

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 14 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1
If ground is nearly level, the cut or fill at side

IMPROVED TABLES
AND
INFORMATION

To find Tangent and External for curve of
any degree, divide by degree of curve and
add correction found in column of correction.
Degree of curve when given, may be found
by dividing tangent, (or external), by
given tangent, (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

0
1
2
3
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49
50

ST
CO
SH
CU
II

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Bacon - Santa Monica to Newport	
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6 th St. Ivy to Hawthorn	21 ✓ 37 ✓
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Felspar Ingraham to Cass	22-27 ✓
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BK 281

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Bench Marks

✓ U.S. Engrs. South side w. Pt. Lema. in cut	between Abbot + Bridge	city datum 1.51
✓ Voltaire + Abbott.	S. W. B. P.	2.47
✓ Voltaire + West Pt. Lema	N. E. B. P.	1.50

2+4781 bench

2+500

1+500

0+10 15 20 25 30 35 40 45 50 55 60 65 70 75 80 85 90 95 100
 2500 2600 2700 2800 2900 3000 3100 3200 3300 3400 3500 3600 3700 3800 3900 4000

4000 4100 4200 4300 4400 4500 4600 4700 4800 4900 5000
 5100 5200 5300 5400 5500 5600 5700 5800 5900 6000

Existing 300
 0+032

Voltaire St. 24" Drain
Abbot to West Pt. Loria Blvd

Sommermeier
Boggy
Bunch
Wierciszewski

3-1-51
W.O. 20608

8385-L 8390-L
8386-L FB 1818
8387-L FB 1830
8388-L FB 1830
8389-L

C.B. = Catch Basin
C.O. = Clean out

S.W. B.P. Abbot &
Voltaire = 2.47
set self reading rot

INDEXED
RAW
MAY 6 1952

2+00 -4.20
1.73
C-5.93

Endi = Typo "D" - C.B.
3+62.72 -4.04

stub
1+50 -4.25
1.74
C-5.99

3+35.32 -4.07

1+00 -4.30
2.08
C-6.38

3+07.92 = C.O. #19 -4.09
0.92
C-5.01

0+50 -4.35
2.20
C-6.55

3+00 -4.10
1.05
C-5.15

N 7.20 RT

Nail 5' RT
0+06 -4.39
2.34
C-6.73

2+50 -4.15
1.52
C-5.67

= 0+00 Voltaire
11+04.97 Bacon St. -4.40

Abbott St. Drain

From San Diego River floodway to Muir Ave.

INDEXED
Lull

MAY 6 1952

Sommermeier
B 099
Bunch
Wierciszewski

C.O. = Clean out.

0+50
-6.42
0.30
C-6.72

0+34.46 = E.C.
-6.45
-0.67
C-5.78

0.16376

0+19.45 = B.C. RT
A=40° R=21.5'
-6.48
+4.75
C-1.73

0+10.21 = E.C.O.#13
-6.50

C.O.#13
0+08.13 Existing 48°
-6.50

C.O.#1A
2+61.75 = A
A=12.13' RT.
-6.09
2.72
C-8.81

15' RT

2+59.49 = E.C.
-6.10
2.72
C-8.82

2+47.71 = B.C. RT.
A=15° R=45'
-6.12
2.73
C-8.85

11.15' RT

D-15' L + RT
-6.12
2.68
C-8.80

2+00
-6.18
1.96
C-8.14

15' RT

1+50
-6.26
1.62
C-7.88

0.16376

1+00
-6.34
0.66
C-7.00

15' RT

Abbott St.

5

✓

4+79.25 = C.O.#15

-5.65

$\square 10'N$ $\triangle 10'S$
 -5.65 -5.65
 $\frac{1.30}{C 6.95}$ $\frac{1.80}{C 7.45}$

6+04.43

-5.38

0.25
 $\frac{0.25}{7.63}$

4+50

-5.72

$\frac{0.24}{C 5.96}$

5+80.82

-5.43

$\frac{2.30}{C 7.73}$

4-Parts
 100' R. - ch = 26.10
 R.A. = 7°30'

4+00

-5.82

$\frac{2.08}{C 7.90}$

Nail 12³ RT.

5+57.26 = B.C.

-5.49

$\frac{1.97}{C 7.46}$

$\Delta = 60^\circ$ R = 90°

0.290

↑

3+59.65 = Std. Lug.

-5.90

$\frac{1.41}{C 7.31}$

5+50

-5.50

$\frac{1.76}{C 7.26}$

3+26.48 = E.C.

-5.96

$\frac{1.60}{C 7.56}$

5+00

-5.60

$\frac{1.45}{C 7.05}$

3+07.72 = B.C. RT.

-6.00

$\frac{1.66}{C 7.66}$

$\Delta = 50^\circ$ R = 21.5'

4+80.64

-5.64

$\Delta 10-54' LT.$

$\frac{0.60}{C 6.24}$

↑
 11.51
 □
 10 N

↑
 10.01
 □
 10 N
 ↓

Abbott St

✓

✓ 6

8+49.77 = C.O.#16

$$\begin{array}{r} -4.91 \\ \underline{1.79} \\ C-6.70 \end{array}$$

11+04.97 = C.O.#17

$$\begin{array}{r} -4.40 \\ \times \end{array}$$

8+00

$$\begin{array}{r} -5.00 \\ \underline{1.97} \\ C-6.97 \end{array}$$

11+00

$$\begin{array}{r} -4.41 \\ \underline{2.38} \\ C-6.79 \end{array}$$

7+50

$$\begin{array}{r} -5.10 \\ \underline{2.10} \\ C-7.20 \end{array}$$

10+50

$$\begin{array}{r} -4.51 \\ \underline{2.22} \\ C-6.73 \end{array}$$

0.270

7+00

$$\begin{array}{r} -5.20 \\ \underline{2.39} \\ C-7.59 \end{array}$$

10+00

$$\begin{array}{r} -4.61 \\ \underline{2.08} \\ C-6.69 \end{array}$$

0.270

6+51.51 = E.C.

$$\begin{array}{r} 6' \text{ off} \\ -5.29 \\ \underline{2.34} \\ C-7.63 \end{array}$$

$$\begin{array}{r} 10' \text{ off} \\ -5.29 \\ \underline{2.39} \\ C-7.68 \end{array}$$

$$\begin{array}{r} 2.39 \text{ Rod} \\ 3.22 \\ \underline{5.61} \\ 1.00 \end{array}$$

$$\begin{array}{r} -5.39 \text{ Top of } 6'' \\ \text{Pipe at} \\ \text{Pump base} \end{array}$$

9+50

$$\begin{array}{r} -4.71 \\ \underline{2.01} \\ C-6.72 \end{array}$$

6+27.94

$$\begin{array}{r} -5.33 \\ \underline{2.25} \\ C-7.58 \end{array}$$

$$\begin{array}{r} 5.61 \text{ #1} \\ \underline{8.06} \\ -2.45 \text{ Top of } 3' \\ \text{cshcl Pipe} \end{array}$$

9+00

$$\begin{array}{r} -4.81 \\ \underline{1.91} \\ C-6.72 \end{array}$$

Abbott st.

Cb. Abbott + Newport.

7

13+50
 -3.90
 1.79
 C-5.69

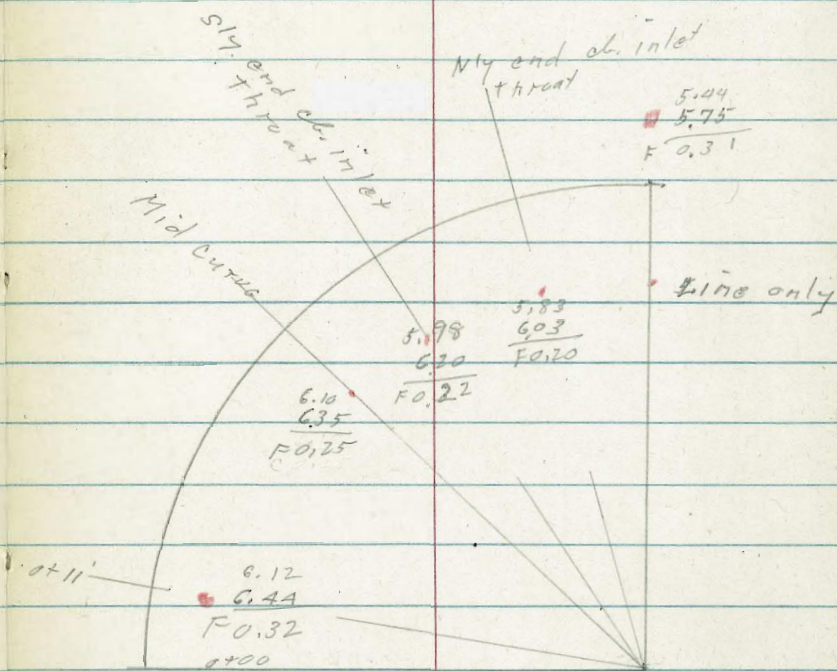
13+00
 -4.00
 2.03
 C-6.03

12+50
 -4.10
 2.03
 C-6.14

12+00
 0.270
 -4.20
 2.14
 C-6.34

11+50
 -4.30
 2.36
 C-6.66

11+10
 -4.39
 2.66
 C-7.05



of pipe.
 +line - Past end
 13+90 = Grad. 3.83
 1.64
 C-5.47

End of pipe
 13+80.93 = C.O.#18 -3.85
 1.67
 C-5.52

0.270

INDEXED
 Law
 MAY 6 1952

INDEXED
MAY 6 1952

Bacon street
storm drain
for Ref.
See page 3

S.D. River Floodway to Muir Ave.

Sommermeier
Begg
Bunch
wierciszewski.

3/1/51
W.O. 20508

3+50
1.65
-6.27
C. 7.92

C.O. = Clean out
C.I. = curb. inlet

3+00
1.94
-6.30
C. 8.24

0+86.73 = E.C.
1.47
-6.45
C. 7.92

2+50
1.80
-6.34
C. 8.14

0+71.55 Mid Curve
~~-6.46~~

2+00
1.92
-6.37
C. 8.29

0+56.36 = B.C. Lt.
-0.35
-6.47
C. 6.12
Δ 20° R = 87°

1+50
1.88
-6.41
C. 8.29

Existing Co.
0+18.79:
-6.54
-6.50
F 0104

1+00
1.57
-6.44
C. 8.01

0.072/96

Bacon

	15' RT.	10' RT
5+34.8A = E.C.	5.49	5.10
	-6.13	-6.13
	<u>C-11.61</u>	<u>C-11.23</u>

5+10.17	4.99
	-6.1A
	<u>C-11.13</u>

A+85.50	3.52
	-6.16
	<u>C-9.68</u>

A+60.82	2.59
	-6.18
	<u>C-8.77</u>

A+36.1A = B.C.	1.59
Δ 65° - A = 87'	-6.20
	<u>C-7.79</u>

A+00	2.18
	-6.23
	<u>C-8.41</u>

Bacon

9

7+50	6.42
	-5.97
	<u>C-12.39</u>

7+00	6.10
	-6.01
	<u>C-12.11</u>

6+56.91 = C.O.*1	10' RT.
Wast. Pt. Loma	6.28
	-6.04
	<u>C-12.32</u>

6+50	-6.05
------	------------------

6+00	5.77
	-6.09
	<u>C-11.86</u>

5+50	5.22
	-6.12
	<u>C-11.34</u>

Bacon

Bacon

10

10+00

8.10
<u>-5.98</u>
C-13.88

12+50

8.78
<u>-5.60</u>
C-14.38

Δ 0°-A1' Lt.
= 9+68.95
9+72.12 Back

7.94
<u>-5.81</u>
C-13.75

12+10.74

8.73
<u>-5.62</u>
C-14.35

12+55.10
Voltaire st.
12+05.74 - C.0.02 -5.63

9+37.25 Std. Luq.
Lotus

7.46
<u>-5.84</u>
C-13.30

12+00.74

8.42
<u>-5.63</u>
C-14.05

9+00

7.25
<u>-5.86</u>
C-13.11

11+50

8.89
<u>-5.67</u>
C-14.56

8+50

7.00
<u>-5.90</u>
C-12.90

11+00

8.72
<u>-5.71</u>
C-14.43

8+00

6.69
<u>-5.93</u>
C-12.62

10+50

8.25
<u>-5.75</u>
C-14.00

Bacon

15+50
 $\begin{array}{r} 6.87 \\ -5.37 \\ \hline C-12.24 \end{array}$

15+31.27 -5.39 out

15+26.57 = C.D.#3 $\Delta = 0^{\circ} 39' 44''$
 Muir Ave
 $\begin{array}{r} 6.52 \\ -5.39 \\ \hline C-11.91 \end{array}$

14+97
 $\begin{array}{r} 6.85 \\ -5.40 \\ \hline C-12.25 \end{array}$

14+47
 $\begin{array}{r} 7.72 \\ -5.45 \\ \hline C-13.17 \end{array}$

13+99
 $\begin{array}{r} 8.08 \\ -5.49 \\ \hline C-13.57 \end{array}$

13+47
 $\begin{array}{r} 8.37 \\ -5.53 \\ \hline C-13.92 \end{array}$

13+00
 $\begin{array}{r} 8.33 \\ -5.56 \\ \hline C-13.89 \end{array}$

Bacon

11

18+50
 $\begin{array}{r} 5.19 \\ -5.14 \\ \hline C-10.33 \end{array}$

18+00
 $\begin{array}{r} 5.45 \\ -5.18 \\ \hline C-10.63 \end{array}$

17

17+91# = Δ x C.D.#4 -5.19 not set.
 $\Delta = 0^{\circ} 39' 18''$
 Long branch
 $\begin{array}{r} 4.97 \\ -5.19 \\ \hline C-10.16 \end{array}$

17+50
 $\begin{array}{r} 5.45 \\ -5.22 \\ \hline C-10.67 \end{array}$

17+00
 $\begin{array}{r} 5.62 \text{ TR} \\ -5.25 \\ \hline C-10.87 \end{array}$

16+50
 $\begin{array}{r} 5.84 \\ -5.30 \\ \hline C-11.14 \end{array}$

16+00
 $\begin{array}{r} 5.96 \\ -5.34 \\ \hline C-11.30 \end{array}$

Bacon

Bacon

21+50
 5.32
 -4.90
 C-10.22

24+48²⁷ A RX
 6.44
 -4.09
 C-10.53

21+00 ^{0.10}
 5.05
 -4.95
 C-10.00
 4.93
 -4.98
 C-9.91

24+29.66 = C.O.#7
 5.8A
 -4.19
 Cape May C-10.03
 Not Painted

20+65 = C.O.#6
 4.15
 -4.98
 C-9.13

24+00
 5.67
 -4.29
 C-9.96

Brighton
 +33.25
 3.65
 -5.00
 C 8.65

20+28.25 = C.O.#5
 -5.01
 2.43
 -5.01
 C 9.44

23+50
 5.92
 -4.46
 C-10.38
 0.342

20+00
 4.50
 -5.03
 C-9.53

23+00
 5.55
 -4.63
 C-10.18

19+50
 4.68
 -5.07
 C-9.75

22+50
 5.24 - T.P.
 -4.80
 C-10.04

19+00 ^{0.0196}
 4.97
 -5.10
 C-10.17

22+00
 5.56
 -4.85
 C-10.41

Bacon

$\Delta 0^{\circ} 54' 30''$ Lt.

27+62.39

7.52
-3.05
C 10.57

0.05 error here

27+50

-3.08

27+00

x 7.28
-3.24
C 10.52

26+50

0.34%
105 RX

□ 7.20
-3.40
C 10.60

26+00

6.53
-3.57
C 10.10

25+50

□ 6.73
-3.74
C 10.47

25+00

□ 6.65
-3.91
C 10.56

Bacon

30+50

-2.08
8.34
C 10.42

30+00

-2.25
8.12
C 10.37

29+50

-2.42
7.97
C 10.39

29+00

-2.59
7.84
C 10.43

28+50

0.34%

-2.76
7.66
C 10.42

28+00

-2.93
7.37
C 10.30

27+70²⁸ = C.O.²⁸ 8
Saratoga

6.96
-3.03
~~6.96~~
C 9.99

SE. 7' Lt.
Saratoga +
Bacon.
= 8.18

Bacon

33+50

$$\begin{array}{r} -1.06 \\ \underline{9.64} \\ C-10.70 \end{array}$$

S.W. L & T 7'
Santa Monica &
Bacon.

