

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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to page # 37
except pages # 1,

MICROFILMED

APR 14 1965

DIRECTIONS FOR USE OF TABLE

TABLE NO. XIV

Distance of slope stake from side of shoulder
stake for any width roadway, slope 1X to 1
If ground is nearly level the cut or fill at
stake is located by the double entry method.

IMPROVED TABLES
AND
INFORMATION

cut larger. If it does not make the slight ad-
justment necessary.

TABLE NO. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external) by L by
given degree (or external).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

$$T = R \sin \frac{D}{2}$$
$$E = R (1 - \cos \frac{D}{2})$$
$$L = R D$$

311.21
 .27
 311.48
 .5
 .98

332.96
 0.64
 333.60
 315.94
 17.66
 9.42
 8.24

313.42
 12.35
 325.77
 0.14
 325.63
 9.31
 334.94
 1.94
 333.00

207.95
 7.17
 215.12
 8.01
 223.13
 215.14
 7.99

17.85
 .004
 .07140
 25
 .004
 .100

11.60
 8.83
 20.23
 317.86
 337.49
 4.53
 332.96

21.62
 .004
 .08648

47+87.61
 29.40
 48+17.01

47+87.61
 58.80
 48+46.41
 20.00
 48+66.41
 20.00
 48+86.41

M.H. #14

308.22	51. + 23.20
<u>300.62</u>	<u>48 + 86.41</u>
7.60	2 36.79

3.80	100
<u>300.62</u>	<u>86.41</u>
309.42	19.59
	<u>.02</u>
315.94	.27 18
<u>311.26</u>	

236.79) 4.7300	(2 002
	4 7358	

	<u>182.47</u>	
75.00		
<u>53.38</u>	54 + 53.38	
21.62	<u>1 + 82.47</u>	
	56 + 35.85	317.99
	<u>.064</u>	.26
<u>184.47</u>	0.73000	.73
	73788	

223.13
<u>0.08</u>
223.05
<u>9.59</u>
232.64

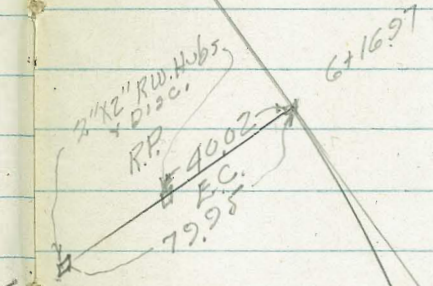
# 13	44 + 45.31
	<u>3 + 28.91</u>
	41 + 20

Access Road - Gibbs Airport
Between State Highway
And Aero Drive - Plan 7761-L

Walker
F. Gregory
G. Pope
R. Gibson
3-23-50

M.O. = 20580

INDEXED
W.K.
MAY 8 1950



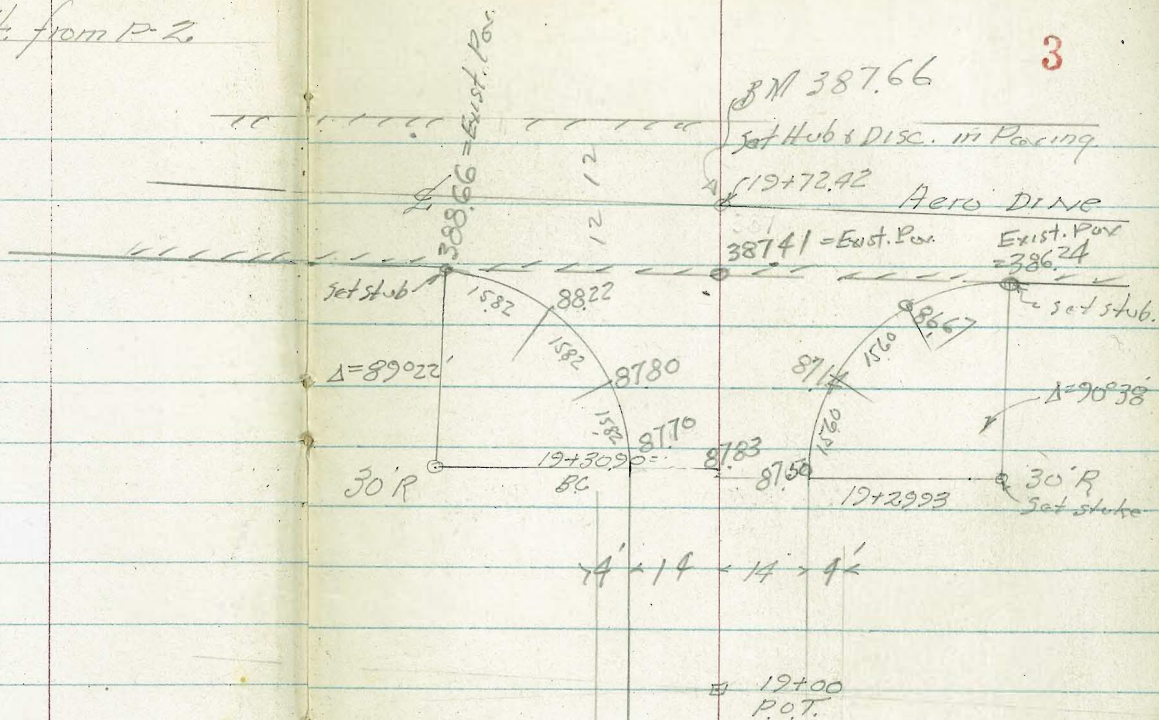
R=1000
Δ=35°21'
L=616.97
T=318.66

E.C.

0+00

MAY 25 1950

Access Road Cont. from P. 2.



Grades
 shown on
 Profile are
 this line,
 excepting Returns

Station	Slope	Lt.	L	Rt.
2+50		14' Lt = 392.35	392.25	392.50
2+00		14' Lt = 392.29 Finish	392.20	392.55
1+50		14' Lt = 392.80 Exist 392.72	392.63	392.96
1+00		392.80 Exist 392.72	393.02	393.04
0+50	2:1	393.21	393.21	393.97
0+00 = B.C.	2:1 Lt	394.65		

Grod. & Line Change
 1440 to 4+00. See P-19

392.50

Rt. Slope	S.R.P.	L
F0.35	F0.2 18.4	F0.50 12' Rt of L
F0.1	C1.6 22.6	F0.40 F0.08 5' Rt of edge of -19' Lt L
0.00	C0.1 18.1	F0.07 5' Rt of P.C. -12' Lt of L
F0.3	F0.1 18.2	
F0.1	0.0 18	
F0.3 5' R.P.	F0.2 18.4	

BM checked MK on Hd. wall

Access Road

Lt

Rt

5

Stations	Slope	Lt.	L	Rt.	Slope	5'RP	L	5'RP
		F 1.11 92.65 93.76		F 0.79 92.77 93.76				
5+50	2:1	393.60	394.00	393.60		0.0 F 1.0 20.0		F 1.3 20.6 0.2 4.0 RP
		C 0.67 94.18 93.51		3.65 89.86 393.58				
5+00	1:1	393.35	393.75	393.35 - shoulder		F 0.6 C 1.45 22.45		F 3.35 24.7 F 0.1
4+50	1:1	393.10	393.50	393.10	2:1	C 0.1 2.0	C 3.3 24.3	F 3.9 25.8 F 0.2
				392.83				
4+00	2:1	392.85	393.25	392.85	2:1	G 2.3 F 1.65 21.3		F 2.65 23.3 C 0.5
3+50	2:1	392.60	393.00	392.60	2:1	← 0.2 F 0.6 19.2 F 1.6 21.2 on Top Pipe		F 0.85 19.7 F 0.5 19.0 on Pipe ← 0.8
3+00	2:1	392.35	392.75	392.35	2:1	G 0.6 F 2.0 22.0		F 1.84 19.7

← Grades & Line Change →
 1440 to 4100 P-15

Access Road

Lt

E

Rt.

6

Stations

5' RP

5' RP

	<u>C 1.40</u>		<u>00.51</u>
	5.40		4.52
	94.01		94.01
7+50	393.85	394.25	393.85

	F0.1	C 1.8	C 0.8
		22.8	21.8
			F0.1

	<u>C 1.60</u>		<u>00.16</u>
	5.74		4.30
	94.14		94.14
7+25 BM	393.98	394.38	393.98

	C 0.2	C 1.5	C 0.5
		22.5	21.5
			F0.2

	<u>00.53</u>		<u>F0.80</u>
	4.79		3.46
	94.26		94.26
Bk 6+75	394.10	394.50	394.10

	C 0.1	C 0.7	F0.5
		21.7	19.0
			F0.1

	<u>F 0.62</u>		<u>F 1.57</u>
	3.52		2.58
	94.14		94.14
Bk 6+25	393.98	394.38	393.98

	0.0	F 0.5	F 1.2
	19	19	20.4
			F 0.3

	<u>F 0.84</u>		<u>392.96</u>
	3.52		4.56
	94.06		94.06
E.C. Bk 6+6.97	393.93	394.33	393.93

BM 2
H.S.B.
6+16.97
F 1.51

	E 0.2	F 0.8	F 1.4
		19.6	20.8
			F 0.20

	<u>F 0.79</u>		<u>F 1.70</u>
	3.22		2.27
	94.01		94.01
6+00	393.85	394.25	393.85

Access Road

Station	slope	Lt		Rt		slope	Lt		Rt 7	
		5'RP	4'	5'RP	4'		5'RP	4'		
10+50	2:1	F 052 1.99 92.51 392.35	392.75	F 067 1.84 92.51 392.35	2:1	0.0	F 0.3 18.6	F 0.6 19.2	0.0	
10+00	1:1	C 117 4.53 92.76 392.60	393.00	C 104 3.80 92.76 392.60	1:1	0.0	C 1.8 22.8	C 1.2 22.2	0.0	
9+50	1:1	C 242 5.43 3.01 392.85	393.25	C 089 2.90 93.01 392.85	1:1	0.0	C 2.5 23.5	C 1.3 22.3	F 0.3	
9+50	42' Rt 9+00 B.M. on Spike									
9+00	1:1	C 013 2.79 93.26 393.10	393.50	F 0.53 2.79 93.26 392.34	2:1	0.0	C 0.3 21.3	F 0.4 18.8	0.0	
8+50	2:1	F 088 2.63 93.51 393.35	393.75	F 148 2.03 3.51 393.35	2:1	0.0	F 0.9 19.8	F 1.3 20.6	0.0	
8+00	1:1	C 087 4.63 3.76 393.66	394.00	C 031 4.07 3.76 393.60	1:1	0.0	C 1.0 22.0	C 0.6 21.6	F 0.1	

