

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 15 1965

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.053	.057	.061
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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W.O. 31611

Beardsley-22'nd Improvements

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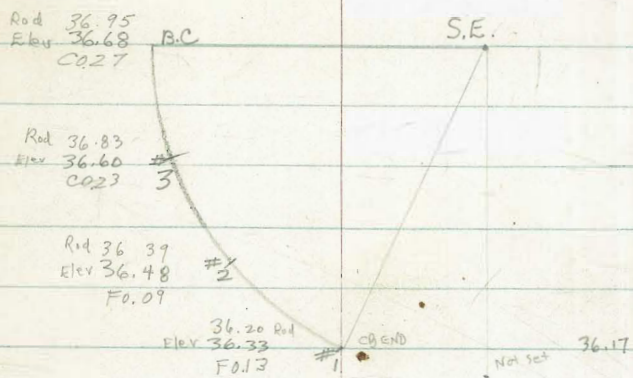
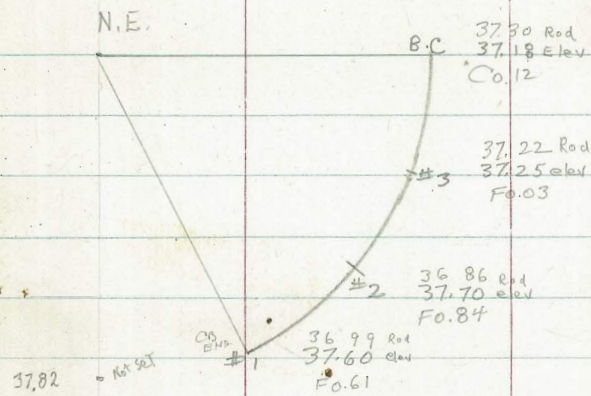
PL		LT	Julian to Commercial		LT		RT				
PL			CB.	♀	CB.	RT	PL	CB.	♀	CB.	PL
1+29.01			44.83 45.35 F 0.52				Alley AT P.L.			45.20 46.42 F 1.22	
1+20.36			44.82 45.25 F 0.43				Alley AT P.L.			44.67 46.23 F 1.56	
1+09.01		EXIST	45.01				1+40.36 Alley E.C.			44.97 46.15 F 1.18	
1+07.01					45.95 45.83 C 0.12		Alley B.C.			44.97 46.11 F 1.14	
0+94.01					45.66 45.68 EXIST.		1+38.36 RT only				
0+89.01		EXIST	44.68				C.B. E.C. = (177.54) ON LT. & STATING		45.27 45.71 F 0.44		
0+69.01		EXIST	44.68		45.49 EXIST.		#3 #2		44.55 43.61 F 0.06 45.24 45.52 F 0.28		
0+19.01		EXIST	44.50		44.97 EXIST.		#1		45.50		
0+00		EXIST Elev	44.37		44.73 Elev EXIST.		1+31.01 CB. B.C. LT.		44.76 45.38 F 0.62	45.27 Rod 46.04 Elev. F 0.77	
			NE/ly PLINE Julian (8 STATIONS)								
			46.04	Direct Elev. Road.	46.04		AM S/E Brass PLUG		Beardsley + Kearny		

LT.			RT.			LT.			RT.		
P.L.	CB.	E.	CB.	P.L.		P.L.	CB.	E.	CB.	P.L.	
2+59.60	46.54 46.64 F 0.10		47.76 47.49 C 0.27								
2+39.60	46.28 46.48 F 0.20		47.41 47.28 C 0.13								
2+19.60	46.32 46.27 C 0.05		47.23 47.07 C 0.16								
1+99.60	45.81 46.01 F 0.20		47.17 46.87 C 0.30								
1+77.54 CB. EC	45.27 45.71 F 0.44		46.52 46.66 F 0.14		3+22.45 P.L. LT.				check 46.99 47.00		
1+70.89 Mid. pt. Rt only			44.99 46.51 F 1.52		3+21.37				46.82 47.00 F 0.18		
1+64.24 CB. BC RT.			44.73 46.36 F 1.63		3+13.37				46.70 46.96 F 0.26		
1+62.36 Alley. B.C RT.			44.90 46.34 F 1.44		3+05.92 opp. P.L. on Irving ave				46.72 46.91 F 0.19		48.00 check 48.00 meet. exist.
Alley EC 1+60.36			44.90 Rod 46.34 Elev F 1.44		2+79.60				Red. 46.72 Elev 46.78 F 0.06		47.64 47.71 F 0.07

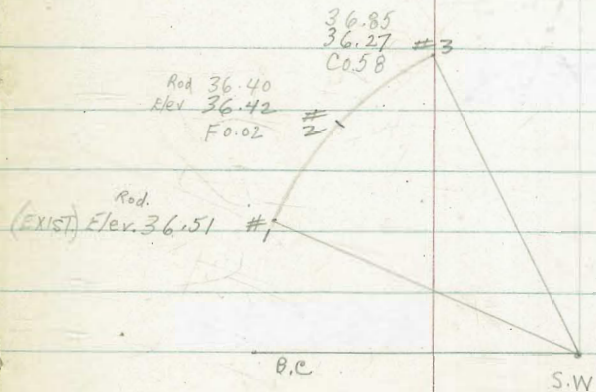
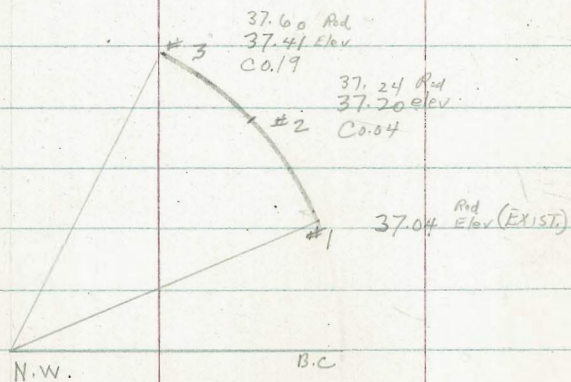
C.B. Returns:

Gresham - Thomas

THOMAS  
↑  
EAST



Gresham



Clark  
Shepherd  
Bruner  
Bryson

4-24-52

W.O. 31760

DWG. 9021-L

THOMAS AVE. IMPROVEMENTS - Gresham to Haines

Indexed 5.

	LT	RT	LT	RT	LT	RT	LT	RT			
	P.L.	C.B.	℄	C.B.	P.L.		P.L.	C.B.	℄	C.B.	P.L.
1+60	40.70 39.60 C1.10	39.53 39.60 Fo.07		39.20 39.10 Co.10	39.33 39.10 Co.23	3+80 <del>B.K.</del>	49.00 <del>49.00</del> 47.82 C1.18	47.55 47.82 Fo.27		47.12 47.32 Fo.20	47.34 48.00 Fo.66 47.32 Grade
1+40	40.14 38.92 C1.22	39.22 38.92 Co.30		38.61 38.42 Co.19	39.04 38.42 Co.62	3+60	47.92 48.14 Fo.22 47.07 Co.85	46.72 47.07 Fo.35		46.56 46.57 Fo.01	46.48 47.19 Fo.77 46.57 Fo.09
1+20	39.25 38.39 Co.86	38.46 38.39 Co.07		38.02 37.89 Co.13	37.91 37.89 Co.02	3+35	47.37 <del>47.08</del> Co.29 46.14 C1.23	45.39 46.14 Fo.75		45.57 45.64 Fo.07	45.98 46.18 Fo.20 45.64 Co.34
1+00	38.93 38.00 Co.93	38.00 38.00 Grade		37.63 37.50 Co.13	37.73 37.50 Co.23	3+10	46.50 <del>46.00</del> Co.50 45.20 C1.30	44.82 45.20 Fo.38		44.72 44.70 Co.02	45.25 45.17 <del>Co.08</del> 44.70 Co.53
0+80	38.69 37.77 B.K.C Co.92	37.62 37.77 Fo.15		37.18 37.27 Fo.09	37.35 37.27 Co.08	2+85	46.20 <del>47.94</del> C1.26 44.27 C1.93	43.93 44.27 Fo.34		43.87 43.77 Co.10	44.20 44.16 <del>Co.04</del> 43.77 Co.43
0+56.67	38.21 37.57 Co.64	37.34 37.57 Fo.23		36.36 37.07 Fo.71	37.01 37.07 Fo.06	2+60	44.58 <del>43.87</del> Co.71 43.34 C1.24	43.03 43.34 Fo.31		42.82 42.84 Fo.02	43.23 43.14 <del>Co.04</del> 42.84 Co.39
0+33.33	37.96 37.38 Co.58	37.38 37.38 Grade		36.81 36.88 Fo.07	36.90 36.88 Co.02	2+35	44.06 <del>42.80</del> C1.26 42.40 Elev C1.66	42.31 42.40 Fo.09		41.83 41.90 Fo.07	41.77 42.73 Fo.36 41.90 Fo.13
0+10-CA	Ad 38.02 BC Elev 37.18 For Returns Sec. B4 Co.84	37.30 37.18 Co.12		36.95 36.68 Co.27	36.75 Red Elev 36.68 Elev Co.07	2+10	42.59 41.74 Co.85 41.47 C1.12	41.29 41.47 Fo.18		40.98 40.97 Co.01	41.21 41.12 <del>Co.04</del> 40.97 Co.24
0+00 - E.A. Gresham						1+85	41.50 Red <del>40.07 Elev</del> Co.83 40.53 C0.97	40.16 40.53 Fo.37 40.09 40.42 Fo.33		39.65 40.03 Fo.38	40.50 Red 40.08 Elev <del>Co.39</del> Co.47
				1+82 W.S. LT							
		Direct Elev. Red.		44.15	H.C.P						
											℄ 199 Gresham + Red



LT

RT

P.L.

CB

L

CB

P.L.

5400	52.37 <sup>chk</sup> Rod 52.38	EXIST	51.93	51.96 <sup>chk</sup> 51.97 <sup>EXIST</sup>
W.L. HAINES				

4189.59 (4190) CB-BC	54.60 (OK) 57.93 C 2.67	51.95 57.93 C 0.02	51.54 51.43 C 0.11	53.68 51.43 C 2.25 51.43 (OK) C 2.25
----------------------------	-------------------------------	--------------------------	--------------------------	--

4468	53.25 57.34 E 1.97 51.11 C 2.14	51.23 51.11 C 0.12	5057 50.61 F 0.04	52.52 50.74 C 1.78 50.61 C 1.91
------	---	--------------------------	-------------------------	---

4446	51.40 50.76 C 0.64 50.29 C 1.11	50.51 50.29 C 0.22 50.51 50.17 C 0.34	49.12 49.78 F 0.66	50.31 50.06 C 0.25 49.78 C 0.53
------	---	--	--------------------------	---

4424	50.46 50.17 C 0.29 49.46 C 1.00	49.59 49.46 C 0.13	4899 48.96 C 0.03	49.25 49.37 F 0.12 4896 C 0.29
------	---	--------------------------	-------------------------	--

4402	40.76 Rod 47.59 Elev C 0.17 48.69 C 1.12	48.52 Rod 48.64 Elev F 0.12	48.09 48.14 F 0.05	48.05 Rod 48.68 Elev F 0.67 48.14 F 0.09
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THOMAS AVE. - HAINES TO INGRAHAM

DWG. 9020-L

Indexed

STA.	P.L.	CB.	℄	CB.	P.L.	P.L.	CB.	℄	CB.	P.L.	
1+60	56.70 55.12 C 1.58	55.06 55.12 Fo.06		54.46 54.62 Fo.16	54.30 54.62 Fo.32	3+40	54.40		54.30 54.40 Fo.10	53.91 53.90 Co.11	53.90
1+40	55.02	54.75 55.02 Fo.27		54.43 54.52 Fo.09	54.52	3+20	57.20 54.64 C 2.56		54.47 54.64 Fo.17	54.14 54.14 Grade	53.60 54.14 Fo.54
1+20	57.40 54.89 C 2.51	55.00 54.89 Co.11		54.55 54.39 Co.16	54.50 54.39 Co.11	3+00	54.82		54.68 54.82 Fo.14	54.39 54.32 Co.07	54.32
1+00	54.72	54.45 54.72 Fo.27		54.43 54.22 Co.21	54.22	2+80	57.50 54.97 C 2.53		55.00 54.97 Co.03	54.40 54.47 Fo.07	54.60 54.47 Co.13
0+82 W.S RT. (EXIST)											
0+80 B.C.	57.80 54.52 C 3.28	54.78 54.52 Co.26		54.23 54.02 Co.21	54.50 54.02 Co.48	2+60	55.08		55.14 55.08 Co.06	54.62 54.58 Co.04	54.58
0+55	57.20 54.25 C 2.95	54.06 54.25 Fo.19		53.95 53.75 Co.20	54.50 53.75 Co.75	2+40	55.26 55.13 C 0.13		54.93 55.16 Fo.23	54.67 54.66 Co.01	54.30 54.66 Fo.36
0+30	57.30 53.97 C 3.33	54.11 53.97 Co.14		53.60 53.47 Co.13	54.60 53.47 C 1.13	2+20	55.20		55.10 55.20 Fo.10	54.60 54.70 Fo.10	54.70
0+10	57.40 53.75 CB. BC. C 3.65	53.73 53.75 Fo.02		53.43 53.25 Co.18	54.29 Red 53.25 Elev C 1.04	2+00	56.80 55.21 C 1.59		54.97 55.21 Fo.24	54.69 54.71 Fo.02	54.30 Red 54.71 Elev Fo.41
0+00 = # 1	E.L. HAINES 53.74 CHK 53.74 EXIST				53.18 CHK 53.19 EXIST	1+80	W.S RT. 55.18 Elev		54.98 53.18 Fo.20	Red 54.05 Elev 54.68 Fo.63	54.68

Direct Elev. Red:

44.15 L.C.T. 9

INGRAHAM + Reed

	P.L.	CB	Q	CB	P.L.	P.L.	CB	Q	CB	P.L.	
# 2	49.93	49.16 <del>48.58</del> 49.43 elev F1.35 Fo.77		48.96 Rod <del>48.32</del> 49.10 elev Fo.78 Fo.14	49.10						
# 1	50.02	49.15 <del>48.52</del> 50.02 elev <del>F1.50</del> Fo.87		49.26 49.40 Fo.14	49.40						
4+89.8 CB8C	52.50 50.25 C2.25	50.11 50.25 Fo.14		49.54 49.75 Fo.21	50.70 49.75 C0.95						
4+65	53.00 51.11 C1.89	50.92 51.11 Fo.17		50.76 50.61 C0.15	51.40 50.61 C0.79						
4+40 E.V.C	55.00 51.97 C3.03	51.97 51.97 Grade		51.73 51.47 C0.26	52.30 51.47 C0.83						
4+20	52.62	52.51 52.62 Fo.11		52.21 52.12 C0.09	52.12					48.26 48.50 Fo.24	
4+07 WS LT	53.12 53.00 C0.12									48.66 48.60 C0.06	
4+00	55.50 53.19 C2.31	53.33 53.19 C0.14		52.58 52.69 Fo.11	52.90 52.69 C0.21						
3+80	53.67	53.76 53.67 C0.09		53.10 53.17 Fo.07	53.17						
3+60	56.60 Rod 54.08 Elev C2.52	53.91 54.08 Fo.17		53.60 53.58 C0.02	53.30 Rod 53.58 elev Fo.28						
						# 4 =	52.10 49.90 C2.20		50.23 Rod 49.59 49.90 elev Fo.34 C0.33	48.63 48.65 Fo.02	50.20 48.63 C1.55
						# 3	49.90	49.73 49.11 49.90 elev Fo.79 Fo.17	48.55 48.82 Fo.27	48.82	

THOMAS AVE. - INGRAHAM to JEWELL

DWG. 9019-L

Indexed

	P.L.	CR.	Q.	CR.	P.L.						
0+80		45.03 45.58 Fo.55		44.52 45.08 Fo.56		2+80	45.98 44.76 C1.22	45.00 44.76 C0.24		44.31 44.47 Fo.16	43.98 44.47 Fo.49
0+60	45.89 46.21 EVC Fo.32	45.78 46.21 Fo.43		45.17 45.71 Fo.54	45.04 45.71 Fo.67	2+50	45.51 44.49 C1.02	44.57 44.49 C0.08		44.05 44.09 Fo.04	43.08 44.09 F1.01
0+35	47.40 47.03 C0.37	46.61 47.03 Fo.42		46.22 46.33 Fo.11	46.47 46.33 C0.14	2+20	45.00 44.22 EVC C0.78	44.41 44.22 C0.19		43.98 43.72 C0.26	43.26 43.72 Fo.46
CR, B, C											
0+10	48.60 47.85 C1.25 C0.75 (0+00) = E. Side Ingraham	47.54 47.85 Fo.31		47.30 47.36 Fo.06	47.28 47.36 Fo.08	2+00		44.42 44.09 C0.33		43.63 43.59 C0.04	
# 1		47.75 48.20 Fo.45		47.52 47.70 Fo.18		1+80	45.33 44.07 C1.26	Box 44.07		43.73 43.57 C0.16	43.31 43.57 Fo.26
# 2		48.15 48.50 Fo.35		47.60 47.90 Fo.30		1+60		44.40 44.16 C0.24		43.14 43.66 Fo.52	
# 3		48.98 48.90 C0.18		47.53 48.00 Fo.47		1+40	45.39 44.36 C1.03	44.46 44.36 C0.10		43.41 43.86 Fo.45	43.15 43.86 Fo.71
# 4	49.00 49.00 Grade	48.64 Rod 49.00 Elev Fo.36		47.74 48.06 Fo.32	47.37 Rod 48.06 Elev Fo.69	1+20		44.62 44.66 Fo.04		43.58 44.16 Fo.58	
						1+00	45.80 Rod 45.06 Elev C0.74	44.87 45.06 Fo.19		44.21 Rod 44.56 Elev Fo.35	43.55 44.56 F1.01
		Direct Elev. Rod:		44.15 Elev. Q. L.C.T. Road	Ingraham						

LT.		RT.	
P.L.	C.B.	C.B.	P.L.
# 1. = W.L.	46.72	46.17 46.72	46.96 47.15
Jewel = 4+99.74		F0.55	F0.29
4+89.74	46.50 46.65	46.22 46.65	46.80 47.08
C.B. B.C.	F0.15	F0.43	F0.28
4+60	46.39 46.38	46.12 46.38	46.78 46.71
	C0.01	F0.26	F0.23
4+30	46.38 46.11	45.81 46.11	46.24 46.33
	C0.27	F0.30	F0.09
4+00	46.60 45.84	45.91 45.84	45.94 45.96
	C0.76	C0.07	F0.02
3+70	46.65 45.57	45.85 45.57	45.63 45.59
	C1.08	C0.28	C0.04
3+40	46.17 45.30	45.50 45.30	45.20 45.21
	C0.87	C0.20	F0.01
3+10	46.14 Rod 45.03 Elev	45.32 45.03	44.61 44.84
	C1.11	C0.29	F0.23
			F0.19

Clark 7/752  
Shepherd W.O. 2006  
Bryner  
Bryson

STAKE CBS. INGRAHAM, North Side

Indexed

11.

From S.L. THOMAS to N. Alley Line: As per DWG. (No. number)

81K 269

(In Fairlane (5-9-52)  
(6-10-52))

RT. ONLY

C.B. P.L.

Alley RT. PL.

48.24 Rod  
47.35 Elev  
C0.89

1424.83 Alley E.C.

46.48 Rod  
47.03 Elev  
F0.55

(4' CB rad.)

1420.83 = Alley B.C.

46.48 Rod  
47.00 Elev  
F0.52

0+85

47.04 Rod  
47.48 Elev  
F0.44

0+60

47.52 Rod  
47.83 Elev  
F0.31

0+35

47.73 Rod  
48.16 Elev  
F0.43

0+10 CB. E.C.  
For Ref. See pg 8

Elev 48.26  
48.50 48.50  
F0.24

(claimed dist. 81K=269.66)

0+00 = S.L. THOMAS

B.M. =

44.15 LGT E INGRAHAM

→ Reed

6" C.I. WATER-MAIN - THOMAS - INGRAHAM to Jewell

Indexed

2+58 EVC

44.17  
39.90  
C 4.27

2+18

43.73  
39.80  
C 3.93

1+78

43.75  
40.10  
C 3.65

1+38

44.40  
40.70  
C 3.70

1+31 (WS) - RT.

43.99  
44.74  
F 0.75

0+98 B.V.C

45.55  
41.90  
C 3.65

0+70 (W.S) LT

46.71  
47.13 Elev.  
F 0.42

0+68

46.62  
42.88  
C 3.74

0+38 - E.L. INGRAHAM

47.62 Rod  
43.80 Elev. Fla. Line  
C 3.82

0+00 = pt. of connection with  
10" C.I. MAIN 38' WEST OF E. LINE  
OF INGRAHAM

MEET EXIST 10" C.I. MAIN

2+81 (WS) RT

42.99  
44.00  
F 1.01

STAKES OFFSET 5' LT.

DIRECT. Elev. Rd: 44.15 L.C.T. E. Road + Ingraham

5+38 - W. LINE Jewell  
(2" below OFF)

46.78  
43.00  
C 3.78

4+98

46.23  
42.56  
C 3.67

4+58

46.23  
42.11  
C 4.12

4+18

45.94  
41.67  
C 4.27

3+78

45.65  
41.23  
C 4.42

3+38

45.29  
40.78  
C 4.51

2+98

44.50  
40.34  
C 4.16

6" C.I. WATER MAIN Reed - INGRAHAM to Jewell

Indexed

2+98 E.V.C	46.60 41.46 C 5.14	
2+58	44.38 39.14 C 5.24	
2+18	42.84 37.86 C 4.98	
2+13 (W.S) R	41.75 37.60 C 4.15	43.87 41.98 C 1.89
1+78	42.37 41.72 C 0.65	
1+45 (W.S) L	42.50 37.82 C 4.68	42.73 41.96 C 0.77
1+38 Arc (W.S) R	43.24 38.53 C 4.71	
1+04.66	43.73 39.27 C 4.46	
0+71.33	43.94 40.00 C 3.94	
0+38 - E.L. INGRAHAM		
0+00 = pt. connect with 10" C.I. Meet MAIN 38' W. OF E. LINE INGRAHAM Stubs offset 5' LT Grade to FL. Line		

5+38 meet EXIST 6" C.I. (meet)

5+04.66 57.13  
53.06  
C 4.07

4+71.33 56.38  
52.10  
C 4.28

4+38 55.38  
51.14  
C 4.24

4+03 54.18  
48.72  
C 5.46

3+68 52.20  
46.30  
C 5.90

3+33 49.10  
43.88  
C 5.22

Direct Elev. Rod: 44.15 = ELEV Reed & INGRAHAM



REED AVE - INGRAHAM TO JEWELL

DWG. 9022-L

Indexed

LT.		RT.			
STA.	P.L.	CB.	E.	CB.	P.L.
1+00	41.56 41.81 F0.25	42.12 41.81 C0.31		42.00 41.91 C0.09	42.60 41.91 C0.69
0+70	42.49 42.59 F0.10	43.20 42.59 C0.61		42.74 42.54 C0.20	42.19 42.54 F0.35
0+40	44.48 43.37 C 1.11	43.65 43.37 C0.28		43.28 43.17 C0.11	43.16 43.17 Grade
0+10	45.89 44.15 C 1.74	44.35 44.15 C0.20		43.88 43.80 C0.08	44.42 43.80 C0.62
# 1	44.40	44.35 44.40 F0.05		43.99 44.00 F0.01	44.00
# 2	44.63	44.61 44.63 F0.02		44.28 44.20 C0.08	44.20
# 3	44.82	44.74 44.82 F0.08		44.55 44.40 C0.15	44.40
# 4	44.95	44.85 44.95 F0.10		44.67 44.51 C0.16	44.51

(Returns)

LT.		RT.			
STA.	P.L.	CB.	E.	CA.	P.L.
2+88	46.11 47.29 F 1.18	47.29 47.29 Grade		49.58 47.64 C 1.94	51.17 47.64 C 3.53
2+60	43.84 45.33 F 1.49	45.34 45.33 C0.01		47.55 45.72 C 1.83	50.35 45.72 C 4.63
2+40		44.22 44.05 C0.17		45.61 44.46 C 1.15	
2+20	42.17 43.01 F0.84	43.17 43.01 C0.16		44.11 43.42 C0.69	47.22 43.42 C 3.80
2+00		42.28 42.21 C0.07		43.15 42.61 C0.54	
1+80	41.15 41.65 F0.50	41.80 41.65 C0.15		42.40 42.02 C0.38	45.32 42.02 C 3.30
1+60		41.25 41.33 F0.08		41.93 41.66 C0.27	
1+40	40.90 41.25 F0.35	41.16 41.25		41.52 41.52 C 1.79	43.31 41.52 C 1.79
1+20		41.11 41.41 F0.30		41.57 41.60 F0.03	

Direct Elev. Rod: 44.15 E L.C.T. Reed + Ingraham

LT.				RT.		LT.				RT.		
STA.	P.L.	CB.	£.	CB.	P.L.	STA.	P.L.	CB.	£.	CB.	P.L.	
4+60	58.06 57.50 C0.56	58.06 57.50 C0.56		57.04 57.69 F0.65	57.88 57.69 C0.19							
4+30	57.44 56.82 C0.62	56.93 56.82 C0.11		56.43 56.74 F0.51	57.31 56.94 C0.37							
												58.00 checks # 3 EXIST 58.00
4+00	55.77 55.13 B.V.C. C0.64	55.19 55.13 C0.06		55.42 55.32 C0.10	56.16 55.32 C0.84					57.81 57.90 F0.09	# 2	
3+72	53.67 53.17 C0.50	53.72 53.17 C0.55		54.67 53.40 C1.27	53.60 53.40 C2.20	4+99.95 w.L. Jewell	check 57.85 meet EXIST. 57.85			57.51 57.85 F0.34	# 1	
3+44	53.55 51.21 C2.34	52.47 51.21 C1.26		53.51 51.48 C2.03	54.30 51.48 C2.82							Ref. RT. only
3+16	47.94 Rod 49.25 Elev F 1.31	49.52 49.25 C0.27		51.99 49.56 C2.43	53.20 49.56 C3.64	4+75 CB. B.C. on RT.	58.25 57.63 C0.62	58.23 57.63 C0.60		57.32 57.78 F0.46		57.82 57.78 C0.04

Clark 5-13-52  
 Shephard W.O. 31931  
 Bryson

As per avg. 9054-L

Indexed

16

ALLEY IMP. B/K 20 FAIRMOUNT ADDTN.  
 UNIV. to Polk bet. Euclid + 47th

L.T.

R.T.

