

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

INDEXED  
*Completely*

MICROFILMED

APR 13 1965

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope made from side of shoulder  
make last angle with roadway slope 1/2 to 1  
If ground unevenly level the cut or fill of this

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IMPROVED TABLES  
AND  
INFORMATION

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TABLE No. VII

To find Tangent and External in curve of  
any other degree divide by degree of curve and  
add external found in column of constants.  
Degree of curve, when given, I may be found  
by dividing tangent (or constant) by  
given tangent (or constant).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the degree.



TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.88	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Ocean View

1

43<sup>rd</sup>, Boundary to National, rough grades 2.

National & 43<sup>rd</sup>, stakes for culvert 4

43<sup>rd</sup>-National to Newton, rough grades 6

43<sup>rd</sup>, Alpha to Boston, curb stakes 17

43<sup>rd</sup>-National to Logan, rough grades 25

Catalina Terrace, stakes new returns

at N'y end 15' alley

28<sup>th</sup> & J- stakes city constr. 30" 32

Conc. culvert

Rogers St. - San Elijo to San Fernando 33

Hancock & Courts - Stake St. drain 34

Univ. Hts. - Alley Bk. 138, Stakes for paving 35

Keating - W. of Linwood - tentative stakes 37

Conde & Pine, Sewer stakes 38

Valencia Park, Bk. 10, Culvert stakes 39

Hayes - Vermont to Johnson 40

Reed, Lamont to Olney 48

La Jolla Shores Drive - stake sewer 52

Oliver - Ingraham to Jewell, rough grades 54

Reed Ave. - Lamont to Olney, pave 71



INDEXED

SEP 1 1950

10 10

Set stakes - 5' Back  
of Prop. for St. Dept.  
To grade - St.

W.O. 20008

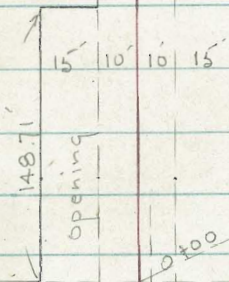
See 3255-B

G-130-P57

San Pasqual St.

opening

312.42



Fd. Cross. in  
Rim of M.H.  
B1748-P.33

15' 10' 10' 15'

opening

Pipe?

Logan Ave.

opening

Ocean View

Fd. Ld. + ct.

Fd. Disk

30'  
30'

1

9-22-49

Osborne  
Hardin  
Hatch  
Shepard

12 + 74.88

10' 10'

San Pasqual St.



Rough Grades - 4<sup>th</sup> Boundary  
To National

**INDEXED**  
mk.  
**SEP 1 1950**

W.O. 22020 10-4-49 - 70.

W. Side

E.

0+00 = Meet cbs. - 27' N. of Boundary

58.00

58.00

0+50 65.78 <sup>65 18</sup> 61.02 C-4.2

57.30

61.03  
57.30

F-3.73

1+00 70.45 <sup>70 45</sup> 64.04 C-6.4

62.23

64.06  
2.23

F-1.83

1+50 73.70 <sup>73 70</sup> 67.06 C-6.6

65.76

67.09  
5.76

F-2.3

2+00 76.62 <sup>6 62</sup> 70.08 C-6.54

67.65

70.12  
7.85

F-2.5

2+39.17 = S.L. Grama 76.93 <sup>6 93</sup> 72.42 C-4.51

69.19

72.49  
9.19

F-3.30

2+79.17 = 75.51 <sup>5 51</sup> 74.90 C-0.61

70.17

74.91  
0.17

F-4.74

3+19.17 = N.L. 81.21 <sup>81 21</sup> 77.40 C-3.81

72.67

77.33  
2.67

F-4.66  
F-4.7



	W.			E.		
3+75	85.28	80.70 <sup>5.3</sup>	C-4.6 C-4.58	80.12	80.70 <sub>12</sub>	F-0.58
4+15	86.35	82.94 <sup>3.5</sup>	C-3.41	82.71	82.94 <sub>1</sub>	F-0.23
4+55	86.76	84.78 <sup>1.76</sup>	C-2.0 C-1.98	84.16	84.78 <sub>16</sub>	F-0.62
4+95	86.65	86.23 <sup>0.5</sup>	C-0.42	85.75	86.23 <sub>5.75</sub>	C-0.48
5+35	86.93	87.29 <sup>0.36</sup>	F-0.36	86.56	87.29 <sub>6.56</sub>	F-0.73
5+75	87.30	87.93 <sup>0.63</sup>	F-0.63	87.04	87.83 <sub>0.79</sub>	F-0.79
6+08.58 = N.L. Beta						
6+28.58 =	86.63	88.54 <sup>1.91</sup>	F-1.91	88.07	88.54 <sub>8.07</sub>	F-0.47



Stakes for Culvert - Nat + 48<sup>th</sup>

BM 29.69 on Pole

4

0+00 = line end at Abutment

0+01

- 8' Rt.

27.57  
26.25 ✓

C 27.32  
28.31  
21.48  
C 6.83 ✓

1+66.00 = ERE.

35.73  
29.67 ✓  
C 7.06

+ 25

INDEXED  
MK.

SEP 1 1950

29.44  
22.75 ✓

C 6.69

1+91

37.09  
29.94 ✓  
C 7.15

+ 49.78 = B.R.C.

2+26

39.30  
31.73 ✓  
C 7.57

+ 64.30

30.16  
23.49 ✓

C 6.67 ✓

2+61

41.55  
33.52 ✓  
8.03

+ 78.83

31.02  
24.23 ✓

C 6.79

2+96

43.61  
35.31 ✓  
C 8.30

+ 93.35

31.36  
24.97 ✓

C 6.39 ✓

3+31

45.72  
37.10  
C 8.62 ✓

1+07.89 = P.R.C.

32.17  
25.71 ✓

C 6.46 ✓

3+66

47.33  
38.89 ✓  
C 8.44

+ 22.41

33.12  
26.48 ✓

C 6.64 ✓

4+01

48.59  
40.68 ✓  
C 7.91

+ 36.94

33.79  
27.19 ✓

C 6.60 ✓

4+17

49.20  
41.48 ✓  
C 7.72

+ 51.46

34.82  
27.93 ✓

C 6.89 ✓

4+33

49.46  
42.21 ✓  
C 7.25



BM 58.90 Culvert

5

4 + 49

50.29  
42.86  
C 7.43 ✓

Set Cut Stakes for water Meter

E Line of 43 St. stakes set 3' E of CB.

0 + 00 = S Line of National

BM

+ 65

50.75  
43.46  
C 7.29 ✓

+ 81

51.12  
44.00  
C 7.12 ✓

0 + 75

$\frac{0}{0}$   
59.00  
59.50  
Fill 0.50

60.09  
59.60  
C 40.49

5 + 16

52.08  
45.03  
C 7.05 ✓

+ 51

52.69  
46.07  
C 6.62 ✓

1 + 81

62.39  
62.55  
F 0.17

64.07  
62.66  
C 1.41

+ 86

53.43  
47.10  
C 6.33 ✓

6 + 21

54.05  
48.14  
C 5.91 ✓

62.33  
62.40  
F 0.20

+ 56

54.87  
49.17  
C 5.70 ✓

6 + 85 =  $\pm$  Box 8" AP

55.73  
50.00  
C 5.73 ✓

10 RP  
on Diag

5.34  
50.  
5.34

Cont on P. 11



Rough Grades - 4<sup>th</sup> rd

Nat. to Newton

Nail - N.E. Pole  
National + 4<sup>th</sup> rd

58.90

6

S' Back stake Grade

W.

N.L. Nat. = end 58.3 <sup>8.3</sup> 57.4 C 0.9 55.1 57.25 <sub>5.1</sub> F - 2.1 ✓

INDEXED

N.S.

SEP 7 1950

± 58.3 <sup>8.3</sup> 57.5 C 0.8 55.8 57.4 <sub>5.8</sub> F 1.6 ✓

S.L. Nat. = 0+00 58.0 58.0 G 56.5 57.5 <sub>6.5</sub> F 1.0 ✓

+ 40 56.0 <sup>9.2</sup> 58.7 <sub>6.6</sub> F 2.7 59.2 58.6 C 0.6 ✓

+ 80 60.1 <sup>60.1</sup> 59.7 C 0.4 59.9 59.7 C 0.2 ✓

+ 27.66 63.1 <sup>3.1</sup> 61.1 C 2.0 61.1 61.1 = G

+ 75.33 64.3 <sup>4.3</sup> 62.5 C 1.8 62.2 62.5 <sub>2.2</sub> F 0.3 ✓

+ 15.33 65.5 <sup>5.5</sup> 63.6 C 1.9 63.1 63.6 <sub>3.1</sub> F 0.5 ✓

+ 55.33 66.9 <sup>6.9</sup> 64.6 C 2.3 64.3 64.6 <sub>4.3</sub> F 0.3 ✓



B.M. - Levels

E

W.

7

PC Ret. - 18' N.

2 + 90.33 =

67.8

7.8

65.5

C 2.3

340 8.33

U.L. Tow.

64.7

65.4

F 0.7

N.I.

67.8

68.0

F 0.2

7.8

4.7

New B.P.'s in Curb.

N.E. - N - Keeler

73.92 ✓

N.E. - N - Boston

79.26 ✓

N.E. - N - Newton

65.58 ✓

N.W. - N - Alpha

86.40 ✓

N.E. - N - Beta

88.05 ✓

N.W. - N.

77.95 ✓

N.E. - N - Delta

58.00 ✓

Nat. + 43.3

N.W. B.P. on Inlet

57.24 ✓

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Rough Grade stakes - Beta - N.

8

W.

E.

0+00 = 20' N. of N.L. Beta	88.5			88.5		
+35	87.2	88.9 7.7	F 1.7	88.8	88.9 8.8	F 0.1
+70	87.9	89.3 7.9	F 1.4	89.2	89.3 9.2	F 0.1
1+05	88.6	89.7 8.6	F 1.1	89.3	89.7 9.3	F 0.4
1+41.4	88.3	90.1 8.3	F 1.8	90.3	90.1 0.3	C 0.2
+81.4	89.4	90.5 9.4	F 1.1	90.6	90.5 0.6	C 0.1
2+21.4	90.4	90.7 0.4	F 0.3	91.1	90.7 1.1	C 0.4
+61.4	90.8	90.7 0.8	C 0.1	91.5	90.7 1.5	C 0.8
3+01.4	91.6	90.5 1.6	C 1.1	91.8	90.4 1.8	C 1.4
3+56	90.7	90.1 0.7	C 0.6	91.5	89.6 1.5	C 1.9

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	W.			E.		
4+01.4	88.6	88.5 <sup>8.6</sup>	C 0.1	90.7	88.6 <sup>0.7</sup>	C 2.1
+41.4	87.6	87.1 <sup>7.6</sup>	C 0.5	88.6	87.4 <sup>8.6</sup>	C 1.2
+66.0	86.8	86.2 <sup>6.8</sup>	C 0.6	87.6	86.6 <sup>7.6</sup>	C 1.0
5+03.7	85.0	85.2 <sup>5.0</sup>	F 0.2	86.6	85.4 <sup>6.6</sup>	C 1.2
5+41.4	83.5	84.2 <sup>3.5</sup>	F 0.7	85.7	84.2 <sup>5.7</sup>	C 1.5
+81.4	82.0	83.0 <sup>2.0</sup>	F 1.0	82.1	83.0 <sup>2.1</sup>	F 0.9
6+21.4	77.2	82.0 <sup>7.2</sup>	F 4.8	80.2	82.0 <sup>0.2</sup>	F 1.8
+61.4	74.1	81.3 <sup>74.1</sup>	F 7.2	79.3	81.3 <sup>9.3</sup>	F 2.0
7+01.4	72.8	80.9 <sup>2.8</sup>	F 8.1	79.6	80.9 <sup>9.6</sup>	F 1.3
7+41.4	72.9	80.6 <sup>72.9</sup>	F 7.7	79.1	80.6 <sup>79.1</sup>	F 1.5











Curb Stakes - E. Side - Newton to Nat.

12

Ret.							
Prop.-E.L.	67.88	66.70 <sup>7.88</sup>	C 1.18	2+10.33	59.83	59.72 <sup>.83</sup>	C 0.11
±	65.83	66.00 <sup>5.83</sup>	F 0.17	+30.33	58.56	59.17 <sup>8.56</sup>	F 0.61
P.C. = 0+00 ahead	65.56	65.55 <sup>.56</sup>	C 0.01	+50.33	58.47	58.69 <sup>.47</sup>	F 0.22
+15	65.14	65.15 <sup>14</sup>	F 0.01	+70.33	57.80	58.29 <sup>7.80</sup>	F 0.49
+45	64.41	64.38 <sup>41</sup>	C 0.03	+90.33	57.58	57.97 <sup>58</sup>	F 0.42
+75	63.45	63.61 <sup>45</sup>	F 0.16	2+10.33	57.61	57.72 <sup>61</sup>	F 0.11
+95	62.85	63.08 <sup>2.85</sup>	F 0.23	+30.33	57.7d	57.51 <sup>7d</sup>	C 0.20
1+15	62.43	62.52 <sup>43</sup>	F 0.09	+50.33	57.90	57.44 <sup>90</sup>	C 0.46
+46.78	61.70	61.59 <sup>70</sup>	C 0.11	+70.33	57.81	57.41 <sup>80</sup>	C 0.40
+78.56	60.86	60.65 <sup>86</sup>	C 0.21				

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Curb Stakes - E. side - Newton to Keeler

W. Side Newton to Keeler

S.E. Newton

N. end

67.92  
67.95 67.86 C 0.09

67.94 67.79 C 0.15

68.00 67.86 C 0.14

PC. 67.61 67.90 F 0.29

Prop. PC 67.43 67.94 F 0.51

Rake to Keeler

N.E. Keeler

Prop. PC 74.0 73.93 C 0.07

PC. Ret. 74.19 74.00 C 0.19

73.81 74.28 F 0.47

73.70 74.56 F 0.86

74.83 74.75 C 0.08

end: 74.90 74.97

5 parts - 9.42 each

S.W. Newton

W. end = PC.

66.30

66.38 66.58.69 F 0.31

66.63 66.83 67.04 F 0.41

66.89 67.10.18 F 0.29

66.86 67.30.23 F 0.37

~~74.57~~ = E.C. 67.37 67.50.35 F 0.13

Rake to Keeler

N.W. Keeler

PC. Ret. 72.40 72.50.40 F 0.20  
4 Parts

~~72.14~~ - 1/4 72.05 72.61 F 0.56

~~72.4~~ 1/2 72.41 72.70 F 0.29

~~72.53~~ 3/4 72.53 72.65 F 0.12

Meet cb. 72.52 72.55

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E. Side, Keeler to Boston

S.E. Ret. Keeler

Meet cb.