EL. = 9.08

33+00

$$\begin{array}{r} -1.23 \\ \underline{9.38} \\ C-10.61 \end{array}$$

Tied Left.
35+71 = std. Ldg.
 $\begin{array}{r} +1.59 \\ \underline{11.44} \\ C-9.85 \end{array}$

35+55.78 = B.C.
 $\Delta = 90 - R = 22$
 $\begin{array}{r} +1.44 \\ \underline{11.25} \\ C-9.85 \end{array}$

32+50

$$\begin{array}{r} -1.40 \\ \underline{9.12} \\ C-10.52 \end{array}$$

35+26.87 = Std. Ldg.
Newport
 $\begin{array}{r} +1.04 \\ \underline{10.35} \\ C-9.31 \end{array}$

35+21.87
 $\begin{array}{r} +0.97 \\ \underline{10.48} \\ C-9.51 \end{array}$

32+00

$$\begin{array}{r} -1.57 \\ \underline{8.44} \\ C-10.01 \end{array}$$

35+00
 $\begin{array}{r} +0.70 \\ \underline{10.35} \\ C-9.65 \end{array}$

0.34%

1.25%

31+50

~~$$\begin{array}{r} -1.74 \end{array}$$~~

34+50
 $\begin{array}{r} +0.07 \\ \underline{10.10} \\ C-10.03 \end{array}$

31+46.77 = Std. Ldg.
Santa Monica

$$\begin{array}{r} -1.75 \\ \underline{8.27} \\ C-10.02 \end{array}$$

34+00
 $\begin{array}{r} -0.55 \\ \underline{9.88} \\ C-10.43 \end{array}$

31+00

$$\begin{array}{r} -1.91 \\ \underline{8.54} \\ C-10.45 \end{array}$$

33+64.7A = C.O.#9
Alley
33+58.7A
 $\begin{array}{r} -1.01 \\ -1.03 \\ \underline{9.28} \\ C-10.31 \end{array}$

Bacon

14

Bacon

15

End. of Const

$36 + 26.88$

$\begin{array}{r} 12.04 \\ + 6.87 \\ \hline C-5.17 \end{array}$

$36 + 00.62 = C.D. \#10$

$\begin{array}{r} 11.80 \\ + 1.94 \\ \hline C-9.86 \end{array}$

$95 + 90.36 = E.C.$

$\begin{array}{r} + 1.83 \\ 11.50 \\ \hline C-9.67 \end{array}$

Drain in Alley BIK. 73 a.B.

1+50

8.79
-0.74
C-9.53

1+00

0.1874

9.08
-0.83
C-9.91

0+50

9.38
-0.92
C-10.30

0+06

9.28
-1.01
C-10.29

=0+00

-1.01

33+64.74 P/A

4+50

6.74
-0.20
C-6.94

4+00

7.04
-0.29
C-7.33

3+50

7.37
-0.38
C-7.75

3+00

7.71
-0.47
C-8.18

2+50

8.09
-0.56
C-8.64

2+00

8.38
-0.65
C-9.03

INDEXED
Laid
MAY 6 1952

Alley Bk. 73 O.B.
+ Abbott to south

17

6.43 P.M.

6+45.57 #1

7+84.64 B.C.
7+98-B.C.
 $\Delta 40^\circ R=22$

5.17
1.75
C-3.42

E. 25' N.P. X'
TO N.E. 7' L + T
Newport + Abbott

~~6.65~~

= 6.72

B.M.P. 12

6+28.29 = B.C. Lt
Line to south
 $\Delta = 90^\circ - A = 44'$

+0.12

7+50

5.01
1.38
C-3.63

6+26.29 = C.O. #11

5.25
+0.12
C-5.13

7+00

6+00

5.87
+0.07
C-5.80

6+97.41 = E.C.

4.98
0.83
C-4.15

5+50

6.11
-0.02
C-6.13

6+80.13 #3

5+00

6.45
-0.11
C-6.36

6+62.85 #2

5

Abbott to South
from alley BIK. 73 O.B.

= End of line

8+20.08
8+18=GI.#21

4.95
+2.53
C- 2.42

8+00
8+15³⁰=E.C.

5.56
2.10
C- 3.46

18

Abbott to North
from alley BIK. 73 O.B.

7+00

6+97.41=E.C. 4.77
 0.32
C- 4.45

6+80.33

6+62.85**

6+45.57*1

6+28.29=B.C.RX +0.12
 $\Delta=90^\circ, R=44'$
From P.17

Drain

West Pt. Loma Blvd. - Bacon East.

INDEXED
MAY 6 1952
Law

20

End of line
2+88.9 = &I.#23

+0.67

= sta. 236.10

Curb. inlet

Existing.

From here to

+0.50

Existing culvert

∅ existing M.H.

0+88.89

-1.95

0+51.53 = E.C.

0+28.23 = B.C.

Δ 30° - R = 44.5

= 0+00

-3.46

6+56.91 P7

Sommernoyor
Boag
R. Sisson
Ottman

6th St. Hawthorn to Ivy

Indexed

(0.8' west Face of wall)

Cut stakes to
cl. grade.

15 May '51

N.O. 20743

N.W. B.P. 5th
+ Hawthorn

sly. Ivy.
3+00

22.20
218.30
C-3.90

198.47
3.87
202.34
2.99

2+84 ob. B.C.

21.99
217.48
C-4.51

199.33
S.W. 7' L+T
6th + Hawthorn.

2+50

X-9'
22.13
215.75
C-6.38

30' west of E.C.
E end of project
221.45

2 ~

8.30
213.20
C-5.10

1+50

0.51 Rate

16.54
210.65
C-5.89

1 ~

15.40
208.10
C-7.36

15' west
of E.C.
21.59
211.45
C-0.27

0+50

13.60
205.55
C-8.05

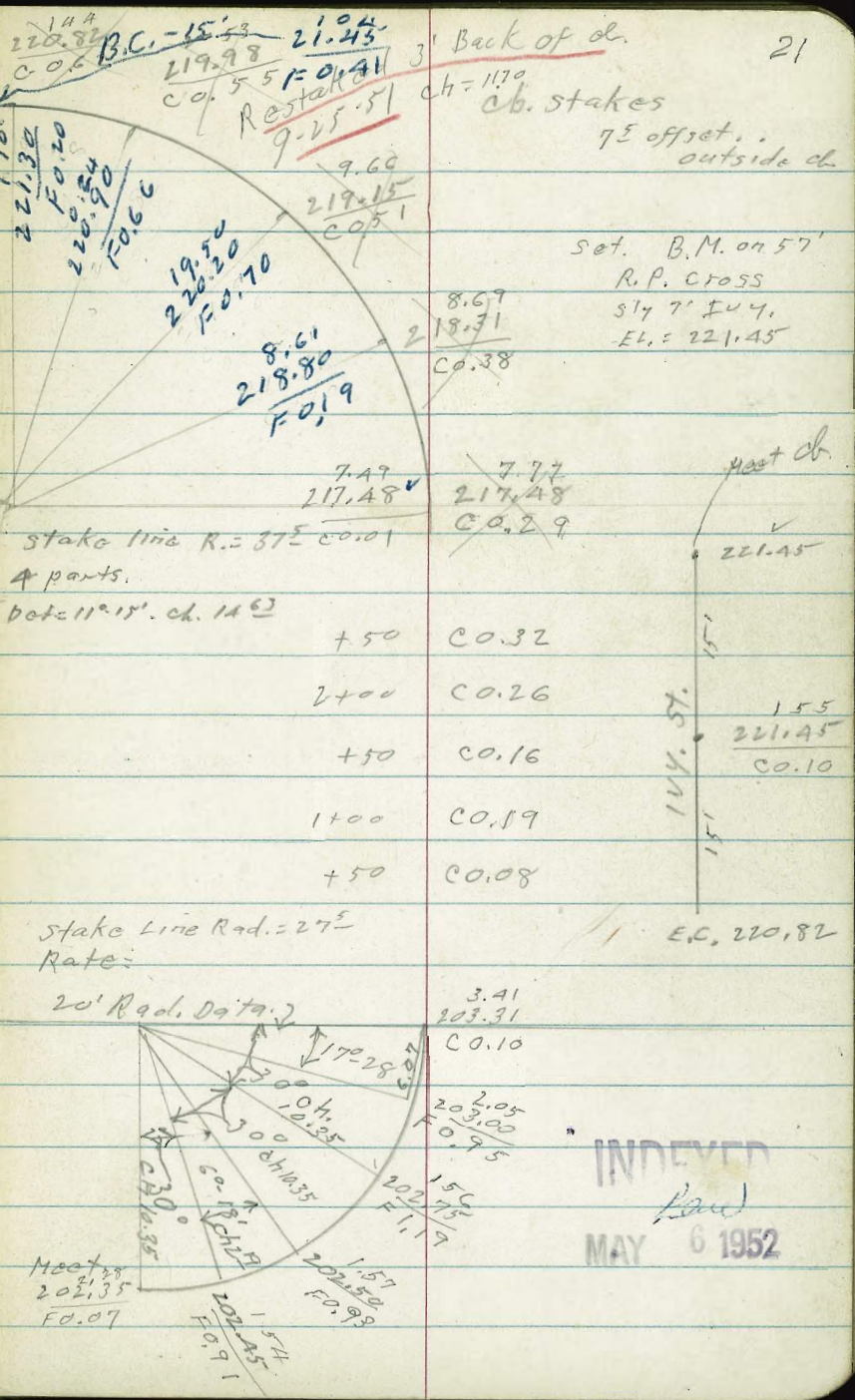
0+06 ob. E.C.

12.30
203.31
C-9.05

ob. E.C.
on 10' W
21.95
220.82
C-1.10

1/4 Hawthorn
0+00

203.00



INDEXED
LAW
MAY 6 1952

Felspar
Ingraham to Carr

12-June '51

100' slt 1/2 R.P. to S. wly. 7' Mon.
Felspar + Haine ELZ 71.17

22

Sommermejer

Beqq

Shepard

oltman

Direct Elevation

Rough
Gr

Rough
Gr

	Rough Gr.			Rough Grade	20' Lt. = Ob. E.C.					
					0+60	2.43 69.59 C 2.84				7.26 70.08 C 2.18
					0+10	71.65 69.93 C 1.72	9.34 69.93			
2+50	N. 0.3 71.20 68.91 C 2.29	C 0.56	C 0.12	70.92 69.22 C 1.70	Wly. Haines 0+00	1.51 69.99 C 1.52	S. End S. W. of R. & L. End. ob.	9.84 70.48 F 0.64	1.64 70.48 C 1.16	
2+00	7.82 68.59 C 1.23	C 0.58	C 0.03	71.14 68.96 C 2.18	Haines			F 0.56 ob.		
1+50	9.70 68.27 C 1.43	C 0.58	Obd.	71.20 68.69 C 2.51	Ely. Haines 5+00	0.19 70.49 F 0.31	S. End ob. S. E. ob. Ret.	9.92 70.50 F 0.58	0.98 70.50 C 0.48	
1+00	9.95 67.95 C 2.00	C 0.45	F 0.23	71.33 68.43 C 2.90	Ob. B.C. 4+90	70.00 70.44 F 0.44				
0+50	9.63 67.63 C 2.00	C 0.51	F 0.25	8.78 68.16 C 0.60	A+50	9.69 70.19 F 0.50	F 0.34	F 0.42	0.71 70.28 C 10.43	
20' Lt. = Ob. E.C. 0+14 ²⁵				9.10 67.90 C 1.20	A+00	9.64 69.87 F 0.23	C 0.05	F 0.50	0.74 70.02 C 0.72	
20' Lt. = Ob. E.C. 0+10	8.74 67.37 C 1.07				3+50	7.82 67.55 C 0.27	C 0.06	F 0.33	0.54 69.75 C 0.79	
Wly Ingraham 0+00	67.00	(Sly end ob. N.W. and S.W. ob. N.W. ob.)		68.05	3+00	9.88 69.23 C 0.65	C 0.37	F 0.14	0.64 69.49 C 1.15	

INDEXED
MAY 6 1952

Ingraham

5108

4.55

Felspar

451

5.30

4.30.01

23

	Rough Gr.	3780	Fo.01	Rough Gr.		Rough Gr.	1		Rough Gr.
3450	5.10 64.35 C 0.75	3740 Fo.12	Fo.01	6.47 64.85 C-1.02	1700	5.03 55.33 Fo.30	1415 C 0.02	C 0.10	6.77 56.33 C 0.44
E.V.C. 3400	6.88 66.46 C 0.42	6.42 66.46 Fo.04	6.72 66.96 Fo.124	7.35 66.96 C 0.39	0750	5.99 56.16 Fo.17	0480 Fo.21	C 0.10	7.38 57.16 C 0.22
2780	7.76 67.26 C 0.50	7.20 67.26 Fo.06	7.37 67.76 Fo.39	7.35 67.76 Fo.41	0710	6.05 56.82 Fo.77	56.82 Fo.31	57.82	7.76 57.82 Fo.06
2760	8.75 67.87 C 0.88	7.98 67.87 C 0.11	7.73 68.37 Fo.64	7.62 68.37 Fo.75	0700	6.19 57.01 Fo.82	slightly end S. wly. cl.	Nly. end N. wly. cl.	7.92 58.30 Fo.48
2740	9.27 68.29 C 0.98	7.80 68.29 Fo.49	8.37 68.79 Fo.42	7.98 68.79 Fo.81	Oriskany	5.30			
E.V.C. 2720	9.54 68.52 C-1.02	8.18 68.52 Fo.34	8.60 69.02 Fo.42	8.34 69.02 Fo.68	5700	8.55 57.50 C 1.05	slightly end S. Ely. cl.	Nly. end N. Ely. cl.	60.16 58.74 C-1.42
1790	1.27 68.72 C-2.55	Fo.21	2500 Fo.25 1760 Fo.12	8.93 69.22 Fo.29	W. B.C. A790	965 58.45 C 0.20	8.71 58.45 C 0.26	9.07 58.95 C 0.12	187 58.95 C-2.92
B.K. 1760	1.49 68.92 C-2.57	C 0.07	1720 Fo.15	2.01 69.42 C-2.59	A750	970 60.13 Fo.43	A 755 C 0.15	Fo.20	3.55 60.63 C-2.92
1710	2.14 69.25 C-2.89	Fo.55	0780 C 0.07	2.14 69.75 C-2.39	A700	267 62.24 C 0.43	A720 Fo.08	Fo.22	5.26 62.74 C-2.52