STA.	L.T.	RT.			
			2+20	346.78 346.53 C0.25	347.12 346.53 C0.59
0+70	346.31 345.38 C0.93	345.73 345.38 C0.35	2+00	346.56 346.80 346.72 E0.08 F0.16	346.94 346.72 C0.22
0+60	346.73 344.83 C1.90	345.52 344.83 C0.69	1+80	346.69 346.78 F0.09	346.97 346.78 C0.19
0+50	345.94 344.13 C1.81	345.37 344.13 C1.24	1+60	346.92 346.69 B.V.C. C0.23	347.20 346.69 C0.51
0+40	344.99 343.30 C1.69	344.29 343.30 C0.99	1+40	347.82 346.53 C1.29	346.78 346.53 C0.25
0+30	344.10 342.47 C1.63	344.03 342.47 C1.56	1+20	347.71 346.38 C1.33	346.80 346.38 C0.42
0+20	343.41 341.78 C1.63	343.13 341.79 C1.34	1+00	346.53 346.23 E.V.C. C0.30	346.59 346.23 C0.36
0+10	342.72 341.21 1/2 C1.51	342.56 341.25 C1.31	0+90	346.20 346.08 C0.12	346.32 346.08 C0.24
0+00 = N.L. UNIV.	meet EXIST. 340.80  cuts + fills to Fin. Grade	340.86	0+80	346.16 Red 345.80 Elev C0.36	346.14 Red 345.80 Elev C0.34

340.68 Direct Elev. Rod:

340.68 = Elev B.M. =

B.P. NW UNIV. & EUCLID

NOTE: From Sta. 2+20 to 4+75 NEW grades established.  
15 per office

(All stakes knocked-out)  
Reset 10-152  
4-10-52 LT

		LT	RT	RT	LT	RT
3+90	340.34 341.63 F 1.29	341.61 <del>340.34</del> 341.22 F 0.88 C 0.39	knocked out 335.94 341.22 F 5.28	335.94 341.63 F 5.69	5+40	341.77 342.22 F 0.45
3+70 (WS) RT only		341.24 <del>341.48</del> 341.51 F 0.03 F 0.27	knocked out 336.76 341.51 F 4.75	336.76 342.37 F 5.59	5+20	342.84 341.16 C 1.68
3+65	341.63 342.56 F 0.93			337.39 342.56 F 5.17	5+10	342.40 340.70 C 1.70
3+50		343.11 341.98 C 1.13	342.51 341.98 C 0.53		4+90	341.14 340.10 C 1.04
3+40	344.39 343.50 E.V.C C 0.89			340.64 343.50 F 2.86		
3+30		344.70 342.80 C 1.90	341.10 342.80 F 1.70			
3+20	345.42 344.21 C 1.21	345.42 343.30 F 2.12 C 1.74	knocked out 341.65 343.30 F 1.65	341.65 344.21 F 2.56	4+85 (WS) RT only	
3+00	345.38 344.82 C 0.56	345.38 344.30 C 1.08	344.26 344.30 F 0.04	344.26 344.82 F 0.56	4+84 1/2 Cleanout Box	341.45 339.78 C 1.72
2+80	345.74 345.36 C 0.38	345.74 345.20 C 0.54	345.13 345.20 F 0.07	345.13 345.36 F 0.23	4+70	340.95 340.08 C 0.87
2+60	346.04 343.80 C 0.24	346.04 343.80 C 0.24	346.40 343.80 C 0.60	346.40 345.80 C 0.60	4+50	339.92 340.22 F 0.30
2+40	346.13 346.20 F 0.07	346.13 346.23 F 0.12	346.29 346.25 C 0.04	346.29 346.20 C 0.09	4+30	338.00 340.60 F 2.60
					4+10	339.54 341.11 F 2.57
						340.51 340.94 F 2.40 F 0.43
						339.78 339.53 338.75 340.08 F 1.10 F 1.33 F 0.55
						339.78 339.78 339.66 339.78 F 0.12
						339.90 336.03 340.37 F 4.34 F 4.47
						340.26 339.49 340.65 F 7.16 F 0.39
						333.49 340.60 F 7.11
						334.92 341.11 F 6.19

L.T.

R.T.

5+99<sup>12</sup> - 342.38 meet  
S.L. POIK

5+80 342.62  
342.72  
F0.10

5+60 343.24 Ad  
342.70 FRY  
C0.54

342.71 Chk.  
342.72 meet EXIST

343.41  
342.91  
C0.50

343.12  
342.70  
C0.42

Clark 5-14-52  
Shepherd W.O. 20828  
Bryson

DRAIN - NILE & UNIVERSITY

LOT 4, BIR 193 CITY HTS.

As per FB# 2066  
+ DWG 9052-L

£

0+71.19 = E.C.

305.221 Meet EXIST.

0+61.41 P.O.C.

305.88  
305.45  
C 0.43

0+51.64 = R.C.

306.03  
305.68  
C 0.35

0+27.64

306.47  
306.21  
C 0.26

0+03.64  
E.T.

308.05 Rod  
306.75 Elev  
C 1.30

0+00 = Ch x END EXIST CONC 4'x4.5'  
DRAIN

MEET  
307.42 EXIST Elev.

Stubs set 4' at 2

Direct Elev. Rod:

322.15 Elev. B.M.  
S/W B.P. NILE & UNIV.

Indexed

Clark  
Shophard  
Bryson

5-15-52  
W.O. 31556

ALLEY IMP. BIK 20 City HTS

Redwood to Thorn

Indexed

LT.		RT		LT.		RT.
				2+90 W.S ON LT.	304.60 at prop. 304.05	305.04 304.56 C0.48
1+10.50	299.24 299.38 E.V.C. F0.14	300.81 299.58 C1.23		2+80.50 E.V.C.	304.36 F0.31	
0+90.50	299.07 298.81 C0.26	299.27 299.01 C0.26		2+70 Sew LAT. # 3 ON LT.	299.30 at prop. line (EXIST)	298.55
0+90 W.S ON RT.		299.57 at prop. line		2+60.50	304.64 303.87 C0.77	304.39 304.07 C0.32
0+70.5	298.16 298.30 F0.14	298.87 298.50 C0.37		2+40.50	303.95 303.34 C0.61	304.11 303.54 C0.57
0+70 SEW. LAT. # 2 ON RT.		298.89 298.89 298.30 at prop. C7.09		2+20.50 B.V.C.	302.89 302.75 C0.14	304.01 302.95 C1.06
0+50.5	298.63 297.87 C0.76	298.60 298.07 C0.53		1+93	302.18 301.91 C0.27	303.73 302.11 C1.62
0+40 W.S. ON RT.		297.84		1+65.50	301.36 301.06 C0.30	302.37 301.26 C1.11
0+30.5	298.39 Red 297.50 Elev B.V.C. C0.89	297.73 297.70 C0.03		1+38	299.75 300.22 F0.47	301.50 300.42 C1.08
0+20 SEWER Lat # 1 ON RT.		297.86 291.80 C6.86				
0+00 = N.L. Redwood	297.00 Elev EXIST.	297.20 Elev EXIST				

299.98 Direct Elev. Red: 299.98 a.p. S/W

Redwood & Vancouver

LT.		RT.		LT.		RT.
4170 SW. LAT. #4 ON RT.	308.48 303.00 C 5.48	308.48 303.30 AT P.L. C 5.18				check: 299.99 = 299.98 = B.P. SW RMCover + Redwood
4160.50 F.V.C.	308.19 307.90 C 0.29	308.30 308.00 C 0.30				
4140.5	307.78 307.65 C 0.13	308.11 307.80 C 0.31	6120.50 = S.L. Thorn	309.30 Meet		309.30
4120.5 B.V.C.	307.33 307.30 C 0.03	307.67 307.50 C 0.17	6100.50	310.55 309.12 C 1.43		312.68 309.14 C 3.54
3196.5	306.71 306.80 F 0.09	307.46 307.00 C 0.46	5172.50	309.99 308.88 C 1.11		310.02 308.91 C 1.11
3172.5	306.68 306.29 C 0.39	306.91 306.49 C 0.42	5144.50	308.98 308.67 C 0.35		309.15 308.68 C 0.47
3148.5	306.44 305.79 C 0.65	306.82 305.99 C 0.83	5116.50	309.03 308.39 C 0.64		309.93 308.46 C 1.47
3124.5	305.54 305.28 C 0.26	306.13 305.48 C 0.65	5115 W.S. ON LT.			
3100.5	304.73 304.78 F 0.05	305.72 304.98 C 0.74	4190. W.S. ON RT.	4188.50	308.44 308.14 C 0.30	309.28 308.23 C 1.05



Clark  
Shephard 5.19.52  
Bryson W.O. 20858

DRAIN "C" ST. EAST OF 294th ST.

Indexed

check 172.92 172.92 T<sub>p</sub> CB at  
EXIST. INlet

0+30.90 9' Cleanout Box  
Flan Line 173.47 Rod  
entering Box 168.49 Elev  
164.98

0+15.43 168.80

0+00-9' EXIST. Curb  
Inlet Flan-Line elev = 169.11 - meet

DIRECT ERU. Rod: 176.05 N/E B.P.  
2844 + 0"

Clark 5-20-52  
Shepherd No. 31710  
Byson

PUTERHAUGH - Pringle to Dead-End

Indexed

PL	LT	TRCB	£	Gutter	RT.	TRCB	LT	TRCB	£	RT.	TRCB
1+40		225.86 226.25 F0.39				227.00 227.20 F0.20					
1+20		227.21 227.40 F0.19				228.54 228.51 C0.03					
1+00		227.84 228.05 F0.21				CHK' / EXIST mod 229.37 229.34					
0+80											
0+60											
0+40											
0+20											
0+00 = N.W. LINE Pringle							1+50	225.03 225.31 F0.28			check 226.41 226.43 EXIST

225.29 = SW hit  
13'

PUTERHAUGH + Pringle



	LT	E	RT		LT	E	RT
5+18	44.92 44.14 C0.78		42.74 43.94 F1.20				
4+98	44.14 43.25 C0.89		41.86 43.15 F1.29			Check: 56.37 = 56.40 N/E B.P. Ebers & Pascadero	
4+78	42.70 42.42 C0.28		41.16 42.22 F1.06				
4+58	41.66 41.35 C0.31		40.87 41.15 F0.28	67.02.45 (4 ahead P.LINE)	48.55 meet	48.12 meet	
4+38	40.12 40.14 F0.02		39.56 39.94 F0.38				
4+18 = B.V.C	40.37 38.79 C1.58		39.30 38.59 C0.71	57.98.45 = w.L. Ebers	48.83 48.78 C0.65	48.26 47.98 C0.28	
3+98	37.95 37.37 C0.58		38.36 37.17 C1.19	57.78	48.51 46.95 C1.56	46.79 46.75 C0.04	
3+78	37.03 35.96 C1.07		37.44 35.76 C1.68	57.58	47.27 45.88 C1.39	45.27 45.68 F0.41	
3+58	35.29 34.52 C0.77		34.22 34.32 F0.10	57.38	45.68 44.95 C0.73	44.75 44.75 Grade	

Clark 6-4-52  
Shephard W.O. 31718  
Bruner  
Bryson

IMP. REX, SHILOH, WIGHTMAN

27

Indexed

INLET & 18" CONC. CULVERT REX AVE SHILOH to 52nd ST. LT. RT.

LT.

STAKES SET ON C.B. LINE 5' FROM EDGE

RT

Q

REX AVE

#2 319.01  
TR.C.C. 323.46  
F 4.45

#2 319.58  
323.03 TR.C.C.  
F 3.45

#2 319.23  
TR.C.C. 323.46  
F 4.23

#1 319.18  
323.03 TR.C.C.  
F 3.85

#2 319.01  
Gutter elev 322.63  
F 3.62

4.5' 319.58 #2  
322.20 = Elev Gutter  
F 2.62

#1 319.23  
Gutter elev 322.63  
F 3.40

319.18  
322.20 = Elev Gutter  
F 3.02

INVERT 316.58

INVERT 316.37

346.13'

350.31'

S.C.B. LINE Box

CB.A.C.

AL.C.B. LINE REX

CB.B.C.

SHILOH Rd.

Limit of Easement

Lot 9

15' EASEMENT

16' 18" CONC. PIPE

LOT LINE

TYPE-H  
CB INVERT

MEET EXIST. 18" CULVERT

319.12  
317.53 Elev. INVERT 18" Pipe  
C 1.59 AT END PIPE

Lot 10

5' Prop. LINE REX

S.C.B. LINE Box

SHILOH Rd.

CB. INLET / CULVERT ; DEAD-END REX

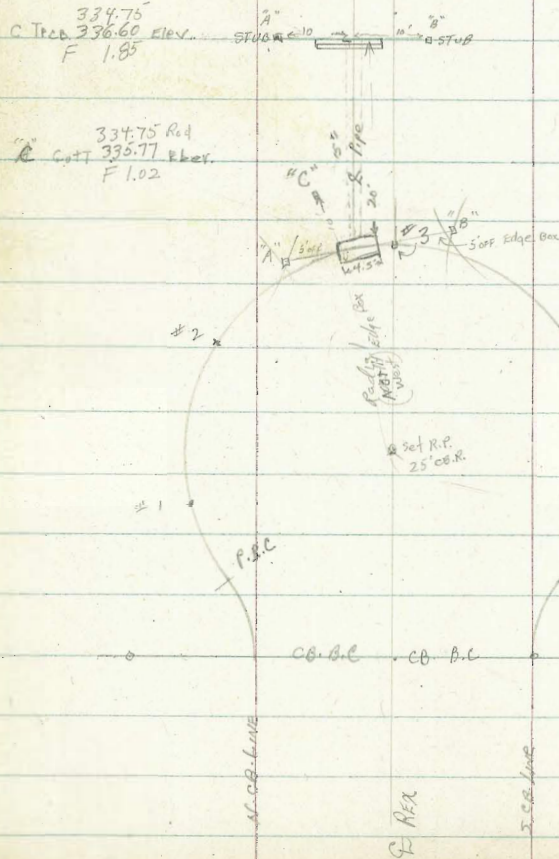
LT.

E

RT.

Q Rex

BOX



HEADWALL A 329.24  
326.00 Elev. Bot  
C 3.24 WALL

B 327.94  
328.60 Elev. INVERT  
C 1.94

328.94  
326.00 Elev  
C 2.94 WALL

Stubs knocked out (See opp. PAGE)

CB. INLET TYPE-A  
A 334.38  
335.77 = GUTT  
F 1.39  
A 334.38  
336.60 Elev  
F 2.22

B 333.82  
336.00 Elev  
C 2.18  
B 333.82  
336.60 Elev  
F 2.78

D 333.82  
335.77 = GUTT  
F 1.95

STUBS 5' RAIL  
OF N & S edge  
BOX

# 3 E. cul de sac (East)

336.60

Rough GRADE CB.

CB. Rough Grade

# 2

333.17  
337.00  
F 3.83

335.92  
337.35  
F 1.43

# 1

338.25

338.75

P.R.C.

338.87  
339.78  
F 0.91

340.36  
340.32  
C 8.04

CB. CC.

340.75  
341.12  
F 0.37

340.96  
341.62  
C 7.34

Rex

REX

Shiloh to 52nd.