1/4

1/2

3/4

cb. P.C.

Prop. P.C.

0+35-Brk.

Rake to Boston

76.51

76.58 76.51<sup>58</sup> C 0.07

76.27 76.47<sup>27</sup> F 0.20

76.17 76.49<sup>17</sup> F 0.32

75.74 76.53<sup>574</sup> F 0.79

76.25 76.52<sup>25</sup> F 0.27

76.94 76.88<sup>94</sup> C 0.06

N.E. Boston

23-N. of Prop P.C. 78.55 78.76<sup>55</sup> F 0.21

Prop P.C. 79.32 79.23<sup>32</sup> C 0.09

cb. P.C. 79.01 79.32<sup>01</sup> F 0.31

1/4 79.11 79.36<sup>11</sup> F 0.25

1/2 79.47 79.38<sup>47</sup> C 0.09

3/4 79.53 79.47<sup>53</sup> C 0.06

29 chord.

Meet.

79.58

14

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W. Side 43rd Boston to Keeler. - cb. Stakes

4.71    5.1  
6    3.2  
3.74    3.2

15

± Boston to E. = N.L. of 25' Alley to W.

2' Back of W. end of N. Ret. 78.80<sup>98</sup> 79.80<sup>8.80</sup> F 1.00  
F 0.88 2+32 75.13 75.29<sub>13</sub> F 0.16

2' Rad. 79.43 79.68<sup>45</sup> F 0.25  
F 0.37 +52 74.45 74.86<sub>45</sub> F 0.41  
0+00 = 120' N. = N.L. Boston

0+00 78.66 79.38<sup>8.66</sup> F 0.72 +75.1 PC. 73.59 74.41<sub>3.59</sub> F 0.82

+35 78.26 78.77<sub>26</sub> F 0.51 1/3 73.16 74.23<sub>5.12</sub> F 1.07

+70 77.84 78.17<sub>7.84</sub> F 0.33 2/3 72.82 74.04<sub>2.82</sub> F 1.22

1+05 77.40 77.57<sub>7.40</sub> F 0.17. end at W.L. 43rd 72.76 73.85<sub>2.76</sub> F 1.09

+40 76.96 76.97<sub>96</sub> F 0.01

+72 76.15 76.42<sub>15</sub> F 0.27

+92 75.86 76.07<sub>5.86</sub> F 0.21

2+12 75.56 75.70<sub>5.56</sub> F 0.14



Curb Stakes - W. Side 43<sup>rd</sup> - Newton to Nat.

Mon - N.W. Cor Newton = 64.18

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End. of cb = w.L. <sup>43<sup>rd</sup></sup>	64.88	65.55 4.88	F 0.67	1+99.33	59.62	59.72 .12	F 0.10
1/2	64.74	65.45 4.74	F 0.71	2+19.33	59.13	59.17 .13	F 0.04
2/2	64.65	65.30 4.65	F 0.65	+39.33	58.70	58.70 0.00	C 0.08
P.C. = 0+00	64.45	65.25 4.45	F 0.80	+ 5' BK. - P.C.	57.70	58.00 7.70	F 0.30
+32	63.91	64.43 3.91	F 0.52	+14.1 around = Inlet		57.61	
+64	63.06	63.61 3.06	F 0.55	+117 more = Inlet		57.31	
+84	62.62	63.08 2.62	F 0.46	1/2		57.00	
+104	62.17	62.52 2.17	F 0.35	F.C.		56.70	
+35.77	61.29	61.58 1.29	F 0.29				
+67.54	60.70	60.65 0.05	C 0.05				



curb Stakes - W. side 43rd Alpha to Boston

17

N.W. Return				1+20	82.45	82.97 <sub>45</sub>	F 0.52
Meet. 17'-W. of P.C.		88.03		+40	82.15	82.47 <sub>15</sub>	F 0.32
P.C.	87.21	87.88 <sub>21</sub>	F 0.67	+60	81.79	82.03 <sub>79</sub>	F 0.24
1/4	87.01	87.65 <sub>01</sub>	F 0.64	+80	81.43	81.65 <sub>43</sub>	F 0.22
1/2	86.39	87.30 <sub>39</sub>	F 0.91	2+00	81.35	81.32 <sub>35</sub>	C 0.03
3/4	85.88	86.88 <sub>88</sub>	F 1.00	+20	81.13	81.05 <sub>13</sub>	C 0.08
E.C. = 0+00	85.52	86.41 <sub>52</sub>	F 0.89	+40	80.92	80.85 <sub>92</sub>	C 0.07
0+05 = Prop. P.C.	85.49	86.23 <sub>49</sub>	F 0.74	+60	80.57	80.70 <sub>57</sub>	F 0.13
+42.5	83.96	85.19 <sub>96</sub>	F 1.23	+80	80.14	80.61 <sub>14</sub>	F 0.47
+80	83.01	84.15 <sub>01</sub>	F 1.14	3+20.5	79.80	80.48 <sub>80</sub>	F 0.68
1+00	82.84	83.53 <sub>84</sub>	F 0.69				

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W. Side. Alpha to Boston - Cont.

3+61 79.698  $\begin{smallmatrix} 0.36 \\ 9.69 \end{smallmatrix}$  F 0.67

+81 79.118  $\begin{smallmatrix} 0.26 \\ 9.11 \end{smallmatrix}$  F 1.15

4+01 79.568  $\begin{smallmatrix} 0.13 \\ 9.56 \end{smallmatrix}$  F 0.57

+21.7 = S.L. Alley  
2' Rad. 78.997  $\begin{smallmatrix} 9.93 \\ 8.99 \end{smallmatrix}$  F 0.94

2' Bk. at W. end of Ret. 79.378  $\begin{smallmatrix} 0.05 \\ 9.37 \end{smallmatrix}$  F 0.68

Cb Stakes - W. Side 43<sup>rd</sup> Alpha - S

Sw. Return

17' W. of PC - Meet. 89.06

18

PC 88.68 89.28 F 0.60  
 $\begin{smallmatrix} 8.68 \\ 8.68 \end{smallmatrix}$

1/4 87.95 89.54 F 1.69  
 $\begin{smallmatrix} 7.85 \\ 7.85 \end{smallmatrix}$

1/2 88.47 89.76 F 1.29  
 $\begin{smallmatrix} 8.47 \\ 8.47 \end{smallmatrix}$

3/4 88.18 89.90 F 1.72  
 $\begin{smallmatrix} 8.18 \\ 8.18 \end{smallmatrix}$

E.C. = 0+00 88.54 90.00 F 1.46  
 $\begin{smallmatrix} 8.54 \\ 8.54 \end{smallmatrix}$

0+05 89.57 90.08 F 0.51  
 $\begin{smallmatrix} 9.57 \\ 51 \end{smallmatrix}$

+20 90.07 90.18 F 0.11  
 $\begin{smallmatrix} 07 \\ 11 \end{smallmatrix}$

+40 90.56 90.33 C 0.23  
 $\begin{smallmatrix} 56 \\ 23 \end{smallmatrix}$

+60 90.98 90.48 C 0.50  
 $\begin{smallmatrix} 98 \\ 50 \end{smallmatrix}$



Alpha-S Cont. - w. side

0+80      90.80 90.57 C0.23  
 $\frac{23}{80}$

1+00      90.60 90.68 F0.08  
 $\frac{60}{68}$   
 $\frac{8}{8}$

+20      90.23 90.74 F0.51  
 $\frac{23}{74}$   
 $\frac{51}{51}$

+40      90.18 90.74 F0.56  
 $\frac{18}{74}$   
 $\frac{56}{56}$

+60      89.89 90.67 F0.78  
 $\frac{89}{67}$   
 $\frac{78}{78}$

+80      89.59 90.54 F0.95  
 $\frac{59}{54}$   
 $\frac{95}{95}$

2+00      89.68 90.35 F0.67  
 $\frac{68}{35}$   
 $\frac{67}{67}$

+35      89.46 89.95 F0.49  
 $\frac{46}{95}$   
 $\frac{49}{49}$

+70      88.91 89.56 F0.65  
 $\frac{91}{56}$   
 $\frac{65}{65}$

3+05      88.54 89.16 F0.62  
 $\frac{54}{16}$   
 $\frac{62}{62}$

19

3+40      88.34 88.77 F0.43  
 $\frac{34}{77}$   
 $\frac{43}{43}$

N.E. Ret. Beta  
 + 60.3 = opp PC.      88.35 88.54 F0.19  
 $\frac{35}{54}$   
 $\frac{19}{19}$

N.W. Return - Nat. + 43<sup>rd</sup>

10' w. of PC = end      54.57 56.43 F 1.86  
 $\frac{57}{43}$   
 $\frac{86}{86}$

PC.      54.99 56.70 F 1.71  
 $\frac{99}{70}$   
 $\frac{71}{71}$

1/2 to end of Inlet.      55.56 57.00 F 1.44  
 $\frac{56}{00}$   
 $\frac{44}{44}$

end of Inlet      57.19

E. end "      57.22

end at NL.      56.07 57.25 F 1.18  
 $\frac{07}{25}$   
 $\frac{18}{18}$



Cb. Stakes - E. Side - Alpha - to Boston

0+00 = opp. S.W. PC. Alpha. 89.72 89.<sup>72</sup><sub>47</sub> C 0.25

+20 89.01 89.<sup>04</sup><sub>04</sub> F 0.03

+40 88.29 88.<sup>55</sup><sub>29</sub> F 0.26

+60 88.08 88.<sup>08</sup><sub>01</sub> C 0.07

+80 87.30 87.<sup>39</sup><sub>30</sub> F 0.09

1+05 = opp. N.W. Prop. PC 86.58 86.<sup>58</sup><sub>57</sub> C 0.01

+42.5 85.10 85.<sup>36</sup><sub>10</sub> F 0.26

+80 83.93 84.<sup>15</sup><sub>93</sub> F 0.22

2+00 83.27 83.<sup>53</sup><sub>27</sub> F 0.26

+20 82.71 82.<sup>97</sup><sub>71</sub> F 0.26

Pole - S.W. Alpha - 90.92

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20

2+40 SEP 12 1950 82.44 82.<sup>47</sup><sub>44</sub> F 0.03

+60 82.08 82.<sup>08</sup><sub>03</sub> C 0.05

+80 81.77 81.<sup>77</sup><sub>65</sub> C 0.12

3+00 81.21 81.<sup>32</sup><sub>21</sub> F 0.11

+20 81.17 81.<sup>17</sup><sub>05</sub> C 0.12

+40 80.92 80.<sup>92</sup><sub>85</sub> C 0.07

+60 80.77 80.<sup>77</sup><sub>70</sub> C 0.07

+80 80.43 80.<sup>61</sup><sub>43</sub> F 0.18

4+20.5 80.28 80.<sup>48</sup><sub>28</sub> F 0.20

4+61 80.29 80.<sup>36</sup><sub>29</sub> F 0.07



cb. Stakes - E Side - Alpha to Beta

21

4+81 79.98 80.26 F 0.38  
 $\begin{array}{r} 9.98 \\ \hline \end{array}$

0+00 = opp. S.W. P.C. - Alpha 89.70  $\begin{array}{r} 70 \\ 89.47 \\ \hline 23 \end{array}$  C 0.23

4+92  
 cb. P.C. 79.90 80.20 F 0.30  
 $\begin{array}{r} 9.90 \\ \hline \end{array}$

+20 90.05  $\begin{array}{r} 0.05 \\ 89.84 \\ \hline 21 \end{array}$  C 0.21

1/3 79.69 80.22 F 0.53  
 $\begin{array}{r} 9.69 \\ \hline \end{array}$

+40 90.51  $\begin{array}{r} 51 \\ 90.14 \\ \hline 37 \end{array}$  C 0.37

2/3 79.55 80.28 F 0.73  
 $\begin{array}{r} 9.55 \\ \hline \end{array}$

+60 90.66  $\begin{array}{r} 66 \\ 90.39 \\ \hline 27 \end{array}$  C 0.27

end 80.86 80.40 C 0.46  
 $\begin{array}{r} 86 \\ \hline \end{array}$

+80 90.88  $\begin{array}{r} 88 \\ 90.57 \\ \hline 31 \end{array}$  C 0.31

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+100 90.78  $\begin{array}{r} 78 \\ 90.68 \\ \hline 10 \end{array}$  C 0.10

+20 90.94  $\begin{array}{r} 94 \\ 90.74 \\ \hline 20 \end{array}$  C 0.20

+40 90.51  $\begin{array}{r} 51 \\ 90.74 \\ \hline 23 \end{array}$  F 0.23

+60 90.22  $\begin{array}{r} 22 \\ 90.67 \\ \hline 45 \end{array}$  F 0.45

+80 90.11  $\begin{array}{r} 11 \\ 90.54 \\ \hline 43 \end{array}$  F 0.43



2+00      89.95   90.35    F0.40  
                     9.95  
                           40

+35      89.54   89.90    F0.36  
                     34

+70      88.61   89.38    F0.77  
                     8.61

3+05      88.73   88.86    F0.13  
                     8.73

+40      87.96   88.34    F0.38  
                     7.96

Beta - NE. Return  
 +60.3 = PC.      87.86   88.04    F0.18  
                           7.86

1/2      87.86   88.02    F0.16  
                     7.86

2/3      87.77   88.00    F0.23  
                     7.77

end at E.L.      87.67   87.98    F0.31  
                           7.67



cb. Stakes - E. Side - Beta to Line

Mail in pole SW. Cor. Beta # 4324 = 88.13

23

S.E. Ret. - Beta

0+00 - 3.58 S. of P.C. 86.40 <sup>out.</sup> ~~87.29~~ F 0.89  
6 40

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+20 86.12 86.70 F 0.58  
12

+40 85.68 86.23 F 0.55  
5 68

+60 85.33 85.56 F 0.23  
5 33

+80 84.30 84.78 F 0.48  
4 30

+100 83.55 83.92 F 0.37  
55

+120 83.26 82.94 C 0.32  
3 26

+140 81.80 81.87 F -0.07  
1 80

S.E. Return - Beta

end 86.92 87.70 F 0.78  
6 12

2/3 87.08 87.45 F 0.37 +60 80.65 80.70 F 0.05  
0 65

1/3 86.82 87.22 F 0.40 +95 78.70 78.59 C 0.11  
8 2

P.C. 86.63 87.00 F 0.37  
6 63



## W. Side Gamma to Beta

N.W. Ret.