Fanuel	Felspar Rough grade	5.14	5.19	Rough Grade		5.85 Rod.	Rod 4.92 .35 1.7		2.4
5+20									N.W. 7'4". Felspar + Fanuel 2.108 8 EL=51.21
					Rough Gr			Rough grade	
ELY. Fanuel 5+00	1.04 51.00	51.00	52.00	1.89 52.00	3+00 BK	TR 8.84 47.78		0.24 48.28	
	C 0.04	4+90 C 0.19	C 0.05	F 0.13		C 1.06	4+45 F 0.15	C 0.07	C-1.96
4+50	1.62 51.47	4+50 C 0.13	C 0.19	3.39 52.47	2+50	9.16 48.22	4+00 C 0.15	C 0.17	51.08 48.73
	C 0.15	4+10 C 0.02	F 0.11	C 0.92		C 0.94	3+50 C 0.45	C 0.10	C-2.35
4+00	1.58 51.94			3.49 52.94	2+00	9.33 49.66	3+20 C 0.40	C 0.17	1.11 49.17
	F 0.36	3+70 C 0.04	F 0.11	C 0.55		C 0.67	2+80 C 0.17	C 0.07	C-1.94
3+50	2.25 52.41			53.62 ^{TR} 53.41	1+50	9.52 49.19	2+40 C 0.02	C 0.02	1.28 49.62
	F 0.16	3+30 F 0.15	F 0.03	C 0.21		C 0.42	2+00 C 0.11	C 0.17	C-1.66
3+00	2.73 52.88			4.19 53.88	1+00	50.03 49.54	1+60 F 0.20	F 0.05	1.66 50.06
	F 0.15	2+90 C 0.11	F 0.16	C 0.31		C 0.49	1+20 F 0.15	F 0.33	C 1.60
2+50	3.05 53.35	2+50 F 0.12	Grade	4.41 54.35	0+50	1.31 49.98	0+80 F 0.20	F 0.33	2.17 50.51
	F 0.30	"		C 0.06		C-1.33	0+40 F 0.50	F 0.43	C-1.66
2+10 BK	3.68 53.72	3.84 53.72	4.78 54.72	5.14 54.72	0+10 BK	50.75 50.33	50.00 50.33	-	-
	F 0.04	C 0.12	C 0.06	C 0.42		C 0.42	F 0.33		
1+80 BK	4.48 54.06	4.27 54.06	5.29 55.06	5.57 55.06	wly. Fanuel 0+00	50.41			50.95
	C 0.42	C 0.21	C 0.23	C 0.51	0				
1+50 BK	4.53 54.50	4.70 54.50	5.77 55.50	6.19 55.50					
	C 0.03	C 0.10	C 0.27	C 0.69					

no Everts } not in this contract.
Fanuel }

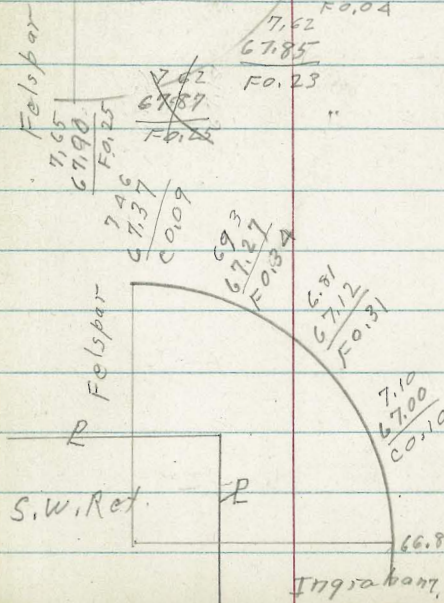
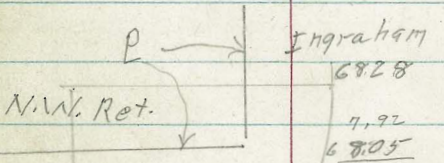
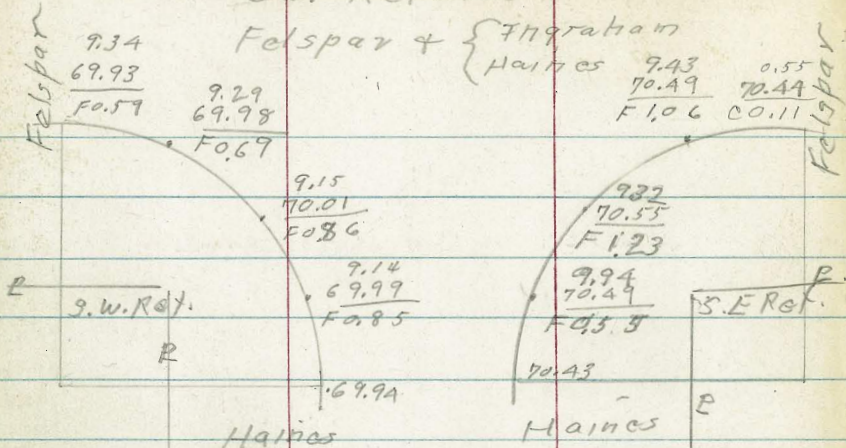
Felspar

Ely Cass
4+99²⁵Rough
33.05Rough
34.03

25

				4+79 ²⁵	3.58 33.23	4.80 34.19
					C 0.35	C 0.61
0+10	7.51 37.41		8.95 37.92	A+50	3.50 33.50	5.15 34.42
52' Roadway	C 0.10		C 1.03		X	C 0.73
Wly Dawes 0+00	see Dawes	Nly. end N.W. of 5' back	9.07 38.49	A+00	4.20 33.95	5.77 34.82
			C 0.58		C 0.25	C 0.95
				3+50	4.93 34.40	6.24 ^a 35.22
					C 0.53	C 1.02
<u>Dawes</u> <u>Events to</u>	Not part of this contract.			3+00	5.00 34.85	6.51 35.62
Events					C 0.15	C 0.89
	see Events at			2+50	4.74 35.30	7.07 36.02
					F 0.56	C 1.05
Ob. B.C. A+90	6.64 46.08		8.09 46.59	2+00	5.55 35.75	7.37 T.P. 36.42
	C 0.56		C 1.50		F 0.20	C 0.95
A+50	7.15 46.43		8.35 46.95	1+50	6.13 36.15	7.69 36.82
	C 0.72		C 1.40		F 0.02	C 0.87
A+00	8.00 46.87	4+45 F 0.11	9.16 47.39	1+00	6.83 36.60	8.31 37.22
	C 1.13		C 1.77		C 0.23	C 1.09
3+50	8.35 47.34	4+50 C 0.29	9.93 47.84	0+50	7.00 37.05	8.73 37.62
	C 1.01		C 2.09		F 0.05	C 1.11

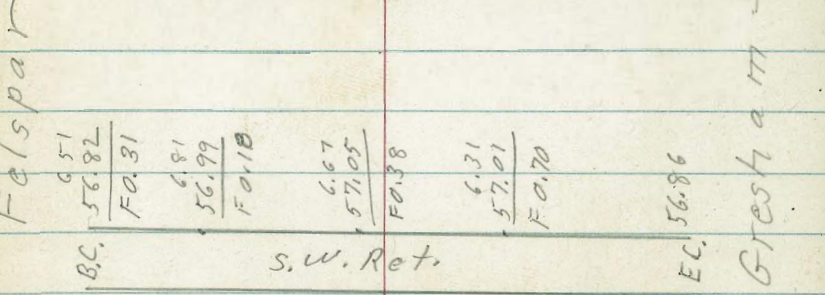
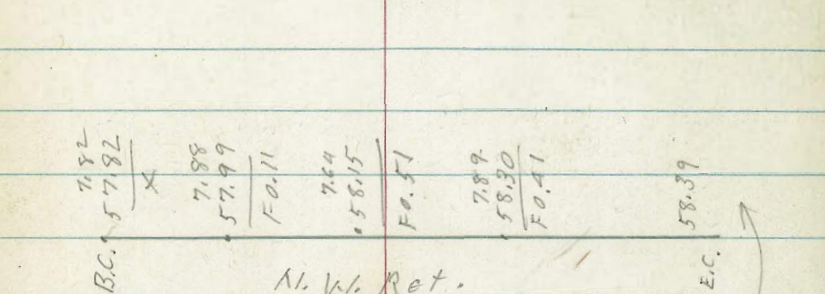
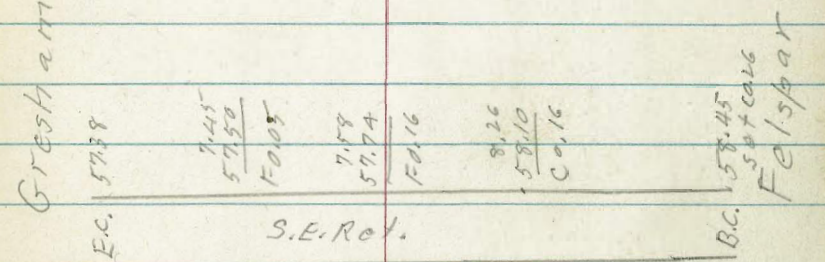
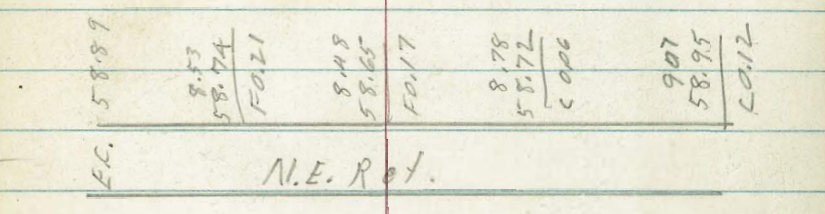
Cb. Returns



Cross & Felspar
& Ingraham
EL. = 67.46

100 sq Mon. R.P.
Felspar & Haines
EL. = 71.17

Curb Ret. + Gutters
Gresham + Felspar 26
6/25/51
g. fixed



See met page

Curb Returns
Dawes + Felspar

DAWES
Garnet to Felspar

DAWES	EC 39.24	0.41 39.07 39.07 C 1.34	0.25 39.00 C 1.25	0.04 39.01 39.01 C 0.99	B.C. 39.14
7.93 37.58 C 0.34	8.13 37.72 C 0.41	8.19 37.89 C 0.30	9.05 38.00 C 1.05	9.05 38.00 C 1.05	FELSPAR
EC	R	S.E. Ret.	R	B.C.	
7.73 37.92 F 0.19	7.88 38.10 F 0.22	8.01 38.49 F 0.48	9.14 38.70 C 0.44	38.88	
B.C.	R	N.W. Ret.	R	EC	
7.17 37.88 F 0.21	7.36 37.26 C 0.10	7.07 37.12 F 0.05	36.98 F 0.04		DAWES
B.C.	R	S.W. Ret.	PL	EC	

	Rough or		Rough or	
2+60 Rt.	—	2+25	2+25	8.90 37.58 C 1.32
B.C.	7.25	B.C.	1+90	
2+54 Lt.	36.98	2+25	C 0.22	—
C 0.27	C 0.03			
2+25	6.96 36.50	1+49	8.98 37.00	
	C 0.46	F 0.17	C 1.98	
1+85	6.38 35.82	1+90 C 0.03	7.83 36.32	C 0.27 Curb end
	C 0.56	1+49 C 0.12	C 1.51	C 0.45 eb end
1+45	5.42 35.14	1+21	6.88 35.64	
Curb 0.14 end C 0.14	C 0.28	C 0.11	C 1.24	
1+25	5.31 34.81	+80 F 0.16	6.65 35.31	
	C 0.50	G	C 1.34	
0+80	4.50 34.06	F 0.24	5.72 34.56	
	C 0.44	0+40 F 0.05	C 1.16	
0+30	3.52 33.21	0.40 C 0.34	5.10 33.71	
	C 0.31	C 0.34	C 1.39	
Nly. Garnet 0+00	32.70		33.57	

FELSPAR & EVERTS

Curb returns

8322-L

Nail in S.W. Pole = 46.57

EVERTS

EC 6.90
46.72
CO.18

E 6.51
46.60
FO.09

N. E. Cor.

6.43
46.54
FO.11

E 6.44
46.57
FO.13

BC 6.56
46.59
FO.03

FELSPAR

BC 45.33

E 6.09
45.97
CO.52

S. E. Cor.

6.20
45.78
CO.42

E 6.73
46.00
CO.73

BC 6.83
46.08
CO.85

FELSPAR ST

BC 45.86

E 6.00
45.97
CO.03

N. W. Cor.

6.41
46.20
CO.21

E 6.56
46.50
CO.06

EC 6.70
46.70
X

EVERTS ST.

BC 44.86

E 5.17
45.00
CO.17

S. W. Cor.

5.16
45.07
CO.09

E 5.08
44.95
CO.18

EC 44.80

EVERTS ST.

EC 4.58
54.88
CO.20

E 4.40
54.19
CO.21

R 4.04
54.00
CO.04

R 3.57
53.75
FO.16

5.17
5.47
45.27

E 3.81
53.52
FO.21

BC 3.05
53.94
FO.19

EMERALD ST

EC 4.91
54.74
CO.17

E 4.63
54.55
CO.08

R 4.34
54.45
FO.11

E 4.51
54.47
CO.04

BC 54.52

BC 2.19
52.85
FO.06

E 2.85
52.37
FO.02

R 2.11
52.20
FO.09

E 1.99
51.97
CO.02

R 1.97
51.81
CO.16

EC 1.74
51.73
CO.01

EMERALD ST.

BC 53.52

E 3.58
53.30
CO.25

R 2.82
52.95
FO.13

E 2.61
52.82
CO.11

EC 2.35
52.28
CO.07

BC 3.14
53.30
FO.16

S. E. Cor.

R 2.61
52.82
CO.11

EC 2.35
52.28
CO.07

BC 52.85

E 3.14
53.30
FO.16

R 2.11
52.20
FO.09

E 1.99
51.97
CO.02

R 1.97
51.81
CO.16

EC 1.74
51.73
CO.01

EC 54.74

E 54.55

R 54.45

E 54.47

BC 54.52

EC 54.88

E 54.19

R 54.00

R 53.75

5.17
5.47
45.27

E 53.52

BC 53.94

EC 54.88

E 54.19

R 54.00

R 53.75

5.17
5.47
45.27

E 53.52

BC 53.94

EC 54.88

E 54.19

R 54.00

R 53.75

5.17
5.47
45.27

E 53.52

BC 53.94

EC 54.88

E 54.19

R 54.00

R 53.75

5.17
5.47
45.27

E 53.52

BC 53.94

EC 54.88

E 54.19

R 54.00

R 53.75

5.17
5.47
45.27

E 53.52

BC 53.94

INDEXED

Law

MAY 6 1952

EMERALD street

3-July-'51

5.03

INDEXED 45.08 29
 MAY 6 1952
 B.M. #3 $\frac{2108}{10}$
 53.26

Rough Gr.	Curbs	Rough Gr.
-----------	-------	-----------

N.E. Cor. L+T
 N. 7' Emerald
 E. 203' Everts

EL. = 54.65

S.W. L+T (7') Dawes + Emerald EL. = 45.08

3+50	8.10 47.60 C 0.50	4+90	9.31 48.25 C 1.06
------	-------------------------	------	-------------------------

3+00	8.77 48.30 C 0.47	4+50 C 0.10	F 0.05 0.13 49.00 C 1.13
------	-------------------------	----------------	-----------------------------------

2+50	0.01 49.00 C 1.01	3+70 C 0.12	C 0.29 1.34 49.75 C 0.59
------	-------------------------	----------------	-----------------------------------

2+00	0.48 49.70 C 0.78	2+90 C 0.30	C 0.30 2.31 50.50 C 1.81
------	-------------------------	----------------	-----------------------------------

1+50	0.91 50.40 C 0.50	2+10 C 0.22	C 0.68 3.34 51.25 C 2.09
------	-------------------------	----------------	-----------------------------------

1+00	1.23 51.10 C 0.13	1+30 C 0.69	C 0.30 3.88 52.00 C 1.88
------	-------------------------	----------------	-----------------------------------

0+50	1.64 51.80 F 0.16	0+50 C 0.14	F 0.04 3.91 52.75 C 1.16
------	-------------------------	----------------	-----------------------------------

0+10 N.E.C.	2.05 52.35 F 0.30	52.35	53.34 4.45 3.45 53.34 C 4.11
-------------	-------------------------	-------	--

wly. Everts
 0+00

Rough Gr.

Rough Gr.

Ely. Dawes
 5+00

Ch. B.C.
 4+90

4+50

4+00

6.05	5.57	6.15	7.32
45.64	45.64	46.15	46.15
C 0.41	F 0.07	x	C 1.17

6.44			8.45
46.20			46.75
C 0.24			C 1.70

6.85			8.60
46.70			47.50
F 0.05			C 1.10

EVERETS ST.
Felspar to Diamond

5.14
5.02 FO.23

INDEXED
Raw

5.30

5.26

30

MAY 6 1952

Rough

Rough

Rough

Rough

				0+90	6.64 56.16 C0.48	0+80 C0.137	Grade	7.18 56.66 C0.52
2+25	1.60 51.14 C0.46	2+20 FO.38	FO.26	2.02 51.50 C0.52	5.48 55.20 C0.28	0+40 C0.23	C0.10	6.35 55.70 C0.65
1+85	0.77 50.32 C0.45	1+80 FO.56	FO.05	0.78 50.61 C0.17	4.70 54.38 C0.32	C0.10	C0.17	—
Nly. Alloy 1+45	Ob. end - FO.26 9.15 49.50 FO.35	1+49 FO.41	called out FO.36	0.41 49.72 C0.69	Ob. E.C. on East 0+10	—	—	5.60 54.74 C0.86
Sly. Alloy 1+25	End of loc - FO.19 8.28 49.08 FO.80	1+21 FO.31	on 41 Rad. & FO.02 FO.23	7.82 49.28 C0.54	Nly. Emerald 0+00	—	—	—
0+90	7.84 48.36 FO.52	0+90 FO.46	FO.15	9.07 48.50 C0.57	Sly. Emerald 2+70	—	—	—
0+50	7.28 47.53 FO.25	+50 FO.46	C0.02	8.60 47.61 C0.99	Ob. B.C. on East 2+60	—	—	3.05 52.28 C0.77
Ob. E.C. 0+10	6.79 46.70 C0.09	0.00	C0.18	7.87 46.72 C1.15	—	—	—	—
Nly. Felspar 0+00	—	—	—	—	Ob. B.C. on west 2+54	—	—	—
					2.12 51.73 C0.39	C0.01	—	—

EVERTS ST.