29

LT.				RT.		LT.				RT.	
STA.	P.L.	C.B.	E.	C.B.	P.L.	STA.	P.L.	C.B.	E.	C.B.	P.L.
0+90 =	339.78 337.30	331.48 337.30		336.19 336.80	336.00 336.80	2+90 =	323.38 325.05	324.68 325.05		325.29 325.25	325.51 325.25
B.V.C.	C2.48	Co.18		F0.61	F0.80	B.V.C.	F1.67	F0.37		Co.04	Co.26
0+66.66	340.57 338.47	338.36 338.47		337.33 338.00	336.40 338.00	2+63.32	326.85	326.68 326.85		327.18 326.92	326.92
	C2.10	F0.11		F0.67	F1.60			F0.17		Co.26	
0+43.33	340.58 339.63	339.32 339.63		338.16 339.20	337.14 339.20	2+36.66	328.56 328.65	328.64 328.65		329.04 328.59	330.94 328.59
	Co.95	F0.31		F1.04	F2.06		F0.09	F0.01		Co.43	Co.2.35
0+20	343.45 340.80	340.80 340.80		338.90 340.40	337.55 340.40	2+10 =	330.88 330.45	330.81 330.45		330.79 330.25	332.38 330.25
	C2.65	Grade		F1.50	F2.85	B.V.C.	Co.43	Co.36		Co.54	Co.2.13
0+03	343.51 341.70	341.68 341.70		340.76 340.89	337.78 340.89	1+90	332.91 331.76	332.00 331.76		331.80 331.77	333.20 331.77
B.C.	C1.81	F0.02		F0.13	F3.11		C1.15	Co.24		Co.33	C1.73
# 1		341.91 341.90		341.07 340.90		1+70	333.01	333.39 333.01		332.98 332.67	332.64
		Co.01		Co.17				Co.38		Co.34	
# 2		342.39 342.25		341.26 340.80		1+50	337.37 334.18	334.75 334.18		333.95 333.75	334.33 333.75
		Co.14		Co.46			C3.19	Co.57		Co.20	Co.58
# 3 (ec)	343.51 342.63	342.63 Ad 342.63 Elev		341.13 340.42	337.78 340.42	1+30	335.28	335.98 335.28		334.98 334.81	334.81
C.B. Returns	Co.88	Grade		Co.71	F2.67			Co.70		Co.17	
(also: W. Line Shiloh Rd)						1+10	339.31 336.31	336.64 Ad 336.31 Elev		335.84 334.97 Ad 335.82 Elev	335.09 335.82
							Co.00	Co.33		Co.02	F0.73

Direct Elev. Rod: 346.61 Nail Pole  
Set 8 M. S. W. Rex - Shiloh 1/4 Cor. Arch 345.12

S/E Rex + Shiloh

LT				RT		LT				RT		
STA	P.L.	C.B.	E	C.B.	P.L.	STA	P.L.	C.B.	E	C.B.	P.L.	
4+70	328.88	329.79 328.88 C 0.91		329.41 329.38 C 0.03	329.38							
4+50	331.77 327.74 C 4.03	328.43 327.74 C 0.69		328.52 328.24 C 0.28	329.61 328.24 C 1.37							
4+30	326.45	327.31 326.45 C 0.86		327.01 326.95 C 0.06	326.95	# 1 - P.L. 5+89.63	333.00	332.70 333.00 F 0.30		332.87 333.48 F 0.61	333.48	
4+10	327.38 325.09 C 2.29	325.84 325.09 C 0.75		325.54 325.59 F 0.05	321.72 325.59 F 3.87	5+84.38 C.B. 0.0	332.58 332.87 F 0.29	332.66 332.87 F 0.21		332.74 333.37 F 0.63	333.20 333.37 F 0.17	
3+70	323.95	324.19 323.95 C 0.24		324.34 324.44 F 0.10	324.44	5+70	332.52	332.41 332.52 F 0.11		332.53 333.02 F 0.49	333.02	
3+70	320.08 323.27 F 3.19	323.62 323.27 C 0.35		323.76 323.73 C 0.03	318.45 323.73 F 5.28	5+50 K.V.C.	332.58 332.02 C 0.56	332.20 332.02 C 0.26		332.22 332.52 F 0.30	332.94 332.52 C 0.42	
3+50	323.03	Box Sec 27. chk. 323.03		Box. Ck 323.45 323.46	323.46	5+30	332.30 331.45 C 0.85	331.53 331.45 C 0.08		331.94 331.95 F 0.01	333.12 331.95 C 1.17	
3+30	319.89 323.25 F 3.36	322.10 323.25 F 1.15		323.37 323.65 F 0.28	321.70 323.65 F 1.95	5+10	330.74	331.23 330.74 C 0.49		331.49 331.24 C 0.25	331.24	
3+10	323.93	323.41 323.93 F 0.49		323.43 324.22 F 0.79	324.22	4+90	332.53 329.89 C 2.64	330.70 329.89 C 0.81		330.60 330.39 C 0.21	333.00 330.39 C 2.61	



SEWER LATERALS - REE - Shiloh to 52nd

NOTE: LOCATION OF SEW. LAT'S AS SHOWN ON SHEET-2 OF DWG # 9057-L 3L  
 CHANGED TO MEET EXIST CONDITIONS AT STA 0+90 LT + 2+40 LT

LT.		STA.	RT.		LT.		RT.	
P.L.	E		E	P.L.	STA.	E	P.L.	
		5+10	(16) 333.45 324.67E C 8.18	333.45 327.23 PL C 6.22				
		4+63	(17) 332.18 324.98 C 7.28	332.18 325.37 PL C 6.79				
328.54 321.55 PL C 6.99	328.54 321.69 (26) C 7.44	4+15						
324.42 318.95 PL C 5.47	324.42 318.00 (25) C 6.42	3+90						
323.14 320.05 PL C 3.09	323.14 318.11 (24) C 5.03	2+90						
329.07 324.00 PL C 5.07	329.07 323.50 (23) C 5.37	2+40 2+30 (See note p 3)						
333.05 326.76 PL C 6.29	333.05 326.30 (22) C 6.75	1+90						
		1+40	(19) 334.56 328.80E C 5.76	334.56 329.28 PL C 5.28				
		0+90	(20) 335.68 331.40 C 4.28	335.68 331.80 PL C 3.88				
340.75 332.80 PL C 7.95	340.75 332.40 (21) C 8.35	0+80			3+60 (15)	332.91 Rod 328.02 Ekv G C 4.95	332.91 328.42 PL C 4.55	

WATER LATERALS - REX, Shiloh to 52nd

Indexed

STA.	LT.	RT.	STA.	LT.	RT.
4710	326.05 325.09 elev. CB C0.96				
3780	324.58 323.58 C1.00	324.18 324.06 elev. CB C0.12			
2780	325.44 325.72 elev. CB F0.28				
1780	332.50 332.46 elev. CB C0.04				
1430		334.93 334.81 elev. CB C0.12	5765		332.35 332.89 Elev. CB F0.54
0480		337.01 337.31 elev. CB F0.30	5720		331.85 331.62 Elev. CB C0.23

SEWER LATERALS - REX - Shiloh to Dead-end.

WATER LATERALS - REX - Shiloh to D. END

Indexed

LT.	E	RT.
P.L.	STA.	P.L.
335.75 333.97 P.L. Elev C 1.81	4+75 #3	346.00 347.78 P.L. C 8.00
350.70 346.18 P.L. Elev C 4.52	2+00 #2	352.00 344.00 P.L. C 8.00
343.79 340.60 elev PL C 3.19	0+75 #1	349.02 339.00 P.L. C 10.02

LT.	RT.
4+60 LT 340.22 340.32 elev CB F 0.10	4+60 RT (IN) 352.80 Elev CB
2+10 LT 351.33 351.45 Elev CB F 0.12	2+60 RT (IN) 352.80 Elev CB
4+60 RT 349.89 350.28 Elev CB F 0.34	
0+85 LT 345.95 346.06 elev CB LT F 0.11	

REX - SHILOH to Cul-DE-SAC

LT.					RT.				
STA.	P.L.	CB	E	P.L.	STA.	P.L.	CB	E	P.L.
0+90	345.18 346.30 F1.12	346.17 346.30 F0.13		350.39 346.80 C3.59	2+80	352.40	352.49 352.40 C0.09		351.72 352.90 F0.98
0+65	345.05	344.68 345.05 F0.37		345.45 345.55 F0.10	2+60	351.73 352.30 F0.57	352.20 352.30 F0.10		351.70 352.80 F1.10
0+40	342.64 343.80 F1.16	343.61 343.80 F0.19		349.21 344.30 C4.91	2+40	352.06	352.19 352.06 C0.13		352.25 352.56 F0.31
0+20	342.84	342.68 342.84 F0.16		344.16 343.65 C0.51	2+20	351.32 351.69 F0.37	351.62 351.69 F0.07		352.20 352.19 C0.01
0+03 = CB, B.C Stox	341.54 342.02 F0.48	342.10 342.02 C0.08		343.22 343.09 C0.13	2+00	351.18	350.94 351.18 F0.24		351.48 351.68 F0.20
# 1	341.90	342.02 341.90 C0.12		343.33 342.95 C0.38	1+80	350.30 350.52 F0.22	350.58 350.52 C0.06		350.83 351.02 F0.19
# 2	341.50	341.18 341.50 F0.32		343.60 342.82 C0.78	1+60	349.73	349.88 349.73 C0.15		349.65 350.23 F0.58
# 3 = E.C Shiloh	341.15	340.97 341.15 F0.18		343.78 343.13 C0.65	1+40 = B.V.C	348.65 348.80 F0.15	348.76 348.80 F0.04		349.09 349.30 F0.21
CB. Returns					1+15	347.55	347.62 347.55 C0.07		348.08 348.05 C0.03
(0+00 = E.L.) Shiloh Rd.									
Direct Elev. Rod:		346.61 = Nail Pole			S/E REX - Shiloh				

STA.	P.L.	CB.	2	CB.	P.L.	STA.	HT.	CUL-DE-SAC	RT
4451.72	340.75 341.12	341.11 341.12		342.38 341.62	348.96 341.62		CB.		CB.
CB. B.C. Cul-de-Sac (See opp. p. 14)	F 0.37	F 0.01		C 0.76	C 7.34				
4440	342.32	342.96 342.32 C 0.64		344.05 342.82 C 1.23	342.82			⊥ #3 CB.	
Get 8m ON WALL (LT) ch- Elev. 344.36	347.64 344.38 C 3.26	345.80 344.38 C 1.42		345.82 344.88 C 0.94	348.72 344.88 C 3.84			33049 Rod 336.60 Elev F 0.11	
4100	340.70 346.44 C 2.26	347.94 346.44 C 1.50		347.32 346.94 C 0.38	350.63 346.94 C 3.69				
E.V.C.									
3480	351.16 348.27 C 2.89	349.58 348.27 C 1.31		349.25 348.77 C 0.48	351.70 348.77 C 2.93	#2	33644 337.00 F 0.56		33753 337.35 C 0.18
3460	349.77	350.41 349.77 C 0.64		350.55 350.27 C 0.28	350.27				
						#1	338.47 338.25 C 0.22		339.74 338.75 C 0.99
3440	352.22 350.93 C 1.29	351.45 350.93 C 0.52		350.94 351.43 F 0.49	354.20 351.43 C 2.77				
3420	351.76	351.99 351.76 C 0.23		351.79 352.26 F 0.47	352.26	P.R.C.	340.34 Rod 339.78 Elev C 0.56		341.12 Rod 340.32 Elev C 0.80
3400	351.82 Rod 352.25 Elev F 0.43	352.07 352.25 F 0.18		352.52 Rod 352.75 Elev F 0.23	354.51 Rod 352.75 Elev C 1.76				



SHILOH - WIGHTMAN TO REX

Indented

LT.		RT.		LT.		RT.			
P.L	CB	E	CB	P.L	P.L	CB	E	CB	P.L
Alley EC	350.45	350.12 350.45 Fo.33	351.37 350.95 Co.42	350.95	2+75.51 OK 343.51 342.63 CB, BC Co.88 For Ref. see Pg 29+34	342.63 342.63 GRADE-		343.78 343.13 Co.65	347.60 345.60 343.13 C2.17 C447
					2+55.4	344.00	344.05 344.00 Co.05	344.55 344.50 Co.05	344.50
1+28.70 = Alley B.C	350.46	350.12 350.46 Fo.34	351.37 350.96 Co.41	352.57 350.57 350.96 Fo.37 C1.61	2+30.4	346.31 344.31 345.71 F1.40 Co.60	345.50 345.71 F0.21	345.98 346.21 F0.23	349.50 347.50 346.21 C1.29 C3.29
1+10.4	350.88	350.59 350.88 Fo.29	351.88 351.38 Co.50	351.38	2+10.4	346.99	347.02 346.99 Co.03	347.00 347.49 Fo.41	347.49
0+90.4		351.65 349.65 351.17 F1.52 Co.48	350.71 351.17 Fo.46	352.91 350.97 351.67 Fo.76 C1.24	1+90.4	349.26 347.26 348.10 F0.84 C1.16	347.96 348.10 F0.14	348.08 348.60 F0.52	350.88 348.88 348.60 Co.78 C2.28
0+70.4	351.29	350.83 351.29 Fo.46	351.83 351.79 Co.04	351.79	1+70.4	349.05	348.58 349.05 F0.47	348.78 349.55 F0.77	349.55
0+50.40		352.03 350.03 351.25 F1.22 Co.78	350.96 351.25 Fo.29	352.80 350.80 351.75 Fo.95 C1.05	1+57.70 Alley B.C	351.14 349.14 349.80 F0.66 C1.34	349.75 349.80 F0.65 349.75 350.00 F0.25	349.50 350.30 F0.80 349.50 350.50 F1.00	351.56 349.56 350.30 F0.74 C1.26 350.50
0+30.40	351.04	350.99 351.04 Fo.05	351.53 351.54 Fo.01	351.54	Alley EC	350.00	351.11 350.06 Co.95	351.54 350.56 Co.98	350.56
0+05 = CB B.C		351.85 349.85 350.67 Fo.82 C1.18	351.21 Elev 350.67 Co.54	352.91 350.91 351.17 Fo.28 C1.74	1+47.70 Alley AT PL (NORTH) 1+32.70 Alley AT P.L. Line (SOUTH)	350.51	Rod 351.25 Elev 350.51 C 0.74	352.10 351.01 C 0.99	Rod Elev 351.01

For Ref. see page 41

0+00 = N.L. WIGHTMAN Direct Elev. Rod: 346.61 Nail-Pole Sp Shilo4 - Rex

WIGHTMAN - SHILOH to OGDEN  
SEWER - LAT'S.

