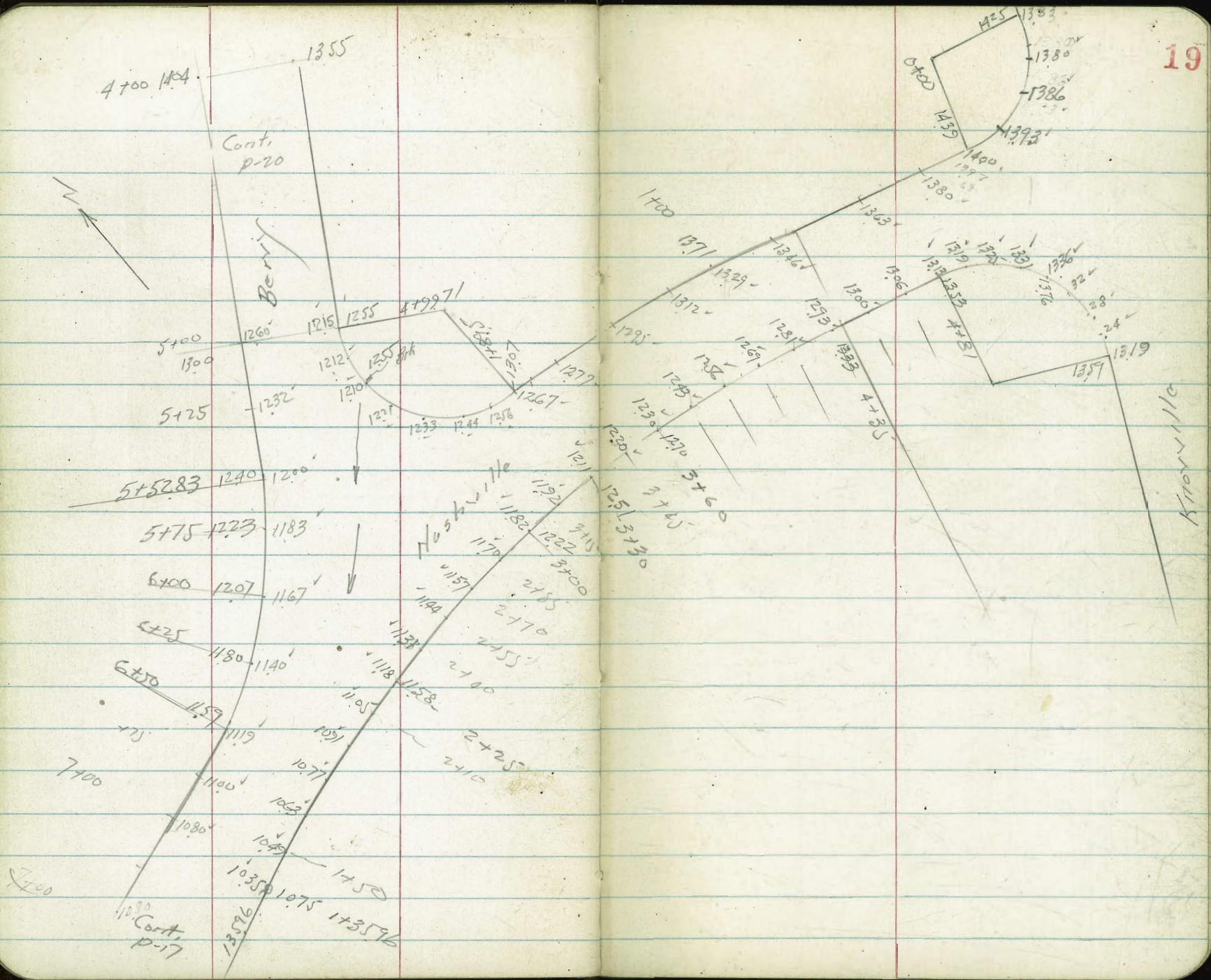
0+50 1633

0+25 1620

0+00 1608

Knoxville
P-16

Littelfield



2+00 1611 1571 1525-1565

1581 1546 1497 1537

1559 1519 1471 1511

1536 1496 1448 1483

TP
3+00 1508 1468 1417 1457

1442 1391

1416 1366

1390 1340

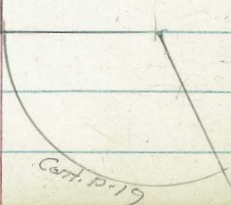
4+00 1404 1364 1315 1355

1338 1290

4+50 1312 1265

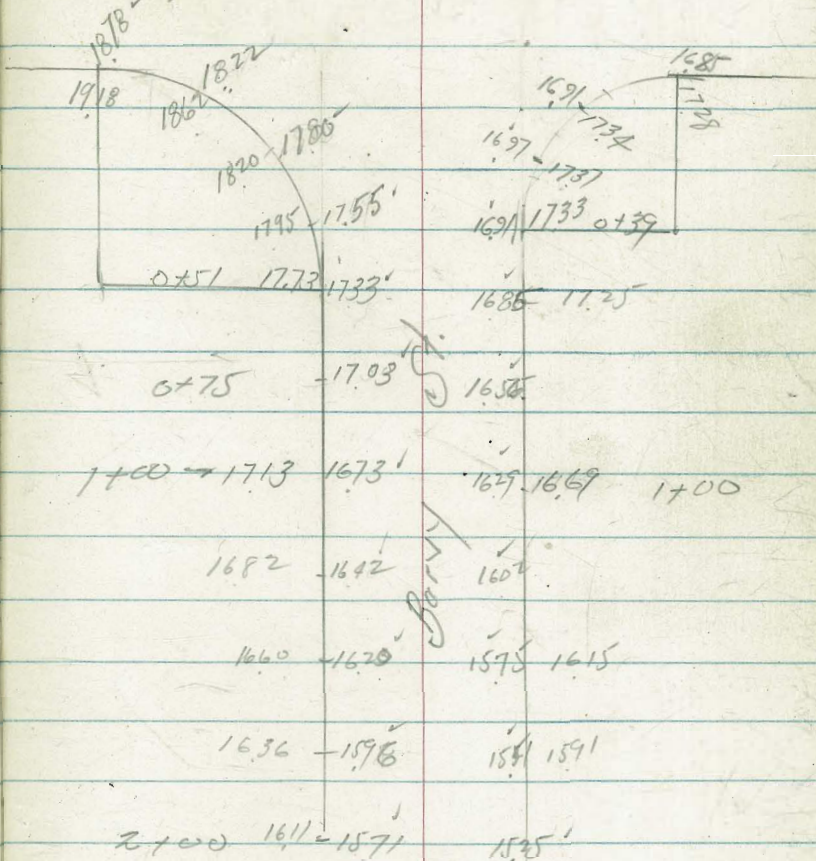
1286 1240

5+00 1260 1215



Littlefield

St.



Cont. p. 19

30" Storm Drain - Grades
 on Lots 23, 24 - Block 260
 Warr. Hts.

South of Myrtle
 Between Florida & Alabama
 Plan 4068-B No 20699
 Prelim Survey = FB 2015-40

	Plan. Stakes	Elev. Invert.	Cuts
2+32.60 = End of Construction	217.02	212.54	4.48
2+04.60	217.54	210.02	7.52
1+76.60 = Beg. 30" C. Invert	216.28	207.50	8.78

on Hub
 BM 2103.7
 FB 2015-52

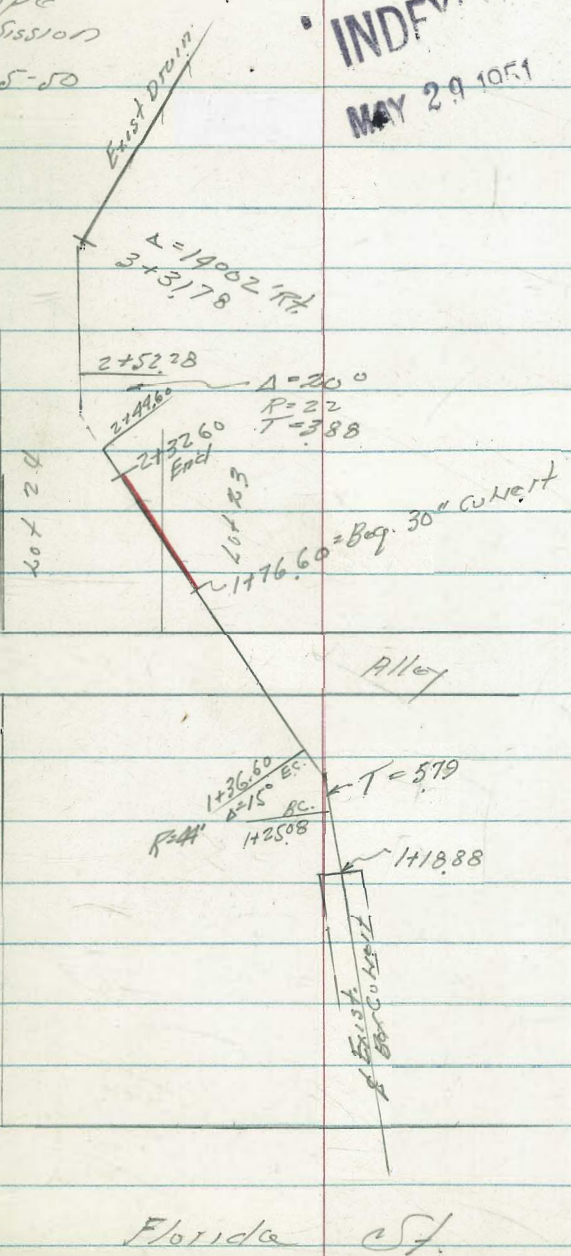
211.30

(Stake set 10' RT of H)

