

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 15 1965

	0
0	0.00
1	1.00
2	2.00
3	3.00
4	4.00
5	5.00
6	6.00
7	7.00
8	8.00
9	9.00
10	10.00
11	11.00
12	12.00
13	13.00
14	14.00
15	15.00
16	16.00
17	17.00
18	18.00
19	19.00
20	20.00
21	21.00
22	22.00
23	23.00
24	24.00
25	25.00
26	26.00
27	27.00
28	28.00
29	29.00
30	30.00
31	31.00
32	32.00
33	33.00
34	34.00
35	35.00
36	36.00
37	37.00
38	38.00
39	39.00
40	40.00
41	41.00
42	42.00
43	43.00
44	44.00
45	45.00
46	46.00
47	47.00
48	48.00
49	49.00
50	50.00

Distance ground is a column and side stake t side stake a cut or fill a If it does n

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for 4:1 width roadway slope 1:1 to 1:1

IMPROVED TABLES AND INFORMATION

TABLE No. XIII

TABLE No. XII

TABLE No. XI

TABLE No. X

TABLE No. IX

TABLE No. VIII

TABLE No. VII

TABLE No. VI

TABLE No. V

TABLE No. IV

TABLE No. III

Index

Chico - Pave		3-4
Kendall - Pave		5-7
Shasta - Pave		8
CHICO Kendall Shasta } Curb returns		9-
Brighton Ave. Sewer	west of Abbott	14
Larnont		20-25
Sewer, Armaffi St.		17-18
" BIK 69 + BIK C.	La Jolla park	18+26-27
" Soledad Ave		27+28
" Torrey Road	}	29-31
" Cowrie St		
" Torrey Rd.	west of Cowrie St.	32 @
Pave	} OLIPHANT NEWEL LOCUST	33-42+43
THOMAS - water line		
Collingwood Dr.	Kendall to Jewell	35
Alley BIK 2 + BIK 27	Ocean Beach	38-41
Storm Drain Sly and Cushman Place		44
Thomas St. Pave + Cbs.		45-47

Index

Muir + W. Pt. Loma Blvd (Sewer)		48
Alley BIK 240 - M. B.	Storm drain	49
Intersection 15 th + Broadway		50
Alley BIK 200 Pacific Beach		51
" BIK. 17 - O. B.		53
" BIK. 7 Ocean Beach		55
" BIK 12 Sunset Cliffs		57
Ties " " " "		61 + 59
Alley " " " "	Sewer + water lots.	60
" BIK 255 Pac. Beach		62
" BIK. { ¹⁵⁶ 157 158 } Pac. Beach		63-68
" " 75 - Ocean Beach		67-68
Storm Drain Forward	+ Lind Rose	69-70
Alley BIK 45 Ocean Beach		71-75
Tie Points BIK 45 - O. B.		72
Sewer BIK. I	Plumosa Manor	76
Storm Drain P. B. Drive	Riviera Dr. to Gresham	77
Reed. Cass to Dawes		78-79
Stake lots 21+22 BIK 10	}	80
Monte Villa track (Dawes + Archer)		

CHICO st.

Lamont to Shasta

Run west to match profile

9-30-52
N.D. 31A05

South

Rough Curb

North

Curb Rough

0+83²

26.05	5.58	6.10	27.35
25.56	25.56	26.06	26.06
C0.49	C0.02	C0.04	C1.29

0+63² X-1'

25.91	5.09	5.51	27.10
25.03	25.03	25.53	25.53
C0.88	C0.06	F0.02	C1.57

EL Rad 1/2
P.O.C.

on South
0+32.29 Ch. B.C.

25.50	4.32
24.24	24.24
C1.26	C0.08

0+23.3 on Rd.

5.00
24.50 24.50
C0.50

Ch. B.C. on North
0+11.34

4.31 25.55
4.37 24.37
F0.06 C1.18

To North
Wly Lamont
0+00

25.79
= EL Rad
1/2

Sequoia
Ely.

2+38² U.C. 30.98

Ch. B.C.
2+25²

29.75	0.26	0.69	30.92
30.50	30.50	31.03	31.03
F0.75	F0.24	F0.35	C0.11

U.C.
1+83²

8.24	8.29	7.28	29.17
28.88	28.88	29.38	29.38
F0.64	F0.59	F0.10	F0.21

1+63²

7.65	7.72	8.62	28.84
28.14	28.14	28.64	28.64
F0.49	F0.42	F0.02	C0.10

1+43²

7.11	7.13	7.83	28.71
27.43	27.43	27.93	27.93
F0.32	F0.30	F0.10	C0.78

1+23² 1

6.75			27.79
26.76		27.26	27.26
F0.01			C0.53

1+03²

6.50	5.89	6.67	28.04
26.15	26.15	26.65	26.65
C0.35	F0.26	C0.02	C1.39

CHICO

3

South
Rough Curb

North
Curb Rough

INDEXED
JER
DEC 15 1953

Boyer
Altman
Johns

5.00
24.50
24.50
C0.50

CHICO

South		North	
Rough	cl.	Rurph	Rough

Ely, Kendall
2+15

cl. B.C.