5130

47
5126

Rough
Gr.

Rough
Gr.

Sly. Diamond
2+70

Exist ch.
60.33

Exist ch.
0.80
60.78
✓

Ch. B.C.
2+60

0.69
60.26
C 0.43

0.04
60.26
F 0.22

0.48
60.76
F 0.28

0.83
60.76
C 0.07

2+25

-1" = 9.93
59.40
C 0.53

2+20
C 0.02

F 0.21

0.3
59.90
C 0.4

1+85

8.94
58.44
C 0.50

1+80
C 0.05

C 0.04

9.25
58.94
C 0.31

Sly. Alloy
1+45

Ch. end = C 0.86
8.06
57.48
C 0.58

1+47
C 0.25

C 0.16

Ch. end = C 0.50
8.51
57.98
C 0.53

Sly. Alloy
1+25

Ch. end = C 0.48
7.90
57.00
C 0.70

1+21 end. ch = C 0.20

C 0.33

8.14
57.50
C 0.64

Walker
 Pope
 clerk
 Huffman

FELSPAR ST. PAVING & CURBS
 from CASS TO DAVES
 7-30-51 Plan 8321-L NO 31445

11
 Curb Gut 1/4 2 1/4 Gut Curb 32
 RT

Station

1+40

C 003
 35.18
 35.15

INDIAN
 flag
 MAY 6 1952

C 0.81
 35.12
 34.31

1+10

C 0.14
 35.05
 34.91

C 0.16
 34.20
 34.04

0+80

F 0.91
 34.26
 34.67

C 0.25
 34.02
 33.77

0+50

F 0.37
 34.06
 34.43

F 0.05
 33.45
 33.50

0+21

F 0.38
 33.82
 34.20

F 0.10
 33.13
 33.23

0+20

0+100 = E. line Cass St.

0.01
 34.04
 34.03

33.06
 33.05

S.N. SW 1/4 & TR. Cass & Felspar 32.08

5' Tr. Back W.L. - C-15

Felspar -
from Cass to Dawes

Station	Curb	Out	1/4	1/2	3/4	Out	Curb
	F 011						C 001
3+50	36.71						36.17
	36.82						36.16
	C 0.67						F 007
3+20	37.25						35.82
	36.58						35.89
	F 0.43						F 0.10
2+90	35.92						35.52
	36.35						35.62
	F 0.33						F 0.24
2+60	35.78						35.11
	36.11						35.35
	C 0.06						C 0.49
2+30	35.93						35.58
	35.87						35.09
	C 0.71						C 1.07
2+00	36.34						35.89
	35.63						34.82
	F 0.11						C 0.94
1+70	35.28						35.52
	35.39						34.58

Felapar
from Cuss to Davies

Lt
Curb Gut. 1/4 L 1/4 Gut. Curb.

34
R.

4+99.28 = W.H. Davies

30 R
4+89.78 = EC. Curb R

37.76
37.92

37.61

37.34
37.41

4+70

F 0.14
37.64
37.78

F 0.03
37.21
37.24

4+40

F 0.08
37.46
37.54

C 0.06
37.03
36.97

4+1.0

C 0.01
37.31
37.30

C 0.53
37.23
36.70

3+80

C 0.04
37.10
37.06

C 0.35
36.82
36.43

DHWES ST - PAVING CURBS

from Garnet St.
To Felspar St.

Lt.

curb

£

35
FT
Curb

1+45 = FC. 4' Alley R

1+45'

Prop = 3534 2518 BC 4' R

1+25'

" = 3501 2481 BC 4' R

1+21 = BC. 4' Alley R

0+90

0+60

0+30 = Bit on Rk

0+00

BM on stake 0+80 P.27

3406

Note used BM on stake To Fit End.

3357'

281 / 27 + 35

DAVIES ST - PAVING & CURBS

from Garnet St
To Felspar St.

4'
curb

£

35
Ft
Curb

INDEXED

MAY 6 1952

1+49 = EC. 4' Alley R

1+45

Prop = 3534 3518 BC 4' R

1+25

" = 3501 3481 BC 4' R

1+21 = BC. 4' Alley R

0+90

0+60

0+30 = BM on Rt

0+00

BM. on stake 0+80 P.27 34.06

Note used BM. on stake to fit exist.

			F020
			35.51
			35.71
	F017	C026	
BC	35.51	36.10	
4' R	35.68	35.84	Prop
	F030	C040	
	35.05	35.21	Prop
BC	35.35	35.51	F019
1st			35.05
			35.24

F037
34.35
34.72

F006
34.15
34.21

C026
33.97
33.71

33.57

H

curb

Lt. curb

2+70 = Sh. Felspar

2+60 = BC. 30' cb R on Rt

37.58

2+54 = BC. 30' cb R on Lt

36.78

2+40

37.24

2+10

36.74

1+80

36.23

Roberts
Cota
Moore
Pullen
Aug. 1, 1957
W.O. 20743
8468L

6th St. Hawthorn to Ivy
grades for Top Ret. Wall
stakes 8' west of wall face
See page 21

Top Ret. Wall

37

2160

22123
21962
C1.61

INDEXED

RAW

MAY 6 1952

Top Wall

221.60
219.13
C2.47

1741

216.48
215.75
C0.68

216.49
Bottom Step
210.74 (Walk)
C5.64

2150

221.02
Bottom Step
215.10 (Walk)
C5.92

221.02
Top Step
220.60
C4.2

1710

215.39
214.68
C0.71

2144

0779

214.45
213.62
C0.83

2140

220.80
219.14
C1.66

TP 214.00

TP 219.49

0748

213.41
212.56
C0.85

2128

219.49
218.73
C0.76

Top Wall
220.60
219.49
F1.11

0717

212.68
211.50
C1.18

2103

218.58
217.87
C0.71

0700

N/4-L. Hawthorn

210.92
204.39
F6.53

204.39
Bottom Step
202.5 down
C1.89

1166

217.29
216.60
C0.69

217.29
211.10
C6.19

BM

19935 SW 7 2A CT Hawthorn S 44

219.60

Top. Ret Wall

3400 sig. 2. Ivy

222.22
219.60
C 2.62

2790

221.24
219.66
C 1.58

2780

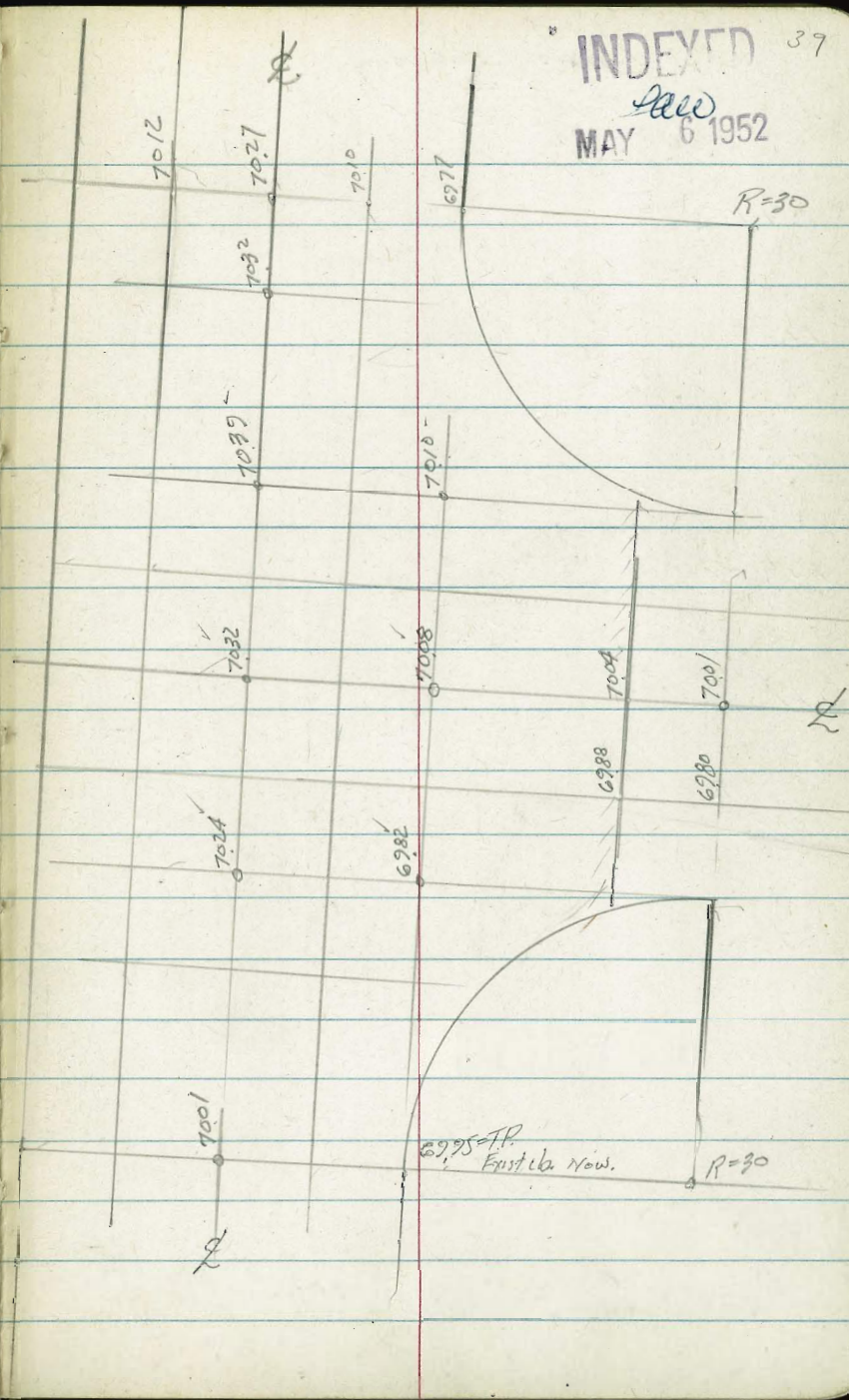
221.87
219.71
C 2.16

2770

221.47
219.72
C 1.75

PAVING -
Felspar from Haines to Ingraham

Intersection
Haines & Felspar



Felspar Paving
from Huinas
To Ingruhum

L

40

2+10		69.09'
1+85	6871-T.P. & sub.	69.24'
1+60		69.38'
1+35		69.53'
1+10		69.68'
0+85		69.83'
0+60		69.97'
0+35		70.12'
0+10 = Bk. = opp ch E.C.		70.27'
0+00 = E. line Huinas		70.32'

Felspar St- Paving

4

41

4+60

6761'

4+85

6776'

4+110

6791'

3+85

6806'

3+60

6820'

3+35

6835'

3+10

6850'

2+85

6865'

2+60

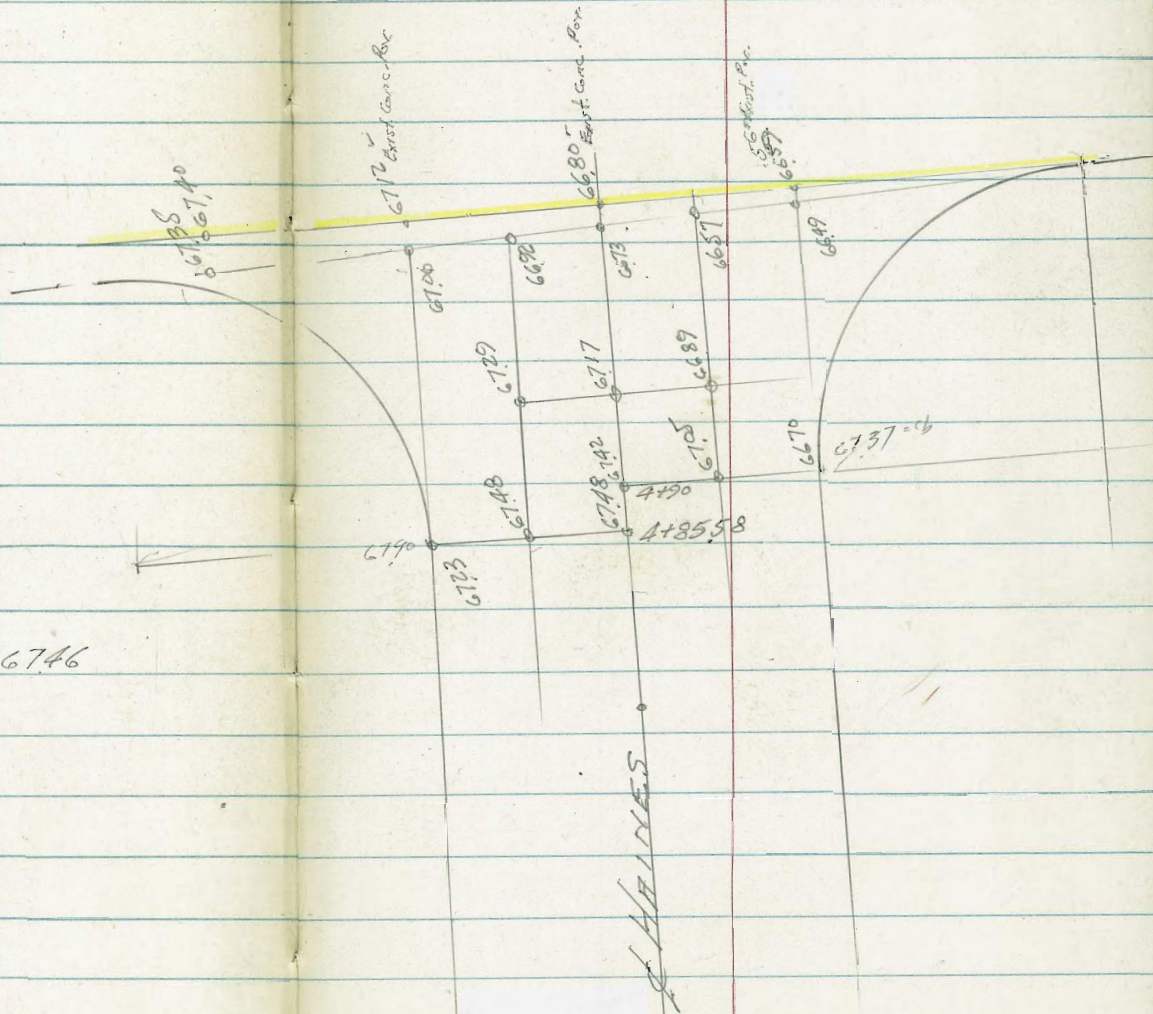
6879'

2+35

6894'

Felspar St. - Paving

INGRAHAM ST.



Page 26
 Christed
 B.M. L. Cross Ingraham & Felspar 67.46

4+90 opp cb B.C.