Walker
 Pope
 R. Sisson
 10-5-50

INDEFFEN
 MAY 29 1951

50' / 252
 22



Myrtle Ave

Alley

Florida St

Curb Grades - BAYARD ST.
from Low St. to Loring

INDEXED

MAY 29 1951

23

Stations	West Curb	W Gutter	W 1/4	East Curb	2	E 1/4	East Gutter	East Curb
1+4802	62.63			62.57	62.80	62.76		63.07
1+45	62.71 62.60 F 0.14 F 0.36	62.23		62.87 63.09 62.87 F 0.12 F 0.17	34	34		62.87
1+2502	62.23 62.44 62.21	62.12-34 61.92 F 0.70		62.23	62.46	62.42 = Sub.		F 0.20
				62.256 62.44 F 0.12 F 0.02				
1+2202	62.02 61.42 F 0.60			61.96 34 61.62	62.20 34 61.86	62.15 34 61.81		62.46 62.44 F 0.02
0+90	61.76 61.11 F 0.15			61.21 34 60.87	61.45 61.11	61.40 61.06		61.71 61.45 F 0.26
0+55	60.44 60.31 F 0.13			60.38 60.4	60.63 34 60.29	60.59 34 60.25		60.90 60.94 60.04
0+20	59.61 59.50 60.11			59.56 34 59.22	59.80 59.46	59.78 34 59.44 = Sub.		60.08 60.36 60.28
N.W. Low St. 0+00	59.14 59.30 60.16							59.61 59.70 60.09

5889 S.W. NW 3/4 Bayard + Low

Stations	West Curb	West Gut	H 1/4	L ₀	F 1/4	E Gutter	East Curb
2+70.04 = SIX Beryl	65.51 = 16 65.49 65.49 0.00						65.92 = 16 65.90 65.97 0.07
2+50	65.03 64.78 F 0.25	64.96 34 64.62		65.18 34 64.84	65.15 34 64.81		65.43 65.51 0.08
2+15	64.21 64.09 F 0.12	64.14 63.80 = sub		64.36 64.07 = sub	64.33 64.00		64.63 64.40 F 0.23
1+80	63.39 63.19 F 0.20	63.32 62.98		63.55 63.21	63.51 63.17 = sub		63.81 63.67 F 0.14

Stations	West Curb	West Gutter	W 1/4	1/4	East 1/4	East Gutter	East Curb
1+48.00	70.88						
1+45 70.95 70.84 71.33 70.83 C 1.38 F 0.01 P 0.0	70.83 F 0.05						
1+25 70.46 70.34 71.02 70.38 C 0.62 C 0.26							
			East curb pc. Prop 71.74 71.85 71.43 72.70 F 0.31 C 0.94 71.22 71.34 70.85 71.68 F 0.37 C 0.34	1/4 71.05 71.33 3/4 70.71 70.99	71.36 71.02		71.79 71.43 F 0.36
1+22.00	70.23 70.38 C 0.15		70.39	70.67 3/4 70.33	70.70 3/4 70.36		71.13 70.85 F 0.28
0+90	69.43 69.14 F 0.29		69.58 3/4 69.24	69.86 3/4 69.52	69.89 3/4 69.55		70.31 70.04 F 0.27
0+55	68.55 68.24 F 0.31		68.69 3/4 68.35	68.97 3/4 68.63 = sub	69.00 3/4 68.66		69.42 69.20 F 0.22
0+20	67.67 67.70 C 0.03		67.79 3/4 67.45 = sub	68.07 3/4 67.73	68.10 3/4 67.76		68.52 68.48 F 0.04
NW Beryl 0+00	67.17 67.19 67.22 C 0.05						68.03 68.01 68.02 C 0.01

Stations	West Curb	West Gutter	West '10	$\frac{d}{L}$	East '10	East Gutter	
527 Wilbur = 2+70	73.93 ^{ch} 73.98 C 0.05						East. 74.92 74.90 74.64 F 0.26
2+50	73.43 ^{ch} 73.17 F 0.26	73.61 ³⁴ 73.27	73.92 ³⁴ 73.58 ^v		73.95 ³⁴ 73.61 = Sub.	74.39 ^{ch} 74.08 F 0.31	
2+15	72.55 ^{ch} 72.78 C 0.23	72.74 ³⁴ 72.40 ^{Sub}	73.05 ³⁴ 72.69 = Sub.		73.06 ³⁴ 72.72 ^v	73.50 ^{ch} 72.96 F 0.54	
1+80	71.68 ^{ch} 71.75 C 0.07	71.86 ^{ch} 71.52 ^v	72.14 ^{ch} 71.80 = Sub.		72.17 ^{ch} 71.83 ^v	72.61 ^{ch} 72.20 F 0.41	

Station	West Curb	West Gutter	West 1/4	d/4	East 1/4	East Gutter	East Curb
1+48.05	80.15 79.59 F0.16		80.24 3X 79.90	80.46 80.12	80.45 80.11		80.80 80.88 C0.08
1+45	80.21 80.39 C0.18	80.05 79.79 F0.10	80.15				80.74 80.88 C0.14
1+25	79.53 80.08 C0.55	79.41 79.55 C0.12					80.70 79.88 F0.22
1+22.05	79.26 79.55 C0.29		79.36 79.12	79.59 79.25	79.60 79.26=Sub.		79.26 79.88 F0.08
0+90	78.16 77.95 F0.21		78.27 3X 77.93	78.52 78.18	78.55 78.21=Sub.		78.23 78.89 F0.04
0+55	76.26 76.86 F0.10		77.08 76.74	77.35 77.01=Sub.	77.40 3X 77.06=Sub.		77.80 77.73 F0.07
0+20	75.77 75.96 C0.19		75.90 33 75.57	76.18 34 75.84	76.23 34 75.99=Sub.		76.67 76.52 F0.15
0+00	75.88 75.09 75.24 C0.15						75.88 76.02 76.71 C0.09

Stations	West Curb	West Gutter	West 14	$\frac{L}{2}$	East 14	East Gutter	East Curb
567 boring -2+70.10	8494 84.34 ^v 84.36 F 0.02						84.74-Exit 84.75 ^v 84.65 F 0.10
2+50	83.65 ^v 83.34 F 0.31		83.68 83.34-Sub	83.87 34 ^v 83.53-Sub	83.80 83.46-Sub		84.10 83.68 F 0.42
2+15	82.45 ^v 82.25 F 0.20		82.50 82.16 ^v	82.70 82.36 ^v	82.65 82.31 ^v		82.97 82.70 F 0.27
1+80	81.25 ^v 81.06 F 0.25		81.32 80.98-Sub	81.53 81.19-Sub	81.50 81.16-Sub		81.84 81.72 F 0.12

Mar Ave
Grades - ~~Prop~~ ^{curb} line
Portion Lot 14

Beverly Hts Profile #4162
NO 62205

INDEXED
MAY 29 1951

	Elev. Top cb	Elev. Stakes	Cuts	offsets from cb.
1+00 Bk	280.93	282.63	C 1.70	7' Lt.
0+80 Bk	282.45	283.86	C 1.41	"
0+65 ^{Bk} = Sub. line Beverly Hts.	283.40	283.82	C 0.42	"
0+60 Bk	283.72			
0+40 Bk	284.55			
0+20 Bk	284.96			
0+00 = E.C. 20' Prop R	285.15			
	278.97			

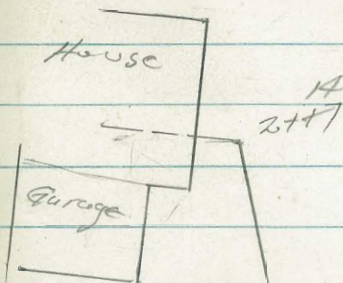
BX7 Flow line MH & Mar Ave
& Dellcrest
Lane
Plan 4118-B

Mar Ave
Proposed Sewer

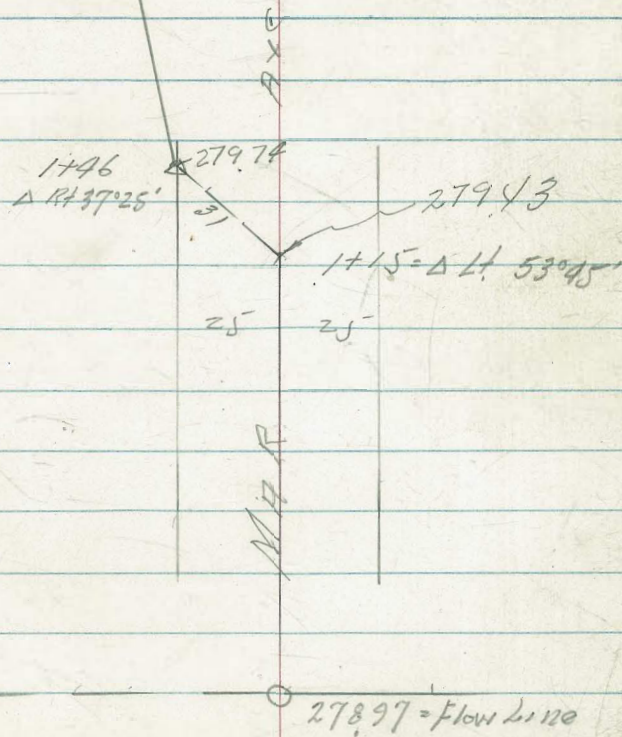
INDEXED

30

MAY 29 1951



Top Fdn. House	2819
¹⁴ 2+17 - 4" Soil Flow	27967
1+82	2818
1+46 = Δ	2831
1+15 = Δ Lt	2899
1+85	2845
1+00	2836
+25	2848
0+05	2840
0+00 - 2 NH	27897