Access Road

Lt

L

Rt

8

Station	Slope	Lt	L	Rt	Slope	5'RP	5'RP
			C 0.54 1.55 91.01	F 0.23 0.78 91.01			
13+50	1:1	390.85	391.25	390.85		F 0.1 C 0.8 21.8	0.0 18 0.0
			C 0.75 2.01 91.26	F 0.22 1.04 91.26			
13+00	1:1	391.10	391.50	391.10		C 0.1 C 0.8 21.8	0.0 2.1 F 0.1
			C 0.79 2.230 91.51	F 0.57 0.94 91.51			
12+50	1:1	391.35	391.75	391.35	2:1	G 0.1 C 0.8 21.8	F 0.3 18.6 F 0.1
			F 0.28 1.48 91.76	F 1.44 0.32 91.76			
12+00	2:1	391.60	392.00	391.60	2:1	C 0.1 F 0.2 18.4	F 1.2 20.4 F 0.1
			F 1.06 0.95 92.01	F 2.68 0.33 92.01			
11+50	2:1	391.85	392.25	391.85	2:1	C 0.3 F 1.2 20.4	F 2.5 23.0 0.0
2 Lath 11+50	1:1		F 1.86 0.41 92.26	F 1.71 0.41 92.16	390.95		
11+00	2:1	392.10	392.50	392.10	2:1	C 0.1 F 1.2 20.4	F 1.6 21.2 0.0

Access Road

Lt

Rt. 9

Stations	Slope	Lt	E	Rt.	5'RP	5'RP
		<u>C2.50</u> 2.57		<u>C2.23</u> 1.74		
16+50	1:1	89.51 389.35	389.75	89.51 389.35	1:1 C0.2 23.5	C2.5 23.4 0.0
		<u>2.34</u> 2.19		<u>C1.71</u> 1.47		
16+00		89.76 389.60	390.00	89.76 389.60	1:1 C0.1 23.5	C2.4 23.0 F0.1
		<u>C1.33</u> 1.34		<u>C1.05</u> 1.06		
15+50	1:1	90.01 389.85	390.25	90.01 389.85	1:1 C0.1 22.4	C1.4 22.2 0.0
		<u>C1.02</u> 1.28		<u>C0.44</u> 0.70		
15+00	1:1	90.26 390.10	390.50	90.26 390.10	1:1 C0.1 22.1	C1.1 21.7 F0.1
B.M. on stub 14+50 26.8 ft.		<u>C0.63</u> 1.14		<u>F0.09</u> 0.42		
14+50	1:1	90.51 390.35	390.75	90.51 390.35	1:1 0.0 21.8	C0.8 21.2 F0.1
		<u>C0.49</u> 1.25		<u>F0.55</u> 0.21		
14+00	1:1	90.76 390.60	391.00	90.76 390.60	1:1 C0.3 21.3	C0.3 21.0 F0.4

Access Road

Lt.

L

Rt.

10

Station	Slope	Lt.	L	Rt.		5' R.P.			5' R.P.
19+30.42			387.83 388.02						
50' Ret. on Rt. 19+29.93				.42 387.62					
			C 5.09 3.00 387.91	C 3.05 0.96 387.91					
19+00			387.75 387.85	388.15 388.25	387.75 387.85	4:1	C 0.2 26.0	C 5.0 24.2	0.00 F 0.1
			C 4.81 3.20 88.39	C 5.15 3.54 88.39					
Brk 18+50	1:1		388.23	388.63	388.23	1:1	C 0.1 25.9	C 5.2 26.2	C 0.2
5' TP on 11" x 2" 25' Rt 18+00			C 4.43 3.16 88.73	393.38 4.33 88.73					
Brk 18+00	1:1		388.57	388.97	388.57	1:1	C 0.1 25.5	C 4.2 25.2	C 0.4
			C 4.00 3.01 89.01	C 3.65 3.66 89.01					
Brk 17+50	1:1		388.85	389.25	388.85	1:1	F 0.1 25.3	C 3.1 24.1	C 0.7
			C 3.08 2.34 89.26	C 1.96 1.22 89.26					
17+00	1:1		389.10	389.50	389.10	1:1	C 0.1 24.1	C 2.1 23.1	0.0

Access Road

Station	Slope	Lt.	L	Rt.	5' RT.
Ret. RT. ③ = EC.				86.16 4' from Par.	
②				86.59 4' from Par.	
①				387.06 C 0.65 8.15 387.50 = Par. 387.42 1:1	00 C 0.1 4.0 from Par.
EC. Ret. RT. 19+29.93					C 0.9 F 0.1 21.9 from Par.
Ret. in Lt ③ = EC.			edge Par. 11	388.54 4' from Par.	388.66
②		388.14			388.22
①		387.72			387.80
EC. Ret. Lt 19+30.90			0.11	387.52 387.60 4' from Par.	C 2.4 90.11 387.70 = edge Par

Water
Spikes on
Ret. RT.
are 2' from
Par.
with
1:1 slope.

C 0.2 C 2.4
23.4

Access Road
Grades - 6" V.C. Sewer
Plan 7761-L

12

1+20 = End.	390.00
0+80	390.40
0+40	390.80
0+00	391.20

Access Road

Grades - Culverts

	Elev. Invert.	Cuts	Offsets
0+72 = End	386.45 384.00	2.45	
0+36	384.60		
0+00 = Beg. 18" Corrug. Iron Pipe	388.39 385.20	3.19	
	387.66		B.M. on Hub P-3
0+62 = End Ditch	389.60		
- Beg. Ditch			
0+44 = End Pipe	392.90 389.70	3.20	
0+00 = Beg. 18" Conc. Culvert	390.92 390.00	0.92	
	392.50		B.M. on Hd. Wall per Plan

Access Road

14

Grades 6" V.C. Sewer

Location sketch P-18

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W.K.
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	El.	Invert	Cuts	offset
17.20	39225	39000	2.25	6' 4"

0 + 00	39601	39120	4.81	6' 4"
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37296

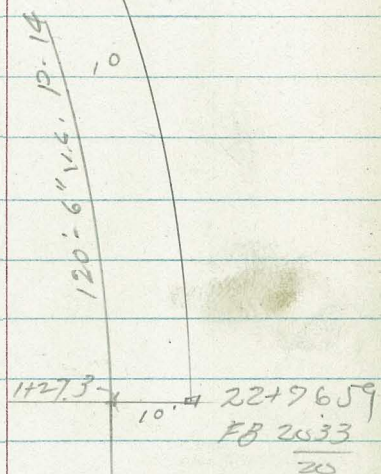
B.M. 2 Hub 6+16.97 P-6

Gibbs Airport

Grades 3" Drain Tile

El. Invert

1+27.3	396.01	391.20	4.81	6' Lt.
+97	397.12	392.13	5.00	3' Rt.
+66	397.72	393.20	4.52	
0+35	398.52	394.27	4.25	
0+00				



1427.3-10.4 22+96.59
 FB 2033
 20

0+35

Exist
 and drain
 tile

Walker
F. Gregory
G. Pope
R. Sisson
3-28-50

Access Road - Gibbs Airport.

Location & Grades
for 30" Concrete Pipe Culvert
at Sta. 11+38.

INDEXED

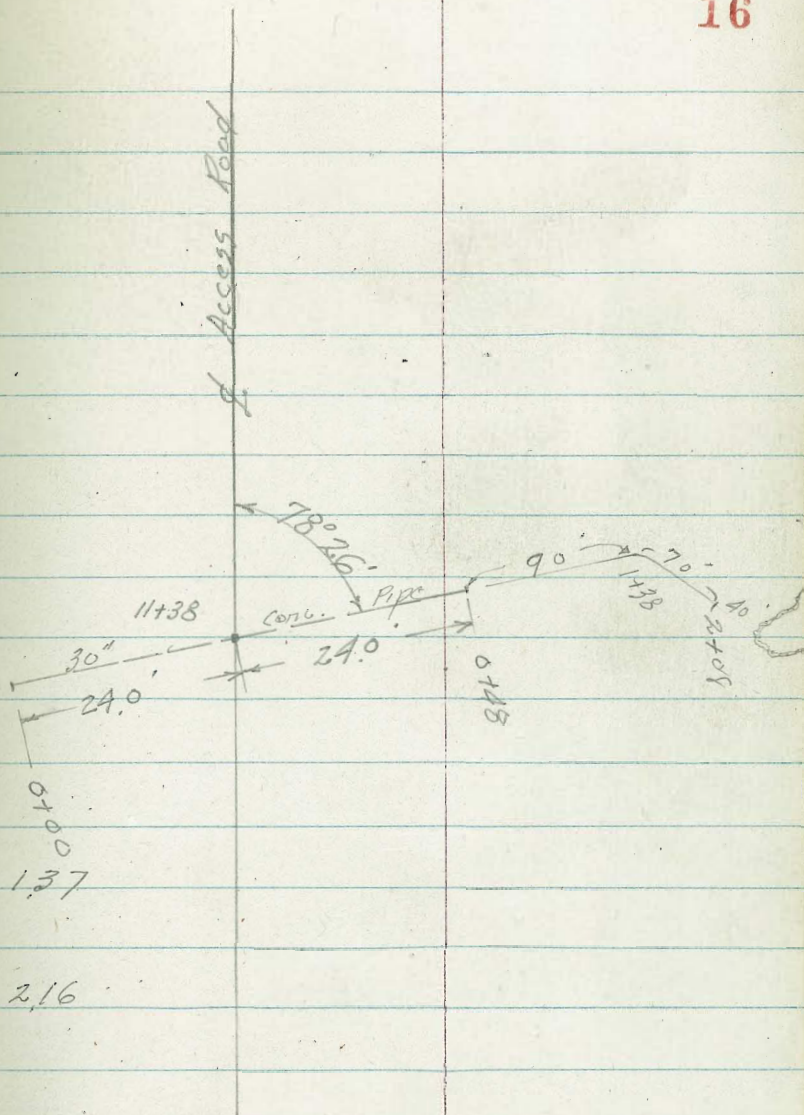
W.K.
MAY 8 1950

2+08	387.29	386.45	C 084
1+38 - ditch	388.20	386.80	C 140
0+48 = End Pipe	388.62	387.25	C 137
0+00	389.66	387.50	C 216