4+85.58 = 8'k

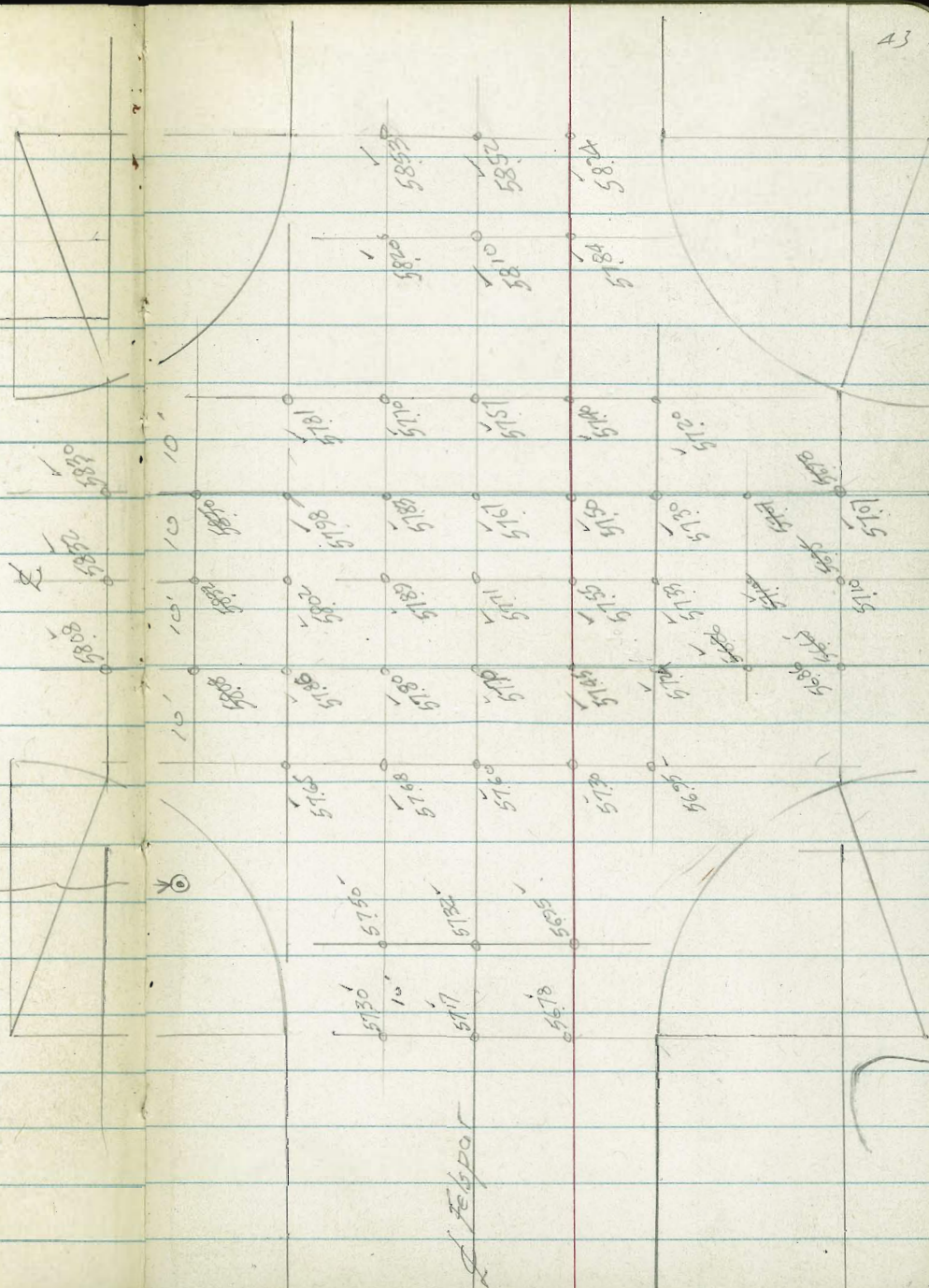
Walker
Pope
Clark
Huffman
8-3-51

Felspar St. Paving Plan 8323-L

110 31445

GRESHAM ST.

B.M. Disk 5809



FELSAPAR

FELSPAR ST. - PAVING
from Gresham to Holmes

£

44

			Get. Lip.		Get. Lip.
1+85			65.82	65.91 ⁸⁰	65.32
1+60	T.P.	64.53 sub. stake	64.79	64.86	64.28
1+35				63.81	
1+10				62.76	
0+85				61.70	
0+60				60.65	
0+35				59.59	
0+10 = opp cb EC.				58.53	
0+00 = E line Gresham				58.10	

Felspar St. Parung

L

45

Gut.
LipGut.
Lip

3+80

6923

69³³~~21~~

6870 68.61

3+55

6896 69.08

69¹⁴~~10~~

6848 6845

3+30

6876 68.90

68⁹⁸~~93~~68.30 68.24
9.4
2.16

3+05

6862 68.76

68⁸²~~76~~

68.12 68.08

2+80 = LVC

6842 68.51

68⁶²~~66~~
68.60

67.98 67.90

2+60

6826

6837¹

67.75

2+40

67.86

67⁹⁷~~95~~

67.35

2+20

67.21

67³⁵~~34~~

66.75

2+00 = PVC

66.44

66⁵⁷~~54~~

65.97

Felspar. St. Peering

£

5+00 = White Haines

4+90 = opp cb 8.C.

4+60

4+30

4+05

70.10

Lip
gutter
Gut. at cb.
62.77 62.90

70.01

Gut.
Lip.
Gut. at cb
62.44 62.33

62.60 62.71

62.⁸⁴~~87~~

62.23 62.14

62.52

62.⁶⁴~~61~~

62.04 62.93

62.34

62.⁴⁷~~44~~

62.83 62.72

FELSPAR & EVERTS ST. 47

Intersection - Parry

Plan 8322-L 140.31445

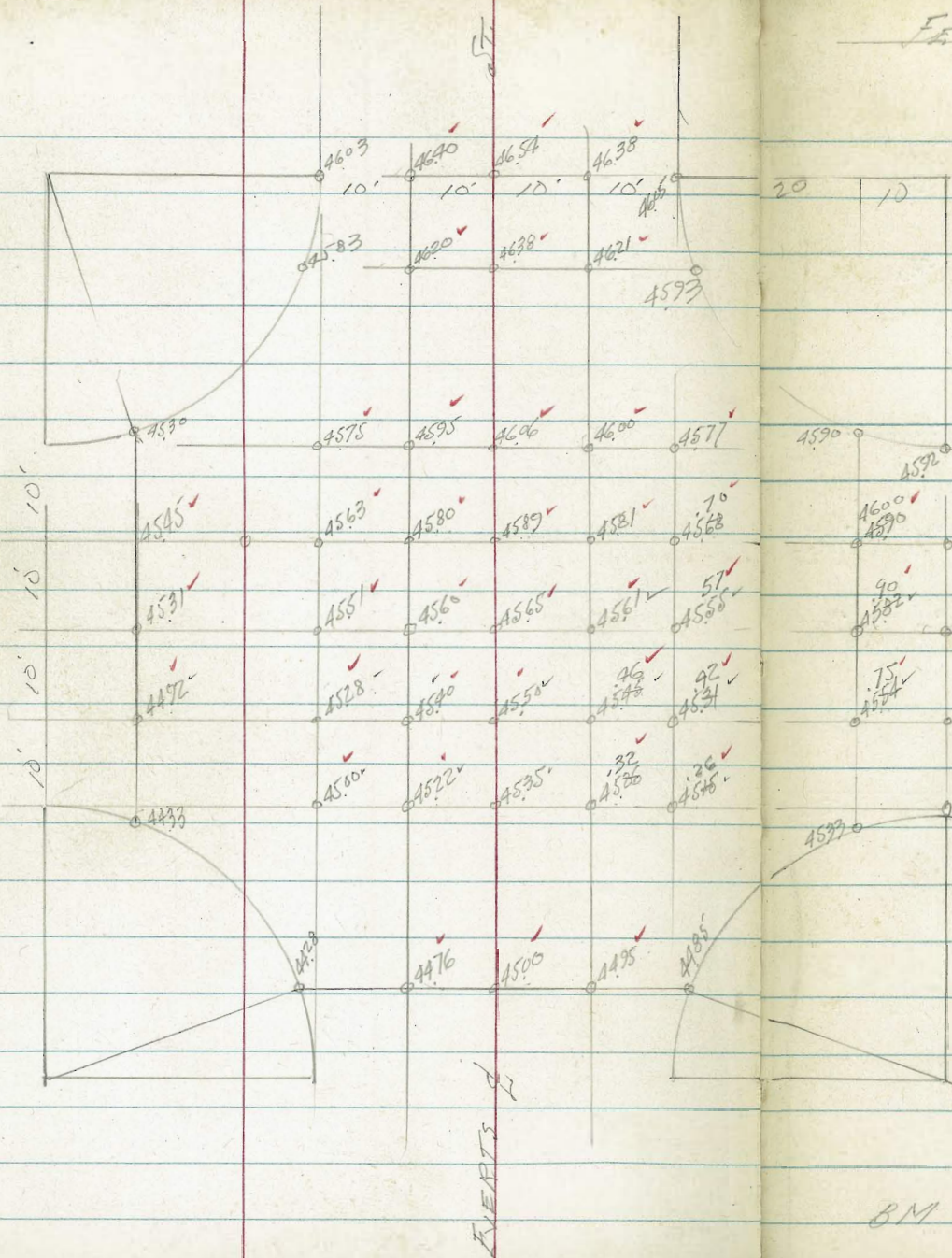
INDEXED

MAY 6 1952

Walter
Pope
Clark
Huffman
8-9-51



FELSPAR ST.

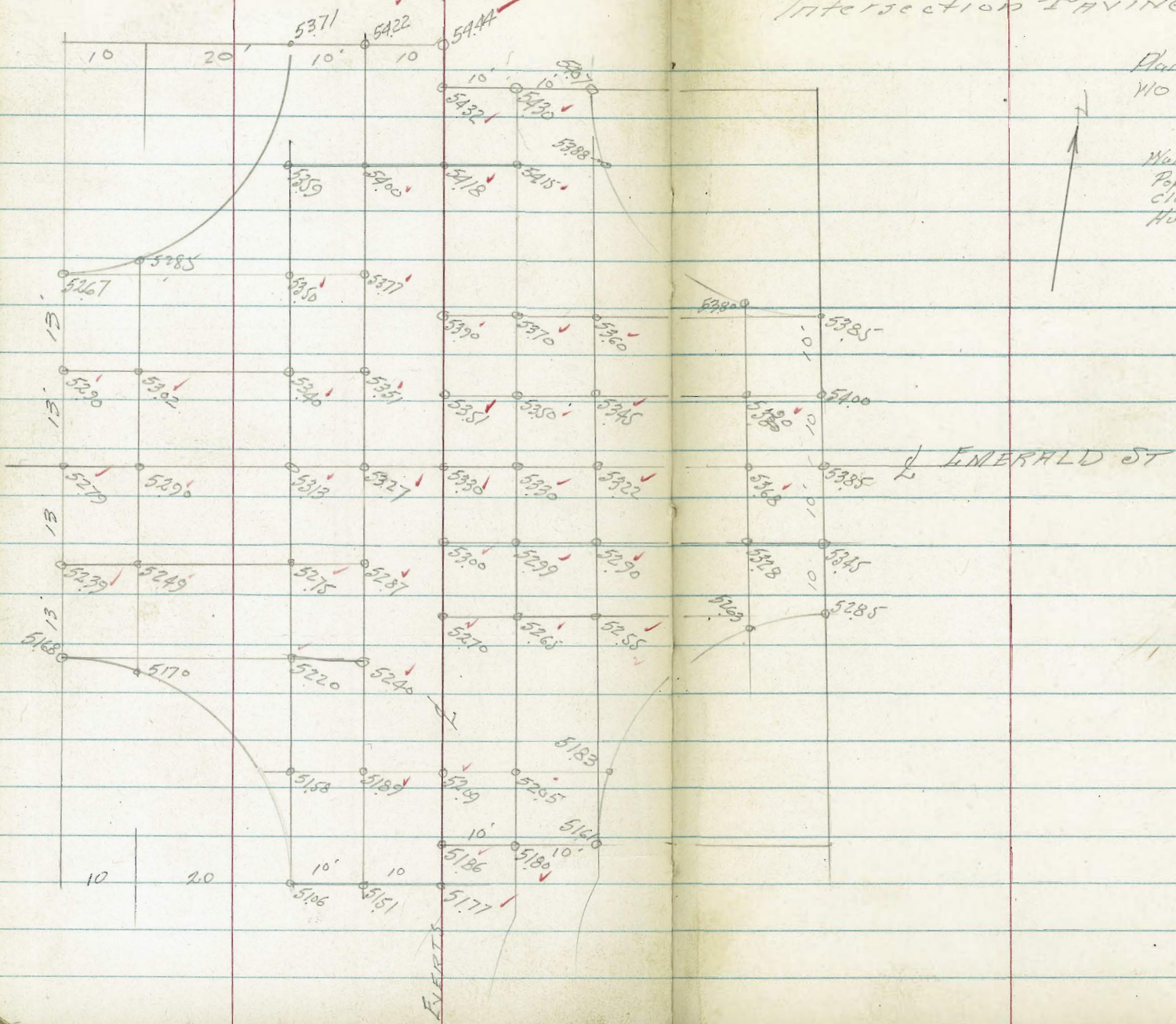


NW Corner of Felspar
BM 3953 = Plan 8322-L

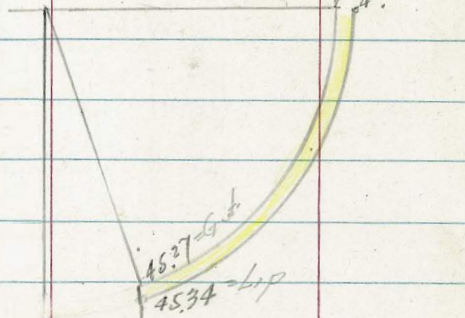
EMERALD ST. + EVERTS ST.
Intersection PAVING. AY

Plan 8327-L
NO 31445

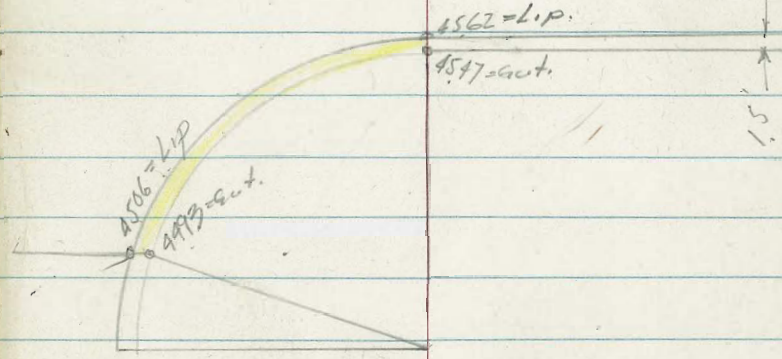
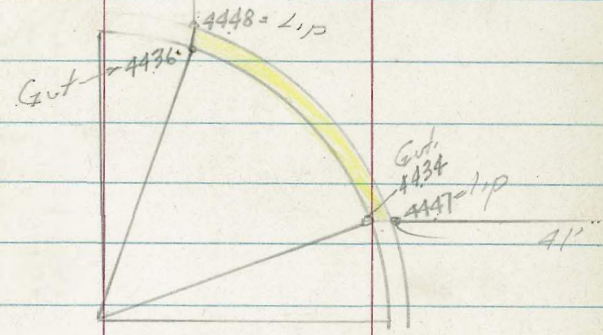
Walker
Pope
Clark
Huttman
8-9-51



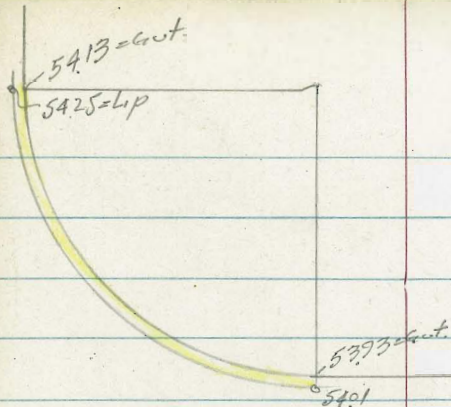
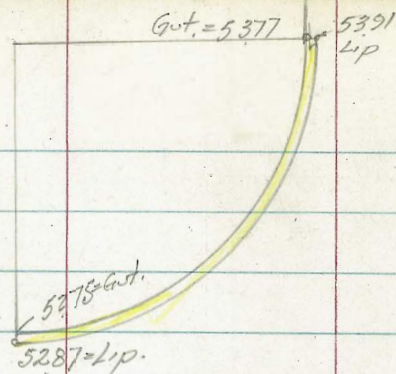
Elevations on
Gutters as Constructed
at Felspar & Everts St



Felspar
15'

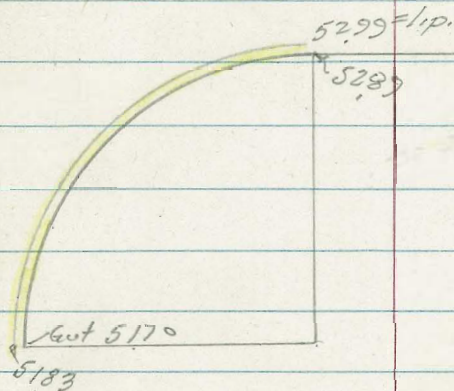
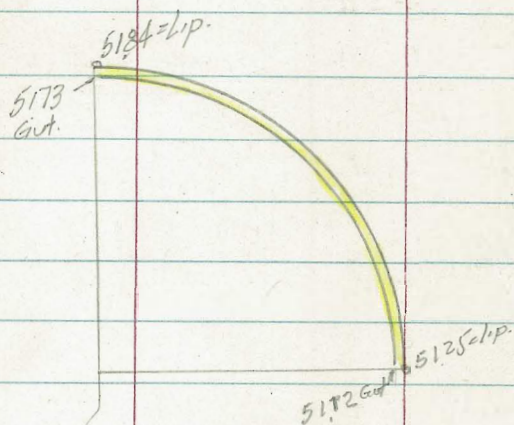


Everts
15'



INDEXED
Law
 MAY 6 1952

EMERALD



FEARTS

Elevation on Gutters as
 Const. at Felaput + Emerald St.