Grades Sewer Mar Ave

Location - P-30

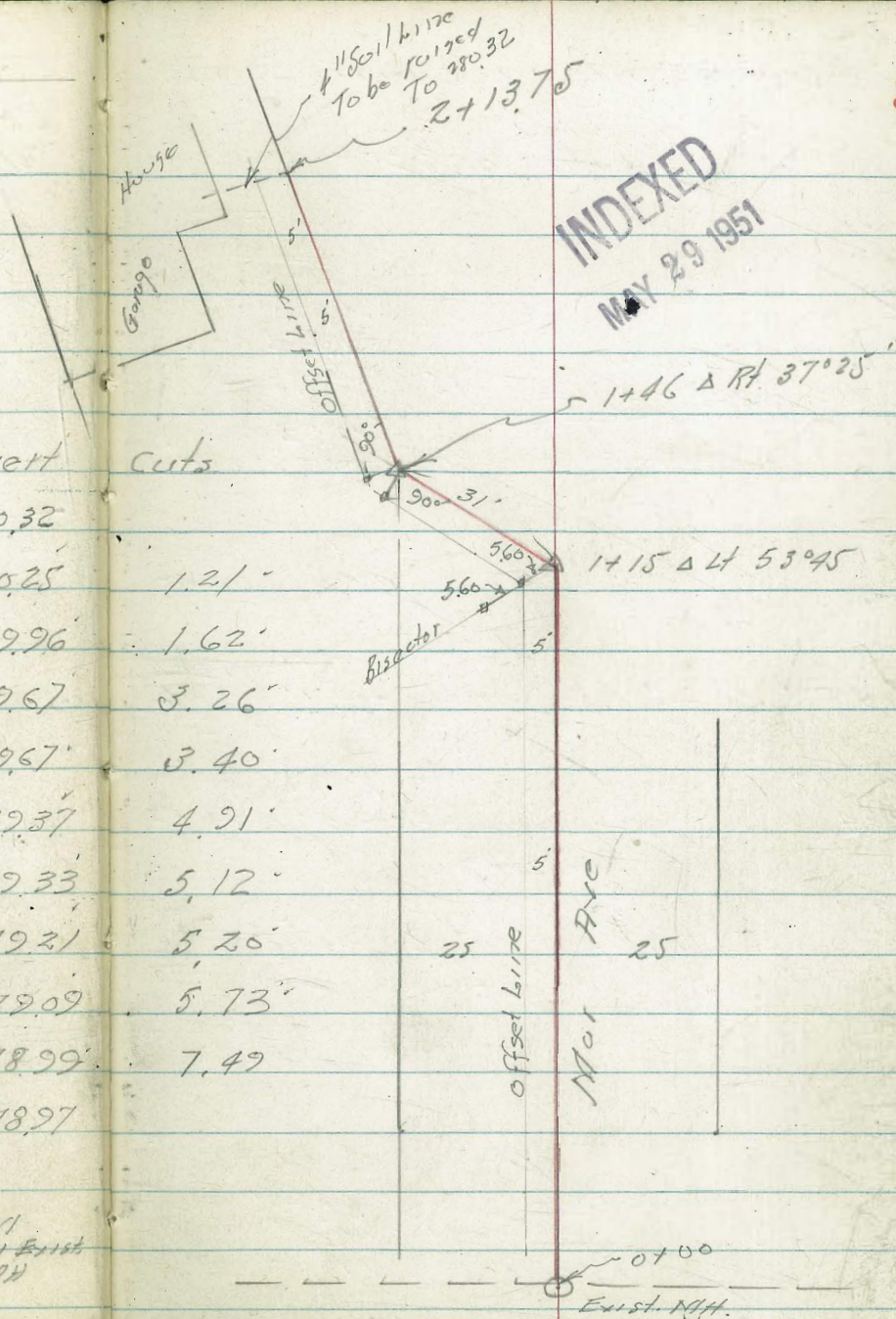
Walker
Popc
R-Session
11-16-50

HO 62205

Stations

Stations	Elev. stakes	El. Invert	Cuts
2+13.75 = Exist. Soil line		280.32	
2+06	281.46	280.25	1.21'
1+76	281.58	279.96	1.62'
1+46 Δ	282.93	279.67	3.26'
1+46	283.07	279.67	3.40'
1+15 Δ Bek.	284.28	279.37	4.91'
1+05	284.45	279.33	5.12'
0+70	284.41	279.21	5.20'
0+35	284.82	279.09	5.73'
0+05	286.48	278.99	7.49'
0+00 = Exist. MH		278.97	

278.97 BM
From Exist
MH



Grades - Storm Drain Extension

on Annulfi St.
 "B" Sheet No 4033-B

Walker
 Huffman
 Kellie
 10-8-51

1410

chk B.M. NW 1/4 Cor
 Chisled square Pumping Plant 495
 on Grating Inlet Annulfi St.
 T.P. 846 10549 1233
 98.49

93.54
 100.34
 90.03 Grating
 97.03

Please with
 check with
 Frank Osborne
 for file.

0+48 = End of Ext.

Void

Void

	Elev. Stakes	Elev. Invert.	Cuts	offset
0+48	10211 107.11	9167 98.67	10.44	7'4"
0+24	9592 92.92	9058 97.58	5.34	7'4"
0+00 = Exist Invert	1286	89.50 96.50		

see Grade Book
 243-79

End
 Exist 24" Corc.
 Pipe

138.48
 104.48

Inlet &
 = Grating

Annulfi

St.

T.P. 809 10236 041
 17.68 94.68 101.68
 77.00 84.00

B.M.
 Invert

PAVING GRADES LA JOLLA HERMOSA AVE.

Walker
 from Camino De La Costa
 Pope To La Canada No 32041
 Huffman
 11-14-51 Plan 7938-L

Inward

Roadway

7963	7913	7994	8043	8037	8103	21083
			8043			
7951	7901	7979	8005	8021	8026	1180 P.M.
			8005		8026	
7889	7965	7984	8005	8008	8013	1160
			8005	8008	8013	
7877	7951	7970	7989	7991		1140 P.M.
			7989	7991		
7862	7934	7953	7970	7969		1115
			7970	7969		
7847	7918	7926	7951	7947		0+90
			7951	7947		
7832	7900	7919	7931	7925		0+65
			7931	7925		
7867	7817	7886	7902	7911	7903	7978
			7902	7911	7903	7978
7808	7865	7883	7894	7894		0+20
			7894	7894		
7798	7800					
7848						
7860						
7811						0+00
7875						0+4.3

Note: Grades shown are finish Conc.

F.B. 1847
 B.M. West Topcb 0+00 P 2 7845
 Above B.M. used to fit Elev. as run
 in F.B. 1827
 Does not chk Plan B.M. by Point
 003 or 004

CAMINO DE LA COSTA

La Jolla Hermosa Ave. Parc

Note: Lowered Grades on West

4762	8198	8255	8288	8294	8296	4765
8253	8179		8279		8292	34
8170						
4748.8	8160		8262	8269	8273	4740
8235	8170		8267		8267	
8150						
4735 Drive	8133					
8151 Drive						
Prop. Line	8122		8228	8244	8250	4715
	8142	8202	8235		8242	
	8054		8204	8221	8228	3790
	8177		8209		8217	
Sub. Edge Drive						
8076						
3+70 Drive	8067	8066	8178	8197	8205	3765
		8151	8182		8192	
3+62		8063				
	8042		8155	8173	8182	3740
	8078	8127	8156		8167	
	8018		8131	8149	8159	3715
	8070	8103	8107		8142	
	7994		8105	8123	8132	3790
	8002	8077	8109		8147	
LP	7970		8080	8097	8105	3765
70	7994	8059	8076		8092	
	7997	7947	8021	8049	8071	3740
			54		8078	
			8049		8083 Drive	
					8067	
					8142	3720
						E.V.C.
	7978	7928	8009	8054	8061	3720
					8046	
					8121	

Lafolla Harmonica Ave
 Parking

8424	8429	8436	8503	8511	8499	8491-Drive	7+15
8467	8472	8478	8496	8504	8498	8558	35
8414	8422	8478	8496	8504	8498	8558	6+95
8400	8413	8465	8485	8494	8486	8555	6+75
8457	8413	8465	8485	8494	8486	8555	6+75
8385	8399	8452	8472	8482	8475	8547	6+55
8446	8399	8452	8472	8482	8475	8547	6+55
8368	8382	8435	8464	8456	8460	8535	6+35
8433	8382	8435	8464	8456	8460	8535	6+35
8348	8366	8416	8476	8448	8442	8517	6+15
8416	8366	8416	8476	8448	8442	8517	6+15
8327	8345	8396	8426	8428	8422		5+95
8375	8345	8396	8426	8428	8422		5+95
8293	8310	8364	8394	8397	8392		5+65
8273	8310	8364	8394	8397	8392		5+65
8264	8282	8335	8368	8369	8367		5+40
8264	8282	8335	8368	8369	8367		5+40
8236	8254	8309	8341	8344	8342	8342-Drive	6+15
8236	8254	8309	8341	8344	8342	8342-Drive	6+15
8207	8226	8282	8345	8319	8317		4+90
8207	8226	8282	8345	8319	8317		4+90

