

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
of stake for any width roadway, slope 1% to 1.
If ground is nearly level the cut or fill at side

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given T may be found
by dividing tangent (or external) by
given tangent (or external).

MICROFILMED

APR 14 1965

Roberts
Garbar
Moore
Clark
4-25-50
W.D. 3/606

Grade Stakes for Water & Sewer
Laterals in Tennyson St.
(Wells St. to Catalina Blvd.)

See FB 1835 pg 44

See 7774L sheet

1785 Water Lat.
on Rt

119.72
115.10
462
Curb in
463

1760 Sewer Lat #9
on Rt

119.72
108.57
11.15
512
C 6.03

1735 Water Lat.
on Rt.

112.50
curb in

1710 Sewer lat. #10
on Rt

119.72
105.92
13.80
894
C 4.86

0+00 West Line Wells St.

BM 12.80

119.72

106.92 Mon. SW Cor
Tennyson & Wells

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2783 water Lat.
on Rt

130.10
120.20
Curb in

2780 water Lat.
on Lt

130.10
120.61
9.49
783
C 1.66

2758 Sewer Lat. #7
on Rt

130.10
114.03
16.07
11.33
C 4.74

2755 Sew. Lat #5
on Lt.

130.10
113.87
16.23
518
C 11.05

2730 Water Lat.
on Rt

117.44
curb in

T.P. 11.09 130.10 071 49.01
↑

2705 Sewer Lat #8
on Rt

119.72
111.22
8.50
389
C 4.63

119.72

Cont'd From Page 1

Grade Stakes for Water 2
 Laterals Atascadero Drive
 (Wells to Catalina)
 See 7772 L

SEBP Tennyson
 #Catalina

INDEXED

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check 396 89.88 = 89.88
 T.P. 2.11 93.74 12.27 91.63

8+80 water Lat. 103.90
 on Rt 93.50
 10.40
 9.59
 C 0.81

8+45 water Lat. 103.90
 on Rt 95.80
 8.10
 6.96
 C 1.14

T.P. 0.31 103.90 13.00 103.59
 T.P. 0.56 116.59 12.93 116.03

5+40 water Lat. 128.96
 on Rt 125.00
 3.96
 2.69
 C 1.27

12560 water Lat. 128.96
 on Lt 125.50
 3.46
 3.87
 F 0.41

3+30 water Lat. 122.64
 on Rt curbin

T.P. - 3.50 128.96 464 125.46
 130.10
 116.52
 13.58
 8.36
 C 5.22

3+05 Sewer Lat. #6
 on Rt 130.10
 116.52
 13.58
 8.36
 C 5.22

Water Lat. 11
 6+15 on Rt

5+75 Water Lat. 128.01
 on Lt 122.20
 5.81
 6.49
 F 0.68

5+15 Water Lat. 128.01
 on Lt 127.10
 0.91
 1.71
 F 0.80

BM 11.17 128.01
 1465 Water Lat. X
 on Rt.

0+15 Water Lat.
 on Rt

0+00 W.L. Wells

T.P. 11.55 160.70
 T.P. 12.30 149.42

BM 12.59 137.33

0.21 149.15
 0.21 137.12

NW Cor Mon
 124.74 Alicia # Wells

130.10

Roberts
#-25-50
no. 31606

Grade Stakes for Sewer & Water
Laterals in Alicia Drive
Wells to Catalina

Sec. EB 1835 pg. 36 see 7773L

Sewer Lat. #3
2+10 on Lt 132.52
11.48
1.10
C 10.38

1+85 Water Lat. on Rt. 135.90
(IN)

T.P. 8.14 144.00 154 135.86
1+60 Sewer Lat. #1 on Rt 130.10
IN ALLEY

7+15 Water Lat. on Rt

112.86
106.60
6.26
6.42
F 0.16

0+38 Water Lat. on Lt. 137.40
128.20
9.20
6.78
C 2.77

6+70 Water Lat. on Lt. 112.86
110.20
2.66
2.73
E 0.07

0+35 Water Lat. on Rt. 137.40
127.20
10.20
9.79
C 0.71

BM 613 112.86

Alicia to Catalina
106.73 SEBP

3+60 Water Lat. on Lt. 137.05
(IN)

0+13 Sewer Lat. #2 on Lt. 137.40
123.06
14.34
4.11
C 10.23

2+35 Water Lat. on Lt. 144.00
138.95
5.15
4.42
C 0.73

BM 12.66 137.40

NW Cor Mon
12474 Alicia to Wells

144.00

INDEVENT
APP 11 1951

Roberts
Garber
Clark
5-2-50
W.O. 31470

Grade Stakes Electric Ave
Sly Line PL 1258 to Palomar

E.E. 1734, 1790 & 2029
774, 15, 16, & 174

INVENT
MAR 17 1950

1700

83.67
6.73
728
F 0.55

2725

848.4
556
559
F003

0+75

83.42
6.78
758
F 0.60

1775

84.62
5.78
538
C0.40

0+50

83.17
7.23
774
F 0.51

1760.10 BRK

84.26
6.14
643
F 0.29

0+25

82.92
7.48
758
F 0.10

1750

84.17
6.23
663
F 0.40

0+00 Ec. cb Ret
on Rt at Palomar
Exist Curb

90.40
82.67
7.73
7.74
✓

1725

83.92
6.48
702
F 0.54

TP 2.18 90.40 4.95 88.22

BN 2.28 93.17 9189 B.P.E. Curb
Dowling
Electric

90.46

3+50

85.86
4.54
418
C 0.36

4+75

86.82
3.58
1.93
C 1.65

3+25

85.66
4.74
448
C 0.26

4+50

86.63
3.77
2.35
C 1.42

3+00

85.46
4.94
487
C 0.07

4+25

86.44
3.96
2.90
C 1.00

2+75

85.26
5.14
510
C 0.04

4+15.40 BRK

86.36
4.04
2.97
C 1.07

2+50

85.06
5.34
540
C 0.06

4+00

86.25
4.15
3.04
C 1.11

2+41.82 BRK

85.00
5.40
554
C 0.14

3+75

86.06
4.34
3.55
C 0.79

90.40

90.40

6700
 87.86
 5.38
 491
 C0.67

7750
 89.12
 4.12
 472
 F0.60

5775
 87.65
 5.59
 489
 C0.70

7725
 88.91
 4.33
 476
 F0.73

5750
 87.44
 5.80
 476
 C1.04

7700
 88.70
 4.54
 480
 F0.26

5725
 87.23
 6.01
 482
 C1.19

6775
 88.49
 4.75
 483
 F0.08

5700
 87.02
 6.22
 495
 C1.27

6750
 88.28
 4.96
 483
 C0.13

TP 5.06 93.24 222 88.18
 4796.87 BRK
 87.00
 3.40
 222
 C1.18

6725
 88.07
 5.17
 470
 C0.47

90.40

93.24

8+75

90.21
3.03
4.60
F 1.57

8+50

90.00
3.24
4.56
F 1.32

8+25

89.79
3.45
4.59
F 1.14

8+00

89.58
3.66
4.34
F 0.68

7+80.47 BRK

89.38
3.86
4.36
F 0.50

7+75

89.33
3.91
4.45
F 0.54

check

1.35 91.89 = 91.89

9+15.02 Exist. Curb
R.C. & P.T.
Mesa way

90.43
2.81
2.77
0.04

9+00

90.31
2.93
4.21
F 1.28

8+84.32 BRK

3070

90.27
2.97
4.37
F 1.40

93.24

93.24

1723.16 Exist
Curb
on Rt.

92.25
4.13
4.09
✓
.04

1700

92.40
3.98
2.13
C 1.15

0775

92.55
3.83
2.53
C 1.30

0750

92.70
3.68
2.62
C 1.06

0725

92.85
3.53
2.69
C 0.84

0700 sly. Line P.L.
1258

93.00
3.38
4.65
F 1.27

BM

449

96.38
X

91.89 E. Cb.
Dovelling
Electric

Roberts
Garber
Moore
Clark
5-9-50
NO 31606

Grade Stakes Tennyson St.
(Wells to Catalina) Lt

2+75

Lt.
120.33⁹
6.96
6.50
60.76

INDEXED

ADD II 11 11 11

2+50

119.13
8.16
762.
60.54

1+00 End Exist Cb. Lt.

111.93
5.21
5.21
✓

2+25

117.93
9.36
857.
60.99

End Cb. P.L. Wells = 0+00

106.89
10.25
1006
60.19

2+00

116.73
10.56
995
60.61

cb BC

0+10

107.00
10.14
983
X ?

TP 11.15

127.29

100

116.14

1+75

115.53
1.61
100
60.61

SWly Curb Ret at Wells

1+50

114.33
2.81
257
60.24

1+25

113.13
4.01
414
60.13

BM

10.22 117.14

106.92

Mon SW cor.
1000 ft. WELLS

117.14

Lt

Lt

Rt 10

4425

$$\begin{array}{r} 126.81 \\ 3.70 \\ \hline 416 \\ \text{FO.46} \end{array}$$
5415 Lt
Rt
$$\begin{array}{r} 125.95 \\ 456 \\ \hline 414 \\ \text{FO.18} \end{array}$$

$$\begin{array}{r} 125.60 \\ 491 \\ \hline 488 \\ \text{C 0.03} \end{array}$$

4405

$$\begin{array}{r} 126.68 \\ 3.83 \\ \hline 416 \\ \text{FO.33} \end{array}$$

4495 Rt

$$\begin{array}{r} 126.31 \\ 4.20 \\ \hline 452 \end{array}$$

$$\begin{array}{r} 125.90 \\ 461 \\ \hline 452 \\ \text{C 0.09} \end{array}$$

E 4400

End Exist
Curb Lt4465 BC
cb Rt
$$\begin{array}{r} 125.97 \\ 454 \\ \hline 449 \\ \text{C 0.05} \end{array}$$

TP

400

130.51

0.78

126.51

C 3450

Exist Curb Lt

$$\begin{array}{r} 123.93 \\ 3.36 \\ \hline 329 \\ \hline \end{array}$$

center cb Rt

N.W.

cb

Rt.

San

Clemente

$$\begin{array}{r} 125.83 \\ 468 \\ \hline 462 \\ \text{C 0.06} \end{array}$$

S 3425

$$\begin{array}{r} 122.73 \\ 456 \\ \hline 453 \\ \text{C 0.03} \end{array}$$
4445 End cb Rt
Rt, Tenuquin
Clemente
$$\begin{array}{r} 125.56 \\ 495 \\ \hline 431 \\ \text{C 0.64} \end{array}$$

3400

$$\begin{array}{r} 121.53 \\ 5.76 \\ \hline 547 \\ \text{C 0.29} \end{array}$$
4450 Exist cb
on Lt

4455 126.52

127.29

	Lt	Rt
8+05	End Exist cb on Lt	101.43 5.05 <u>5.08</u>
T.P.	0.76	116.48
TP	0.19	118.60
6+05	Exist cb on Rt	121.25 926 913 <u>13</u>
5795		121.90 861 <u>837</u> C0.24
5775		123.40 7.11 <u>684</u> C0.27
5+55		124.40 6.11 <u>575</u> C0.36
5735	Lt Rt	125.30 521 547 <u>530</u> C0.26
		130.51

	Lt	Rt
9+32	cb BC on Rt	89.87 = 89.88
9+20	Rt	87.10
	End cb	89.59 7.42 <u>744</u>
29.6	Exist cb BC	89.50
9+07	on Lt	7.71
		6.61
		673
		<u>F0.12</u>
8+75	Rt Lt	93.87 3.14 <u>336</u> F0.22
8765	Rt only	94.67 2.34 <u>262</u> F0.28
T.P.	1.33	97.01
8755	End Exist cb on Rt	96.03 10.45 <u>1080</u> F0.35
8+30		98.93 9.75 <u>812</u> F0.37
		10.80
		95.68
		95.81
		10.67
		<u>10.82</u>
		15
		X
		106.48

Reberts
59-50

Grade Stakes Atascadero
(Walls to Catalina)

TBM

INDEXED

APR 11 1951

12

1.38 159.29 chisel sy. 1450 Lt
Conn. Ret. Wall

0+80

7772L H
157.07
3.60
372
FO.12

Rt
156.47

2+00

Rt
152.30
8.37
844

0+60

156.91
3.76
416
FO.40

156.31
4.36

1+80 Rt

153.58
7.09
720
FO.11

0+40

156.54

155.94
4.73
518
FO.45

1+60 Rt

154.65
6.02
624
FO.22

0+20

155.93

155.20
5.47
641
FO.94

1+50 End ch Rt

0+10 C.B.E.C.