Grade Stakes

Beech - Felton to 33rd

9-20-51

W.O. 31590

Sommer meyer
Bo 99
R. Sisson
oltman

B.M. { 33rd + Beach
25' Nly R.P. Cross for 7' L + t. = 220.83

Rough Rough

1+30	10.90 222.92 F 1.02	2.72 222.92 F 0.20	3.18 223.42 F 0.24	7.42 223.42 C 4.00
------	---------------------------	--------------------------	--------------------------	--------------------------

1+10	1.16 222.76 F 1.54	2.80 222.70 C 0.16	3.05 223.20 F 0.15	7.28 223.20 C 4.08
------	--------------------------	--------------------------	--------------------------	--------------------------

0+90	1.21 222.12 F 0.91	2.30 222.12 C 0.18	2.70 222.62 C 0.14	X-" 7.30 222.62 C-4.74
------	--------------------------	--------------------------	--------------------------	---------------------------------

0+70	0.94 221.20 F 0.26	1.40 221.20 C 0.20	1.89 221.70 C 0.19	X-+2' ⁰ 7.50 221.70 C 6.10
------	--------------------------	--------------------------	--------------------------	--

0+50	X-" 20.19 219.92 C 0.27	20.09 219.92 C 0.16	0.45 220.42 C 0.03	X-+2' ⁰ 6.63 220.42 C 6.21
------	----------------------------------	---------------------------	--------------------------	--

0+30	8.14 218.30 F 0.96	7.95 218.30 F 0.35	8.50 218.80 F 0.30	X-" 23.80 218.80 C 5.00
------	--------------------------	--------------------------	--------------------------	----------------------------------

W.E.C. 0+10	6.34 216.50 F 0.16	6.42 216.50 F 0.08	6.78 217.00 F 0.22	6.92 217.00 F 0.08
----------------	--------------------------	--------------------------	--------------------------	--------------------------

Wly. Felton. 0+00	215.90		216.40	216.40
----------------------	--------	--	--------	--------

33rd St.

Ec. 220.00

7.87
220.10
F 0.23

N.E. Ref.
10.36 10.37

0.34
220.50
F 0.16

10.47

B.C. 221.00

Ec. 219.00

8.50
219.57
F 0.77

S.E. Ref.
10.36 10.37

19.19
220.00
F 0.81

10.47

B.C. 220.50
F 0.41

Beach St.

Rough Rough

Elv. -33 rd 2+20	220.00			220.50
--------------------------------	--------	--	--	--------

on Rad. 19.56 220.50 F 0.94	0.09 220.50 F 0.91	0.73 221.00 F 0.27	on Rad. 4.64 221.00 C 3.64
--------------------------------------	--------------------------	--------------------------	-------------------------------------

20.22 221.50 F 1.28	1.50 221.50 X	1.57 222.00 F 0.43	5.87 222.00 C 3.87
---------------------------	---------------------	--------------------------	--------------------------

20.41 222.32 F 1.91	2.18 222.32 F 0.14	2.43 222.82 F 0.39	6.78 222.82 C 3.96
---------------------------	--------------------------	--------------------------	--------------------------

21.05 222.80 F 1.75	2.57 222.80 F 0.23	3.03 223.30 F 0.27	7.32 223.30 C 4.02
---------------------------	--------------------------	--------------------------	--------------------------

Beech
33rd to Bancroft

Curb Returns
(check as built)

52

33
E.C. 210.00

220.10

220.50

211.00

N.E. Ret. Beech 433rd

B.C.

Beech

Rough cl. cb. Rough

2+10 213.04 213.04 214.22 214.22
4.19 4.19
F 0.03^v

1+90 213.50 213.50 214.50 214.50
4.16 3.54 4.50 9.68
C 0.66 C 0.04 X C-5.18

1+50 214.50 214.50 215.50 215.50
4.68 20.28
C 0.18 C-4.78

1+00 215.75 215.75 216.75 216.75
5.13 7.61
F 0.62 C-2.86

0+50 217.00 217.00 218.00 218.00
5.81 9.32
F 1.19 C 1.32

0+20 217.75 217.75 218.75 218.75
6.61 7.58 8.47 9.40
F 1.10 F 0.17 F 0.28 C 0.65

w/ly. line 33rd
0+00 218.02 218.02 219.05 219.05

33
E.C. 219.00

219.57

220.00

220.50

S.E. Return. Beech 433rd

B.C.

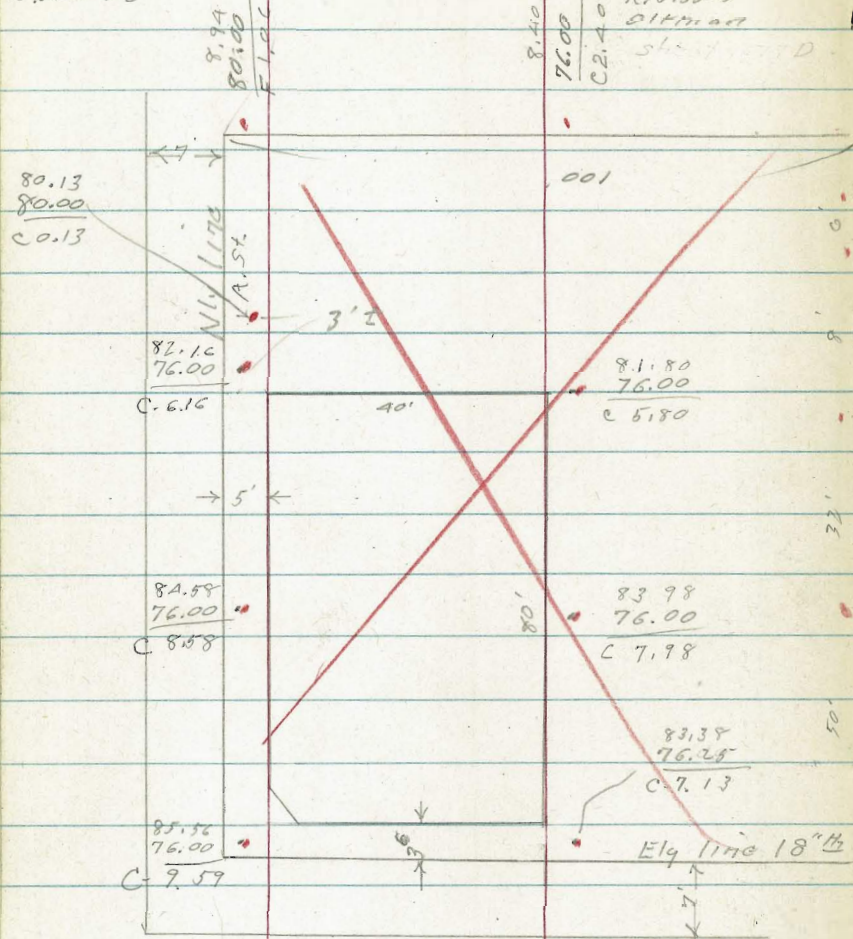
Beech

INDEXED
Law
MAY 6 1952

Sewer Dept. Bldg 18th + A.

10-1-51
W.D. 20716

Summer Meyer
B 99
R. Sisson
21271007
sl. 1677-D



INDEXED
53
MAY 6 1952
N.E.B.M. B+18=68.07

set B.M. N.E. 7' L+T.
18th + A. EL. = 85.75

stations scaled in
from sheet 1677-D.

See P-78
this book

Void
Restaked
from new
plan. 1677-D
6/9/52 *[Signature]*

Grading line is 3' inside of Prop. line
Rough grade stakes set 1' inside Prop. line
(= 2' outside of grade limits for Bldg.)

Prop. grade Tustin st
 Oliphant - to 200' sly.

10-8-51

see P. 67
Change in grade

54

INDEXED
 MAY 6 1952

Sommermeier
 BC 99
 Altman
 Brunner

E. cl.	E. Prop.	w. cl.	w. Prop.
3.82 122.88 C 0.94	4.16 122.76 C -1.40	5.35 123.18 C -2.17	7.63 123.30 C 4.33
8.07 119.76 F 1.89	9.57 119.84 F 0.27	2.84 120.25 C -2.59	4.37 120.37 C 4.00
5.02 107.42 F 2.40	5.23 107.34 F 2.11	9.51 108.09 C 1.42	11.52 108.21 C 3.31
5.04 105.49 F 0.45	4.47 105.37 F 0.99	7.68 106.40 C 1.28	10.26 106.52 C 3.74
2.20 102.62 F 0.38	2.25 102.50 F 0.25	6.17 104.00 C 2.17	8.5 104.12 C 4.4
1.83 101.82 x	8.22 104.02 C 4.12		

Stake cuts or fills on ch. & Prop. lines 2+00

pencil grades as on profile #1384

B.M. = wly. X in M.H. Rim + Tustin Oliphant EL. = 102.25

10+02 T.P.

1+75

1+50

1+23.86

1+03.86

0+83⁸⁶

0+61

0+63.86

0+41 P.O.C.

0+43.86 P.O.C.

0+15 P.O.C.

0+10 ch. E.C.

Sly. Oliphant
 0+00

JEWELL St.
Moorland Dr. to La Playa Ave

4.92

□ - 20⁵ Lt. of otoc = 23.88
in ob.

55

W.O.# 31922

10-11-51
Sommermeier
Betg

	Rough grade	ch.	ch.	Rough grade
5+14	6.00 2A.97	4.80 2A.97	4.85 25.07	5.40 25.07
	C-1.03	FO.17	FO.22	C-1.33

MAY

6 1952

75' street

Sheet-8655-L
F.B. 1867-12465

oltman
Brunner

4+84	5.69 25.08	4.94 25.10	5.01 25.20	6.85 25.18
	C0.61	FO.16	FO.19	C-1.67

41' Road way.

Rough Gr. stakes
5' back of Prop.

Rough grade Lt. ch. ch. Rough grade Rt.

4+54	5.79 25.18	4.96 25.22	4.98 25.32	5.91 25.28
	C0.61	FO.26	FO.34	C0.63

2+70.2

5.28
2A.97
C0.31

FO.39

FO.11

4.97
2A.77
C0.20

chisel x 4+34	5.64 25.25	5.09 25.30	5.14 25.39	5.84 25.34
	C0.39	FO.21	FO.25	C0.50

2+26.4

4.85
2A.78
C0.07

FO.24

FO.24

4.63
2A.45
C0.18

chisel x 4+14	5.58 25.28	5.00 25.26	5.02 25.25	5.54 25.37
	C0.30	FO.36	FO.43	C0.17

1+82.6

4.77
2A.59
C0.20

FO.20

FO.06

4.32
2A.14
C0.18

3+74	5.58 25.30	4.94 25.40	5.09 25.46	5.67 25.36
	C0.28	FO.40	FO.37	C0.31

1+38.8

4.65
2A.40
C0.25

FO.10

C-0.10

4.16
23.83
C0.33

3+74	5.05 25.29	4.98 25.35	5.07 25.20	5.51 25.34
	C0.30	FO.37	FO.33	C0.17

walk.
End existing cl.
0+95

24.20 24.20 23.51 23.51

chisel x 3+54	5.54 25.27	5.14 25.30	4.98 25.31	5.60 25.28
	C0.27	FO.16	FO.33	C0.32

ink figures = change of
grade for better drainage. C.H.S.

3+34	5.55 25.22	5.10 25.25	4.97 25.24	5.47 25.21
	C0.33	FO.15	FO.27	C0.26

Exist. Pave. (8655-L)
0+00 = N1/4 edge.

3+14	5.60 25.16	4.98 25.20	4.80 25.19	5.47 25.09
	C0.44	FO.22	FO.33	C0.38

JEWELL

56

	LH.		RT.	
	Rough grade	Cbs.	Obs.	Rough grade.
End. of Job.	4.55	2.95	2.87	4.96
6+54	<u>23.09</u>	<u>23.09</u>	<u>23.14</u>	<u>23.04</u>
	C 1.46	F 0.14	F 0.27	C 1.82
6+24	5.65	3.37	3.55	6.36
	<u>23.67</u>	<u>23.67</u>	<u>23.67</u>	<u>23.67</u>
	C 1.98	F 0.30	F 0.12	C 2.69
5+9A	5.91	3.97	4.07	6.67
	<u>24.25</u>	<u>24.25</u>	<u>24.21</u>	<u>24.21</u>
	C 1.66	F 0.28	F 0.14	C 2.46
5+74	5.80	4.35	4.45	6.54
	<u>24.57</u>	<u>24.51</u>	<u>24.53</u>	<u>24.53</u>
	C 1.29	F 0.16	F 0.08	C 2.00
5+54	5.75	4.61	4.62	6.52
	<u>24.72</u>	<u>24.72</u>	<u>24.78</u>	<u>24.78</u>
	C 1.03	F 0.11	F 0.16	C 1.74
5+34	6.01	4.73	4.86	6.00
	<u>24.87</u>	<u>24.87</u>	<u>24.96</u>	<u>24.96</u>
	C 1.14	F 0.14	F 0.10	C 1.04

E+W. Alley BIK 69 O.B.
original staking @ 277
66

11/1/51

N.W.B.R. Bacon 4 +	Del. Monte = 24104		C.H.S. Bogg R. Sisson Oltman	3+50	D-2' Bath ways	1.65 41.13 C 0.52	4 2.62 41.13 C 1.49	Nail - 170 line
1+60	5.59 33.80 C-1.79	4.15 33.80 C 0.35		3+30		1.86 40.63 C 1.23	1.38 40.63 C 0.75	D-2.20
1+40	3.04 31.93 C 1.11	3.00 31.93 C 1.07		3+10		0.76 40.12 C 0.64	40.65 40.12 C 0.54	D-1.50
1+20	31.61 30.31 C 1.30	32.19 30.31 C 1.88		2+90		40.49 39.61 C 0.88	40.79 39.61 C 1.18	D-2.10.
1+00	30.98 29.02 C 1.95	30.61 29.02 C 1.59	INDEBTED law 6 1952 MAY	2+75		39.23 39.23 F 0.62	39.23 F 0.62	51'
0+80	9.23 28.08 C 1.15	7.14 28.08 F 0.94		2+55		9.62 38.73 C 0.89	9.50 38.73 C 0.77	F-21 2+50 Lt. 39.55 38.58 C 0.97
0+60	7.29 27.47 F 0.18	6.80 27.47 F 0.67	X-2'	2+25		7.54 37.83 F 0.29	40.42 37.83 C 2.59	
0+40	7.54 27.20 C 0.34	6.71 27.20 F 0.49		2+00		6.40 36.70 F 0.30	6.90 36.70 C 0.20	
0+00	27.06	26.97	X-2'	1+80		5.69 35.40 C 0.29	5.55 35.40 C 0.15	

E+W. Alley Bik 69 O.B

58

A+30
D-2'
both ways

1.32
42.35
F1.03

A+20

1.86
42.35
F0.49

A+10

1.76
42.30
F0.54

A+00

2.10
42.20
F0.10

3.28
42.15
C1.13

3+90

1.85
42.06
F0.21

3.45
42.06
C1.39

D-1.90

3+80

1.36
41.89
F0.53

5.04
41.89
C3.15

D-2.60

3+70

D-2back
both ways

1.17
41.64
F0.47

5.18
41.64
C3.54

D-2.70

Drainage Ditch along So Levee
Midway to Lapwai

W.O.# 20853

Sheet 9152-L

F.B. 2066-61

B.M. = 0000 Hub.

stakes - 10' Lt. of ±

3+00
10
0.110

2+50

B.M.
2+00 A

1+50

1+00

0+50

0+00

FB 2066
62

El. = 10.77

3.53
-2.48
C-2.01

3.45
-2.53
C-5.98

2.82 ✓
-2.58
C-5.40

3.59 ✓
-3.16
C-6.75

3.59
-3.74
C-7.23

3.30
-4.32
C-7.62

2.89
-4.71
C-7.80

11/9/51

C.H.S

Boyer

R. Sisson

Altman

0.16

S.D. River

8+00

7+50

7+00 Δ

6+50

6+00

5+50

5+00 Δ

4+50

4+00 Δ

3+50

0.42
-1.98
C-2.40

0.51 ✓
-2.03
C-2.54

1.05
-2.08
C-3.13

2.77
-2.13
C-4.90

2.43
-2.18
C-4.61

2.72
-2.23
C-4.95

2.21
-2.28
C-4.47

3.44
-2.33
C-5.77

3.58 ✓
-2.38
C-5.96

3.29
-2.43
C-5.72

INDEXED

FILED

MAY 6 1952

59

10+82 1.72
-1.70
C-3.42

10+50 2.18
-1.73
C-3.91 ✓

10+00 2.57
-1.78
C-4.35

9+50 1.28
-1.83
C-3.11

9+00 0.24
-1.88
C-2.12

8+50 1.00
-1.93
C-2.93

Sewer Crossing Nly.
approach Morena bridge

11-9-57

sheet 9087-L

stations from 9087-L

13+98.06

11.67
- 2.30
C 13.97

13+63.06

16.37
- 2.35
C 18.74

Δ off Hy. = 90° - 59' 17" S. E. Quad.
Also = Highway Sta. 13+43.17

13+28.06

16.84
- 2.40
C 19.24

12+93.06

16.64
- 2.45
C 19.09

12+58.06

8.21
- 2.51
C 10.72

Alley BIK 245 Mission Beach

11-13-51

C.H.S.