24

2 + 30	76.45	$\begin{array}{r} 6.47 \\ 6.45 \end{array}$	F 0.02	End of cb.	77.84	$\begin{array}{r} 7.84 \\ 76.70 \\ \hline 1.14 \end{array}$	C 1.14
+ 65	74.42	$\begin{array}{r} 4.42 \\ 4.35 \end{array}$	C 0.07	1/3	78.66	$\begin{array}{r} 8.66 \\ 77.00 \\ \hline 1.66 \end{array}$	C 1.66
3 + 00	72.32	$\begin{array}{r} 2.32 \\ 2.23 \end{array}$	C 0.09	2/3	77.64	$\begin{array}{r} 6.4 \\ 77.45 \\ \hline 19 \end{array}$	C 0.19
+ 35	70.26	$\begin{array}{r} 0.26 \\ 0.11 \end{array}$	C 0.15	P.C. = 0 + 00	78.12	$\begin{array}{r} 8.12 \\ 77.88 \\ \hline 24 \end{array}$	C 0.24
+ 70	68.23	$\begin{array}{r} 8.23 \\ 7.99 \end{array}$	C 0.24	0 + 46.65	80.78	$\begin{array}{r} 78 \\ 80.70 \\ \hline 8 \end{array}$	C 0.08
4 + 05	66.58	$\begin{array}{r} 6.58 \\ 6.58 \end{array}$	C 0.71	+ 66.65	81.90	$\begin{array}{r} 90 \\ 81.87 \\ \hline 3 \end{array}$	C 0.03
+ 40	63.98	$\begin{array}{r} 3.98 \\ 3.75 \end{array}$	C 0.23	+ 86.65	83.01	$\begin{array}{r} 3.01 \\ 82.94 \\ \hline \end{array}$	C 0.07
+ 75	61.84	$\begin{array}{r} 1.84 \\ 1.63 \end{array}$	C 0.21	+ 06.65	83.98	$\begin{array}{r} 98 \\ 83.92 \\ \hline 6 \end{array}$	C 0.06
5 + 10	59.44	$\begin{array}{r} 9.51 \\ 9.44 \end{array}$	F 0.07	+ 26.65	84.82	$\begin{array}{r} 82 \\ 84.78 \\ \hline 4 \end{array}$	C 0.04
				+ 46.65	85.43	$\begin{array}{r} 85.56 \\ 43 \\ \hline 13 \end{array}$	F 0.13
5 + 35 = Meet cb.	57.96	58.00					

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92 cb. Rad = B.M. = 63.66

26

N. side Logan - 0+00 = W.L. 43<sup>rd</sup>

= 0+00

+22.6 = E.C.

64.0 64.5 F 0.5  
4.0

0+00

50.4 60.9 F 10.5  
50.4

+35

65.1 65.7 F 0.6  
5.1

+29.66

52.0 62.1 F 10.1  
52.0

+70 - ?

65.8 67.0 F 1.2  
5.8

+59.32

55.6 63.1 F 7.5  
55.6

W. Side - 0+00 = N.L. Nat.

+89.55'

59.5 63.9 F 4.4  
4.4

0+00

+119.55'

63.1 64.7 F 1.6  
3.1

+40

56.0 57.6 F 1.6  
6.0

+49.55'  
3.3 2.2

64.3 65.5 F 1.2  
4.3

+80

57.1 58.1 F 1.0  
2.1

+79.77

65.3 66.4 F 1.1  
5.3

1+20

58.3 58.8 F 0.5  
8.3

2+1000

67.4 67.4 C 0.2  
7.4

+57.13

59.3 59.5 F 0.2  
9.3

+20 = Meet. cb.

67.45 67.47

+97.13

59.4 59.8  
9.4

To W. S.L. Logan

59.4 60.0 F 0.6  
9.4



cb. Stakes - W. Side 4<sup>th</sup> Gamma - S. to line. curb Stakes - Nat + 4<sup>th</sup>.

27

S.W. Return - Gamma

End. of Ret.	73.67	73.55 <sup>67</sup>	C 0.12	S.W. Return			
1/3	71.88	73.00 1.88	F 1.12	10' W. of P.C.	55.83	56.43 5.83	F 0.60
2/3	70.87	72.36 0.87	F 1.49	P.C.	55.83	56.70 5.83	F 0.87
P.C. = 0+00	70.20	71.81 0.20	F 1.61	1/2	55.97	57.00 5.97	F 1.03
0+35	68.24	69.69 8.24	F 1.45	W. end of Inlet.		57.31	
+70	66.38	67.57 6.38	F 1.19				
1+05	64.67	65.45 <sup>5</sup> 4.67	F 0.78				
+40	62.31	63.33 2.31	F 1.02				
+75	60.33	61.21 0.33	F 0.88				
2+10	58.58	59.09 8.58	F 0.51				
2+28 end = Meet cb.	58.03	58.00					



Curb Stakes - E. Side 4<sup>th</sup> - Nat. to Logan

0+00 = N.L. Nat. Prod.

57.41

4

61.79

61.80  
79

F 0.01

+18 = opp. P.C.

57.64

57.45<sup>64</sup>

C 0.19

5

63.15

63.10<sup>15</sup>

C 0.05

+40

57.86

57.58<sup>86</sup>

C 0.28

6 = F.C.  
= 0+00

64.08

64.50<sup>08</sup>

F 0.42

+60

57.99

57.78<sup>99</sup>

C 0.21

+35.2

65.11

65.73<sup>11</sup>

F 0.62

+80

57.65

58.05<sup>7.65</sup>

F 0.40

= 0+70.48' end.

66.28

66.97<sup>28</sup>

F 0.69

1+04.05'

58.27

58.48<sup>27</sup>

F 0.21

+48.10 = P.C.

58.56

58.92<sup>56</sup>

F 0.36

Curve in 6 parts

1

59.20

59.40<sup>20</sup>

F 0.20

2

60.13

59.90<sup>0.13</sup>

C 0.23

3

60.71

60.70<sup>71</sup>

C 0.01



Curb Stakes - W. side 43rd - Nat. to Logan

cb. Stakes - N. Side Logan -

29

N.L. Nat. = 0+00

+18 = P.C.

out.

1#00 = Beg. cb.

57.63 58.38  
7.63 F 0.75

+20

57.96 58.81  
7.96 F 0.85

+37.13

58.42 59.11  
8.42 F 0.69

+57.13

59.07 59.45  
107 F 0.38

+77.13

59.40 59.65  
40 F 0.25

+97.13

59.46 59.80  
46 F 0.34

2+12.8 = P.C.

59.86 59.95  
80 F 0.09

end at S.L.  
Logan

59.19 59.97  
19 F 0.78

W. end cb.

59.10 60.90  
9.10 F 1.80

1/2

61.31 61.50  
1.31 F 0.19

P.R.C.

61.81 62.10  
1.81 F 0.29

1/2

62.38 62.58  
2.38 F 0.20

= 0+00

E. end cb.

62.86 63.07  
2.86 F 0.21

0+30.23

63.77 63.90  
2.77 F 0.13

+60.23

64.59 64.72  
59 F 0.13

+90.23

65.59 65.54  
59 C 0.05

1+20.45

66.11 66.36  
11 F 0.25

+60.67

67.06 67.19  
19 F 0.13

= end cb.

67.44 67.47



Sewer Stakes - 38<sup>th</sup> + 2"

Plan 3861-B 11-29-49 - 7.0

W.O. 20009

B.M. - S.E.B.P. - 38<sup>th</sup> + Alpha 11.06w.L. 38<sup>th</sup>0+00 = end =  
5' S.

36.82 32.20 C 4.62

+30 = E

37.19 31.99 C 5.20

INDEXED

+65

SEP 7 1950

36.40 31.74 C 4.66

1+00 = M.H.

34.80 31.50 C 3.30

Join old pipe about 3' East

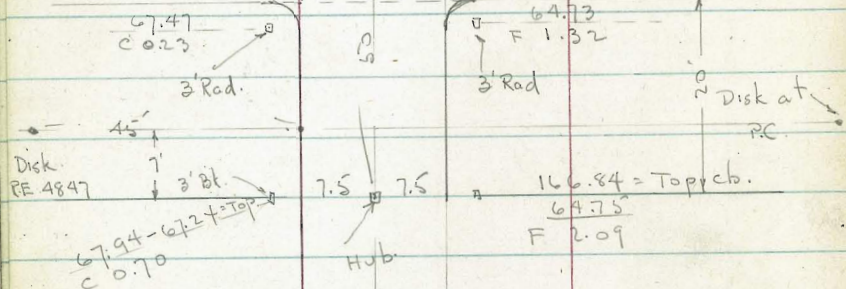
F.L. =

31.32



Niagara

To Jenico

Aye

To Catalina

 Stakes for New Returns at Nly end  
 of 15' Alley in Catalina Terrace.

Book 1783 - P. 74 - Plan - 3863-B.

# 4151

12-30-49

W.O. 20006

7.0

B.M. 157.52 = N.E. B.P. - Catalina + Nanragansett.

INDEXED

 MK.  
 SEP 11 1950



Stakes for City Const. of 30" Conc.  
 Culvert - 28<sup>th</sup> + J. Sec B. 2044 P. 6  
 for Prel. Notes.  
 stakes 10' Rt.

0+00 = Conn. to 30" Pipe	84.07	84.07	
0+32.85	88.00	84.82	C 3.18
0+65.70 = B.C.	88.39	85.57	C 2.82
+93.82 =	88.69	86.21	C 2.48
1+21.94 = E.C.	88.89	86.86	C 2.03
1+44 = end.	87.85	87.37	C 0.48

INDEXED

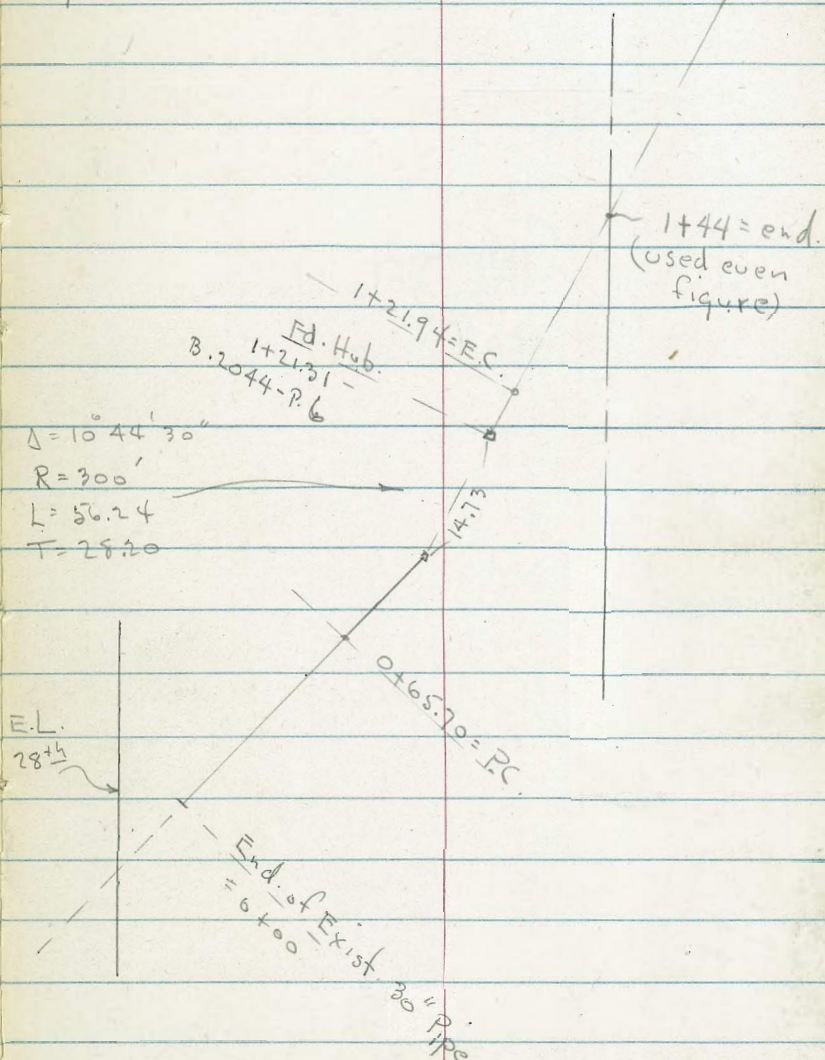
SEP 11 1950

W.O. 26588

1-23-50

7.0

End. 30" Pipe 32  
 3+23.60





INDEXED  
MK  
SEP 12 1950

Stakes for Sewer on Rogers St. -  
from San Elijo to San Fernando  
Plan - 7848-L - staked to Plan.  
W.O. 62171 1-25-50 - 7.0.