ENST
155.57
5.10
508

154.70
5.97
692
FO.95

Curb Ends = 0+00 P.L. Walls

153.37
5.30
516
FO.14

154.08
6.59
735
FO.76

1+00

156.96
3.71
380
X

156.36

T.P.

12.68 149.67

0.00 149.99

T.P.

12.80 149.99

0.16 137.19

BM

12.61 137.35

124.74 NW Cor. Mon
Alicia + Wall

160.67

6700 Ent cb
on Rt
$$\begin{array}{r} 120.16 \\ 7.65 \\ \hline 816 \\ F0.51 \end{array}$$

$$\begin{array}{r} 119.45 \\ 8.36 \\ \hline 839 \\ \checkmark \end{array}$$

5780 BRK

$$\begin{array}{r} 121.83 \\ 598 \\ \hline 643 \\ F0.45 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ \text{cb.} \end{array} \begin{array}{r} 117.83 \\ 9.98 \\ \hline 999 \end{array}$$

$$\begin{array}{r} 116.82 \\ 10.99 \\ \hline 1101 \end{array}$$

5760

$$\begin{array}{r} 129.49 \\ 434 \\ \hline 475 \\ F0.41 \end{array}$$

6+28.37

$$\begin{array}{r} 117.53 \\ 10.28 \\ \hline 1030 \\ F0.02 \end{array}$$

5740

$$\begin{array}{r} 125.11 \\ 2.70 \\ \hline 322 \\ F0.52 \end{array}$$

6+20 BC Lt

$$\begin{array}{r} 118.52 \\ 9.29 \\ \hline 975 \\ F0.46 \end{array}$$

$$\begin{array}{r} 117.97 \\ 9.84 \\ \hline 986 \\ F0.02 \end{array}$$

5720

$$\begin{array}{r} 126.75 \\ 1.06 \\ \hline 148 \\ F0.42 \end{array}$$

6+10

$$\begin{array}{r} 119.34 \\ 8.47 \\ \hline 882 \\ F0.35 \end{array}$$

$$\begin{array}{r} 118.64 \\ 9.17 \\ \hline 926 \\ F0.09 \end{array}$$
5700 Ent cb
on Lt
$$\begin{array}{r} 128.37 \\ 10.58 \\ \hline 1055 \end{array}$$

BM

10.97

127.81 π SEPP
116.87 Atasadores # Catalina127.81 π

MINVED
 APP 11 1951

Grade Stake Alicia Dr.

Wells to Catalina

1700 Lt

135.63
 131.71
 3.92
384
 C 0.08

3780 Lt

135.65
 C 43
 7.16
 F 0.73
 137.05
 5.03
575
 F 0.72

14

433

2740 Lt

142.08
 137.04
 3.04
292
 X

0775 Lt

135.63
 130.31
 5.32
 5.48
F 0.16

2725 Lt

142.08
 138.45
 3.63
 3.88
F 0.25

0750 Lt

135.63
 128.71
 6.72
 6.57
C 0.15

2700 Lt PVC

142.08
 137.37
 4.71
 3.36
F 0.65

142.08
 136.76
 5.32
525
 X

0720 BRK Lt + Rt

135.63
 127.23
 8.40
 7.33
C 1.07

1775 Lt + Rt

135.63
 126.30
 9.33
 9.28
C 0.05

142.08
 135.91
 6.17
 6.23
F 0.06

142.08
 135.48
 6.60
 6.60
 Grade

0710 EC Cb Pot Lt + Rt

135.63
 126.80
 8.83
 7.60
C 1.23

1750 Lt + Rt

135.63
 125.70
 9.93
 10.06
F 0.13

142.08
 134.51
 7.57
 6.63
C 0.94

142.08
 134.20
 7.88
 7.86
 C 0.02

0700 PL Wells End curb Lt + Rt

135.63
 126.60
 9.03
 7.61
C 1.42

1725 Lt

135.63
 125.00
 10.63
 10.69
F 0.06

142.08
 133.11
 8.97
 8.34
C 0.63

BM 10.89

135.63 X

conc Men SW Cor.

12474 Alicia + Wells T.P. 8.70 142.08 X

225 133.38

Robert
Garber
Mount
check
9-18-50

Grade Stakes Water Line
Rose St. (Miller to 63rd)

1430-D
1433-D

INDEXED
Apr 11 1951

15

2+10 BRK

461.75
8.93
5.03
C 3.90

4+80

460.94
9.74
6.33
C 3.41

1+68

461.33
9.35
4.93
C 4.42

4+35

461.07
9.61
6.06
C 3.55

1+26

460.91
9.77
4.99
C 4.78

3+90

461.21
9.47
6.14
C 3.33

0+84

460.49
10.19
5.13
C 5.06

3+45

461.34
9.34
6.05
C 3.29

0+42

460.07
10.61
6.17
C 4.44

3+00

461.48
9.20
5.40
C 3.80

0+00 (10'E. of Miller)

459.65
11.03
7.29
C 3.74

2+53

461.61
9.07
5.01
C 4.06

BM

8.27

470.68 X

472.41 5079.61 GB266

470.68 X

INDEVEN
APR 11 1951

Grade Stakes for Water Line in 16
Millar St.
5-23-50 (Rose to Stewart to Hobart)

2+03.5
457.58
9.64
412
C 5.52

1+62.8
457.99
9.23
378
C 5.45

1+22.1
458.41
8.81
345
C 5.36

0+81.4
458.82
8.40
460
C 3.80

6±05 Exist
Water line

461.06
9.62

0+48.7
459.23
7.99
400
C 3.99

5+70 BRK

460.67
10.01
6.25
C 3.26

5+25

460.80
9.99
6.26
C 3.62

0+00 { 5% E Rise = 0+00 pg 15
10' E of Millar

459.65
7.57
3.84
C 3.73 = 374

BM 4.81 462.2 X

462.41

470.68 X

4+44.3

454.73
12.49
676
C 5.73

4+08.25 BRK

455.56
11.66
670
C 4.96

3+67.2

455.96
11.26
560
C 5.66

T.P. 7.00

~~465.48~~
↑

8.74

458.48 25RT MH

3+26.2

456.36
10.86
475
C 6.11

5+31.61

7.07 on Split.
10' E & Miller
5' No. & Hubert

453.09

14.13

10 74
C 3.39

2+85.2

456.76
10.46
491
C 5.55

5+16.61 BRK

453.07

14.15

1020
C 3.95

2+44.25

7.07' off on Split
10' E & Miller
10' S. & Stewart

457.17
10.05
450
C 5.55

4+80.4

453.90

13.32

890
C 4.42

467.22 X

467.22 X

Roberts

5-24-50

Grade Stakes Water Line Hobart

Millar to Pembroke

INDEXED
APR 11 1951

7+59

455.38
10.10
454
C 5.56

7+17^z

454.31
11.17
474
C 6.43

6+76⁶¹ BRK

453.24
12.24
11.49
C 0.75

6+40^z

453.21
12.27
966
C 3.21

6+04

453.17
12.31
713
C 5.18

8+4/61 END
Connect Exist line
Hobart to Pembroke

457.53
7.95
512
C 2.83

5+67^z

453.13
12.35
708
C 5.27

8+00^z

456.45
9.03
439
C 4.64

465.48 π

See pg 17

465.48

π

Roberts
at
5-24-50

Change in Sewer Line Catoctin
From Art St. East to Dead End.
See F.B. 2008 pg. 647

See GB266 pg 71

14+49Z

449.39
14.12
380
C 10.32

16+29Z

450.11
13.40
460
C 9.80

INDEXED
APR 11 1951

19

T.P.

3.67 463.51X

524 457.84 IN #OUT to M

14+19⁶⁹ MH #5A
5' x 20" RP on Splip
IN Catoctin

449.27
15.81
T.P. → 524
C 10.57
243

15+99Z

449.99
13.52
452
C 9.00

13+84Z

449.13
15.95
972
C 11.23
171

15+69Z

449.87
13.64
446
C 9.18

13+49Z

448.99
16.09
422
C 11.87
113
116

15+39Z

449.75
13.76 ✓
423
C 9.53

13+14Z

448.85
16.23
383
C 12.40

15+09Z

449.63
13.88
415
C 9.73

12+7969 MH #5
2 Art # & Catoctin

IN # out to MH5A
448.71
C 12.90

14+79Z

449.51
14.00
399
C 10.01

TBM

1.69 465.08
X

See FB 2008 pg 11
463.39

463.51

18+14²

450.85
12.66
546
C7.20

17+83²

450.72
12.79
545
C7.34

17+52²

450.60
12.91
536
C7.55

17+21²

450.47
13.04
526
C7.78

check

3.50 463.37 - 463.39

T.P.

7.48

466.87

4.12

459.39

16+90²

450.35
13.16
499
C8.17

18+76⁹⁹ DE
Catocin Dr.
opposite Lot 7 Alvarado Hts.

451.10
12.41
556
C6.85

16+59⁶⁹ MH6

5.03 RP 50 & 25 RP No. on split
In Catocin Dr. opposite Lot 9 Alvarado Hts

IN & TO DE
450.23
13.28
468
C8.60

18+45²

450.97
12.54
540
C7.14

463.51A

463.51A

Robert
5-24-50

Grade Stakes For Water Line in Stewart
Miller to 63rd St

INDEXED
APR 11 1951

21

2+05

467.71
457.99
9.72
474
C 4.99

4+52.8

467.71
458.97
8.74
518
C 3.56

1+64

467.71
457.82
9.89
441
C 5.42

4+10 Fire Hydrant

467.71
458.80
8.91
481
C 4.10

1+23

467.71
457.66
10.05
467
C 5.38

3+69

467.71
458.64
9.07
477
C 4.30

0+82

467.71
457.49
10.22
496
C 5.26

3+28

467.71
458.48
9.23
466
C 4.57

0+41

467.71
457.33
10.38
478
C 5.60

2+87

467.71
458.32
9.39
456
C 4.83

0+00

= 2+44.25 ^{See} Page 17
20' E of Miller
10' S of Stewart

457.17
C 5.55

2+46

467.71
458.15
9.56
433
C 5.21

BM

530

467.71
↑

462.41

Miller &
Stewart
T. P. R.

