

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
state for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill at side

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external), opposite L by
given tangent (or external).
The distance from a point on the tangent to
the curve is necessarily the square of the tangent
length divided by twice the radius.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.58	.65	.72	.79
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.42	1.51
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.78	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

⊗ = change in grade 1

- ↓ Albion st. - to Silvergate & Dupont ⊗ 3 -
- ↓ Jennings - Albion Wly 4 + 5 + 5A
- ↓ Alley Bk. 2. Lorna Viewwards 5.A
- ↓ " " 4 " " 6
- ↓ Albion - Charles - Dupont 6 - 8
- ↓ Silvergate South of Dupont 9
- ↓ Alley Bk. 4. Warner Villas ⊗ 10
- ↓ Silvergate - North of Dupont. 10 - 11
- ↓ Ely. and Alley Bk. 3 Warner Villas ⊗ 12
- ↓ " " " " 2 Warner Villas ⊗ 12-13
- ↓ Jennings - West of Silvergate 13
- ↓ Silvergate - South of Jennings ⊗ 14-15
- ↓ Wilcox - West of Silvergate ⊗ 16.
- ↓ Catalina 16-20
- ↓ Easement to P.L. 143 South of Warner Villa 20-21
- ↓ Alley between } East of ⊗
- ↓ Wilcox + Charles } Catalina ⊗ 22
- ↓ Alley between } Bk. I ⊗
- ↓ Charles + Dudley } W.V. tract. ⊗ 24

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Benchos - P. 79

- ✓ Alley Blk 2 Warner Villa Tracts Ely of Catalina
- ✓ " " 3 " " " " " "
- ✓ " " 4 " " " " " "
- ✓ P.L. 143 - 10' so. Sly. line Warners Villa
- ✓ Ties - Silvergate - Dupont to Charles
- ✓ " Dupont + Albion
- ✓ " Albion - Inez to Jennings
- ✓ Alley Blk 3 Point Loma Highlands
- ✓ " Thru. Por. of P.L. 143 Nor. of Rosecroft
- ✓ Line Change on Catalina Blvd.
- ✓ Ties Lot 14 + 15 Blk. 2. Warner Villas
- ✓ Scott. St. Dickens to Harbor Drive
- ✓ Fenelon St. Scott to Rosecrans
- ✓ Garrison St. Scott to Rosecrans
- ✓ Extension of line thru P.L. 143
Upshur St. - Scott St. w/ly
- ✓ Alley Blk 3 Carmel Hgts
- ✓ " " 2 Univ Hgts
- ✓ Lots - 2-3-4+5 - of County Paradise
- ✓ Alley Blk 99 - City Hgts. 59-60
- ✓ Morena Blvd. Buena Vista to Custerman - 61

- Alley Blk 52 Fairmount Add. to City Hgts - 62-63
- Fire Engine House #5 - Univ + 9th - P 64
- Felspar. Morrell to Noyes water meter + grades } 65-66
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- Felspar. Haines to Cass (w) - 70 to 67
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- (X) 30-31

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- Univ to Polk Highland 55
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*
Albion St.
from Alley So. of Talbot - Sly

T.P.

2+50 INDEXED
MAY 15 1950

232.00
13.05
3.02
C 10.03

2+00

245.05 X
228.98
16.07
7.73
C 8.34

1+50

225.95 T.P.
7.72
0.84
C 6.88

1+00

222.92
10.75
4.53
C 6.22

0+50

+ 0.09
because M.H.
15 0.19 high

219.99
13.68
7.59
C 6.09

0+00: Exist M.H.

233.67 X
216.88
16.79
16.60
+ 0.19

5+00

2.21990

245.74
9.96
1.94
C 8.02

John St.
M.H. #33
4+6512

244.97
10.73
3.18
C 7.55

4+50

244.06
11.64
3.77
C 7.87

4+00

241.06
14.64
5.90
C 8.74

3+50

6.0590

238.03
17.68
7.87
C 9.80

3+00

255.70 X
235.02
20.68
9.98
C 10.70

3

B.M. #1 - P. 77

263.97
1.39
265.36
11.60
253.76
1.02

254.78
12.74
242.04
1.04

243.08
10.45

232.63
1.04

233.67
84

232.83
12.22

245.05
0.45

244.60
11.10

255.70
1.94

253.76
11.20

264.96 X
0.53

(Cross in Dr.)

33rd S. Ely. R.P. Cross

From E. Men.

Albion + Jennings = B.M. #2

6.33

270.76

Albion St. - Cont P. 54.

6' + 12' South
Jennings + Albion.

M.H.# 30

7+85⁰

$$\begin{array}{r} 252.00 \\ 12.96 \\ 1.15 \\ \hline C-1681 \end{array}$$

B.M. 2 - P. 79

264.43

7+50

$$\begin{array}{r} 251.24 \\ 13.72 \\ 2.03 \\ \hline C-1169 \end{array}$$

7+00

$$\begin{array}{r} 250.14 \\ 14.82 \\ 4.00 \\ \hline C-10.82 \end{array}$$
8+50
2.21990
$$\begin{array}{r} 249.04 \\ 15.92 \\ 5.78 \\ \hline C-10.14 \end{array}$$

8+00

$$\begin{array}{r} 247.94 \\ 17.02 \\ 7.52 \\ \hline C-9.50 \end{array}$$

5+50

$$\begin{array}{r} 264.96 \times \\ 246.84 \\ 18.12 \\ 7.39 \\ \hline C-8.73 \end{array}$$
Jennings St. Stub.
Wly. from AlbionINDEXED
MAY 15 1950

1+30 stub. end.

$$\begin{array}{r} 263.25 \\ 7.51 \\ 0.34 \\ \hline C-6.67 \end{array}$$

1+00

$$\begin{array}{r} 261.00 \\ 9.76 \\ 3.04 \\ \hline C-6.72 \end{array}$$

0+50

$$\begin{array}{r} 270.76 \times \text{FROM P. 3} \\ 257.25 \\ 13.51 \\ 5.44 \\ \hline C-8.07 \end{array}$$
0+00 = M.H. #30
Albion St.
+ Jennings
$$\begin{array}{r} \text{TP} \\ 264.96 \times \text{FRM} \\ \text{West} \\ 253.50 \\ 11.46 \\ 1.15 \\ \hline C-10.37 \end{array}$$

Albion St.

x

5

T.P.

9+75

252.76
12.07
9.77
C-2.30

BH #2 P79

264.43
0.40
264.83 X
9.75
255.08
10.10
265.18 X

9+50

252.66
12.17
9.20
C-2.97

9+25

0.40%

252.56
12.27
7.48
C-4.79

Cont. 5A-rt.

9+00

252.46
12.37
5.38
C-6.97

10+51.32 M.H. # 28

253.07
12.11
7.20
C-4.71

Tang =
Sec. = 5.80

Ely. end Jennings

8+74.10 M.H. # 29

252.36
12.47
5.26
C 7.21

10+21.32 %
0.40%

252.95
12.23
9.00
C-3.23

8+29.55

0.40%

264.83 X
252.18
12.65
3.43
C 9.22

Tang =
Sec. =

9+91.32 = Δ 28°-08' rt.

265.18
252.83
12.35
11.96
C-0.39

* Alley BIK 2. Lotna View

(Cont. P. 6)

Albion line (From P. 5)

5A

Dead end.
2+09.56

263.97

10.03

2.55

C-7.48

INDEXED

2+00

MAY 15 1950

263.47

10.53

3.19

C-7.34

1+50

260.87

13.13

5.57

C-7.56

1+00

5.20%

258.27

15.73

7.98

C-7.75

0+50

255.67 T.P.

7.51

18.4

C-7.67

From P. 5

265.18

1.94

263.34

10.66

274.00

13+81.47=M.H. 24-Δ 1st-Adkt.
Alley BIK. A Lotna View

13+50

13+00

12+50

12+00

11+50

11+00

From P. 5

P. 5

258.98

12.53

5.35

C-7.18

258.43

13.08

6.01

C-7.07

257.53

13.98

6.29

C-7.69

256.63

14.88

7.88

C-7.00

271.51 X

255.95

15.98

8.54

C-7.24

254.83

10.35

4.44

C-5.91

265.18 X

253.93

11.25

4.62

C-6.63

From P. 5

265.18 X

2.74

262.44 X

9.07

271.51

0.75

270.76

Mon.

S. Line Charles

S. East of

Ely line

Albion

BM #3

✓ Alley Bk.A Loma View

Albion St. line
Also Charles St.

6

Dead end
2+15⁴⁶

280.93X
269.97
10.96
3.52
C-7.44

5' L.O.P
M.H.#2A
Ov. L.O. = 258.98
C = 7.18
Elev. Sta. = 266.16
8.21
274.37X

16+00

INDEXED
MAY 15 1950

J.P.
274.51X
263.63
108.8
1.44
C-9.44
BM#3
270.76
3.75
274.51X
0.50

2+00

INDEXED
MAY 15 1950

280.93X
269.18
11.75
4.26
C-7.49

273.81
7.12
280.93X

15+50

2.20%

Reset,
275.37X
262.53
128.4
4.64
C-8.20

262.53
117.8
4.72
C-7.26
274.01
7.43
283.44X

1+50

274.37X T.P. 5' L+ stub
266.63
7.74
0.56
C-7.18

tan θ =
Sec θ = 7.03
15+24⁴⁷ M.H.# 23
Δ 89°-18' RT.

261.98
125.3
4.30
C-8.23

1+00

5.10%

264.08
10.29
3.33
C-6.96

15+00

261.47
13.04
5.47
C-7.57

0+50

261.58
12.84
5.29
C-7.55

14+50

2.10%

260.42
14.07
7.47
C-6.60

M.H.# 2A
= 13+81.47 P.5
0+00

274.37X
258.98
15.39
7.80
C-7.59

7.07 @ 45° S.W.

14+00

274.51X
259.37
15.14
8.26
C-6.89

✓ Charles st.
Also Albion st.

19+50

265.83
17.61
6.20
C-11.37

19+00

INDEXED
MAY 15 1950

265.43
17.81
5.83
C-11.98

18+50

265.43
18.01
5.55
C-12.46

18+00

265.23
18.21
5.74
C-12.47

17+50 0.40%

17+00

265.03
18.41
6.29
C-12.12

17+00

264.83
18.61
7.15
C-11.46

16+50

264.63
18.81
8.32
C-10.47

Tang =

Sec = 7.06

16+43.43 = M.H.# 22, Δ89°-49'4".

Charles + Albion

283.447
264.60
18.84
8.37
C-10.47

Albion

7

22+00

266.83

19.01
4.43
C-8.58

283.447
7.08
276.36
3.48

21+50 0.40%

279.847
266.63
19.21
3.85
C-7.36

279.847

Tan = 0.97
Sec = 5.09

21+25.45 M.H.# 16
Δ 23°-02' Lt.

283.447
266.53
16.91
7.08
C-7.83

T.R. - 5.09 stub

21+00

266.43
17.01
7.08
C-7.93

20+50

266.23
17.21
6.94
C-10.27

20+00 0.40%

266.03
17.41
6.75
C-10.46

Albion

Albion
(+ Dupont.)

8

24+50

267.85
11.99
4.02
C-7.97

Tang. = 5.00
SEC = 7.07
27+19.9A M.H. #12
Δ 90° Rt.
51+10' East.

268.99
16.22
8.52
C-7.70

24+00

0.42%

267.64
12.20
4.10
C-8.10

27+00

268.90
16.31
8.44
C-7.87

279.84X
392
275.92
9.29
285.21X

23+50

267.43
12.41
4.43
C-7.98

26+50

268.69
16.52
8.66
C-7.86

Tang = 0.97
SEC = 5.09

23+25 M.H. #15
Δ 23° 00' - 30' Rt

267.33
12.51
4.75
C-7.76

26+00

285.21X
268.48
16.73
8.80
C-7.93

0.10
2
4
0

23+00

267.23
12.61
4.88
C-7.73

25+50

279.84 - T.P. 5' stub.
268.27
14.57
3.92
C-7.65

22+60

22+50

0.40%

267.07
12.77
4.16
C-8.12

25+00

268.06
11.78
4.16
C-7.62

x Dupont.
(Albion 1170)

Silvergate - South of Dupont x

9

30+00

279.07
16.09
7.42
C-8.67

285.21
4.90
283.31
11.85
295.16A
2.32

32+39.96 to West.
M.H.#10

changed to 298.10

289.00
12.49
469
C-7.80

29+50

295.16
277.27
17.89
9.61
C-8.28

292.84 = 2/2
Tie 50' w/ly
from Silvergate
+ Dupont (to Se. -
Sta 30+53.19)

32+39.96 = M.H.#10
Alley

2 cuts
287.98 To North
13.51
4.69
C-8.82

29+00

285.21
275.47
9.74
1.90
C-7.84

T.A.S. Nail

32+00

INDEXED
M.K.
MAY 15 1950

B.M.#A-P.79
272.84
8.65
301.49
286.70
14.79
6.38
C-8.41

28+50
3.60 %

273.67
11.54
4.10
C-7.44

31+50
3.20 %

285.10
16.39
8.26
C-8.13

28+00

274.87
18.34
5.67
C-7.67

31+00

301.49
283.50
17.99
10.10
C-7.89

27+50

285.21
270.07
15.14
7.27
C-7.87

605.86
Silvergate
30+53.19 = M.H.#11
Δ Lt

605.86
E.N.
1906.50 295.16
605.86
South
281.00
14.16
4.47
C-9.69
282.00
13.16
4.47
C-8.69
C.9.00

Alley. Bika. Warner Villas

INDEXED

MAY 15 1950

Change
change grade to cut
out high drop at
M.H. #10
4/27/50

Dead end.