M.H.  
Sta. 0+00 = Exist.  
stakes 6 ft.

INDEXED  
MK  
SEP 11 1950

	147.39		
+26	$\frac{12.90}{56.20}$	$\frac{6.20}{50.33}$	C 5.87
+60.17	$\frac{11.74}{56.76}$	$\frac{6.76}{54.19}$	C 2.57
+94.34	$\frac{7.36}{61.14}$	$\frac{61.14}{59.05}$	C 3.09
1+28.5	$\frac{2.10}{65.40}$	$\frac{65.40}{61.90}$	C 3.50
+48.5 = Anchor	$\frac{11.60}{69.18}$	$\frac{69.18}{65.11}$	C 4.07
+68.5	$\frac{19.05}{73.48}$	$\frac{3.48}{70.18}$	C 3.30
+98.5 - Anchor	$\frac{10.28}{82.25}$	$\frac{82.25}{79.18}$	C 3.07

2+28.5	$\frac{1.85}{90.68}$	$\frac{90.68}{88.18}$	C 2.50
+48.5 - Anchor	$\frac{8.23}{96.59}$	$\frac{6.59}{92.73}$	C 3.86
+68.5	$\frac{3.63}{01.19}$	$\frac{01.19}{94.38}$	C 6.81
3+08.5	$\frac{3.90}{05.06}$	$\frac{05.06}{94.78}$	C 10.28
+48.5 = M.H. 1	$\frac{4.64}{04.32}$	$\frac{04.32}{95.18}$	C 9.14
+89.83	$\frac{5.45}{03.51}$	$\frac{03.51}{95.59}$	C 7.92
4+21.16	$\frac{5.71}{03.25}$	$\frac{03.25}{96.00}$	C 7.25
+72.5 = Plug	$\frac{5.97}{02.99}$	$\frac{02.99}{196.42}$	C 6.57

179.58 = Nail in Pole - B-1846-P.41

$\frac{120}{180.78}$   
 $\frac{12.73}{168.05}$   
 $\frac{0.45}{168.50}$

$\frac{12.93}{55.57}$



Stake St. Drain - Hancock + Coutts

Plan - 7816-L - W.O. 20581  
7.0. - 1-27-50

1+35'	10.50	10.50	4.85	C 5.65
+70	9.96	9.96	4.55	C 5.41

staked as per plan + Book 1846 - P. 21 + 38

B.M. - N.E. 7' Mon.

12.69

09.34  
2 + 11.54 2' Back  
F.L. Box

9.99	9.99	4.22	C 5.77
		4.92	C 5.07

Coutts. = 0+00

End of 18" Pipe in

9.98	9.98	7.36	C 2.62
------	------	------	--------

+45'

10.87	10.87	3.92	C 6.95
-------	-------	------	--------

INDEXED

SEP 11 1950

0+30

11.76	11.76	6.68	C 5.08
-------	-------	------	--------

+80

10.73	10.73	3.62	C 7.11
-------	-------	------	--------

= Top cb.  
10' A-2

9.52	10.24	F 0.72	
------	-------	--------	--

0+60 = 0+00 ahead =  $\frac{1}{2}$  of Inlet

9.52	9.52	6.00	C 3.52
------	------	------	--------

3+15'

10.66	10.66	3.32	C 7.34
-------	-------	------	--------

2 stakes - 8 + 16 - 90° to Coutts.  
 $\frac{1}{2}$  of Inlet.

0+34.5 = P.C.  
22.5 Rad.

9.80	9.80	5.71	C 4.09
------	------	------	--------

+50

10.45	10.45	3.02	C 7.43
-------	-------	------	--------

0+69.84 = E.C

10.23	10.23	5.41	C 4.82
-------	-------	------	--------

+85'

10.18	10.18	2.72	C 7.46
-------	-------	------	--------

0 + 71.34 =  $\frac{1}{2}$  C.L.

10.23	10.23	5.39	C 4.84
-------	-------	------	--------

8' B.  
4 + 15.46 = end.

9.98	9.98	2.47	C 7.51
------	------	------	--------

1+00

10.26	10.26	5.15	C 5.11
-------	-------	------	--------

2 + 09.34  
Top of Grate

9.99	9.99	9.91	C 0.08
------	------	------	--------



Stakes for pave - in Alley Blk. 138  
 Univ. Hts. - Plan - 7632-L

35

INDEXED

B.M.

SEP 11 1950

3-9-50 - 7.0.

Vermont +  
Lincoln

292.84 - SEBP

N. side  
Grade

292.56

S. side  
Grade

292.67

0+00 = F.L. Vermont.

+20	Cross - .43 B	95.16	<sup>5.16</sup> 93.46	C 1.70	2' B.	93.89	<sup>89</sup> 93.46	C 0.43
+40	" .50 B	95.62	<sup>5.62</sup> 94.03	C 1.59	2' B.	94.30	<sup>30</sup> 94.03	C 0.27
+60	- 2' B.	95.35	<sup>5.35</sup> 94.46	C 0.89	Cross - 0.80 B	95.50	<sup>5.50</sup> 94.46	C 1.04
+80	- 2' B	95.27	<sup>5.27</sup> 94.75	C 0.52	" 0.10 B	95.92	<sup>5.92</sup> 94.75	C 1.17
38								
1+18	- 2' B.	95.85	<sup>85</sup> 95.19	C 0.66	2' B.	95.30	<sup>30</sup> 95.19	C 0.11
+56	- 2' B	96.11	<sup>6.11</sup> 95.63	C 0.48	1' B	96.26	<sup>6.26</sup> 95.63	C 0.63
+94	- Cross - .50 in	96.65	<sup>65</sup> 96.07	C 0.58	1' B	96.62	<sup>6.62</sup> 96.07	C 0.55
2+32	- 2' B.	97.11	<sup>7.11</sup> 96.51	C 0.60	1' B	96.83	<sup>6.83</sup> 96.51	C 0.32



N.

S.

36

2+70 - Nail - 54 B.	97.34	<sup>7.34</sup> 96.95	C0.39	1' B.	97.52	<sup>7.52</sup> 96.95	C0.57
+90 - 2' B.	97.32	<sup>32</sup> 97.12	C0.20 C0.14	N. - 0.90 B.	98.04	<sup>8.04</sup> 97.18	C0.86 C0.92
3+10 - N. 0.79' B.	97.89	<sup>7.89</sup> 97.22	C0.67 C0.39	N. - 0.23 B.	98.27	<sup>8.27</sup> 97.50	C0.77 <del>C1.05</del>
+30 - .95 B.	97.72	<sup>7.72</sup> 97.06	C0.66 C0.22	N. - 0.102 B.	98.49	<sup>8.49</sup> 97.50	C0.79 <del>C1.43</del>
+50 - 1.10 B.	97.53	<sup>7.53</sup> 96.64	C0.89 C0.39	2' B.	97.74	<sup>7.74</sup> 97.14	C0.60 <del>C1.10</del>
+70 - 3' B.	96.73	<sup>6.73</sup> 96.02	C0.71 C0.31	2' B.	97.50	<sup>7.50</sup> 96.42	C1.08 <del>C1.48</del>
+90 - 4' B.	96.39	<sup>6.39</sup> 95.03	C1.36 <del>C1.07</del>	2' B.	97.15	<sup>7.15</sup> 95.32	C1.83 C2.12
4+10 - 2' B.	95.85	93.86	C2.00	2' B.	96.95	93.86	C3.09
		93.17			93.53	93.55	



Tenatauc Stakes on N. side of  
Keating - W. of Linwood

Plan - 7861-L  
 W.O. 21158

2-10-50  
 7.0.

① = Back of cb. = 10.33 out from Prop.

② = Back of walk = 7 " " "

③ = Top of cut  $\frac{3}{4}$ :1 Slope from ①

④ = " " " " " " " " ②

INDEXED

SEP 11 1950

Grade-Top cb

		①	②	③	④
0+00 = W.L. Linwood	33.50	35.15 $\frac{3.50}{3.50}$ C 1.65	36.52 $\frac{3.50}{3.50}$ C 3.02	35.2 = C 1.7 $\frac{3.5}{1.2}$	37.8 $\frac{3.5}{4.0}$ C 4.3 $\frac{3.2}{3.2}$
+50	35.18	40.3 $\frac{5.2}{5.2}$ C 5.1	42.4 $\frac{5.2}{5.2}$ C 7.2	43.1 $\frac{5.2}{6}$ C 7.9	46.2 $\frac{5.2}{11.0}$ C 11.0 $\frac{8.2}{8.2}$
+90	35.95	41.25 $\frac{5.95}{5.95}$ C 5.30	45.1 $\frac{36.0}{36.0}$ C 9.1	47.1 $\frac{8.2}{8.2}$ C 11.0	48.2 $\frac{9.2}{9.2}$ C 12.2
1+30	35.40	43.6 $\frac{5.4}{5.4}$ C 8.2	44.5 $\frac{5.4}{5.4}$ C 9.1	45.2 $\frac{7.4}{7.4}$ C 9.8	45.2 $\frac{7.4}{7.4}$ C 9.8
1+50	34.80	42.8 $\frac{4.8}{4.8}$ C 8.0	43.3 $\frac{4.8}{4.8}$ C 8.5	43.3 $\frac{6.4}{6.4}$ C 8.5	43.7 $\frac{6.7}{6.7}$ C 8.9



Sewer Stakes - Conde + Pine  
for City Crew.

3-13-50 - 7.0.

B.M. 245.94 = NE. 7 ct. Trista + Pine  
Set B.M. 240.47 =  $\square$  in  $\&$  of Ret. S.W. Cor. Conde + Pine

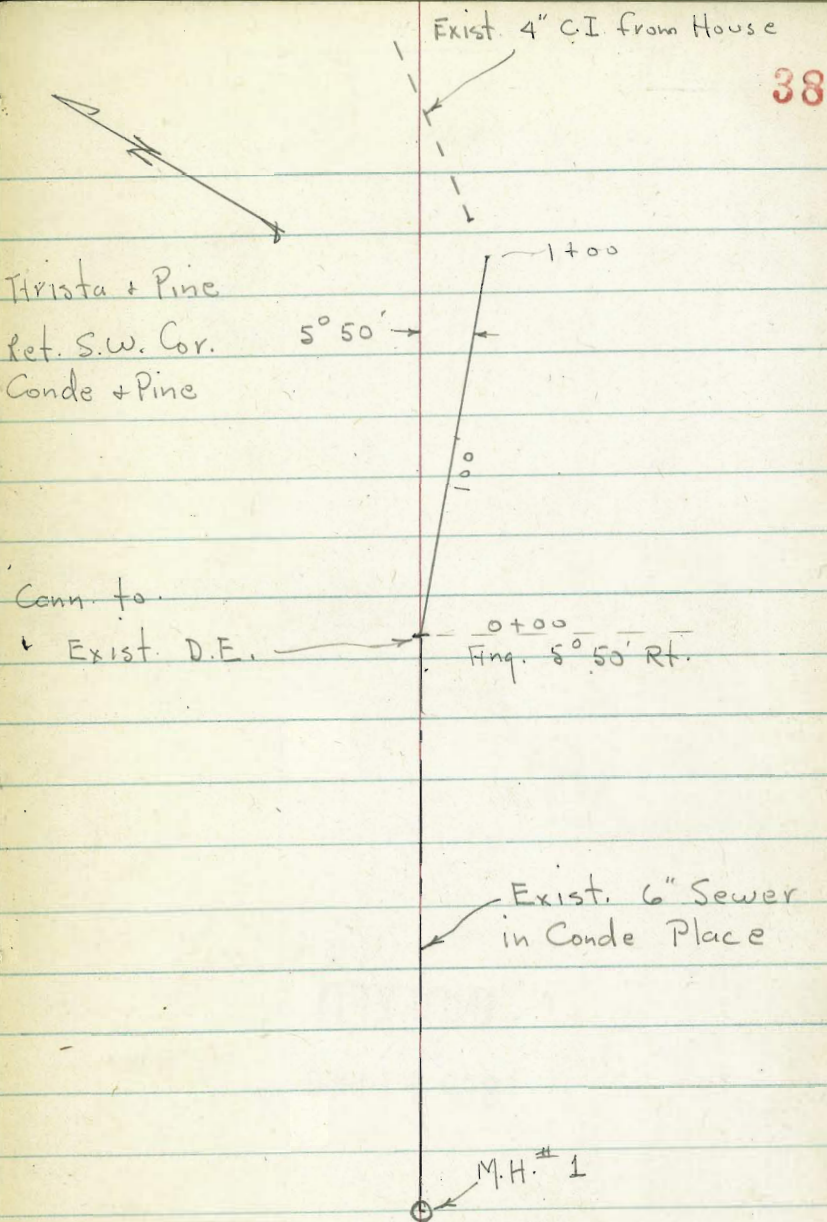
0+00 = D.E. 236.84 <sup>6.84</sup> 231.24 c 5.60

+50 39.42 <sup>9.42</sup> 34.59 c 4.83

0+85 = 16" Main Top 36.58 36.94

0+90 = Tel. Cond. Top 36.95 37.28

1+00 = end 43.41 <sup>43.41</sup> 37.94 c 5.47





Top. c.b. & w. inlet - Los Angeles P.L. = 192.27  
B.M.