467.71

check

444 463.40 = 463.39

7710 END
 Make Connection
 Exist. Water Line
 63" Stem

460.00

6+67^L

467.84
 459.82
 8.02
 491
 C 3.11

6+24^E

467.84
 459.65
 8.19
 477
 C 3.42

5+81^E

467.84
 459.48
 8.36
 470
 C 3.66

5+58^E

467.84
 459.31
 8.53
 508
 C 3.45

7P 5.15 467.84 ~~71~~ 502 462.69

4+95^L

467.71
 459.14
 8.57
 502
 C 3.55

467.71

Garber Rough Grade - Bradford bet. 60th &
 McCoy College Way
 Moore
 Clark

INDICATED
 AD-IT

+80

cb ✓ Lt. ✓
 3.98 436.90
 4.14 4.97
 F0.16 C-3.44

Rt ✓ ✓
 435.90 4.98
 5.97 5.22
 7.84
 F 1.89 F0.24

+80

cb ✓ Lt. ✓
 4.45 436.43
 4.77 5.44
 7.44 1.84
 F0.32 C-3.60

435.43 5.45
 6.44 5.10
 7.44 F0.25
 F-1.0

+60

4.04 436.84
 4.13 5.03
 F0.09 C-2.59

435.74
 6.13 5.14
 8.06 5.36
 F 1.93 F0.22

+60

4.14 436.74
 4.44 5.13
 F0.30 C-2.36

435.74 5.14
 6.13 5.63
 7.81
 F-1.68 F0.49

+40

3.91 436.97
 4.10 4.90
 F0.19 C-2.72

435.55
 6.32 5.33
 8.57 5.74
 F 2.25 F0.41

+40

3.95 436.93
 4.21 4.94
 F0.26 C-2.63

435.93 4.95
 5.94 5.26
 7.14
 F-1.20 F0.31

+20

3.69 437.20
 4.02 4.67
 F0.34 C-2.67

435.12 5.76
 6.75 6.07
 8.64 F0.31
 F 1.89 434.68

+20

3.84 437.04 chis. X
 4.06 4.83
 F0.22 C-2.58

436.04 4.84
 5.83 5.05
 7.14
 F-1.31 F0.21

0+08 EC

434.33
 3.55
 3.98
 F0.43

0+00 #1
 RL. 60th
 343
 386
 F0.41

437.43
 4.44
 1.1.67
 C-2.77

434.26
 7.61 6.62
 8.74 6.67
 F 1.13 F0.05

+00

3.87 437.01
 4.15 4.86
 F0.28 C-3.35

436.01 4.87
 5.86 5.10
 7.94
 F-2.08 F0.27

441.87 (See P-25)

cb ✓ Lt. ✓

Rt. ✓ cb ✓

✓ Lt.

Rt. ✓

+ 80

7.88
830
 F 0.42

433.00
 5.17
3.70
 C -1.47

432.00 8.88
 6.17 9.16
6.75 F 0.28
 F -0.58

+ 60

6.94
729
 F 0.35

433.94
 4.23
2.59
 C -1.64

432.94 7.94
 5.23 8.16
5.79 F 0.22
 F -0.56

EC College

431.33
 9.55
9.12
 C 0.43

429.18
 11.70
11.71
 F 0.01

+ 40

6.13
628
 F 0.15

434.75
 3.42
1.62
 C -1.80

433.75 7.13
 4.42 7.47
4.76 F 0.34
 F -0.34

2

431.12
 9.76
9.32
 C 0.44

429.37
 11.51
11.37
 C 0.14

3.23 438.17 6.93 434.94

+ 20

5.44
541
 C 0.03

435.44
 6.43
4.35
 C -2.08

434.44 6.44
 7.43 6.71
7.75 F 0.27
 F -0.32

Rad. Pt. 4.97

8.15 430.02 T.B.M.

Rad Pt. 7.91

2+00

4.88
503
 F 0.15

436.00
 5.87
2.24
 C -3.63

435.00 5.98
 6.87 6.05
7.44 F 0.14
 F -0.57

3+11.4 Rep L #1

431.43
 9.15
9.89
 F 0.44
 431.83
 9.05
9.56
 F 0.51

429.90
 10.78
10.68
 C 0.30

3+03.4 BC

430.42
 10.46
10.40
 C 0.06

441.87 Rough

440.88 Tcb

440.88 Tcb

Garber
McCoy
Moore
Clark
5/29/50

Grade Stakes for water meters
in Bradford btw. 60th & College Way

25

INDEXED
APR 11 1951

2+75 Rt. 432.81
5.36
5.72
F-0.36

2+70 Rt. 3.23 438.17 6.93 434.94

2+18 Rt. 434.58
7.29

1+52 Lt. 434.94 6.93 437.96.95

2+03 Lt. 436.02
5.85
4.40
C-0.34

2+13 Rt. 4.40
C-1.45

1+84 Rt. 435.43
6.44
6.89
F-0.45

1+52 Lt. 436.89
4.98
3.87
C-1.11

5.83 441.87 1.83 436.04 / 430.02
Chapel H. N. Cor.
7.85 of E. Inlet. Estell

8.91 437.87 12.89 428.96

0.65 441.85 12.90 441.20
5.26 448.84 F. Plg. College
Ave & College
Way

0.55 454.10 13.06 453.55

1.34 466.61
465.27 NWBP
E/la Jan
& College Ave

Garber Grade stakes for water meters, Estelle
McGoy - 60th to 61st
Moore
Clark
5/31/50

Lt.

4+02

2+25

+83

1+43

0+88

INDEXED

APP 11 1951

Lt

5+03

4+54.5

430.02 Chisel □
N. Cor. E Inlet
College Way 100
N. of Estelle

Garber
McCoy
Moore
Clark

5/31/50

1+24.26 →

1+20

1+03.55 →

0+82.84 →

+80

0+62.13 →

0+41.42 →

+40

0+20.71 →

B.C.
+08 Rad. Pt.

420.61

12.10

10.22

C-1.88

#/0+00 Rl. 60th

420.50

12.21

10.64

C-1.57

Rough 2.69

432.71

K

Comb 1.18

431.20X

Estelle

Lt. ✓

Rough

422.12

10.59

9.39

C-1.20

421.58

11.13

9.66

C-1.47

421.04

11.67

10.12

C-1.55

60th to College

cb ✓

422.23

8.77

9.19

F0.22

421.96

9.24

9.49

F0.23

421.69

9.51

9.73

F0.22

421.42

9.78

10.37

F0.59

421.15

10.05

10.34

F0.29

420.88

10.32

10.60

F0.28

420.61

10.59

10.81

F0.22

420.60

10.60

9.66

C0.94

430.02

NE. Cor. East
Inlet, College

430.08 Way 100 N. Estelle

Chisel

□

NE. Cor. East
Inlet, College

Way 100 N. Estelle

INDEXED

APR 11 1951

Rough ✓

424.30

8.41

6.72

C-1.69

423.70

9.01

7.02

C-1.99

423.30

9.41

7.87

C-1.54

1786.39 →

2+00

423.20

9.51

1165.68 →

+60

422.66

10.05

8.66

C-1.39

1144.97 →

422.50

9.70

8.82

F0.12

431.20X cb

cb ✓

4+26.71 →
4+10.57

Rough
433.43
9.15
8.64
C-0.57

cb ✓
434.20
7.81
7.80
C 0.01

4+03.19 →

432.83
9.18
9.22
F 0.14

+79.67 → 431.46
B.C. 11.12
10.00
C-1.12

431.46
19.55
10.89
F 0.38

T.P. cb 11.11 442.01 X
10.26 442.58 X

0.30 430.90
0.39 432.32

3+03.67
B.C. 427.11
5.60
4.95
C-0.65

427.11
4.09
4.37
F 0.28

+87^L
E.V.C. 426.10
6.61
5.48
C-1.13

426.10
5.10
5.39
F 0.29

+67^L
425.15
7.56
6.09
C-1.47

425.15
6.05
6.26
F 0.21

432.71 X
431.20 Xcb

432.71 X

442.01 Xcb

5° Out on 438.71 28

438.60
7.32
5.72
C-7.60
R 0.33

61st St.
439.10
6.82
2.24
C-4.58

439.04cb
2.97
0.57
C 2.40

432.54cb → 3.47
438.05cb R=200 2.89
C 0.58

396
400

3.96 430.02 T.B.M.

0.88 Center L. Estelle 433.98 12.82 433.10

#1 5.17 445.92 X
1.83 440.75
438.90

5+27.28 438.90
Wly Line 3.68
College Ave 1.94
C-1.74
5+22.28 BC

438.80
3.21
2.40
C 0.81

+97.28 BRK 438.30
Wly Line 61st 4.28
3.88
C-0.40

438.30
3.71
3.69
C 0.02

4+73.75 →

436.94
5.07
5.11
F 0.04

4+49.47 435.87
6.71
6.65
C-0.06

4+50.23 →

435.57
6.44
6.38
C 0.06

INDEXE
APR 11 1957

College Way - Estelle to College Ave

	Lt.	Rt.
+80	428.96	429.23
	862	8.35
	828	7.19
	<u>C 0.34</u>	<u>C 1.16</u>

+60	429.00	429.39
	858	8.19
	850	7.09
	<u>C 0.08</u>	<u>C 1.10</u>

+40	429.28	429.55
	830	8.03
	942	6.10
	<u>F 1.12</u>	<u>C 1.93</u>

+20	429.10	429.71
	848	7.87
	948	5.55
	<u>F 0.00</u>	<u>C 2.32</u>

0 + 10 E.C.	428.79	429.95
	8.79	7.63
	975	5.12
	<u>F 0.96</u>	<u>C 2.51</u>

	Lt	Rt.
+89.90	College 429.18	Bradford 420.42
B.C.	8.40	7.16
	731	731
	<u>C 1.09</u>	<u>F 0.15</u>
		<u>C 0.68</u>

+60	429.01	429.39
	857	8.19
	871	7.79
	<u>F 0.14</u>	<u>C 0.90</u>

+30	428.85	429.23
	8.73	8.35
	961	7.91
	<u>F 0.28</u>	<u>C 0.44</u>

+20	428.84	429.18
	8.74	8.40
	866	8.01
	<u>C 0.08</u>	<u>C 0.39</u>

1400	428.79	429.13
	8.79	8.45
	847	7.86
	<u>C 0.32</u>	<u>C 0.59</u>

TBN

756

437.58 T

5. Pg 27
N. End. Colbrt
E. Side Colbrt

430.02

437.58 T

T.P. 12.34 447.62 X 230 435.28
 3+39.90 435.93 435.06
 1.65 2.52
 0.51 411
 C 1.14 F 1.59

R.C. Cb.
 5764.52 Ret. — 447.51
 Ret.

