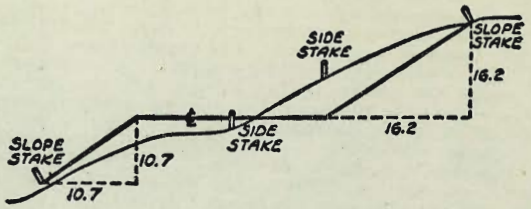
G-268

BANK BOOK



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Index

01

PASEO DORADO.

Ch. = Chimney WO 31720

See P 42 for restake 5/29/50

BM #8 P. 75
7.67
2.91
10.58 ✗

1+00	-8.36 18.94 5.04 C 13.90	
0+75	-8.44 19.02 5.67 C 13.35	
0+50	-8.51 19.09 5.28 C 13.81	
0+25 0.39Q	-8.59 19.17 4.70 C 14.47	
0+05	-8.65 19.23 4.51 C 14.72	
Exist D.M.H. #43 0+00 Δ 85°-19' in N.W.	-8.66	

1+80± = Ch.

1+75	-8.14 18.72 4.73 C 13.99
1+60±	-8.18 18.76 4.88 C 13.88
M.H. #1 1+55 40± Δ 34°-26' Lt.	-8.19
1+50±	-8.21 18.79 4.95 C 13.84
1+25 0.30Q	-8.29 18.87 5.17 C 13.70

✓ Paseo Dorada

			Lt.	Rt
3+00	-7.76 18.34 5.45 C-12.89		M.H. #2 A+03.55 Δ 26°-23' Rt.	-7.45	8.75 X -7.45
2+80 ± = Ch.			3+98.55	-10.58 X -7.46 18.04 6.04 C 12.00	X 10.58 604 4.54 4.21 8.75 X
2+75	-7.84 18.42 5.16 C 13.26		3+80 ± Ch.		
2+50	-7.91 18.49 4.91 C-13.58	0.30%	3+75	-7.54 18.12 5.99 C-12.13	0.30%
2+25	-7.99 18.57 4.78 C-13.79		3+50	-7.61 18.19 5.87 C-12.32	12.32 7.61 4.71 = Pave EL.
2+00	-8.06 18.64 4.70 C-13.94		3+25	-7.69 18.27 5.73 C-12.54	

Paseo Dorado

5+00	-7.16	-7.16	6+47.24	-6.71	8.75 x -6.71 15.46 6.19 C-9.27
	15.91	15.91		15.46	
	4.87	5.40		C.11	
	C-11.04	C10.51		C-9.35	
4+80.55 = Ch.			6+25	-6.83	-6.83
				15.58	15.58
				5.93	5.99
				C-9.65	C-9.59
4+75	-7.24	-7.24	6+00	-6.89	-6.89
	15.99	15.99		15.64	15.64
	4.66	5.25		5.74	5.85
	C-11.33	C-10.74		C-9.90	C-9.79
4+50	-7.31	-7.31	5+75	-6.95	-6.95
0.30 90	16.06	16.06	0.30 90	15.70	15.70
	4.49	4.82		5.47	5.76
	C-11.57	C-11.24		C-10.23	C-9.94
4+25	-7.39	-7.39	5+50	-7.02	-7.02
	16.14	16.14		15.77	15.77
	4.24	4.47		5.30	5.66
	C-11.90	C11.67		C-10.47	C10.11
4+08.55	-7.44	-7.44	5+25	-7.09	-7.09
	16.19	16.19		15.84	15.84
	4.11	4.31		5.69	5.55
	C-12.08	C-11.88		C-10.76	C-10.29

✓ Pasco Dorado

6

BM #9
2.12
4.51
6.63 ✓
4.79
1.84
B.M. #10 1.85
.01 ✓

7+50 — X
-6.41
13.04
5.47
C-7.57

7+25
-6.49
13.12
5.07
C 8.05

7+00
-6.56
13.19
4.64
C-8.55

0.30%

6+75
-6.64
13.27
4.29
C-8.98

6+57.24
6.63 ✓
-6.69
13.32
4.15
C-9.17

6+57.24 M.H. #3
-6.70
023°-24'-30" Rt.

9+00
-5.96
12.59
5.71
C-6.88

X-4' Rt.

8+75
-6.04
12.67
5.75
C-6.92

□ 5 Rt.

8+50
-6.11
12.74
5.20
C-7.54

□ 5' Rt

8+25
-6.19
12.82
5.15
C-7.67

□ 5 Rt

8+00
-6.26
12.89
5.19
C-7.70

□-5 Rt

7+75
-6.34
12.97
5.10
C-7.87

✓ Paseo Dorado

✓ 7

10+52 81	-5.50	11+50	-5.21
	12.13		12.09
	5.23		5.17
	C-6.90		C-6.92
10+25	-5.59	11+25	-5.29
	12.22		12.17
	5.26		5.20
	C-6.96		C-6.97
10+00	-5.66	11+00	-5.36
	12.29		12.24
	5.34		5.29
	C-6.95		C-6.95
9+75	-5.74	10+75 0.30 Q/O	-5.44
	12.37		12.32
	5.44		5.31
	C-6.93		C-7.01
9+50	-5.81	10+62 81	-5.47
	12.44		
	5.50		
	C-6.94		
9+25	C.C3 π	10+57 81 M.H. # 4	6.88 π
	-5.89	~~Pavt.~~ 17 ½	-5.48
	12.52		12.36
	5.57		5.29
	C 6.95		C-7.07

B.M. # 10
1.85
5.03
6.88 π

✓ Paseo Dorado

		6.88 ℄ 1.88 5.00 11.99 16.99 ℄
12+68.85 M.H.#5 Δ 33°-50' Lt.	~~-4.85~~ ~~11.73~~	
12+63.85	-4.86 11.74 4.51 C-7.23	
12+50	-4.91 11.79 4.65 C-7.14	
12+25 0.30 ↓	-4.99 11.87 4.80 C-7.07	
12+00	-5.06 11.94 4.93 C-7.01	
11+75	6.88 ℄ -5.14 12.02 5.05 C 6.94	

Spindrift ✓

Drop. M.H.
13+67.83 M.H.#5A -4.54 | -3.04
Δ 50°-12' Lt.

13+62.83	-4.55 21.54 11.29 C-10.25	Rt 21.54 11.44 C-10.10
13+50	16.99 ℄ -4.61 21.60 11.89 C-9.71	Rt 21.60 11.99 C-9.61
	X in ch. 3' Lt. 6.88 ℄.	
13+25 0.31 ↓	-4.69 11.57 2.74 C-8.83	Rt. 11.57 3.00 C 8.57
13+00	-4.76 11.64 4.06 C-7.58	Rt 11.64 3.93 C-7.71
12+73.85	-4.84 11.72 4.46 C 7.26	Rt. 11.72 4.45 7.27

Spindrift.

B.M.#2-P75
13.31
12.63
25.94 π
0.20
25.74
15.17

14+75 2.47

15+75 9.56

14+50 + 1.18
15.81
7.08
C-8.73

15+50 7.33
18.61
8.38
C 10.23
8.92%

7.33
18.62

14+25 - 0.11

15+28.90 5.45
20.49

5.15-90

14+00 -1.38
18.37
9.46
C-8.91

15+23.90 M.M.#6 25.94 π
Δ 2°-17' Rt. 5.00
20.94
10.89
C 10.05

16.99 π
5.00
11.99
1.97
C-10.02 ✓ 0.03

13+75 -2.67

15+18.90 4.74

13+72.83 16.99 π
-2.78
19.77
10.87
C-8.90

15+00 16.99 π
3.76
13.23
4.31
C-8.92

Spindrift

25.74 B.P.
11.22.
36.96 π
0.25
36.71
12.93
49.64
12.21
37.43 =
S.E. B.R.
St. Louise for.
+ Spindrift.
37.42 2019/14

37.42
12.21
49.63 π

	16+69	17.90 19.06 7.71 C 11.35		17+76.32 M.H.#8 Δ 1°-48' Lt.	26.60	
1	16+64 ○ M.H.#7 Δ 36°-19 Rt.	17.50		17+71.32	36.96 π 26.19 10.77 0.70 C 10.07	
1	16+59 ○	17.05 19.91 8.24 C 11.67		17+50	24.46 12.50 1.41 C 11.09	
1	16+50	36.96 π 16.25 20.71 8.11 C 11.60		17+25	22.44	
1	16+25	14.02		17+00	20.41 16.55 3.45 C 11.10	
13	16+00	25.94 π 11.79 14.15 3.31 C 10.84		16+75	18.39	

Spindrift

49.63 – P16
0.43
49.20
11.55
60.75 ★
6.11
54.64 =
21+10.07 2019.15
54.64
54.64
11.20
65.84 ★

19+00
32.54
17.09
6.42
C-10.67

18+75
31.34

18+50
30.14
19.49
9.53
C-9.96

18+25 At 8 0/0
28.94

18+00
27.74
21.89
12.49
C-9.40

13 17+81.32
49.63 ★
26.84
22.79
13.10
C 9.69

60.75 ★
39.74
21.01
8.78
C-12.23

20+50

20+31.97 = ch.

20+25
38.54

20+00
49.63 ★
37.34
12.29
0.43
C-11.86

19+75 At 8 0/0
36.14

19+50
34.94
14.69
3.49
C-11.20

19+25
33.74

To M.H. #9.

Spindrift

		65.84 P.11
		0.77
		64.87
		9.14
		74.01
21+50	65.84	
	48.67	
	17.17	
	7.63	
	C-9.54	
1.4%		
21+25	67.22	
	48.32	
	18.90	
	10.95	
	C-7.95	
21+01.97	65.84	
	48.00	
	17.84	
	11.24	
	C 6.60	
Drop.		
20+96.97 M.H.#9	41.99	47.93
Δ 16°-00' Lt.		
20+91.97	60.75	
	41.75	
	19.00	
	6.80	
	C 12.20	
4.8%		
20+75	40.94	

		Δ · P.11
		54.64
		12.58
		67.22
22+75	67.22	
	50.42	
	16.80	
	1.13	
	C-15.67	
22+50	65.84	
	50.07	
	15.77	
	0.97	
	C-14.80	
22+26.97 = Ch.		
22+25	67.22	
	49.72	
	17.50	
	3.78	
	C-13.72	
1.4%		
22+00	65.84	
	49.37	
	16.47	
	4.05	
	C-12.42	
21+75	67.22	
	49.02	
	18.20	
	7.13	
	C-11.07	

Spindrift

24+00

52.17
21.84
5.68
C-16.16

23+75

23+62.8 = ch.

23+50

51.47
22.54
6.03
C-16.51

1.4%

23+25

23+00

74.01
50.77
23.24
7.01
C-16.23

25+00

60.43
13.58
4.92
C-8.66

24+75

1.4%

24+67.80

60.06
13.95
5.47
C-8.48

Drop.

24+62.8 = M.H. #10

Δ 53°-34' Lt.

53.05 - 60.00

24+57.8

1.4%

24+50

52.98
21.03
5.82
C-15.21

52.87
21.14
5.76
C-15.38

Spindrift

26+24.37

~~26+34.37~~ out — 61.96 / 17.05 / 4.68 / C-7.37 — 62.03 / 18.30 / 11.12 / C-7.18

Δ 9°-14'-44"
26+19.37 = M.H. #11 — 61.79 = New EL.