STA.            LT.            E            RT.

1+55  
RT.

43  
Pipe  
See

0+75  
LT.

348.05

Rod  
Elev

347.66



WIGHTMAN - 52nd to Shiloh

Indexed

STA.	P.L.	CB.	ℓ.	CB.	P.L.	STA.	P.L.	CB.	ℓ.	CB.	P.L.
1+20	344.34	344.42 344.34 Co.08		345.71 344.84 Co.87	344.84	2+80	345.86 347.27 F1.41	347.13 347.27 F0.14		348.93 347.77 C1.16	350.54 347.77 C2.77
1+05	342.02 338.65 SEW. LAT #7 LT. C3.37	342.02 ℓ 338.00 C4.02				2+55	347.01	347.32 347.01 Co.31		348.52 347.51 C1.01	347.51
1+00	342.75 343.15 Fo.40	343.13 343.15 Fo.02		344.16 343.65 Co.51	347.51 343.65 C3.86	2+52	345.48 341.55 SEW. LAT. #8 LT. C3.93	345.48 ℓ 339.00 C6.48			
0+80	341.68	341.44 341.68 Fo.24		343.16 342.18 Co.98	342.18	2+30	347.07 346.75 Co.32	346.95 346.75 Co.20		348.57 347.25 C1.32	349.55 347.25 C2.30
0+60	339.39 339.93 B.V.C. Fo.54	339.83 339.93 Fo.10		340.62 340.43 Co.19	343.74 340.43 C3.31	2+05	346.49	346.89 346.49 Co.40		347.95 346.99 Co.96	346.99
0+30	337.19 337.09 Co.10	337.40 337.09 Co.31		338.05 337.66 Co.39	342.10 337.66 C4.44	1+80	346.00 346.23 E.V.C. Fo.23	346.52 346.23 Co.29		347.54 346.73 Co.81	349.93 346.73 C3.20
0+05.25	335.07 334.75 CB.BC Co.32	335.38 334.75 Co.63		338.07 335.25 C2.82	338.06 335.25 C2.81	1+78	SEW. LAT. #12 RT.			350.20 339.00 C11.20	350.20 341.55 C8.65
#1-pl	335.07 334.30 Co.77	Red Elev 335.04 334.30 Co.74		335.76 334.90 Co.86	338.06 334.90 C3.16	1+60	345.88	345.74 345.88 Fo.14		346.47 346.38 Co.09	346.38
0+00 = E.LINE WIGHTMAN						1+40	344.58 345.25 Fo.67	345.60 345.25 Co.35		345.99 345.75 Co.24	349.12 345.75 C3.37
	4.78	Direct Elev Rods		354.78 =	NAIL 3/4 Pole						WIGHTMAN + Shiloh

STA.	P.L.	CB.	E	CB.	P.L.						
4+55	349.09	349.15 349.09 C 0.06		349.77 349.59 C 0.18	349.59	# 3 = E.C SHILOP	351.21 350.67	351.21 350.67 C 0.54		351.49 351.18 C 0.31	351.18
4+50 SEW. LAT. #10 LT. #14 RT.	348.45 348.10 C 4.35	348.45 348.00 C 5.45	351.36 344.00 C 7.36	351.36 #14 344.60 C 6.76		# 2	351.05 350.60	351.05 350.60 C 0.45		351.67 351.11 C 0.56	351.11
4+30	347.00 348.83 F 1.83	348.81 348.83 F 0.02		349.14 349.33 F 0.19	350.26 349.33 C 0.93	# 1	351.24 350.50	351.24 350.50 C 0.74		352.57 351.00 C 1.57	351.00
4+05	348.57	348.63 348.57 C 0.06		348.76 349.07 F 0.31	349.07	5+86.82 = CB. BC.	351.85 350.47 C 1.38	351.33 350.47 C 0.86		352.70 350.97 C 1.73	353.13 350.97 C 2.16
3+80	345.49 348.31 F 2.82	348.13 348.31 F 0.18		348.78 348.81 F 0.03	349.02 348.81 C 0.21	6+80	350.39	351.07 350.39 C 0.68		351.81 350.89 C 0.92	350.89
3+55	348.05	347.63 348.05 F 0.42		348.66 348.55 C 0.11	348.55	5+55	350.13	350.83 350.13 C 0.70		351.93 350.63 C 1.30	350.63
3+52 SEW. LAT. #13 RT.			348.97 348.00 C 6.97	348.97 #13 348.50 C 5.47		5+30	351.02 349.87 C 1.15	350.35 349.87 C 0.48		350.99 350.37 C 0.62	352.45 350.37 C 2.08
3+30	344.88 347.79 F 2.91	346.77 347.79 F 1.02		348.50 348.29 C 0.21	350.31 348.29 C 2.02	5+05	349.61	350.21 349.61 C 0.60		350.50 350.11 C 0.39	350.11
3+05	347.53	347.33 347.53 F 0.20		348.74 348.03 C 0.71	348.03	4+80	350.16 349.35 C 0.71	349.84 Red 349.35 Elev C 0.49		350.15 349.85 C 0.30	351.21 349.85 C 1.36

WIGHTMAN - SHILOH to OGDEN

Indexed

STA.	LT.		E.	RT.	
	P.L.	CB.		CB.	P.L.
1+00	353.48	353.79 353.48 C 0.31		354.13 353.98 C 0.15	353.98
0+80 = B.V.C.	353.64 353.05 C 0.59	353.45 353.05 C 0.40		353.80 353.55 C 0.25	354.80 353.55 C 1.25
0+53	353.96 352.43 C 1.53	353.08 352.73 C 0.65		353.52 352.93 C 0.59	354.78 352.93 C 1.85
0+28	351.85	352.61 351.85 C 0.76		353.32 352.35 C 0.97	352.35
0+03 = BC WIGHTMAN	352.92 351.27 C 1.65	351.66 351.27 C 0.39		352.24 351.77 C 0.47	354.29 351.77 C 2.52
# 1 - prop	351.20	351.90 351.20 C 0.70		352.30 351.70 C 0.60	351.70
# 2	351.10	351.92 351.10 C 0.82		352.49 351.60 C 0.89	351.60
# 3 = BC Shiloh	351.17 Elev	351.51 351.17 C 0.34		352.17 351.67 C 0.50	351.67 Elev
(0+00 = F. Line) SHILOH					

STA.	P.L.	LT.		E.	RT.	
		CB.			CB.	P.L.
2+62.98 RT only					355.50 355.36 C 0.14	355.58 355.36 C 0.22
2+60 LT. only			354.99 354.79 C 0.20			
2+40	355.73 354.74 C 0.99	355.39 354.74 C 0.65			355.37 355.27 C 0.10	355.70 355.27 C 0.43
2+20		354.83 354.68 C 0.15			355.50 355.18 C 0.32	
2+00	355.48 354.62 C 0.86	354.77 354.62 C 0.15			355.26 355.12 C 0.14	355.93 355.12 C 0.81
1+80		354.67 354.53 C 0.14			354.91 355.03 F 0.12	
1+60	354.80 354.38 C 0.44	354.33 354.36 F 0.03			355.32 354.86 C 0.46	355.52 354.86 C 0.66
1+40		354.16 354.14 C 0.02			355.03 354.64 C 0.39	
1+20	354.57 353.85 C 0.72	354.12 353.85 C 0.27			354.60 354.35 C 0.25	354.96 354.35 C 0.61

Indersed

SEWER LATERALS - WIGHTMAN

SHILOH to OGDEN

STA.	P.L.	LT.	CB.	♀	CB.	P.L.	RT.
------	------	-----	-----	---	-----	------	-----

STA.	P.L.	LT.	♀	P.L.	RT.
------	------	-----	---	------	-----

355.75 Rod  
 2+72.30 = 354.83 Elev  
 CB. END C 0.92

355.05  
 354.83  
 C 0.22

355.43 Rod 355.50  
 355.39 elev 355.39  
 C 0.04 C 0.11

(#18)  
 1+55 LT.  
 set stub 5' bk P.L.

354.80	354.00
349.36 Elev	347.88
C 5.44	C 6.92

(#11)  
 0+78 LT.  
 set stub 5' bk P.L.

353.55	353.55
348.05 Elev	347.66
C 5.50	C 5.89

WIGHTMAN - SHILOH to OGDEN  
WATER-SERVICES

Indexed

44

WIGHTMAN - 52nd to SHILOH  
WATER-SERVICES

4+70 RT

4+60 LT.

3+60 RT.

2+75 LT.

1+85 RT.

1+15 LT

1+00 LT.

(set off SB)

(set off CB)

Clark 6-25-52  
Shepherd W.O. 31756  
BRUNER  
Bryson

WATER SERVICES-REED ST.

Indexed

45.

MISSION BLD. to CASS  
RT

STA.

LT.

RT

1+80

7.03 Rod  
6.41 T.P.C.B.  
C.O. 62

1+30

6.69 Rod  
5.99 T.P.C.B.  
C.O. 70

0+80

6.27 Rod  
5.57 T.P.C.B.  
C.O. 70

0+30

5.81 Rod  
5.15 T.P.C.B.  
C.O. 66

0+00 =  
ELY LINE BRAYFORD

1+87.08

0.17 Rod  
0.53 ELEV. T.P.C.B.  
F.O. 36

1+37.08

0.08 Rod  
0.46 Elev. T.P.C.B.  
F.O. 38

ELY LINE MISSION BLD.  
= 0+00

DIRECT ELEV. ROD:

6.38 N/E B.P.

BRAYFORD + THOMAS

C. Clark  
Shepherd  
Brewer  
Byrson  
Johns  
8-29-52  
W.O. 31756

REED AVE. - MISSION BLVD to

BAYARD

Indexed

L.T.				R.T.		L.T.				R.T.	
STA.	P.L.	C.B.	±	C.B.	P.L.	STA.	P.L.	C.B.	±	C.B.	P.L.
1+00 LT ±E only	1.14 0.42 C0.72	0.79 0.42 C0.37	-0.50	-1.30 GUTT		Alley AT P.L. N. EAST.		0.18 1.07 F0.89			
0+70-EC EASEMENT RT. ONLY				-1.33 GUTT	-0.79	Alley AT P.L. N. WEST.		1.30 0.99 C0.31			
0+84 LT ±E only = ±E DRAINAGE SECT.	1.20 0.50 C0.70	0.87 0.50 C0.37	-0.60			Alley E.C.	0.61	0.52 0.61 F0.09			
0+78-PC EASEMENT RT. ONLY Most Exist.				-1.33 GUTT	-0.74 EXIST	(Appor. Error) (2+06.08) 2+05.08 B.C. Alley LT.	0.57	0.52 0.57 F0.05			
0+50	1.19 0.83 C0.36	1.09 0.83 C0.26	-0.11	0.12 -0.12 C0.24	+0.94 -0.12 C1.06	2+00	1.44 0.55 C0.89	0.42 0.55 F0.13	+0.02	-0.85 GUTT	
0+20 GUTT ±E only	TPCB Elev 1.15 Elev 1.14 C0.01	GUTT 0.38	0.30	GUTT -0.17	0.66 0.55 (TPCB Elev) C0.11	1+80	1.42 0.52 C0.90	0.66 0.52 C0.14	-0.06	-0.97 GUTT	
0+00-EC	chk. 1.34 Rod 1.34 elev		0.78	0.69 Rod 0.79 Rod 1.00 Elev F0.21 F0.31	knocked-out	1+60	1.35 0.49 C0.86	0.54 0.49 C0.05	-0.12	-1.07 GUTT	
#1 S.E. Ret.				Rod Elev 1.04 EXIST		1+40	1.27 0.47 C0.80	0.43 0.47 F0.04	-0.18	-1.17 GUTT	
(0+00 = E. Line) MISSION BLVD.)						1+20	1.34 Rod 0.45 Elev C0.89	0.51 0.45 C0.06	-0.24	-1.27 GUTT	
	6.38 Direct Elev. Rod			6.38	N.E. B.P. Bayard Thomas						

REED AVE. - MISSION Blvd. to Bayard

STA.	P.L.	LT. CB.	±	RT. CB.	P.L.
3+50		GUTT. 1.05		0.88 GUTT.	
3+20		GUTT 0.50	+0.90	0.30 GUTT.	
3+00. ♀ only		GUTT. 0.29	+0.62	-0.05 GUTT	
2+89.42		0.72 <sup>Red</sup> EXIST			
MEET EXIST (PLAN) CB. LT. (2+85 NEW CB END. MEET EXIST)					
2+80		0.70 0.88 F0.18	0.54 0.88 F0.34	+0.46	-0.30 GUTT.
2+50	LT. ♀ only	0.54 <sup>Red</sup> 0.75 <sup>EXIST</sup> F0.21	0.18 <del>0.18</del> 0.75 F0.64 F0.57	+0.28	-0.52 GUTT.
2+29.08	BC alley LT	0.67	0.03 0.67 F0.64		
ALLEY E.C			0.03 0.67 F0.64		
(2+25 RT. only)					-0.68 GUTTER

	GUTTER
ALLEY BIK. 7 (REED ST. ON RT.)	
B.C.	1.45
E.C	1.71
P.L.	2.19
P.Line	1.96
E.C	1.36
3+57.08 P.C. Alley	1.03 <sup>Red</sup> EXIST
0+00 = E.L. INS MISSION Blvd	