TR

8559 on 16

37
46

TR

on Finish ^{stake} on Rt.
4190

319

La Jolla Hermosa Ave - Parking

La Canada

36

	8456	8497	8446	8462	8471	8478	8544 my El.	8498	8542	9+263
14		7	7		7	7				
	8402	8473	8495	8506	8503	93H				9+05
14		7	7		7	7				
6	8408	8479	8502	8512	8510	93H				8+80
21				21		12				
	8414	8486	8508	8518	8516	93H				8+55
Drive 8401	8420	8491	8512	8524	8520	908H				8+35
8+25	8425	8494	8515	8526	8521	8559				8+15
8463	8430	8497	8517	8527	8519	8561				7+95
8464	8434	8492	8517	8526	8525	8561				7+75
Appt	8466	8435	8498	8515	8522	8510				7+55
8467	8431	8493	8510	8517	8505					7+35

Imperial Ave - Paving Grades
from Merlin Drive

Walker
Pope
Huffman
11-16-51

Plan 9135-L NO 9135-L

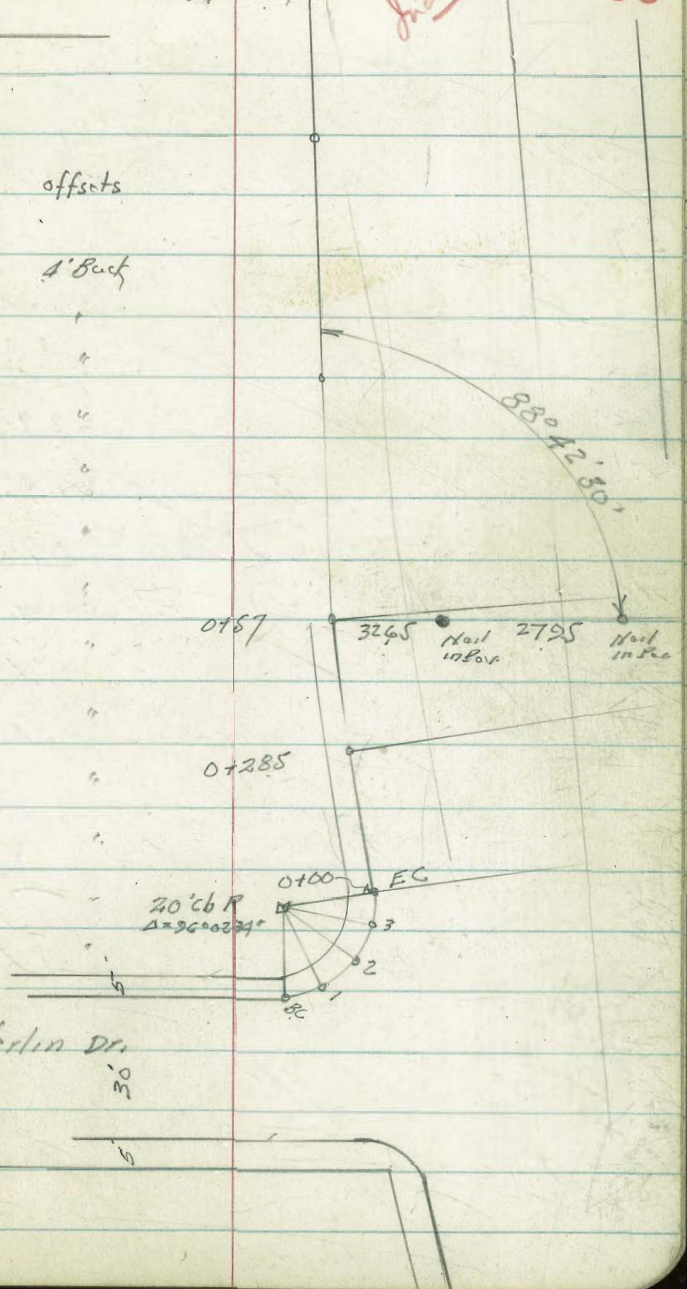
	Elev.	Elev.	Cuts & Fills	offsets
5+07.2 End	162.43	Gutter		
4+57.5 End	162.25	161.88	C 0.37	4' Back
4+07	160.85	161.49	F 0.69	
3+57	161.74	161.35	F 0.11	
3+07	163.27	161.26	C 2.01	
2+57	161.36	161.17	C 0.19	
2+07	162.35	161.08	C 1.27	
1+57	158.23	160.99	F 2.76	
1+07	163.34	160.90	C 2.44	
0+57	162.10	160.81	C 1.29	
0+28.5	162.48	160.78	C 1.70	
0+00	161.81	160.74	C 1.07	
#4 = E.G.	161.42	160.56	C 0.86	
#3	161.03	160.35	C 0.68	
#2	160.46	160.10	C 0.36	Merlin Dr.
#1	159.84	159.95		
BC				
B.M. B.P. Bridge Merlin	161.28			
H. of Imp				

Restaked
4-15-52 7.0
N ←

5107
= Exist. Pav

Indicated

38



GRADES on Drain North End

Brant St.

bet. Lewis & Washington

Walker

Pope

Hoffman

12-25

Plan 6214-L

NO 31594

26938

Indexed 39

	VA	Tan	Diff	Elev. Stake	Elev. Invert	Cuts	offsets
0 + 67 = End	-30°43'	594	-39.80	248.38	227.20	1.18	5' Rt.
0 + 57 Bk	-31°53'	622	-35.45	232.73	230.00	2.73	"
0 + 47 Bk	-33°08'	653	-30.69	237.49	234.00	3.49	"
0 + 32 Bk	-34°45'	694	-22.21	245.97	242.00	3.97	"
0 + 17 Bk	-39°45'	572	-9.72	258.46	252.00	6.46	"
1" N. cb face				267.71	263.63	4.08	13' Lt.

check levels by Trig.
final by level
on P. 40

Levels by Trig. Reading from L Nail 26818

F. cb 268.98 268.98 267.33 1.65 5' Back cb face

M. cb 267.71 267.71 266.83 0.88 5' Back cb "

T.R. 268.36

260.09

Direct Rod

B.M. SE 7' Tick Washington & Brant.

FB 179
64

Grades Drain North end

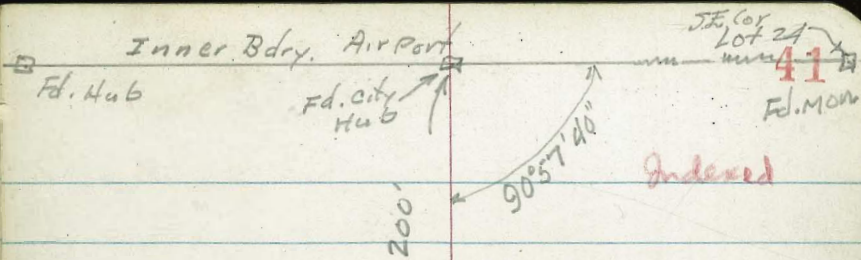
Bunt St.

Cont. from p. 39

12-2-51

0+67		1832	228.41	227.20	1.21	
0+57		1995	232.78	230.00	2.78	
0+47		919	237.54	234.00	3.54	
T.P.						
0+32	0.68	246.73	1296	246.05	4.05	
T.P.						
0+17	0.08	258.51	10.68	258.43	6.43	
0+100			0.95	268.16	267.63	4.53
1.40		269.11		267.71		

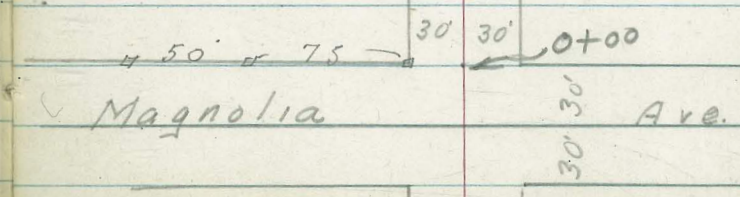
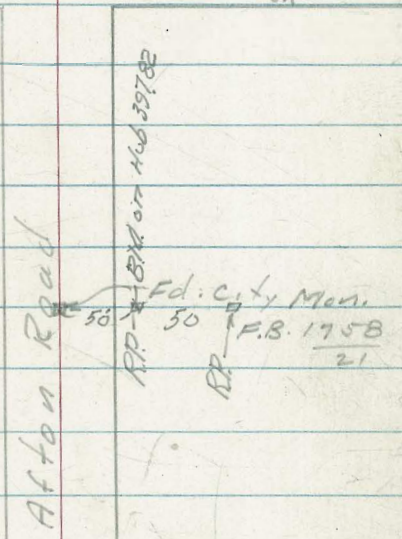
Grades Alton Road



Indexed



1146572



2-27-52

Pope
Huffman
Bishop

W.D. #

"Atton Road"
Gutter Grades

42

Lt.

Rt.

3400

394.70
395.81
C-1.11

394.70
397.27
C-2.57

2450

394.95
395.70
C-0.65

394.95
396.80
C-1.85

2400

395.20
395.52
C-0.32

395.20
396.60
C-1.40

1450

395.00
395.37
C-0.37

395.00
396.70
C-1.70

1400

394.80
395.65
C-0.85

394.80
396.10
C-1.30

0450

394.60
395.33
C-0.73

394.60
395.72
C-1.12

0400

N. Live Magnolia

394.40
394.95
C-0.55

394.40
394.95
C-0.55

B.M. Hub NE. Cor. Proposed School site Elev 393.92

Direct Elev. Rod Used

Lt.