+89.90 433.05 432.18
 4.53 5.40
 340 506
 C 1.13 C 0.34

PIC college
 5761.40 Ave 447.91 447.41
 948 998
 825 1230
 C 1.23 F 2.32

TP 12.30 457.39 X 253 445.09
 R.C. Sem. Lat. Nat.
 5709.80 Carol 445.05 439.33 444.55
 2.57 829 3.07
 050 334 502
 C 2.07 C 4.95 F 1.95

+69.90 431.16
 6.42
 575
 C 0.67
 20 R.P. college Bradford
 431.33 431.83
 625 575
 440 440
 C 1.85 C 1.35

4774.80 R. Carol — 442.69
 4.93
 730
 F 2.37

+49.90 N.L. Bradford — 430.40
 7.18
 626
 C 0.92

4739.80 R.C. Cam) 441.68 440.81
 5.94 6.81
 332 971
 C 2.62 F 2.90

2+29.90 — 429.90
 7.68
 645
 C 1.23

3+89.90 438.80 437.93
 8.82 9.69
 700 12.62
 C 1.82 F 2.93

437.58 X

447.62 X

6+79.84

$$\begin{array}{r} 454.48 \\ 13.55 \\ 11.05 \\ \hline C 2.50 \end{array}$$

T.P. 11.94

468.03A 120 456.09

6+59.84

$$\begin{array}{r} 453.38 \\ 4.01 \\ 2.00 \\ \hline C 2.01 \end{array}$$

6+39.84

$$\begin{array}{r} 452.27 \\ 5.12 \\ 4.17 \\ \hline C 0.75 \end{array}$$

6+19.84

$$\begin{array}{r} 451.15 \\ 6.24 \\ 4.93 \\ \hline C 1.31 \end{array}$$

5+99.84

$$\begin{array}{r} 450.04 \\ 7.35 \\ 6.03 \\ \hline C 1.32 \end{array}$$

5+79.84

$$\begin{array}{r} 446.93 \\ 8.46 \\ 7.25 \\ \hline C 1.21 \end{array}$$

457.39A

8+49.84 BC of
College
Ave
$$\begin{array}{r} 461.70 \\ 6.33 \\ 5.75 \\ \hline C 0.58 \end{array}$$

8+14.84

$$\begin{array}{r} 460.62 \\ 7.41 \\ 6.65 \\ \hline C 0.76 \end{array}$$

7+79.84 EVC

$$\begin{array}{r} 459.55 \\ 8.48 \\ 7.62 \\ \hline C 0.86 \end{array}$$

7+59.84

$$\begin{array}{r} 458.82 \\ 9.21 \\ 5.01 \\ \hline C 1.20 \end{array}$$

7+39.84

$$\begin{array}{r} 457.83 \\ 10.20 \\ 8.52 \\ \hline C 1.68 \end{array}$$

7+19.84

$$\begin{array}{r} 456.72 \\ 11.31 \\ 9.20 \\ \hline C 2.11 \end{array}$$

6+99.84

$$\begin{array}{r} 455.60 \\ 12.43 \\ 10.19 \\ \hline C 2.24 \end{array}$$

468.03A

Curb Stakes College Way Ave from 32
Carol to El Cajon (West Side Only)

Robert
MCCOY
MOORE
CLARK
6-8-50
W.D. 31258

INDEXED
ADD IT

57 79.84 P.V.C.

448.93
5.75
6.09
F 0.34

57 61.40

447.91
6.77
7.11
F 0.34

check

2.76

465.27 = 465.27

NWSP El Cajon
College Ave

975637 ^{EWIT} 96

464.74

57 35.60

446.48
8.20
8.68
F 0.48

9750.67 ^{cb BC} ~~EXIST~~

464.64
3.39
3.51

5709.80 EC. College Ave ^{EC Same}
25.50 # Carol

970

445.05
9.63
9.96
F 0.33

9727.37 BRK

464.08
3.95
3.47
C 0.48

#2 on Cb Ret
from Carol

444.76
9.92
9.46
C 0.46

8488.60

462.89
5.14
5.00
C 0.14

#1 on Cb Ret
from Carol

444.74
9.94
9.37
C 0.57

468.037

TBM

5.84

454.687

see pg. 25

448.94

6+99.84

$$\begin{array}{r} 455.60 \\ 9.76 \\ \hline 993 \\ \hline F 0.17 \end{array}$$

8+26.50

$$\begin{array}{r} 460.78 \\ 4.38 \\ \hline 467 \\ \hline F 0.29 \end{array}$$

6+79.84

$$\begin{array}{r} 454.48 \\ 10.88 \\ \hline 1025 \\ \hline C 0.63 \end{array}$$

8+03.17

$$\begin{array}{r} 460.26 \\ 5.10 \\ \hline 5.30 \\ \hline F 0.20 \end{array}$$

TP 12.35 465.367 167

$$\begin{array}{r} 453.01 \\ 453.38 \\ TP 1.30 \\ 1.67 \\ \hline F 0.37 \end{array}$$

6+59.84

7+79.84 EVC

$$\begin{array}{r} 459.55 \\ 5.81 \\ \hline 608 \\ \hline F 0.27 \end{array}$$

6+39.84

$$\begin{array}{r} 452.27 \\ 2.41 \\ \hline 303 \\ \hline F 0.62 \end{array}$$

7+59.84

$$\begin{array}{r} 458.82 \\ 6.54 \\ \hline 701 \\ \hline F 0.47 \end{array}$$

6+19.84

$$\begin{array}{r} 451.15 \\ 3.53 \\ \hline 402 \\ \hline F 0.49 \end{array}$$

7+39.84

$$\begin{array}{r} 457.83 \\ 7.53 \\ \hline 794 \\ \hline F 0.41 \end{array}$$

5+99.84

$$\begin{array}{r} 450.04 \\ 4.64 \\ \hline 509 \\ \hline F 0.45 \end{array}$$

7+19.84

$$\begin{array}{r} 456.72 \\ 8.64 \\ \hline 887 \\ \hline F 0.23 \end{array}$$

454.687

465.367

check

0.10 465.26 465.27 B M El Cajon College

34

old P.L.

464.74
0.62
0.61

Exist cb B.C. 9+50.12

464.64 464.53
0.72
0.83
11 *15

9+37.82 P.L. BC
12 50

464.40 464.34
0.96 1.02
1.34
1.34
~~F0.38~~ F0.32

9+27.37
10 40

464.08
1.28
1.69
F0.41

9+0.52
25 55

463.29
2.07
2.25
F0.18

8+75.68
25 54

462.49
2.87
3.02
F0.15

8+49.84 B.C. of College Ave
25.88

461.70
3.66
3.96
F0.30

46536T

Roberts
McGoy
Moore
Clark
6-1-50
WA 20593

Stake Sewer Outfall
University Ave. to Chollas Roady²⁹
Along Ely Line Lemon Villa 88

321B

INDEXED
APR 17 1951

35

1+34.25

262.79
13.34
559
7.75

1+07.40

261.34
1479
754
7.25

Exist NH
2+68.46 Univ. Ave.

Exist
270.28 270.00
1701
550
11.51 = 11.51

0+80.55

259.89
1624
901
7.23

2+41.65

268.59
19.70
539
13.31

0+53.70

258.44
17.69
1024
7.45

TP 11.70 287.29X

054 275.59

2+14.80

267.14
899
054
8.45

0+26.85

256.99
19.14
1267
6.47

1+87.75

265.69
1044
205
8.39

0+00

Exist NH
Chollas Rd.

255.34
20.59
2061
✓

1+61.10

264.24
1189
411
7.78

TP

0.21 276.13 T

11.95

275.92

BM

0.84 287.89

12.23

287.03

1.14 299.26

12.86

298.08

NWBP

0.92 310.94

310.02

54 Univ.

276.13 T

Robert
Nley
Moore
Clark
6-9-50
W.O. 21258

Curo Grades for College Way
Bradford to Carol
(West Side Only)

INDEXED

APP 11 1051

36

3 + 75.54

437.98
2.74
316
FO.42

E.C. Carol (Exits)

444.47
3.60
359

3 + 54.13

436.75
397
428
FO.32

2

443.82
4.25
389
C. 0.36

3 + 32.72

435.52
5.20
364
FO.44

1

442.52
5.55
453
C1.00

3 + 11.31

434.28
6.44
688
FO.44

college #
4 + 39.80 E.C. Carol

441.68
6.39
647
FO.08

2 + 87.90 BRK

433.05
767
796
FO.29

TR 7.96 448.07 X
4 + 18.36

0.61 440.11
440.45
0.29
0.61
FO.34

2 + 59.90 EC college #
Bradford

431.33
9.39
895
co. 43 = co. 44

3 + 96.95

439.22
1.50
1.71
FO.21

TBM

10.70

440.72 X

430.02

448.72 X

Roberts
Niley
Moore
Clark

6-12-50
W.O. 31254

0+60

429.12
8.41
874
F 0.33

429.39
8.14
843
F 0.29

1+60

429.01
8.52
887
F 0.35

429.39
8.14
832
F 0.18

0+40

429.29
8.24
851
F 0.27

429.55
7.98
828
F 0.30

1+30

428.85
8.68
895
F 0.27

429.23
8.30
853
F 0.23

0+20

429.10
8.43
869
F 0.26

429.71
7.82
772
C 0.05

1+21.5 First cb

428.84
8.69
870
-

429.18
8.35
858
F 0.23

0+10 EC
curb Kot
Estelle

428.79
8.74
892
F 0.18

429.95
7.58
732
C 0.23

1+05.4 New cb Inlet

429.13
8.40
859
F 0.19

#2

428.34
9.19
920
F 0.01

430.34
7.19
579
C 1.40

Half Exist cb.
0+94.4 New cb Inlet

428.79
8.74
827
✓

429.15
8.38
856
F 0.18

#1

427.60
9.93
10.30
F 0.39

431.06
6.47
617
C 0.30

0+80

428.96
8.57
886
F 0.29

429.23
8.30
868
F 0.38

TBM

7.51 #37.53X

430.02

437.53X

Curb Grades College Way
Estelle to College Ave.

INDEXED
APR 11, 1951

2+70

$$\begin{array}{r} 431.16 \\ 6.37 \\ \hline 680 \\ F 0.43 \end{array}$$

4+15

$$\begin{array}{r} 439.38 \\ 9.39 \\ \hline 1019 \\ F 0.80 \end{array}$$

2+50

$$\begin{array}{r} 430.65 \\ 6.88 \\ \hline 727 \\ F 0.39 \end{array}$$

3+90

$$\begin{array}{r} 437.94 \\ 1083 \\ \hline 1140 \\ F 0.59 \end{array}$$

2+30

$$\begin{array}{r} 429.90 \\ 763 \\ \hline 781 \\ F 0.19 \end{array}$$

T.P. 12.53 448.77 129 436.24

3+65

$$\begin{array}{r} 436.50 \\ 1.03 \\ \hline 129 \\ F 0.26 \end{array}$$

2+10

$$\begin{array}{r} 429.66 \\ 7.87 \\ \hline 810 \\ F 0.23 \end{array}$$

3+40

$$\begin{array}{r} 435.06 \\ 2.47 \\ \hline 258 \\ F 0.11 \end{array}$$

2+00

$$\begin{array}{r} 429.61 \\ 792 \\ \hline 812 \\ F 0.20 \end{array}$$

3+15

$$\begin{array}{r} 433.62 \\ 3.91 \\ \hline 414 \\ F 0.23 \end{array}$$
1+89⁹⁰ BC
cub RT
SW Cor.
Bradford
$$\begin{array}{r} 429.14 \\ 8.35 \\ \hline 835 \\ \text{Grade} = \text{fool} \end{array}$$

$$\begin{array}{r} 429.56 \\ 797 \\ \hline 820 \\ F 0.23 \end{array}$$

2+90

$$\begin{array}{r} 432.18 \\ 5.35 \\ \hline 545 \\ F 0.10 \end{array}$$

437.537

437.537

5+37.16

$$\begin{array}{r} 446.03 \\ 2.74 \\ \hline 358 \\ F 0.84 \end{array}$$

TBM Five Plug

4.31

448.86 = 448.84

5+09.80

$$\begin{array}{r} 444.55 \\ 4.22 \\ \hline 483 \\ F 0.61 \end{array}$$

EXIST CB

$$\begin{array}{r} 445.89 \\ 7.28 \\ \hline 721 \\ \checkmark \end{array}$$
4+99⁸⁰ N.L. Carol
$$\begin{array}{r} 444.00 \\ 4.77 \\ \hline 535 \\ F 0.56 \end{array}$$

EC.

curb Ret.
college Ave
$$\begin{array}{r} 446.15 \\ 7.02 \\ \hline 674 \\ C 0.28 \end{array}$$
4+774⁸⁰ S. Carol
$$\begin{array}{r} 442.69 \\ 6.08 \\ \hline 638 \\ F 0.30 \end{array}$$