26+14.37 — 61.73 / 18.60 / 11.43 / C-7.17

Stub
26+00 — 61.57 / 12.44 / 5.12 / C-7.32

1.14%

25+75 — Line Change 4-6-50

26+44.37 = I.E. 62.27 / out = 7.40 / Elb Nail = 69.67 / 10.66 / 80.33 A

25+50 — 61.00 / 13.01 / 4.72 / C-8.29

25+25

Princess

27+25

27+00 — out: ~~74.01~~ / ~~65.18~~ / 8.83 / 2.11 / C-6.72 — T.P. 65.72 / 14.61 / 8.37 / C-6.28

~~5.23%~~ / ~~4.88%~~

26+75

26+50 — out: ~~62.57~~ / 11.44 / 4.14 / C-7.30 — 63.28 / 17.05 / 10.34 / C-6.71

~~26+44.37~~ out — 62.27 / 11.74 / 4.34 / C-7.40

26+39.37 M.H. #11 — 62.01
Δ 10°-06' Rt.
26+19.37 = New location M.H. #11 = 9°-14'-44"
Changed 4/6/50
To miss water line

Princess St.

℄ = End of line		✓ ok.	
28+49.37 M.H. #12	72.99	72.99	✓ 74.01 ℸ
	11.62	7.34	2.11
	4.46	0.18	71.90
	C-7.16	C-7.16	12.71
			84.61 ℸ
~~28+44.37~~			
28+25			
28+00	out		
~~4 88%~~	~~70.41~~		70.60
	~~14.20~~		9.73
	~~7.20~~		2.90
	~~C-7.00~~		C-6.83
27+75			
	out		
	~~84.61 ℸ~~		
27+50	~~67.80~~		68.16
	~~16.81~~		12.17
	~~10.03~~		5.71
	~~C-6.78~~		C-6.46

ROSELAND DRIVE

1+00
11.20
14.75
7.79
C- 6.96

0+75
9.65

0+50
8.10
17.85
9.98
C- 7.87

0+25
6.55
19.

0+05
25.95 ℄
5.31
20.64
10.38
C- 10.26

0+00 = M.H #6 (A99)
81°27'Lt. off Fwd. Tang.
Spindrift
5.00
20.95

BM #2
13.31
12.64
25.95 ℄
-0.75
25.20
+12.78
37.98 ℄

2+50
37.98 ℄
20.50
17.48
9.96
7.52

2+25
18.95

2+00
25.95 ℄
17.40
8.55
1.75
C- 6.80

1+75
15.85

1+50
14.30
11.65
5.04
C 6.61

1+25
12.75

Roseland Dr.

3+71.85 = M.H. #23
P.O.T.

37.98 T.
28.05
9.93 T.P.
0.27
C-9.66

3+62

27.48 check.
10.50
0.90
C-9.60

3+50

26.70
11.28
1.84
C-9.44

3+25

6.20 D/O

25.15

3+00

37.98 T
23.60
14.38
5.71
C-8.67

2+75

22.05

49.58 T

5+00

35.75
13.83
4.49
C-9.34

37.98
-27
37.71
11.87
49.58

4+75

34.25

4+50

32.75
16.83
7.00
C 9.83

6.10

4+25

31.25

4+00

29.75
19.83
10.00
C-9.83

3+76.85

49.58 T
28.35
21.23
11.52
C-9.71

V Rosecland Dr.

5+92.25 3.10%	60.54 T 41.18 19.36 17.00 C 8.36	49.58 T 0.38 49.20 11.34 60.54 T
5+87.95 M.H.24 Δ - 40-31' Rt.	41.02	
5+82.95	49.58 T 40.73 8.85 0.38 C - 8.47	
5+75	40.25	
5+50 6%	49.58 T 38.75 10.83 1.95 C - 8.88	
5+25	37.25	

End: Plug 7+47.95	60.54 T 45.98 14.56 5.21 C - 8.35
7+25	45.27
7+00	44.50 16.04 7.78 C - 8.26
6+75	43.72
6+50 3.10%	42.95 17.59 9.42 C - 8.17
6+25	42.17
6+00	41.40 19.14 10.75 C - 8.39

Easement (Por. PL 1285)
South of Roseland Dr.

Line set 5' Nly. 4/18/50

BM = 3776.85
G268
17
EL = 38.06
+ 11.63
49.69 ℄
119

0+75		~~38.70~~	49.69 ℄ 38.30 11.39 1.19 C 10.20	48.50 10.65 59.15 ℄		
0+50		~~35.20~~	34.80 14.89 5.02 C- 9.87		Plug 1+70	~~52.00~~	59.15 ℄ 51.60 7.55 0.94 C- 6.61
0+25	1A 0/0	~~31.70~~	31.30		1+50	~~49.20~~	48.80 10.35 2.48 C- 7.87
0+10		~~29.60~~	49.69 ℄ 29.20 20.49 13.10 C- 7.39		1+25	~~45.70~~	59.15 ℄ 45.30 13.85 4.74 C- 9.11
0+00 = M.H. # 23 57°-55' off back tang. (P. 17)		~~28.20~~	27.80		1+00	~~42.20~~	59.15 ℄ 41.80 17.35 7.55 C- 9.80

Ties - P. 41

Hypatia Dr.
S.Wly. off Roseland

BM = TP #3
G 268
31

49.03
10.92
59.95 ℄
0.49
59.46
12.63
72.09 ℄
- 1.62
TP #1 70.47
6.44
76.91 ℄
7.05
69.86 = 1+30
5'RT. G 268
31
(69.82)

0+75
48.53
5'LT. TP #1 = 1.62
TP #1

0+50
5'RT
46.09
13.86
6.81
C - 7.05

59.95 ℄
46.09 LT
13.86
6.19
C - 7.67

9.76 ℄/0

0+25
43.65

0+05
5'RT
41.70
18.25
10.93
C - 7.32

59.95 ℄
41.70 LT
18.25
10.44
C - 7.81

5'RT
41.70
7.88
.56
C 7.32

0+00 = M.H. #24
70°06' off Back Tang.
(P-18)
41.21

2+15
72.09 ℄
62.19
9.90
1.62
C - 8.28

2+00
60.73
11.36
2.54
C - 8.82

1+75
58.29

1+50
55.85
16.24
6.86
C - 9.38

9.76 ℄/0

1+25
53.41

1+00
72.09 ℄
50.97
21.12
12.01
C - 9.11

✓ Hypatia - S.wly from Roseland

Line change 4/18/50

= plug.

3+10 = End

	76.91 T	
	64.03	64.03
	12.88	13.02
	5.09	5.12
	C- 7.79	C 7.90

3+00

63.88	
13.63	
4.93	
C 8.10	

2+75

63.51	63.51
	13.54
	4.78
	C-8.76

2+50 1.50 %

63.13	63.13
13.78	13.92
5.01	5.10
C- 8.77	C-8.82

2+25

76.91 T	
62.76	62.76
14.15	14.29
5.82	5.98
C- 8.33	C-8.31

2+20 = M.H. #21

~~Δ 6°00' Rt.~~

Δ 10° Rt.

76.91 T
62.68

2+15 Brs = 62.19

cut 8.28

70.47

6.58

77.05 T

St. Louis Terrace.

1+00	34.48 15.12 6.88 C- 8.24	B.M.#3 37.42 12.18 49.60 X 0.43 49.17 12.51 61.68 X	2+41.55	45.47 16.21 7.88 C- 8.33	
0+75	32.54		2+25	44.18	
0+50	30.60 19.00 10.51 C- 8.49		2+00	61.68 42.24 19.44 10.61 C- 8.83	
1.76 90			1.76 90		
0+25	28.66		1+75	40.30	
0+05	49.10 X 27.11 22.49 12.72 C- 9.77		1+50	49.68 X 38.36 11.24 2.02 C- 8.22	
0+00 = M.H.# 8 Spindrift (P.10)	26.72		1+25	36.42	

St. Louis Terrace

✓ 23

3+50

61.68 ↗
53.10
8.58
1.61
C. 6.97

61.68 ↗
0.04
61.64
12.39
74.03 ↗

3+25

51.35

3+00

49.60
12.08
5.53
C-6.55

7%

2+75

47.85

2+51.87

61.68 ↗
46.23
15.45
7.56
C-7.89

2+46.87 M.H #16
Δ 11°-52' Lt.

~~61.68 ↗~~
~~45.88~~
~~15.80~~
~~7.56~~
~~C-7.24~~

4+25

58.48

7.80%

4+13.57

74.03 ↗
57.60
16.43
8.73
C-7.70

4+08.57 = M.H #17
Δ 21°-28' Lt.

57.20

4+03.57

56.85
17.18
9.56
C-7.62

4+00

74.03 ↗
56.60
17.43
9.87
C-7.56

7%

3+75

54.85

St. Louis Terrace

Torrey road.

5+72.00 = M.H. #18		69.95 6'	B.M. #5 77.25 5.75 83.00 ↗
5+66	5' Lt.	83.00 ↗ 69.48 13.52 5.97 C-7.55	
5+50	5' Lt. 68.23 14.77 6.35 C-8.42	68.23	
5+25		66.28	
5+00	5' Lt. 83.00 ↗ 64.33 18.67 10.29 C-8.38 1.80 ↘	64.33 (5' Rt) 9.70 1.24 C-8.46	check Lt. out. 64.33 9.70 1.31 C-8.39 8.38 0.01 ✓
4+75		62.38	
4+50		74.03 ↗ 60.43 13.60 5.67 C-7.93	

Torrey Road
West from St. Louis Terrace.

1+00	88.06 ℄ 75.65 12.41 0.37 C 12.04	
0+75	74.25 13.81 3.98 C- 9.83	
0+50	72.85 15.21 7.13 C- 8.08	
0+25	71.45 16.61 9.69 C- 6.92	
0+06	88.06 ℄ 70.39 17.67 10.54 C- 7.13	
0+00 = M.H. #18 (P.24)	7005	

5-6 0/0

End. 2+24 70 M.H. #15	95.68 ℄ 82.63 13.05 4.02 C- 9.03	B.M. #5 - 878 77.25 10.81 88.06 ℄ 37 87.69 7.99 95.68 ℄
2+00	81.25 14.43 4.65 C 9.78	
1+75	79.85 15.83 4.51 C- 11.32	
1+50	78.45 17.23 4.23 C 13.00	
1+25	95.68 ℄ 77.05 18.63 5.25 C- 13.38	

5-6 0/0

Torrey Road

East from St. Louis Terrace.