0+00	-10' B.	92.45	<sup>92.45</sup> 183.50	C 8.95
+28		89.64	<sup>96.4</sup> 81.30	C 8.34
+56 = P.C.		86.97	<sup>86.97</sup> 79.10	C 7.87
+63.85 = E		86.20	<sup>96.20</sup> 78.48	C 7.72
+71.70 = E.C.		85.18	77.86	C 7.32
+87.70 = end.		80.16	<sup>80.16</sup> 76.60	C 3.56

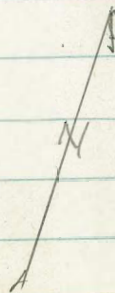
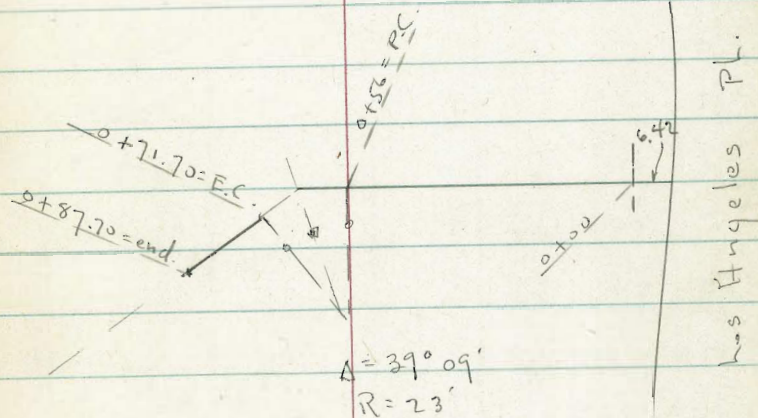
INDEXED  
 MK.  
 SEP 11 1950

Stakes for Culvert - Block 10  
Valencia Park - Plan 7034-L

39

3-27-50 - 7.0.

INDEXED  
 MK.  
 SEP 12 1950





curb cuts + Pavc Stakes - Hayes - Vermont  
to Johnson

40

	N. Side = Gut.	±	S. = Gut.
E.L. Vermont = 0 +00	291.68	92.34	91.45
+25'	91.76	92.23	91.60
+50'	91.88	92.36	91.75
+75'	92.00	92.50	91.90
1 +00	92.12	92.63	92.05
+25'	92.24	92.77	92.20
+50.84	92.36	92.90	92.34
+70.84 = w.L. to N.	92.46	92.92	92.38
+90.84	92.39	92.74	92.25
2 +26.45'		92.27	91.87
+62.06			91.49

3688 E

Note: these are profile grades  
Set stakes 0.10' lower.



curb. Stakes - Hayes - Vermont to 10<sup>th</sup>

Nail in Pole 276.61

41

3' Back S. Side

N. Side

0+00 = W.L. Vermont

91.00 290.90

90.95

90.90

+30

88.14

89.23  
8.14

F 1.09

89.07

89.65  
1.07

F 0.58

+40

INDEXED  
Y.K.  
SEP 11 1950

87.52

88.67  
7.52

F 1.15

88.43

89.21  
8.43

F 0.78

+50

87.04

88.09  
7.04

F 1.05

87.49

88.72  
7.49

F 1.23

+60

86.47

87.52  
6.47

F 1.05

87.05

88.20  
7.05

F 1.15

+70

86.07

86.93  
6.07

F 0.86

86.13

87.63  
6.13

F 1.50

-5-38'

1+08

84.17

84.69  
4.17

F 0.52

84.23

85.39  
4.23

F 1.16

+46

81.74

82.44  
1.74

F 0.70

82.32

83.14  
2.32

F 0.82

+84

79.76

80.19  
79.76

F 0.43

80.32

80.89  
32

F 0.57



		S.			N.	12	
2+22	77.86	77.94 7.86	F 0.08		77.72	78.64 7.72	F 0.92
2+60	75.09	75.69 5.09	F 0.60		75.52	76.39 5.52	F 0.87
+80	74.38	74.68 .38	F 0.30		74.72	75.38 4.72	F 0.66
3-	73.44	74.03 3.44	F 0.59		73.52	74.73 3.52	F 1.21
+20-5'B.	73.02	73.74 3.02	F 0.72	5'B.	74.61	4.66 74.44	C 0.17
+40	73.56	73.80 3.56	F 0.24		74.15	74.50 4.15	F 0.35
+60	74.24	4.24 74.04	C 0.20		74.35	74.74 4.35	F 0.39
5-36.17							
+96.17	74.44	74.47 .44	F 0.03		74.50	75.17 4.50	F 0.67
4+32.34	74.53	74.90 .53	F 0.37		74.87	75.60 4.87	F 0.73
+68.51	74.75	75.33 4.75	F 0.58		75.23	76.03 5.23	F 0.80



S

N.

43

5+04.68

75.44

75.76  
F 0.32  
.44

75.88

76.46  
5.88

F 0.58

P.C. 4' Rad.

76.70

76.85  
70

F 0.15

+40.85 = E.L. Alley  
41.15

75.74

76.20  
F 0.46  
5.74

76.90

\* W. side 2' B.  
on N.L.

77.33

77.36  
33

F 0.03

+51.15 - W.L. Alley

75.91

76.36  
F 0.45  
5.91

77.06

P.C. 4' Rad.

76.73

77.12  
6.73

F 0.39

34.9-3

cb.

+85.75 =

(7.53)

77.60

+86.07

76.56

76.93  
F 0.37  
6.56

6+21

77.52

77.52  
77.50  
C 0.02

+51.1

8.02

78.00

+55.90

78.07

+75.90 = E.L. 10<sup>th</sup>  
N.

75.30 = S



Culvert on Hayes.

INDEXED  
M.K.  
SEP 11 1950

44

U. Side.		Grade	
5' Back at E. of Inlet.			
I.E. of Box:	74.25	74.25 269.90	c 4.35

S. side		I.E. Box	
5' Back - E. end		67.90	
5' Back - W. end.	73.73	73.73 67.90	c 5.83

1.67 Back of cb = 0.00		67.90	
8' E.		67.80	
+32	67.90	57.80	c 10.00

+64 = end.	54.31	54.31 47.69	c 6.62
------------	-------	----------------	--------



Water Line Stakes - on Winona St.  
 S. of Univ. - Plan - 7740 - L  
 4-13-50 - 7.0 W.O. 31215

B.M. =  $\square$  on N.E. Cor. Steps - on W. - 2+20

332.59

45

6+40	15.4	<sup>15.4</sup> 9.0	C 6.4
+80.93 =	11.0	<sup>1.0</sup> 30 <sup>1.0</sup> 5.9	C 5.1

Conn.

0+00 = opp. S.W. Prop. Cor. Univ. + Winona

Conn.

+40	30.6	<sup>30.6</sup> 326.7	C 3.9	cb. Grade
+80	32.5	<sup>2.5</sup> 27.8	C 4.7	F.H. - 5' Back on E. side
1+20	33.4	<sup>3.4</sup> 28.6	C 4.8	5'-S. of S.L. 30.0 29.76 C 0.24
+60	33.2	<sup>3.2</sup> 28.6	C 4.6	
2+00	32.5	<sup>2.5</sup> 28.0	C 4.5	4+05 = F.H.
+40	31.8	<sup>1.8</sup> 27.3	C 4.5	5' Back 29.23 <sup>9.23</sup> 27.64 C 1.59
+80	31.1	<sup>1.1</sup> 26.5	C 4.6	
3+20	30.2	<sup>0.2</sup> 25.8	C 4.4	
+60		24.8		
4+00	28.4	<sup>8.4</sup> 23.5	C 4.9	
+40	27.0	<sup>7.0</sup> 22.1	C 4.9	
+80	27.2	<sup>7.2</sup> 20.2	C 7.0	
5+20	24.8	<sup>4.8</sup> 17.8	C 7.0	
+60	22.1	<sup>2.1</sup> 15.0	C 7.1	
6+00	19.4	<sup>9.4</sup> 12.0	C 7.4	

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 MK.  
 SEP 11 1950



Rough grades - Winona

332.59 = D.M.

46

5' Back

E. Side

W. side

0+00

29.68<sup>cb.</sup>

28.66<sup>cb.</sup>

+40

31.2 31.0<sup>2</sup> C 0.2

27.2 30.0<sup>2</sup> F 2.8

+80

32.3 32.1<sup>2.3</sup> C 0.2

28.1 31.1<sup>28.1</sup> F 3.0

1+20

33.6 32.9<sup>3.6</sup> C 0.7

33.9 31.9<sup>3.9</sup> C 2.0

+60

33.2 32.9<sup>3.2</sup> C 0.3

33.1 31.9<sup>3.1</sup> C 1.2

2+00

32.7 32.3<sup>2.7</sup> C 0.4

32.2 31.3<sup>2.2</sup> C 0.9

+40

32.6 31.6<sup>2.6</sup> C 1.0

31.2 30.6<sup>1.2</sup> C 0.6

+80

31.6 30.9<sup>1.6</sup> C 0.7

30.5 29.9<sup>30.5</sup> C 0.6

3+20

31.1 30.1<sup>1.1</sup> C 1.0

29.7 29.1<sup>9.7</sup> C 0.6



	E. Side					w. side		47
3+60		30.3	<sup>0.3</sup> 29.1	C 1.2	27.5	28.1 7.5		F 0.6
4+00	C 2.2	30.2	<del>27.8</del> 28.0	<del>C 2.4</del>	Top wall on line 27.9	27.9 26.8		C 1.1
+40	C 1.8	28.5	<del>26.4</del> 26.7	C 2.1	F 2.6	23.1	25.7 25.4	F 2.3
+80	C 2.7	27.8	<del>24.5</del> 25.1	<del>C 3.3</del>	F 3.1	21.1	24.2 23.5	F 2.4
5+20	C 3.1	26.3	<del>22.1</del> 23.2	C 4.2	F 2.8	19.4	22.2 21.1	F 1.7
+60	C 4.5	25.1	<del>4.2</del> 20.6	<del>C 5.9</del>	F 3.3	16.3	19.6 18.2	F 1.9
6+00	C 6.0	23.6	<del>16.2</del> 17.6	C 7.4	F 4.3	12.3	16.6 15.2	F 2.9
+40	C 4.9	18.9	<del>12.3</del> 14.0	<del>C 5.6</del>	F 5.1	07.9	13.0 12.3	F 4.4
+80.93 = end	C 5.1	15.8	<del>10.2</del> 10.4	<del>C 5.3</del>	F 5.1	04.3	09.4 09.2	F 4.9



Rough Grades - Reed - Lamont  
to Olney Plan 7796-8-L

W.O. 31630

5-4-50 - 7.0

	5' Back	Grade	
E.L. Lamont = 0+00		S. Side	
		40.00	
+ 40		37.7	
+ 80		35.5	
INDEXED M.K. SEP 11 1950	34.6	33.2	C 1.4
+ 60	30.6	31.0	F 0.4
2+00	29.1	29.4	F 0.3
+ 50	27.4	28.5	F 1.1
3 ~	25.0	28.1	F 3.1
+ 50	25.0	27.8	F 2.8
4 ~	26.7	27.5	F 0.8
+ 50	29.0	27.2	C 0.8
5 ~ = W.L. Morrell	29.3	26.9	C 2.4
0+00 = E.L.	28.9	26.3	C 2.6
+ 40	27.7	25.2	C 2.5
+ 80	24.6	23.4	C 1.2

BM = N.W. Morrell + Reed = 32.02  
Top - E. Cor. of Bottom Step

48

SE 7' ct. - Lamont = 40.37

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SEP 12 1950

5' Back	N. Side	
	39.50	
38.1	37.5	C 0.6
34.8	35.5	F 0.7
33.1	33.4	F 0.3
30.8	31.5	F 0.7
29.5	30.1	F 0.6
28.6	29.2	F 0.6
28.4	28.8	F 0.4
30.8	28.5	C 2.3
30.6	28.2	C 2.4
31.3	27.9	C 3.4
30.7	27.7	C 3.0
30.5	27.1	C 3.4
29.2	26.0	C 3.2
26.4	24.2	C 2.2



Noyes - NE. Cor. □ in walk

B.M. 20.76

S. Side

N. Side

49

INDEVENT  
SEP 12 1950

1+20 = T.P.	22.07	<sup>22.1</sup> 21.0	C 1.1 ✓
+60	18.3	18. <sup>3</sup> 2	C 0.1
2~	15.5	15.8	F 0.3
+40	15.8	14. <sup>8</sup> 3	C 1.5
+80	11.9	13. <sup>9</sup> 7	F 1.8
3+20	12.4	13. <sup>4</sup> 5	F 1.1
+60	11.9	13. <sup>9</sup> 3	F 1.4
4~	11.8	13. <sup>8</sup> 0	F 1.2
+50	10.7	12. <sup>7</sup> 8	F 2.1
5- = W.L. Noyes	9.1	12. <sup>1</sup> 5	F 3.4
0+00 = E.L. Noyes	12.5	13. <sup>5</sup> 3	F 0.8
+40	14.6	15. <sup>6</sup> 0	F 0.4
+80	17.9	16. <sup>9</sup> 8	C 1.1
1+20	19.8	18. <sup>8</sup> 1	C 1.7
+60	19.9	19. <sup>9</sup> 1	C 0.8
2~	20.0	19. <sup>0</sup> 7	C 0.3
+40	20.0	19. <sup>0</sup> 8	C 0.2
+80	19.4	19. <sup>4</sup> 6	F 0.2
3+20	19.2	19. <sup>2</sup> 0	C 0.2