#2

$$\begin{array}{r} 447.51 \\ 5.66 \\ \hline 581 \\ F 0.15 \end{array}$$
4+49⁸⁰ S.L. Carol
$$\begin{array}{r} 441.38 \\ 7.37 \\ \hline 801 \\ F 0.62 \end{array}$$

#1

$$\begin{array}{r} 448.20 \\ 4.97 \\ \hline 574 \\ F 0.77 \end{array}$$
4+39⁸⁰

$$\begin{array}{r} 440.81 \\ 7.76 \\ \hline 857 \\ F 0.61 \end{array}$$

T.P. 6.52 453.17A

2.12

446.65

5+64⁵² BCcurb Ret.
college way & Ave.
$$\begin{array}{r} 447.51 \\ 1.26 \\ \hline 212 \\ F 0.86 \end{array}$$

448.77A

448.77A

Roberts
Moore
Clark
6-15-50
W.O. 20632

Stake Storm Drain Market St.
Morrison's Marsden Park
From Exist Drain North 89°
Between Hill & Morrison
3926 B

INDEXED
APR 11 1951

Stake Storm Drain Lots 5 & 6 9/6
South Pacific Unit A
Loring St. West of Electric

6-15-50
W.O. 20662

INDEXED
APR 11 1951

0+84

126.09
117.00
9.09
567
C 3.42

0+95.6

55.01
46.65
8.36
6.16
C 2.20

0+13

126.09
116.30
9.79
876
C 1.93

0+44.8 EC

55.01
45.73
9.28
536
C 3.72

0+42

126.09
115.61
10.48
7.17
C 1.31

0+30.4 ^{Curve} Midpoint

55.01
44.29
10.72
1.72
C 9.00

0+21

126.09
114.92
11.17
924
C 1.93

0+16 BC

55.01
43.77
11.24
4.24
C 7.00

0+00 Exist Drain

Exist
114.06

126.09
114.23
11.86
1203
F 0.17

0+00 Exist Drain

Exist
42.94

43.19
F 0.15

Exist Drain Invert 12.03 126.09 X

114.06

Exist Drain Invert 12.07

55.01 X

42.94

Rough Grades Calle Serena from
 Winchester South to Subd. line 41
 Roberts
 Moore
 Clark
 6-16-50
 No. 62170
 Profile 3124
 R+

0+76.19 267.49 267.99
 7.04 754
 044 864
 C 6.56 F 110

0+56.19 269.27 268.77
 7.26 776
 058 891
 C 6.68 F 115

0+36.19 268.94 268.44
 7.59 809
 076 956
 C 6.83 F 117

0+16.19 PK 268.50 268.06
 8.03 853
 220 973
 C 5.83 F 140

Prop. EC. 267.10 267.60
 0+0 @ Serena 843 893
 Winchester 837 1013
 F 122

TP 12.59 276.53 T 0.09 263.94
 TP 13.01 264.03 0.18 251.02
 BM 6.02 251.20

P.S.M.P.
 245.18
 See Bronze #
 Edgwater 20

1+46.3 End Drain

INDEXED
AUG 22 1952

1+21

5507
 48.50
 6.51
 494
 C 1.57
 5507
 47.57
 7.44
 6.31
 C 1.13

5501 T

1+96.19

268.39
8.14
284
C 5.30

267.89
8.64
960
F 0.96

1+76.19

268.86
7.67
225
C 5.42

268.36
8.17
906
F 0.89

check

TP 0.05 251.66

T.P. 0.39 264.52

6.49 245.17 = 245.18

12.91 251.61

12.40 264.13

1+56.19

269.22
7.31
166
C 5.65

268.72
7.81
844
F 0.63

Sat TBM

6.71 269.8 > EC. Curb Ref.
N.W. Cor.
Calle Serena
Winchester

1+36.19

269.45
7.08
098
C 6.10

268.95
7.58
788
F 0.30

End. Subd. Line
2+76.19

265.90
10.63
686
C 3.67

265.40
11.13
1250
F 1.37

1+16.19

269.58
6.95
062
C 6.33

269.08
7.75
791
F 0.46

2+46.19

266.86
9.67
542
C 4.25

266.36
10.17
1142
F 1.25

0+96.19

269.59
6.94
034
C 6.60

269.09
7.44
818
F 0.74

2+16.19 EVC

267.81
8.72
394
C 4.78

267.31
8.22
1014
F 0.92

276.53 X

276.53 X

Roberts
Moore
Clark
6-20-50
WA 2190

Curb Grades Calle Serena
(Winchester to Calle Pintoresca)

INDEXED
APR 11 1951

Profile 3188

1+33	280.35 2.70 <u>2.99</u> F0.29	280.85 2.20 <u>1.82</u> C0.38	2+53	286.84 7.06 <u>7.27</u> F0.21	287.34 6.56 <u>6.21</u> C0.35
1+13 P.V.C.	278.83 4.22 <u>4.60</u> F0.38	279.33 3.72 <u>3.45</u> C0.27	2+33	286.67 7.83 <u>7.82</u> C0.01	286.57 7.33 <u>7.04</u> C0.29
0+84.75	276.49 6.56 <u>7.23</u> F0.67	276.99 6.06 <u>5.80</u> C0.26	2+13	285.18 8.72 <u>8.61</u> C0.11	285.68 8.22 <u>7.76</u> C0.46
0+56.50	274.16 8.89 <u>8.82</u> C0.07	274.66 8.39 <u>8.08</u> C0.31	1+93	284.75 9.75 <u>9.77</u> F0.02	284.65 9.25 <u>8.44</u> C0.81
0+28.25	271.83 11.22	272.33 10.72 <u>10.31</u> C0.41	1+73	283.01 10.89 <u>10.87</u> C0.02	283.51 10.39 <u>9.41</u> C0.98
0+00 E.C. Curb Ret Winchester	269.50 13.55 <u>13.50</u> ✓	270.00 13.05 <u>13.07</u> ✓	J.P. 1+53	11.09 293.90 X 281.74 1.31 <u>1.26</u> C0.05	0.24 282.81 282.24 0.81 <u>0.24</u> C0.57
TBM	13.23 283.05 X	269.82 13.42			

3773
 288.83
 507
 512 ✓
 F0.05

289.33
 4.57
 404 ✓
 C0.53

5753 FVC
 287.56
 6.34
 648 ✓
 F0.14

288.06
 5.84 ✓
 572
 C0.12

3753
 288.81
 5.09 ✓
 504
 C0.05

289.31
 4.59
 386
 C0.73

5721
 287.78
 6.12 ✓
 606
 C0.06

288.28
 5.62 ✓
 556
 C0.06

3733
 288.66
 5.24 ✓
 542
 F0.18

289.16
 4.74 ✓
 424
 C0.45

4789
 288.00
 5.90 ✓
 574
 C0.16

288.50
 5.40 ✓
 522
 C0.18

3713
 288.40
 5.50 ✓
 583
 F0.33

289.90
 5.00 ✓
 445
 C0.55

4757
 288.22
 5.68 ✓
 543
 C0.25

288.72
 5.18 ✓
 512
 C0.06

2793
 288.00
 5.90 ✓
 623
 F0.33

288.50
 5.40 ✓
 463
 C0.77

4725
 288.44
 5.46 ✓
 554
 F0.08

288.94
 4.96 ✓
 401
 C0.95

2773
 287.48
 6.42 ✓
 686
 F0.44

287.98
 5.92 ✓
 539
 C0.53

3793 FVC
 288.67
 5.23 ✓
 527
 F0.04

289.17
 4.73 ✓
 388
 C0.85

6+73

$$\begin{array}{r} 284.36 \\ 2.18 \checkmark \\ \hline 244 \\ \hline F0.26 \end{array}$$

$$\begin{array}{r} 284.86 \\ 1.68 \checkmark \\ \hline 138 \\ \hline C0.30 \end{array}$$

#3

$$\begin{array}{r} 279.20 \\ 7.34 \checkmark \\ \hline 738 \\ \hline F0.84 \end{array}$$

$$\begin{array}{r} 280.70 \\ 5.84 \\ \hline 544 \checkmark \\ \hline C0.40 \end{array}$$

TP 124

6+53

$$\begin{array}{r} 286.54 \checkmark \\ 285.22 \\ 8.68 \checkmark \\ \hline 920 \\ \hline F0.52 \end{array}$$

9.20 284.70

$$\begin{array}{r} 285.72 \\ 8.18 \\ \hline 826 \checkmark \\ \hline F0.08 \end{array}$$

#2

$$\begin{array}{r} 279.84 \\ 6.76 \checkmark \\ \hline 629 \checkmark \\ \hline C0.41 \end{array}$$

$$\begin{array}{r} 280.70 \\ 5.84 \checkmark \\ \hline 556 \checkmark \\ \hline C0.28 \end{array}$$

6+33

$$\begin{array}{r} 285.95 \\ 7.95 \checkmark \\ \hline 812 \\ \hline F0.17 \end{array}$$

$$\begin{array}{r} 286.45 \\ 7.45 \checkmark \\ \hline 782 \\ \hline F0.37 \end{array}$$

#1

$$\begin{array}{r} 280.50 \\ 6.04 \checkmark \\ \hline 560 \\ \hline C0.44 \end{array}$$

$$\begin{array}{r} 281.00 \\ 5.54 \checkmark \\ \hline 518 \checkmark \\ \hline C0.36 \end{array}$$

6+13

$$\begin{array}{r} 286.55 \\ 7.35 \checkmark \\ \hline 744 \checkmark \\ \hline F0.09 \end{array}$$

$$\begin{array}{r} 287.05 \\ 6.85 \checkmark \\ \hline 727 \checkmark \\ \hline F0.42 \end{array}$$

$$\begin{array}{r} 7+28.79 \text{ B.C. Curb } 281.30 \\ \text{Ret. } 5.24 \checkmark \\ \text{Calle Pintoresca } 505 \\ \hline C0.19 \end{array}$$

$$\begin{array}{r} 281.80 \\ 4.74 \checkmark \\ \hline 454 \checkmark \\ \hline C0.20 \end{array}$$

5+93

$$\begin{array}{r} 287.02 \\ 6.88 \checkmark \\ \hline 693 \\ \hline F0.05 \end{array}$$

$$\begin{array}{r} 287.52 \\ 6.38 \checkmark \\ \hline 652 \\ \hline F0.14 \end{array}$$

7+13

$$\begin{array}{r} 282.24 \\ 4.30 \checkmark \\ \hline 436 \\ \hline F0.06 \end{array}$$

$$\begin{array}{r} 282.74 \\ 3.80 \checkmark \\ \hline 283 \\ \hline C0.97 \end{array}$$

5+73

$$\begin{array}{r} 287.36 \\ 6.54 \checkmark \\ \hline 677 \checkmark \\ \hline F0.23 \end{array}$$

$$\begin{array}{r} 287.86 \\ 6.04 \checkmark \\ \hline 586 \\ \hline C0.18 \end{array}$$

6+93

$$\begin{array}{r} 283.37 \\ 3.17 \checkmark \\ \hline 342 \\ \hline F0.25 \end{array}$$

$$\begin{array}{r} 283.87 \\ 2.67 \\ \hline 194 \\ \hline C0.73 \end{array}$$

293.90X

286.54X

S#TBM

275.26

3.05

283.49

Fire Hyd.