1+00	83.00 ℄ 73.41 9.59 2.50 C - 7.09	℄ from P. 24 83.00 0.35 82.65 9.71 92.36 ℄ 2.18 90.18
0+75	72.54	
0+50	71.68 11.32 4.65 C - 6.67	
0+25 (3.46 90)	70.81	
0+05	70.12 12.88 5.70 C - 7.18	
0+00 = M.H. # 18 (P 24)	83.00 ℄ 69.95	

2+50	92.36 78.60 13.76 4.53 C - 9.23
2+25	77.13
2+00	76.87 15.49 7.11 C - 8.38
1+75 (3.46 90)	7600
1+50	92.36 ℄ 75.14 17.22 9.71 C - 7.51
1+25	74.27

✓ Torrey Road
East of St. Louis Terrace -

3+05 = M.H. #19. 80.50
11.86
2.02
C - 9.84

3+00 80.33
12.03
2.11
C - 9.92

3.46%

2+75 79.46

Viking Way

1+00
65.52 ✗
52.76
12.76
0.35
C-12.41

0+75
51.07
14.45
3.42
C 11.03

0+50
6.75 %
49.38
16.14
6.92
C-9.22

0+25
47.69
17.83
10.31
C-7.52

0+05 32
65.52 ✗
46.36
19.16
11.73
C-7.43

0+00 = M.H.#16
(P.23)
46.00

2+50
77.94 ✗
62.90
15.04
4.91
C-10.13

2+25
61.21
16.73

2+00
59.52
18.42
6.56
C-11.86

1+75
57.83
20.11

1+50
56.14
21.80
8.62
C-13.18

1+25
77.94 ✗
54.45
23.49
10.15
C-13.34

B.M.#3-P75
37.42
12.48
49.90
8.77
49.13
11.36
60.49
5.50
54.99 B.M.#4
Chisel X and S.E.Ch.Rot.
Viking Way + St Louis Ter.

B.M.#4 54.99
10.53
65.52 ✗
0.34
65.18
12.76
77.94 ✗

Viking Way

3+25 — 66.58

3+00 — 65.18 / 12.46 / 2.65 / C-9.81

2+75 — 64.38 / 13.56 — 4.1%

2+71.70 — 64.24 / 13.70 / 4.07 / C-9.63

2+66.70 MH. #14 — 64.02

2+61.70 — 77.94 ↑ / 63.68 / 14.26 / 4.58 / C-9.68

4+75 — 73.18

4+50 — 5'Lt. 72.08 / 17.19 / 7.73 / C-9.46 ; 5'Rt. 72.08 = / 17.19 / 7.56 / C-9.63

4+25 — 70.98

4+00 — 89.27 ↑ / 69.88 / 19.39 / 9.63 / C-9.76 — 4.4%

3+75 — 68.78

3+50 — 77.94 ↑ / 67.68 / 18.26 / 0.33 / C-9.93

77.94 ↑ / 33 / 77.61 / 11.66 / 89.27 ↑ / 5.37 / 83.90 = / 72.43 + 11.93 / 2019 / 27 / LL-83.2 / OK

Viking Way

5+50

77.34
11.93
3.76
C- 8.17

3 5+25

75.59

7%

2 5+21.93

75.38
13.89
5.23
C- 8.66

2 5+16.93 M.H. #13

7503

2 5+11.93

5' Lt.	5' Rt.
74.81	74.81
14.46	14.46
5.12	5.69
C- 9.34	C- 8.77

89.27 T

2+ 5+00

5' Lt.	5' Rt.
74.28	74.28
14.99	14.99
5.46	5.98
C- 9.53	C- 9.01

6+06.93 Plug.

89.27 T
81.33
7.94
0.06
C- 7.88

6+00

80.84
8.43
0.55
C- 7.88

7%

5+75

79.09

Hypatia Drive

East of St. Louis Terrace.

BM # 5 Page 75

BM = 77.25

TP #1 = 4+13.57 Page 23-

0.72
7802 T
13.72
65.30
9.92
75.22 T
10.00
65.22
0.38
65.60 T

TP #2 = E.H. Roseland + Hypatia
11.11
TP #2 = 54.49
5.45
59.94
- 10.92
TP #3 = 49.02

TP #2 = A 5+87.95
Roseland Drive + Hypatia Way
2019 (49.03)
33

0+75 — 59.97

0+50 — 75.22 T
59.05
16.17
8.88
C - 7.29

0+25 — 58.12

0+05 — 75.22 T
57.38
17.84
10.57
C - 7.27

0+00 = M.H. #17 (P. 23) — 75.22 T
57.20
18.02

1+30 - plug. — 75.22 T
62.01
13.21
5.40
C + 7.81

1+00 — 75.22 T
60.90
14.32
6.58
C - 7.74

Easement Sly. from Pasea Dorado.

	Lt.	Rt.	13.78 ℄
1+00	3.10	3.10	
	10.68	10.68	
	3.72	2.73	
	C-6.96	C-7.95	

BM #9 - P.75
2.12
4.60
6.72
4.87
1.85 = chisc
Δ in Ely el.
15' sly. from
M.H. # 4

0+75			1.85
			11.93
			13.78 ℄
			143
			12.35
			12.47
			24.82 ℄
	Lt.	Rt.	138
0+50	-0.70	-0.90	23.44
	14.47	14.48	9.81
	19.82	10.24	33.25 ℄
	C-4.66	C-4.24	

7.60 %

0+25			
0+05		-4.12	
		17.90	
		12.24	
		C-5.66	
111°-05 of Back Tang		13.78 ℄	
0+00 = M.H. # 4		-4.50	
(A.T.)		1828	

11.93

32

APPROVED

1+75		
	5.30 %	
1+50		6.60 Rt.
		18.22
		9.07
		C-9.15
	4.90 %	
1+47.15		
= 1+42.15 Ahead M.H. # 22		~~6.08 and 6.19~~
Δ 89°-39' Lt.		
1+39.15 Back		

		Lt.
1+34.15		24.82 ℄
		5.70
		19.12
		10.80
		C 8.32

1+25	

Easement Sly from Paseo Dorado

3+25

3+00

Lt.
14.55
10.27
1.38
C-8.89

24.82 ✕
Rt.
14.55
10.27
0.46
C-9.81

2+75

2+50

3.30 Rt = Nail
11.90
12.92
2.38
C-10.54

2+25

2+00

24.82 ✕ Rt
9.25
15.57
6.48
C 9.09

4+75

4+50

Lt.
22.50
10.75
3.81
C-6.94

4+25

4+00

Lt.
19.85
13.40
5.44
C-7.96

3+75

3+50

Lt. 33.25 ✕
17.20
16.05
7.56
C-8.49

Rt
17.20
16.05
6.26
C-9.79

Easement Sly from
Paseo Dorado

M.H.#25
5+13.15

33.25 ★
25.85
7.40
.70
C-6.70

5+00

25.15
8.10
1.35
C-6.75

5-0

AVENIDA ALAMAR.

0+75		
0+50	-3.20 17.43 9.86 C- 7.57	
1st 0+25		
0+05	14.23 ℄ - 6.35 20.58 11.86 C- 8.72	
94°-27' off Back Tang 0+00 = M.H. #3	-6.70	
2+25		
2+00	24.64 ℄ 7.30 17.34 8.98 C- 8.36	
1+75		
1+50 1st	14.23 ℄ 3.80 10.43 2.27 C- 8.16	
1+25		
1+00	+ 0.30 13.93 6.07 C- 7.86	

B.M. #8
7.67
2.80
10.47
5.62
4.85
3.52
8.37
6.25
chain 2.12
Top ab. Alamar + Dorado = B.M. 9

B.M. # 9 - 2.12
12.11
14.23 ℄
0.42
13.81
10.83
24.64 ℄

Avenida Alamar

3+25

3+00 6.40%

24.64 ↗
14.28
10.36
2.91
C-7.45

2+86.54

13.35
10.29
3.78
C-7.51

Δ-10°-26'-30" Lt.
2+81.54 M.H.# 27

13.01

2+76.54

12.66
11.98
4.45
C-7.53

2+50 1%

24.64 ↗
10.80
13.84
5.92
C 7.92

4+75

4+50

24.63
12.09
4.69
C-7.40

4+25

4+00

21.18
15.54
8.30
C-7.24

3+75

3+50

36.72 ↗
17.73
18.99
11.45
C-7.54

24.64 ↗
0.37
24.27
12.45
36.72
0.02
36.70
10.18
46.88 ↗

Avenida Alamar

Rosecland Dr.
Δ 22°-49'-24.
5+85.14 M.M.#28 — 33.96

5+80.14
46.88 ℄
33.61
13.27
3.47
C-9.80

5+75

5+50 6.90%
46.88 ℄
31.53
15.35
4.56
C-10.79

5+25

5+00
36.72 ℄
28.08
8.64
0.02
C 8.62

Rosecland Dr.
S.Ely. of Alamar

7+00
43.61
15.45
5.88
C-9.57

℄ 47.12 P.39
0.66
46.46
12.60
59.06 ℄

6+75

6+50
59.06 ℄
39.41
19.65
9.55
C-10.10

6+25 8.40%

6+00
47.12 ℄
35.21
11.91
2.34
C-9.57

5+90.14
47.12 ℄
34.38
12.74
3.74
C-9.00

34.38
12.50
3.18
C 9.02 ✓

Roseland Dr.
S. Ely. from Alamar Dr.

7+65 14 plug.

49.08
9.98
1.24
C- 8.74

7+50

59.06 X
47.81
11.25
2.34
C- 8.91

7+25 8.40 ?

Roseland Dr.
NWly from Alamar

0+75

38.46
13.77
8.05
C-5.72

0+50

36.96

0+25

35.46
16.77
9.11
C 7.66

0+05

52.23 ✗
34.26
17.97
9.21
C-8.76

63°08' off Alamar Dr.
0+00 = M.H.# 28
(P.37)

33.96

2+29.48

59.80
47.73
12.07
3.20
C-8.87

2+00

59.80 ✗
45.96
13.84
5.69
C-8.15

1+75

52.23 ✗
44.46
7.77
0.57
C-7.20

1+50

42.96
9.27
2.47
C-6.80

1+25

41.46
10.77
4.84
C-5.93

1+00

39.96
12.27
6.79
C-5.48

58.18 B.M.#6
0.63
58.81
12.70
46.11
1.01
47.12
2.35
44.77 B.M.#7 = 44.75
47.12 ✗

B.M.#7
44.75
7.48
52.23 ✗
57
51.66
8.14
59.80 ✗
1.65
58.15 B.M.#6

Roseland Drive

Wly. from Alamar.

3+25

3+00

71.76℄
54.65
17.11
9.31
C-7.80

2+75

10.10 o/o

2+50

60.58℄
49.60
10.98
1.46
C-8.52

2+39.48

60.58℄
48.53
12.05
3.42
C-8.63

2+34.48 M.H.#26
Δ 40°-05'-Lt.

48.03

End. of Job

4+66.45 M.H.#20

80.39
71.46
8.93
0.99
C-7.94

4+50

69.80
10.59
1.94
C-8.65

4+25

4+00

10.10 o/o

80.39℄
64.75
15.64
7.56
C-8.08

3+75

3+50

71.76℄
59.70
12.06
4.41
C-7.65

℄- from P.18
60.54
2.40
58.14
58.18
-0.04
B.M.#6

B.M.#6
58.18
2.40
60.58℄
0.65
59.93
11.83
71.76℄
0.93
70.83
9.56
80.39℄

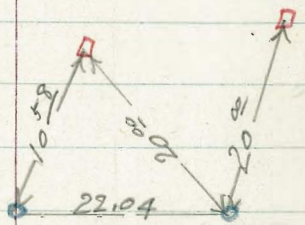
Easement Por. P.L. 1285
S.Wly. from Roseland Dr.