33+79.96
306.59X
298.80
7.79
1.12
C-6.67

~~298.80
7.79
1.12
C-6.67~~

301.49X
4.48
297.01
9.58
306.59X

33+50

296.50
10.09
2.68
C-7.41

~~296.70
7.89
2.68
C-7.21~~

33+00

306.59X
292.68
13.91
5.50
C-8.41

~~306.59X
293.20
13.39
5.50
C-7.89~~

32+50

301.49X
288.86
12.63
4.48
C-8.15

301.49X T.P.
289.70
11.79
4.48
C-7.31

M.H. #10-P.9

301.49X
288.10
13.39
4.69
C-8.70

Silvergate
North of Dupont

10

2+00 INDEXED
MAY 15 1950

282.40
11.95
4.78
C-6.77

B.M. #4 R.79
29.284
1.51
29.35X

1+63.23 M.H. #1A

294.75X
282.14X
12.21
5.09
C-7.12

1+50

282.05
12.30
4.95
C-7.35

1+00

281.70
12.65
4.85
C-7.80

0+50

281.35
13.00
4.70
C-8.30

Dupont. (R9)
0+00 = M.H. #11

294.35X
281.00
13.85
3.66
C-9.69

✓ Silvergate - Dupont North

Silvergate
North of Dupont ✓

11

5+00

284.50
15.12
7.31
C-7.81

7+28.45 Dead end

299.02 X
288.52
11.10
3.41
C-7.69

299.03 X
288.52
10.51
2.82
C-7.69
check

4+50

284.15
15.47
8.28
C-7.20

7+00

288.01
11.61
3.64
C-7.97

4+00

283.80
15.82
9.13
C-6.69

294.35 X
4.50
289.85 TR
9.77
299.62 X

6+50

287.11
12.51
2.48
C-8.03

3+50

0.798

299.62 X
283.45
16.17
9.38
C-6.79

6+00

286.21
13.41
5.46
C-7.95

3+00

283.10 T.P.
11.25
4.50
C-6.75

16.5/2
9.77
C-6.75

5+50

285.31
14.31
6.39
C-7.92

2+50

294.35 X
282.75
17.60
4.80
C-6.80

5+08.23 = M.H. #17

284.56
15.06
7.24
C-7.82

Ely. End. Alley BIK 3
 Warner Villa Tract

INDEXED
 MAY 15 1950

Set to this change so as
 to cut out drop at
 M.H. #1A

1+40 D. end.	290.00	290.00
	8.83	8.83
	174	174
C-	7.09	7.09
1+00	287.75	288.04
	1108	10.79
	3.86	3.86
C-	7.22	6.93
0+50	284.94	285.59
	13.89	13.24
	6.84	6.84
C-	7.05	6.40
0+00 = M.H. #1A	282.14	283.14
Silvlegate (P.10)	16.69	15.69
	9.57	7.57
C-	7.12	6.12

A. 90% 5.614%

1+63.23 M.H. #1A
 P.10
 282.14 = EL.
 7.12 = cut
 289.2 C = stub.
 9.57
 298.83 X

Ely. End Alley BIK. 2 + + 12
 Warner Villa Tract.

cut out drop at M.H. #17 Change in
 grade. 4/28/50

2+50	310.11	297.75	297.37
	12.36	372	1274
	8.64	3.72	3.72
			C 9.02
2+00	310.11 X	295.40	294.82 (P.11)
	14.81	6.55	299.62
	8.16	6.55	1.18
			298.44 ✓
1+50	310.11 X	292.26	310.30 X
	17.06	17.85	111.86
	9.09	9.09	298.44 ✓
	7.9 X	8.76	310.30 X
			C 8.76
1+00	289.71	290.70 TP	283.10
	9.91	8.92	6.75
	1.18	1.18	289.85 = stub.
			9.72
			299.57
			1.13
			298.44
			11.67
0+50	287.15	288.35	310.11
	12.47	11.27	1.20
	3.65	3.65	308.91 X
			2.25
			311.16
			5.88
0+00 = M.H. #17	294.60	299.02	305.28
(Silvlegate P.11)	15.02	13.62	Iron pin.
	7.24	7.24	3 RT. Sta.
			3+80 ± P.26
			= B.M. #5

5.17%

Cont. P.13

Ely end Alley BIK 2
 Warner Villas Tract.

305.28 = B.M.#5
 5.88

311.16
 10.77

300.39
 00.07

300.46
 7.98

292.48
 1.48

293.96
 1.21

292.55 = B.M. Ely, Oc. Silvergate + 2 charles
 1.41

293.96 = X

293.96 = X
 11.73

282.23
 1.92

284.15
 11.26

272.89
 0.56

273.45
 9.00

264.45 = B.M.#2 (264.45)
 .47
 .02

INDEXED

MAY 15 1950

N.G.

B.M.#5 = 11' RT P. 17

5' RT + 3+80 = (C.P. 26)

311.48
 6.00

305.48

310.30 X
 1.19

309.11
 2.37

311.48 X
 10.88

300.50
 0.07

300.67
 4.23

296.44 = 4' stub
 7+29.45
 P. 11

3+40 = M.H.#18

310.11 + T.P.
 301.98

301.98 T.P.

301.98

8.13
 1.20

8.32
 1.19

8.13
 1.20

C 6.93

C 7.13

C 6.93

3+00

310.11 X
 300.10

310.30
 300.10

299.93

10.01
 2.09

10.20
 2.09

10.18
 2.09

C 7.92

C 8.11

C 8.09

Jemmings

West of
 Silvergate

13

stakes 5' RT, opp

INDEXED

MAY 15 1950

2+50

2+00

1+50

1+00

0+50 = M.H.#32
 Δ 70-51' RT

0+00 = Exist. M.H.

277.63 X

260.76

16.87
 10.35

C 6.52

265.94 X

258.35 TIP

7.59
 0.74

C 6.85

255.94

10.00
 4.00

C 6.00

253.53

12.41
 6.22

C 6.19

251.12

14.82
 8.22

C 6.60

265.94 X

250.77

15.17
 8.69

C 6.48

264.43 B.M.#3
 12.28 P. 17

276.71

2.21
 274.20 = 3 stakes

11.20
 Jemmings +
 Silvergate.

C 6.52

B.M.#6
 274.20
 2.51

276.71

11.81
 265.20

0.74

265.94 X

12.43

277.63 X

3.43

274.20

B.M.#6

4.8290

✓ Silvergate

Silvergate ✓
South of Jennings

14

INDEXED
MAY 15 1950

5+00 $\frac{269.82}{13.88}$
6.50
C-7.38

4+50 $\frac{268.50}{15.20}$
7.33
C-7.87

2.37%
2.64%

4+00 $\frac{267.18}{16.52}$
7.60
C-8.92

7074 1A.14 in S.W. Quad.
3+59+00 M.H.# 31
Silvergate
Δ 90° 16' Rt.

	277.63x	283.70 x
west	$\frac{266.00}{11.63}$	$\frac{266.10}{17.60}$ south
	2.32	8.40
	C-9.31	C-9.20

3+50 $\frac{265.58}{12.05}$
2.58
9.47

3+00 $\frac{277.63x}{263.17}$
14.46
7.87
C-6.59

4.82%

7+50 $\frac{276.50}{15.81}$
8.41
C-7.40

7+00 $\frac{275.10}{17.21}$
out.

2.80%

6+96.02 = M.H. 27 T.P. ↓
N.T.S. $\frac{283.70x}{274.99}$
8.71
1.01
C-7.70

$\frac{292.31x}{275.09}$ west
17.22 Page
9.62 16.
C-7.60

6+50 $\frac{273.78}{9.92}$
2.48
C-7.44

B.M. 46
 $\frac{274.20}{9.50}$
283.70x
1.01
 $\frac{282.69}{9.62}$
292.31x

6+00 $\frac{272.46}{11.24}$
3.94
C-7.30

2.87%
2.64%

5+50 $\frac{271.14}{12.56}$
5.31
C-7.25

✓ Silvergate
South of Jennings

5' Lt.

10+50

$$\begin{array}{r} 299.03 \\ 284.90 \\ \hline 14.13 \\ 6.19 \\ \hline C-7.94 \end{array}$$

10+00

$$\begin{array}{r} 292.31 \times \\ 283.50 \text{ T.P.} \\ \hline 8.81 \\ 1.17 \\ \hline C-7.64 \end{array}$$

$$\begin{array}{r} 292.31 \\ 1.17 \\ \hline 291.14 \\ 7.89 \\ \hline 299.03 \end{array}$$

9+50

$$\begin{array}{r} 282.10 \\ 10.21 \\ 2.89 \\ \hline C-7.32 \end{array}$$

9+00

$$\begin{array}{r} 280.70 \\ 11.61 \\ 4.41 \\ \hline C-7.120 \end{array}$$

12+01.07 = M.H.# 21

289.13 check 7+28²⁵

$$\begin{array}{r} 9.90 \\ 3.07 \\ \hline C-6.83 \end{array}$$

 P. 11
 OK

8+50

$$\begin{array}{r} 279.30 \\ 13.01 \\ 5.83 \\ \hline C-7.18 \end{array}$$

11+50

287.70

$$\begin{array}{r} 11.33 \\ 4.00 \\ \hline C-7.33 \end{array}$$

8+00

$$\begin{array}{r} 292.31 \times \\ 277.90 \\ \hline 14.41 \\ 7.18 \\ \hline C-7.23 \end{array}$$

11+00

286.30

$$\begin{array}{r} 12.73 \\ 4.89 \\ \hline C-7.84 \end{array}$$

+ Wilcox
Silvergate West.

2+40 = D. End.

282.11

INDEXED

10.39

2.64

C-7.75

MAY 15 1950

2+00

280.93

11.57

2.45

C-9.12

1+50

279.47

13.03

2.87

C-10.16

1+00

278.01

14.49

4.95

C-9.54

0+50

276.55

15.95

9.34

C-6.61

0+00 = M.H. 27
Silvergate (P-1A)

292.50 X

275.09

17.41

7.81

C-7.60

Catalina Blvd. +
Wilcox - South

16

2+00

INDEXED

MAY 15 1950

255.21

12.29

4.37

C-7.92

75+114 S.W. quad.
1+64.75 - M.H. #1
Δ 0°-51' Lt.

1+50

1+00

0+50

0+00 = Exist. M.H.

254.49 N45

13.01

4.86

C-8.15

254.10

13.40

5.62

C-7.78

252.77

14.73

6.59

C-8.14

251.43

16.07

7.78

C-8.29

267.50 X

250.10

17.40

17.41

.01

stub 2/475-21
1899 +
63

EL. =
262.62
4.88

267.50
4.76

262.74
Set as 84
#7-P-79

262.62
4.88

267.50 X
1.60

265.90 =
spite
& Charles
+ Catalina
= B.M. 28

5+00

$$\begin{array}{r} 261.36 \\ 14.08 \\ 7.16 \\ \hline C-6.92 \end{array}$$

4+50

$$\begin{array}{r} 260.34 \\ 15.10 \\ 8.25 \\ \hline C-6.85 \end{array}$$

4+00

$$\begin{array}{r} 259.31 \\ 16.13 \\ 8.73 \\ \hline C-7.40 \end{array}$$

3+50

2.05%

$$\begin{array}{r} 275.44 \times \\ 258.29 \\ 17.15 \\ 9.45 \\ \hline C-7.70 \end{array}$$

3+00

$$\begin{array}{r} 267.50 \times \\ 257.26 \\ 10.24 \\ 2.69 \\ \hline C-7.55 \end{array}$$

2+50

$$\begin{array}{r} 267.50 \times \\ 256.24 \\ 11.26 \\ 3.64 \\ \hline C-7.62 \end{array}$$

7+00

$$\begin{array}{r} 275.44 \times \\ 266.76 \\ 8.68 \\ 2.92 \\ \hline C-5.76 \end{array}$$

6+50

$$\begin{array}{r} 265.40 \\ 10.04 \\ 4.00 \\ \hline C-6.04 \end{array}$$

6+29.8A

 $\Delta 10-15' \text{ Rt.}$

$$\begin{array}{r} 264.86 \\ 10.58 \\ 4.62 \\ \hline C-5.96 \end{array}$$

6+00

$$\begin{array}{r} 264.04 \\ 11.40 \\ 4.87 \\ \hline C-6.53 \end{array}$$

5+50

2.72%

$$\begin{array}{r} 262.68 \\ 12.76 \\ 5.87 \\ \hline C-6.89 \end{array}$$
7²⁹+14⁰⁸ in S.W. Quad.

5+0A, 8A = M. H. #2

 $\Delta 0-512' \text{ Rt.}$

$$\begin{array}{r} 261.46 \text{ N+5} \\ 13.98 \\ 6.90 \\ \hline C-7.08 \end{array}$$

275.44

3.25

272.19 =

Set B.M.