2+02^E

1+58.75 Nail

1+17

Wly Alloy
1+15Ely, Alloy
1+00

(4375) 0+99

0+56.25 X-1'

(4375) 0+50

cl. B.C.
0+12^EWly, Sequoia
0+00

39.76

38.60

C 1.16

40.43

37.23

C 3.20

8.31

35.86

C-2.45

37.19

35.39

C 1.80

35.71

34.02

C 1.69

3.66

32.65

C 1.01

38.60

38.40

F0.04

C0.14

F0.36

F0.67

1.98

32.65

F0.15

32.26

North	
Rurph	Rough

40.60

38.40

C 2.20

39.48

37.18

C 2.30

37.91

35.95

C 1.96

37.70

35.54

C 2.16

36.32

34.32

C 2.00

2.39

33.10

F0.71

32.76

C 1.98

N. Ely, disk
Chico + Sequoia
Eli = 31.84Ely, Shasta
2+15cl. B.C.
2+02.5

1+50 cl

- 0.3'
1+58.75

1+17 v' Rad.

Wly Alloy
1+15Ely Alloy
1+00

0+98 v' Rad.

0+56.25

0+50

cl. B.C. on RR
0+13

cl. B.C. on H.

0+12^E NailWly, Kendall
0+00

CHICO

South	
Rough	curb

46.91

46.56

C 0.35

46.20

45.04

C 1.16

4.95

43.52

C 1.43

3.07

43.00

C 0.07

42.21

41.48

C 0.73

42.38

39.96

C 2.42

North	
curb	Rough

49.78

47.02

C 2.76

8.59

45.40

C 3.19

7.14

43.78

C 3.36

5.95

43.25

C 2.70

4.95

41.63

C 3.32

4.17

40.01

C 4.16

39.96

40.01

~~40.01~~

4

INDEXED

HER

DEC 15 1953

KENDALL

West

East

Rough On stubs

11 Ba

Rough

curb

curb

Rough

West

West

East

5+50

8.46
27.43

6.29
27.43

6.42
26.93

8.02
26.93

Rough

curb

curb

Rough

C 1.03

F 1.14

F 0.51

C 1.09

2+50

0.57

29.05
26.48
C 2.57

F 0.43

C 0.16

8.07
25.98
C 2.09

5+30

8.17
27.54
C 0.63

6.48
27.54
F 1.06

6.48
27.04
F 0.56

8.29
27.04
C 1.25

2+00

0.57

8.57
26.22
C 2.35

C 0.09

Grade

7.10
25.72
C 1.38

5+10

7.98
27.60
C 0.38

6.55
27.60
F 1.05

6.71
27.10
F 0.49

7.94
27.10
C 0.84

BTK

1+50

7.92
25.97
C 1.95

5.65
25.97
F 0.32

5.45
25.47
Existing
ch.

25.47

A+90

8.44
27.61
C 0.83

6.52
27.61
F 1.09

6.14
27.11
F 0.97

7.56
27.11
C 0.45

Ch. Sta. 1+96 on east

1+00

6.91
25.82
C 1.09

F 0.48

25.14
25.60
F 0.06

25.32

A+70

9.80
27.58
C 2.22

6.75
27.38
F 0.63

6.45
27.01
F 0.56

8.37
27.01
C 1.36

0+50

0.32

7.22
25.66
C 1.56

F 0.58

25.16

P.V.C.
A+50

9.37
27.50
C 1.87

6.42
27.50
F 1.08

6.71
27.00
F 0.29

8.15
27.00
C 1.15

on east
0+31 ch. f.c.