Ties to prop. pipes - From P19
see sheet 1499-D.

□ = set stub.

⊙ = Fd 3/4" pipe + disk

S.Wly line Roseland



Replaced
5/10/50

Paseo Dorada
Restake 5/29/50

		BM#8 7.67
		2.83
		10.50 X
3+25	-7.69	
3+00	-7.76	
2+75	-7.84	
2+50	-7.91	
	18.41	
2+25	-7.99	
	18.49	
	4.77	
C-	13.72	
	10.50 X	
2+00 -	-8.06	
	18.56	
	4.70	
C-	13.86	
1+75	-8.14	
	18.64	
	4.83	
C-	13.81	
1+60	-8.18	
	18.68	
	4.96	
C-	13.72	
M.H.#1		
1+50	-8.21	
	18.71	
	4.92	
C-	13.79	
1+25	-8.29	
	18.79	
	5.27	
C-	13.52	
	10.50 X	
1+00	-8.36	
	18.86	
	5.22	
	13.64	

Stake 48th Ocean View Blvd
to Franklin
Sec 1853/48 WO31482
Aug 31 '50 final grades

Begg
Johnson
Allan
Pope

116.49
11 18
127.67
0 11
127.56
13 21
140.77 HI
10 33
130 44

BP SW
47 @ Ocean View Blv

SBM on 100 RP Point
℄ 48 st. S.

10 33
140.77 HI
4 71
136 06 FP

set curb stake 21 from ℄
= 3 out

13
8

2+16

1+66

1+16

0+66

0+16

0+10 BC

0+00 Prop

rough

135.81 135 81 136 56 136.56
496 4.53 3.92 4 21
486 411
699 F 0.33 F 0.19
F 2.02 F 0.22 F 0.34 2 59
C 1.62

135.47 135 47 136 22 136.22
5 30 5 08 4.26 4 55
5.10 435
633 F 0.10 F 0.09
F 1.03 F 0.09 2.59
C 1.96

135.13 135 13 135 88 135.88
5 64 5 32 4.60 4.89
474 5 50 4.60 1.15
C 0.90 F 0.25 0 00 C 3.74
F 0.15 C ~~2.90~~

West curb

134.79 134 79 135 54 135.54
5 98 5.69 4.94 5 23
3.94 586 486 0 51
C 2.04 F 0.11 C 0.08 C 4.72
134 45 C 0.08
134.45 134.66 135 20 135 20
5 36 6.03 5 28 5 57
C 0.96 6.16 5 40 0.96
F 0.13 F 0.12 C 4.61
140 77 140 48 140 77
134 30. 134.30 134 25 135 09 135 09
6 47 6 18 5 34 5 68
5 70 6 45 5 12 1 35
C 0.77 F 0.27 C 0.27 C 4.33

E curb

134 41 135.16
6 07 5 32
6 27 5 42
F 0.20 F 0.10

130.44
10 04
140 48 41
2 78 5

0.6838 0/0

5:07

3+97 33

3+77 33. VCBG

11·33

3+66 ✓

3+52 (W) ✓

136·06 TP
10 18
146·24 H1.

3+16

Tan

140 48
2·89
137 59
4 71
142 30

2+66

8 34
133 96

137 04
8 26
5 38
F 0·14
6 44
5 38
C 0·06

146 24 H1
137 04 ✓
9 20
10·60
F 1·40

136 92 ✓ 136·92
9 32 5·38
10 78 5·47
F 1·46 F ·09

146 24 140 48
136·83 136·83
9 41 3 65
3 76
11·00 F0·11
F 1·59 F0·39

140 77 H1 140 77 H1
136·49 136 49
4 28 3·99
4 20
5 99 F 0·21
F 1·71 F0·20

136·15 136 15
4 62 4·33
4 53
6 67 F0·20 ✓
F 2·05

146 24 H1
137·79 137·79
4 51 8 45
4 57 4·78
0·00 C 3·67

142 30
137 67 137 67 ✓
4·63 8 57
4 55 4 37
C 0·08 C 4·20

140 48 146 24 H1
137 58 137 58
2·90 8 66
2·90 4 52
0·00 F0.14 C 4 14

140 77 H1
137 24 137 24
3·24 3 53
3 22
C 0·02 0 71
C 0·09 C 2·82

136 90 136 90
3·58 3·87
3·58
0·00 2·23
F0,32 C 1·64

4+97 33

146 24 H1

136 71 ✓ 13671
9 53 5.59
10 45 5.67
F 0.92 F F0.08

4+77 33

136 89 ✓ 13689
9 35 5.41
10.33 C 5.40
F 0.98

4+57 33

137 02 ✓ 13702
9 22 5.28
10.55 5.34
F 1.33 F0.06

4+53 (W) R

4+37 33

137.09 ✓ 13709
9 15 5.21
10 46 5.30
F 1.31 F 0.09

4+17 33

146 24
137 09 ✓ 13709
9 15 5.21
10 42 5.35
F 1.27 F0.14

146 24 H1
14230
13746 137 46
484 8 78
492
F 0.08 3.87
C 4.91

13764 137 64
466 8.60
480
F 0.14 4.67
C 3.93

13777 137.77
453 847
466
F 0.13 492
C 3.55

13784 137 84
4.46 840
460
F0.14 529
C 3.11

14230
13784 137.84
4.46 840
457
F 0.11 472
C 3.68

604

6+07 33

134.63 ✓ 134 63
11 61 7.67
7 39
12.46 C 0.28
F 0.85

142 20
136 15
6.15
6 30
F 0.15

146 24
136.15
10 09
604
C 4 05

5+97 33 BC

10

135 10 ✓ 135 10
11 14 7.20
7 54
11 82 F 0.34
F 0.68

135 95
6.35
6 19
C 0.16

135.95
10 29
5 85
C 4 44

5+87 33

50

135.32 ✓ 135 32
10 92 6.98
7 13
11 55 F 0.15
F 0.63

136 07
6.23
5 95
C 0.28

136 07
10 17
4 85
C 5.32

5+37 33

136 16 ✓ 142 30
10 08 136 16
6.14
10 34 6 29
F 0.24 F 0.15

136 91
5.39
5 30
C 0.09

136 91
9 33
4 91
C 5.32

146 24 H

5+17 33

136 46 ✓ 136 46
9 78 5.84
6 06
10 03 F 0.22
F 0.25

142 30
137 21
4 09
5 17
F 0.08

137 21
9 03
3 79
C 5 24

Paving Grades Pynchon St

Franklin -to- Imperial

9-12-50

W.O. #31516

Sommermeyer
Johnson
Allen

B.M. = N.W. L + T.
Pynchon & Franklin
2015 / 36 / 99.94 / 6.93 / 106.87

Elevations shown on 7942 L are set from B.M. on ocean view + 47th. Misses B.M. 17 Orig notes by 0.31 to 0.34

Use Exist. Ob. B.C. for B.M. El.

1+65.9

0+10-Lt

Ob El.: 99.73 / 6.80 / 106.53 / 2.75 / 103.78 / 3.29 / 107.07

1+25.9 P.V.C.

Rake

0+10 = Ob. E.C.

107.42 / 99.73 / 7.69 / 7.68 / .01

99.56 / 7.86 / 107.42 / + 0.33 / 107.75 - Sub On 1.

0+00 = N. line Franklin

INDEXED

JUL 5 1951

48

Ob	G	1/A	℄	1/A	G	℄
	102.43 / 4.10		103.08 / 4.67		102.93 / 3.63	
106.87 / 102.40 / 4.47 / 4.25	106.53 / 101.73 / 4.80		102.38 / 5.37 / 5.37		106.53 / 102.23 / 4.30	106.87 / 102.90 / 3.97 / 3.63 / 0.34
106.87 / 99.73 / 7.14 / 6.80 / .34	99.06 / 7.47		107.75 / 99.71 / 8.04		99.56 / 6.97	106.87 / 100.23 / 6.64 / 6.33 / .31
	106.53 / 98.83 / 7.70		107.75 / 99.48 / 8.27		106.53 / 99.33 / 7.20	

Pynchon St.

6+06.3 = Sly. line Imperial

5+96.3 = ob. B.C.

100.93
5.92
1068 5 ℄
33
1071.8 = 54 ob. Croft.

5+86.3 = Brk

Rake

2+85.9 E.V.C.

2+45.9

2+05.2

	G	1/A	℄	1/A	G	
101.30	100.93		107.18		101.68	100.29
	6.3 A		101.25		5.39	
	×		5.93		×	
			×			
	100.93		101.50		101.50	
	6.14		5.68		5.57	
	×		×		×	
			107.18 ℄		107.07 ℄	
	101.03		101.68		101.53	
	6.04		5.50		5.54	
	×		×		×	
	107.07		107.75 ℄		106.53 ℄	
	103.03		103.68		103.53	
	4.04		4.07		3.00	
	×		×		×	
	106.53 ℄					
	103.13		103.78		103.63	
	3.40		3.97		2.90	
	×		×		×	
					106.53	
	102.93		103.58		103.43	
	3.60		4.17		3.10	
	×		×		×	

Tourmaline St

Dawes to Cass

W.O. 31623
9-13-50

Sommermeyer
Johnson
Allen

BM#3
P.59
120.00
3.46
123.46 ℄

	Rough	cl.	G.	¼	℄	¼	G	cl.	Rough
1+20	115.73 7.73 7.65 C 0.08	115.73 115.79 C 0.06	115.23		116.01		115.98	116.73 116.34 F 0.39	116.73 6.73 6.77 F 0.04
1+00 P.V.C.	116.17 7.29 7.42 F 0.13	116.17 116.19 C 0.02	115.67		116.45		116.42	117.17 116.85 F 0.32	117.17 6.29 6.82 F 0.53
0+55	117.22 6.24 5.50 C 0.74	117.22 117.55 C 0.33	Rake				Rake	118.22 117.97 F 0.25	118.22 5.24 4.97 C 0.27
0+10 = cl. E.C.	118.27 5.19 4.18 C 1.01	118.27 118.89 C 0.62	117.77		Rake		118.52	119.27 119.41 C 0.14	119.27 4.19 2.94 C 1.25
W. line Dawes 0+00	123.46 ℄ 118.50 4.96 4.22 C 0.74	118.50 119.07 C 0.57	118.00		118.78		118.75	119.50 119.58 C 0.08	123.46 ℄ 119.50 3.96 2.66 C 1.30

B.M. SW Tourmaline P-59 = R 0.00
& Dawes R Raspike

Tourmaline

	Rough	ch	G	1/A
	123.46 x			
3+30	112.95	112.95		
	10.51	113.36		
	9.55	C 0.41		
	C-0.96			
2+80	113.55	113.55		
991	1991	113.71		
881	8.81	C 0.16		
110	C-1.10			
2+30	114.15	114.15		
	9.31	114.29		
	8.18	C 0.14		
	C-1.13			
1+80 = E.V.C.	114.75	114.75	114.25	
	8.71	114.72		
	790	F 0.03		
	C 0.81			
1+60	115.03	115.03	114.53	
	8.43	114.90		
	7.84	F 0.13		
	C 0.59			
1+40	115.35	115.35	114.85	
	8.11	115.48		
	7.70	C 0.13		
	C 0.41			