23.6	<sup>3.6</sup> 21.7	C 1.9
22.0	<sup>22.0</sup> 19.0	C 3.0 ✓
17.6	<sup>17.6</sup> 16.6	C 1.0
14.9	<sup>14.9</sup> 15.1	F 0.2
14.2	<sup>14.2</sup> 14.4	F 0.2
13.9	<sup>13.9</sup> 14.2	F 0.3
13.2	<sup>13.2</sup> 14.0	F 0.8
12.3	<sup>12.3</sup> 13.5	F 1.5
12.3	<sup>12.3</sup> 13.5	F 1.2
14.9	<sup>14.9</sup> 13.3	C 1.6
19.1	<sup>19.1</sup> 14.2	C 4.9
20.0	<sup>20.0</sup> 15.8	C 4.2
21.6	<sup>21.6</sup> 17.5	C 4.1
23.6	<sup>23.6</sup> 18.9	C 4.7
24.6	<sup>24.6</sup> 19.9	C 4.7
23.8	<sup>23.8</sup> 20.4	C 3.4
23.0	<sup>23.0</sup> 20.6	C 2.4
23.4	<sup>23.4</sup> 20.3	C 3.1
23.1	<sup>23.1</sup> 19.7	C 3.4



S. Side  
Grade

3+60	19.2	<sup>19.2</sup> 18.3	C 0.9
4+00	19.2	<sup>19.2</sup> 17.5	C 1.7
+40	18.0	<sup>18.0</sup> 16.5	C 1.5
465	17.8	<sup>17.8</sup> 15.9	C 1.9
5~ = W.L. Olney	17.4	<sup>17.4</sup> 15.0	C 2.4

Sw. Olney - W. Top  
Bottom step. 17.86 = B.M.

N. Side

50

22.2	<sup>22.2</sup> 19.0	C 3.2
21.9	<sup>21.9</sup> 18.2	C 3.7
21.3	<sup>21.3</sup> 17.2	C 4.1
20.6	<sup>20.6</sup> 16.5	C 4.1
19.3	<sup>19.3</sup> 15.7	C 3.6



5' off.

0+00 - 3' D. - E of Box - 70.34 <sup>70.34</sup> 65.20 c 5.14

0+33.5 69.50 <sup>9.50</sup> 64.85 c 4.65

0+67 = Meet Pipe 70.28 <sup>0.28</sup> 64.50 c 5.78

Capistrano + Quimby - S.W. Cor.

27 w. on Capist. 88.89

P.C. 89.86 <sup>86</sup> 89.65 c 0.21

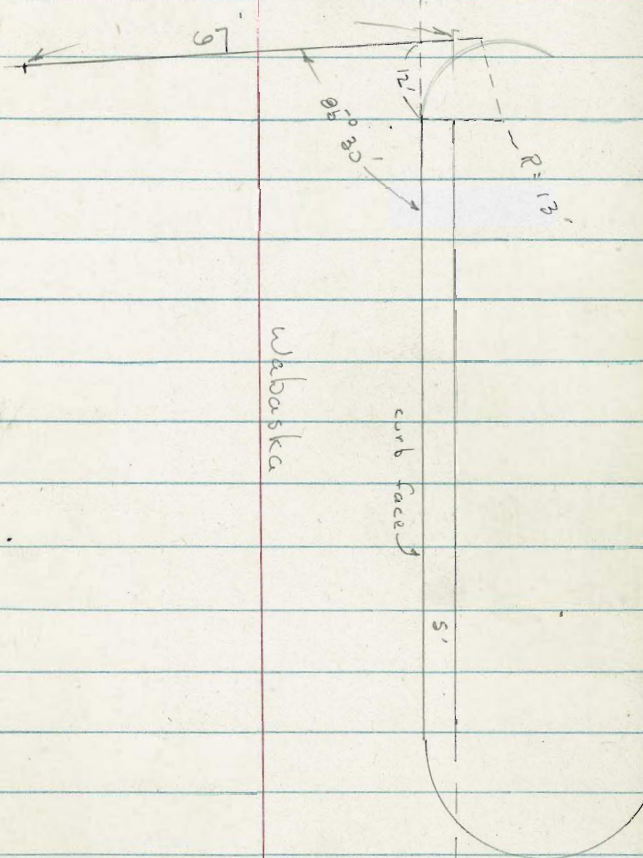
1/4 90.04 <sup>04</sup> 89.95 c 0.09

1/2 90.66 <sup>66</sup> 90.25 c 0.41

3/4 90.65 <sup>65</sup> 90.55 c 0.10

E.C. 90.99 <sup>99</sup> 90.87 c 0.12

28's on Quimby 91.49





B.M. =  $\square$  -  $\oplus$  S.W. Ref. Fresno + La Jolla Shores.

= 22.65

52

Stake Sewer - La Jolla Shores Dr.

+ P.L. 1280 - Plan 7923-L

2+24

<sup>25.44</sup>  
25.44 14.62

10.82

w.o. 62175

5-12-50 - 7.0.

0+00 = M.H. 1

<sup>6+12</sup>

20.35

<sup>20.35</sup>

13.50

6.85

6'5"

+28

INDEXED  
MK.

SEP 12 1950

<sup>21.42</sup>  
20.35

21.42

13.64

7.78

+56

20.78

<sup>20.78</sup>

13.78

7.00

+84

20.71

<sup>20.71</sup>

13.92

6.79

+112

21.42

<sup>21.42</sup>

14.06

7.36

+140

22.11

<sup>22.11</sup>

14.20

7.91

+168

22.97

<sup>22.97</sup>

14.34

8.63

+196

24.10

<sup>24.10</sup>

14.48

9.62



Water Stakes - Reed - Lamont to  
Morrell 5-16-50 - 70.

stakes. 2.5' N.

0+00 = E.L. Lamont = Conn.

+40	36.5	<sup>6.5</sup> 34.0	C 2.5
+80	34.4	<sup>4.4</sup> 31.8	C 2.6
1+20	32.1	<sup>2.1</sup> 29.6	C 2.5
+60	30.1	<sup>0.1</sup> 27.5	C 2.6
2+00	28.9	<sup>8.9</sup> 26.0	C 2.9
+50	27.8	<sup>7.8</sup> 25.0	C 2.8
3~	27.3	<sup>7.3</sup> 24.7	C 2.6
+50	27.0	<sup>7.0</sup> 24.4	C 2.6
4~	27.2	<sup>7.2</sup> 24.1	C 3.1
+50	26.9	<sup>6.9</sup> 23.8	C 3.1
5 = W.L. Morrell	26.7	<sup>6.7</sup> 23.3	C 3.4

INDEXED

JMK.

SEP 11 1950

± Grades - Noyes - Reed. S.

53

0+00 = S.L. Reed

+40	9.0
+80	6.7
1+20	5.1
+60	4.3



Rough Grades - Oliver - Ingraham to Jewell  
 w.o. 31033 - Plan - 7699-L - 5-16-50  
 7.0.

47.99 =  $\pm$  ct Ingraham + Oliver

54

S. Side  
 Grade

N. Side

0+00 - E.L. Ingraham 48.5 <sup>8.5</sup> 47.9 C 0.6

INDEXED

SEP 12 1950

48.8 <sup>48.8</sup> 47.7 C 1.1

+25 49.2 <sup>9.2</sup> 48.0 C 1.2

49.2 <sup>9.2</sup> 48.0 C 1.2

+50 48.9 <sup>8.9</sup> 48.1 C 0.8

INDEXED

SEP 11 1950

49.2 <sup>9.2</sup> 48.1 C 1.1

1- 48.4 <sup>8.4</sup> 48.2 C 0.2

49.0 <sup>9.0</sup> 48.2 C 0.8

+50 48.2 <sup>8.2</sup> 48.4 F 0.2

49.2 <sup>9.2</sup> 48.4 C 0.8

2- 48.3 <sup>8.3</sup> 48.6 F 0.3

49.1 <sup>9.1</sup> 48.6 C 0.5

+50 48.6 <sup>8.6</sup> 48.8 F 0.2

49.2 <sup>9.2</sup> 48.8 C 0.4

3- 48.6 <sup>8.6</sup> 48.9 F 0.3

49.5 <sup>9.5</sup> 48.9 C 0.6

+40 49.0 <sup>9.0</sup> 49.1 F 0.1

50.1 <sup>50.1</sup> 49.1 C 1.0



S. Side

N. Side

3+80

49.3

49.5  
4.3

F 0.2

50.8

50.5  
49.6

C 0.9

4+20

50.2

50.5  
0.2

F 0.3

51.1

50.7

C 0.4

+68

51.1

51.9  
1.1

F 0.8

52.2

52.3  
2.2

F 0.1

5+00 = W.L. Jewell

51.97

51.99 = cb.

53.07 = cb.







Curb stakes - Oliver - Ingraham to Jewell

57

INDEXED

SEP 11 1950

s. Side-Grade

N. Side

P.C. Ingraham	47.78	47.86 <sub>78</sub>	F 0.08	47.50	47.67 <sub>53</sub>	F 0.17
10	47.94	47.90 <sup>.94</sup>	C 0.04	47.66	47.72 <sub>66</sub>	F 0.06
	48.21	47.93 <sup>8.21</sup>	C 0.28	47.99	47.85 <sup>99</sup>	C 0.14
	48.79	47.95 <sup>8.79</sup>	C 0.84	49.05	47.90 <sup>9.05</sup>	C 1.15
	48.99	47.96 <sup>8.99</sup>	C 1.03	49.39	47.91 <sup>9.39</sup>	C 1.48
= 0+25 = P.C.	48.61	47.97 <sup>8.61</sup>	C 0.64	49.63	47.97 <sup>9.63</sup>	C 1.66
+ 60	48.91	48.09 <sup>91</sup>	C 0.82	49.48	48.09 <sup>9.48</sup>	C 1.39
+ 95	48.74	48.21 <sup>74</sup>	C 0.53	48.93	48.21 <sup>93</sup>	C 0.72
1+30	48.50	48.34 <sup>50</sup>	C 0.16	48.96	48.34 <sup>96</sup>	C 0.62



S. Side

N. side

1+65	48.40	48.46 <sub>40</sub>	F 0.06	48.78	48.78 <sup>78</sup> 48.46	C 0.32
2+00	48.37	48.58 <sub>37</sub>	F 0.21	49.07	49.07 <sup>07</sup> 48.58	C 0.49
+35	48.65	48.70 <sub>65</sub>	F 0.05	48.94	48.94 <sup>94</sup> 48.70	C 0.24
+70	48.38	48.82 <sub>38</sub>	F 0.44	49.05	49.05 <sup>05</sup> 48.82	C 0.23
3+05	48.37	48.95 <sub>37</sub>	F 0.58	49.25	49.25 <sup>25</sup> 48.95	C 0.30
+40	48.82	49.07 <sub>8.82</sub>	F 0.15	49.62	49.62 <sup>62</sup> 49.07	C 0.55
+60	49.17	49.21 <sub>17</sub>	F 0.04	49.71	49.71 <sup>71</sup> 49.22	C 0.49
+80	49.41	49.49 <sub>41</sub>	F 0.08	49.79	49.79 <sup>79</sup> 49.54	C 0.25
4+00	49.67	49.90 <sub>67</sub>	F 0.23	50.33	50.33 <sup>33</sup> 50.02	C 0.31
+20	50.03	50.46 <sub>03</sub>	F 0.43	50.72	50.72 <sup>72</sup> 50.67	C 0.05



s. side

4+65

50.76 51.86 F 1.10  
0.76590 52.31 F 0.41  
1.90

+75 = P.C.

51.01 52.00 F 0.99  
1.0152.02 52.60 F 0.58  
0.02

13.25

51.40 52.05 F 0.65  
1.4052.59 52.87 F 0.28  
0.59

= Meet cb.

51.97 51.99

53.06 53.07



Stake Culvert along lot line of lot 16  
L.P. Delano Tract - Map. 1746 - See 3712-B.

W.O. 20461

5-23-50 - 70.

INDEXED

SEP 12 1950

Exist. Culvert =

Top cb.

259.00

Flow. of Box

256.34

New I.E.

59.00 2 59.00 53.72 c 5.28

5' - Rt.

0+17

59.29 9.29 53.36 c 5.93

<sup>5+10</sup>  
+34 =  $\pm$  Clean out

60.39 60.39 53.00 c 7.39

+59

59.02 59.02 46.57 12.45

+84

46.61 6.61 40.15 c 6.46

1+08 - End.

34.71 34.71 34.0 c 0.71

B.M. 286.08 - S.E. Kalmia + 29<sup>th</sup>

B.M. 259.19 = Pipe Bet. lots 17+18

60

INDEXED

SEP 12 1950



Curb Stakes - Winona — 7740-L

1 5-23-50 7.0.

332.59 - □ in step.