Rt.

6+50

392.95
395.49
C-2.54

392.95
395.83
C-2.88

6+00

393.20
394.91
C-1.71

393.20
395.84
C-2.64

5+50

393.45
394.84
C-1.39

393.45
395.88
C-2.43

5+00

393.70
395.18
C-1.48

393.70
396.00
C-2.30

4+50

393.95
395.38
C-1.43

393.95
396.16
C-2.21

4+00

394.20
395.73
C-1.53

394.20
396.17
C-1.97

3+50

394.45
395.70
C-1.25

394.45
396.46
C-2.01

Lt.

Rt.

10+00

$$\begin{array}{r} 393.31 \\ 393.25 \\ \hline C-1.94 \end{array}$$

$$\begin{array}{r} 393.31 \\ 396.07 \\ \hline C-2.76 \end{array}$$

9+50

$$\begin{array}{r} 393.03 \\ 394.40 \\ \hline C-1.37 \end{array}$$

$$\begin{array}{r} 393.03 \\ 395.30 \\ \hline C-2.27 \end{array}$$

9+00

$$\begin{array}{r} 392.75 \\ 393.83 \\ \hline C-1.08 \end{array}$$

$$\begin{array}{r} 392.75 \\ 394.11 \\ \hline C-1.36 \end{array}$$

8+50

392.47

$$\begin{array}{r} 392.47 \\ 392.62 \\ \hline C-0.15 \end{array}$$

8+00

$$\begin{array}{r} 392.20 \\ 392.47 \\ \hline C-0.27 \end{array}$$

$$\begin{array}{r} 392.20 \\ 393.84 \\ \hline C-1.64 \end{array}$$

7+50

$$\begin{array}{r} 392.45 \\ 394.11 \\ \hline C-1.66 \end{array}$$

$$\begin{array}{r} 392.45 \\ 394.97 \\ \hline C-2.52 \end{array}$$

7+00

$$\begin{array}{r} 392.70 \\ 395.00 \\ \hline C-2.30 \end{array}$$

$$\begin{array}{r} 392.70 \\ 395.50 \\ \hline C-2.80 \end{array}$$

Lt.

Rt.

13+50

$$\begin{array}{r} 395.25 \\ 396.35 \\ \hline C-1.10 \end{array}$$

$$\begin{array}{r} 395.25 \\ 398.25 \\ \hline C-3.00 \end{array}$$

13+00

$$\begin{array}{r} 394.97 \\ 396.16 \\ \hline C-1.19 \end{array}$$

$$\begin{array}{r} 394.97 \\ 397.94 \\ \hline C-2.97 \end{array}$$

12+50

$$\begin{array}{r} 394.69 \\ 396.51 \\ \hline C-1.82 \end{array}$$

$$\begin{array}{r} 394.69 \\ 397.85 \\ \hline C-3.16 \end{array}$$

12+00

$$\begin{array}{r} 394.42 \\ 396.14 \\ \hline C-1.72 \end{array}$$

$$\begin{array}{r} 394.42 \\ 397.34 \\ \hline C-2.92 \end{array}$$

chk.

$$\begin{array}{r} 0.02 \\ 396.90 \\ 396.88 \end{array}$$

11+50

$$\begin{array}{r} 394.14 \\ 396.35 \\ \hline C-2.21 \end{array}$$

$$\begin{array}{r} 394.14 \\ 397.15 \\ \hline C-3.01 \end{array}$$

11+00

$$\begin{array}{r} 393.86 \\ 395.91 \\ \hline C-2.05 \end{array}$$

$$\begin{array}{r} 393.86 \\ 397.21 \\ \hline C-3.35 \end{array}$$

10+50

$$\begin{array}{r} 393.58 \\ 395.82 \\ \hline C-2.24 \end{array}$$

$$\begin{array}{r} 393.58 \\ 396.79 \\ \hline C-3.21 \end{array}$$

Afton Rd.

46

Lt.

Rt.

17+00

16+00

15+00

15+20

15+00

14+50

14+00

396.20

396.20

396.08
397.16
C-1.08

396.08
397.58
C-1.50

395.80
397.35
C-1.55

395.80
398.03
C-2.23

395.53
396.91
C-1.38

395.53
397.85
C-2.32

GRADES - STORM DRAIN

open Rubble Bottom with Bank Protection
Bank Sides

South of CAMINO DEL RIO
at the Easterly Boundary of
the Pueblo of San Diego

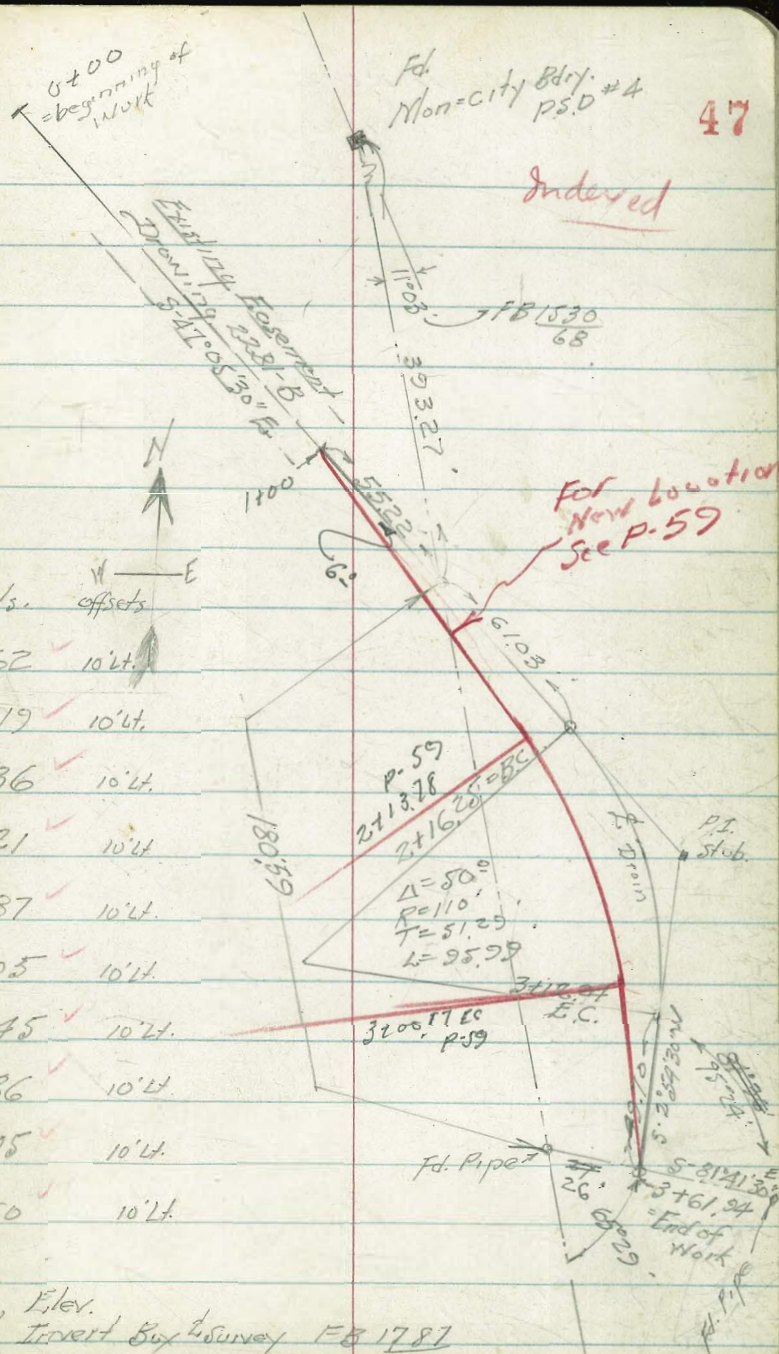
Walker Plan 4509-B
Huffman Pt. of Way Plot = 4508-B
Bishop 1-28-52 No. 20964

References, Original Survey FB. 1787-45,
Not followed exactly in the Above Plans.

For Revised Location see P-59

		Elev. Stakes	Elev. Invert	Cuts.	Offsets
2+61.94 = End work	+ 1.80	116.82	114.20	C 2.62	10' Lt.
2+12.24 = E.C.	2.87	112.15	110.96	C 1.79	10' Lt.
2+80.25	6.46	108.56	108.92	F 0.36	10' Lt.
2+48.25	4.93	110.09	106.88	C 3.21	10' Lt.
2+16.25 = BC	8.31	106.71	104.84	C 1.87	10' Lt.
2+00	2.17	108.85	103.80	C 2.05	10' Lt.
1+50	11.97	103.05	100.60	C 2.45	10' Lt.
T.P.					
1+00	15.26	115.02	99.76	C 2.36	10' Lt.
0+50	6.32	94.25	94.20	C 0.05	10' Lt.
0+00	6.07	94.50	91.00	C 3.50	10' Lt.
	12.65	100.57	87.92		

Elev.
B.M. Invert Box 2 Survey FB 1787
47



ROUGH GRADES - 53rd ST.