℄	1/A	G	ch	Rough
				123.46 x
			113.95	113.95
			114.02	951
			C 0.09	7.20
				C 2.31
			114.55	114.55
			114.74	891
			C 0.19	5.93
				C 2.98
			115.15	115.15
			115.29	8.31
			C 0.14	5.36
				C 2.95
115.03		115.00	115.75	115.75
			115.81	7.71
			C 0.06	4.37
				C 3.34
115.31		115.28	116.03	x cross 116.03
			116.03	7.43
			0.001	4.37
				C 3.06
115.63		115.61	116.35	116.35
			116.21	711
			F 0.14	655
				C 0.56

TOURMALINE

Chk SE B.P.
Cass + Tourmaline
110.09
110.10 = P-59

	Rough	cl.	G.	1/4
Fly. line Cass A+99	110.80 6.94	111.01 110.81	110.51	
Rough / cl.				
4+93 = sc. B.C.		110.92 111.09 C 0.17	110.37	
4+89 = sc. B.C.	111.01 6.73 7.05 F 0.32	111.01 111.25 C 0.24	110.51	
4+69	111.26 6.48 6.15 C 0.33	111.26 111.47 C 0.21	110.67	
4+30	111.74 6.00 5.80 C 0.20	111.74 112.03 C 0.29		
3+80	117.74 T 112.35 5.39 5.23 C 0.16	112.35 112.57 C 0.22	Rake	

	℄	1/4	G	cl.	Rough	
			111.42	112.01 111.93 cb	111.93 5.81 5.79 .02	123.46 T 10.95 112.51 5.23 117.74 7.63 110.11 B.M. # 4 P.59
	110.2		111.41	111.98 112.08 C 0.10		
	—		111.42	112.01 112.05 C 0.04	D-3 112.01 5.73 3.38 C 2.35	
	111.42		111.49	112.26 112.26 0.001	N.-0.10 112.26 5.48 2.25 C 2.23	
				112.74 112.57 F 0.17	112.74 5.00 3.0 C 2.0	
				113.35 113.33 F 0.02	113.35 4.39 2.80 C 1.49	
	Rake		Rake	Rake		

Sapphire
Dawes to Bayard

	Rough	ch.	G	¼		℄	¼	G	ch.	Rough	BM#2-P57
											127.00
											6.63
											133.63 ✗
											10.24
											123.39
											8.65
											1320.4 ✗
											7.89
1+50	125.21	125.21							126.21	126.21 ✓	124.15
	8.42	125.26							126.22	7.42	B.M.#1 P59
	5.68	C 0.05							C 0.01	4.07	=124.16
	C 2.74									C 3.35	
1+00	125.60	125.60							126.60	126.60 ✓	
	8.03	125.58							126.87	7.03	
	6.93	F 0.02 ✓							C 0.27 ✓	4.32	
	C 1.10									C 2.71	
0+50	126.00	126.00							127.00	127.00 ✓	
	7.63	126.11							127.15	6.63	
	6.88	C 0.11 ✓							C 0.15 ✓	4.13	
	C 0.75									C 2.50	
ch. E.C.											
0+10	126.32	126.32	125.82			126.60		126.56	127.32	127.32 ✓	
	7.31	126.47							127.23	6.31	
	6.42	C 0.15 ✓							F 0.09 ✓	4.15	
	C 0.89									C 2.16	
	133.63 ✗									133.63 ✗	
W. line Dawes	126.40	126.40	125.90			126.68		126.66	127.40	127.40 ✓	
0+00	7.23	126.55							127.35	6.23	
	6.57	C 0.15 ✓							F 0.05 ✓	4.15	
	C 0.66									C 2.08	
B.M. Spk Nail No. 1 in Pole		→ 127.00									
Dawes & Sapphire P59											

Sapphire

	Rough	cl.	G	1/4		℄	1/4	G	cl.	Rough
4+50	122.84	122.84							123.84	123.84
	9.20	122.89							123.56	8.20
	9.20	C.05							F.0.28	4.09
	X									C.4.11
	B-1									
4+00	123.23	123.23							124.23	124.23
	8.81	123.08							124.20	7.81
	10.20	F.0.15							F.0.03	3.88
	F.1.39									C-3.93
	133.63									133.63
3+50	123.63	123.63							124.63	124.63
	10.00	123.47							124.41	9.00
	10.72	F.0.16							F.0.22	7.11
	F.0.72									C-1.89
3+00	124.02	124.02							125.02	125.02
	9.61	123.99							124.92	8.61
	9.37	F.0.03	Rake			Rake		Rake	F.0.10	6.68
	C.0.24									C.1.93
										TP
2+50	124.42	124.42							125.42	125.42
	9.21	124.57							125.18	8.21
	7.78	C.0.15							F.0.24	5.40
	C-1.43									C-2.81
2+00	124.81	124.81							125.81	125.81
	8.82	124.88							125.7	7.82
	7.02	C.0.07							F.0.11	4.47
	C-1.80									C-3.35

Sapphire

	Rough	ab	G	1/4	℄	1/4	G	cb.	Rough
E. line Cass									
4+99 26	9.63 9.64 -0.01	122.41' 122.43	121.90		122.79		123.20	123.76 123.77	
4+93 26 cl. B.C.		122.50' 122.42 F0.08'	121.95		—		123.14	123.68' 123.71 C.0.03'	
cl. B.C.	D-3								
4+73 26 Brk	122.66 9.38 10.80 F1.42	122.66' 122.51 F0.15'	122.16		122.94		122.91	123.66' 128.70 C0.04'	123.66 8.38 4.03 C-4.35

Sapphire - Cass to Bayard

	Rough	ch.	G	1/A	E	1/A	G.	ch.	Rough	
P.V.C. 1+50 ~~Brk~~	117.63 6.83 6.36 C 0.47	117.63	116.96		117.67		117.57	118.24	118.24 6.22 3.72 C 2.50	Bk #1 p59 124.16 .50
0+95	Nail 5' 119.49 4.97 5.23 F 0.26	Rake	Rake		Rake		Rake	Rake	120.26 4.20 1.50 C 2.70	124.46 ℄
0+40 Brk.	121.36 3.10 4.08 F 0.98		120.69		121.55		121.60		122.27 2.19 0.50 C 1.69	
0+26 Brk	121.83 2.63 3.68 F 1.05	121.83	121.16				122.11	122.78	122.78 1.68 0.18 C 1.50	
ch. E.C. 0+06		122.15	121.58				122.83	123.50		
W. line Cass 0+00	124.46 ℄ 122.24 2.22	122.24	121.74		122.78		123.17	123.73	123.73 0.73 0.73 ℄	

Sapphire

	Rough	cl.	G.	V/A
3+20	114.21 10.25 9.91 C034			
2+75	114.93 9.53 9.63 F0.10	Rake	Rake	
2+30 E.V.C.	115.64 8.82 8.88 F0.06	115.64	114.97	
2+10	116.00 8.46 8.54 C-0.08	116.00	115.33	
1+90	116.46 8.00 7.79 C0.21	116.46	115.79	
1+70	117.00 7.46 7.25 C0.21	117.00	116.33	

℄	V/A	G.	cl.	Rough
				114.71 9.75 6.79 C-2.98
Rake		Rake	Rake	115.43 9.03 6.62 C2.41
115.62		115.47	116.14	116.14 8.32 5.85 C-2.47
115.99		115.84	116.51	116.51 7.95 4.42 C3.53
116.45		116.32	116.99	116.99 7.47 4.16 C-3.31
117.01		116.89	117.56	117.56 6.90 3.92 C2.98

Sapphire

	Rough	cl.	G.	¼
E. line Bayard				
3+79½	113.10	113.10	112.43	
	11.36			
	11.64			
	F0.28			
3+71.7		113.40	112.73	
cl. B.C.				
3+64½	113.50	113.50	112.83	
	10.96			
	10.94			
	C0.02			

	±	¼	G	cl.	Rough
	113.27		113.35	114.02	114.02
					10.44
					7.71
					C2.73
	113.38		113.25	113.92	
	113.48		113.33	114.00	114.00
					10.46
					7.02
					C-3.44

Benches { Tourmaline / Sapphire

		12.23	110.10	BM #4	S.E. B.P. Cass + Tourmaline	
2.33	122.33	8.32	120.00	BM #3	S.W. tourmaline + Dawes	R.R. spike in pole 5098
1.32	128.32	4.17	127.00	BM #2	S.W. Dawes + Sapphire Nail in Pole # 5148	
7.01	131.17	—	124.16	BM #1	N.W. 7' L+T. Sapphire + Cass	

Alley.

Blk 6 - City Hgts Annex #2
" 2 " " " " "
" 11 " " " " #1 (Sheet 7756-L)

Dwight to Landis between Highland + 44th

Sommerneyer
Johnson
Allen

9-20-50
W.O. #31384

	Lt. West	±	Rt. East
P.V.C.	N.-0.20		D-2'
1+40.3	348.14		348.44
	8.50		8.20
	7.11		7.63
	C 1.39		C 0.57
	N-0.50		D-2'
1+03.2	347.36		347.66
	9.28		8.98
	8.05		8.66
	C 1.23		C 0.32
	D-2'		D-2'
0+66	346.58		346.88
	10.06		9.76
	10.13		9.12
	F 0.07		C 0.64
Sly. line City Hgts Annex #1	D-0.30		D-2'
0+28	345.80	345.65	346.10
	10.84		10.54
	10.38		10.00
	C 0.46		C 0.54
Nly. line Dwight	356.64±	356.64	356.64±
0+00	345.20	345.05	345.50
	11.44	11.59	11.14
	11.38	11.52	11.00
	C 0.06	0.07	0.14

	Lt. West	±	Rt. East
Enic.	D-2'		D-2'
2+60 3	356.64±		356.64±
	349.98		350.28
	6.66		6.36
	6.85		5.88
	F 0.19		C 0.48
	D-2'		X-4'
2+40 3	349.77		350.07
	6.87		6.57
	7.02		6.13
	F 0.15		C 0.44
	D-2'		D-2'
2+20 3	349.51		349.81
	7.13		6.83
	7.44		6.46
	F 0.31		C 0.37
	D = 0.15		D-2'
2+00 3	349.23		349.53
	7.41		7.11
	7.29		6.74
	C 0.12		C 0.37
	D-2		X-3'
1+80 3	348.91		349.21
	7.73		7.43
	7.77		6.92
	F 0.04		C 0.51
	D-2'		X-3
1+60 3	348.54		348.84
	8.10		7.80
	8.24		6.97
	F 0.14		C 0.83

N.W. 7'L+T. Landis + Highland

353.59
5.09
358.68 ↑
6.28
352.40
4.24
356.64 ↑

	N-0.34	D-3'
	358.68	358.68 ↑
5+10 3	352.41	352.71
	6.27	5.97
	5.06	4.91
	C 1.21	C 1.06
	D-2'	D-2'
	358.68 ↑	356.64 ↑
4+60 3	351.92	352.22
	6.76	4.42
	6.36	3.34
	C 0.40	C 1.08
	D-5	D-2' x
	358.68 ↑	356.64
4+10 3	351.44	351.74
	7.24	4.90
	6.55	4.38
	C 0.69	C 0.52
	D-2'	N-0.52
	356.64 ↑	356.64
3+60 3	350.95	351.25
	5.69	5.39
	4.93	3.63
	C 0.76	C 1.76
	D-2'	D-2'
	350.47	350.77
3+10 3	6.17	5.87
	5.80	4.67
	C 0.37	C 1.20