REED AVE. - BAYARD to CASS

Indexed

STA.	P.L.	CB.	±	G.U.T.T.
1+50	6.84 6.15 C0.69	6.21 6.15 C0.06		
1+30 RT. only				4.80
1+25	5.95	6.05 5.95 C0.10		
1+00	6.31 5.74 C0.57	5.77 5.74 C0.03		4.53
0+75	5.53	5.60 5.53 C0.07		4.31
0+60	TP. 5.45 <sup>RD</sup> CB 5.40 Elev C0.05	G.U.T.T. 4.73	4.95	4.17
0+50	6.49 5.32 C1.17	5.25 5.32 F0.07		
0+30 RT. only				4.09
0+25	5.11			
0+20 CB	TP. 5.15 Rd → 5.07 Elev C0.08	5.15 5.07 C0.08		
0+20 G.U.T.T.		G.U.T.T. 4.40	4.76	
0+00	4.90 TP. CD EXIST			
(0+00 = E. LINE) BAYARD)				4.01

STA.	P.L.	CB.	±	G.U.T.T.
3+75	8.04	8.02 8.04 F0.02		
3+50	8.52 7.83 C0.69	7.75 7.83 F0.08		
3+25	7.62	7.48 7.62 F0.14		
3+00	8.30 7.71 C0.89	7.31 7.41 F0.10		
2+75	7.20	7.21 7.20 C0.01		
2+50	7.91 6.99 C0.92	6.97 6.99 F0.02		
2+25	6.78	6.93 6.78 C0.15		
2+00	7.28 6.57 C0.71	6.68 6.57 C0.11		
1+75	6.36	6.35 6.36 F0.01		5.07

DIRECT Elev. Rod:

6.38 NE B.P THOMAS +

BAYARD

G.U.T.T. GRASSES RAISED IN

REED AVE. - BAYARD to CASS. (CONT)

Indexed

STA.	P.L.	LT. C.B.	♀	GUTT	STA.	P.L.	LT. C.B.	♀	GUTT
							ALLEY BIK 1 (Reed)		
± / EXIST	9.07 chad. 9.08 EXIST			7.79 EXIST	1+55 = B.C				5.07
4+93.25 = C.B. B.C. LT.	9.03	9.25 9.03 C.O. 22			E.C.				5.17
4+79.25 RT WY				7.57	P.L.				5.81
4+75	8.87	8.48 8.87 Fo. 39							
4+50	9.02 8.66 C.O. 36	8.12 8.66 Fo. 54			P. Line				5.71
4+25	8.45	8.40 8.45 Fo. 05			F.C				5.14
4+00	8.85 8.24 C.O. 61	8.32 8.24 C.O. 08			(Alley BIK 1) ON RT. B.C. 1+30				4.80
					0+00 = F. LINE BAYARD				

Clark  
Shepherd  
Bruner  
Johns  
9-5-52  
W.O. 3/178

LANGLEY: K ST. to  
ISLAND

15 per DWG. 9304 L

Indexed

STA.	P.L.	LT	CB	E	CB	RT	P.L.	STA.	P.L.	LT	CB	E	CB	RT	P.L.
								2175							
0+50	107.33 103.10 C4.23		102.78 103.10 Fo.32												
								2+50	129.63 127.50 C2.13						
0+25			99.60 100.05 Fo.45												
								2+25							
CB B.C 0+06	100.03 97.73 C2.30		97.54 97.73 Fo.19					2+00	122.39 121.40 C0.99						
#1			96.95 97.36 Fo.41					1+75							
#2			96.94 97.12 Fo.18					1+50	116.10 115.30 C0.80						
#3			97.23 97.08 C0.15					1+25							
#4 EC K ST. EXIST.	97.19							1+00	111.72 109.20 C2.52						
(0+00 = N. Line K ST.)								0+75							

B.M. Direct Elev. 800:

102.99 = N.W. B. P. 2746 ST.  
4" K"

105.96 Red  
106.15 Elev  
Fo.19

104.65  
103.15  
Fo.50

STA.	LT		E	RT	
	P.L.	C.B.		C.B.	P.L.
4470	126.87 125.75 C1.12	125.40 125.75 Fo.35		124.55 124.75 Fo.20	125.44 124.75 C0.69
4445	129.18	128.55 128.18 Fo.63		127.77 128.18 Fo.41	128.18
E.V.C. 4420	133.03 132.60 C0.43	132.26 132.60 Fo.34		134.09 131.60 Fo.51	131.35 131.60 Fo.25
4400	135.27 134.80 C0.47	134.29 134.80 Fo.51		133.05 133.80 Fo.75	133.82 133.80 C0.02
3480	136.63 135.60 C1.03	135.12 135.60 Fo.48		134.36 134.60 Fo.24	134.38 134.60 Fo.22
3460	136.55 135.80 C0.75	135.32 135.80 Fo.48		134.38 134.80 Fo.42	135.31 134.80 C0.51
3440	136.55 135.70 C0.85	135.31 135.70 Fo.39		134.55 134.70 Fo.15	135.20 134.70 C0.50
3420	135.65 135.00 C0.65	134.65 135.00 Fo.35		133.43 134.00 Fo.57	133.94 134.00 Fo.06
B.V.C. 3400	134.05 Rod 133.60 Elev C0.45	132.87 133.60 Fo.73		132.07 132.60 Fo.53	132.89 132.60 C0.29

STA.	LT		E	RT	
	P.L.	C.B.		C.B.	P.L.
6450	107.42 105.40 C2.02	105.46 105.40 C0.06		104.21 104.60 Fo.39	104.00 104.60 Fo.60
6440 LT only	106.06 105.75 C0.31	105.69 105.75 Fo.06			
6430	106.26 106.26 Grade	106.15 106.26 Fo.11		105.10 105.35 Fo.25	104.23 105.35 F1.12
6410	108.56 107.66 C0.90	107.51 107.66 Fo.15		106.59 106.73 Fo.14	105.71 106.73 F1.02
5490	110.80 109.59 C1.21	109.16 109.59 Fo.43		108.36 108.60 Fo.24	107.70 108.60 Fo.90
B.V.C. 5470	113.42 112.06 C1.36	111.62 112.06 Fo.44		110.74 111.06 Fo.32	110.81 111.06 Fo.25
5445	115.49	115.01 115.49 Fo.48		113.98 114.49 Fo.51	114.49
5420	120.91 Rod 118.91 Elev C2.00	118.81 118.91 Fo.10		117.46 117.91 Fo.45	118.18 117.91 C0.27
4495	122.33	122.04 122.33 Fo.29		120.99 121.33 Fo.34	121.33

Indusod

WATER METERS  
LANGLEY ST: K to ISLAND

STA.	P.L.	LT	CB.	♀	CB.	RT.	P.L.	STA.	LT	♀	RT.
								5+85	LT		110.02 elev CB.
								5+55	RT.		113.13 elev CB.
								5+20	LT.		118.91 elev CB.
								4+90	RT.		122.01 elev CB.
								3+40	RT.		134.70 elev CB.
#3	not set							1+65	RT.		116.13 elev CB.
#2	not set							1+30	LT.		112.86 elev CB.
#1			104.67		103.47			1+20	RT.		111.86 elev CB.
			105.12		103.80						
			F0.45		F0.33						
CB.B.C	108.08		104.77		103.48		103.72				
(+74.83 LT)	105.05		105.05		104.00		104.00				
(+74.95 RT)	C 3.03.		F0.28		F0.52		F0.28				
								0+85	LT		107.37 elev CB.
LT			105.24								
6+60 only	105.10	Rod elev	105.10								
			C0.14								
											(0+00 = N. line K)

check: 98.01 98.03 =

S.W. B.P. Island 42844

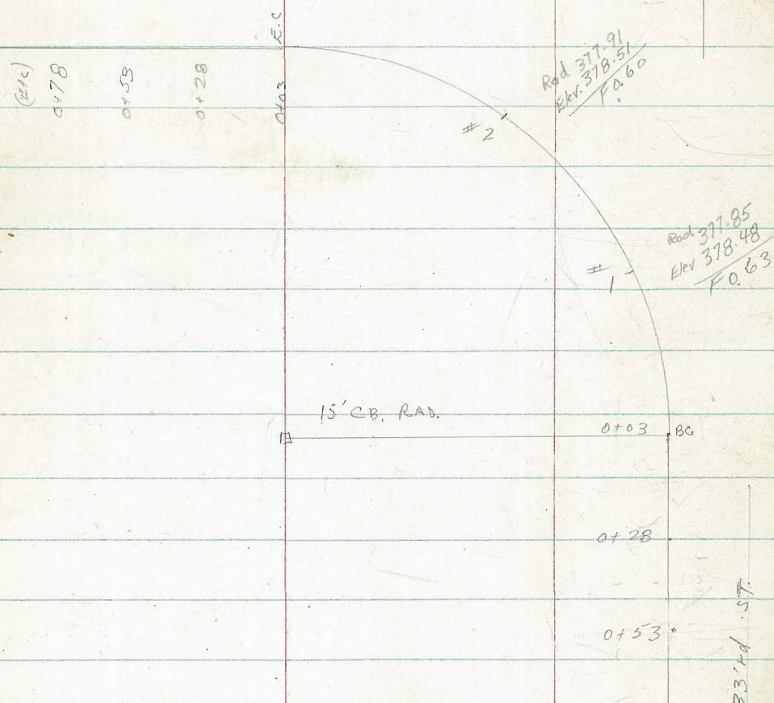
C/ark  
Shepherd  
Brunner  
Parkins

N.O 20008  
10-6-52

CBS. & Return S/W  
MEADE & 33rd ST.

*Indexed*

MEADE



STA.	CB	Notes	Got. EXIST. S. Line Meade	Elev. TP CB
(MEET EXIST. CB)				
1+28	377.93 Rod		377.88	377.93 378.38 F.O. 45
1+03	377.99 378.42 F.O. 24		377.94	377.99 378.44 F.O. 45
0+78	378.18 378.45 F.O. 27	↑ (according to grade sheet) CAN'T USE THIS gradient Does NOT give sufficient offset.	378.05	378.18 378.55 F.O. 31
0+53	378.14 378.48 F.O. 34		378.05	378.14 378.55 F.O. 41
0+28	378.14 378.51 F.O. 37		378.05	378.14 378.55 F.O. 41
0+03 = BC	378.05 Rod 378.54 Elev F.O. 49		378.04 Elev	378.05 378.54 F.O. 49

CBS. MEADE - 33rd South to EXIST. CB.  
LT. only

Note: It was desired to hold to 0.50' CB. Face on Meade

Got. EXIST. S. Line Meade

Elev. TP CB

USE THESE grades ↓

B.M. DIRECT Elev. P.O.:

378.56 N/E TCT. 33rd PL Meade

CBS. 33rd - made west to exist CB

54

STA.

RT. only  
CB.

Note: IT was desired to hold to  
0.67' CB Fc on west  
side 33rd

(Meet EXIST. CB)

1+53

~~377.02~~  
Meet → 377.69  
CB.

1+28

377.16  
377.82  
Fo.66

1+03

377.42  
377.95  
Fo.53

0+78

377.46  
378.08  
Fo.62

0+53

377.68  
378.21  
Fo.53

0+28

377.71  
378.33  
Fo.62

0+03 = F.C.

377.88  
378.46  
Fo.58

Clark  
Shepard  
Bruner  
Perkins  
W.O. 31899  
10-8-52

PYTHON ST. CB. GRADES  
LOGAN to "T" STREET

Indexed

LT.

RT.

STA.	P.L.	CB.	±	CB.	P.L.	STA.	P.L.	CB.	±	CB.	P.L.
1+40		110.97 110.16 Co.81		110.93 110.66 Co.27		3+40		107.70 107.69 Co.01		108.21 108.19 Co.02	
1+20		110.63 110.28 Co.35		111.04 110.78 Co.26		3+20 = E. side of 1st pipe.		107.49		107.99	
1+00 = B.V.C.		110.54 110.30 Co.24		110.98 110.80 Co.18		3+00		107.16 107.76 Fo.30		107.52 107.96 Fo.44	
0+77.5		110.45 110.23 Co.22		110.92 110.73 Co.19		2+80		107.38 107.61 Fo.23		107.77 108.11 Fo.34	
0+55		110.20 110.15 Co.05		110.73 110.65 Co.08		2+60 = B.V.C.		107.55 107.93 Fo.38		108.02 108.43 Fo.41	
0+32.5		109.98 110.08 Fo.10		110.64 110.58 Co.06		2+33.3		107.98 108.48 Fo.50		108.21 108.98 Fo.77	
0+10		109.65 110.00 Fo.35		110.49 110.50 Fo.01		2+06.6		108.44 109.03 Fo.59		108.79 109.53 Fo.74	
0+00 = E.C. caps at Python.		109.86 (Elev) EXIST CB		110.69 (Elev EXIST CB)		1+80 = E.C.		109.65 109.58 Co.07		109.44 110.08 Fo.64	
(0+00 = N. line LOGAN)						1+60		110.44 Rod. 109.93 elev. Co.51		110.03 110.43 Fo.40	
B.M.		118.77	Dir. T. Elev. Rod.	118.77	N/W.B.P. LOGAN	1+47.4					

Note: All "underground" & "Rough Grade" STAKES set previous to this date by Osborne.



PYTHON ST. (CONT.)

LT.					RT.				
STA.	P.L.	CB.	Σ	P.L.	STA.	P.L.	CB.	Σ	P.L.
5+20 = NYC		111.82 111.54 Co.28			112.11 112.04 Co.07				
5+00		111.45 111.38 Co.07			111.55 111.88 Fo.33				
4+80		110.98 111.13 Fo.15			110.98 111.63 Fo.65				
4+60		110.71 110.80 Fo.09			110.91 111.30 Fo.39				
4+40		110.31 110.38 Fo.07			110.61 110.88 Fo.27	# 2.0 P.L. Python	115.50 112.01 C.349		115.23 112.73 - P.L. Python C.250
4+20		109.98 109.88 Co.10			110.08 110.38 Fo.30	# 1.0 P.L. Python	111.77 111.99 Fo.22		112.56 112.55 Co.01
4+00		109.35 109.27 Co.08			109.48 109.77 Fo.29		5+90.25 = CB. BC 111.98 111.93 Co.05		112.36 112.43 Fo.07
3+80		108.84 108.63 Co.21			108.70 109.13 Fo.43		5+66.8 112.20 111.80 Co.40		112.43 112.30 Co.13
3+60		108.25 Rod 108.07 Elev Co.18			108.17 108.57 Fo.40		5+43.4 111.89 Rod 111.67 Elev Co.22		112.16 112.17 Fo.01

PYNCHON ST.