Walker
Rope
Huffman
5-7-52
Plan 9259-L NO 62242

Cont. P. 49

1+80	
1+60	
1+40	
1+20	
1+00	
0+80	
0+60 = P.V.C	
0+30	
300' South of S.W. Redwood = 0+00 B.M. NE B.P. 54th Redwood & 53 rd St. = PLAN 9259-L	283.35

25' L

274.00
74.90
C 9.90

273.94
75.37
C 1.43

273.69
75.56
C 1.87

273.27
74.52
C 1.35

272.67
74.09
C 1.42

271.90
73.25
C 2.05

270.94
74.00
C 3.06
1.59

269.41
73.75
C 4.34

267.87
72.31
C 4.44

Indexed

25' R 48

274.41
71.88
F 2.53

274.32
72.04
F 2.28

274.03
72.39
F 1.64

273.58
72.89
F 0.69

272.93
72.98
C 0.05

272.12
72.49
C 0.37

271.11
72.16
C 1.05
1.65

269.47
71.03
C 1.56

267.83
69.56
C 1.73

53rd St. Cont. from P-48

49

3+00 = SL. Redwood

25' L

⊘

25' RT

2+80 = B.C. Curb Return

273.08

273.63

2+00 = R.V.C. Existing Curb

273.89⁰
74.71
C.O. 82.

274.33⁻
73.16
F 1.17

Cont. P-48.

5319 ST. SEWER GRADES

from Redwood St. South

Walker Plan 2259-L

Pope

Huffman

5-13-52

	El Stake	El. Invert	Cuts	offsets
Lat #5	27583	26802	7.81'	5' from End
Lat #4	27156	26831	3.25'	" " "
Lat #3	27264	26833	4.31'	" " "
Lat #2	27312	26890	4.32'	" " "
Lat #1	27328	26939	4.59'	" " "
2+60 - End	27147	26754'	3.93'	45' RT
2+30 = 1/2 MH	27244	26742	5.02'	"
2+10	27301	26734	5.67'	"
1+75	27381	26720	6.61'	"
1+40	27360	26706	6.54'	"
1+05	27373	26692	6.81'	"
0+70	27339	26678	6.67'	"
0+35	27308	26664	6.44'	"
0+00	26650	26650		
0+00 Rim MH	5.97	27293		
0+00 Invert	12.00	26640		
	27389			

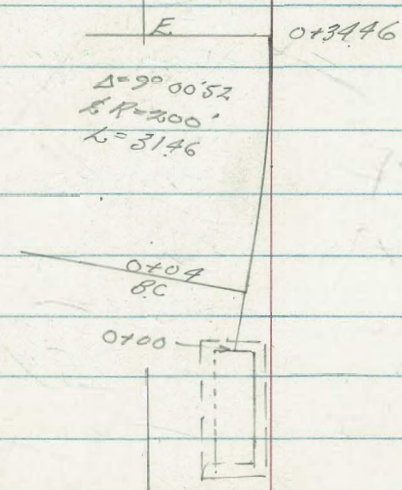
R.M. Top cb 2+00 on lt P-49

GRADES FOR CULVERT, LOGAN AVE
 Bet 46th & Pryncheon Sts
 Plan 4552-B NO 20845

Walker
 Pope
 Huttman
 5-9-52

	Elav. Stakes	Elav. Invert.	Cuts	Offsets.
N.L. Logan 2+60.34 Δ 90° Lt	109.25	103.32	5.93	5' RT. Pryncheon
2+46.34 = Δ Clearance	109.40	103.24	6.16	"
2+20	109.00	103.11	5.89	"
1+80	108.41	102.90	5.51	"
1+40	107.85	102.69	5.16	"
1+00	107.16	102.48	4.68	"
0+60	106.45	102.27	4.18	"
0+34.46 = E.C.	106.06	102.13	3.93	"
0+12.73	105.78	102.05	3.73	"
0+04 = B.C.	105.17	101.97	3.20	"
0+00 = Inside Edge Inlet	105.06	101.95	3.11	"
0+00 Invert Existing Box		101.69		

2+60.34 = End
 14'



118.77 ←

B.M. NW B.P. Logan + 47th
 46th St.

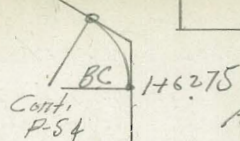
GRADES FOR CULVERT - PLUM ^{AND} ADDISON ST.

Between Canyon Road & Clove St.

Walker
Pope
Presley
Parks 10-16-52.

PLAN # 2399-4 110 20751

INDEXED
FEB 13 1953



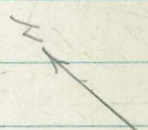
53

ADDISON

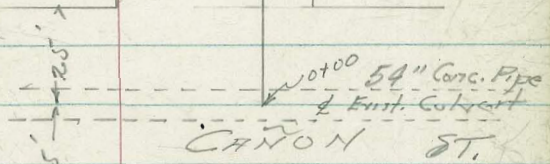
Station	Cont. P. 54	Elev. stakes	Elev. Invert	Cuts.	offsets
TP 7.91	100.39	176	92.48		
1+00		176	92.48	83.85	8.63 C.U.
0+73.28 = E.V.C.		562	88.62	82.60	6.02 "
0+65.52		608	88.16	81.55	6.61 "
0+57.88		678	87.46	79.83	7.63 "
0+50.42		917	85.07	77.45	7.62 "
TP 13.26	94.24	374	80.98		
0+43.20		374	80.98	74.43	6.55 "
0+36.27		593	78.79	70.79	8.00 "
0+29.54		912	75.60	66.47	9.13 "
0+26.00		1273	71.99	64.61	7.38 "
0+22.19		1299	71.73	63.40	8.33 "
0+18.23 P.V.		1359	71.13	62.87	8.26 "
TP 12.87	84.72	936	71.85		
0+00		208	70.13	62.01	8.12 "
11.01	72.21	6120			

← 50 → 20'

PLAN OF



20'



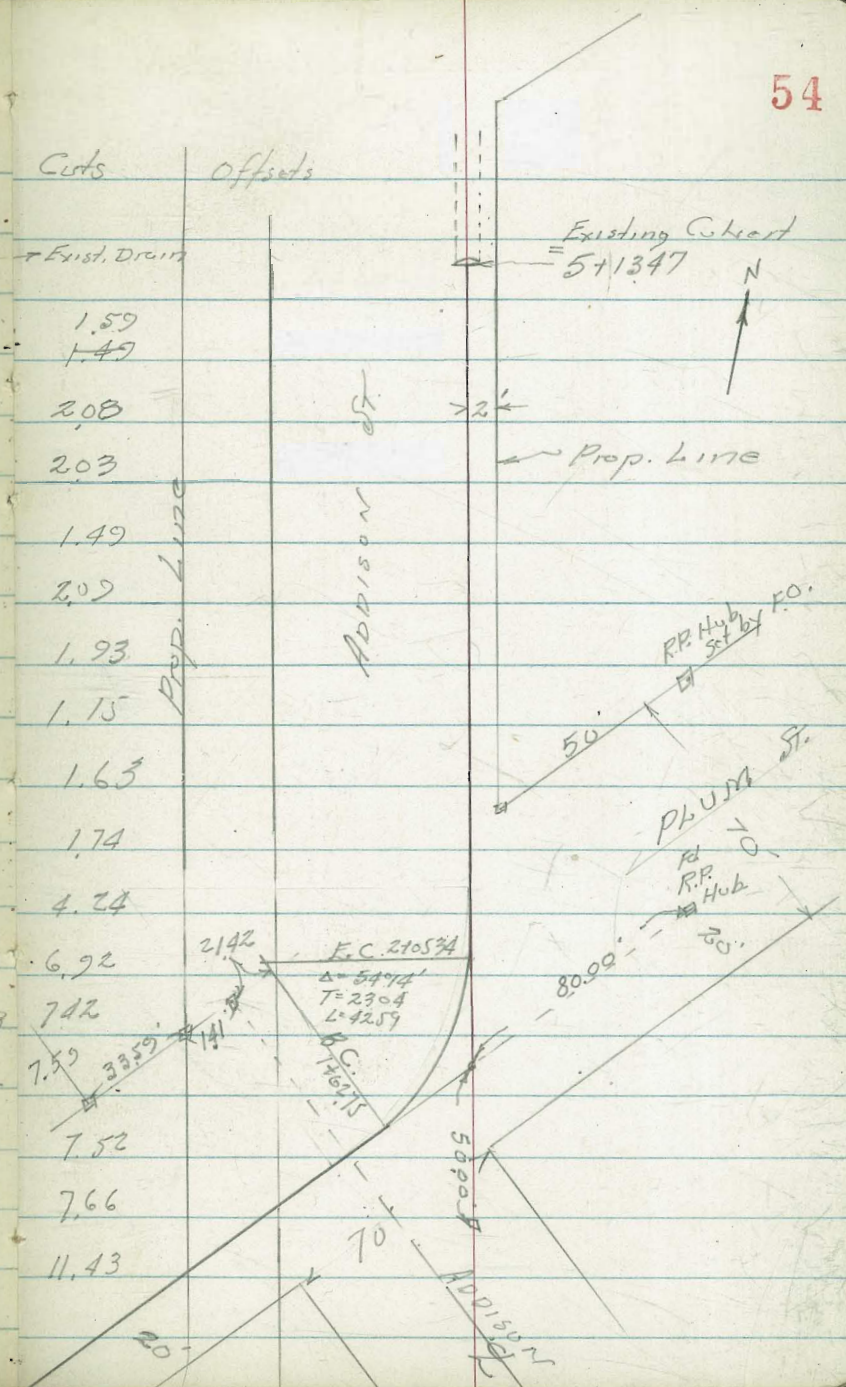
CANYON ST.