Sly. line Landis. 6+00 29	↑ 358.68		358.68 ↑
	353.10		353.10
	5.58		5.58
			5.02
			.04
Brk. 5+60 3	N.-0.03		D-2'
	352.90		353.20
	5.78		5.48
	3.86		5.33
	C-1.92		C-0.15

Cub stakes 48th
Reset 9/21/50

B.M. 130.44
10.55
140.99 ✗
3.26
137.73
4.48
142.21 ✗

Sommermeyer
Johnson
Allen

west

3+77.33	142.21 ✗	142.21 ✗
	136.92	137.67
	5.29	4.54
	5.40	4.48
	F 0.11	C 0.06

Rake

0+16 = Brk.	140.99 ✗	140.99 ✗
	134.45	135.20
	6.54	5.79
	6.67	5.90
	F 0.13 ✓	F 0.11 ✓

0+10 = B.C.	140.99	
	134.41	135.16
	6.58	5.83
	6.77	5.93
	F 0.19 ✓	F 0.10 ✓

0+00	140.99	
	134.30	135.09
	6.69	5.90
	6.97	5.63
	F 0.28 ✓	C 0.27 ✓

SURVEYED

62

4+97.3	136.72 WL	5 1957 AC
	5.50	4.75
	5.58	4.87
	F 0.08	F 0.12

4+77.3	136.89	137.64
	5.32	4.57
	5.31	4.80
	C 0.01	F 0.23

4+57.3	137.02	137.77
	5.19	4.44
	5.34	4.58
	F 0.15	F 0.14

4+37.3	137.09	137.84
	5.12	4.37
	5.22	4.52
	F 0.10	F 0.15

4+17.3	137.09	137.84
	5.12	4.37
	5.26	4.48
	F 0.14	F 0.11

3+97.3	137.04	137.79
	5.17	4.42
	5.30	4.62
	F 0.13	F 0.20

Gutter check + Fine Grade 48th

Ocean View - Franklin

		West	℄	East	
3+97		141.58	141.89	141.59	
		136.54	137.25	137.04	
		5.05	4.62	4.55	
		5.03		4.47	
		C 0.02		C 0.08	
3+77	141.58	140.81	141.87	141.58	
	136.42	136.42	137.13	136.92	
	5.16	4.39	4.74	4.66	
	5.14	4.36		4.52	
	C 0.02	C 0.03		C 0.08	
0+16		133.95	134.66	134.45	
		6.82	6.48	6.36	
		6.93		6.33	
		F 0.07		C 0.03	
0+10		133.15	134.66	134.45	
N.L. Oceanview			141.14		
0+00		133.80	134.25	134.30	
			6.89		

141.59
33
141.92
05
141.87 Sub G.

B.M. Page 43
130.44
10.37
140.81
4.01
136.80
4.79
141.59

℄ Raised 0.05 so as to better meet gutters as constructed

6+07 33	142.21	142.21	
	134.63	136.15	
	7.58	6.06	
	7.30	6.22	
	C 0.28	F 0.16	
5+97 3 = C.B.C.	135.10	135.98	
	7.11	6.26	
	7.45	6.11	
	F 0.34	C 0.15	
5+87 3	135.32	136.07	
	6.89	6.14	
	7.03	5.94	
	F 0.14	C 0.20	
5+37 3	136.16	136.91	
	6.05	5.30	
	6.21	5.27	
	F 0.16	C 0.03	
5+17 3	136.46	137.21	
	5.75	5.00	
	6.05	5.27	
	F 0.30	F 0.27	

48th

	West	℄	East
4+97	136.24	136.92	136.71
	5.38 ✓	4.95 ×	4.88
			4.83
			CO.05
4+77	136.39	137.10	136.89
	5.20 ✓	4.77 ×	4.70
			4.61
			CO.09
4+57	136.52	137.23	137.02
	5.07	4.64 ×	4.57
	5.02		4.49
	CO.05		CO.08
4+37	136.59	137.30	137.09
	5.00	4.57 ×	4.50
	4.96		4.43
	CO.04		CO.07
4+17	136.59	141.87 ℄ 137.30	137.09
	5.00	4.57 ×	4.50
	4.95		4.43
	CO.05		CO.07

48th

	West	℄	East
S.L. Franklin 6+07 22	134.13	141.8 ℄ 134.87	135.20
	7.46 ✓	7.00 ×	6.39
			6.31
			CO.08
5+97	134.60	135.22	135.20
	6.99	6.65 ×	6.39
	6.97		6.31
	CO.02		CO.08
5+87	134.82	135.53	135.32
	6.77	6.34 ×	6.27
	6.76		6.22
	CO.01		CO.05
5+62	135.24	135.95	135.74
	6.35	5.92 ×	5.82
	6.31		5.80
	CO.04		CO.02
5+37	135.66	136.37	136.16
	5.93	5.50 ×	5.43
	5.93 ✓		5.33
	CO.✓		CO.10
5+17	135.96	136.67	136.46
	5.63	5.20 ×	5.13
	5.63 ✓		5.07
			CO.06

Kurtz St. Sewer

W.O. 20009

℄ Emory to 300' wly,

stakes set 4' south of ℄ Kurtz

0+00 = Exist. M.H. ℄ Emory & ℄ Kurtz

Sommermeyer
Boggs
Allen

12-1-50

0.3% Grade

1+00	19.30 9.52 4.47 C-5.05	
0+75	19.22 9.60 3.88 C-5.72	
0+50	19.15 9.67 4.06 C 5.61	
0+25	19.07 9.75 4.38 C 5.37	
0+00 = Exist M.H.	19.00 9.82	

B.M. = I.E. M.H. Emory & Kurtz
19.00
9.82
28.82 ✓

882
28
720

RECEIVED
JUL 5 1951

3+00		19.90 8.92 5.60 C-3.32
2+75	19.82 9.00 5.60 C-3.40	
2+50		19.75 9.07 5.50 C-3.57
2+25	19.67 9.15 5.30 C-3.85	
2+00		19.60 9.22 5.11 C 4.11
1+75	19.52 9.30 4.90 C 4.40	
1+50		19.45 9.37 4.92 C-4.45
1+25	28.12 ✓ 19.37 9.45 4.61 C-4.84	

Alley Blk. 11 - Ocean Beach Park
" " 9A - Ocean Bay Beach

Sommermeyer
Begg
Allen
Bunch

12/12/50
W.O. 31823

FB 1825
74

Sheet 7949-L

	South ℄	North
0+80	X-2' 16.19 / 5.31 / 4.83 / C 0.48	A-2' 16.19 / 5.31 / 4.68 / C 0.63
0+60	A-2' 16.43 / 5.07 / 4.74 / C. 0.33	A-2' 16.43 / 5.07 / 4.59 / C- 0.48
0+40	A-2 16.58 / 4.92 / 4.64 / C-0.28	A-2' 16.58 / 4.92 / 5.02 / F 0.10
0+20	X-2' 21.50 * / 16.65 / 4.85 / 4.31 / C 0.54	N. "90" 21.50* / 16.65 / 4.85 / 4.30 / C 0.50
0+00 - W'ly line Cable	16.53	16.55

2+00	A-1' 20.52* / 13.86 / 6.66 / 6.53 / C 0.13	D-1' 20.52* / 13.86 / 6.66 / 6.29 / C-0.37	SWBP Cable + Voltaire ~~17.01~~ Gone
1+80	A-2' 14.19 / 6.33 / 5.98 / C 0.35	D-2' 14.19 / 6.33 / 5.26 / C 1.07	N.E of Voltaire & Bacon 1825/74 9.50 / 7.65 / 17.15 / 1.98 / 15.17
1+60	N-0.10 in 20.52* / 14.57 / 5.95 / 5.46 / C 0.49	D-2 20.52* / 14.57 / 5.95 / 4.83 / C 1.12	6.73 / 21.90 / 5.17 / 16.73 / 4.77 / 21.50*
1+40	21.50* D-0.5 / 15.00 / 6.50 / 6.11 / C 0.39	21.50* N.-0.15 / 15.00 / 6.50 / 5.29 / C 1.21	6.88 / 14.62 / 5.90 / 20.52*
1+20	A-2' 15.46 / 6.04 / 5.80 / C 0.24	D-2' 15.46 / 6.04 / 5.30 / C 0.74	
1+00	A-2 15.87 / 5.63 / 5.21 / C-0.42	D-2' 15.87 / 5.63 / 5.22 / C 0.41	

	Lt. South	℄	Rt. North	
	X-2' 16.35 X 10.98 5.37 5.10 C 0.27		D-2' 16.35 X 10.98 5.37 5.05 C-0.32	20.52 X 7.90 12.62 3.73 16.35 X 5.80 10.55 = T.P. = 9 = Rtd 4+60
4+20				
	D-2' 11.50 4.85 4.52 C-0.33		D-2' 11.50 4.85 4.11 C 0.74	10.55 T.P. 4.07 14.62 X
3+80				
	D-2' 12.02 4.33 4.03 C 0.30		X-2' 12.02 4.33 3.91 C 0.42	
3+40				
	D-2' 16.35 X 12.54 3.81 3.81 X		D-2' 16.35 X 12.54 3.81 3.72 C 0.09	
3+00				
	20.52 X D-2' 13.06 7.46 7.90 C 0.16		20.52 X D-0.05 13.06 7.46 7.46 X	
2+60				
	D-2' 20.52 X 13.58 6.94 6.71 C 0.23		D-2' 20.52 X 13.58 6.94 6.37 C 0.57	
2+20				

E. line Bacon

	Lt South	℄	Rt. North	
5+97 =	8.59 6.03 6.02 .01		8.58 6.04 6.04 ✓	A+90 Rt. Lat #1 14.62 X 5.07 9.55 4.50 C 5.05
				A+15 Rt Lat #2
5+80 ~~Bch~~	N.003 W 8.90 5.72 4.10 C 1.62		D-12 8.90 5.72 5.58 C 0.14	16.35 X 6.05 10.30 4.76 C-5.54
5+40	D-2' 9.42 5.20 4.82 C 0.38		D-2 9.42 5.20 5.13 C 0.07	3+10 Rt Lat #3 16.35 X 7.41 8.94 3.90 C 5.04
5+00	D-2' 9.94 4.68 4.46 C 0.22		D-2' 9.94 4.68 4.68 X	
4+60	D-2' 14.62 X 10.46 4.16 4.00 C 0.16		D-2' 14.62 X 10.46 4.16 4.07 C-0.09	1+90 Rt. Lat #4 20.52 X 9.02 11.50 5.53 C 5.97

Stake Curb – N. side Myrtle
East of Florida

Sommermeyer
Begg
Allen
Bunch

12-14-50

Profile #1812
FB 1354 - 79
~~1594 - 52~~
1671 - P28

10' Prop. line to curb line

S.W.B.P. Myrtle & Florida
198.01
11.08
209.09 ℄
0.18
208.91
10.01
2189 2 ℄

N. ch. Myrtle

214.88 = End Alley ch.
4.04
3.46
C 0.58
214.31
4.61
3.46
C 1.15

3'
10.00
3' Rad.