322.34

43 RT
BM on stake 9+00 P-7

16



Finish Grades of 2" Water Main
Access Road - Gibbs

17

Access Road

7+87

El.
Finish
13' off of $\frac{1}{2}$
39436 392.68

C 0.68

7+61

39536 393.80

C 1.50

7+87
2" Water
7+61

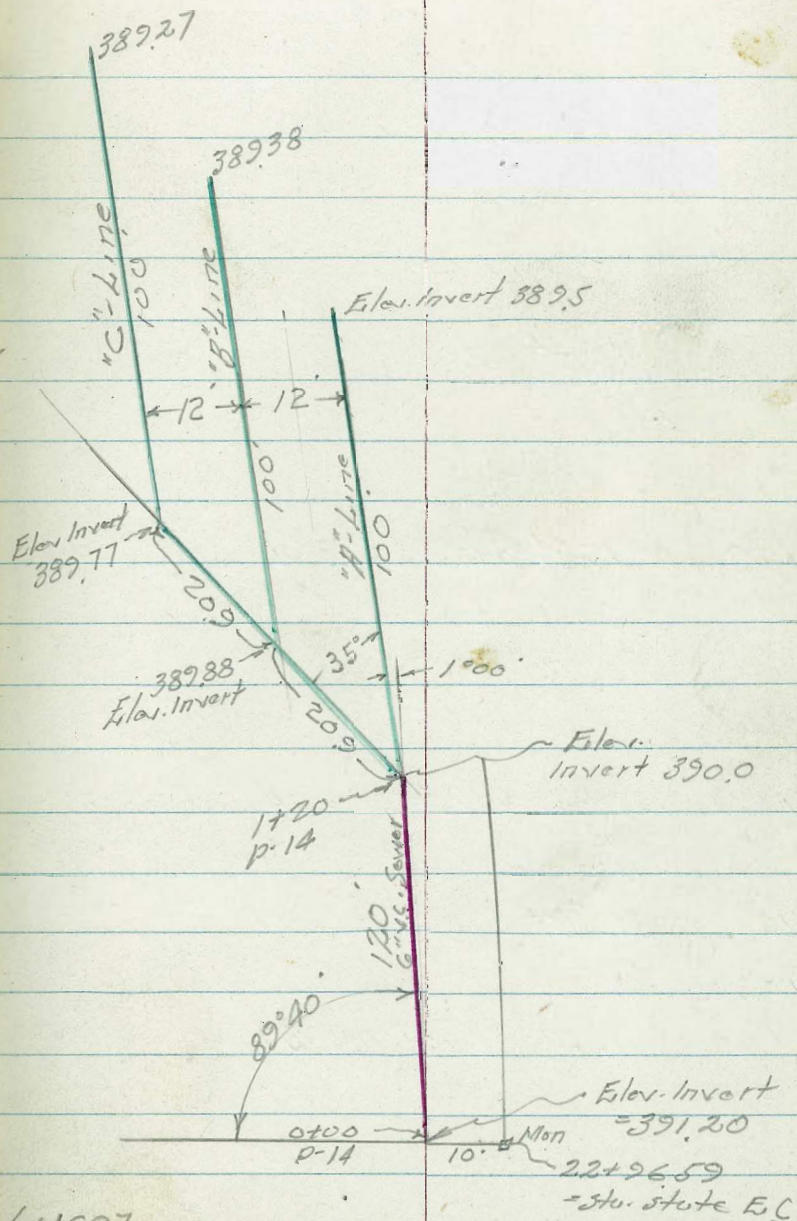
392.34 BMP-7

Gibbs Airport
Access Road

Grades for Drain Tile

	Elev. stakes	Elev. Invert	Cuts
1+00 "C" line	392.30	389.27	3.03
0+50 "C" line	392.77	389.52	3.25
	392.37		2.60
0+00 "C" line	392.93	389.77	3.16
1+00 "B" line	392.14	389.38	2.76
0+50 "B" line	392.16	389.63	2.53
0+00 "B" line	392.20	389.88	2.32
1+00 "A" line	391.67	389.50	2.17
0+50 "A" line	392.23	389.75	2.48
0+00 "A" line	392.25	390.00	2.25

392.96 B.M. & Hub Sta 6+1697



Access Road - Gibbs

Change in Line & Grade
from 1+40 to 4+00

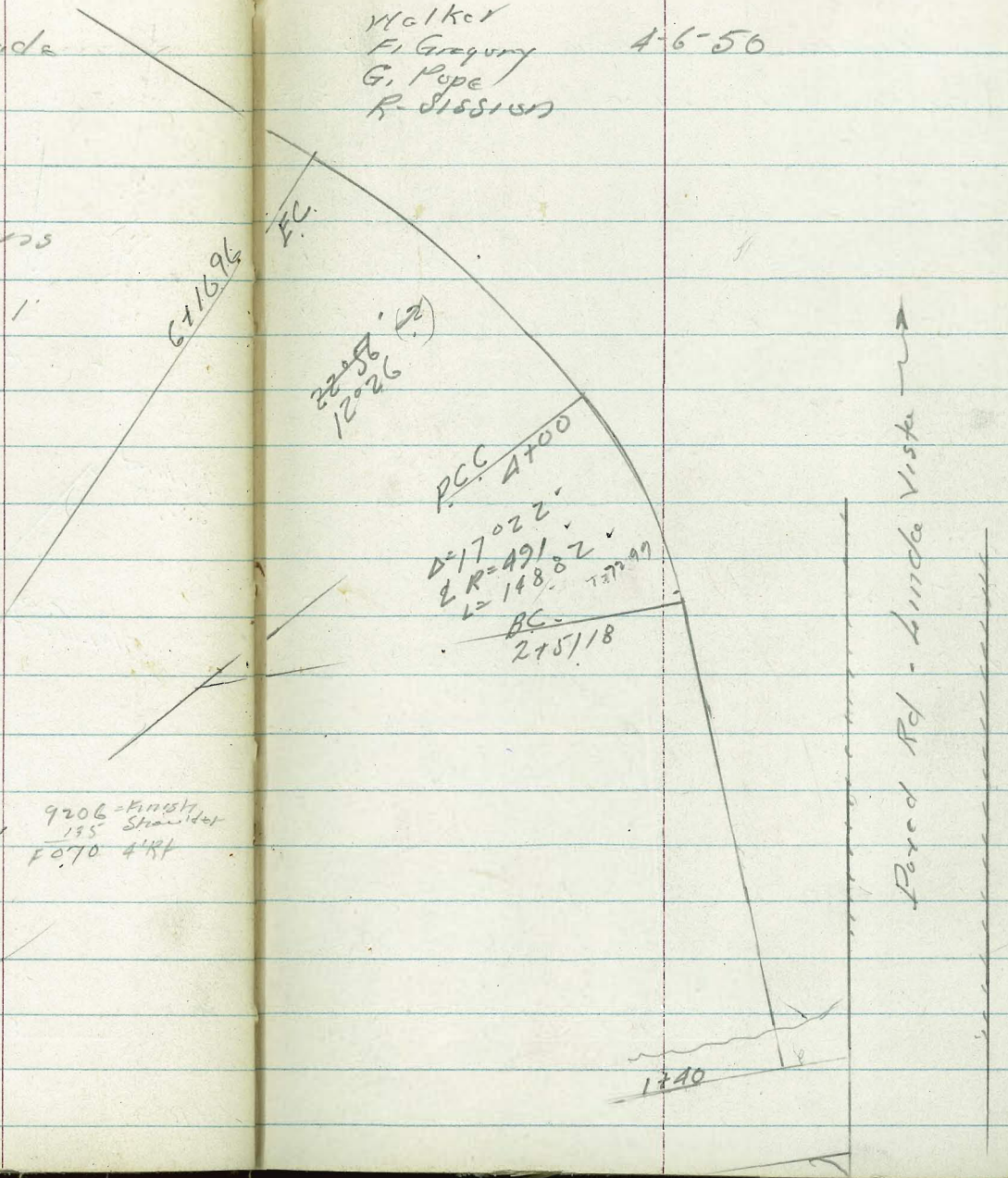
Finish Elevations

Station	14'L	2'	14'R	1'
4+00	393.01	393.25	393.01	
3+50	392.76	393.00	392.76	
3+00	392.36	392.60	392.36	
2+50	392.21	392.45	392.21	
2+00	392.27	392.51	392.27	
1+40	92.80	92.78	93.02	

9206 - Finish
195 Station
E070 4'R

Change etc
Per Inst. F.F. Gabrielson

Walker
F. Gregory 4-6-56
G. Pope
R. Sisson



~ Clinton Street ~

Walker
F. Gregory
C. I. Opt
R. Sission
1-21-50

Grades Sewer Laterals

on South Side from 37th to 38th

INDEXED

MAY 8 1950
W.R.