SE Cor
Calle Serena #
Pintaresca

EC curb Ret
Calle Serena

276.75
89.79 ✓
1078
F0.99

276.98
277.25
9.29 ✓
956
F0.27

27

#3

277.55
87.96 ✓
978
F0.79

277.80
8.74 ✓
856
C0.18

#2

278.25
8.29 ✓
912
F0.83

279.25
7.29 ✓
716
C0.13

#1

278.40
8.14 ✓
891
F0.77

280.06
6.54 ✓
629
C0.25

North Side
curb Ret
BC Calle Pint.

278.00
8.54 ✓
949
F0.75

280.50
6.04 ✓
687
F0.63

EC curb Ret
Calle Pintaresca

278.50
8.04 ✓
821
F0.17

281.00
5.54 ✓
517
C0.37

Check

10.24 269.80 = 269.82

T.P. 0.44 280.04 11.24 277.60

T.P. 4.41 280.84 0.11 286.43

286.547

Roberts
Moore
Clark
6-21-50
No. 2190

Curb Grades Calle Pintoresca
(Calle Serena to Calle Trepadora)

Profile 3247

INDEXED

T.P. APP 11 1950

0.29

47

9.01 30 0.51 2.79 296.50

1+66.66	286.07 8.22 <u>796</u> C 0.26	286.57 7.72 <u>785</u> F 0.13	3+73.70	292.58 1.71 <u>201</u> F 0.30	293.08 1.21 <u>131</u> F 0.10
---------	--	--	---------	--	--

1+33.33	284.96 9.33 <u>936</u> F 0.03	285.46 8.83 <u>884</u> F 0.01	3+36.85	291.44 2.85 <u>311</u> F 0.26	291.94 2.35 <u>248</u> F 0.13
---------	--	--	---------	--	--

1+00	283.84 10.45 <u>1038</u> C 0.07	284.34 9.95 <u>999</u> C 0.16	3+00 B.C. Curb Ret. Aguadulce	290.30 3.99 <u>414</u> F 0.15	290.80 3.49 <u>391</u> C 0.08
------	--	--	----------------------------------	--	--

0+66.66	282.73 11.56 <u>1187</u> F 0.31	283.23 11.06 <u>1086</u> C 0.20	2+66.66	289.26 5.03 <u>502</u> C 0.01	
---------	--	--	---------	--	--

0+33.33	281.61 12.68 <u>1285</u> F 0.17	282.11 12.18 <u>1193</u> C 0.25	2+33.33	288.23 6.06 <u>598</u> C 0.08	
---------	--	--	---------	--	--

0+00 B.C. on East Calle Serena	290.50 F 0.93	291.00 C 0.37 1329 1292 C 0.37	2+00 B.C. Curb Ret. Agu Dulce	287.20 7.09 <u>698</u> C 0.11	287.70 6.59 <u>658</u> C 0.01
-----------------------------------	------------------	--	----------------------------------	--	--

TBM 10.70

294.29X

293.49 46

294.29X

check 8.12 285.48 = 283.47

T.P. 1.50 291.60 10.41 290.10

B.C. curb Ret.	296.83	297.33
- 5710.54 Trepadora	3.68 ✓	3.19 ✓
	<u>3.56</u>	<u>3.05</u>
	C0.12	C0.13

4777.21 ^{RL}	—	296.29
		4.22 ✓
		<u>4.04</u>
		C0.18

4743.88 ^{RL}	—	295.26
		5.25 ✓
		<u>5.05</u>
		C0.20

B.C. Curb Ret.	293.73	294.23
4710.55 Trepadora	6.78 ✓	6.29 ✓
	<u>7.17</u>	<u>6.11</u>
	F 0.39	C0.17

300.517

Roberts
Moore
Chick
6-21-50
No. 31258

Curb Grades College Ave.
(El Cajon to Exist Curb & Pav.)

75682

INDEXED

APR 11 1951

49

1+08.86 BC Curb/Ret Peck/Place

Rd. Pl. $\frac{443.06}{3.38}$
 $\frac{351}{F0.13}$

1+90.07

$\frac{460.34}{6.10}$
 $\frac{647}{F0.37}$

0+87.07

$\frac{463.73}{2.71}$
 $\frac{269}{C0.02}$

BC Cb Ret + 53.38
26.69

$\frac{461.52}{4.92}$
 $\frac{504}{F0.12}$

0+65.27

$\frac{464.40}{2.04}$
 $\frac{216}{F0.12}$

Midpoint

$\frac{461.72}{4.72}$
 $\frac{486}{F0.14}$

0+46.72

$\frac{464.68}{1.76}$
 $\frac{197}{F0.21}$

EC

$\frac{461.92}{4.52}$
 $\frac{451}{C0.01}$

0+26.51

$\frac{464.76}{1.68}$
 $\frac{175}{F0.07}$

End Cb. Ret.
So. Side Peck Pl.

$\frac{461.98}{4.46}$
 $\frac{457}{F0.11}$

NE PL
0+00 Intersection

$\frac{464.60}{1.84}$
 $\frac{180}{}$

End Cb. Ret.
Peck Pl.

$\frac{462.47}{3.97}$
 $\frac{377}{C0.18}$

BM

11.7

466.447

465.27 NNEP
College & El Cajon

North

466.447

T.P. 127 45540x 12.31 454.13

1 3+10

454.29
12.15
12.31 ✓
F 0.16

4 + 20.91 Exist Pav.

446.79
8.91
✓

0 2+90

455.62
10.82
11.20 ✓
F 0.38

440.252 FC
11.29

447.79
7.61
7.82 ✓
F 0.21

2+70

456.83
9.61 ✓
10.02
F 0.41

3+90
12.25

448.67
6.73 ✓
7.12
F 0.39

0 2+50

457.88
8.56 ✓
8.88
F 0.32

3+70

450.08
5.32
5.65 ✓
F 0.33

2+30

458.84
7.60 ✓
7.91
F 0.31

3+50

451.48
3.92 ✓
4.10
F 0.18

2+10

459.66
6.78 ✓
7.23
F 0.45

3+30

452.89
2.51 ✓
2.42
C 0.09

466.44T

455.40 T

Roberts
Moore
Clark
6-28-50
NO. 2 439

Stake Storm Drain La Jolla Hermosa
La Jolla Blvd. to Camino de la Costa

77252 FB2000

Cont'd

51

INDEXED

APR 11 1951

Commercial to La Jolla

9+27.29 Exist
culvert

45.66
COVERED 10'

6+80.59 EC Exist
culvert

61.82
covered

29.75

8+92.71

46.57
16.87
761
C 9.26

6+50.84

64.92
10.98
690
C 4.08

29.75

8+58.15

49.48
1396
556
C 8.40

6+21.09 BC

68.03
787
449
C 3.38

2066

8+23.59

52.39
11.05
372
C 7.33 ±

5+96.43 EC

70.61
5.29
400
C 1.29

15.18

7+89.03 Exist
Culvert

55.30 ±
COVERED 10'

5+81.25 BC Exist
culvert

72.20
To Be Cut

TBM

7.46

6.3447

53.98 curb

13 1/2 TBM
FB2000

3.92

75.907

FB 2000
Spec P
71.97 RL
Type

Cont'd from page 51

From La Canada & RR Row to
Avenida Commercial

52

1+48.7

84.18
1382
591
C 7.91

3+61.1

82.07
1593
639
C 9.54

1+13.3

84.54
1346
576
C 7.70

3+25.7

82.42
1558
623
C 9.35

0+77.9

84.89
1311
544
C 7.67

2+90.3

82.77
1523
603
C 9.20

0+42.5 EC

85.25
1275
499
C 7.76

2+54.9

83.15
1487
507
C 9.80

0+08 BC

85.60
1240
548
C 6.92

2+19.5

83.48
1452
554
C 8.98

025E of E.L. & RR ROW
0+00 & La Canada

85.68
1232
549
C 6.83

1+84.12

83.83
1417
572
C 8.45

BM

522

98.00 T

92.78

Chisel + = 0+00 FE 2000 pgk

98.00 T

5700

78.43
1694
955
C 7.39

4775

79.93
1544
812
C 7.32

4750

80.93
1444
677
C 7.67

T.P. 569

95.37A 832

89.68

check

10.75

84.62 = 84.61

FB2000
Pg 7

4733 EC

21.27
1673
TP → 832
C 8.41

3798.5 BC

81.70
1630
658
C 9.72

5720.4 EC ^{connect} Exist

76.90
1847
1066
C 7.81

3796.5 BRK

81.72
1628
659
C 9.69

5709 BC

77.76
1761
1041
C 7.20

9800 T

Roberts
Moore
Clark
7-26-58
W020449

State Storm Drain BIK2
University place (lots 16, 17)
Robinson to Alley
FB1413 pg 51

INDEXED
APR 11 1954

0x0
3689-B 3690-B
288.63
282.25
13.78
9.43
C-3.95

0x80
296.63
282.65
13.58
9.22
C-4.36

0x60
296.63
282.85
13.78
9.12
C-4.66

0x40
296.63
282.65
13.98
8.31
C-5.87

0x20
296.63
282.75
14.18
5.84
C-8.34

0x0 Exist Storm Drain 15' So. No. Line Robinson
296.63
282.25
14.38
6.01
C-9.37

1780.51 EC
296.63
287.05
12.58
9.10
C-3.48

1745.17 BC
296.63
282.70
12.93
9.39
C-3.54

1720
296.63
283.45
13.18
9.65
C-3.53

BW 258 296.63 T 294.05 SWBP Robinson & Richard 296.63 T

Grade Stakes For Storm Drain In Midway St., La Jolla Blvd. to San Rosa

Reber's
Moore
Clark
Lathrop
Aug 15, 1950
W. 2066

INDEFINITE
APR 17 1951

1+25
8071-L 72.54
32.56
19.84
10.82
C 9.02

2+50

59.98
44.63
15.35
732
C 8.03

1+0
72.34
57.26
18.08
10.56
C 7.52

2+25

57.92
46.11
13.81
584
C 8.03

0+75
72.34
56.02
16.32
9.57
C 6.75

-5.76 54.22
Conc. Man 54.20

2+0

59.98
47.58
12.40
4.23
C 7.57

0+50
72.34
57.78
14.56
8.81
C 5.75

1+72 BRK

59.98
49.23
10.75
3.42
C 7.33

0+25
72.34
59.54
12.80
5.43
C 7.37

1+64 BRK

59.98
49.74
10.54
2.71
C 7.53

Stakes 10' No.
0+0
Begin Drain
at Cleanout
90° to Conc. Man
72.34
61.30
11.04
3.67
C 7.37

T.P. 0.67 59.98 X

1+50

13.03 59.31
72.34
50.74
21.60
13.03
C 8.57

BM

0.29 72.34 A

72.06 NEBP
La Jolla & Midway

72.34 A

3772 BRK

$$\begin{array}{r} 4930 \\ 3717 \\ 1013 \\ \hline 350 \\ \hline C 6.63 \end{array}$$

3764 BRK

$$\begin{array}{r} 4730 \\ 3781 \\ 949 \\ \hline 300 \\ \hline C 6.49 \end{array}$$

3756 BRK

$$\begin{array}{r} 4730 \\ 3837 \\ 893 \\ \hline 142 \\ \hline C 7.51 \end{array}$$

T.P. Q14 47.30 \uparrow 12.82 47.16

3725

$$\begin{array}{r} 59.98 \\ 40.21 \\ 19.77 \\ \hline 11.25 \\ \hline C 8.52 \end{array}$$

370

$$\begin{array}{r} 59.98 \\ 41.68 \\ 18.30 \\ \hline 8.66 \\ \hline C 9.64 \end{array}$$

2775

$$\begin{array}{r} 59.98 \\ 43.16 \\ 16.82 \\ \hline 709 \\ \hline C 9.73 \end{array}$$