EL. 214.78
1+50
1+47

214.81
4.11
3.46
C-0.65
= EC. Alley ch.

213.20
5.72
2.95
C-2.77

11.90
1+40

210.32
8.60
3.77
C-4.83

12.00
1+20

℄ = 218.92

208.95
9.97
5.66
C 4.31

11.75
1+10

206.44
12.48
8.87
C-3.61

12.00
0+90

℄ to Here = 209.09

204.54
4.55
4.59
-0.04
204.33

0+72 = End exist ch.
0+70

202.64
6.45
6.40
+0.05

0+50

201.35
7.74
7.59
+0.15

0+30

200.00
9.09
8.58
+.51

0+10

199.35
9.74

0+00

Florida

Sewer Alley Blk 2.
Stephens Add.

12/13/50
W.O. 62199

Sommermeyer
Begg
Allen
Bunch

Sheet 8646-L
F.B. 2008/63

0+00 = Exist. M.H. & Glendora St.

B.M. = wly. Prop. Mon. Glendora & Del Rey.

23.94
2.02
25.96 ✗

1+50	11.59 14.37 5.31 C-9.06	
1+00	9.83 16.13 5.90 C-10.23	
0+50	8.06 17.90 6.44 C-11.46	
0+00 on Rim of M.H.	6.30 19.66 8.01 C-11.65	
3+20 = end.	13.84 12.12 4.21 C-7.91	9' Lt. ℄
2+80	13.68 12.28 4.32 C-7.96	
2+40	13.52 12.44 4.64 C-7.80	
2+00 = M.H. #1	13.36 12.60 4.93 C-7.67	

℄ grades

Alley Blk 143 Elmw. Hgts

Polk to Howard

Between Florida + Georgia

Sommermeyer 12-18-50

Begg W.O.

Allen

Bunch

0+80		305.98	
		6.01	
		×	
0+60		306.57	
		5.42	
		×	
0+40	5.09	306.90	
	42	5.09	
	top of M.H. = 4.67		
	×		
0+20		311.99 ℄	
		307.11	
		4.88	
		×	
N. line Polk		311.57 ℄	
0+00		306.98	
		4.59	
		L	

2+00	303.28 ℄	311.99 ℄	stub. 3' back.
	301.63	301.63	0+20 - on west
	1.65	10.36	grade. = 308.63
	×		cut. = 2.21
			El. stub 310.84
			0.73
			311.57 ℄
1+80		302.32	5" pave = .42
		9.67	311.99 ℄
		×	10.20
			301.79
			1.49
1+60		303.05	303.28 ℄
		8.94	
		×	
1+40		303.78	
		8.21	
		×	
1+20		304.51	
		7.48	
		×	
1+00		305.24	
		6.75	
		×	

Alley Blk. 143
Unio Hgts

3+20	299.10 4.18 ×	
3+00	299.45 3.83 ×	
2+80	℄ Grade 298.80 30C = Top. M.H. 3.48 ×	
2+60	300.15 3.13 ×	
2+40	300.55 2.73 ×	
2+20	303.28 * 301.04 2.24 ×	
4+40	298.90 4.38 ×	303.28 = Subgrade *
4+20	298.56 4.72 ×	
4+00	298.30 4.98 ×	4.98 42 4.56 0.04 4.60 = Top. Catch Basin ×
3+80	298.35 4.93 ×	
3+60	298.48 4.80 ×	
3+40	303.28 * 298.75 4.53 ×	

Alley Blk. 143
Unio. Hgts

Sub-grade ✗
303.28

5+60	302.82	
	0.46 ✗	
5+40	302.29	
	0.99 ✗	
5+20	301.61	
	1.67 ✗	
5+00	300.82	
	2.46 ✗	
4+80	300.02	
	3.26 ✗	
4+60	303.28 ✗	
	299.38	
	3.90 ✗	

6+00	302.81	
	0.47	
5+80	303.03	
	0.25 ✗	

Florida Court

Florida to Georgia

12-18-50
W.O.# 3573

Sommermeyer
Begg
Allen
Bunch

Void

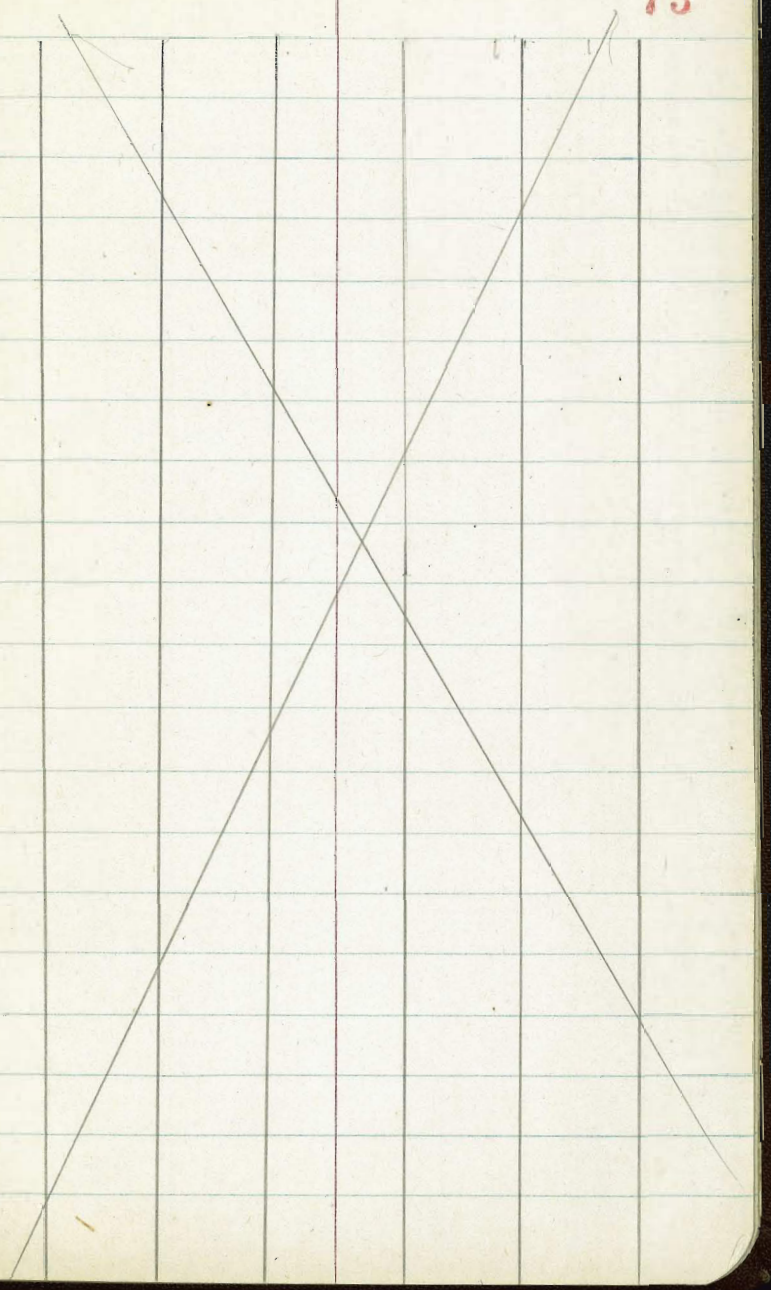
1+00

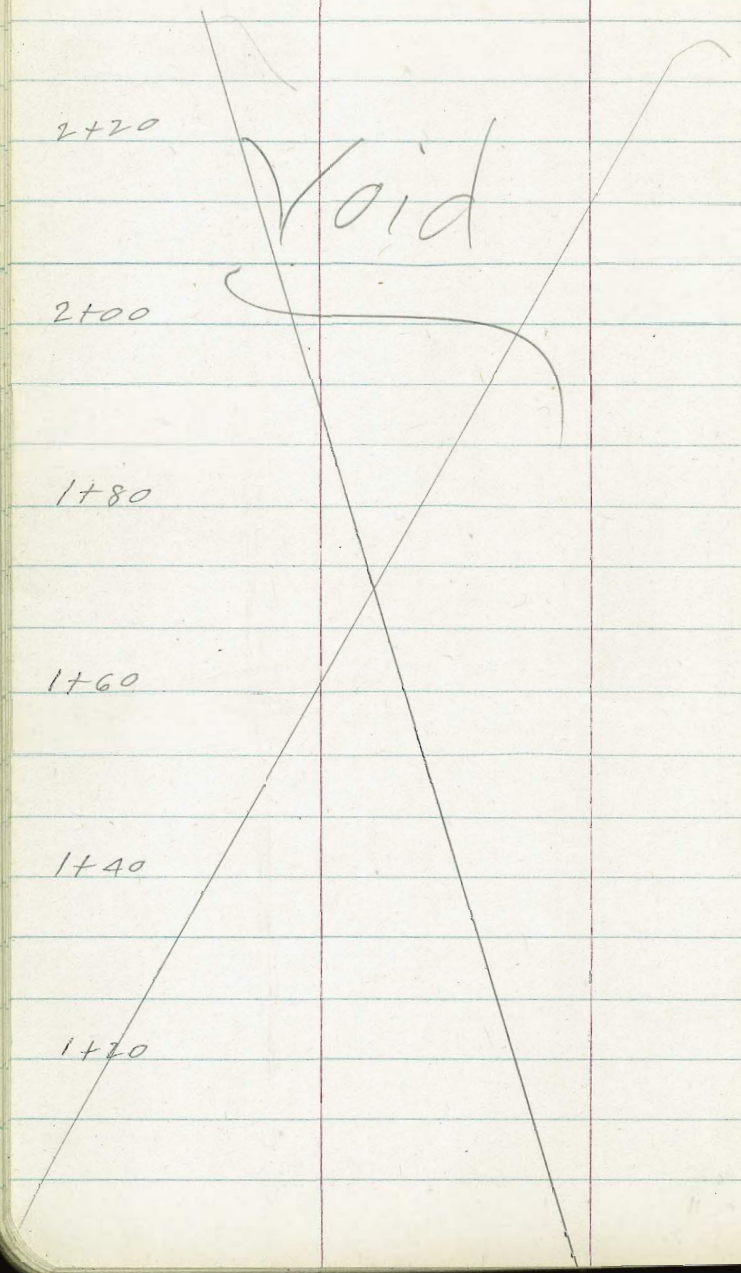
0+60

0+20

0+10

0+00.25 = W'ly line Florida St.