N.W. BR. CANYON & WILLOW

Grades Culvert - Plum & Addison St.
Contd. from P-53

Station	Elev. Stakes	Elev. Invert	Cuts	Offsets
5+13.47	314 106.08	103.97 104.10	Exist. Drain	
5+09	412 105.10	103.51 103.61	1.59 1.49	
5+01	434 104.88	102.80 102.85	2.08	
4+93 = P.V.C	486 104.36	102.33	2.03	
4+50	742 101.80	100.31	1.49	
4+15	846 100.76	98.67	2.09	
3+80 T.P.	1026 102.22	98.96	1.93	
3+45	386 96.53	95.38	1.15	
3+10	502 95.37	93.74	1.63	
+75	658 93.84	92.10	1.74	
2+40	570 94.69	90.45	4.24	
2+05.34 F.C.	27°07' 464 95.75	88.83	6.92	
1+94.70	20°20'15" 464 95.75	88.33	7.42	
1+84.05	13°33'30" 498 95.41	87.82	7.59	
1+73.40	6°46'45" 555 94.84	87.32	7.52	
1+62.75 = B.C.H.	592 94.47	86.81	7.66	
1+22.70	3.71 96.68	85.25	11.43	

Contd. from P-53 100.39



MEADE AVE. (PAVING)

GRADES FOR SEWER

Plan 94064 NO 32079

55

Walker
Pope
Presley
10-21-52

INDEXED
law

FEB 16 1953

Lateral No 2	342.53	345.00	4.53	5' West
Lateral No 1	342.58	345.40	4.18	5' West
2+30.54	349.66	343.82	5.84	5' South
1+82.82	342.22	344.43	4.79	5' North
0+00 = E Line Meade	343.62			B.M. S.E.B.P. Monroe & Meade

Curb Grades - MERIDE AVE.

from Menlo to 47th

Welker Plan 9406-L NO 32079

Papa
Prestley
10-21-52

INDEXED

Law

FEB 16 1953

1+25

1+00

0+75

0+50

0+20

0+00

S.M. SE. B.P. Norvac & Menlo 343.62

Left

±

Right

56

Curb	Gut.			Gut.	Curb
349.73	349.23		349.64	349.44	349.94 49.45 F 949
349.84	349.34		349.76	349.55	350.05 50.13 C 008
349.95	349.45		349.87	349.66	350.16 50.15 F 001
350.06	349.56		349.99	349.77	350.27 350.49 C 022
350.17	349.67		350.13	349.88	350.38 50.22 C 054
350.27	349.77		350.05	350.09	350.50 50.52 C 002

MELHUR, AVE.

Left

L

Right

57

2+80

Curb Gut

348.89 348.49
48.76
F 0.13

348.94

Gut. cb

348.85 349.25

2+76

(Rt. of Prop)
349.60
49.01
F 0.59

348.92 348.51

348.92 349.51
49.10
F 0.41

2+50

349.08 349.64
49.14
C 0.06

349.08

349.94 349.38
49.23
F 0.15

2+25

349.24 349.77
49.68
C 0.44

349.19

349.02 349.49
49.82
C 0.33

2+00

1+88.8

East. cb
349.52

349.40 348.90
49.72
C 0.32

349.30

349.10 349.60
49.62
C 0.02

1+75

349.51 349.01

349.41

349.21 349.71
349.58
F 0.16

1+50

349.62 349.12

349.53

349.32 349.82
49.51
F 0.31

MEADE, AVE.

Lt.

Q

Right.

58

Curb Gut

Gut. cb.

V.L. 471b
= 3+75.64

34879 34824
48.79
000

34866

34862 34917
49.17

3+55.64

34881 34829
48.82
C 0.01

34878

34867 34919
49.24
C 0.05

3+25

34884 34837
48.95
C 0.11

34885

34873 34921
49.08
F 0.13

3+00

Rt at Prop
34933
34903
F 0.30

34887 34844
49.74
C 0.87

34890

34879 34923
49.91
F 0.22

PROPOSED EXTENSION DRAINAGE CHANNEL

South of CAMINO DEL RIO

At the Easterly Boundary

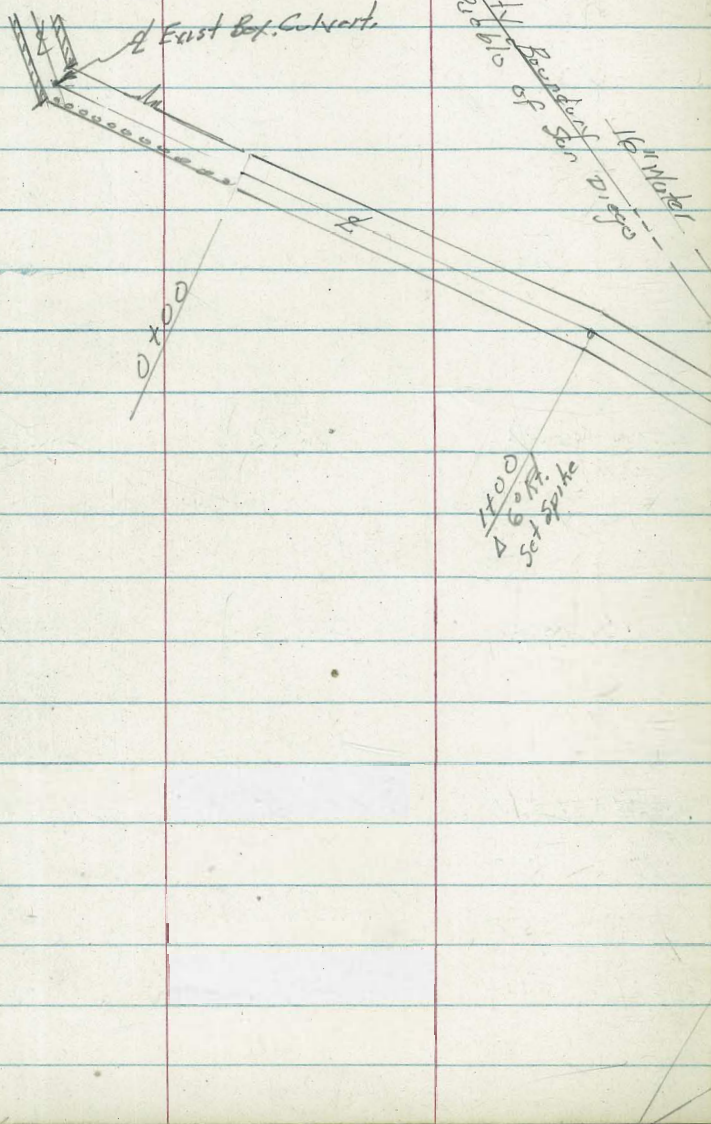
Walker
Rope
H. H. H. H.
Presley
11-19-52

Drawing 4509-B

NO 20964

East Bx. Convent

16" Metal
Diggs
of San Diego



INDEXED
Law
FEB 1 1953

2+12.78 BC

$\Delta = 33^\circ$
 $R = 150$
 $L = 86.39$
 $T = 44.43$

3+00.17 EC

3+32.59

3+52.39

26'