± spike
Catalina

Dudley,

= B.M. #9

9+50
274.26
 10.44
 2.87
 C-7.57

9+00 3.74%
284.90x
272.59
 12.31
 4.74
 C-7.57

6.96 + 13.92 ins. manual
 8+61.8A M.H.# 3
 $\Delta 1^\circ - 15' Lt.$
280.29x
276.17 N+S
 9.12
 1.51
 C-7.61

8+50
270.84
 9.45
 2.49
 C-6.96

8+00 2.72%
269.48
 10.81
 4.40
 C-6.41

7+50
280.29x
268.12
 12.17
 6.42
 C-5.75

707 14.9 ins. manual.
 12+0A 8A - M.H.# A

12+00

11+50

11+00

10+50 3.74%

10+00

M.H.# 3 to M.H.# A
 Use stakes for grade
 " Red heads for line - 5' offset.

28400 B.M.# 9
12.93 272.19
 4.70 1271
 C-8.23 284.90x
 59

283.81 284.31
13.12 12.62
 4.96 296.93x
 10.90
 C-8.16 286.03 =
 B.M.# 10 =
 spike & warning
 + Catalina

281.94
14.99
 6.27 296.93x
 C-8.72

280.07
15.86
 8.21
 C-8.65

296.93x
278.20
 18.73
 10.21
 C-8.52

284.90x
276.33
 8.57
 0.59
 C-7.98

Catalina
stakes 4' RT. of Φ

19

15+00	$\begin{array}{r} 288.21 \\ 14.82 \\ 5.50 \\ \hline C-9.32 \end{array}$	
14+50	$\begin{array}{r} 287.50 \\ 15.53 \\ 6.03 \\ \hline C-9.50 \end{array}$	$\begin{array}{r} 296.93 \times \\ 107 \\ \hline 295.86 \\ 7.17 \\ \hline 303.03 \times \\ 6.32 \\ \hline 296.71 = \end{array}$
14+00	$\begin{array}{r} 303.03 \times \\ 286.79 \\ 18.24 \\ 6.30 \\ \hline C-7.94 \end{array}$	$\begin{array}{r} 303.03 \times \\ 6.32 \\ \hline 296.71 = \end{array}$
13+50	$\begin{array}{r} 296.93 \times \\ 286.07 \\ 10.86 \\ 1.07 \\ \hline C-9.79 \end{array}$	$\begin{array}{r} B.M. \# 11 = \text{spike} \\ \& \text{ Dupont } \& \text{ Catalina.} \\ 303.03 = \times \\ 3.65 \\ \hline 299.38 = B.M. \# 12 \\ \& \text{ spike } \text{Pio } \text{Pio} \times \\ \text{Catalina} \end{array}$
13+00	$\begin{array}{r} 285.36 \\ 11.57 \\ 1.79 \\ \hline C-9.78 \end{array}$	$\begin{array}{r} 303.03 = \times \end{array}$
12+50	$\begin{array}{r} 296.93 \times \\ 284.64 \\ 12.29 \\ 3.11 \\ \hline C-9.18 \end{array}$	

17+50	$\begin{array}{r} 290.56 \\ 12.47 \\ 3.98 \\ \hline C-8.49 \end{array}$	$303.03 \times$
17+00	$\begin{array}{r} 290.16 \\ 12.87 \\ 4.16 \\ \hline C-8.71 \end{array}$	
16+50	$\begin{array}{r} 289.77 \\ 13.26 \\ 4.38 \\ \hline C-8.88 \end{array}$	0.79%
16+00	$\begin{array}{r} 289.37 \\ 13.66 \\ 4.98 \\ \hline C-8.68 \end{array}$	
15+54.84 = M.H. # 5	$\begin{array}{r} 289.01 \\ 14.02 \\ 5.27 \\ \hline C-8.75 \end{array}$	
15+50	$\begin{array}{r} 288.93 \\ 14.10 \\ 5.29 \\ \hline C-8.81 \end{array}$	

✓ Catalina also → Easement in P.L. #143. South of Warner Villa Tract. ✓ 20

20+00

292.53
12.83
4.27
C-8.56

19+50
0.79%

292.13
13.23
5.06
C-8.17

19+00

305.367
291.74
13.62
5.27
C-8.35

87-55-15°H.
1 18+57.04 = M.H.#6
89-55-15°H.

291.40 T.P.#1 EL. 299⁶⁵
11.63
3.35
C-8.28

1 18+50
0.79%

303.037
291.34
11.69
3.34
C-8.35

1 18+00

303.037
290.95
12.08
3.52
C-8.56

22+50

294.95
10.41
3.29
C-7.12

22+00

1.50%
stakes 5' pt.
from here

294.20
11.16
3.95
C-7.21

INDEXED
M.R.
MAY 15 1950

21+86.71 = M.H.#6A

294.00
11.36
2.57
C-8.79

21+50

stakes 4' pt. to here

293.71
11.65
3.30
C-8.35

21+00

0.79%

293.31
12.05
3.77
C-8.28

20+50

292.92
12.44
4.43
C-8.01

Easement P.L. 143

Stakes 5' RT. of E.

See p. 49 for Extension of 105' E.L.

25+22.71 = M.H. # 6.B. 299.04

End. of line 15.12

Now R.O.T. 1/17/50 C-9.44

25+00 298.70

15.46

7.93

C-7.53

24+50 314.16 X

297.95

16.21

9.03

C-7.18

24+00 305.96 X

297.20 T.P.

8.16

1.68

C-6.48

23+50 296.45

8.91

2.98

C-5.93

23+00 305.36 X

295.70

9.66

3.10

C-6.56

305.36 X

1.68

303.68

10.48

314.16 X

0.73

31343

10.68

324.11 X

3.53

320.58 = 5+50. Easement Sacof Pio Pico = T.B.M. I

2.22

322.80

9.41

313.39 = 6+00 = Alley So. of Dupont = T.B.M. #2

1.80

335.19

9.07

306.12 = 6+00 = Alley So. of Warner = T.B.M. #3

9.07

315.19

12.95

302.24

1.08

303.32

10.72

292.60 = B.M. #4 292.84

Alley Between Wilcox + Charles

Catalina - East,

Block 181 Pt. Loma Highlands,

3 home view

2+50

268.70

11.33

5.12

C-6.21

B.M. #7

262.74

6.80

269.54 X

1.92

267.62

12.41

280.03 X

1.06

278.97

12.58

291.55

1.24

290.31

10.04

300.35

5+00

291.55 X

280.32

11.23

1.24

C-9.99

277.50 X

278.82

12.73

3.51

C-7.22

291.55 X

277.50

14.05

6.73

C-7.32

4+50

4+05.74 = M.H. #26

4+00

277.16

14.39

9.22

C-7.17

3+50

291.55 X

274.34

17.21

10.98

C-6.23

3+00

280.03 X

271.52

8.51

2.72

C-5.79

INDEXED

M.R.

MAY 15 1950

2+00

265.88

14.15

7.43

C-6.72

1+50

280.03 X

263.06

16.97

9.80

C-7.17

1+00

269.54 X

260.24

9.30

1.93

C-7.37

0+50

257.42

12.12

4.05

C-8.07

0+00 = M.H. #1

(P-16)

269.54 X

254.60

14.94

6.87

C-8.07

stakes 5' int. of #

Alley between
Wileot & Charles

23

7+92.57 = M.H.#25

300.35

End. of line

289.14

11.21

6.30

C-4.91

7+50

287.82

1253

4.18

C-8.35

7+00

286.32

14.03

3.85

C-10.18

~~6+50~~

284.82

15.53

4.11

C-11.42

~~2.75~~
3.01

6+00

283.82

17.03

3.56

C-11.47

5+50

300.35

286.82

18.53

7.33

C 1120

Alley Bk. I Warner Villa Tract,
between Charles & Dudley

24

2+50

297.46^x
278.71
18.75
11.98
C-16.77

5+50

295.30
13.06
3.65
C-7.41

B.H.#9

272.19

129

273.48^x

0.68

27280

12.32

285.12^x

0.16

28496

12.50

297.46^x

1.77

295.69

12.67

308.36^x

INDEXED
MAY 15 1950

2+00

285.12^x
275.28
9.84
3.08
C-6.76

5+00

293.20
15.16
6.32
C-8.84

3.84%
4.12%

1+50

271.86
13.26
6.47
C-6.79

4+50

308.36^x
291.10
17.26
9.45
C-7.81

6.75%
7.54%
8.85%

1+00

285.12^x
268.44
16.68
10.40
C-6.28

4+00 = M.H.# 20

West.

297.46^x
289.00
8.46
1.77
C-6.69

0+50

273.48^x
265.02
8.46
3.20
C-5.26

5

3+50

285.57
11.89
5.23
C-6.66

stakes 5' RT of \pm

0+00 = M.H.# 2
Catalina (P17)

273.98^x
261.60
11.88
4.94
C-6.94

3+00

6.75%
6.85%

282.14
15.32
8.52
C-6.80

5' RT

✓ Alley Bk. I
Warner Villa Tract.

25

INDEXED
MAY 15 1950

6+86.50 D. End
D

308.36
301.00
7.36
0.71
C-6.65

6+50

299.50
8.86
0.85
C-8.01

6+00

3.84%
4.20%

297.40
10.96
2.08
C-8.88

5' RA

Alley BIK. 2 Warner Villa tract.

between Dudley + Warner
East from Catalina.

INDEXED

MAY 15 1950

2+50

288.00
14.58
5.00
C-9.58

B.M.# 9
272.19
10.43
282.62 X
0.65

2+00

302.58 X
284.65
17.93
8.42
C-9.51

281.97
11.30
293.33 X
0.69
292.64
9.92

1+50

293.33 X
281.30
12.03
2.83
C-9.20

302.58 X
1.15
301.43
6.33
307.76

1+00

6.40
6.70

277.95
15.38
6.12
C-9.26

3+82.95 = M.H.#19
End of line.

296.89
108.7
3.10
C-7.77

0+50

293.33 X
274.60
18.73
9.84
C-8.89

3+50

307.76 X
294.70
13.06
4.50
C-8.56

0+00 = M.H.#3
(P.18)

282.62 X
271.25
11.37
3.84
C-7.53

3+00

6.70
6.70

302.58 X
291.35
11.23
1.32
C-9.91

stakes 5' LT of #

5' LT.

Alley BIK.3 Warner Villa Tract, Ely. from Catalina — between Warner + Dupont. ✓

27

5+88.40 = D.E.
End

301.00
13.49
7.81
C-5.68

2+50

INDEXED

293.85
15.20
6.79
C-8.41

MAY 15 1950

5+50

300.73
13.76
6.49
C-7.27

B.M.#11
296.71
2.50

2+00

309.05 X
291.90
17.15
7.15
C-8.00

5+00

300.38
14.11
4.76
C-9.15

299.21 X
1.25
297.96
11.09
309.05 X
1.05
308.00
6.49

1+50

299.21 X
289.95 T.P.
9.26
1.25
C 8.01

4+50

300.03
14.46
4.72
C-9.74

314.49 X
8.39
306.10 =
306.12
T.B.M.#3 P.21

1+00

~~3.67%~~
3.90%

288.00
11.21
2.87
C-8.34

A+00 = M.H.# 13

314.49 X
299.68
14.81
5.63
C-9.18

0+50

286.05
13.16
4.35
C-8.81

3+50

309.05 X
297.75
11.30
2.09
C-9.21

0+00 = M.H.# A
(P18)

284.10
15.11
6.78
C-8.13

3+00

~~3.67%~~
3.90%

295.80
13.25
4.43
C-8.82

Alley BIK #A Warner Villa
Ely of Catalina

(Between Dupont + Pio Pico)

28

INDEXED

MAY 15 1950

2+00

313.11X
298.58
14.53
5.69
C-8.84

B.M.#11
296.71
9.40
306.11X
128
304.83
8.28
313.11X
129
311.82

4+00

0.76%

307.59
11.20
3.38
C-7.87

307.24
11.55
4.00
C-7.55

1+50

306.11X
296.21 T.P.
9.90
128
C-8.62

318.79X
5.43
313.36

3+80 = M.H.#9

307.10
11.69
4.73
C-6.96

1+00

A.50%
A.737%

293.84
12.27
3.59
C-8.68

T.B.M.# 2-P21
313.39

3+50

318.79X
305.69
13.10
5.51
C-7.59

0+50

291.47
14.64
5.75
C-8.89

3+00

A.50%
A.737%

313.11X
303.32 T.P.
9.79
1.29
C-8.50

0+00 = M.H.#5
(P.19)

306.11X
289.10
17.01
8.35
C-8.66

2+50

300.95
12.16
3.37
C-8.79

Alley. BIK. 4 - Catalina Ely.
between Dupont + Pio Pico

5786.95 = D.E.

318.79
308.55
10.24
4.67
C-5.57

5750

308.29
10.50
3.52
C-6.78

5700
0.70%

307.94
10.85
3.04
C-7.81

Easement in P.L. #143 - 10' south of South line Warner Villa Tract. 30
 Catalina - Ely.