T<sup>h</sup> ST. to OCEAN VIEW

Indexed

STA.	LT.	P.L.	C.B.	E	RT.	P.L.
1+60 = BVC			105.95 106.12 Fo.17			106.99 106.62 Co.37
1+35			106.77 107.02 Fo.25			107.76 107.52 Co.24
1+10			107.63 107.91 Fa.28			108.56 108.41 Co.15
0+85			108.68 108.81 Fa.13			108.80 109.31 Fa.51
0+60			108.88 109.71 Fa.83			110.12 110.21 Fa.09
0+35			110.37 110.60 Fa.23			111.23 111.10 Co.13
0+10 = CB.B.C			111.84 111.50 Co.34			112.12 112.00 Co.12
# 1 - P.L. 17'			111.98 111.77 Co.21			112.36 112.36 GRADE
# 2 - P.L. Pynchon			114.31 Rod 111.91 Elev C 2.40			114.96 112.72 C 2.24
0+00 = N.L. T <sup>h</sup> ST.						

B.M

118.77 Direct. Elev. Rod.

118.77 NW B.P. Logan & 97' 4"

STA.	LT.	P.L.	C.B.	E	RT.	P.L.
3+45			101.25 102.52 F 1.27			102.80 103.02 Fo.22
3+20 = EVC			102.70 102.69 Co.01			102.86 <del>103.86</del> 103.19 Co.67 Fo.33
3+00			102.94 102.87 Co.07			103.17 103.37 Fa.20
2+80			103.18 103.17 Co.07			103.74 103.61 Co.13
2+60			103.46 103.43 Co.03			103.48 103.93 Fa.45
2+40			103.93 103.83 Co.10			104.35 104.33 Co.02
2+20			104.43 104.29 Co.14			105.06 104.79 Co.27
2+00			104.82 104.83 Fo.01			105.65 105.33 Co.32
1+80			105.55 Rod 105.44 Elev Co.11			106.09 105.94 Co.15

STA.	LT. P.L.	CB.	E	CB.	RT. P.L.	STA.	LT. P.L.	CB.	E	CB.	RT. P.L.
5770		101.01 100.94 Co.07		101.75 101.44 Co.31					Checks	115.91	=115.39= NAIL IN Pole S/W "T" + Pynchon F.B. 2037-54
5445		101.37 101.12 Co.25		102.09 101.62 Co.47							
5720		101.69 101.29 Co.40		102.04 101.79 Co.25							
4795		101.83 101.47 Co.36		102.11 101.97 Co.14							
4770		101.98 101.64 Co.34		102.17 102.14 Co.03							
4445		102.05 101.82 Co.23		102.30 102.32 Fo.02							
4420		101.96 101.99 Fo.03		102.70 102.49 Co.21		# 2 - PL Pynchon	100.18 100.33 Fo.15			101.99 101.79 Co.20	
3795		102.23 102.17 Co.06		102.69 102.67 Co.02		# 1 - PL OCEAN VIEW	100.16 100.60 Fo.44			101.10 101.41 Fo.31	
3770		102.27 Rd 102.34 Elev Fo.07		102.56 102.84 Fo.28		5790 = CB B.C.	100.53 Rd 100.80 Elev Fo.27			101.16 101.30 Fo.14	

Clark  
Shepherd  
BRUNER  
PERKINS  
W.O. 31903  
10-10-52

ALLEY BIK A' - BELMONT SUB.  
EL CAJON to Talley BET. EUCLID & 48TH

Indexed

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STA.	LT.	RT.	STA.	LT.	E	RT.
			3+25	358.76 358.41 C 0.35		357.30 358.71 C 0.59
1+50	350.99 351.62 F 0.69	352.72 351.92 C 0.80	SEW LAT # 3 2+16.40 on LT →	358.39 353.40 PL C 4.99		358.39 351.009 C 7.39
1+30	351.74 350.59 C 1.15	350.68 350.89 F 0.21	3+00	359.96 358.21 C 1.75		359.23 358.51 C 0.72
1+10	350.22 349.90 C 0.32	349.88 350.20 F 0.32	2+80 = E.V.C.	358.22 358.05 C 0.17		358.74 358.35 C 0.39
0+90-B/C	349.54 349.55 F 0.01	352.05 349.85 C 2.20	2+60	357.52 357.75 F 0.23		358.63 358.05 C 0.58
0+66.66	349.10 349.38 F 0.28	351.28 349.68 C 1.60	2+40	356.81 357.18 F 0.37		358.06 357.48 C 0.58
0+43.33	349.52 349.20 C 0.32	351.25 349.50 C 1.75	2+20	356.00 356.32 F 0.32		356.52 356.62 F 0.10
0+20	349.41 Rod 349.03 Elev C 0.38	349.46 349.33 C 0.13	SEW LAT # 2 2+16.40 on LT →	355.47 351.00 PL C 4.47		355.47 349.10 G C 6.47
0+00 - N/W LNK EL CAJON (E STATIONS)	348.80 Check. 348.80 Elev EXIST PAV	349.16 CHK. 349.18 Elev EXIST PAV	2+00	354.35 355.79 F 0.84		355.43 355.79 F 0.06
R.M.	351.53 DIRECT Elev. Rod:	351.53 = R.P. N/W CORN. EL CAJON & ESTRELLA	1+80	352.65 353.78 F 1.13		353.82 354.08 F 0.26
			1+70	352.07 353.00 F 0.93		353.06 353.30 F 0.24
			SEW LAT # 1 on LT → Elev	351.00 347.75 C 3.25		351.00 346.60 Elev C 4.40
			1+66.40			

ALLEY BIK "A" (CONT.)

STA.	LT.	RT.	STA.	LT.	RT.
5+50 = BVC	360.21 360.23 Fo.02	360.54 360.53 Co.01	7+50	359.33 359.30 Co.03	361.18 359.60 C1.58
5+25	360.09 360.03 Co.06	360.02 360.33 Fo.31	7+25	359.56 359.50 Co.06	360.25 359.80 Co.45
5+00	359.94 359.83 Co.11	360.03 360.13 Fo.10	7+00	359.68 359.69 Fo.01	360.39 359.99 Co.70
4+75	359.90 359.63 Co.27	359.72 359.93 Fo.21	6+75	359.80 359.89 Fo.09	360.72 360.19 Co.53
4+50	359.59 359.42 Co.17	359.58 359.72 Fo.14	6+50	360.25 360.08 Co.17	361.19 360.38 Co.80
4+25	359.29 359.22 Co.07	359.67 359.52 Co.15	6+30 = EVC	360.20 360.24 Fo.04	361.25 360.54 Co.71
4+00	359.17 359.02 Co.15	359.76 359.32 Co.44	6+10	360.38 360.35 Co.03	361.18 360.65 Co.53
3+75	359.22 358.82 Co.40	359.46 359.12 Co.34	5+90	360.38 360.39 Fo.01	361.17 360.69 Co.48
3+50	359.28 Rod 358.62 EVC Co.66	359.10 358.92 Co.18	5+70	360.41 360.35 Co.06	360.47 360.65 Fo.18

ALLEY BIK "A" (cont)

STA.	LT.	E	RT.
8+81.15	358.02 chk: 358.01 = EXIST. Fly Edge Cone Pav. "T" Alley	358.33 (EXIST)	358.63 chk: 358.63 = EXIST.
8+70=BIK	359.67 358.63 C 1.04		360.19 358.93 C 1.26
8+50	359.54 358.71 C 0.83		360.05 359.01 C 1.04
8+25	359.27 358.81 C 0.46		360.87 359.11 C 1.76
8+00=BIK	359.43 358.91 C 0.52		360.89 359.21 C 1.68
7+75	359.09 Rd 357.11 Elev F 0.02		361.32 359.41 C 0.91

Clark  
Shepherd  
BRUNER  
PERKINS

BALBOA PK. CLUB BLDG.

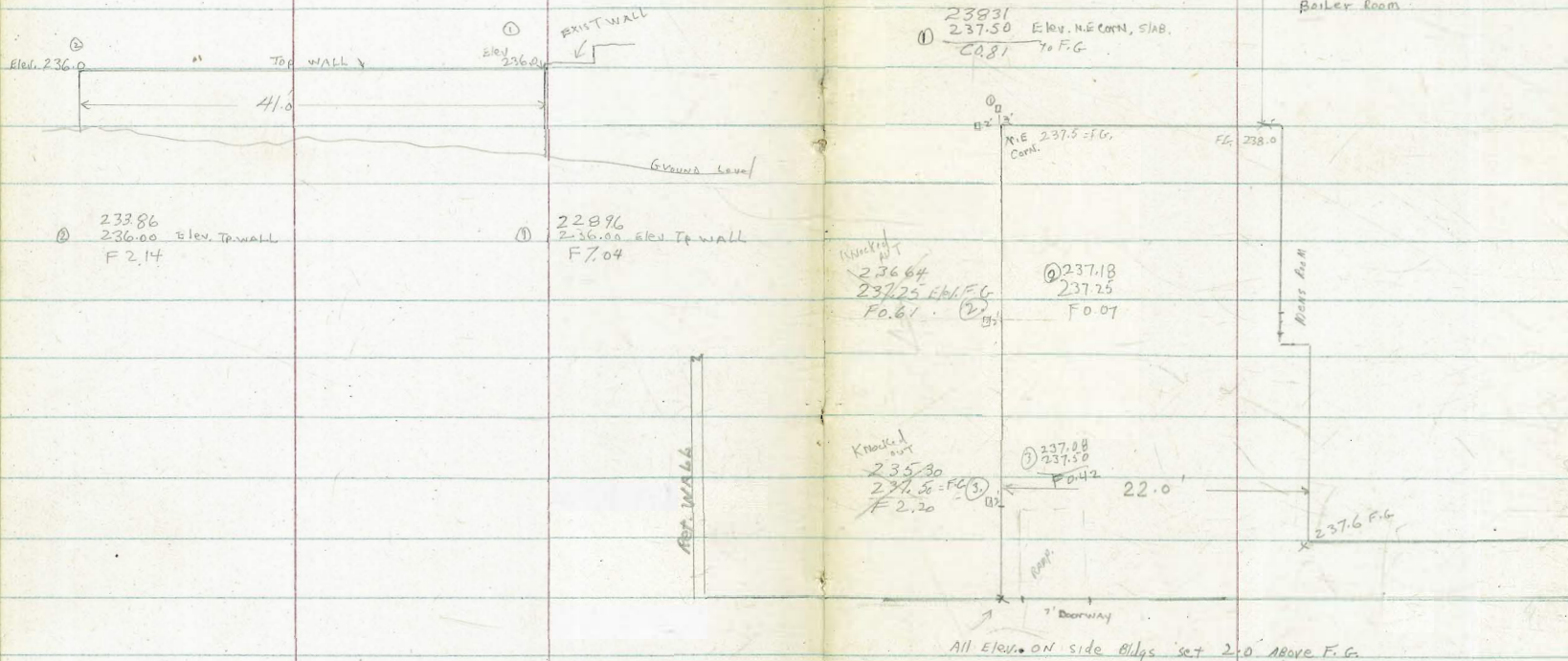
N.O. 20902

10-29-52

RET. WALL

Indexed

CONC. SLAB



B.M.

DIRECT ELEV. ROD: 237.46 = Elev. Floor - MEN'S ROOM

Clark  
Bruner  
Perkins

12-1-52  
W.D. 21014

TEMPORARY DRAINAGE DITCH.  
Frontier, N.W. side, between Rosecrans  
& MIDWAY Drive

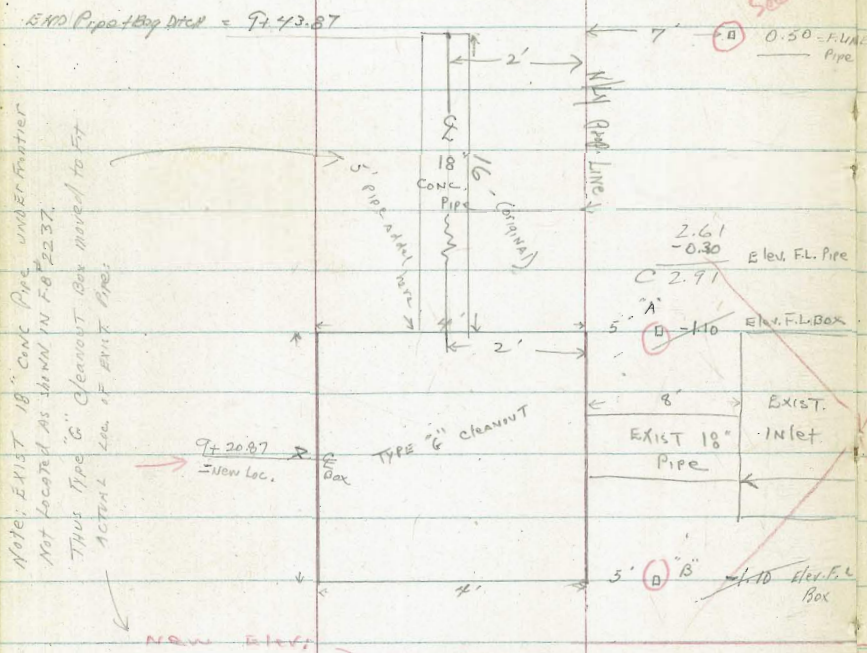
Indexed

DETAIL TYPE "G" Cleanout

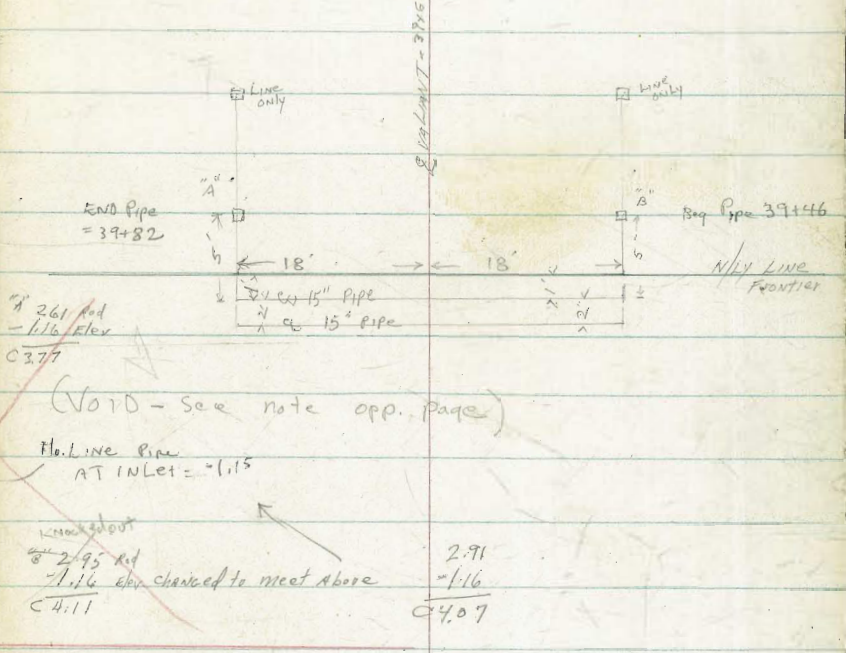
See P 64

DETAIL - Culverts VALIANT ST.