Station

5+99.9 = W.L. 38th

5+35 Lot # 8

357 100.09 95.01

5.08

4+35 = Lot # 7

390 99.76 94.71

5.05

4+10 Lot # 6

395 99.71 94.63

5.08

Lot # 5

3+60 already installed by city

3+35 Lot # 4

326 100.40 94.40

6.00

3+10 = Lot # 3

273 100.94 94.33

6.61

2+10 = Lot # 2

308 100.58 93.87

6.71

0+60 = Lot # 1

712 96.54 90.85

5.69

0+00 = E. Line 37th

816 103.66

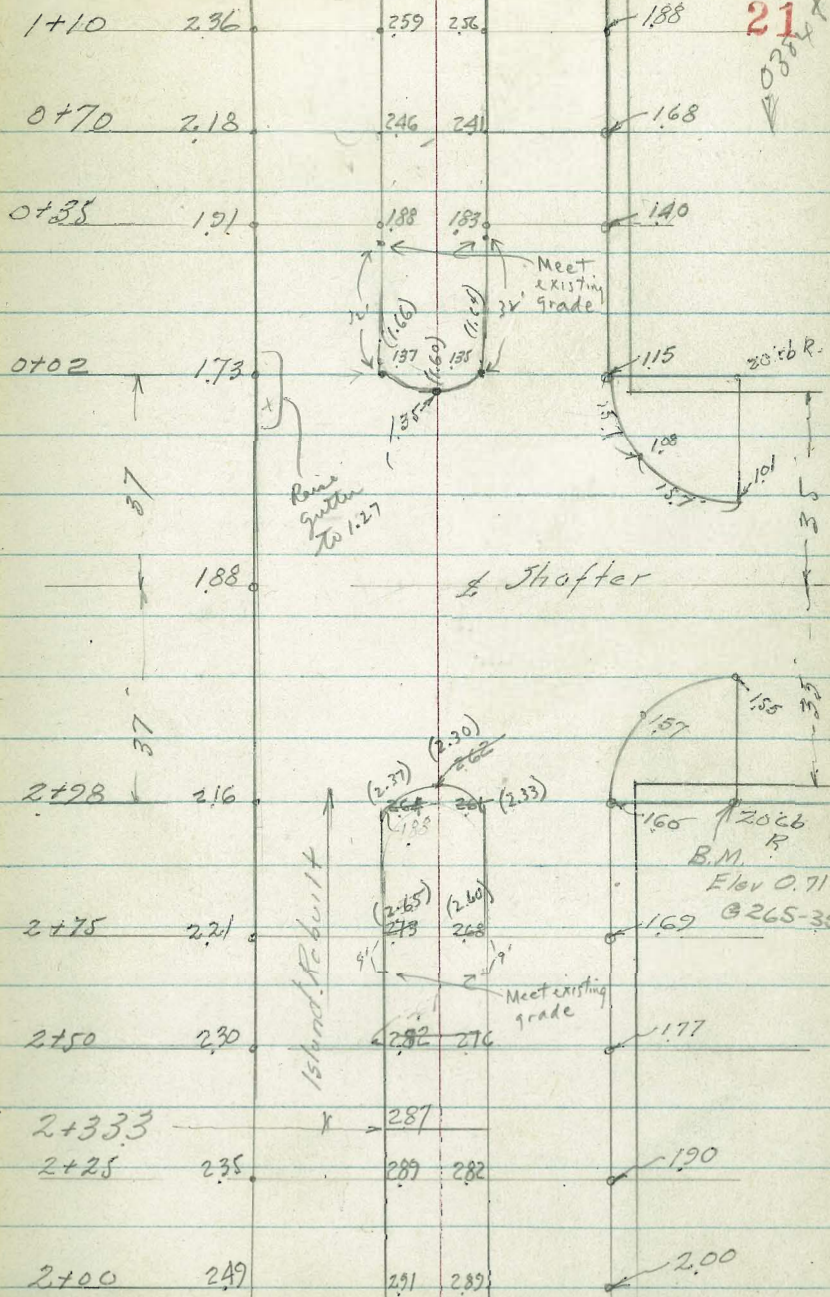
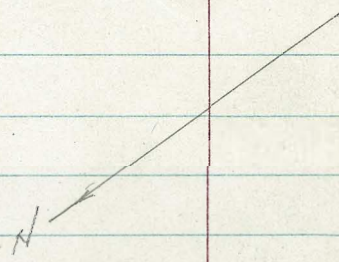
95.50

B.M. = Top cb 0+00 FB 1827-44

CURB Elevations
Lowell & Shafter

Walker
F. Gregory
G. Pope
R. Bission
5-8-50

INDEXED
W.K.
MAY 8 1950



Grades - Extension Culvert

Block - From Southlook

Mulker Plan 8026-L

F. Gregory

G. Pope

R. Sisson

5-17-50

INDEXED
 MK
 SEP 8 1950

11.98' East
 (2+18.93) FB 2029-17

0.01
~~34.95~~
 34.96

Chk. Flow East Pipe

Elev.

Invert

Cuts

offsets

1+12 = End

4061 35.30

5.31

7' Lt.

0+80

4309 35.88

7.21

"

0+40

4486 36.50

8.26

"

0+00 = beg. 18" Con. Pipe

4305 37.30

5.75

"

North end Inlet

Fl. Ch.
 93
~~42.90~~

East cb.

South end "

42.85

42.93
~~42.90~~

F008

42.95

B.M. Chisled Mark in walk

0+00' A line FB 2029-14

Ditch Grades

47th & S.D. & E. R.R.

2
Survey
10110

23

Walker
F. Gregory
G. Pope
R. Sisson
5-17-50

Plan 3938-B

Slopes 1:1

NO 20622

INDEXED

mk.
SEP 8 1950

0+61

86.00
87.3
C 1.3
33

86.00
87.7
C 1.7
7.7

0+40

86.00
87.0
C 1.0
3.0

86.00
88.2
C 2.2
6.2

0+12

0+12

86.00
89.0
C 3.0
5.0

86.00
89.5
C 3.5
7.5

0+00

GD = 86.00
87.69
C 1.69
5.1

8418

BM NE.B.D PERH +97th

Curb Grades - ORANGE AVE.
on South Side
Between Chamoune & 46th

Walker

cb.
line

24

2+70.08 = 146th

353.60^{66=East.}

2+40.08

353.41⁴⁵

2+10.08

INDEXED
M.K.
SEP 8 1950

353.22²⁵

1+80.08

353.02⁰⁴

1+47.04 = F.C. 2' Radius

352.81

1+45.⁰⁴ = Reg. Curb = E. Line Alley

Prop Line
352.82 352.95 - Grad
2 353.80 - Stake
= F.C.
3'R C 0.85

0+00 = E. Line Chamoune

353.94

Walker
F. Gregory
G. Pope
R. Sisson
5-31-50

Orange Ave - Parking

From Highland Ave to 46th

Actions Cont. p. 26

2 + 70 = - W.L. 45th

2 + 40 = - B.K.L.

2 + 10

1 + 80

+

1 + 47 = E.C.

1 + 48 = E.L. Alley

1 + 25 = E.C. 2' R

1 + 23 = B.C. 2' Alley R

0 + 90

0 + 60

0

0 + 30

0 + 00 = E.L. Highland

Lt.

L

Rt

25

cb.

Ent

1/4

1/4

Ent

cb.

352.04

352.47

351.71

352.15

352.51

351.21

352.27

352.11

352.39

352.31

352.52

352.52

352.93

353.04

352.62

352.62

352.74

352.90

352.86

353.11

352.98

353.62

353.31

353.10

353.95

353.52

INDEXED

MS.

SEP 8 1950

Orange Ave. - Peunoy

Cont. from P-25

Stations

Cont. on P-27

2+70 = W.L. Chamoune

2+40

2+10

1+80

1+47 = E.C. 2' R

1+45 = B.C. Alley R on Alley

1+25 = E.C. Alley R

1+23 = B.C. 2' Alley Roadway

0+90

0+60

0+30 = Bk on L

0+00 = E.L.M.C 45th

Lt

FF

26

Gutter

1/4

1/2

1/4

Cent.

350.39

350.35

350.55

350.46

350.71

350.57

350.87

350.68

351.03

350.79

351.13

350.94

351.30

351.05

351.45

351.15

351.60

351.90

351.36

351.75

352.13

351.37

Orange Ave - Paving
 Cont. from P-26

Stations	Lt		L	Rt	
	Out.	$\frac{1}{4}$		$\frac{1}{4}$	Out.
2+70 = W.L. 46 th	353.32			352.96	
2+40	353.07			352.76	
2+10	352.82			352.56	
1+80	352.57			352.36	
1+47 = E.C. 2' Alley R	352.29			352.14	
1+45 = B.C. 2' Alley R. on Alley					
1+25 = E.C. 2'R					
1+23 = B.C. 2' Alley R	352.10			351.98	
0+90	351.86			351.78	
0+60	351.69			351.60	
0+30 = Bk E	351.41	351.91		351.41	
0+00 = E. line Chamoune	351.19	351.49		351.23	

27

Grades - Extension 30" Culvert
 N.Y. of California St.
 at Alameda Place

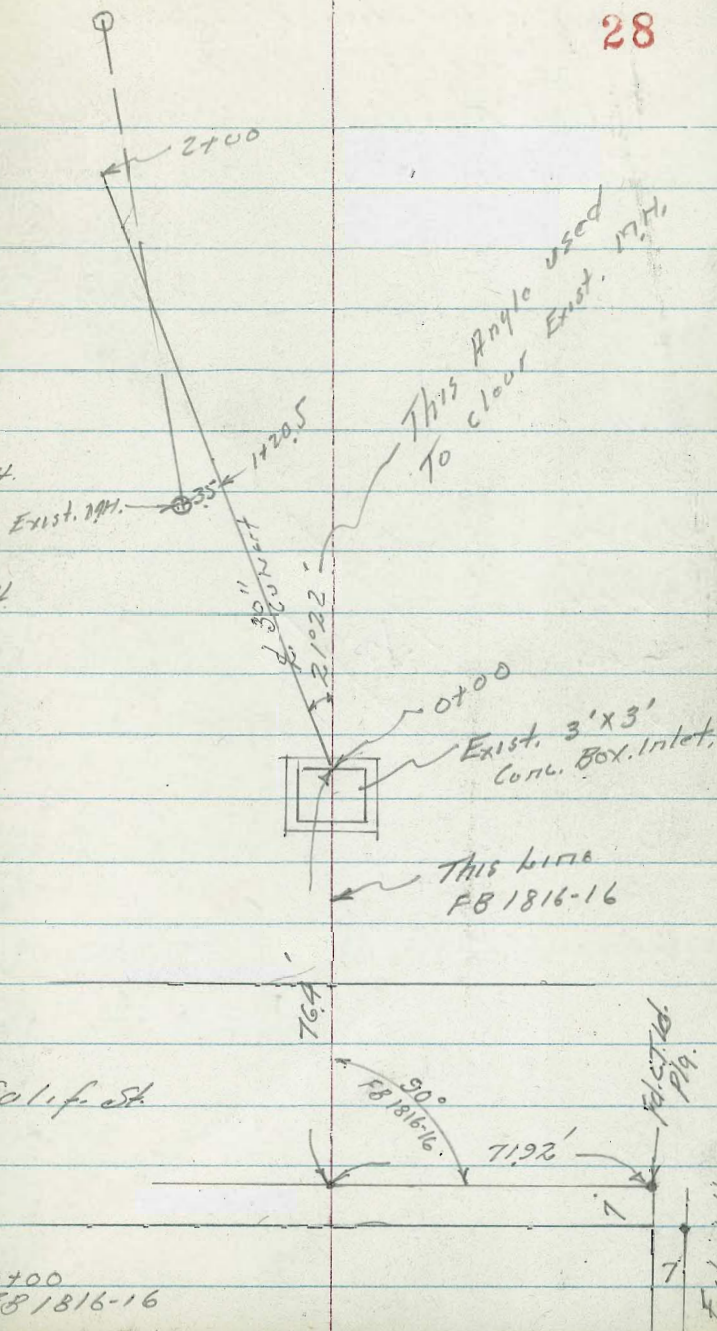
Walker Plan 4015-B No 20686
 G. Pope
 R. Sisson
 8-18-50