2+50
~~313.11~~
~~302.44~~
~~10.67~~
~~2.85~~
 C-7.82

5+00
~~325.75~~
~~309.50~~
~~16.25~~
~~5.99~~
 C-10.26

2+00
~~300.25~~
~~12.86~~
~~5.77~~
 C-7.09
 B.M. #12
~~299.38~~
~~6.07~~
~~305.45~~
~~1.87~~
~~303.58~~
~~9.53~~
~~313.11~~

A+50
 0.70%
~~320.93~~
~~309.15~~ T.P.
~~11.78~~
~~2.68~~
 C-9.10

1+50
~~313.11~~
~~298.06~~
~~15.05~~
~~7.68~~
 C-7.37
~~0.59~~
~~312.52~~
~~8.41~~
~~320.73~~
~~2.68~~
~~318.25~~

4+00
~~308.80~~
~~12.13~~
~~4.13~~
 C 8.00

1+00
~~305.45~~
~~295.87~~
~~9.58~~
~~2.45~~
 C-7.13
~~7.50~~
~~325.75~~

3+95.00 = M.H. #7
~~308.77~~
~~12.16~~
~~4.42~~
 C-7.74

0+50
~~293.69~~
~~11.76~~
~~4.23~~
 C-7.53

3+50
~~320.93~~
~~306.80~~
~~14.13~~
~~6.29~~
 C-7.84

0+00 = M.H. #6
 (P. 20)
~~305.45~~
~~291.50~~
~~13.95~~
~~5.77~~
 C-8.18

3+00
~~313.11~~
~~304.62~~ T.P.
~~8.49~~
~~0.59~~
 C-7.90

Stakes - 5' Left of Φ .

✓ Easement P.L. 143
10' So. side Warner-Villa Tract.

31

7+85.70 = M.H. #8
Ehd of line
311.50
14.25
7.66
C- 6.59

7+50
311.25
14.50
6.57
C- 7.93

7+00
310.90
14.85
5.09
C- 9.76

6+50
0.70
310.55
15.20
4.86
C- 10.34

* 325.75
519
320.56
T.B.M. #1
P21

6+00
310.20
15.55
4.88
C- 10.67

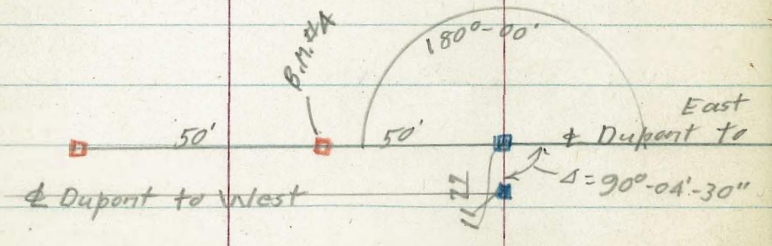
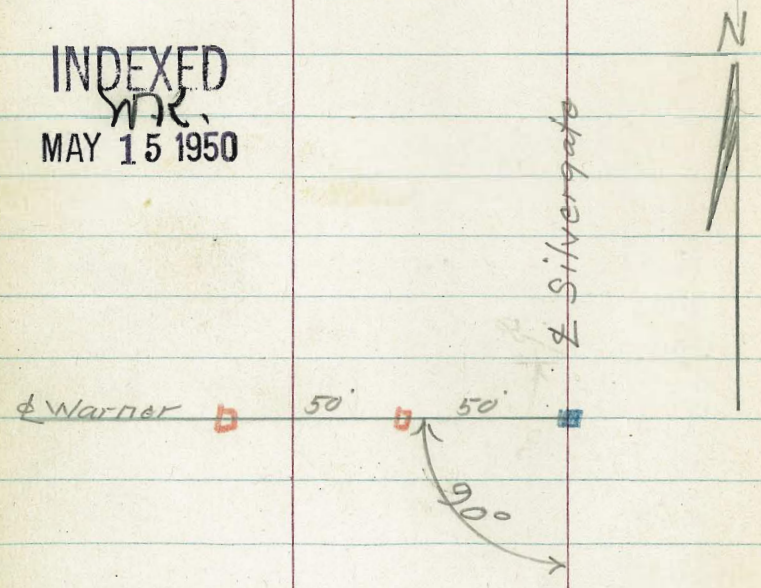
(320.58)

5+50
309.85
15.90
5.19
C- 10.71

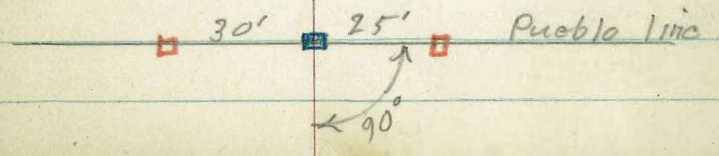
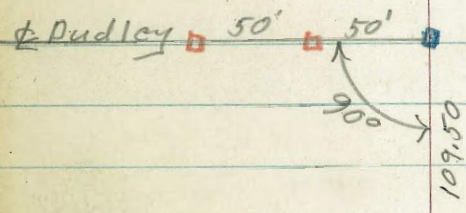
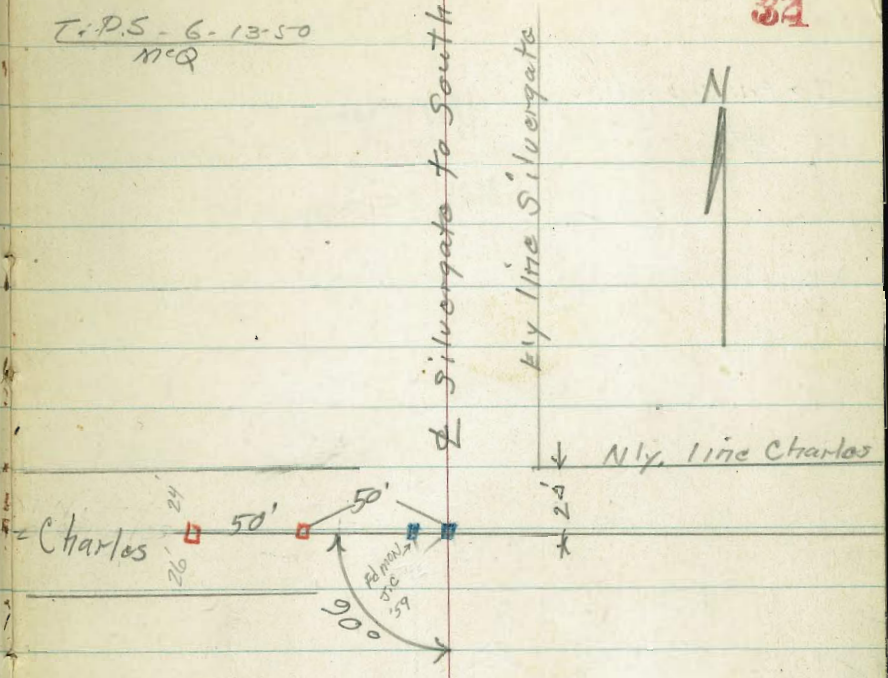
Tie outs - Silvergate.
Dupont to Charles

■ = Ed. Mort.
□ = Set 1/2 disk.

INDEXED
MAY 15 1950



T.P.S - 6-13-50
N^oQ



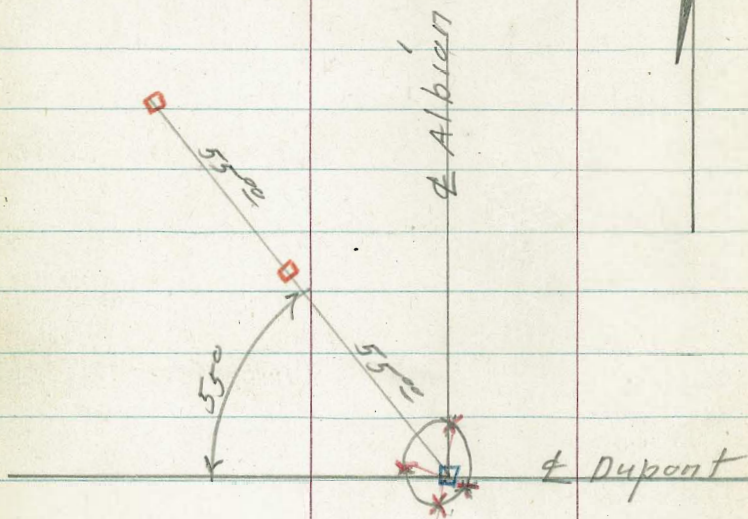
Ties Dupont + Albion

Noted on TP Sheet 6-13-50

□ = Fd. Hub + disk

◻ = Set " " "

INDEXED
MAY 15 1950



Cut 4 crosses in M.H. Rim 4/21/50
Dupont + Albion on intersection of lines of crosses

Ties Albion

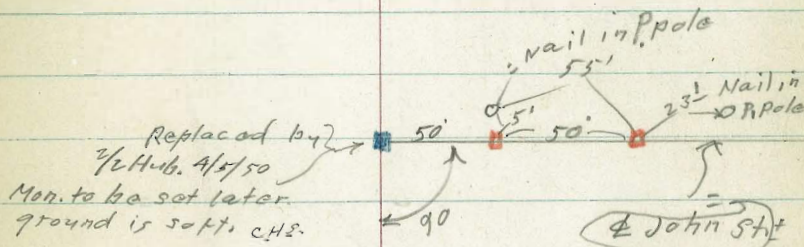
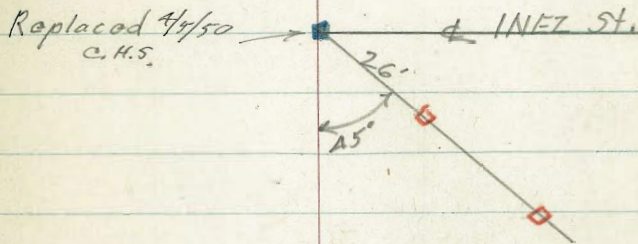
INEZ to Jennings

Noted on TP Sheet - 6-13-50

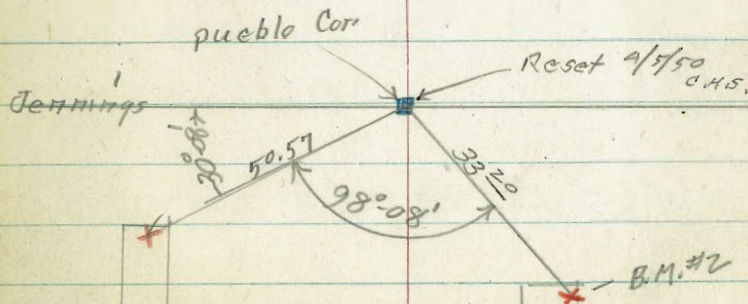
INDEXED

MAY 15 1950

X = Chisel Cross in Conc. Drive



Por. Pit. 183



Ties for Prop. Cors. Alley BIK 3
Pt. Lorna Highlands

Between Wilcox & Charles. streets

INDEXED

MAY 15 1950

- = Fd. Pipe LS# 2201
- = " 2" pipe
- ◻ = set 1/2 + disk

Replaced 4/21/50
1/2 + disk
C.H.S.

Alley

55.00

40.00

○

10.00

15.00

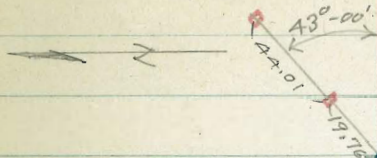
90.00

Catalina Blvd

Ties for Prop. Cors. Portion of P.L. 143 34
North of Rosecraft: T.P. 857 M.Q.
2-13-50

INDEXED

MAY 15 1950



- = Fd. spike
- = Fd pipe
- = Set disk
11' tree 2' above
ground
- ◻ = set 1/2 + disk

Points taken out by
sewer const. were
replaced by 1/2 + disk
4/21/50 (C.H.S.)

86.98

106.98

107.00

107.01

107.02

Catalina Blvd

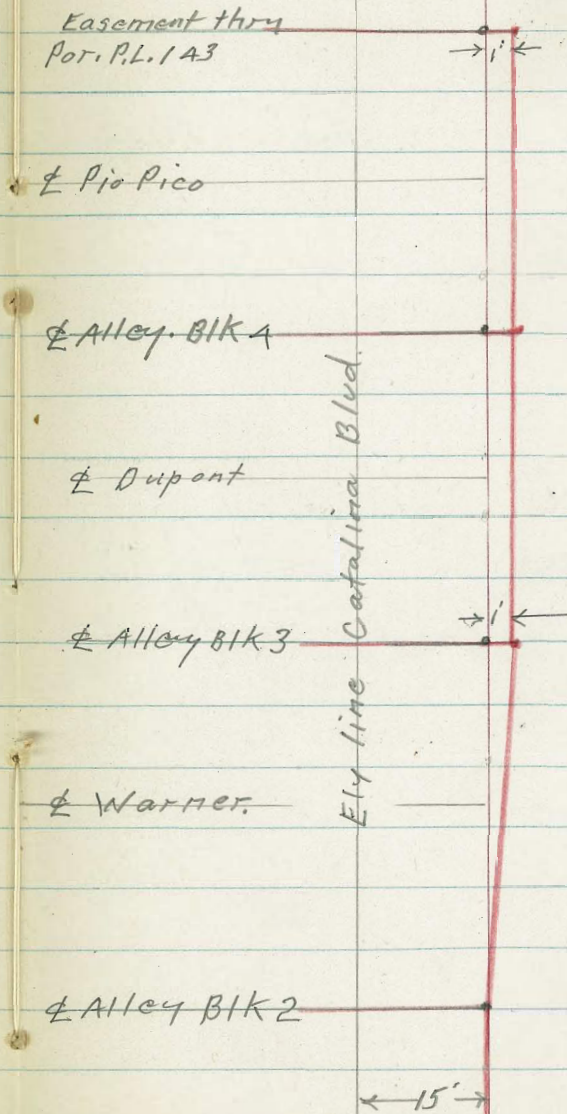
Line change along Catalina Blvd. from

Alley BIK 2 south to easement North of Rosecroft 3/9/50

Line shifted 1' wly. from \pm alley BIK 2, Warner Villas to south end of Catalina Blvd. line. (154^E North of Nly line Rosecroft.)