59.98 \uparrow

5725

$$\begin{array}{r} 34.91 \\ 23.34 \\ 11.57 \\ \hline 324 \\ \hline C 8.33 \end{array}$$

TP 0.06 34.91 \uparrow 12.45 34.95

570

$$\begin{array}{r} 47.30 \\ 25.60 \\ 21.70 \\ \hline 10.74 \\ \hline C 10.96 \end{array}$$

Set TBM 8.04 39.26 $\frac{1}{2}$ Rip N.P.L. 47.632

4774 EC

$$\begin{array}{r} 47.30 \\ 27.95 \\ 19.35 \\ \hline 723 \\ \hline C 12.12 \end{array}$$

4750 Midpoint

$$\begin{array}{r} 47.30 \\ 30.12 \\ 17.18 \\ \hline 766 \\ \hline C 9.52 \end{array}$$

4726 BC

$$\begin{array}{r} 47.30 \\ 32.29 \\ 15.01 \\ \hline 691 \\ \hline C 8.10 \end{array}$$

470

$$\begin{array}{r} 47.30 \\ 34.64 \\ 12.66 \\ \hline 551 \\ \hline C 7.15 \end{array}$$

47.30 \uparrow

#5	28.86					
	12.19	5#C				See FB 1213 pg 63
	16.67		check		3.19	42.12 = 42.07
	4.89					
	<u>C 11.78</u>		T.P.	10.47	45.31	007 3484

#4	28.86				54.91	16.87
	15.02	6#7	#10 (5490.34)	End Storm Drain on Beach	0.00	0.00 Reset
	13.84				34.91	16.87
	4.97				15.20	7.77
	<u>C 8.87</u>				<u>C 19.11</u>	<u>C 9.70</u>

#3	28.86				16.87	
	17.16	7#8	#9		0.68	
	11.70				16.19	1#2
	4.72				6.40	
	<u>C 7.28</u>				<u>C 9.79</u>	

#2	28.86				16.87	
	14.82	8#9	#8		2.03	2#3
	10.04				14.84	
	4.15				3.31	
	<u>C 5.89</u>				<u>C 11.53</u>	

#1	28.86				16.87	
	19.96	9#10	#7		4.00	
	8.90				12.87	3#4
	3.67				1.87	
	<u>C 5.23</u>				<u>C 11.00</u>	

			T.P.	0.26	16.87	12.25	16.81
57 56 PVC	34.91	28.86			28.86		
	20.54	20.54	Reset		6.53		4#5
	14.37	8.32			2.23		
	4.9	3.06			1.092		
	<u>C 10.28</u>	<u>C 5.26</u>			<u>C 11.41</u>		

T.P.	1.15	28.86	12.19	27.71	28.86
TBM	0.64	39.90		39.26	

34.91

34.91

Roberts
Clark
Finney
Aug. 11, 1950

Curb Ret.
La Tolla & Midway

8071L

EC Exist

71.50
450
460

Ret 20

71.20^e
4.80
452
C 0.28

BC 20 Rd.

70.70
5.30
529
C 0.01

End Inlet

69.54
646
734
F 0.88

Ch. Enlet

68.90
7.10
785
F 0.75

EC Midway

68.00
8.00
852
F 0.52

BM

394

76.00A

72.06

58

BC IMPROVED
APP 11 1951

70.49
551
555
F 0.04

Begin Inlet

70.28
572
603
F 0.31

Ch. Inlet

69.95
6.05
620
F 0.15

End EC Inlet

69.48
652
610
C 0.42

5' W. EC

69.21
6.79
582
C 0.97

15.79 W. EC

68.40
7.60
662
C 0.98

Westerly

Southerly

Roberts
Clark
Hatch
Lockhead
August 23, 1950
No. 20709
1745.60

Grade Stakes For Sewer

From Anna Ave. North to East Sewer

20'	15'
4058 5.67	1337 1282
-5.03	-5.03 503
17.72	1840 1285
498	537 1390
C 12.74	C 13.03

17 16.48

12.69	1337 1282
-4.99	-4.99 499
17.68	1836 1781
474	491
C 12.94	C 12.93

07 8.736

12.69	1337 1282
-4.94	-4.94 494
17.63	1831 1776
485	322
C 12.78	C 13.73

07 58.24

12.69	1337 1567
-4.90	-4.90 490
17.59	1827 2057
514	472
C 12.71	C 15.85

07 29.12

12.69	1337 1609	1609
-4.85	-4.85 485	-4.85
17.54	1822 2094	2094
450	452	424
C 13.04	382 C 16.42	C 16.70

Reet from 20' 15' Reet

07 00 @ Anna Ave

12.69	1337 E	W
-4.81	-4.81 1635	1635
17.50	1818 2176	-4.81
389	529	21.76
C 13.61	414 C 16.47	C 16.58

10.51 16.75T

9.65
9.23
6.31

6.93

BM

6.25

6.44
16.09
15.67
12.82T
13.37T
12.69T

6.44
6.44
6.44 Reet
6.44 Reet
6.44 Conc. Man

@ Sherman 25' S of My Line

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1794
155
1639

395 59

20'	15'
12.69	1337
-5.25	-5.25
17.94	1862
806	886
C 9.88	C 9.76
12.69	1337
-5.21	-5.21
17.90	1858
791	891
C 9.99	C 9.67
12.69	1337
-5.17	-5.17
17.86	1854
686	810
C 11.00	C 10.44
12.69	1337 1282
-5.12	-5.12 512
17.81	1849 1724
612	669 650
C 11.69	C 11.80
12.69	1337 1282
-5.08	-5.08 508
17.77	1845 1790
531	576
C 12.46	C 12.60

12.69 13.37T

Morgan

INDEXED

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Grade Stakes For Alley BIK 132

Manasse & Schiller
16th to Sigsbee
Between Newton & National

FB2008 pg 37 7806L

2+

£

Rt 60

1720
0.10
852
4.90
3.72
3.59
C 0.13852
4.78
3.74
3.29
C 0.452+30
nail 11.42
0.20 5.70
3.23
C 2.771712
11.42
5.70 2'
5.11
C 0.591700
1'
852
4.30
4.22
3.08
C 0.14852
4.20
4.32 2'
4.29
C 0.052+10
nail 10.35
0.10 6.77
5.95
C 0.821712
10.35
6.77 2'
6.05
C 0.720+80 PVC 2'
852
4.20
4.32
4.47
C 0.15852
4.10
4.42 2'
3.96
C 0.461790 2'
17.12
8.94
8.18
7.13
C 1.058.94
8.18 2'
7.08
C 1.150+40
chisel
0.15
852
3.61
4.91
4.47
C 0.44852
3.49
5.03
2.52
2.52
C 1.511780 2'
17.12
8.16
8.96
8.06
C 0.901712
8.16
8.96 2'
7.77
C 1.190+00 East Pl.
16th St
852
3.02
5.50
3.50
L

2.88

T.P. 9.25 17.12 T 0.65 7.27
1760
nail 8.52
0.05 6.73
1.79
1.05
C 0.748.52
6.73 2 1/4"
1.79 0.30
1.17
C 0.621+40 1'
852
5.61
2.71
2.80
C 0.11852
5.61
2.93 2'
1.87
C 1.06

BM

6.78

8.52 T

1.82 NWBP

16th & Newton

8.52 T

Cont'd From Pg. 60

	Lt	£	Rt	Lt	£	Rt	
3760	2'	17.12 13.45 3.67 <u>3.43</u> C 0.22	13.45 3.62 <u>2.93</u> C 0.69	5720	4'	13.77 4.90 1.72 <u>C 3.18</u>	20.67 15.77 4.90 4.50 <u>C 0.40</u>
3730	nail 1.07	17.12 13.14 3.98 <u>3.30</u> C 0.68	13.14 3.98 <u>3.67</u> C 0.31	5700	chisel 1'	15.20 5.47 <u>4.87</u> C 0.58	20.67 15.20 5.47 <u>3.88</u> C 1.59
3700	Pipe chisel 0.21	17.12 12.73 4.29 <u>3.62</u> C 0.67	12.83 4.29 4.12 <u>C 0.17</u>	4780	2'	14.76 5.91 5.41 <u>C 0.50</u>	20.67 14.76 5.91 <u>4.35</u> C 1.56
2785	Sewer Lat Nail on Rt	17.12 Exist 7.10 10.02 <u>3.42</u> C 6.60	17.12 P.L. 8.55 8.57 <u>3.42</u> C 5.15	4760	PVC 2'	5.80 20.67 14.48 2.64 <u>2.35</u> C 0.29	2.25 14.87 17.12 14.48 2.64 <u>1.34</u> C 1.30
2770	FVC 2'	12.52 4.60 <u>5.05</u> F 0.45	17.12 12.52 4.60 4.67 <u>F 0.07</u>	4720	1'	17.12 14.07 3.05 <u>2.92</u> C 0.13	14.07 3.05 <u>2.60</u> C 0.45
2750	nail 1'	17.12 12.14 4.98 <u>4.51</u> C 0.47	12.14 4.98 5.06 <u>F 0.08</u>	3790	nail 2.23	17.12 13.76 3.36 <u>2.35</u> C 1.01	13.76 3.36 <u>2.08</u> C 1.28

17.12 X

17.12 X

Cont'd from pg. 61

23.94 NE BP
Notions &
Rt Sigsbee

check 2.45 23.93 = 23.94

TP 2.69 26.38 1.98 18.69

6701.02 west P.L. 20.67 20.67
Sigsbee 19.12 18.92
1.55 1.75
1.68 1.88

5770 2' 20.67 20.67
17.99 17.69
2.88 2.98 nail 1.40
1.26 2.00
C 1.62 C 0.98

chisel 0.07
5768.49 End 19.29 17.70
Retaining wall on Lt. 1.38 2.97
1.50 1.50
F 0.12 C 1.47

chisel 0.20
5752.49 Begin 20.67 18.24
Retaining wall on Lt. 19.29 17.00
1.38 3.67
1.63 1.63
F 0.25 C 2.04

5740 EVC 16.50 20.67
4.17 16.50 nail 0.30
1.24 4.17
C 2.93 C 1.33

20.67A

Roberts
Clark
Hatch
Lochhead
8-29-50
W.O. 31437
1+15

Grade Stakes Evergreen St.
Carlton to Fenelon

INDEXED

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	7608L	26.15		22.41	
	22.16	21.66	#4		
	4.0	4.49			
	21	4.9			
	C1.9	F0.4			
0+85	26.15	26.15			
	22.84	22.34	#3	21.36	1962 Exist
	3.31	3.81			
	07	3.9			
	C2.6	F0.1			
0+55	26.15	26.15			
	23.52	23.02	#2	20.60	1982
	2.63	3.13			
	01	3			
	C2.5	C0.1			
0+25 EC	26.15	26.15			
	24.20	23.70	#1	20.50	20.05
	1.95	2.45			
	1.1	2.26			
	C2.7	C0.4			
		0.2			
0+12.5	24.50	23.82	1+95 BC	26.15	26.15
				20.80	20.30
				5.35	5.85
				23	5.7
				C3.1	C0.2
Pl. Carlton	24.93	26.15		26.15	26.15
0+00 Exist Cb.		23.97	1+45	21.48	20.98
		2.18		4.67	5.17
		2.18		2.5	5.2
		✓		C2.2	F0.4

BM 7.65 26.15 T 18.50 Disc Sly Cor. Emerson & Evergreen

#4 20.10

$$\begin{array}{r}
 26.15 \\
 19.30 \\
 6.85 \\
 \hline
 39 \\
 \hline
 C 3.0
 \end{array}$$