2+20
Void
2+00
1+80
1+60
1+40
1+20

Construction benches

S.E. La Jolla Shores Sewer

Chiseled □ S.Ely cb. Paseo Dorado		1.85 = B.M. # 10	15' S'ly. From M.H. # 4
cut. chisel sq. in N'ly. curb.		2.12 B.M. # 9	Top cb. & Avinida Alamar + N'ly cb. Paseo Dorado
N.E.B.P.		7.67 B.M. # 8	N.E.B.P. Calle de la Plata & Paseo Dorado. 2019/2
Spike in pole #		44.75 BM # 7	N'ly. Roseland Dr. + Alamar FB
Spike in Pole # 2181		58.18 B.M. # 6	Roseland + Little Sts. N'ly. side FB 2019/19
Chisel □ Back of walk		77.25 B.M. # 5	N'ly. Cor. St Louis Terrace + Torrey Rd 2019/22
Set B.M. Page 28		54.99 = BM # 4	Viking Way + St Louis Terrace Chisel □ - So. end S.Ely. cb. Ret.
S.E.B.P. St 2019/14 Terrace		37.42 = BM # 3	S.E.B.P. St. Louis terrace & Spindrift.
Set B.M.	4.37	13.31 = BM # 2	Spike N.Ely. P. pole # J.P. 1945 Roseland Dr. + Spindrift.
11.58	17.68	6.10	13+88 55 FB 2019 - P. 12

INDEXED 6 1951 JM

Florida Court

Florida St. to Georgia St.

Recheck turns sly ∅ Florida

Sommermeyer
Beggs
Allen
Bunch

12-18-50
W.O.# 31573

South

		Rough	Curb
	Florida + Florida	257.64 ✗	254.68 ✗
1+00	248.60	250.19	250.19
This Rod = 5.45	4.45	7.45	4.49
All ✗s. 1' Low	253.05 ✗	9.73	3.88
	1.72	F 2.28	C 0.61
	250.33	F 1.28	
	7.31		
	257.64 ✗	253.05 ✗	X-3'
0+60	40	249.54	249.54
	257.24	3.51	5.14
	11.39	5.20	4.80
	268.63 ✗	F 1.69	C 0.34
	0.49	F 0.69	
	268.14	253.05 ✗	
0+20	12.97	248.90	248.90
	281.11 ✗	4.15	5.78
	1.16	4.25	5.86
	279.95	F 0.10	F 0.08
	10.61	C 0.90	
0+10	290.56 ✗	~~248.75~~	248.75
			5.93
			6.04
			F 0.11
0+00.25 = Wly. line Florida		248.60	254.68 ✗
		4.45	248.60
			5.08
			6.07
			.01

Set chisel ⊡ Sly. Pine 4" sq. 18" [illegible] ⊡ Sly. from [illegible]

					North	
		Gutter	℄	Gutter	Curb	Rough
	248.60					
	8.98					
	257.58					
	6.25					
	251.33				254.68 ✗	257.64 ✗
	11.78				250.69	250.69
	263.11 ✗				3.99	6.95
	4.87				4.02	6.10
	258.24				F 0.03	~~C 0.85~~
	11.70					C 1.85 ✓
	269.94					
	0.79					253.05 ✗
	269.15				250.04	250.04
	12.65				4.64	3.01
	281.80				5.09	1.22
	0.85				F 0.45	~~C 1.79~~
	280.95					C 2.79 ✓
	10.36					
	291.31					253.05 ✗
					249.40	249.40
					5.28	3.65
					5.21	0.90
					C 0.07	~~C 2.75~~
						C 3.75 ✓
					249.40	
					5.28	
					5.18	
					C 0.10	
					254.68 ✗	
					249.58	249.58
					5.10	3.47
					5.09	
					.01 ✓	

Florida Court

		South		Gutter	℄	Gutter	North	
	0+60.A+ 250.04 C. 2.79	Rough	Curb				Curb	Rough
	EL, 141 252.83 1.83		264.52✗				264.52✗	
2+20	254.68✗ 1.80	262.90 5.73 6.48	262.90 1.62 1.32				263.40 1.12 1.48	263.40 5.23 4.50
	252.88 11.64	~~F 0.75~~ C 0.25 ✓	C 0.30				F 0.36	~~C 0.73~~ C 1.73 ✓
	264.52✗ 1.48	268.63✗						268.63✗
2+00	263.04 11.52	259.50 9.13 9.79	259.50 5.02 4.69				260.00 4.52 4.56	260.00 8.63 7.42
	274.56✗ 0.28	~~F 0.66~~ C 0.34 ✓	C 0.33				F 0.04	~~C 1.21~~ C 2.21 ✓
	274.28 12.79	257.64✗						257.64✗
1+80	287.07✗	256.40 1.24 0.96	256.40 8.12 7.86				256.90 7.62 7.28	256.90 0.74 0.40
		~~C 0.28~~ C -1.28 ✓	C 0.26				C 0.34	~~C 0.34~~ C 1.34 ✓
			264.52✗				264.52✗	
1+60		253.93 3.71 5.57	253.93 10.59 10.63				254.43 10.09 9.77	254.43 3.21 3.71
		~~F 1.86~~ F 0.86 ✓	F 0.04				C 0.32	~~F 0.50~~ C 0.50 ✓
			254.68✗				254.68✗	
1+40		252.07 5.57 8.05	252.07 2.61 2.70				252.57 2.11 1.80	252.57 5.07 3.93
		~~F 2.48~~ F 1.48 ✓	F 0.09				C 0.31	~~C 1.14~~ C 2.14 ✓
		257.64✗					254.68✗	257.64✗
1+20		250.82 6.82 8.90	250.82 3.86 3.79				251.32 3.36 3.18	251.32 6.32 5.98
		~~F 2.08~~ F 1.08 ✓	C 0.07				C 0.18	~~C 0.34~~ C 1.34 ✓

Florida Court.

South ↓ | Gutter & Gutter | ↓ North

	South Rough	South Curb	Gutter	Gutter	North curb.	North Rough
3+20 = Ely Nine Georgia	291.31 ✗	285.90			287.07 ✗	291.31 ✗
	285.90				286.33	286.33
	5.46	1.17			0.74	4.98
	5.37	1.11			0.68	4.94
	±0.04 ✓	C0.06			C0.06	0.04 ✓
3+15	290.56 ✗	287.07 ✗				290.56 ✗
	285.00	285.00			285.50	285.50
	5.56	2.07			1.57	5.06
	6.59	2.45			0.80	4.70
	~~F 1.03~~	✓F0.38			C 0.77	~~C 0.36~~
	F 0.03.					C 1.36 ✓
2+87.5	281.11 ✗	287.07 ✗			287.07 ✗	281.11 ✗
	278.15	278.15			278.65	278.65
	2.96	8.92			8.42	2.46
	5.62	10.18			7.40	2.08
	~~F 2.66~~	F1.26			C 1.02	~~C 0.38~~ ✓
	F 1.66	✓				C 1.38
2+60	281.11 ✗	274.56 ✗			274.56 ✗	281.11 ✗
	271.29	271.29			271.79	271.79
	9.82	3.27			2.77	9.32
	10.53	3.76			2.82	7.75
	~~F 0.71~~	✓F0.49 ✓			F0.05 ✓	~~C 1.57~~ ✓
	C 0.29					C 2.57
2+40	268.63 ✗	274.56 ✗			274.56 ✗	268.63 ✗
	266.70	266.70			267.20	267.20
	1.93	7.86			7.36	1.43
	4.58	7.43			8.08	1.27
	~~F 2.65~~	C0.43			F0.72	~~C 0.16~~ ✓
	F 1.65	✓				C 1.16

Linda Vista Library

Grades - Drive - walk + grounds

12/22/50

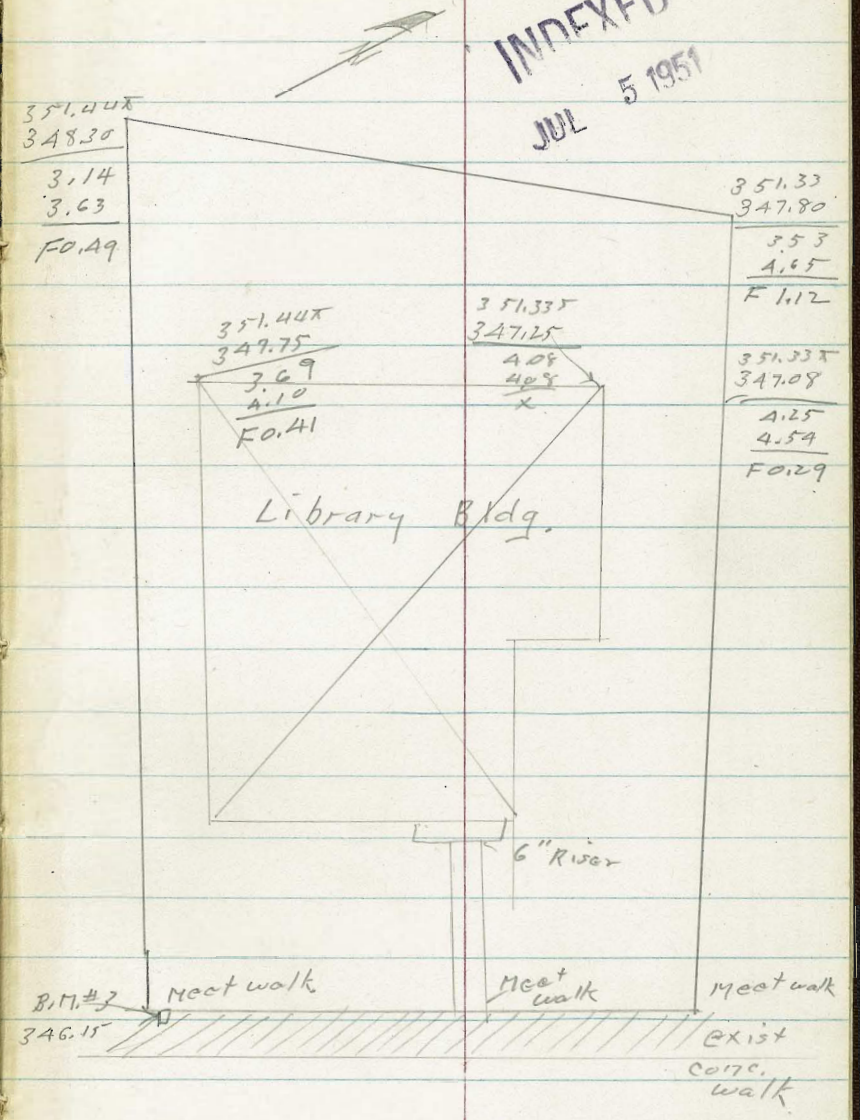
sheet 1550-D.

Grades set as shown.

O = intermediate stakes staked in.

B.M.#3 346.15
5.29
351.44 ±

BM#3 346.15
5.18
351.33 ±



2.04

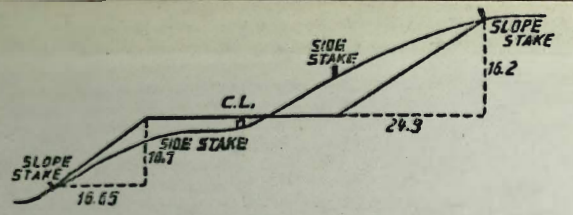
5,9
6,2
11 8
354
365 9

.16955
23
11568 5
33510
45778 5
9 15

.16955
9 15
84775
16955
15 2595
15 13825

.17
30
V2 0 2
8

.17
27
19
1 3 4
1.59
V 18
9 1



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
HOLYOKE MASSACHUSETTS
NEW YORK CHICAGO BOSTON SAN FRANCISCO