- = M.H. as per sheet # 1403 D
- • = M.H. as constructed.

INDEXED
MK
MAY 15 1950



Alley BIK 2

WARNER VILLAS.

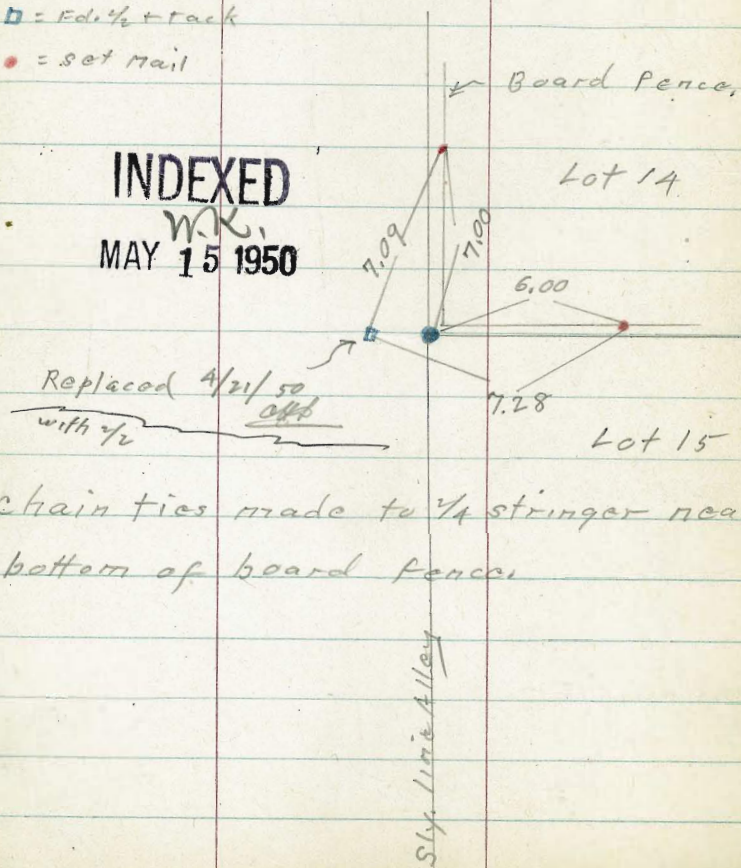
36

Cor. between Lots 14+15 on Nly. line
of lots. This is Sly. line of Alley

- = Fd. $\frac{3}{4}$ " Iron pin
- = Fd. $\frac{1}{2}$ " tack
- = set nail

INDEXED

W.K.
MAY 15 1950



chain ties made to $\frac{1}{4}$ " stringer near
bottom of board fence

Scott St. Benches

INDEXED
 MK
 MAY 15 1950

Set. B.M. #5

4.84 1.64

B.P. Ctr. W.ely. Ret Emerson & Scott

4.73 6.48 - 1.75

↓

spike in pole. S.W. Cor. Emerson & Scott

B.M.#4

P.P. 4.06 5.81 3.62 1.75

N.W. +15' +25' disk Fenelon & Scott

B.M.#3

SS 4.85 0.52

4.86 5.37 6.54 0.51

S.W. 15' +25' disk Scott & Garrison

B.M.#2

SS 5.54 1.51

B.M.#1 4.30 7.05 - 2.75

S.W. B.P. Rosecrans + Garrison

Curb Returns

Dickens & Scott.

INDEXED
MK
MAY 15 1950

B.M.#5 1.64
 484
 648 X
 +.33

 Sub. On X = 6.81

Dickens
E.C.

Elly Ret

Scott
B.C.

	• 1.400	• 12.69	
2.18		2.15	2.10
4.63		4.66	4.71
✓		✓	✓

Dickens
E.C.

Nly. Ret

Scott
B.C.

	• 1.4.00	• 12.68	
2.55		2.49	2.37
4.26		4.32	4.44
✓		X	✓

Scott St.
Dickens to Emerson

39

1+95 = cl. B, C. on east.

1+75 = cl. B, C. on west

0+25 = E.C

0+00 = Nly. line Dickens

Wly gutter

Ely. gutter

$$\begin{array}{r} 6.81 \times \\ 1.14 \\ \hline 5.67 \\ \text{check} \end{array}$$

1.31

$$\begin{array}{r} 6.91 \\ 1.25 \\ \hline 5.56 \\ \checkmark \end{array}$$

2.37

2.10

Scott St.

Emerson to Fenelon
1+75 - Sly line Fenelon,

1+57⁵⁰ line Fenelon.

1+50 = B.C.

B.M. #4 - P.37

1.75
4.06
5.81 π

5.81
33

1+47⁵⁰

Sub. grade π 6.14

1+37⁵⁰

1+27⁵⁰ = P.V.C.

0+00 = E.C. on west

0+20 = E.C. on East

0-25 = Nly line Emerson

West
Cutter

\pm

East
gutter

Set to sub grade
4" pave

40

X 6.14

-0.49
6.57

-0.30
6.44

-0.77
6.91

-0.61
6.75

-0.77
6.91

-0.61
6.75

-0.35
6.49

-0.21
6.35

0.50
5.64

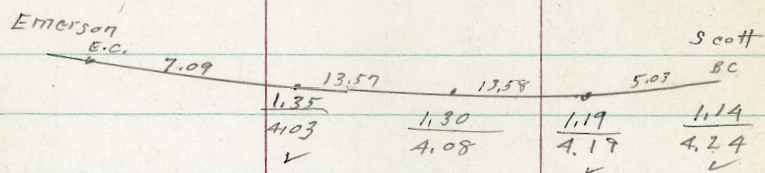
0.50
5.64

0.64
5.50

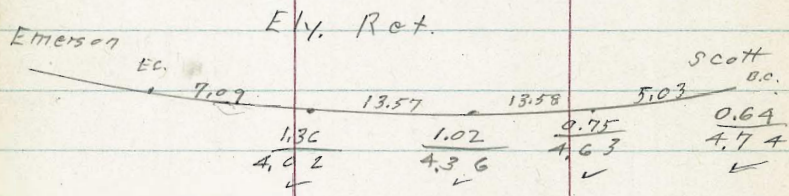
Returns
Emerson + Scott

INDEXED
MAY 15 1950

Sl^y. Ret.



Σ 5.38



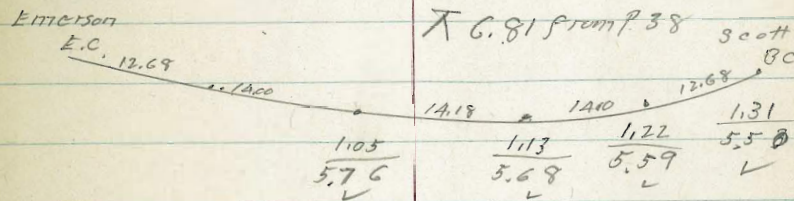
BM #3 = 0.52
4.29
48.17
 $\frac{33}{5.14} = \text{sub Gr. T}$
To Page 43

41

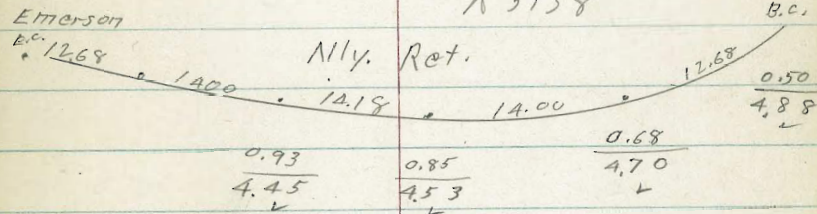
BM #A = 1.75
3.30
 $\frac{5.057}{+ 33}$

sub. Gr. T. = → 5.38

Nl^y. Ret.



Σ 5.38



Scott St.

Fenelon to Garrison

BM#3 - P.37

5.

$$\begin{array}{r}
 0.52 \\
 \hline
 5.29 \\
 5.81 \pi \\
 + 33 \\
 \hline
 6.14 \pi \\
 \text{Sub. Grade}
 \end{array}$$

1+75.25 East.
 1+75 West = O.C.B.C.

W. gutter

±

E. Gutter

$$\begin{array}{r}
 0.70 \\
 \hline
 5.44 \\
 \checkmark
 \end{array}$$

$$\begin{array}{r}
 1.00 \\
 \hline
 5.14 \\
 \checkmark
 \end{array}$$

0+25 = B.C.

$$\begin{array}{r}
 -0.06 \\
 \hline
 6.20 \\
 \checkmark
 \end{array}$$

$$\begin{array}{r}
 0.21 \\
 \hline
 5.93 \\
 \checkmark
 \end{array}$$

0+00 = Nly line Fenelon

$$\begin{array}{r}
 0.10 \\
 \hline
 6.04 \\
 \checkmark
 \end{array}$$

0+30 = Nly line Fenelon

Scott St.

44

Garrison to Harbor Dr.

1+77 = B.C. on West (Lt.)

1.51
4.04
5.55 X
33
5.88
5.26 GrT

W.gutter

2.82

3.06
✓

E.gutter

0+52.1A = Brk.

1.57

4.31
✓

1.57

0+25 = B.C. on Lt. (West)

1.30

4.58
✓

1.30

0+00 = Nly. Garrison

1.26

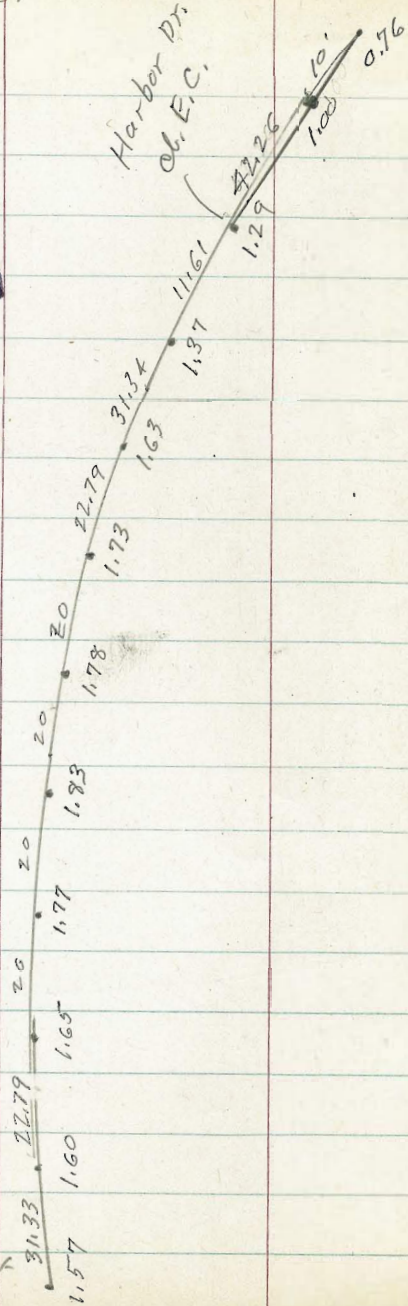
0-15 on East. = Cl. E.C.

1.24

Sly. Ret. Harbor Dr. + Scott

46

INDEXED
MK.
MAY 15 1950



E.C. 52th North of
N. Line Garrison

Fenelon

47

Scott to Rosecrans

2+75 = Ely line Rosecrans

South
Gutter

±

North
gutter

2.33

2.43

~~2+615~~

INDEXED

MAY 15 1950

2+48 = B.C.

1.79

1.99

2+15

1.66

1.83

0+00 = E.C. -25' west of W. line Scott

-0.10

0.00

GARRISON

Scott to Rosecrans

48

2+48 = Exist Pave.

South
gutter

±

North
gutter

1.59

1.92

2+43⁵

INDEXED
MK
MAY 15 1950

1.28

2+25

1.62

1.91

1+95

1.53

1.90

0+175

1.25

1.55

0+00 = E.C. Scott (25' W. W. line Scott)

0.97

1.27

105³' Extension Ely. thru. P.L. 143
Continued from P 21 7/17/50

49

Sommermeier
Begg
Shepard

INDEXED

W.O. 20009

JUL 5 1951

staked to 1+10 to avoid wood
pile pipe will stop at 1+05⁵

Stubs - A' RT. of Φ

BM = I.F.M.H. #68 = 299.04

1+10
300.62
15.99
3.48
C-12.51

9.63 - Boot to ring

7.94

316.61 = π

1+00 8' RT

300.54
16.07
4.36
C-11.71

0+70

300.09
16.52
6.37
C-10.15

0+35

316.61
299.57
17.04
6.90
C-10.14

2 0+00

Now P.O.T.