61

	Grade - W. Side		
		cb.	
0+00 = S.L. Univ. tow.	28.04	328.66	
+20	28.53	29.36	F 0.83
+40	29.47	29.98	F 0.51
+80	30.60	31.11	F 0.51
1 ~	31.27	31.58	F 0.31
+20	31.60	31.86	F 0.26
+40	31.78	31.97	F 0.19
+60	31.65	31.89	F 0.24
+80	31.27	31.63	F 0.36
2+20	30.72	30.93	F 0.21
+60	29.90	30.22	F 0.32
3 ~	29.17	29.51	F 0.34
+20	28.79	29.12	F 0.33
+40	28.23	28.64	F 0.41
+60	27.70	28.09	F 0.39
4 ~	26.54	27.00	F 0.46
+40	25.25	25.70	F 0.45
+80	23.92	24.10	F 0.18

INDEXED

SEP 12 1950

Grade - E. Side:

cb.		
	329.68	
29.94	29.85	C 0.09
30.87	30.47	C 0.44
30.71	30.98	F 0.27
31.86	32.11	F 0.25
32.17	32.58	F 0.41
32.32	32.86	F 0.54
32.65	32.97	F 0.32
32.27	32.89	F 0.62
32.10	32.63	F 0.53
31.54	31.93	F 0.39
30.87	31.22	F 0.35
30.20	30.51	F 0.31
29.67	30.12	F 0.45
29.25	29.64	F 0.39
28.81	29.09	F 0.28
27.80	28.00	F 0.20
26.40	26.70	F 0.30
24.95	25.10	F 0.15



W. Side

E. Side

5+00	22.85	23.20 <sub>35</sub>	F 0.35	24.49	24.20 <sub>19</sub>	F 0.01
+20	21.85	22.20 <sub>35</sub>	F 0.35	22.97	23.20 <sub>19</sub>	F 0.23
+40	20.70	20.95 <sub>70</sub>	F 0.25	21.77	21.95 <sub>17</sub>	F 0.18
+60	19.31	19.60 <sub>31</sub>	F 0.29	20.73	20.63	C 0.13
+80 - T.P.	17.79	18.20 <sub>79</sub>	F 0.41	19.09	19.20 <sub>09</sub>	F 0.11
6 ~	16.01	16.60 <sub>01</sub>	F 0.59	17.49	17.60 <sub>49</sub>	F 0.11
+20	14.35	14.90 <sub>35</sub>	F 0.55	15.80	15.90 <sub>80</sub>	F 0.10
+50	11.51	12.19 <sub>51</sub>	F 0.68	13.07	13.19 <sub>07</sub>	F 0.12
+80.93	09.41	09.40 <sub>41</sub>	C 0.01	10.39	10.40 <sub>39</sub>	F 0.02

sw. Ref. - Univ. + Winona

S.L. Univ. 27.83 28.66<sub>83</sub> F 0.83P.C. 27.73 28.47<sub>73</sub> F 0.7427.64 28.16<sub>64</sub> F 0.52

27.84 27.84 00

27.77 27.77



Stake Sewer - to Scripps inst.  
 Sec P. 56 - w.o. 20569 6-2-50  
 70

31.17 = Plug in end cb. - Paseo Grande

12.39  
 2.45  
 9.97  
 63

INDEXED

W.K.

SEP 12 1950

stakes - 12' Rt.	Grade	C.J.T.
0+00 = Exst. Mt.	11.63	
+35	30.74	18.98
+70	31.09	19.21
1+05	30.48	18.47
+40	29.69	17.56
+75	29.03	16.77
2+10	28.00	15.61
+45	27.82	15.31
+82.40 = M.H. 1	27.40	14.76
+35	26.60	13.84
+70	23.21	10.32
1+05	22.25	9.24
+34	21.69	8.57
+52	4.54	8.64
+70	9.97	7.57
+88	21.39	8.05
2+23	24.75	11.31

2+58	25.92	25.92	13.57	C 12.35
2+98.6 = M.H. 2	26.58	26.58	13.72	C 12.86
+35	27.18	27.18	13.85	C 12.33
+70	28.07	28.07	13.97	C 14.10
1+05	28.90	28.90	14.10	C 14.80
+40	29.46	29.46	14.22	C 15.24
+75	30.08	30.08	14.35	C 15.73
2+10	30.91	30.91	14.48	C 16.43
+45	31.29	31.29	14.60	C 16.69
+80	31.79	31.79	14.73	C 17.06
3+20.90 = M.H. 3	31.95	31.95	14.88	C 17.07
end - 25' ahead	32.43	32.43	14.97	C 17.46

INDEXED

M.K.

SEP 12 1950



Change Grade on W. side Dawson  
El Cajon S.

INDEXED

~~YIX~~  
SEP 12 1950

0+00 = opp. S.W. Cor.

0+02.04 = end. cb. 82.31 382.28 C 003 Exist. cb = 82.44

+25.8 80.26 80.32 F006

+60 77.00 77.51 F051

+95 74.40 74.63 F023

1+30 71.84 71.75 C009

+65 68.99 68.87 C012

2+00 65.60 65.99 F039

+50 61.57 61.87 F030



## Curb Stakes - Conde + Pine

Mon = 246.79

240.48 = 8 in cb

65

INDEXED

WJK

SEP 12 1950

0+00 = P.C.	48.22	48.50 <sub>22</sub>	F 0.28
+15	47.75	47.90 <sub>15</sub>	F 0.15
+30	46.23	46.82 <sub>23</sub>	F 0.59
+45 = P.C. 16.5 Rail.	44.83	45.30 <sub>45</sub>	F 0.47
1/2	44.00	44.45	F 0.45
2/3	43.31	43.50 <sub>31</sub>	F 0.19
E.C. = 6' from Gav.	43.31	42.75 <sub>31</sub>	C 0.56
6' from W. end Gav.	41.16	42.82 <sub>16</sub>	F 1.66
11.02 = P.R.C.	41.59	42.35 <sub>59</sub>	F 0.76
1/2	41.68	41.85 <sub>68</sub>	F 0.17
P.C. = end. cb.	✓ 241.34		



Curb. Stakes - Reed - Lamont to Morrell

INDEXED

SEP 12 1959

S. Side

N. Side

66

0+00 = E.L. Lamont	40.00		39.59	39.50	
+20	38.87		38.62	38.49 <sup>62</sup>	C 0.13
+60	36.60		36.54	36.47 <sup>54</sup>	C 0.07
1 ~ cb	34.44	34.33	33.95	34.45 <sup>45</sup>	F 0.50
+40	31.54	32.06 <sup>86</sup>	32.32	32.43 <sup>32</sup>	F 0.11
+60	30.05	31.00 <sup>89</sup>	31.26	31.49 <sup>29</sup>	F 0.23
+80	29.75	30.13 <sup>91</sup>	30.68	30.76 <sup>68</sup>	F 0.03
2 ~	29.12	29.41 <sup>29</sup>	29.84	30.07 <sup>84</sup>	F 0.23
+20	28.60	28.87 <sup>60</sup>	29.36	29.58 <sup>36</sup>	F 0.22
+40	27.80	28.50 <sup>80</sup>	28.54	29.23 <sup>54</sup>	F 0.69
+60	27.25	28.29 <sup>25</sup>	28.36	29.04 <sup>36</sup>	F 0.68
3 -	27.68	28.05 <sup>68</sup>	28.59	28.80 <sup>59</sup>	F 0.21
+40	27.63	27.81 <sup>63</sup>	28.45	28.56 <sup>45</sup>	F 0.11
+80	27.42	27.58 <sup>42</sup>	28.57	28.33 <sup>57</sup>	C 0.24
4 +20	27.50	27.34 <sup>50</sup>	28.39	28.69 <sup>39</sup>	C 0.28
+60	27.22	27.11 <sup>22</sup>	28.00	27.86 <sup>22</sup>	C 0.14
+90 = P.C.	27.03	26.93 <sup>03</sup>	27.65	27.68 <sup>03</sup>	F 0.03
around Ret.	26.64	26.85 <sup>64</sup>	27.48	27.76 <sup>48</sup>	F 0.28
	26.66	26.72 <sup>66</sup>	27.67	27.98 <sup>66</sup>	F 0.31
end: Prop.	26.73	26.50 <sup>73</sup>	28.21	28.34 <sup>73</sup>	F 0.13



Marrell to Neyes

S. Side

27.09	26.08	C 1.09	
26.21	26.23	F 0.02	
26.11	26.37	F 0.21	
26.00	26.15	F 0.15	
+20	26.04	25.87 <sup>6.04</sup>	C 0.17
+40	25.27	25.23	C 0.04
+60	24.56	24.41 <sup>5.6</sup>	C 0.15
+80	23.38	23.43 <sup>3.8</sup>	F 0.05
1 ~	22.12	22.29 <sup>1.2</sup>	F 0.17
+20	20.78	20.97 <sup>0.78</sup>	F 0.19
+60	18.39	18.19 <sup>1.9</sup>	C 0.20
+80	17.15	16.90 <sup>1.5</sup>	C 0.25
2 ~	15.85	15.83 <sup>5.85</sup>	C 0.02
+20	14.83	14.97 <sup>4.83</sup>	F 0.14
+40	14.34	14.32	C 0.02
+60	14.15	13.90 <sup>4.15</sup>	C 0.25
+80	13.58	13.68 <sup>3.58</sup>	F 0.10
3 ~	13.15	13.57 <sup>1.15</sup>	F 0.42
+40	13.18	13.35 <sup>3.18</sup>	F 0.17
+80	12.88	13.14 <sup>2.88</sup>	F 0.26
4 +20	12.62	12.92 <sup>6.2</sup>	F 0.30
+60	12.46	12.71 <sup>4.6</sup>	F 0.25
+90 = P.C.	12.57	12.55	C 0.02

INDEXED

W.K.  
SEP 12 1950

N. Side

27.35	27.80	F 0.45
26.98	27.40	F 0.42 <b>67</b>
26.93	27.10	F 0.17
26.55	26.90	F 0.35
26.19	26.62 <sup>6.19</sup>	F 0.43
25.67	25.98 <sup>6.7</sup>	F 0.31
24.86	25.16 <sup>4.86</sup>	F 0.30
24.26	24.18 <sup>4.26</sup>	C 0.08
22.86	23.04 <sup>2.86</sup>	F 0.18
21.65	21.72 <sup>1.65</sup>	F 0.07
18.62	18.94 <sup>6.2</sup>	F 0.32
17.36	17.65 <sup>7.36</sup>	F 0.29
16.25	16.58 <sup>6.25</sup>	F 0.33
15.15	15.73 <sup>5.15</sup>	F 0.57
14.30	15.07 <sup>4.30</sup>	F 0.77
14.08	14.65 <sup>4.08</sup>	F 0.57
13.56	14.43 <sup>3.56</sup>	F 0.87
13.68	14.32 <sup>3.68</sup>	F 0.64
13.04	14.10 <sup>3.04</sup>	F 1.06
13.34	13.89 <sup>3.34</sup>	F 0.55
13.32	13.67 <sup>3.32</sup>	F 0.35
13.18	13.46 <sup>3.18</sup>	F 0.28
12.89	13.30 <sup>2.89</sup>	F 0.41



S. Side

N. Side

68

12.19 12.42 F 0.23

13.18 13.34 F 0.16

12.14 12.10 C 0.04

13.19 13.48 F 0.29

end. Ret. 11.42 11.50<sub>4</sub> F 0.08

13.94 13.90 C 0.04

Noyes to Olney

end Ret. 11.83 11.97<sub>83</sub> F 0.1414.96 14.59<sup>96</sup> C 0.37

12.68 12.60 C 0.08

14.11 14.10 C 0.01

13.54 13.25<sup>54</sup> C 0.29

13.94 14.14 F 0.20

P.C. = 0 + 10 14.08 13.69<sup>4</sup> C 0.39

14.37 14.44 F 0.07

+35 14.65 14.80 F 0.15

15.55 15.55 0.0

+60 16.04 15.92<sup>04</sup> C 0.12

16.54 16.67 F 0.13

+80 16.94 16.76<sup>94</sup> C 0.18

17.60 17.51 C 0.09

1 ~ 17.82 17.49<sup>82</sup> C 0.33

18.19 18.24 F 0.05

+20 18.06 18.12 F 0.06

19.07 18.87 C 0.20

+40 18.73 18.66<sup>73</sup> C 0.07

19.52 19.41 C 0.11

+60 19.10 19.10 0.0

19.66 19.85 F 0.19

+80 19.41 19.43 F 0.02

19.81 20.18 F 0.37

2 - 19.85 19.66<sup>85</sup> C 0.19

20.30 20.41 F 0.11

+20 20.10 19.79<sup>10</sup> C 0.31

20.49 20.54 F 0.05

+40 19.74 19.82<sup>74</sup> F 0.08

20.50 20.57 F 0.07

+60 19.58 19.75<sup>58</sup> F 0.2020.20 20.50<sub>20</sub> F 0.30



## S. Side

2+80	19.10	19.57 <sub>10</sub>	F0.47
3~	18.94	19.39 <sub>9</sub>	F0.36
+20	18.85	18.98 <sub>85</sub>	F0.13
+40	18.57	18.64 <sub>57</sub>	F0.07
+60	18.17	18.27 <sub>17</sub>	F0.10
+80	17.79	17.87 <sub>79</sub>	F0.08
4~	17.62	17.74 <sub>62</sub>	C0.18
+20	16.99	16.99	0.0
+40	16.53	16.53 <sub>53</sub>	C0.03
+65	15.99	15.87 <sub>99</sub>	C0.12
+90 = PC	15.19	15.25 <sub>19</sub>	F0.06
end.	14.96	15.00 <sub>96</sub>	F0.04

## N. Side

69

20.04	20.32 <sub>04</sub>	F0.28
19.77	20.05 <sub>77</sub>	F0.28
19.42	19.73 <sub>42</sub>	F0.31
19.06	19.38 <sub>06</sub>	F0.32
18.52	19.01 <sub>52</sub>	F0.49
18.02	18.60 <sub>02</sub>	F0.58
17.85	18.15 <sub>85</sub>	F0.30
17.48	17.68 <sub>48</sub>	F0.20
17.03	17.17 <sub>03</sub>	F0.14
16.36	16.51 <sub>36</sub>	F0.15
15.91	15.86 <sub>91</sub>	C0.05
15.64	15.70 <sub>64</sub>	F0.06