Begg

R. Sisson

Oltman

B.M. = B.P. York Ct. & Sea Wall. EL = 7.08

W.O. 31869
Sheet 8353-L

see G 277 for sewer
74 laterals

6.1

INDEXED

MAY 6 1952

1+00	0.38 0.24 Co.14	0.13 0.24 Fo.11		3+24 ^A	—	Meet. pave.	←
0+80	0.90 0.49 Co. A 1	1.78 0.49 Cl. 29	N-191	W. line Mission Blvd 3+13 ^A	-0.60	-0.43	
0+60	X-3' 1.41 1.10 Co. 31	1.71 1.10 Co. 61	X-120	2+90 X-0.28	0.81 -0.36 Co. 1.17	0.75 -0.36 Co. 1.11	
0+30	X-124 2.97 2.30 Co. 67	3.87 2.30 Co. 57	Hinge -1.87	2+52	0.46 -0.24 Co. 70	0.09 -0.24 Co. 33	N.-0.38
0+20	3.06 2.64 Co. 42	3.45 2.64 Co. 81		2+14 N-0.57	-1.02 -0.12 Fo. 90	-10.21 -0.12 Fo. 09	N-0.55
0+10	3.30 2.88 Co. 42	3.27 2.88 Co. 39		1+76 N-0.32	0.29 -0.00	0.11 0.00 Co. 11	N-0.85
0+00	3.00 E. Lorie Strand way.	2.98		1+38	-0.17 +0.12 Fo. 31	+0.03 +0.12 Fo. 09	N-1.44

E.C.
10+62.76

5.95
423.64
C 2.31

4.29
423.88
C 0.91

Emp. Cl.
10+60.76

5.59
423.50
C 2.09

4.25
423.28
C 0.97

10+50

4.82
423.04
C-1.78

4.10
422.90
C 1.20

10+40

4.25
422.60
C 1.65

3.97
422.60
C 1.37

Cl. B.C.
10+27.79

3.76
422.20
C 1.56

3.15
422.31
C 0.84

11+40

428.50

428.00

10+20

3.47
422.09
C-1.78

2.90
422.10
C 0.80

11+20

8.57
427.12
C-1.45

15.85
426.60
F 0.75

10+00

421.77

421.79

11+00

8.47
425.85
C-2.63

4.93
425.30
F 0.37

9+97.76

421.76

421.78

10+80

5.86
424.60
C 1.26

4.28
424.20
C 0.08

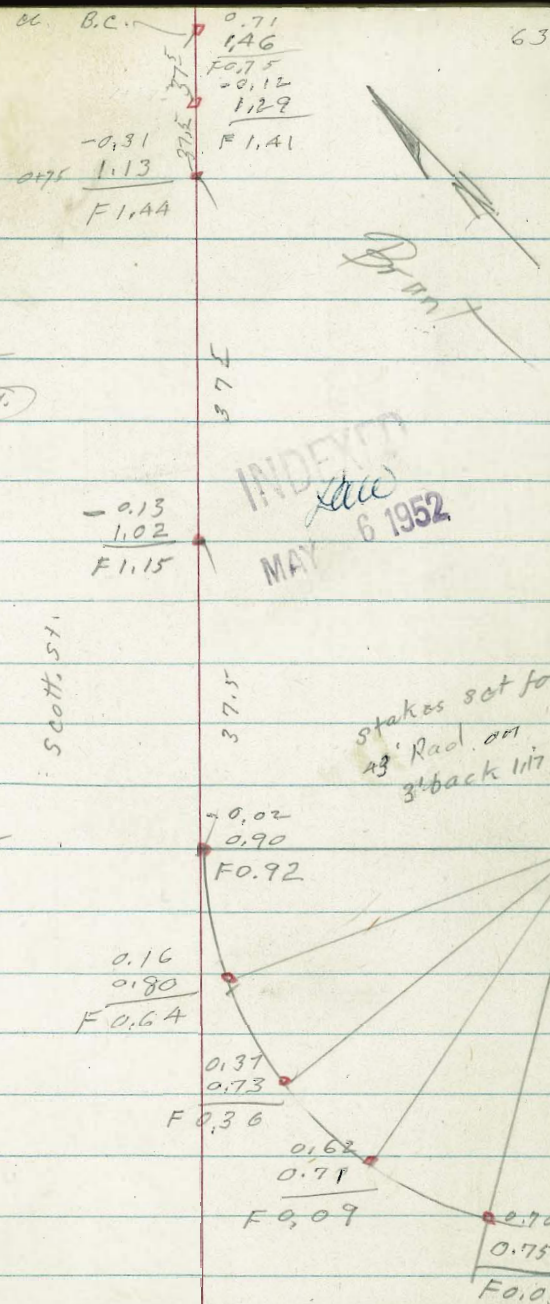
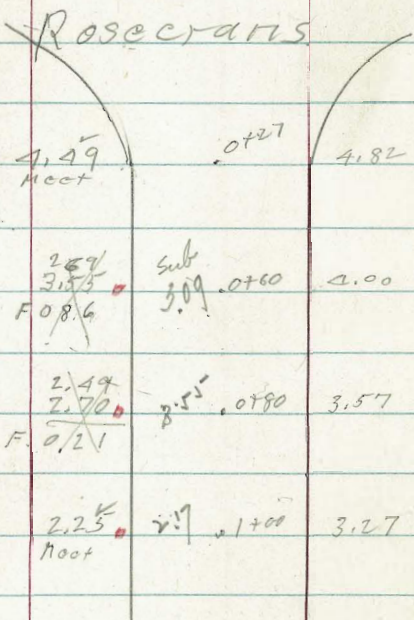
INDEXED
LW
MAY 6 1952

$$\begin{array}{r} 3.47 \\ 33 \\ \hline 3.09 \end{array}$$

$$\begin{array}{r} 9 \\ 2.93 \\ \hline 2.93 \end{array}$$

Scott St.
Jarvis St.

Pave
11/20/51



Olivet St.

S.Wly. from Ivanhoe Ave East

11-30-51
W.O. 31560

CHS
Boyer
R. Sisson
Oltman

Sheet 8010L

INDEXED
Indexed Raw
MAY 6 1952

stakes on curb line

1+30	—	—	6.65	4.42				
			F1.18	F1.18				
1+20	C 2.22	350	—	—	153.13	51.77	150.97	149.0
						151.77	150.77	
1+00	—	—	6.30	4.02		grade	C 0.20	
			F1.13	F1.13				
0+91	C 2.72	300	—	—		5.25	5.00	2.70
						C 0.47	C 0.11	C 0.20
						5.50	—	—
						F 0.08	—	—
0+60 Brk.		187.82	183.70	—		—	5.70	3.20
		186.75	185.75				F 0.53	F 0.30
		C 1.07	F 2.05			5.65	—	—
						C 0.07	—	—
0+40 Brk.		189.05	186.77			—	5.95	3.19
		188.63	187.69				F 0.71	F 0.28
		C 0.42	F 0.92			6.40	6.57	1.30
						F 0.68	F 1.35	F 0.80
0+20 Brk.		190.10	189.54			6.16	6.90	3.95
		190.02	189.24			F 0.44	F 1.23	F 1.05
		C 0.08	C 0.130			5.80	6.40	3.27
						F 0.14	F 1.23	F 0.37
0+03 Brk.		190.55	190.06			4.17	—	—
		190.85	190.30			C 1.55	—	—
		F 0.30	F 0.24			4.32	5.57	2.10
						C 1.40	F 0.93	C 0.80
Ivanhoe East		190.95	—			3.50	—	—
S.Wly line		191.00	190.00			C 2.22	—	—
0+00		F 0.05	—			—	—	—

Rate rod = 5.72

Rate rod = 5.17
Return take rod = 2.90

Void - wrong rods

1+50 28.81
127.45
C-1.36

1+25 28.96
126.89
C-4.14

1+00 29.84
126.20
C-3.64

+75 131.14
125.57
C-3.57

+50 133.76
124.95
C-8.81

+25 137.68
124.32
C-13.28

0+00 37.60
123.50
C-13.40

Sewer

B.K. H - Plumosa Park

66

Sly from Amaryllis Dr.

12-7-51

C.H.S.

Boyer

R. Sisson

Oltman

W.O.

INDEXED
RQW
MAY 6 1952

+50

128.81

124.90

C 3.91

3+25

137.48

126.30

C 11.18

+25

128.96

124.70

C 4.26

3+00

135.04

126.10

C-8.94

+100

129.84

124.50

C 5.34

2+75

132.58

125.90

C-6.68

+75

131.14

124.30

C 6.84

2+50

130.92

125.70

C 5.22

+50

133.79

124.10

C 9.69

2+25

129.95

125.50

C-4.45

+25

137.60

123.90

C 13.70

2+00

128.79

125.30

C 3.49

+00

137.10

123.70

C 13.40

1+75

28.64

125.10

C 3.54

Existing Sewer
Amaryllis Dr.

	Tustin	12/10/51	3+85	Ch. 144.18	Prop. 144.30	67
	Oliphant - South					
	for inspection only,					
	Ely line Tustin } Popilo 1384		3+60	141.38	141.50	
	" " " }					
			3+40	139.00	139.12	
	curb.	Prop.				
1+80	20.03 119.96 C 0.07	19.26 120.08 F 0.82	3+20	136.62	136.74	
1+60	117.42 ^{T.P.} 117.58 F 0.16	16.50 117.70 F 1.20	3+00	134.24	134.36	
1+40	4.00 115.20 F 1.20	11.13 115.32 F 4.19	2+80	131.86	131.98	
1+20	112.16 112.82 F 0.66	109.63 ^{T.P.} 112.94 3.31	2+60	30.30 129.48 C-0.82	29.63 129.60 C 0.03	
1+00	9.49 110.48 F 0.99	8.88 110.60 F 1.72	2+40	9.24 127.10 C 2.14	8.99 127.22 C 1.97	
0+80	7.31 108.22 F 0.71	7.90 108.34 F 0.44	2+20	125.28 ^{T.P.} 124.72 C 0.56	4.62 124.84 F 0.12	
0+60	5.28 106.22 F 0.94	4.82 106.34 F 1.52	2+00	4.31 122.34 C-1.97	3.94 122.46 C 1.48	

EL. 102.25

B.M. = wly. X in N.H. Rim Oliphant & Tustin FD 1803
10

Orchard. - Cl. stakes

N. Ely. side Orchard } as per A193-B
 S. Ely. from Catalina)

11-12-51
 W.O. 20750

C. H. 5
 B 999
 R 915307
 W. Ottman

B.M. = SW.B.P. Catalina + Orchard EL = 19650

stakes 3' back cl. face

68

195.19 cl. E.C.
 ✓ OK

12' R.

INDEXED
 faw
 MAY 6 1952

5.41
~~195.32~~
 00.09

10100

BIK. E
 Catalina
 Manor.

5.120
~~195.44~~
 F 0.24

101325

5.27
~~195.55~~
 F 0.28

0469

572

195.180
 ✓
 OK

Emma lands
 park

Del Mar.
Catalina - Easterly. 1/4/52

sheet 8710-L

@+00 = Ely. line Catalina

B.M. = S.W. B.P. Del Mar + Catalina EL: 187.53

Existing el.

3+0A 84

7.19
187.26
FO.07

187.78
✓

2+85

6.58
186.58
✓

7.38
187.11
C 0.27

2+65

6.04
186.04
✓

6.67
186.58
C 0.09

Existing el.

2+45

5.64
185.62
C 0.02
✓

186.17
✓

Orchard St. 67
Catalina Blvd. - Ely. 12-7-52
Curb stakes (3' back of face)

Sewer Lat #1 (sheet 8709-L)

obs. sheet 8710-L

Meet Existing el.

2+86

2+66

2+50

2+00

1+50

1+00

0+50

0+31.19

11.46 Sta. of S. Line Catalina.
0+00 = E.C. Rt.

4.66
190.01
C-4.65

6.87
196.85
C 0.02 ✓

6.36
196.78
FO.42

FO.54

FO.40

FO.30

F-0.06

C-0.12

6.25
195.98
C 0.27

5.73
196.21
FO.48

B.M. = S.W. B.P. Orchard + Catalina = 196.50

6" Sewer Thomas + Noyes

1-9-52
W.O. 80009

CHS.
Begg
Oltman
Taylor

EL. ex. IE. existing line Assumed 0.00

Direct Elevation used

Elevation Tie in - See below

right.
as assumed. EL. 0.00 in notes on
Actual EL. existing 8" = 20.07 shown

EL. existing 8" line

at 0+00		9.07	20.67
			28.74
T.P.	1.00	29.74	8.13 29.74
		36.87	12.75 35.97
T.P.	0.90	37.87	14.75 36.97
T.P.	0.31	48.72	11.63 48.41
T.P.	1.80	60.04	6.85 58.24
			N.W. D.P.
	3.07	65.07	— 62.02
			Barnet & Noyes



2.78
1.08
C1.70

3.53
0.90
C2.63

4.73
0.72
C4.01

6.58
0.55
C6.03

8.07
0.37
C7.70

40.00
0.20

0+00
0.20 Above existing line

Thomas

Noyes
Existing 8"
Sewer

RECEIVED
MAY 6 1952

Existing (W) - change to grade.

Jewell St. 12/30/52

Fortuna to P.B. Drive

0+00 = N.Y. line Fortuna-

9.E. Lt. P.B. Dr + Jewell EL = 45.78

Cuts on sly. stubs.