INDEXED

WTK.
 SEP 8 1950

	Elev. Stakes	Elev. Invert	Cuts
2+00	125.0	122.00	C 3.00
1+60	121.32	119.70	C 2.62
1+20.5 = Exist. MH 3.5' dia			
1+20	118.45	117.40	C 1.05
0+80	116.90	115.10	C 1.80
0+40	116.50	112.80	C 3.70
0+00	116.74	110.50	C 6.24

BM.
 114.16 on long box 0+00
 FB 1816-16



Walker
Rope
D. Sisson
Hatch
8-21-50

Promontory-Grades

6" Water Main

from Fortuna to Pacific Beach Drive

Plan # 775-B-14031396

	Elev. Stakes	Elev. Bottom Trench	Cuts	Offsets
5+25.21		38.63		
5+00				
4+80		38.85		
4+40		39.05		
4+00		39.25		
3+60		39.45		
3+20		39.65		
2+80		39.85		
2+40 = P.V.C.		40.06		
2+00		40.32		
1+60		40.57		
1+20 = P.V.C.		41.30		
0+80		41.76		
0+40		42.32		
0+00		42.88		

Void

43.54

BM. on Cul stake 0700 3' Bolt
FB-rod 260-19

5+25 21	40.46
5+25 21	42.46
5+00	
4+60	
4+20	40.60
4+00	40.47
3+60	40.26
3+20	40.15
2+80	40.03
2+40	39.83
2+00	39.63
1+60	39.43
1+20	39.23
0+80	39.03
0+40	38.83
0+00	38.63

~~Void~~

Promontory - Grades 6" Water Main

Plan 775-L No. 31396

from Fortuna
to Pacific Beach Drive

chk 41852) cut on R. 002
GN 26049 1568
1566

INDEXED

W.K.

SEP 8 1950

5+252) Top Exist. Pipe

El. stake Elev. Bottom Ditch

Cuts offsets

Station	El. stake	Elev. Bottom Ditch	Cuts	offsets
5+252)	46.01	42.66		
4+80	45.02	42.08	2.94	5' R.
4+40	44.55	41.56	3.0	"
4+00	44.06	41.05	3.01	"
3+60	43.76	40.60	3.16	"
3+20	43.39	40.20	3.19	"
2+80	43.04	40.03	3.01	"
2+40	42.88	39.83	3.05	"
2+00	42.74	39.63	3.13	"
1+60	42.54	39.43	3.11	"
1+20	42.41	39.23	3.18	"
0+80	42.36	39.03	3.33	"
0+40	42.25	38.83	3.42	"
0+00 = H.L. Fortuna	42.25	38.63	3.62	"

43.54

Elev. stake
0+00 GN 260-49

PAVING GRADES - DRAPER

ST.

32

from Gentry to Marine

Walker Plan 7818-L No 31622

Pope
K. Sisson
Hubb
8-21-50

Station	Finish	Subgrade	offsets
2+87.5	101.17	100.75'	15' 2"
2+60	101.43	101.01'	"
2+30	101.71	101.29'	"
2+00	102.00	101.58'	"
1+75 = E.V.C	102.24	101.82'	"
+65 B.K	102.36	101.94'	"
+55 "	102.52	102.10'	"
+45 "	102.67	102.25'	"
1+35 = B.K	102.90	102.48'	"
1+10 = B.K	103.52	103.10'	"
0+85	104.15	103.73'	"
0+60	104.78	104.36'	"
0+35	105.40	104.98'	"
0+10 B.K	106.03'	105.61'	"
0+00	106.17	105.75'	"

INDEXED
SEP 8 1950

106.32

511
B.N. B.P. Draper & Gentry

Draper Cont. from p. 32

Stations	Elev. Finish Grade ±	
4+84.85 = 8th. Main St	98.81 [✓]	98.39
+75' Bk.	99.17	98.75 [✓]
+65' Bk.	99.37	98.95 [✓]
4+55' Bk.	99.57	99.15 [✓]
4+27	99.83	99.41 [✓]
3+99.5	100.09	99.67 [✓]
+71	100.36	99.94 [✓]
3+43	100.63	100.21 [✓]
2+15	100.90	100.48 [✓]

TYRIAN ST. PAVING
Plan 7712-4 NO 31347

34

Walker Gutter Grades
Pipe
P. Sission
Hatch
8-21-50

INDEXED
MK
SEP 8 1950

6890 6930

6889 6929 0+95

6882 6922 0+75

6875 6915 0+50

6867 6907 0+25

6860 6900 0+00

6855 6897

6845 6896

Tyrian

SURVEY - PROPOSED DRAIN

Lot 10 - Block 172 - Roseville

Walker
R. Sisson
9-5-50

Mo 20703

----- Proposed Drain

Stations on Proposed Drain

Levels - P-36

INDEXED

W.K.

SEP 8 1950

Junction

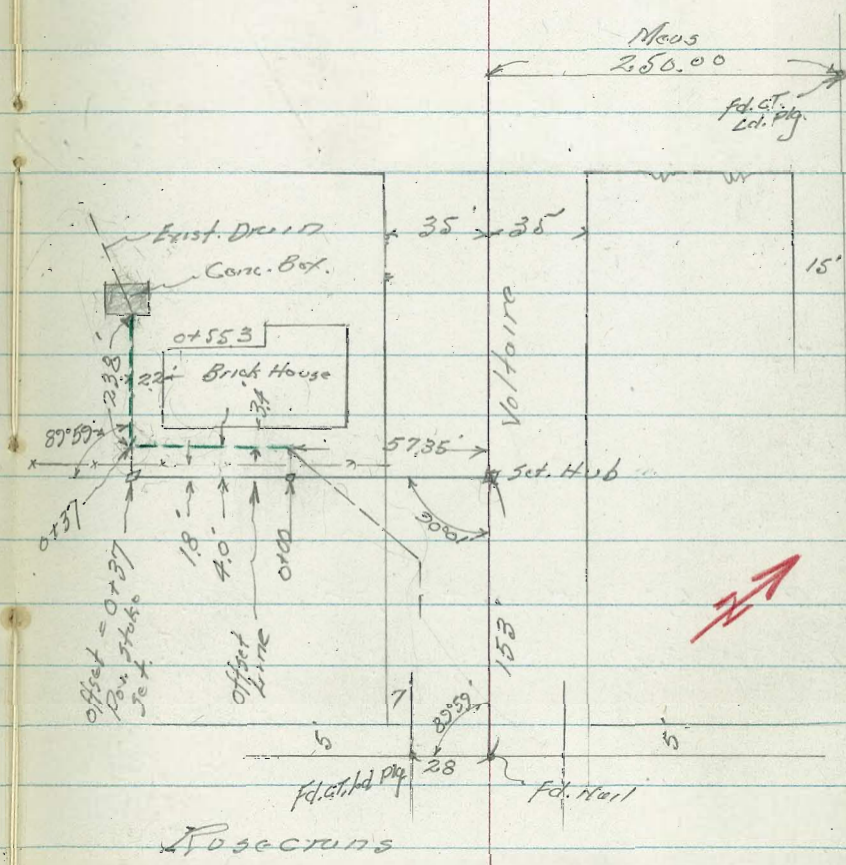
Req. Exist. Drain To West

0+60.8 = Exist. face Conc. Box

0+37 = Δ Rt. 89°59'

0+00.25 Pav. Hub Set 4" ht.

0+00 = Exist. 18" Corrugated Iron Pipe



Rosecrans

Levels - Proposed Drains
 Lot 10 - Blk - 172 - Roseville
 Location P-35

0+37 = A R₁

0+03 to doorway to Basement.

0+00

0-23

TR 6.07 H=43.42 0.84 37.35 ✓

TR 12.49 38.19' 0.60 25.70 ✓

12.92 3W City Disc.
 7' line Voltaire
 5' line Roseville 13.38

TR 12.72 26.30' 2.38 13.58 ✓

TR 10.64 15.96' 5.59 5.32 ✓

TR 4.54 10.91' 5.93 6.37 ✓

TR 3.59 12.30' 6.97 8.71 ✓

6.91 15.68' 8.77 ✓

38.1
 5.3
 4

38.2
 4.9

38.60
~~38.2~~
 3.4
 Basement Floor

38.1
 5.3
 5

35.9
 8.35
 invert

39.1
 4.3
 0

39.1
 4.3
 3

36.9
 6.5
 5

38.2
 5.2

38.2
 5.2
 5

H=43.42 ✓

B.M. on City Disc. Roseville & Lowell
 Grade Book 265 - P-8

Lot. 10 Block 172
 Roseville
 Levels - Drain

Lt. 2 Rt. 37

chk BC 43' R 5.44
 Top cb Resections & volume 13.34 18.35
 T.P. 0.99 26.69 1233 28.70
 T.P. 0.68 38.03 607 37.35

0 + 50

0 + 40.4 = E. Edge Brick Bld.
 43.42

44.4	44.3	40.83	42.5
+1.0	+0.90	2.59	5.9
5	0	Invert.	
	Top Box.		
	44.0	40.37	43.3
	5.4	3.7	4.1
			2.2
	40.2	39.2	38.9
3.2	4.2	4.5	
5		2.2	