25+12.71 M.H. 68

From P. 21

299.04

Uppshur Grades

50

Sheet # 7808-L

INDEXED

JUL 5 1951

South

North

	cl.	G.	7/11	±	7/11	G	cl.
	B.M. #1 R.56 19/19/50 $\frac{19.55}{0.24}$ 19.79 X						
2+50	B.M. #1 19.55 $\frac{1.65}{21.20X}$	$\frac{17.67}{2.12}$ 2.22 F0.10	$\frac{17.00}{4.120}$ X	$\frac{17.66}{3.74}$ X	17.72	$\frac{17.74}{3.66}$ X	$\frac{17.43}{3.77}$ X $\frac{18.10}{1.69}$ 1.78 F0.09
2+40		$\frac{17.45}{2.34}$ 2.57 F0.23	$\frac{16.78}{4.42}$ X	$\frac{17.42}{3.98}$ X	17.52	$\frac{17.54}{3.86}$ X	$\frac{17.26}{3.94}$ X 17.93 $\frac{1.86}{1.94}$ F0.08
2+30		$\frac{17.19}{2.60}$ $\frac{2.39}{C0.21}$	$\frac{16.52}{4.68}$ X	$\frac{21.40X}{17.16}$ $\frac{4.24}{X}$	17.27	$\frac{21.40X}{17.30}$ $\frac{4.10}{X}$	$\frac{17.02}{4.18}$ X $\frac{17.69}{2.10}$ 2.43 F0.33
0+20		$\frac{11.67}{8.12}$ $\frac{7.85}{C0.27}$	$\frac{11.00}{10.20}$ X	$\frac{11.64}{9.76}$ X	11.75	$\frac{11.78}{9.62}$ X	$\frac{11.50}{9.90}$ X $\frac{12.17}{7.62}$ 7.58 C0.04
W by Scott 0+00		$\frac{11.15}{8.64}$ $\frac{8.27}{C0.37}$	$\frac{10.48}{10.72}$ X	$\frac{21.40}{10.88}$ $\frac{10.52}{X}$	10.98	$\frac{21.40}{11.03}$ $\frac{10.37}{X}$	$\frac{21.20X}{10.98}$ $\frac{10.22}{X}$ $\frac{11.65}{8.14}$ 7.61 C0.53

Rake

Up stair
Scott to Rosecrans

INDEXED

51

South

JUL 5 1951

North

	cl.	G.	7'4"	±	7'10"	G.	cl.	
	B.M. - P56 19.55 185 <u>21.40</u> X		17.64	18.02 <u>4.39</u> X	18.04	17.97 <u>4.44</u> X	17.45	
Ely. Rosecrans 3400 ⁰²	B.M. 19.55 286 <u>22.41</u> X	18.46 1.33 1354 <u>-0.02</u>	21.20 17.64 <u>3.56</u> X	17.56 <u>3.84</u> X	17.51 <u>3.89</u> X	17.49 <u>3.91</u> X	17.45 <u>3.75</u> X	18.35
2490	17.47 <u>4.94</u>	1.49 <u>1.47</u> CO.01	17.61 <u>3.59</u> X	21.40 17.87 <u>3.53</u> X	17.86	21.40 17.86 <u>3.55</u> X	17.57 <u>3.83</u> X	
2480	18.03 <u>4.38</u> ✓	<u>1.63</u> 1.65 EO.02	17.50 <u>3.70</u> X	18.03 <u>3.37</u> X	18.07	18.04 <u>3.36</u> X	17.63 <u>3.57</u> X	
2470		18.02 <u>1.77</u> 1.70 CO.07	17.35 <u>3.85</u> X	17.90 <u>3.50</u> X	17.98	17.97 <u>3.43</u> X	17.61 <u>3.59</u> X	18.28
2460		17.86 <u>1.93</u> 1.96 CO.17	17.19 <u>4.01</u> X	17.77 <u>3.63</u> X	17.87	17.88 <u>3.52</u> X	17.55 <u>3.65</u> X	Exit Cl. 18.22 <u>1.57</u> 1.54 <u>CO.02</u> ✓

Upstair.
Rosecrans - Westly

52

		cl.	G.	7/11.	F	7/10.	G	cl.
1+44 ⁰²	$\begin{array}{r} 19.55 \\ 8.10 \\ \hline 27.65X \end{array}$	$\begin{array}{r} 25.17 \\ 2.48 \\ 2.72 \\ \hline 20.24 \end{array}$	$\begin{array}{r} 24.50 \\ 2.37 \\ \hline \end{array}$	$\begin{array}{r} 28.75X \\ 24.96 \\ 3.79 \\ \hline \end{array}$	24.98	$\begin{array}{r} 28.75X \\ 24.96 \\ 3.79 \\ \hline \end{array}$	$\begin{array}{r} 24.50 \\ 2.37 \\ \hline \end{array}$	$\begin{array}{r} 25.17 \\ 2.48 \\ 2.17 \\ \hline 20.31 \end{array}$
1+28 ⁰²	$\begin{array}{r} 19.55 \\ 7.32 \\ \hline 26.87X \end{array}$ B.M. = 19.55 $\begin{array}{r} 7.20 \\ \hline 28.75X \end{array}$		23.90	$\begin{array}{r} 24.27 \\ 4.48 \\ \hline \end{array}$	24.31	$\begin{array}{r} 24.27 \\ 4.48 \\ \hline \end{array}$	23.90	
1+14 ³⁰		$\begin{array}{r} 24.00 \\ 3.65 \\ 3.37 \\ \hline 20.28 \end{array}$	$\begin{array}{r} 23.33 \\ 3.54 \\ \hline \end{array}$	$\begin{array}{r} 23.76 \\ 4.99 \\ \hline \end{array}$	23.80	$\begin{array}{r} 23.76 \\ 4.99 \\ \hline \end{array}$	23.33	
0+67 ¹⁵								
0+20			$\begin{array}{r} 19.62 \\ 7.25 \\ \hline \end{array}$	$\begin{array}{r} 20.08 \\ 8.67 \\ \hline \end{array}$	20.12	$\begin{array}{r} 20.08 \\ 8.67 \\ \hline \end{array}$	$\begin{array}{r} 19.61 \\ 7.26 \\ \hline \end{array}$	
Wly. Rosecrans 0+00		$\begin{array}{r} 19.50 \\ 8.15 \\ 8.05 \\ \hline 20.00 \end{array}$	$\begin{array}{r} 26.87X \\ 19.21 \\ 7.66 \\ \hline \end{array}$	$\begin{array}{r} 28.75X \\ 19.56 \\ 9.19 \\ \hline \end{array}$	19.58	$\begin{array}{r} 19.57 \\ 9.18 \\ \hline \end{array}$	$\begin{array}{r} 19.25 \\ 7.62 \\ \hline \end{array}$	19.51

10392

Alley Bik 3 - Carmel Hqts
 Palm to Redwood
 between 33rd & Felton

10031855

INDEXED
 5 1951

53

	West Lt.	East Rt.		West Lt.	East Rt.	SW 7/2 nd Felton + Palm
2+20	0-2' 308.01 5.30 5.01 C-0.29	0-2' 308.01 5.30 5.83 F0.53		4+00	0-2' 309.19 5.32 5.07 C-0.25	0-2' 309.19 5.32 3.94 C-1.38
1+70	0-2' 307.86 5.45 5.08 C-0.37	0-2' 307.86 5.45 5.15 C-0.10	3+80	0-2' 308.85 5.66 4.75 C-0.91	0-2' 308.85 5.66 5.36 C-0.30	305.64 6.22 311.86X 2.90 308.96 4.85 313.31X 2.31 309.00 5.51 314.51X
1+20	A-2' 313.31X 307.71 5.60 4.53 C-1.07	X-2' 313.31X 307.71 5.60 4.31 C-1.29	3+60	A-0.50 314.51X 308.59 5.92 5.57 C-0.35	0-2' 314.51X 308.59 5.92 5.51 C-0.41	
0+70	311.86X N-0.37 307.56 4.30 2.35 C-1.95	311.86X 0-2' 307.56 4.30 3.36 C-0.94	3+40	313.31X 0-2' 308.41 4.90 4.87 C-0.03	313.31X N-0.23 308.41 4.90 4.07 C-0.83	
0+20	N-0.55 307.41 4.45 2.21 C-2.24	0-1' 307.41 4.45 3.58 C-0.87	3+20	0-2' 308.31 5.00 4.83 C-0.17	N-0.09 308.31 5.00 4.17 C-0.81	
Nly Palm 0+00	307.35 4.51	311.86X 307.48 4.38	2+70	0-2' 308.16 5.15 5.33 F0.18	0-2' 308.16 5.15 5.55 F0.40	

Sewer Lat.
Alley Bk 3 - Carmel Hqts. 54

INDEXED

JUL 5 1961

5788⁸⁶

West. L ₁	±	East RT ₁
317.21 X	317.21 X	317.21 X
311.55	311.39	311.65
5.66	5.82	5.56
4.74	5.81	5.1
	0.01	

5780

B-0.50		B-2'
311.84		311.90
5.37		5.31
4.74		4.55
C-0.63		C-0.76

5760

B-1'		B-2'
311.94		311.97
5.27		5.24
4.80		4.40
C-0.47		C-0.84

5740

B-2'		B-2'
311.85		311.86
5.36		5.35
5.31		5.11
C-0.05		C-0.24

5720

B-2'		B-2'
311.57		311.57
5.64		5.64
5.50		5.47
C-0.14		C-0.17

4780

X-2		B-2'
317.21 X		317.21 X
310.77		310.77
6.44		6.44
5.68		5.90
C-0.76		C-0.54

4740

B-2		B-2'
314.51 X		314.51 X
309.98		309.98
4.53		4.53
4.00		4.03
C-0.47		C-0.50

0 + 58⁶⁰ on RT₁ = (S) #1 - FL = 313.31

302.47

10.84

4.80

314.51 X

2.98

311.53

5.68

317.21 X

C-6.04

Alley BLK 2 Univ Hqts
 Univ. to Polk between 44 + Highland

INDEXED

JUL 5 1951

B.M. = Temp B.M. on Ch. $\frac{1753}{52} = \frac{358.42}{3.75}$
 $\underline{359.17}$

End of Job

0 + 9885

West	±	East
0.2'		X-1'
<u>353.14</u>		<u>353.27</u>
6.03		590
<u>4.88</u>		<u>5.21</u>
C-1.15		C-0.67

0 + 4992

0.2'		X-1190
<u>354.07</u>		<u>354.11</u>
5.10		506
<u>4.57</u>		<u>4.31</u>
C-0.43		C-0.75

0 + 00 = Nly. line Univ.

<u>355.00</u>		<u>354.95</u>
4.17		4.22
<u>4.15</u>		
0.02		

Upshur St.
Scott to Rosecrans

Water Meter box grades

Cut or fill on Ely stake to Box
stakes 2' E + 2' W. of Box 3' back of Ch.

INDEXED

JUL 5 1951

R.M.#1
S.W. 7' L + T.
Upshur + Rosecrans
E.L. = 19.55
1.03
20.58X

S.E. End. Ch. 18.46

1 + 68 LT

15.56
5.02
4.59
C. 0.43

N.E. End. Ch. 18.35

2.23
2.25
F002 ✓

1 + 26⁵ LT

14.46
6.12
6.02
C 0.10

0 + 68 LT

12.93
7.65
7.39
C. 0.26

2 + 28 LT

17.14
3.44
3.24
C 0.20

0 + 31 LT

11.96
8.62
8.10
C 0.52

1 + 97 RT

16.82
3.76
4.22
F 0.46

Sewer - in Public R² of way.
Lots 2-3-145 of County Paradise
1-5-51

Sommermaier
Begg
Allen
Burch

sheet 931-D.
G-193 P-77

0.80% Grade

INDEXED
JUL 5 1951

B.M. = I.E. Dardard
0+29+00
EL = 391.04
10.15
401.19 ✓

0+65

391.54
9.65
5.05
C.A. 60

0+30

391.28
7.91
4.97
C. 4.94

0+00 = D.E. 2+55 sheet 931 D EL 391.04

391.04
10.15
✓

Sewer BIK 340 - Old Town.

Alley Kurtz - east of Greenwood

Sommermeier
899
Bunch
Bruner

1-34-51
W.O. 20009

INDEXED

JUL 5 1951

58

0+00 = Existing stub off trunk sewer
150' East of East line Greenwood St.

1+15
- 4.71
11.65
4.38
C-7.27

Laid on 1% grade to give
5' cover at 3+00

1+00
- 4.86
11.80
4.32
C-7.48

B.M. = L++
E Greenwood
Sty. cl. Kurtz
3.02
3.92
6.94X

0+75
- 5.11
12.05
4.60
C-7.45

0+50
- 5.36
12.30
4.58
C-7.72

0+25
- 5.61
12.55
4.58
C-7.97

0+00
- 5.86
12.80
4.82
C-7.98

Alley BIK 99 City Hqts.
Myrtle to Dwight
Between 42 + Van Dyke.