Excavations



Note: EXIST 18" CONC. Pipe under Frontier  
Not located as shown in F-8 2237.  
THIS TYPE "G" Cleanout Box moved to 5'  
ACTUAL Elev. of EXIST. Pipe



"A"

2.99  
- 0.30  
C 3.29

"A"

2.99  
- 1.26 EXIST. Pipe  
C 4.25 F.L. Box

• stubs set AS ABOVE (5' BOX Edge Box)



Temp. Ry Ditch - Frontier

STA.	ELEVATIONS:		N/ly Prop.
	Ft. Line		
11+35 - N/ly PK. area			
11+25	2.63 1.09 C 1.54		C 0.54
11+00	2.65 1.05 C 1.60		C 0.60
10+94 Ely PK. Line			
10+75	3.19 1.01 C 2.18		C 1.18
10+50	3.24 0.97 C 2.27		C 1.27
10+25	2.99 0.93 C 2.06		C 1.06
10+00	3.40 0.87 C 2.51		C 1.51
9+75	3.16 0.85 C 2.31		C 1.31
94387 SEND PIPE Beg. Ditch	Rod 2.75 Elev. Ft. Line Pipe 0.50 C 2.25		C 1.25
B. M.	3.03 = Ch	ON WALK 11+70.14	

STAT.	ELEVATIONS:	
	Ft. Line	N/ly Prop
13+50	2.88 1.45 C 1.43	C 0.43
13+25	2.99 1.41 C 1.58	C 0.58
13+00	3.03 1.37 C 1.66	C 0.66
12+75	3.17 1.33 C 1.84	C 0.84
12+67 - W/ly Line PK. area		
12+50	Kunskadout 1.86 1.73 1.29 1.29 C 0.57 C 0.44	F 0.43
12+25 = Ely PK. area	2.34 1.25 C 1.09	C 0.09
12+00	3.03 1.21 C 1.82	C 0.82
11+70.14 = E.C. Frontier	3.18 1.16 C 2.02	C 1.02
11+50	3.37 Rod 1.13 Ely C 2.24	C 1.24
25' RT. Prop.		

TEMPRY Ditch FRONTIER

Elevations:

Elev's:

STA.	Flow Line	Wdy Prop.	STA.	Flow Line	Wdy Prop.
15125	2.88 1.73 C 1.15	C 0.15	17151 = Wly Line PK area		
15100	2.76 1.69 C 1.07	C 0.07	17150	3.32 2.09 C 1.23	C 0.23
14172 = Wly edge 20' PK area	Knacked out 1.71 1.68 C 0.04 C 0.07	C 0.02	17134 = Wly Line PK area	2.82 Rod 2.06 Elev C 0.76	
14162 = S <sub>2</sub> arc	1.63		17125	1.89 2.05 F 0.16	F 1.16
14152 = Ely Edge 20' PK Area	1.81 1.61 C 0.20		17100	1.94 Rod 2.01 Elev F 0.87	F 1.07
14150	1.61		16888 = Ely Line PK area	3.36 Rod 1.99 Elev C 1.37	
14125	Knacked out 2.24 1.95 1.57 1.37 C 0.70 C 0.38		16775	3.01 1.97 C 1.04	C 0.04
14100	2.80 1.53 C 1.27	C 0.27	16750	3.02 1.93 C 1.09	C 0.09
13175	2.78 Rod 1.79 Elev C 1.29	C 0.29	16225	2.73 1.89 C 0.84	F 0.16
			16200	3.01 1.85 C 1.16	C 0.16
			15775	2.93 1.81 C 1.12	C 0.12
			15750	3.18 Rod 1.77 Elev C 1.41	C 0.41

## Templey Ditch - Frontier

STA	Flow-Line	Elev's:	
		N/ly Prop	
19+27.5	W/ly Edge 20 PK. area	2.55 Rod 2.37 Elev C 0.18	
19+17.5			
19+07.5	W/ly Edge 20 PK. Area	2.37 Rod 2.34 Elev C 0.03	
19+00		2.07 2.33 F 0.26	Knocked-out 2.34 2.33 C 0.01 F 1.26
18+75		3.38 2.29 C 1.09	
18+50		3.21 2.25 C 0.96	F 0.04
18+25		3.13 2.21 C 0.92	F 0.09
18+00		3.20 2.17 C 1.03	C 0.03
17+75		3.26 Rod 2.13 Elev C 1.13	C 0.13

STA	Flow-Line	Elev's:	
		N/ly Prop	
21+50		3.38 2.73 C 0.65	
21+25		3.52 2.69 C 0.83	
21+00		3.48 2.65 C 0.83	
20+90	W/ly Line PK. area	3.39 Rod 2.63 Elev C 0.76	
20+75		2.61 2.61 GRASS	
20+50		2.64 2.57 C 0.07	
20+46	W/ly Line PK. area	3.49 Rod 2.56 Elev C 0.93	
20+25		3.58 2.53 C 1.05	
20+00		3.65 2.49 C 1.16	
19+91	80' Ch 3.63 Chd 25' RT=3.62		
19+75		3.46 2.45 C 1.01	
19+50		3.31 Rod. 2.41 Elev C 0.90	

## TEMP'ry Ditch - Frontier

Elev's		Elev's:	
STA.	Flow-Line N/ly Prop	STA.	Flow-Line N/ly Prop
23+36	chk 3.11 2.98 C0.13 N/ly Line Freedom	25+50	2.69
23+20 = E Freedom - (break Pt. in GARDNER)	rand 3.26 3.00	25+25	2.72
23+04	chk. 3.16 2.97 C0.19 E/ly Line Freedom	25+00	2.75
23+00	3.74 2.97 (Do not tear out exist Pav.) C0.77	24+75	2.79
22+75	3.51 2.93 C0.58	24+50	2.83
22+50	3.59 2.89 C0.70	24+25	2.86
22+25	3.62 2.85 C0.77	24+00	2.89
22+00	3.56 2.81 C0.75	23+75	2.93
21+75	3.70 2.77 C0.93	23+50	2.96

Note: Grades from this Pt. on, set by D. Smith

## TEMP'RY DITCH - FRONTIER

Elev's:		Elev's:	
STA.	Flow-Line	Flow-Line	N/ly Prop.
27+75	2.39	29+50	2.15
27+50	2.42	29+25	2.19
27+25	2.45	29+00	2.22
27+00	2.49	28+72 = N/ly line 20' PKng	2.25
26+75	2.52	28+62 = E PKng area	2.27
26+50	2.56	28+52 = E/ly Line 20' PK Strip	2.29
26+42 = N/ly Line PK area	2.59	28+50	2.29
26+25	2.59	28+25	2.32
26+00 = E/ly Line PK area	2.62	28+00	2.35
25+75	2.65		

STA:	Elev's: Flow-Line	Wly Prop
31+75	1.85	
31+50	1.88	
31+25	1.92	
31+00	1.95	
30+75	1.98	
30+70 = Wly Line PK. area		
30+50	2.02	
30+28 = Wly Line PK. area		
30+25	2.05	
30+00	2.08	
29+75	2.12	

STA:	Elev's: Flow-Line	Wly Prop
33+50	1.61	
33+25	1.65	
33+00	1.68	
32+75	1.71	
32+55 = Wly Line 20' PK. Drive	1.74	
32+45 = E. PKing ATCA	1.75	
32+35 = Ely Line 20' PK. Drive	1.77	
32+25	1.78	
32+00	1.81	

## TEMP'RY DITCH - FRONTIER

Elev's:		Elev's:	
STA:	F/w-Line Nly Prop	STA:	F/w-Line Nly Prop
35+75	1.31	37+50	1.07
35+50	1.34	37+25	1.11
35+25	1.38	37+00	1.14
35+00	1.41	36+75	1.17
34+75	1.44	36+50	1.21
34+50	1.48	36+26.5 = Nly Line 20' PK Drive	1.24
34+30 = Nly Line PK area			
34+25	1.51	36+16.5 = 20' PK Drive	1.26
34+00	1.55	36+06.5 = Ely Line 20' PK Drive	
33+90 = Ely Line PK area			
33+75	1.58	36+00	1.28

TEMPORARY DITCH: Frontier

STA.	Elev's:		STA:	Elev's:	
	Flow-Line	Wly Prop.		Flow-Line	Wly Prop.
39+64 = E VALIANT		2.50 = Adj. Pav. E. GRADE			
	For Flo-Line } see pg. 63 15" Pipes }		41+75		0.50
39+48 = Ely Line VALIANT ST.			41+50		0.53
39+25	0.84		41+25		0.57
39+00	0.87		41+00		0.60
38+75	0.90		40+75		0.64
38+50	0.94		40+50		0.67
38+25	0.97		40+25		0.70
38+00	1.01		40+00		0.73
37+75	1.04		39+80 = Wly Line VALIANT.		



TEMPERARY DITCH FRONTIER

STA:

Elev's:  
Flow-Line Nly Prop

42+65.8 = END-DITCH

0.35

42+50

0.38

42+25

0.42

42+00

0.46

Clark  
Shepherd  
Bruner  
Perkins  
12-9-52  
W.O. 20007

CB. Ret. S/E IMPERIAL  
& EUCLID

Indexed

12-10-52

Note: Eng. Dept. Changed Pkg From  
17' to 9', on S/Sy Imp.  
See next Pg. For New DATA & Grades. →

E.C. (S/Sy IMPERIAL)

21.18  
20.30  
C0.88

E.C. (S/Sy Imp.)

21.65  
21.75  
C0.50

# 3

21.60  
20.75  
C0.85

# 2

21.78  
21.60  
C0.18

# 2

21.69  
21.30  
C0.39

# 1

21.99  
22.10  
F0.11

# 1

22.19  
21.85  
C0.34

B.C. (S/E EUCLID)

22.45 Rod.  
22.60 ELEV  
F0.15

B.C. (S/E EUCLID)

Meet Rod.  
22.50 ELEV

CB. RAD = 20'  
Δ = 62° 05'  
L = 21.67'  
T = 12.36'  
AS PER O. JOHNSON

CB. RAD = 33'  
Δ = 62° 05' 00"  
T = 19.86'  
L = 35.75'

B.M. DIV. ELEV. ROD:

22.50 END EXIST

CB S/E EUCLID (ASSUMED, AS PER PLAN)

Clark  
Shepherd  
Bruner  
Perkins  
12-11-52  
W.O. 20566

STORM-DRAIN EXT.

OLIVE WOOD TERRACE

Indexed

74

STA:

Elev:

CHK: 11.78' E of 2+18.93 = Beg 24" Iron pipe - 37.90 = 37.95 - FB 2029 P. 17

1+60 END Pipe

41.15  
34.04  
C 7.11 F.LINE

1+36

39.46  
34.18  
C 5.28 F.LINE

1+12 = END EXIST. 18"  
CONG. PIPE

Subs cut 10' RT

meet (35.3 = F.LINE ON PLAN 8026-L)  
34.31 → Elev F.LINE AT THIS PT.  
EXIST 18" PIPE

TP,

44.85

B.M

Dir. Elev. Rod.

50.38 N.W. B.P. 35 + Florence's

Clark  
Shepherd  
Bruner

TMP PORTION ALLEY BRK 51  
CITY HTS. - UNIV. Stg. 175'

Indexed

75

12-16-52 DATA: 9904-L  
W.O. 62286

STA.	LT.		RT.	STA.	LT.	RT.
1+60	350.07 349.98 C 0.09		352.61 350.30 C 2.31			
1+35	351.71 350.50 C 1.21		352.16 350.81 C 1.35			
1+10	352.00 351.02 C 0.98	352.00 350.78 C 1.22	351.40 351.33 C 0.15			
0+95	352.24 351.34 C 0.90		353.25 351.65 C 1.60			
0+70	352.57 351.88 C 0.69		353.15 352.18 C 0.97			
0+45	353.15 352.41 C 0.74		353.88 352.71 C 1.17			
0+20	353.32 Rod. 352.94 elev. to Pav. C 0.38		353.50 Rod 353.24 elev. C 0.26			
0+00 =	353.31 OK. 353.31 EXIST. Sly Line UNIV. (Meet EXIST.)		353.22 CL. 353.26 EXIST.	1+75 = END GRADING	349.23 349.67 FOA4	351.31 349.98 C 1.33
B.M.			347.09	N.W. B.P. WIGHTMAN + North Borough		
B.M.	DIF. Elev. Rod:		355.49	N.W. B.P. WIGHTMAN + 41' ST.		
	* ABOVE Plug changed when NEW Ret. PUT IN. Does Not Chk Elev ON PLAN					