43.42

REDUCED 9-6-50 AEX

Ingram St. Curb Grades East Side
 Between Grand Ave & Hornblend

Indexed
 11-5-51

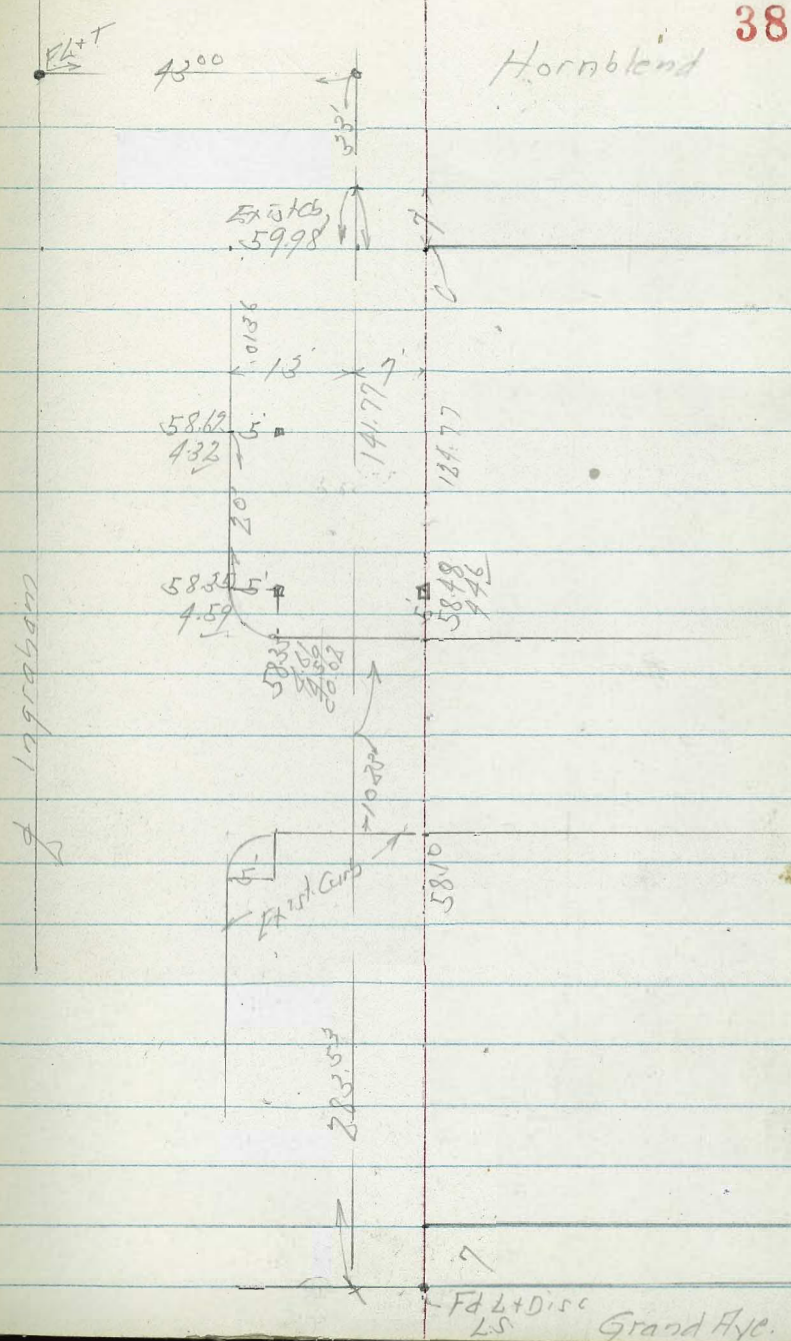
BM 7.25 5909
 6.60 62.94 2.75 5634

N.A.R.P.
 51.84 Grand Ave
 + Sewer

July 5. 51
 F. Sisson
 Rorer
 Bertolucci
 Fritz

NO. 20 007

LOT 1-2 BLK. 236 ADD. Pac. Beach
 OWNER Henry Rigali
 CONTR. Silver Strand Constr
 PERMIT NO. 48301



Garber
Shepherd
Bartolucci
Fritz
W.O. 20773

Aug. 15, 51
Sewer Replacement
Lexington Ave. Wabash Free-
Way east

Indexed
11-5-51
2010

1+00
172.04
156.16
15.88
8.89
C-6.99

+25

172.04
159.54
12.50
5.62
C-6.88

+50

172.04
162.91
9.13
2.91
C-6.22

+75

182.31
166.29
16.02
9.89
C-6.13

10.47 182.31 0.20 171.84

+75
172.04
155.49
16.55
9.34
C-7.21

2+00

172.04
158.86
13.18
6.22
C-6.96

+25

172.04
162.24
9.80
3.28
C-6.52

+50

172.04
165.61
6.43
0.20
6.23

+50
172.04
154.81
17.23
9.70
C-7.53

+75

172.04
158.19
13.85
6.78
C-7.07

3+00

172.04
161.56
10.48
4.10
C-6.38

+25

172.04
164.94
7.10
1.14
C-5.96

+25
172.04
154.14
17.90
10.24
C-7.46

+50

172.04
157.51
14.53
7.46
C-7.07

+75

172.04
160.89
11.15
4.55
C-6.60

4+00

172.04
164.26
7.78
1.77
C-6.01

0+00
172.04
153.46
18.58
10.84
C-7.74

+25

172.04
156.84
15.20
8.11
C-7.09

+50

172.04
160.21
11.83
5.16
C-6.67

+75

172.04
163.59
8.45
2.43
C-6.02

10.59 172.04

161.45 N-edge
Ex.M.H. 0+00

6+00	182.31 <u>169.58</u> 12.73 <u>6.36</u> C-6.31	+25	182.31 <u>172.82</u> 9.49 <u>3.58</u> C-5.91	+50	190.27 <u>176.06</u> 14.21 <u>7.78</u> C-6.43	+75	190.27 <u>179.30</u> 10.97 <u>4.06</u> C-6.91
------	---	-----	--	-----	---	-----	---

8.22 190.27

182.31 0.26 182.05

+75	182.31 <u>168.93</u> 13.38 <u>7.05</u> C-6.33	7+00	182.31 <u>172.17</u> 10.14 <u>3.93</u> C-6.21	+25	182.31 <u>175.41</u> 6.90 <u>0.26</u> C-3.64	+50	190.27 <u>178.65</u> 11.62 <u>5.24</u> C-6.38
-----	---	------	---	-----	--	-----	---

5+50 Ahead	182.31 <u>168.28</u> 14.03 <u>7.79</u> C-6.24 M.H.#1 12°16' RT Ref. Pt. on L Split. 4.52-14.52-24.52 (C-6.58) 14.52	+75	182.31 <u>171.52</u> 10.79 <u>4.58</u> C-6.21	8+00	182.31 <u>174.76</u> 7.55 <u>0.87</u> C-6.68	+25	190.27 <u>178.00</u> 12.27 <u>5.60</u> C-6.67
------------	--	-----	---	------	--	-----	---

+25	182.31 <u>167.64</u> 14.67 <u>8.62</u> C-6.05	+50	182.31 <u>170.87</u> 11.44 <u>5.44</u> C-6.00	+75	182.31 <u>179.11</u> 8.20 <u>1.71</u> C-6.49	9+00	190.27 <u>177.35</u> 12.92 <u>6.46</u> C-6.46
-----	---	-----	---	-----	--	------	---

5+00	182.31 <u>166.96</u> 15.35 <u>9.46</u> C-5.89	+25	182.31 <u>170.22</u> 12.09 <u>5.77</u> C-6.32	+50	182.31 <u>173.46</u> 8.85 <u>2.65</u> C-6.20	+75	190.27 <u>176.70</u> 13.57 <u>7.26</u> C-6.31
------	---	-----	---	-----	--	-----	---

Garber Aug. 17, 51
 Shepherd
 Bertolucci
 Fritz.

10+50 $\frac{197.29}{181.22}$ 11+00
 $\frac{16.07}{9.35}$
 C-6.72

10+25 $\frac{197.29}{180.59}$ 10+75
 $\frac{16.70}{9.90}$
 C-6.80

10.05 197.29

1.97 169.92 11.17 167.95

7 0.37 179.12 11.52 178.75

3.03 187.24
 Chis. □ Old M.H.
 Lt. 10+25

10+15.00 $\frac{190.27}{180.34}$
 M.H. #2 $\frac{9.93}{2.68}$
 Δ 0°09 Rt.
 Ref. Pts. on L Split. 7.25-C
 4.58 14.5 Rt.
 1x1 on Line Lt.
 10+52.10

10+00 $\frac{190.27}{179.94}$
 $\frac{10.33}{2.81}$
 C-7.52

190.27

197.29
 182.47
 $\frac{14.82}{7.79}$
 7.03

197.29
 181.84
 $\frac{15.95}{8.81}$
 C-6.64

187.24 T.B.M.
 No. Rim M.H. 0+00
 8.50 161.42 Rec. 161.45

167.95

178.75

+50 $\frac{197.29}{186.22}$
 $\frac{11.07}{4.43}$
 C-6.64

+25 $\frac{197.29}{185.59}$
 $\frac{11.70}{6.14}$
 C-5.56

12+00 $\frac{197.29}{184.97}$
 $\frac{12.32}{6.57}$
 C-5.75

+75 $\frac{197.29}{184.34}$
 $\frac{12.95}{7.02}$
 C-5.93

+50 $\frac{197.29}{183.72}$
 $\frac{13.57}{7.77}$
 C-6.40

11+25 $\frac{197.29}{183.09}$
 $\frac{14.20}{7.55}$
 C-6.65

14+00 $\frac{203.44}{189.97}$ 41
 $\frac{13.47}{5.07}$
 C-8.40

+75 $\frac{203.44}{189.34}$
 $\frac{14.10}{3.47}$
 C-8.63

+50 $\frac{203.44}{188.72}$
 $\frac{14.72}{5.95}$
 C-8.77

6.85 203.44 0.70 196.59

+25 $\frac{197.29}{188.09}$
 $\frac{9.20}{0.70}$
 C-8.50

13+00 $\frac{197.29}{187.47}$
 $\frac{9.82}{1.98}$
 C-7.84

+75 $\frac{197.29}{186.84}$
 $\frac{10.45}{3.25}$
 C-7.20

Sewer Connection No 1.

+50
 211.24
~~195.57~~
 15.73
~~12.23~~
 3.50

+25
 211.24
~~193.65~~
 17.59
~~11.86~~
 C-5.73

0+00
 14+52.10
 Δ 86° 18' off back
 tangent
 211.24
~~191.78~~
 19.46
~~11.69~~
 C-7.77

11.73 211.24 199.51
 See Page 43 203.44 3.93 199.51 X on Old
 M.H. #3 M.H. Lt. M.H. #3
 M.H. #3 203.44
 14+52.10 191.27
 Δ 9° 14' 20" Rt. 12.17
 Ref's. 4.51 & 14.51 Rt. 3.89
 (C-9.30 on 14.51 Ref.) C-8.28

Check Levels

T.B.M.

11.38 187.25

10.11 198.63

12.06 188.52

203.44
 14+25 190.59
 12.85
 4.57
 C-8.28
 1.07 200.58
 199.51
 X on Old
 M.H. Lt.
 M.H. #3

+75
 220.66
~~204.84~~
 15.82
~~8.76~~
 C-7.06

12.01 220.66 2.59 208.65

+50
 211.24
~~202.97~~
 8.27
~~2.59~~
 C-5.68

3+00

232.10
~~214.16~~
 17.94
~~8.98~~
 C-8.96

11.53 232.10 0.09 220.57

+25
 211.24
~~201.11~~
 10.13
~~6.37~~
 C-3.76

+50

220.66
~~210.43~~
 10.23
~~1.83~~
 C-8.40

1+00
 211.24
~~199.24~~
 12.00
~~8.45~~
 C-3.55
 187.24
 Rec.