INDEXED

59

JUL 5 1951

				West	±	East		
				= Lt		= Rt.		
Sommermeyer (601 ¹⁸ long) 2-2-51 W.O.# 31833 Begg Sheet # 8029-L.								
Bunch				3+32				
Brucher								
B.M. = N.W. B.P. Myrtle + Van Dyke 326.11								
□ = stub	West	±	East					
N = nail	= Lt		= Rt.					
X = cross in conc.								
0+80 = L.W.C.	N-0.30'			2.20				
	328.60	328.40	328.80	328.77x				
	6.17		5.97	29				
	4.70		5.10	328.08	2+88			
	C-1.47		C-0.87	6.69				
				334.77x				
				2.58				
				332.191				
0+60	N-0.25'		0-2'	6.46				
	328.00	327.80	328.20	338.65x	2+44			
	6.77		6.57	4.37				
	4.77		5.87	334.28				
	C-2.00		C-0.70	6.59				
				340.87x				
0+40	X-2'		0-2'					
	327.00	326.80	327.20	334.77x	2+00 BTK.			
	7.77		7.57	N-1.0				
	6.58		6.22	331.00	330.80			
	C-1.19		C-1.35	3.77				
				2.52				
				C-1.25				
0+20	X-2'		0-2'					
	334.77x		334.77x	330.20	1+60			
	325.60	325.40	325.80	4.57				
	9.17		8.97	3.59				
	6.68		6.69	C-0.98				
	C-2.49		C-2.28					
N. line Myrtle	328.37x		328.37x					
0-01 = P.O.C.	323.70	323.70	323.70	1+20				
	4.67		4.47					
	4.66							
	.01							

Alley Bk. 99 City Hqts

	West = Lt.	±	East = Rt.
5+60 P.U.C.	0-2' 335.60	335.30	0-2' 335.60
	5.27 4.51		5.27 4.70
	C.0.76		C.0.57
5+25	0-2' 335.25		0-2' 335.25
	5.62 5.21		5.62 5.08
	C.0.41		C.0.54
4+90	0-2' 334.90		0-2' 334.90
	5.97 5.50		5.97 5.48
	C.0.47		C.0.49
4+55	0-2' 334.55		0-2' 334.55
	6.32 6.08		6.32 5.92
	C.0.24		C.0.40
4+20 Bk.	0-2' 340.87X 334.20	333.90	0-2' 340.87X 334.20
	6.67 6.62		6.67 6.32
	C.0.05		C.0.35
3+76	0-2' 338.65X 333.56		338.65X 333.60
	5.09 4.78		5.05 4.92
	C.0.31		C.0.13

S. line Dwight
6+00

West = Lt.	±	East = Rt.
335.49	335.22	335.52
5.38		5.35 5.37
		-0.02
0-2' 335.67	335.37	0-2' 335.67
5.20 4.57		5.20 4.55
C.0.63		C.0.65

Morena Blvd. Paue.

Topping Paue Buena to Cushman

A+97t = N.Y. Cushman

61

Sommormeyer
Bagg
Bunch
Bruner

Feb. 5, 1951
No. 20008

4+50

±

west.
edge
✓

INDEXED

JUL 5 1951

0-10
20.46
20.60

F 0.14

Chiselet D in Ely.
and S. Ely. Eb. Ret.

4+00

✓

Morena + Dorcas
Eh = 18.80

Set self reading
Rod on 18.80

0-10
20.53
20.70

F 0.17

1+00

± West
edge
0-10
21.50
21.45
C 0.05
21.50
21.40
C 0.10

3+50

✓

0+50

0-10
22.18
21.30
C 0.88
22.18
21.25
C 0.93

3+00

✓

0-10
20.79
20.80
F 0.01

Sly Buena
0+00

0-10
21.39
21.05
C 0.34
21.39
21.00
C 0.39

2+50

✓

0-10
20.80
20.95
F 0.15

0-60

0-10
23.15
20.80
C 2.35

2+00

20.90
21.30
F 0.40

0-10
20.90
21.10
F 0.20

S
0+110'

1+50

0-10
20.74
21.40
F 0.66
20.74
21.30
F 0.56

Alley Blk. 52
Fairmount Add. to City Hqts.

Alley Blk. 52.
0+00 - Nly line Polk

62

				West	±	East	
Sommertmeyer	INDEXED JUL 5 1951	Feb. 7, 1951		0-0.20 9.67 349.34		0-2' 9.35 349.22	N.W. B.P. 46th + orange.
Beggs		NO. 317A2	2+00	C 0.33		C 0.13	353.94 3.58
Bunch		Street # 8033-L					
Bruner				0-2' 349.09 349.00	1+80	0-1' 9.35 349.10	348.33 3.17
				C 0.69		C 0.25	353.52 3.17
1+35 - Rt. Sewer lat. #1		349.08 349.27 C - 3.81		N-0.10 50.49 349.35	1+50	0-2' 48.95 349.31	4.96 348.56
				C - 1.14		F 0.3 C	= 7' 2" over on station drain nail.
1+26.5	18" conc. pipe storm drain.	349.28 342.10 I.E. C 7.18	349.28 Type "D" C.B. 348.10 = Grate C - 1.18	N-0.10 50.02 348.70	1+20	0-1' 8.85 348.52	T.P. Rock. E.L. = 349.60 set. red.
					C 1.32		C - 0.33
1+00			348.96 341.85 C - 7.11		N-0.33 50.45 348.60	1+00	0-2' 8.94 348.40
					C - 1.85		C 0.54
0+75			348.90 341.60 C - 7.30		0-2' 348.85 348.60	0+80	0-2' 8.87 348.40
					C 0.25		C 0.47
0+50			348.81 341.35 C - 7.46		N-0.15 350.14 348.69	0+50	0-2' 8.81 348.19
					C - 1.45		C 0.32
0+25		348.86 341.10 C 7.46		N-0.10 9.54 348.78	0+20	0-2' 8.61 348.58	
				C 0.76		C 0.03	
0+00		348.60 340.87 = I.E. to North C - 7.73		N-0.11 348.54	0+00	348.43	
± Type "G" Cleanout 26' S. of Nly 1170 Polk.							

	Lt = West	±	Rt = East		Lt = West	±	Rt = East
5+00	3.72 353.87 F 0.14		4.37 353.86 C 0.51				
4+80	0-2' 3.66 353.66 X		0-2' 3.90 353.65 C 0.25	3.28 = Rod set.			
4+60	X-2' 3.39 353.10 C 0.29		0-2' 4.04 353.30 C 0.74				OK on orig B.M. 3.94 = 353.94 = 352.17 Rod set 2.17
4+16	0-2' 2.64 352.45 C 0.19		0-2' 353.48 352.58 C 0.90	T.P. 353.28 Rod set on 3.28			2.17 = Rod T.P.
3+72	0-2' 2.45 351.80 C 0.65		X-2' 2.58 351.87 C 0.71				
3+28	0-2' 5.129 351.14 C 0.15		0-2' 1.45 351.15 C 0.30	orange sly line 5+77	2.47 352.70 F 0.23	2.16 352.40 F 0.24	2.43 352.70 F 0.27
2+84	0-2' 50.65 350.48 C 0.17		0-1' 50.83 350.44 C 0.39	5+60	0-2' 4.00 353.18 C 0.82		0-2' 4.30 353.18 C 1.12
2+40	0-0.10 50.16 349.82 C 0.34		0-1' 50.58 349.73 C 0.85	5+40	0-2' 3.98 353.63 C 0.55		0-2' 3.94 353.63 C 0.31
2+20	0-0.20 9.80 349.55 C 0.25		0-2' 50.07 349.44 C 0.63	5+20	0-2' 3.62 353.86 F 0.24		0-2' 4.12 353.86 C 0.26

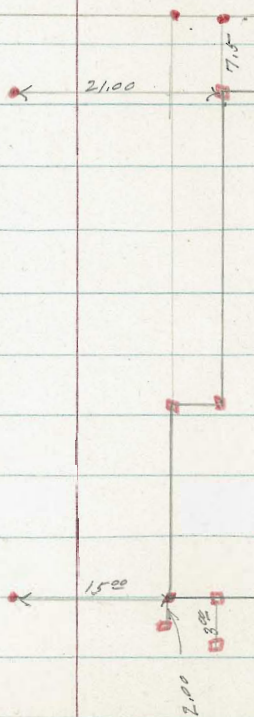
Fire Engine House #5
University at 9th

Feb. 6, 1951
W.O. 20673

Sammermeyer
Boqq
Bunch
Brutter

- = Fd. LAT.
- = set 1/2 hub + tack
- X = out cross in cone.
- = set nail in Pav.

w/ly. 7' line
9th Ave.



INDEXED

JUL 5 1951

64

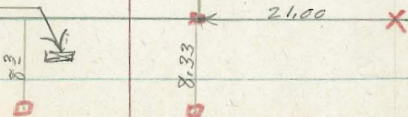
set L + Disk
Also set. EL. = 383.53

B.M. = N.W.C.P. Univ + 9th = 283.76

This L&T. will be taken out
by construction



set 3/4 as B.M.
EL. = 284.50



63.00

w/ly. 7' line
Univ. Ave.

N.E. of L&T.
8th + Univ.

Felspar
Water Meter Box Grades
Noyes to Marrell 3/5/51

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JUL 5 1951

65

Sommertmeyer
Be99
Bunch

W.O. 60020

3+51 S 70.58
1.84
C. 1.26

0+00 = Wly lilia Noyes
cuts from west stub

3+39 N

71.45
2.99
C. 1.54

Lt.
South

Rt.
North

2+87 N

71.24
2.48
C. 1.24

1+00 S

68.56
8.56
C. 0.10

2+70 S 70.25
1.27
C. 1.04

0+75 N

69.05
9.70
C. 0.65

2+35 N

71.11
3.50
C. 2.39

0+42 S

67.39
7.58
C. 0.19

2+29 S 70.08
1.89
C. 1.81

0+25 N

68.05
8.77
C. 0.72

1+80 S 69.78
71.99
C. 2.19

0+07 S

66.67
7.21
C. 0.54

1+75 N

70.72
72.40
C. 1.68

0+04 N

67.67
8.53
C. 0.86

0+01 S

66.52
7.29
C. 0.77

1+25 N

70.03
70.64
C. 0.61

INDEXED

JUL 5 1951

Felspar
Water Meter grades
Noyes to Morrell

66

5403 S

$$\begin{array}{r} 71.15 \\ 1.83 \\ \hline 69.09 \end{array}$$

4469 N

$$\begin{array}{r} 72.00 \\ 1.97 \\ \hline 70.03 \end{array}$$

4422 N

$$\begin{array}{r} 71.80 \\ 1.81 \\ \hline 69.01 \end{array}$$

3484 S

$$\begin{array}{r} 70.72 \\ 70.96 \\ \hline 60.24 \end{array}$$

3469 N

$$\begin{array}{r} 71.57 \\ 2.27 \\ \hline 69.70 \end{array}$$

INDEXED
5 1951

Roselawn Ave.

Curb.

6-Mar-'51

W.O. 31830

67

JUL

3' Back of Ob.

~~START~~ culvert.

0+75³

315.00
A.77
E 0.23

0+50²

319.42
320.82
C 1.40

0+25¹

323.84
29.76
C 5.31

0+00 = Ob. Inlet A

33.00
328.27
C 4.73

0-30[±]

328.87
33.96
C 5.09

41°-57'
Ch. = 11.97
2+50 40°-35' 333.30 - 4' back of Ob.
3.43
9°-33' C 0.13
2+30 31°-02' 333.21
3.16
9°-33' F 0.05
2+10 11°-29' 333.20
3.00
9°-33' F 0.20
1+90 Ch. 25.88 333.29
2.61
F 0.68
1+70 11°-56' 333.47
2.83
Ob 2°-23'-15" Ch. 6.03 F 0.64
1+65 = B.C. 333.52 334.02
2.93
F 0.59
1+32⁵ 3.89
3.81
F 0.08
1+00 - Meet. Ob.
0+50 Meet. Ob. 3
0+00 = wly line Euclid Meet. Ob. 335.85 335.85

0-10' Lt.

0-10' LT
+10' RT.

0-9' back
of Ob.

placed
to existing Ob.

2+90

333.76

334.26
2.48
C 0.22

2+70

~~333.49~~

E.C.
2+59.21
Ob 4°-24'

333.38
3.63
C 0.25

INDEXED

JUL 5 1951

Felspar - Rough grades
Noyes to Morrell

68

	Rough Gr. South		Rough Gr. North		Rough Gr. South		Rough Gr. North
1+40	69.28 <u>71.10</u> C-1.82		70.28 <u>71.45</u> C-1.17	3+00	70.37 <u>72.40</u> C-2.03		71.37 <u>73.08</u> C-1.71
1+20				2+50 ^{0.41%}	70.17 <u>71.00</u> C-0.83		71.07 <u>73.58</u> C-2.41
1+00	68.56 <u>68.53</u> F0.03		69.56 <u>70.00</u> C0.44	2+20	70.05 <u>71.75</u> C1.70		71.05 <u>74.36</u> C-3.31
0+55	67.65 <u>66.96</u> F0.69		68.65 <u>70.04</u> C1.39	2+00			
0+10 = E.C. ch	66.75 <u>66.80</u> C0.05		67.75 <u>9.24</u> C-1.49	1+80	69.78 <u>72.06</u> C-2.28		70.78 <u>73.10</u> C-2.32
W.L. Noyes 0+00	66.50 <u>66.59</u> C0.09		67.58 <u>9.12</u> C-1.54	1+60			

Felspar

69

Rough Cr.
SouthRough Cr.
North.

E Lina Marrell.

5+00

71.15

Meat 06

72.22

Meat 02

A+90

71.15

70.75

F 0.40

72.15

73.45

C 1.30

A+50

70.99

68.48

F 2.51

71.99

2.93

C 0.94

A+00

70.78

69.25

F 1.53

71.78

3.82

C 2.04

3+50

70.58

71.50

C 0.92

70.58

4.18

C 2.60

0.112

P.K

Felspar - Haines to Gresham
water Meters

19-Mar. 1951

Sommermeier
B 899
Wierciszewski

sheet 10A-S-B.

sheets 8321-L thru. 8327-L

F.B. 2108
South

North

B.M. = 7' Men.
S.W. Haines
Felspar.
= 71.21

4+52 S

0.57
60.06
C 0.51

4+00 S

2.51
62.25
C 0.26

3+40 S

5.52
64.78
C 0.74

3+07 S

6.96
66.17
C 0.79

2+44 S

69.69
68.21
C - 1.47

1+91 (D)

71.07
68.72
C - 2.35

0+00 = why line Haines

Gresham to Farnuel

INDEXED

70

JUL 5 1951

South North

5+00 = Fly. Farnuel.