Sewer Stakes - 6" Line Laid by City  
in 54+5 - N. of Collier

0-20 = Exist M.H.	stake SRT	03.39 = I.E.	
0+00 = N.L. = Exist plug.	14.72	14.72 403.75	< 10.97
+ 0.70%			
+ 35	13.81	13.81 04.00	9.81
+ 70	13.08	13.08 04.24	8.84
+ 05	11.88	11.88 04.49	7.39
+ 40	10.73	10.73 04.73	6.00
+ 80	10.27	10.27 05.01	< 5.26
2+30	9.82	9.82 05.36	< 4.46

INDEXED

mk  
SEP 12 1950

B.M. = 413.40 = NE. Adams + 54+5  
W.O. 20009 - 6-20-50 - 7.0

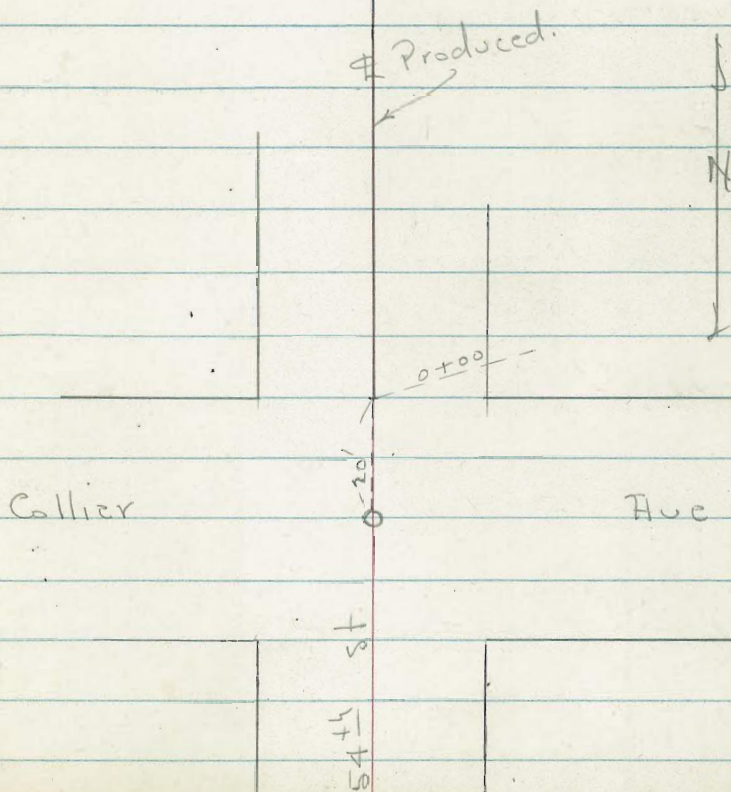
70

= should be

2+30 = end.

INDEXED

mk  
SEP 12 1950





Walker  
Pops  
Mission  
7-19-50

REED AVE.

Paving & Gutter Grades  
from Lummont to Olney Sts.

Stations

Cont. P-72

1+80 Brk

1+60 Brk

1+40 = PVC

TR

1+15

0+90

0+55

0+20 = Brk

0+00 = E line Lummont

Lt.  
Gutter

L

RT  
Gutter 71

30.04

30.82

31.76

33.08

34.40

36.26

38.11

39.03

30.15

31.02

31.98

33.35

34.72

36.64

38.55

39.83

29.46

30.33

31.39

32.81

34.23

36.21

38.20

39.43

INDEXED

SEP 12 1950

32.07

Final Gb  
36.48

40.37

B.M. Lummont & Reed  
SE. CT 7' line P-4B



REED AVE. Prov.

Cont. from p 71

Lt.  
Gutter

±

Rt  
Gutter 72

4+70

27.13

27.16  
 $\frac{.03}{26.79}$

26.38

4+35

27.33

27.36  
 $\frac{.03}{26.94}$  Sub.

26.58

4+00

27.54

27.57  
 $\frac{.03}{27.15}$  Sub.

26.79

3+65

27.74

27.77  
 $\frac{.03}{27.35}$  Sub.

27.00

3+30

27.95

27.98  
 $\frac{.03}{27.56}$  Sub.

27.20

2+95

28.16

28.19  
 $\frac{.03}{27.77}$  Sub.

27.41

2+60 = E.V.C.

28.37

28.40  
 $\frac{.03}{27.98}$  Sub.

27.62

2+40 Bk

28.56

28.60  
 $\frac{.04}{28.18}$  Sub.

27.83

2+20

28.91

28.96  
 $\frac{.05}{28.34}$

28.20

2+00

29.40

29.47  
 $\frac{.07}{29.05}$  Sub.

28.74



~ REED AVE - Paving,  
Cont. from P-72

Lt.  
Gutter

E

St. 73  
Gutter

0+10 - Bk

2623

2626

2578

$\frac{42}{25.84 \text{ Sub.}}$

0+00 Ahead

5+72.68 = E. Line Marrell

2650

2655

2640

2618

2568

20

10

25.98 - Sub.

10

5+59.68 = E.Cb.

2753

2728

2700

2690

2672

2650

2620

2580

2511

30

40

20

10

$\frac{42}{26.30}$

10

20

40

30

5+49.68 = E. 1/4

2740

2710

2702

2680

2662

2631

2570

40

20

10

26.33 - Sub.

10

20

40

5+39.68 = E. Marrell

2748

2712

2705

2684

2665

2635

2575

40

20

10

26.42 - Sub.

10

20

40

5+29.68 = E. Marrell

2745

2708

2690

2680

2660

2632

2580

40

26.38 - Sub.

10

20

40

5+19.68 = H.Cb. Marrell

2803

2743

2685

2670

2660

2640

2610

2578

2561

40

20

10

26.78 - Sub.

10

20

40

30

TR

Hail SW 1/4  
Reed  
Marrell

2757

4+99.68 = H. Line Marrell

2700

2675

2620

$\frac{42}{26.33 \text{ Sub.}}$

4+90 = Bk

2701

2704

2626

$\frac{42}{26.62 \text{ Sub.}}$



Reed Ave. Parc. Marrell to Hayes

H  
-11. Gut

E

S. Gut.  
Rt. 74

Cont. P-75					
2+20			1505'	1508 $\frac{42}{14.66}$ Sub. ✓	1430'
2+00			1591'	1594 $\frac{42}{15.82}$ Sub. ✓	1516'
+80			1698'	1701 $\frac{42}{16.59}$ Sub. ✓	1623'
+60			1827'	1830 ✓ $\frac{42}{17.88}$ Sub. 1+60	1752'
TR	1+40	2106	1966'	1969 $\frac{42}{19.27}$ Sub. 1+40	1891'
1+20			2105'	2108 $\frac{42}{20.66}$ Sub. ✓	2030'
1+00			2237'	2240 $\frac{42}{21.98}$ Sub. ✓	2162'
+80			2351'	2354 $\frac{42}{23.12}$ Sub. ✓	2276'
+60			2449'	2452 $\frac{42}{24.10}$ Sub. ✓	2374'
+40			2531'	2534 $\frac{42}{24.92}$ ✓	2452'
0+20			2595'	2598 $\frac{42}{25.56}$ Sub. ✓	2520'



Reed Ave - Port.  
Marrell to Hoyes

Lt.  
cut

L

Rt.  
cut 75

Cont. P. 76  
4+90

12.63'

12.66 ✓  
12.24 = Sub.

11.88 ✓

4+55

12.82'

12.85 ✓  
12.43 = Sub.

12.07 ✓

4+20

13.01'

13.04 ✓  
12.62 = Sub.

12.26 ✓

TP

12.80

3+85

13.20'

13.23 ✓  
12.81 = Sub.

12.45 ✓

3+50

13.39'

13.42 ✓  
13.00 = Sub.

12.64 ✓

3+15

13.58'

13.61 ✓  
13.19 = Sub.

12.83 ✓

2+80 = F.S.C

2+80 = F.S.C

13.76'

13.79 ✓  
13.37 = Sub.

13.01 ✓

2+60

13.98'

14.01 ✓  
13.59 = Sub.

13.23 ✓

2+40

14.40'

14.43 ✓  
14.01 = Sub.

13.65 ✓



Reed Arc Pass - Noyes to Olney

N  
Gut

E

76  
S. Gut

Stations

Cont. P-77

0+40

1511

1514

1436'

1472'

0+10 = Bk

1377

1380

1302'

1338'

0+00 = E. line Noyes

Gut at R

1347

20  
1345

1/4  
12.40

1332

1/2  
1304

20  
12.62

Gut on Ret. cb face

12.58

12.70 Sub.

E. cb.

50

1461

40

1398

Gut

1318

1/4

1300

12.82

1/2

12.60

Gut

12.26

40

11.70

50

10.63

12.40 Sub.

E. 1/4

40

1400

Gut

1328

1/4

1309

12.92

1/2

12.72

Gut

12.33

40

11.38

12.50 Sub.

E. Noyes

40

1398

Gut

1321

1/4

1305

12.85

1/2

12.67

Gut

12.30

40

11.35

12.73 Sub.

W. 1/4

40

1383

Gut

1300

1/4

12.80

12.65

1/2

12.42

Gut

12.12

40

11.25

12.37 Sub.

W. cb Noyes

50

1386

40

1325

Gut

1270

10.4

12.58

12.45

12.20

11.78

Line

50.74

10.80

10.13

12.03 Sub.

10 Gut

4+29.78 - W. Noyes

1253

1260

11.85

12.18 Sub.



Reed Ave Per.

Notes to  
Olroy

N. Gut.

S. Gut  
77

2+40		1990 <sup>✓</sup> 1990	1993 <sup>✓</sup> 1951-sub. 1973	1915 <sup>✓</sup>
2+20		1987 <sup>✓</sup>	1990 <sup>✓</sup> 1978-sub.	1912 <sup>✓</sup>
2+00		1974 <sup>✓</sup>	1977 <sup>✓</sup> 1935-sub.	1899 <sup>✓</sup>
1+80		1951 <sup>✓</sup>	1954 <sup>✓</sup> 1912-sub.	1876 <sup>✓</sup>
TR	2, Sub 1+60 1879			
1+60		1918 <sup>✓</sup>	1921 <sup>✓</sup> 1879-sub.	1843 <sup>✓</sup>
1+40		1874 <sup>✓</sup>	1877 <sup>✓</sup> 1835 <sup>✓</sup>	1799 <sup>✓</sup>
1+20		1820 <sup>✓</sup>	1823 <sup>✓</sup> 1781-sub.	1745 <sup>✓</sup>
1+00		1757 <sup>✓</sup>	1760 <sup>✓</sup> 1718-sub <sup>✓</sup>	1682 <sup>✓</sup>
0+80		1684 <sup>✓</sup>	1687 <sup>✓</sup> 1645-sub.	1609 <sup>✓</sup>
0+60		1600 <sup>✓</sup>	1603 <sup>✓</sup> 1561-sub	1525 <sup>✓</sup>



Read the Pac. Notes to Olney

Neut

2

S. Gut

78

Actions

4+40	16.50 <sup>✓</sup>	16.57 <sup>✓</sup> 16.15=Sub.	15.83 <sup>✓</sup>
4+20	17.01 <sup>✓</sup>	17.07 <sup>✓</sup> 16.65=Sub.	16.32 <sup>✓</sup>
4+00	17.48 <sup>✓</sup>	17.52 <sup>✓</sup> 17.10 Sub.	16.77 <sup>✓</sup>
3+80	17.93 <sup>✓</sup>	17.96 <sup>✓</sup> 17.54 Sub.	17.20 <sup>✓</sup>
3+60	18.34 <sup>✓</sup>	18.37 <sup>✓</sup> 17.95=Sub.	17.60 <sup>✓</sup>
3+40	18.71 <sup>✓</sup>	18.74 <sup>✓</sup> 18.32=Sub.	17.97 <sup>✓</sup>
3+20	19.06 <sup>✓</sup>	19.09 <sup>✓</sup> 18.67=Sub.	18.31 <sup>✓</sup>
3+00	19.38 <sup>✓</sup>	19.41 <sup>✓</sup> 18.99 Sub.	18.63 <sup>✓</sup>
2+80	19.65 <sup>✓</sup>	19.68 <sup>✓</sup> 19.26 Sub.	18.90 <sup>✓</sup>
2+60	19.83 <sup>✓</sup>	19.86 <sup>✓</sup> 19.44=Sub.	19.08 <sup>✓</sup>



4799.56 = 74 line of day

15.05

15.10 ✓  
14.68 = Sub.

14.35 ✓

4790

15.19 ✓

15.29 ✓  
14.87 = Sub.

14.58 ✓

4765

15.84 ✓

15.93  
72 ✓  
15.51 = Sub.

15.20 ✓



80.61  
80.36  
97  
48

61  
36  
97  
48

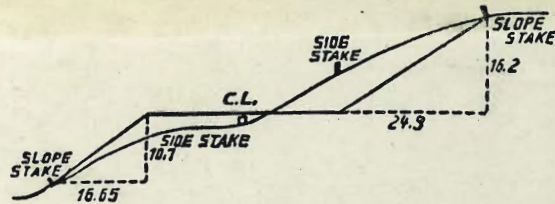
6.52  
4.15  
10.72  
5.36

80.49  
22  
80.170

89.74  
22  
52

55.16  
5.16  
60.32  
56.3  
4.0

38.55  
61.0  
14.6  
14.7  
38.1  
61.2  
4.0  
38.1  
61.2  
4.0



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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