+25

220.66
~~208.57~~
 12.09
~~3.66~~
 C-8.43

+75

211.24
~~197.38~~
 13.86
~~10.03~~
 C-3.83

2+00

220.66
~~206.70~~
 13.96
~~5.89~~
 C-8.07

End of Lateral

+25
232.10
223.49
8.61
2.57
C-6.04

+400
232.10
221.62
10.48
3.57
C-6.91

+75
232.10
219.76
12.34
4.28
C-8.06

+50
232.10
217.89
14.21
5.67
C-8.54

+25
232.10
216.03
16.07
7.06
C-9.01

0.56 210.78

1.09 221.47

4+45.36

Rec. 199.51

11.26 199.52

11.25 210.22

11.72 220.38

232.10
225.00
7.10
1.33
C-5.77

+75
211.30
194.95
16.35
10.05
C-6.30

+50
211.30
194.20
17.10
10.84
C-6.26

+25
211.30
193.45
17.85
11.14
C-6.71

15+00
211.30
192.70
18.60
11.37
C-7.23

14+75
211.30
191.95
19.35
11.55
C-7.80

11.79 211.30
Cont. from P. 42

43

17+00
211.30
198.70
12.60
4.26
C-8.34

+75
211.30
197.95
13.35
5.33
C-8.02

+50
211.30
197.20
14.10
6.47
C-7.63

+25
211.30
196.45
14.85
7.80
C-7.05

16+00
211.30
195.70
15.60
8.93
C-6.67

199.51 X
on M.H.
Lt. M.H. #3

	211.30		217.75
+25	<u>202.45</u>	+50	<u>206.20</u>
	8.85		11.55
	1.66		4.42
	C-7.19		C-7.13

	211.30		217.75
18+00	<u>201.70</u>	+25	<u>205.45</u>
	9.60		12.30
	1.92		5.39
	C-7.68		C-6.71

	211.30		217.75
+75	<u>200.95</u>	19+00	<u>204.70</u>
	10.35		13.05
	2.02		6.35
	C-8.33		C-6.70

7.14 217.75

	211.30		217.75
+50	<u>200.20</u>	+75	<u>203.95</u>
	11.10		7.35
	2.49		0.69
	C-8.61		C-6.66

	211.30		211.30
17+25	<u>199.45</u>	+50	<u>203.20</u>
	11.85		8.10
	3.32		1.33
	C-8.53		C-6.77

Rec. 199.51 X on Old M.H.
988 199.51 Oppo. M.H.#3

0.66 209.49

8.92 208.83

2.61 215.14
Chis. H W
Rim old M.H.
Opp. M.H.#4

A 3⁰3230 Rt
M.H.#4 217.75
+08.10 207.95
Refs. 4.51 @ 14.51 Rt 9.80
(14.51 - C7.04) 2.63
C-7.17

	217.75
20+00	<u>207.70</u>
	10.05
	2.86
	C-7.19

	217.75
+75	<u>206.95</u>
	10.80
	3.57
	C-7.23

240.58
 221.79
 18.79
 12.73
 6.06

+50 240.58
 224.97
 16.11
 9.73
 C-6.38

+75

240.58
 227.40
 13.18
 5.87
 C-7.31

18+00 240.58
 230.34
 10.24
 3.42
 C-6.82

+25 251.22
 233.27
 17.95
 8.77
 C-9.18

+25 240.58
 223.88
 16.70
 10.65
 C-6.05

+50

240.58
 226.82
 13.76
 6.30
 C-7.46

+75 240.58
 229.75
 10.83
 4.15
 C-6.68

19+00 251.22
 232.69
 18.53
 9.49
 C-9.04

25+00 240.58
 223.79
 17.79
 11.80
 C-5.99

+25

240.58
 226.23
 14.35
 6.85
 C-7.50

+50 240.58
 229.16
 11.42
 4.77
 C-6.65

+75 251.22
 232.10
 19.12
 10.35
 C-8.77

+75 240.58
 222.71
 17.87
 11.46
 C-6.41

26+00

240.58
 225.64
 14.94
 7.63
 C-7.31

+250 240.58
 228.58
 12.00
 5.10
 C-6.98

11.62 251.22 0.98 239.60
 +50 240.58
 231.51
 9.07
 0.98
 C-8.09

24+50 240.58
 222.12
 18.46
 12.22
 C-6.24

+75

240.58
 225.06
 15.52
 8.60
 C-6.92

27+00 240.58
 227.99
 12.59
 5.57
 C-7.02

+25 240.58
 230.93
 9.65
 3.19
 C-6.76

11.88

240.58

228.70 Chis. D
 Old M.H. Lt. 24+40

	251.22	M.H.#8	259.98		259.98		270.02
+25	236.41	31+53.90	241.01	+75	246.38	34+00	251.94
	14.81	Δ 12°50'30" Lt.	18.97		13.60		18.08
	6.64		8.49		4.69		6.05
	C-8.17		C-10.48		C-8.91		C-12.07
	251.22	9.81 259.98	1.05 250.17 P		259.98		270.02
30+00	235.57	+25	251.22 R.P. 28.95	+50	245.27	+75	250.83
	15.71		239.98 Rt. M.H.#8		14.71		19.19
	7.50		11.24		6.34		6.55
	C-8.21		2.20		C-8.37		C-12.54
	251.22		251.22		259.98		270.02
+75	234.62	31+00	239.09	+25	244.16	+50	249.72
	16.60		12.13		15.82		20.30
	7.64		3.90		7.49		8.88
	C-8.96		C-8.23		C-8.33		C-11.42
M.H.#7	251.22		251.22		259.98	11+56	270.02
+60.72	234.11	+75	238.19	32+00	243.05	+25	259.98
Δ 3°56' Rt.	17.11		13.03		16.93		248.61
	8.33		5.06		7.76		11.37
	C-8.78		C-7.97		C-9.17		1.52
	251.22		251.22		259.98		259.98
29+50	233.86	+50	237.30	+75	241.94	33+00	247.50
	17.36		13.92		18.04		12.48
	8.46		5.80		7.96		2.95
	C-8.90		C-8.12		C-10.08		C-9.53

Eggs.

35+25.00 270.02
 35+26.97 257.57
 M.H.#9 12.45
 2.73
 C-9.72

+50

285.99
 263.32
 22.67
 9.70
 C-12.97

10.00 285.99 0.30 275.99

35+00 270.02
 256.38
 13.64
 3.39
 C-10.25

+25

276.29
 262.17
 14.12
 2.71
 C-11.41

+75 270.02
 255.27
 14.75
 4.25
 C-10.80

36+00

276.29
 261.02
 15.27
 5.51
 C-9.76

+50 270.02
 254.16
 15.86
 5.05
 C-10.81

+75

276.29
 259.87
 16.42
 6.98
 C-9.44

+25 270.02
 253.05
 16.97
 4.65
 C-12.32

+50

276.29
 258.72
 17.57
 8.11
 C-9.46

9.01 276.29 2.74 267.28

R.P.N.H.#9

M.H.#10 285.99
 +74.00 269.02
 16.97
 8.41
 C-8.56

298.04
 39+00 276.01
 22.03
 11.76
 C-10.27

12.31 298.04 0.26 285.73

285.99
 +50 267.92
 18.07
 9.20
 C-8.87

285.99
 +75 274.62
 71.37
 1.69
 C-9.68

+25 285.99
 266.77
 19.22
 10.23
 C-8.99

285.99
 +50 273.24
 12.75
 3.79
 C-8.96

285.99
 37+00 265.62
 20.37
 9.15
 C-11.22

285.99
 +25 271.85
 14.14
 5.53
 C-8.61

+75 285.99
 264.47
 21.52
 8.39
 C-13.13

285.99
 38+00 270.46
 15.53
 7.33
 C-8.20

See P. 50 for M.H. #11 to M.H. #12

Thorn &
Van Dyke
NEBP
Rec. 308.66

5.21 314.07

5.57 308.50
10.96 308.86

319.55

320.47

2.01 317.81 SEBP Rec. 317.97

298.35

+50 298.86

10.01 319.82

0.10 309.81 Fairmount & Thorn

+25

21.20

21.61

5.12

2.77

12.23 309.91

0.36 297.68

C-16.08

C-18.84

R.P. 6.36 L Split 8/16.36

M.H. #11 298.04

39+83.00 280.67

(X in Ex. M.H.) 17.92

10.65 7.60

C-9.82

42+00

319.55

320.47

298.25

+25 298.76

21.30

21.71

6.73

2.05

C-14.57

C-19.66

+75 298.04

280.17

17.87

7.71

C-10.16

+75

319.55

320.47

298.14

43+00 298.65

21.41

21.82

8.86

2.09

C-12.55

C-19.73

2.50 320.47

317.97

+50 298.04

278.78

19.26

9.35

C-9.91

41+50

319.55

319.55

298.04

+75 298.55

21.51

21.00

11.19

1.76

C-10.32

C-19.24

+75 298.04

277.40

20.64

10.60

C-10.04

M.H. #12

319.55

319.55

41+35.00

297.98

+50 298.45

L 30° 12' Lt.

21.57

21.10

12.08

3.05

C-9.49

C-18.05

1.58 319.55

317.97 SEBP
Fairmount & Thorn

+75

308.19
291.20
 16.99
6.99
 C-10.00

see Opposite Page

45+00

308.97
299.47
 C-9.50

+25

304.11
299.97
 C-4.14

R. M.H.#13

9.59 308.19 0.77 298.66

320.47
~~44+53.45~~ 299.28 +50
 21.19
 9.13
C-12.09

299.43
288.37
 11.06
0.77
 C-10.29

+75

310.31
299.37
 C-10.94

46+00

303.95
299.87
 C-4.08

+25

320.47
299.16
 21.31
7.44
 C-13.87

+25

299.43
285.54
 13.89
4.21
 C-9.68

M.H.#13

44+53.45

311.37
299.28
 C-12.09

+75

304.91
299.77
 C-5.14

Self Reading Rod

44+00

320.47
299.06
 21.41
5.55
 C-15.86

40+00

299.43
282.70
 16.73
7.74
 C-8.99

M.H.#12

+35

308.19
297.98
 10.21
1.15
 C-9.06

+50

306.30
299.67
 C-6.63

+75

320.47
298.96
 21.51
3.88
 C-17.63

M.H.#11

39+83

280.78
 El. Equa. 280.62

299.43
280.78
 18.65
8.83
 C-9.82

41+00

308.19
294.03
 14.16
4.69
 C-9.47

+25

307.60
299.57
 C-8.03

2.10 299.43 10.40 297.33
 0.68 307.73 11.22 307.05
 0.30 318.27 317.97

SEBP Fairmont & Thorns

325.77
 $+66.41$
 310.26
 $\frac{15.51}{7.51}$
 $C-8.00$

$+50$ 309.83
 300.47
 $C-9.36$

R

325.77
 $+46.41$
 308.27
 $\frac{17.50}{8.76}$
 $C-8.74$

$+25$ 308.16
 300.37
 $C-7.79$

G

325.77
 $48+17.01$
 304.47
 $\frac{21.30}{10.74}$
 $C-10.56$

$47+00$ 306.38
 300.27
 $C-6.11$

12.35 325.77 313.42 T.B.M.