#3 20.35

$$\begin{array}{r}
 26.15 \\
 19.44 \\
 6.71 \\
 \hline
 43 \\
 \hline
 C 2.4
 \end{array}$$

#2 21.25

$$\begin{array}{r}
 26.15 \\
 19.58 \\
 6.57 \\
 \hline
 39 \\
 \hline
 C 2.7
 \end{array}$$

#1 22.43

$$\begin{array}{r}
 26.15 \\
 19.72 \\
 6.43 \\
 \hline
 37 \\
 \hline
 C 2.7
 \end{array}$$

EC on Dickens 23.50

$$\begin{array}{r}
 26.15 \\
 19.86 \\
 6.29 \\
 \hline
 34 \\
 \hline
 C 2.9
 \end{array}$$

EC on Dickens 23.50

$$\begin{array}{r}
 26.15 \\
 BC \text{ on Evergreen } 20.00 \\
 0+25 \quad 6.15 \\
 \hline
 33 \\
 \hline
 C 2.9
 \end{array}$$

 1
 5
 +
 11

 1
 5
 +
 11
26.15 π Rough

0+50	2843	²⁷⁰⁵ 2159 546	2843
0+55	21.71	<u>364</u> 6.72 C1.82	21.20
		<u>47</u>	7.23
		22.0	<u>72</u>
			GRD

2100 PL Fenelon ↑

24.04 Exist

0+25 EC	28.43	²⁷⁰⁵ 21.00 7.43	28.43
		<u>6.05</u> 4.99	20.50
		<u>45</u>	7.93
		22.9	<u>18</u>
			20.1

17875

24.10

0+12.5	20.85		20.10
--------	-------	--	-------

1775 BC

2843	2705	28.43
24.53	24.53	24.00
3.90	252	443
390	<u>252</u>	42
		20.2

1750

0+00 Emerson	PL. EXIST 20.96		19.66
	6.09		
	6.07		

1745

1725 →

2705
23.95
310

2705	28.43
2336	23.70
369	4.73
<u>288</u>	45
0.81	20.2

2700 Emerson	PL. EXIST 19.97
--------------	-----------------

1715

1400 H. EXIST

28.43	2705	28.43
22.76	22.77	22.60
5.67	428	5.85
5.03	<u>308</u>	55
	1.20	20.3

EXIST

17875	19.42
-------	-------

0+85

0+75

2843	2705	28.43
22.42	22.77	21.90
6.01	428	6.53
38	<u>308</u>	62
2.2	1.20	20.3

BM	855	27.05X	18.50 For City Crew
	9.93	28.43A	18.50

28.43

Roberts
8-29-56

Grade Stakes Dickens St.
Evergreen 200' North

66

INDEXED

7609L

APR 11 1951

1+50

41.19
35.79
5.40
66
F0.8

41.19
35.70
6.09
56
C0.5

1+30

41.19
32.92
8.27
86
F0.3

41.19
32.30
8.89
78
C1.1

1+10 PVC

41.19
30.81
10.38
96
C0.8

41.19
30.30
10.89
75
C1.4

TP
0+75

12.24

41.19 T 0.12
27.80
1.27
09
C0.4

28.95

27.50
1.57
08
C0.8

2+00

41.19
End 46.25
+5.06
+31
F2.0

41.19
45.50
+4.31
0.8
F5.1

0+50

29.07
25.65
3.42
34
GRD

29.07
25.50
3.57
35
C0.1

1+90

41.19
43.85
+2.66
14
F4.1

41.19
43.10
+1.91
-1.8
F3.9

EC 0+25

29.07
23.50
5.57
48
C0.8

23.50
5.57
44
C1.2

1+70

41.19
37.43
1.76
49
F3.1

41.19
38.70
2.49
42
F1.7

10.57

29.07 T

18.50

41.19 T Rough

Roberts
Cota
Moore
Clark

Grade Stakes for Alley BK 53
Ocean Beach
Cable to Sunset Cliffs

12-20-50
W.P. 31782

Between Santa Monica & Newport 2021
19.40
19.40
1939
F0.01

1+00 ETC 3' BK

3' BK C 0.81

2+40 3' BK

20.11
20.10
F0.01

2' BK C 0.01

T.P.

19.40

19.60

19.20

3' BK C 0.40

Sow. Lat #1
2+35 on Right

20.08
14.02
C 6.06

20.08

15.08

C 5.00 5' BK

0+80

3' BK

19.20
19.18

F0.02

19.03
18.80

3' BK C 0.23

19.20

18.80

3' BK

C 0.40

2+20 PVC 3' BK

20.06
20.00
C 0.06

3' BK

20.11

20.00

C 0.11

0+60

18.64
18.20

1' BK C 0.44

18.77
18.20

3' BK

C 0.57

1+90

0.7' BK

20.08
17.85
C 0.23

3' BK

20.40

19.85

C 0.55

0+40

18.42
17.40

3' BK C 1.02

18.65
17.40

C 1.25 3' BK

1+60

0.1' BK

20.20
19.70
C 0.50

3' BK

20.22

19.70

C 0.52

0+20

0+00 E.L. Cable
PVC
Exist

16.47

16.46

✓

16.39

16.40

✓

1+30

1' BK

19.55
19.19
F 0.36

3' BK

20.25

19.55

C 0.70

BM

Direct Rod

NEBP
16.01 Cable Newport

CE
IMPROVED

APR 11 1951

R

R

67

Lt	Q	Rt	Lt	Q	Rt 68
					2300
					22.88
			4+85	3'BK	22.76
					F 0.12
3+60	3'BK	2162 21.19 C 0.43			3'BK C 0.12
					2350
					0.5BK 22.46
			4+60	EVC	C 1.04
3+40	2.7BK	2110 20.99 C 0.11			3'BK C 0.09
					22.55
					22.46
					22.48
					22.13
			4+40	2'BK	C 0.32
3+20	P.L.	21.46 20.79 C 0.67			0.5BK C 0.35
					22.45
					22.13
					22.77
					21.84
			4+20	0.35BK	C 0.93
3+00	EVC 0.1BK	2112 20.59 C 0.53			0.3BK C 1.08
					22.92
					21.84
					22.41
					21.60
			4+00	0.5BK	C 0.81
2+80	0.8BK	2117 20.41 C 0.76			3'BK C 0.44
					22.04
					21.60
					21.80
					21.38
			3+80	PVC	C 0.42
2+60	3'BK	20.25 20.15 F 0.10			3'BK C 0.06
					21.44
					21.38
					20.25
					20.22
					F 0.03
T.P.		20.29			

5799 ⁸⁸	w.L. Sunset EVC EXIST	24.55 24.52 ✓	24.47
--------------------	-----------------------------	---------------------	-------

5780	3' BK	25.26 24.38 C 0.88	2' BK 24.79 24.38 C 0.41
------	-------	--------------------------	-----------------------------------

5760 PK	3' BK	24.81 24.15 C 0.66	2' BK 24.74 24.15 C 0.59
---------	-------	--------------------------	-----------------------------------

5735	3' BK	24.67 23.72 C 0.35	3' BK 23.92 23.72 C 0.20
------	-------	--------------------------	-----------------------------------

5710	3' BK	23.62 23.30 C 0.32	2' BK 23.93 23.30 C 0.63
------	-------	--------------------------	-----------------------------------

T.P.

23.43

STAKE SOUTH CURB RETURN
CUMBERLAND & CAJAL TRES LOMAS

76

INDEXED
OCT - 2 1952

#5
300.18
301.25
F 1.07

#4
300.90
301.92
F 1.02

#3
301.69
302.21
F 0.52

#2
301.85
302.25
F 0.40

#1
301.46 STAKE ELEV.
302.10 GRADE ELEV. CHECK B.M. 304.18 = 304.18
F 0.64

BC CUMBERLAND 301.83 EXISTING
301.80 EC CAJAL TRES LOMAS

299.42
300.50
F 1.08

BM. DIRECT ELEV. ROD. 304.18 CHISELED SQUARE
NEST CURB
CUMBERLAND & TRES LOMAS

STAKE WEST CURB RETURN
CUMBERLAND & CALLE TRES LOMAS

71

CHECK BM. 304.18 = 304.18

BC CALLE TRES LOMAS

304.80
304.70
C-0.10

#1

304.42 STAKE ELEV.
304.38 GRADE ELEV.
C-0.04

BC CUMBERLAND

304.06 EXISTING
304.06

BM

DIRECT ELEV. ROD

304.18 CHISELED SQUARE WEST CB
CUMBERLAND & CALLE
TRES LOMAS

STAKES N.E. CURB RETURN
CUMBERLAND & CALLE TREPADORA

72

CHECK BM 278.15 = 278.15

EC TREPADORA
294.30
295.10
F 0.80

#3
294.52
295.32
F 0.80

#2
295.68
295.68
GRADE

#1
296.11 STAKE ELEV.
296.02 GRADE ELEV.
C-0.42

BC CUMBERLAND
✓ EXISTING
296.37

BM. DIRECT ELEV. P.D. 278.15 CHISLED SQUARE N.W. CO.
CUMBERLAND &
CALLE SERENA

STATES CURB RETURNS
 CUMBERLAND & CALLE AGUADULCE

S.W. RETURN

SOUTH EAST RETURN

WICK BM. 27815 = 27815

EC, CALLE AGUADULCE
 292.89
 290.50
 C-2.39

292.83
 291.00
 C-1.83

#3
 292.04
 289.72
 C-2.32

291.98
 290.40
 C-1.58

#2
 291.19
 288.90
 C-2.29

291.84
 290.30
 C-1.54

#1
 288.55 STATE ELEV
 288.15 GRADE ELEV
 C 0.40

290.91 STATE ELEV.
 290.45 GRADE ELEV
 C 0.46

BC CUMBERLAND
 287.54 EXISTING STOPS 2' SHORT OF BC
 287.70

290.84 EXIST
 290.80

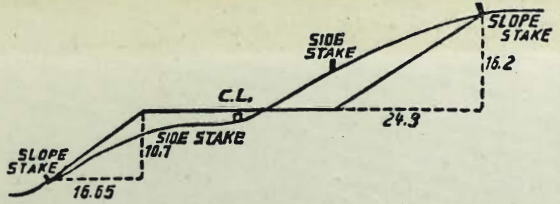
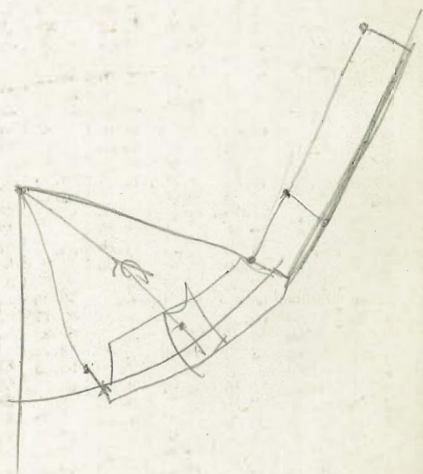
BM. DIRECT ELEV ROD 27815 CHISELED SOURCE N.W. CB.
 CALLE SERENA & CUMBERLAND

The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. Each page is divided into four vertical columns by three red lines. The leftmost column is the narrowest, followed by two wider columns of equal width, and the rightmost column is the narrowest. The pages are otherwise blank, with no handwriting or printed text. The notebook's dark cover is visible at the edges, and the central binding is visible between the two pages.

Africa
 Lt
 6+60 - C.O. 12
 6+80 - C.O. 05
 7+00 - C.O. 22
 7+14 - F.O. 10
 Rt
 7+W - F.O. 11

45909
 11
 944
 564.49
 13.3

8.06



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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