3+15	4.27
	<u>43.20</u>
	C 1.07

2+67	3.66
	<u>42.69</u>
	C 0.97

2+05	3.03
	<u>42.04</u>
	C 0.99

1+53	42.12
	<u>41.39</u>
	C 0.73

0+13	39.31
	<u>37.35</u>
	C 1.96

Water Services

71

40.48
<u>1.17</u>
39.31

4+53

45.61
<u>44.65</u>
C 0.96

3+89

44.52
<u>43.98</u>
C 0.54

3+72

44.46
<u>43.80</u>
C 0.66

3+47

44.32
<u>43.54</u>
C 0.78

INDEXED
7-11
MAY 6 1952

INDEXED
Law
6 1952

Sewer thru La Jolla Country Club
(Delcrest Lane to La Jolla Country Club Hgts)

NO 20733 8228-L FB 2095-2	2-452 C.H.S. B 299 RS 15500 W. Ottman	6+00 10' Lt.	317.49 327.48 X 9.99 3.88 C 6.11
	Mo7 S.E. Cor. Beverly Hgts 296.12 8.62	5+95 ^Δ M.H.# 34-33 Lt	317.00
2+60 = M.H.# 2	304.74 X 1.80 302.94 11.40	296.03 314.34 X 5+90	316.68 10.80 4.14 C-6.66
2+50	314.34 X 0.23 314.11 13.37	295.65 X	314.18 13.30 5.34 C-7.96
2+00	327.48 X 0.11 327.37 7.10	293.72 304.74 X 5+00	311.05 16.43 9.28 C-7.15
1+50 3.85 96	334.47 5.75 328.72 B.M.# 2 2095	291.80 12.94 3.37 C-9.57	307.92 19.56 10.74 C-8.82
1+00	Should be 328.64 12.66	289.87 14.87 4.74 C 10.13	304.79 327.48 X 22.69 12.35 C-10.34
0+50	341.30 X 1.63 339.67 11.82	287.95 16.79 7.09 C 9.70	301.66 314.34 X 12.68 4.07 C 8.61
Exist. 8" 0+00 = M.H.# 1	351.49 X	286.02 304.74 X 3+00	298.53 15.81 9.49 C-6.32

9+50
1532%
9+00
9+00

375.07 X
356.26
18.81
13.91
C-4.90
363.79 X
348.60
15.19
9.62
C-5.57

351.49 X
0.60
350.89
12.90
363.79 X
1.95
361.84
13.23
375.07 X
0.95
374.12
12.21

Δ 0° 28' RT.
8+70 - M.H.# 4

363.79 X
344.00
19.79
12.01
C-7.78

2/2 = 60' N 1/4 R.P. - 10+47.02 →

386.33
1.87
384.46

8+50

363.79 X
342.04
21.75
13.18
C-8.57
351.49 X
337.13

8+00

14.36
7.61
C-6.75
341.30 X
337.22 T.R.
49.08
1.63
C-7.45

End Contract.
10+47.02 M.H.# 5

Reset 3/28

386.33 / 83.87
377.98 / 77.98
8.35 / C-5.89
1.63
C-6.72

7+50

9.82%

341.30 X
327.31
13.99
6.39
C-7.60

2 1/2% bond.
10+32 B.K. 5

386.33 X
368.82 ← 378.24
17.51 368.82
8.09 9.42
C-9.42

7+00

6+50

334.47 X
322.40
12.07
6.47
C-5.60

10+00

375.07 X
363.92 363.92
11.15 5.65
5.50 89.57
C-5.65

Jewell St.

Fortana to Pac. Beach. Drive

2-5-52
W.D. 31740C.H.S.
Begg
R. Sisson
W. Oltman

75' street. stakes 5' back of prop.

F.B. $\frac{2033}{43}$ sheet 8890-L

0+00 = Nly line Fortuna

#2
B.M. = Chiseled \square ctr S.E. Rot. Fortuna + Jewell

EL = 35.81

Rough cl. ± cl. Rough

#1 = SE 7' L + T. P.B. Dr. + Jewell EL = 45.78

1+25

0.39	0.16
<u>40.25</u>	<u>40.25</u>
C0.14	F0.09

0.61	2.91
<u>40.85</u>	<u>40.85</u>
F0.24	C 2.06

1+05

40.00	9.67
<u>39.78</u>	<u>39.78</u>
C0.22	F0.11

0.13	42.28
<u>40.38</u>	<u>40.38</u>
F0.25	C-1.90

0+85

9.61	9.16
<u>39.22</u>	<u>39.22</u>
C0.39	F0.06

9.68	41.99
<u>39.82</u>	<u>39.82</u>
F0.14	C 2.17

0+65

w. cl.

E. cl.

9.16	8.60
<u>38.58</u>	<u>38.58</u>
C0.58	C0.02

9.20	41.86
<u>39.18</u>	<u>39.18</u>
C0.02	C 2.68

0+38⁷

7.80
<u>37.67</u>
C0.13

8.51
<u>38.27</u>
C0.24

0+12⁵

8.24	
<u>36.75</u>	36.75
C1.49	

	40.72
37.35	<u>37.35</u>
	C-3.37

0+00

8.47	
<u>36.47</u>	
C1.00	

	40.28
	<u>37.08</u>
	C 3.20

INDEXED
file
MAY 1952

Exist	Rough	cl.	±	cl.	Rough
4+50	3.98 4A.03 FO.05	4.04 4A.03 CO.01	4.44 4A.62 FO.18	6.68 4A.62 C2.06	
4+00	3.53 43.50 CO.03	3.61 43.50 CO.11	4.05 4A.10 FO.05	6.31 4A.10 C 2.21	
3+50	3.15 42.98 CO.17	3.12 42.98 CO.14	3.54 42.57 FO.03	5.66 43.57 C 2.09	
3+00	2.62 42.45 CO.17	2.50 42.45 CO.05	2.96 43.05 FO.09	5.36 43.05 C 2.31	
2+50	2.35 41.93 CO.42	41.98 ^{T.P.} 41.93 CO.05	2.50 42.52 FO.02	4.96 42.52 C 2.44	
2+00	1.35 41.40 FO.05	1.50 41.40 CO.10	1.88 42.00 FO.12	4.35 42.00 C 2.35	
1+85	1.42 41.24 CO.18	1.12 41.24 FO.12	1.65 41.83 FO.18	3.89 41.83 C-2.06	
1+65	1.12 40.98 CO.94	0.88 40.98 FO.10	1.35 41.58 FO.23	3.47 41.58 C 1.89	
1+45	0.70 40.66 CO.04	0.53 40.66 FO.13	1.10 41.25 FO.15	3.33 41.25 C 2.08	

Fortuna

37.28

7.17
37.19
FO.01

6.88
37.04
FO.16

7.05
37.00
CO.05

7.48
37.12
CO.16

7.49
37.35
FO.06

12.89

9.99

9.43

9.43

9.42

N.E. Ret.

±

Jewell

Jewell

6.78
36.75
CO.03

4.60
36.47
CO.13

6.47
36.18
CO.19

6.34
36.11
CO.23

6.30
36.05
CO.25

9.42

9.43

9.42

5.99

12.89

N.W Ret.

Prop

Jewell
Fortuna

Exist	Pave	Rough	cl	±	cl.	Rough
5+25	4.82 44.82 ✓	4.82 44.82 ✓	77 45.39	5.40 45.39 ✓		
5+00	5.00 44.55 CO.45	4.86 44.55 CO.31	5.00 45.15 FO.15	6.95 45.15 C 1.80		

Alley Bk. 8 La Jolla Park

Pearl to Kline
between Girard + Fay
Sheet 80A1-L
FB 1853-37

115.17 = B.M.

115.17
12.91
102.26 B.M. #1

B.M. = S.E.B.P. Girard + Pearl. E.L. = 115.17

PROP. PIPS 10' LT 1 + 50 = 102.26 B.M. #1

D-V back

Indexed
part
MAY 1952

	West	±	East	
2+40 E.V.C.	0.59 99.49 C1.10		1.23 99.79 C-1.44	
2+20	0.72 100.04 C0.68		1.32 100.34 C0.98	
2+00	1.75 100.65 C1.10		1.58 100.95 C0.63	
1+80	2.12 101.33 C0.79		3.14 101.63 C-1.51	X + 1012
1+60	2.21 102.09 C0.12		3.26 102.39 C-0.87	N + 10120
1+50	2.38 102.50 F0.12		2.70 102.80 F0.10	N - - 0.05

	West	±	East
Exist. Pave 4+00	94.78	94.63	95.02
3+50	6.95 96.74 C0.71		7.67 96.51 C-1.16
3+00	9.10 97.70 C-1.40		9.18 98.00 C1.18
2+70	100.03 98.59 C1.44		9.76 98.89 C0.87

0.2927

0.0298%

0+00 = Nly line Pearl.

Nashville St. 2-18-52

Moreno to Tonopah St.

N. wly
line

S. Ely. line

FB 1707
Profile 4109

Tonopah
S. wly line
5+15.95

B.M. = B.P. & Tealote bridge
N. wly.

EL. 1004
at Moreno
S. Ely.

8.80

7.05

2+50

7.70
7.83
F0.13

6.10
8.23
F2.13

5+00

9.00
8.75
C0.25

6.55
9.01
F2.46

2+00

7.52
7.64
F0.12

6.61
8.08
F1.47

4+50

8.60
8.56
C0.04

6.32
8.85
F2.53

1+50

7.12
7.45
F0.33

6.68
7.92
F1.24

4+00

8.32
8.38
F0.06

6.18
8.70
F2.52

1+00

7.95
7.27
C0.68

7.08
7.76
F0.68

3+50

7.91
8.20
F0.29

6.16
8.54
F2.38

0+50

7.57
7.08
C0.49

6.47
7.61
F1.14

line Moreno
0+00 = N. Ely.

7.87
6.90
C0.97

6.17
7.46
F1.29

3+00

7.78
8.01
F0.23

6.61
8.38
F1.77

INDEXED
LHW
MAY 6 1952

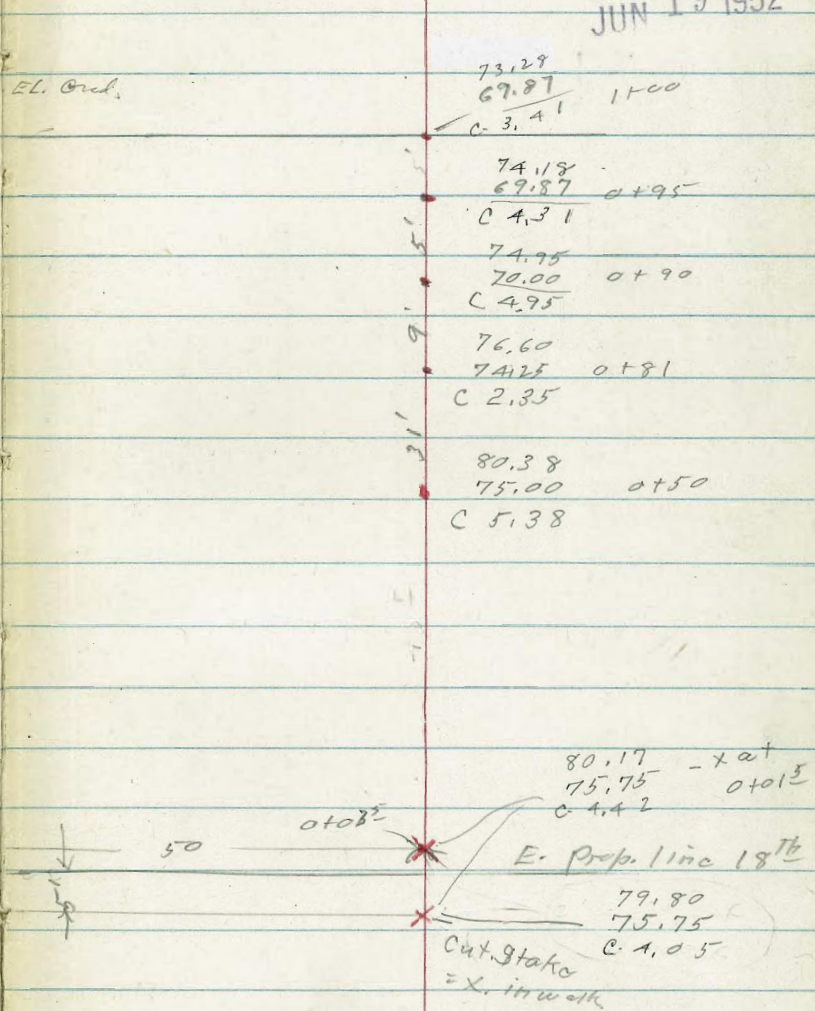
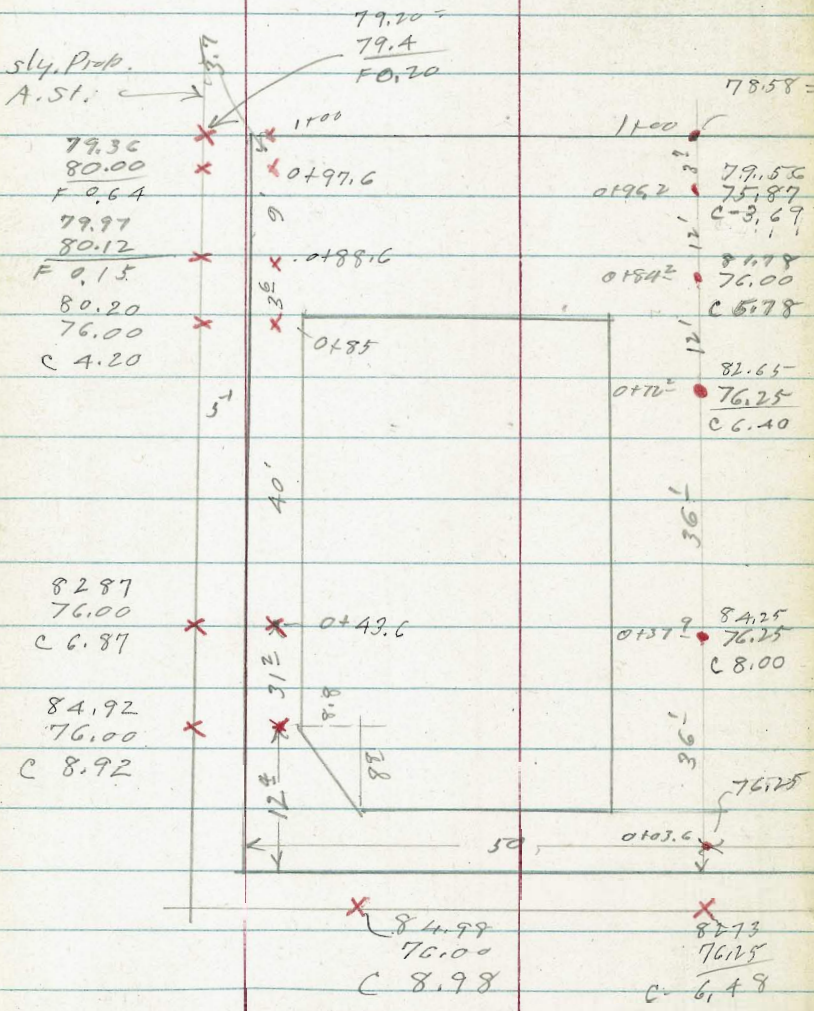
W.D. 2071C

6-9-52
C.H.S.
Boyer
Altman
Johns

80.28 T.P.

INDEXED
Law

JUN 19 1952



w.p.

sly. P.
A. S.I.

79
80
F 0.
79.
80.
F 0.
80.
76.
C 4.

828
76.0
C 6.8

84.9
76.0
C 8.9

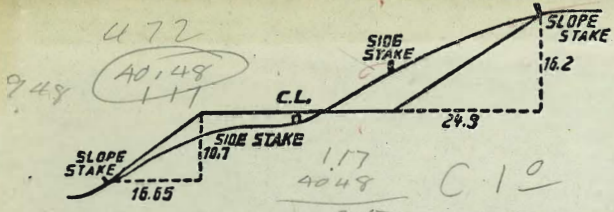
37.10
13.3
380

~~36~~
3.50
3
129.02
222
124.80 128.02
280
125.22

125.22
23.70
1.52

190
109
7
1520
1237 ✓ 28.02
522
12522 2.92

23.14
 2421
 735 56
 14
 366
 20.25 42
 30
 570
 59
 526
 4.56
 13
 4.69
 273
 96
 4.15
 29
 4.74
 513
 54
 4.55
 51.20
 49.64
 1.56
 508
 60
 4.84
 9.33
 -0.67
 51
 41
 441
 342 381
 6.58
 4663
 50
 4.01
 43
 3.58
 -245 23.31
 323
 5.68
 -5.92
 448
 831
 9.15
 1746
 873
 585
 37
 3.70
 59
 6.18
 3.13
 3.02
 .11
 11.70
 1.17
 10.53
 518
 416
 831
 915
 746
 877
 81
 4.80 4.95
 525 441
 475
 CORR
 CORR
 CORR



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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