Stake

P.L. set spike

set Nail

Nail

0 x 00

1400
60 ft.
set spike

CONST. GRADES - DRAIN - BLK. 9

VALENCIA PARK

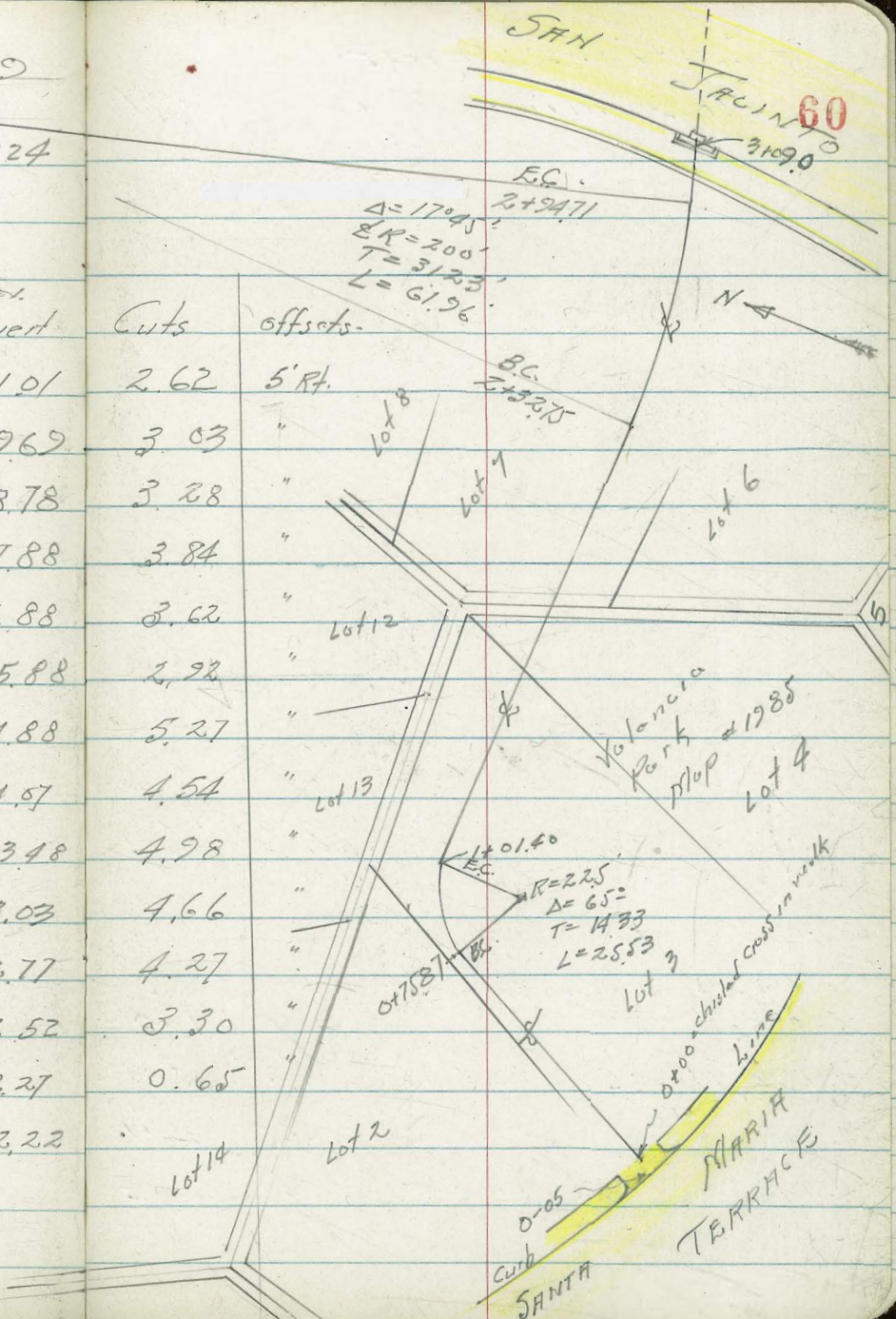
Walker Plan 4622-B 110 20124

Poppe
Hoffman
Presley
11-12-52

INDIVIDUAL
Law

FEB 16 1953

Station	Elev. Stakes	Elev. Invert	Cuts	Offsets
2+62.5	4°15.67	163.63	161.01	2.62 5' Rt.
2+50	2°28.25	162.72	159.69	3.03 "
2+32.75 = BC. H.		162.06	158.78	3.28 "
2+25		161.72	157.88	3.84 "
2+00		160.50	156.88	3.62 "
1+75		158.80	155.88	2.92 "
1+50 T.P.		160.15	154.88	5.27 "
1+25		158.61	154.57	4.04 "
1+01.40 = EC		158.46	153.48	4.98 "
0+75.87 = BC		157.69	153.03	4.66 "
0+50		157.04	152.77	4.27 "
0+25		155.82	152.52	3.30 "
0+00 = Prop line		152.92	152.27	0.65 "
0-05		152.22	152.22	
B.N. Chisled Cross 0+00 15 2126 58		152.80		



Const. Grades - Culverts

Blk. 2, Valencia Park Unit #1

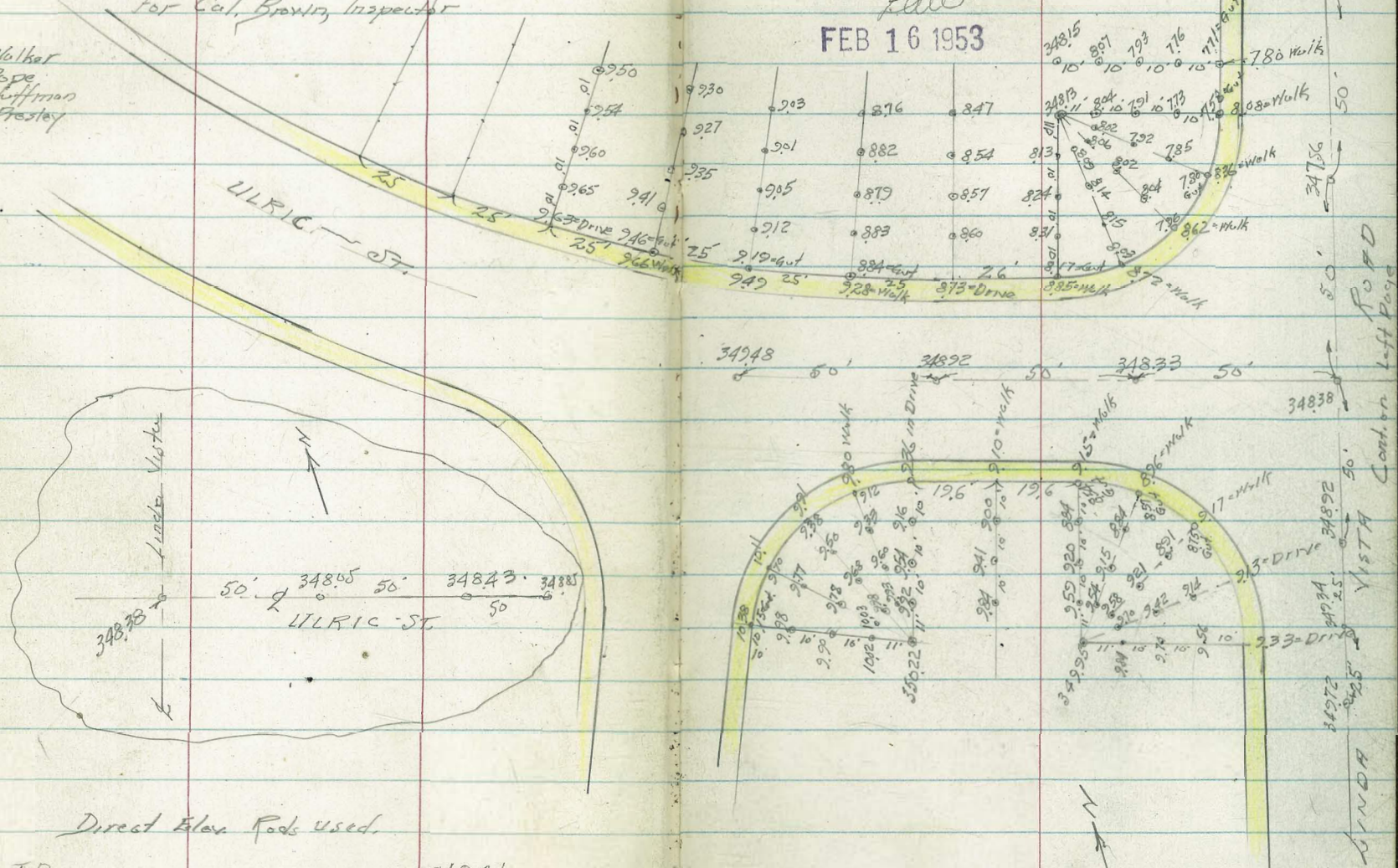
		Elev. Stakes	Elev. Invert	Cuts	offsets
3 + 09.0	Inside Edge Box		167.60		
2 + 13.7					
2 + 24.71	= F.C. 8°52.5	174.05	165.39 84	8.66	5' RA
2 + 85	TP 7°29.03	168.55	163.89 71	4.66 84	'
2 + 75	6°03.59	165.42	162.34	3.08	'

Elevations Existing Pavement & Walks
 LINDA VISTA ROAD AND ULRICH STS.
 To determine Patch Work
 For Cal. Boring Inspector

Walker
 Pope
 Huffman
 Foster

12-4-52
 345.57
 82

INDEXED
 FEB 16 1953



Direct Elev. Rods used.

T.P. 349.21

B.M. Painted Cross on Curb 345.53

South curb Linda Vista Rd & Alley East of Ulrich



LINDA VISTA ROAD
 Cont. on Left Page

Const. GRADES SEWER - GLORIA ST.
Between Franklin & Ocean View

Walker
Hoffman
12-10-52

NO 20009

Plan 942-D

INDEXED

Law
FEB 16 1953

63

OCEAN

	Elev. Stakes	Elev. Invert	Cuts	Offsets	
1+32.5 - End of M.H.	141.66	139.26	2.40	4' RT	0+39.5
1+25	141.90	139.16	2.74	"	
1+00	142.71	138.98	3.73	"	
0+75	143.44	138.80	4.64	"	
0+50	144.24	138.63	5.61	"	30' 30'
0+25	144.96	138.45	6.51	"	
0+00	145.70	138.28	7.42	"	0+00

146.25
140.5
Exist. Sewer

136.42

144.42

FRANKLIN

M.H. #6 - Plan 942-D

B.M. from M.H.

GRADES

FOR DRAINAGE EXTENSION

South CAMINO DEL RIO.

Walker Location Page 59

Bope
Ryan

2-10-53

See

3+32.59

3+00.17=FC 7.17 113.28

3+78.58 8.25 112.20

3+56.98 9.15 111.30

TP 11.21 120.45 0.40 109.24

2+35.38 0.40 109.24

2+13.78=80 4.62 104.25

1+50 6.27 103.37

1+00 2.79 99.65

TP 1310 109.64 2.61

~~1+00=ACR~~ 2 2 96.54

0+50 1.53

0+00 4.60

11.23 22.15

87.92

B.M. - Invert Exist Box Culvert
p-47Indexed

(Ditch had been graded
by Street Dept. Wilhens
We had this half stated
They informed us that no
grades were necessary.)

393,92

395,37

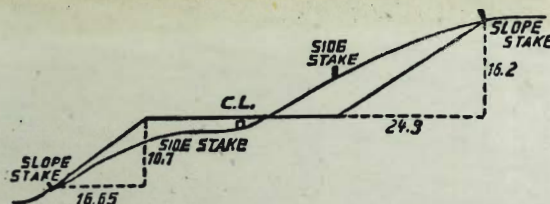
2 2 2
2 2 ?

2

555
555
1110

55
27

1233
535
1768



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
HOLYOKE MASSACHUSETTS
NEW YORK CHICAGO BOSTON SAN FRANCISCO