4+98 S

1.37
51.02
C 0.35

4+63 N

2.38
52.34
C 0.04

4+25 N

2.32
52.70
F 0.38

3+41 S

2.52
52.49
C 0.03

3+15 N

3.58
53.73
F 0.15

2+76 S

3.10
53.10
X

2+24 S

3.65
53.59
C 0.06

1+73 S

4.59
54.13
C 0.46

0+98 N

6.60
56.37
C 0.23

0+55 S

5.80
56.08
F 0.28

0+00 = why line Gresham

Felspar (111)
Fauvel to Events

INDEXED
JUL 5 1951

71

3157 S	8.57 <u>47.28</u> C 1.29			
3107 S	9.43 <u>47.72</u> C 1.71			
2156 S	9.45 <u>48.17</u> C 1.28	5070 <u>49.02</u>		
2122 N				
210A S	9.76 <u>48.63</u> C 1.13	C 1.68		
1163 S	50.00 <u>49.00</u> C 1.00			
1125 N		50.95 <u>49.90</u>		
1108 S	50.22 <u>49.47</u> C 0.75	C 1.05		
0188 N		132 <u>50.24</u> C 1.08	4180 S	7.00 <u>46.20</u> C 0.80
0182 S	50.70 <u>49.70</u> C 1.00			
0145 N		148 <u>50.63</u> C 0.85	4140 N	8.00 <u>47.05</u> C 0.95
0126 S	115 <u>50.19</u> C 0.96			
0100 = wly Fauvel			4113 S	8.10 <u>46.79</u> C 1.31

Felspar (W)

Dawes to Cass

$$\frac{FB2108}{.23} \left\{ \begin{array}{l} \text{New } 7\frac{1}{2} \text{ Dawes} \\ + \text{Felspar} = 38.73 \end{array} \right.$$

	South	North
4+17 S	4.57 <u>33.69</u> C 0.88	
3+88 N		5.45 <u>35.90</u> F 0.45
3+67 N		5.70 <u>35.06</u> C 0.64
3+48 S	5.30 <u>34.40</u> C 0.90	
3+05 N		6.20 <u>35.56</u> C 0.64
2+66 N		6.56 <u>35.87</u> C 0.69
1+95 S	5.94 <u>35.76</u> C 0.18	
1+91 N		7.02 <u>36.47</u> C 0.45
1+13 S	6.97 <u>36.49</u> C 0.48	
0+86 S	7.15 <u>35.73</u> C 0.42	
0+76 N		7.85 <u>37.39</u> C 0.46

0+00 = W 1/2 Dawes

INDEXED

JUL - 5 1951

Felspar. Noyas to Morrell
 Curb stakes 20-Mar. '51
 W.O. 31785

B.M. #1 $\frac{2098}{5}$

73.45

2+00	9.94	1.28
	<u>69.94</u>	<u>70.94</u>
	X	C 0.34

1+80	9.88	1.09
	<u>69.78</u>	<u>70.78</u>
	C 0.10	C 0.29

1+60	9.68	0.75
	<u>69.55</u>	<u>70.55</u>
	C 0.13	C 0.20

1+40	9.37	0.26
	<u>69.28</u>	<u>70.28</u>
	C 0.09	F 0.02

1+20	9.09	7.95
	<u>68.95</u>	<u>69.95</u>
	C 0.14	X

1+00 P.V.C.	8.74	9.60
	<u>68.56</u>	<u>69.56</u>
	C 0.18	C 0.04

0+55	7.96	8.75
	<u>67.65</u>	<u>68.65</u>
	C 0.31	C 0.10

0+10 E.C.	7.10	7.82
	<u>66.75</u>	<u>67.75</u>
	C 0.35	C 0.07

Wily. line Noyas	6.89	7.66
0+00	<u>66.50</u>	<u>67.58</u>
	C 0.39	C 0.08

INDEVEN

13

JUL 5 1951

Morrell	N.W. Ret.	Felspar
B.C.		
73.76 - 10.10 #1	13.36 #2 - 13.36 #3 - 10.20 #4 = E.C.	
73.70	73.52	73.70
C 0.11	C 0.42	C 0.16

B.C. Morrell	S.W. Ret.	Felspar
71.70 - 10.20 #1	13.36 #2 - 13.36 #3 - 10.20 #4 = E.C.	
71.70	72.24	72.70
X	C 0.16	C 0.24

Felspar	N.E. Ret.	Morrell
B.C. - 10.20 #1	13.36 #2 - 13.36 #3 - 10.20 #4 = E.C.	
72.15	72.22	72.38
2.22	2.35	2.60
C 0.07	C 0.13	C 0.22

Morrell E.C.	S.E. Ret.	Felspar
S.E. Ret #1 = 10.10 #2 + 13.36 #3 + 13.36 #4 - 10.20 #5 = B.C.		
70.75	70.70	71.07
	1.00	0.93
	C 0.10	F 0.14
		F 0.05
		C 0.02

AT 90 = B.C. 71.15 72.15

Rate

2+20 E.V.C.	9.93	1.25
	<u>70.05</u>	<u>71.05</u>
	F 0.12	C 0.20

Alley BIK.16 Sunset Cliffs
 Sower Laterals (Alhambra)
 Quizot to Fraude (Bet. Osprey &

INDEXED
 JUL 5 1951

FB 1834-41
 Sheet 8352-L
 B.M. SE. B.P. Quizot &
 Osprey 116.34

9892
 6.5
 557

64.51
 3.29
 6780
 5.61
 62.19 - Paue. on so.
 109.59
 0.84
 110.43X
 11.61

3+00.5 #8s

110.43X
 94.31
 116.12
 10.82
 C-5.28
 78.82
 0.72
 99.54
 13.07
 86.47
 1.12
 87.59

2+38 #7s

110.43X
 98.92
 11.51
 4.86
 C-6.65
 12.63
 74.96
 0.85
 75.81X
 11.30
 64.51 = top Hyd. Fraude & Alley

1+80.5 #4N

119.06X
 103.33
 15.73
 9.47
 C-6.26
 6+10.5 #1N

75.81X
 59.49
 16.32
 9.65
 C-6.67

1+20.5 #5N

119.06X
 105.48
 13.58
 8.40
 C-5.18

4+20.5 #2N

99.54X
 83.60
 15.94
 10.77
 C-5.17
 8360
 417
 8877

0+00 = wly Quizot

Alley BIK 16 Sunset Cliffs
 Guizot to Froude
 between Osprey & Alhambra

75

				JUL 5 1951		SE B.P. Guizot + Osprey	
Sommermeyer Boyer Wierciszewski		□ = IXI N = Nail M = scratch or mark on wall X = cross in conc.		N-1'		□ -3'	116.34
			3+30 ⁵	9.00 96.34 C-2.66		4.93 96.34 F 1.41	
				□ -1'		□ -2'	
1+50 ⁵	X-2'	□ -2'	2+80 ⁵	0.79 100.64 C-0.15		1.04 100.64 C 0.40	
	0.50 109.58 C 0.92	0.73 109.58 C-1.15					
				□ -2'		□ -2'	
1+07 ¹	M-0.30 1.25 110.88 C 0.37	□ -2' 0.93 110.88 C 0.05	2+30 ⁵	6.71 104.94 C-1.77		5.47 104.94 C 0.53	
				□ -2'		□ -2'	
0+63 ⁸	M-0.63 2.55 112.18 C-0.37	□ -2' 2.07 112.18 F 0.11	2+10 ⁵	8.15 106.52 C-1.63		7.52 106.52 C-1.00	
				□ -2'		□ -2'	
0+20 ⁵	M-0.65 3.88 113.48 C 0.40	□ -2' 3.74 113.48 C-0.26	1+90 ⁵	7.49 107.82 C-1.67		8.95 107.82 C-1.13	
				M-0.40		□ -2'	
Guizot, 0+00 = wly line	4.22 114.23 ✓	4.22 114.22 ✓	1+70 ⁵	0.42 108.84 C-1.58		10.00 108.84 C-1.16	

5+40 ⁵	M.-1.15 7.90 76.18 C 1.72	M.-0.26 8.30 76.18 C 2.12			
5+20 ⁵	X-2' 9.34 79.06 C 0.28	M.-0.18 0.36 79.06 C 1.30			
5+00 ⁵	X-2' 9.94 81.49 F 1.55	X-2' 1.35 81.49 F 0.14			
4+80 ⁵	X-2' 3.82 83.44 C 0.38	□-2' 4.40 83.44 C 0.96	Ely. line Froude 6+20 ⁵	2.24 62.30 F 0.06 Meet	1.77 61.80 F 0.03 Meet
4+30 ⁵	-0.50 X-on wall 1.01 87.74 C 3.28	□-2' 7.46 87.74 F 0.28	6+00 ⁵	□-2' 9.90 65.64 C 4.32	□-2' 8.47 65.64 C 2.83
3+80 ⁵	M-0.75 2.58 92.04 C 0.54	□-2' 92.00 92.04 F 0.04	5+60 ⁵	□-2' 4.20 72.82 C 1.38	□-2' 4.65 72.82 C 1.83

Felspar.
Ingraham to Haines (W)

S.W. Mon (7)
Haines & Felspar
71.21

3+95 S
70.00
69.84
C 0.16

3+26 S
7.98
69.40
C 0.58

2+60 S
70.10
68.97
C 1.13

2+11 S
9.86
68.66
C 1.20

1+57 S
9.60
68.32
C 1.28

1+12 S
9.30
68.03
C 1.27

0+28 S
8.99
67.49
C 1.50

0+00 = wly. Ingraham.

A+59
69.72
70.24
F 0.32

A+11 S
9.90
69.94
F 0.04

72
IMPROVED
JUL 5 1951

EMERALD ST.
Water Meter Grades

Everts to Dawes

Sommermeier
Boggs
Wierciszewski

21-Mar, 51

B.M. = 7' disk S.W.
Dawes + Emerald
A.F. 08 - F.B. 2108
10
Self reading rod.

INDEXED 78
JUL 5 1951

2+77	N.		<u>0.58</u> 49.42
2+42	S.	50.10 49.1A C 0.90	C-1.16
1+75	S.	1.46 49.96 C-1.50	
1+70	N.		2.48 51.00
1+53	S.	1.48 50.26 C 1.22	C 1.48
1+47	S.	1.46 50.34 C-1.12	
1+38	N.		3.00 51.46 C-1.54
0+67	N.		3.28 52.50
0+34	S.	2.15 52.02 C 0.13	C-0.78

0+00 = wily line Everts

A+59	S.	6.65 46.18 C 0.47
A+17	N.	8.35 47.37 C 0.98
A+12	S.	6.95 46.82 C 0.13
3+77	S.	7.30 47.30 x
3+67	N.	8.85 48.10 C 0.75
3+28	N.	9.35 48.67 C 0.68
2+98	S.	9.00 48.37 C 0.63

Construction Benches

£ Mon Albion + Jennings	(B.M.#10 1699 61)	263.97 = B.M.#1
Cross in conc. Drive 33.20 S.Ely £ Albion + Jennings (P.3)		264.43 = B.M.#2
Mon. 84' Ely. line Albion on S. line Charles P.5A.		270.76 B.M.#3
50' Wly. R.P. Dupont + Silvergate (on Hub.)		292.84 = B.M.#4
Iron pin 5' RT. sta. 380' (P.26) (B.M. set on P.-12) Alley BIK 2. Wly.		305.28 = B.M.#5
3 Nails in post + Silvergate + Jennings Pole # R.3601		274.20 B.M.#6
Nail £ Catalina + 2' soil £ Alley between Wilcox + Charles (P.16)		262.74 B.M.#7
Spike £ Charles £ Catalina P.16		265.90 B.M.#8
Spike £ Pudley + £ Catalina P.17		272.19 = B.M.#9
Spike £ Warner + £ Catalina P.18.		286.03 = B.M.#10
Spike £ Dupont + £ Catalina P.19.		296.71 = B.M.#11
" £ Pio Picot - £ Catalina P.19		299.38 = B.M.#12
		(299.63) 0.25

Entire Catalina line is 0.25 low as
compared with line on Silvergate.
Difference is in starting benches

Index Cont.

79

Felspar. Morrill. obs.	73
Alley BIK 1.6 Sunset Cliffs Sewer Lats	74-77
Emerald. (W) Everts to Dawes	78

Contractor - Carter
Supt. - Wing
Foreman - Angelo

Schmidt

63.77
19.70
44.07

320
128.30

47

320

940

141

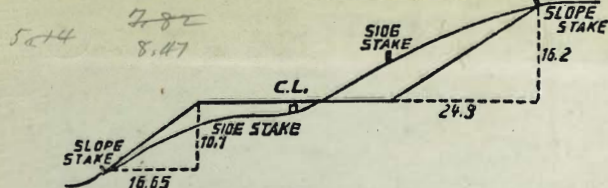
750.40

252.85
109.10
143.35

9.50
6.35

7.65
6.94
71

856
675
1539
765



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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