$M.H.# 14$
 $47+87.61$
 312.85
 300.62
 $C-12.23$

$+75$ 304.96
 300.17
 $C-4.79$

325.77
 $+75$
 311.89
 300.57
 $C-11.32$

$+50$ 304.18
 300.07
 $C-4.11$

325.77
 $+75$
 312.98
 $\frac{12.79}{3.70}$
 $C-9.09$

$51+00$ 325.77
 315.48
 $\frac{10.29}{1.83}$
 $C-8.46$

325.77
 $+50$
 312.48
 $\frac{13.29}{3.76}$
 $C-9.53$

$+75$ 325.77
 314.98
 $\frac{10.79}{2.16}$
 $C-8.63$

325.77
 $+25$
 311.98
 $\frac{13.79}{4.02}$
 $C-9.77$

$+50$ 325.77
 314.98
 $\frac{11.29}{2.44}$
 $C-8.85$

325.77
 $49+00$
 311.48
 $\frac{14.29}{5.30}$
 $C-8.99$

$+25$ 325.77
 313.98
 $\frac{11.79}{2.72}$
 $C-9.07$

325.77
 $+86.41$
 311.21
 $\frac{14.56}{6.19}$
 $C-8.37$

$50+00$ 325.77
 313.48
 $\frac{12.29}{3.29}$
 $C-9.00$

	333.60		333.60
52+00	<u>316.25</u>	+75	<u>316.55</u>
	17.35		17.05
	<u>8.72</u>		<u>7.97</u>
	C-8.63		C-9.08

	333.60		333.60
+75	<u>316.15</u>	+50	<u>316.45</u>
	17.45		17.15
	<u>9.02</u>		<u>8.05</u>
	C-8.43		C-9.10

	333.60		333.60
51+50	<u>316.05</u>	52+25	<u>316.35</u>
	17.55		17.25
	<u>9.10</u>		<u>8.40</u>
	C-8.45		C-8.85

0.64	333.60		NWBPT 10th & Chamoune
9.31	334.94	194	333.00 (332.96)

		0.14	325.63
M.H.#15	325.77		
51+23.20	<u>315.94</u>		
	9.83		
	<u>1.55</u>		
	C-8.28		

	333.60		337.49
54+00	<u>317.05</u>	+25	<u>317.54</u>
	16.55		19.95
	<u>6.04</u>		<u>7.35</u>
	C-10.51		C-12.60

	333.60		337.49
+75	<u>316.95</u>	55+00	<u>317.44</u>
	16.65		20.05
	<u>6.63</u>		<u>7.79</u>
	C-10.02		C-12.26

	333.60		337.49
+50	<u>316.85</u>	+75	<u>317.34</u>
	16.75		20.15
	<u>7.30</u>		<u>8.22</u>
	C-9.45		C-11.93

	337.49	NWBPT & C	
4.53	337.49	332.96 B.M.	
	M.H.#16	333.60	
+25	<u>316.75</u>	+53.38	<u>317.26</u>
	16.85		16.34
	<u>7.63</u>		<u>4.75</u>
	C-9.22		C-11.59

	333.60		333.60
53+00	<u>316.65</u>	+25	<u>317.15</u>
	16.95		16.45
	<u>7.87</u>		<u>5.46</u>
	C-9.08		C-10.99

Center Ex. M.H. 337.49
 + 37.85 317.99
 19.50
 5.31
 14.19

+25 337.49
 317.93
 19.56
 5.43
 C-14.13

56+00 337.49
 317.83
 19.66
 5.76
 C-13.90

+75 337.49
 317.73
 19.76
 6.21
 C-13.55

+50 337.49
 317.64
 19.85
 6.78
 C-13.07

Sewer Connections #2

1+00 223.13
 214.88
 8.25
 1.62
 C-6.63

+10 232.64
 222.35
 10.29
 4.09
 C-6.20

+75 223.13
 213.18
 9.95
 3.37
 C-6.58

2+00 232.64
 221.67
 10.97
 4.53
 C-6.44

+50 223.13
 211.48
 11.65
 6.65
 C-5.00

+75 232.64
 219.97
 12.67
 6.20
 C-6.47

+25 223.13
 209.79
 13.34
 8.38
 C-4.96

+50 232.64
 218.27
 14.37
 8.02
 C-6.35

0+00 223.13
 208.09
 M.H. #4 15.04
 Mainline 6.41
 C-8.63

9.59 232.64 0.08 223.05
 +25 223.13
 216.57
 6.56
 0.08
 C-6.48

7.99 223.13

215.14
 Chis. Old M.H.

+50 259.12
249.14
 9.98
 4.72
 C-5.26

5.90 259.12
 254.254.30 1.08 253.22

+25 254.30
248.12
 6.18
 1.08
 C-5.10

+ HI - FI
 1.53 251.53 9.08 242.45
 259.12 9.12 250.00

242.45

3+00 254.30
247.09
 7.21
 2.03
 C-5.18

+16.06
 Ex. M.H.

259.12
251.83
 7.29
 1.82
 C-5.47

+75 254.30
246.07
 8.23
 2.94
 C-5.29

+4+00.17
 M.H.#7A

259.12
251.19
 7.93
 4.23
 C-3.70

+50 254.30
245.04
 9.26
 3.86
 C-5.40

+75

259.12
250.17
 8.95
 4.43
 C-4.52

1+00 288.28
279.30
 8.98
 4.56
 C-4.42

+75 288.28
276.88
 11.40
 6.80
 C-4.60

+50 288.28
274.45
 13.83
 9.57
 C-4.26

+25 288.28
272.03
 16.25
 10.34
 C-5.91

+33 288.28
282.50
 Ex. M.H. 5.78
 0.61
 C-5.17

0+00 288.28
269.60
 18.68
 9.13
 C-9.55

+25 288.28
281.73
 6.55
 1.96
 C-4.59

7.82 288.28

280.46
 Hub 4.5 Rt. Sta. 38+25

Garber Oct. 25, 51
 Shepard T Cold-Rain
 Bruener

Bryson Check Levels M.H.s. No 13, 14,
 15 & 16 (Thorn E. of Fairmount)

			SWBP Thorn & Chamounie	
		3.55	332.98	Rec. 332.96
#				
M.H. # 16		7.03		
	9.30	336.53		329.50
#		1.77		327.23
M.H. # 15		4.69		324.31
	12.03	329.00		
#		3.32		316.97
M.H. # 14		7.28		313.01
#		8.73		311.56
M.H. # 13				
	2.32	320.29		317.97 SEBP Fairmount & Thorn

Garber
Shepard T
Bruener
Bryson

Nov. 2, 51
Warm-clear
W.O. 25020
Tye Pt. BK. 14 - P. 48

Green Profile 229

0+00	0+50	1+00	1+40
13.21	13.21	13.21	13.21
9.00	9.25	9.50	9.70
4.21	3.96	3.71	3.51
4.97	5.37	6.72	6.97
F-0.76	F-1.41	F-3.01	F-3.46

2+00	2+50	3+00	3+50
13.21	13.21	13.21	13.21
10.00	10.25	10.50	10.75
3.21	2.96	2.71	2.46
6.70	7.00	6.82	6.50
F-3.49	F-4.04	F-4.11	F-4.04

4+00
13.21
11.00
2.21
5.92
F-3.71

0.15 13.21

13.06 SW l d e TK & Wasen
Disc.
Dalbergia

Grade stake for
Drainage

INDEXED

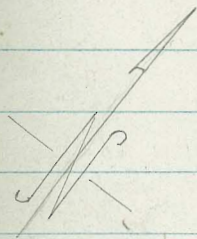
NOV 5 1951

57

Felldg/TK

Woden

4+00



Curb line

Note - stakes set on
curb line

16' 34' 34' 16'

0+00 50' 50'

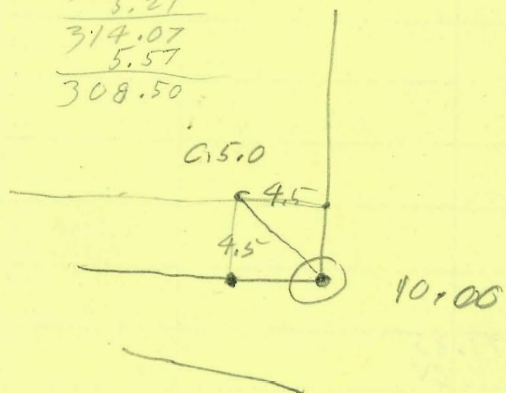
Fel. Con. Men

60'

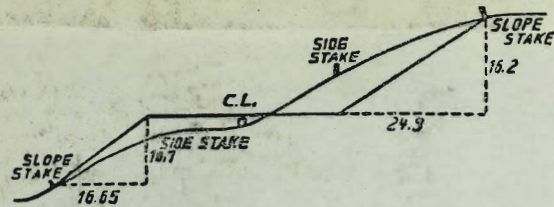
37'

Yama

267.28	276.29	9.67
<u>9.01</u>	<u>256.38</u>	
276.29	19.91	317.81
<u>0.30</u>	<u>8.67</u>	<u>16</u>
275.99	10.24	317.97
<u>10.00</u>	<u>10.01</u>	
285.99	<u>25</u>	
<u>0.26</u>		
285.73		
<u>12.31</u>		
298.04	319.82	
<u>0.36</u>	<u>2.01</u>	
297.68	317.81	HW SEBP
<u>12.23</u>		Fair & Thorn
309.91		
<u>0.10</u>		
309.81		NEBP Th & Van
<u>10.01</u>		
319.82		308.66
<u>10.96</u>		
308.86		
<u>5.21</u>		
314.07		
<u>5.57</u>		
308.50		



17.87
 1.39
 17.87
 19.26
 1.38
 19.25
 20.64



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

311.37
99.28
12.09

0.51
1.84
3.35

645
15
835