0+31

9.84
27.25
C 2.59

F 0.75

A+00

A+00

9.84
27.25
C 2.59

F 0.75

F 0.20

8.68
26.75
C 1.93

Ch. B.C. on west

0+12

6.26
25.54
C 0.72

5.25
25.54
F 0.29

24.96

3+50

9.73
27.00
C 2.73

F 0.80

C 0.11

28.38 T.P.
26.50
C 1.88

N by La Playa

0+00

25.50

25.00

3+00

9.50
26.74
C 2.76

F 0.36

F 0.18

8.31
26.24
C 2.07

	Kendall					KENDALL			
	West		East			West		East	
	Rough	curb	curb	Rough		Rough	curb	curb	Rough
1+30	8.67 27.67	7.31 27.67	7.57 27.60	7.56 27.60	4+50	2.34 31.66	F0.50	F0.08	2.10 31.32
	C1.00	F0.36	F0.03	F0.04		C0.68			C0.78
P.V.C. 1+10	8.53 27.55	7.09 27.55	7.44 27.42	7.75 27.42	4+00	1.93 31.02	F0.62	F0.05	1.68 30.73
	C0.98	F0.46	C0.02	C0.33		C0.91			C0.95
0+61 ²⁵	7.95 27.30	7.15 27.30	6.89 27.01	7.37 27.01	3+50	0.42 30.38	F0.62	F0.15	1.01 30.14
	C0.65	F0.15	F0.12	C0.36		C0.04			C0.87
0+12 ⁵ d.E.C.	7.35 27.06	7.00 27.06	6.55 26.60	7.51 26.60	3+00	TIP 30.51 29.73	F0.29	F0.28	30.51 29.55
	C0.29	F0.06	F0.05	C0.91		C0.78			C0.96
Nly Roosevelt. 0+00	27.00			26.50	2+50	30.28 29.08	F0.50	F0.34	8.88 28.96
						C1.20			F0.08
Roosevelt.					2+00	29.60 28.43	F0.53	F0.59	8.28 28.37
						C1.17			F0.09
slg Roosevelt. 6+00	27.00				E.V.C. 1+90	9.23 28.30	7.70 28.30	27.89 TIP 28.35	8.31 28.25
	Ch. Rad. EL=28.31		Ch. Rad. EL=28.83			C0.93	F0.60	F0.46	C0.06
Ch. B.C. 5+87E	7.59 27.10	6.59 27.10	6.47 26.60	7.90 26.60	1+70	8.96 28.05	7.63 28.05	7.71 28.02	7.91 28.02
	C0.49	F0.51	F0.13	C1.30		C0.91	F0.42	F0.31	F0.11
E.V.C. 5+70	8.04 27.27	6.91 27.27	6.86 26.77	7.88 26.77	1+50	9.04 27.84	7.63 27.84	7.52 27.80	7.72 27.80
	C0.77	F0.36	C0.09	C1.11		C1.20	F0.31	F0.28	F0.08

1.3% West
1.18% East

Kendall

West
Rough | curb

East
Curb | Rough

Beach. Dir. } 2+51E 45W Kendall 45.25
sly Pa. } Rough curb curb Rough 7
2+00 44.10 44.00
2+00 = (W) Lt.

1+00	8.43 36.75 C-1.68	CO.14	FO.12	6.86 36.25 C 0.61	1+50	42.95		42.75
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0+50	6.60 35.37 C 7.23	FO.09	FO.06	6.56 34.87 C-1.69	1+00	41.88	FO.12	41.92 41.50 C 0.42
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0+12 1/2 Cl. E.C.	5.63 34.31 C 1.32	4.31 34.31 X	3.93 33.84 FO.11	5.90 33.84 C 2.06	0+50	40.65	FO.05	41.75 40.25 C 1.50
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Fortuna 0+00 Nly.	34.00			33.50	Cl. E.C. 0+11 1/2	39.77		40.81 39.30 C 1.51
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Fortuna					Nly Chico 0+00 Est. 39.50			39.00
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Fortuna. 6+00 sly.	33.59			33.09	CHICO			
Rad. El. = 34.38				Rad. El. = 34.62				

5+87 1/2 Cl. B.C.	4.71 33.43 C 1.28	3.38 33.43 FO.05	2.92 32.94 FO.02	4.49 32.94 C 1.55	sly. Chico 2+00	39.50		3 39.00 Rad. = 39.93
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5+50	3.75 32.95 C 0.80	FO.18	FO.12	3.63 32.50 C 1.13	Cl. B.C. 1+85 Nail	42.56 38.61 C 3.95	8.32 38.61 FO.29	8.07 38.59 FO.52	9.58 38.59 C 0.99
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5+00	3.05 32.30 C 0.75	FO.5A	FO.20	2.76 31.91 C 0.85	Nail 1+50	9.53 38.12 C 1.41	FO.14	FO.17	8.75 37.62 C 1.13
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INDEXED
 JER
 DEC 15 1953

SHASTA

48.60 T.P.

West
 Rough curb

East
 Curb Rough

8

0+00 = Nly. Fortuna

Meat cl.
 Sly. P.B. Drive
~~5+25~~

51.00

51.00

West Rough	West Curb	East	
		Curb	Rough

5+25	51.08 51.00	✓ 51.00	51.00	51.15 cl. 51.00
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Sly. Chico
 2+00

8.87 46.87 C 2.00	C.87 46.87 X
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= 46.62
 EL Rad 1/2

4+77	2.50 50.42 C 2.08	FO.15	FO.08	2.11 50.35 C 1.76
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Ob. B.C. on Rt.
 1+85

8.64 46.50 C 2.14

46.60	C.74 46.60 C 0.14
-------	-------------------------

A+29	51.96 49.84 C 2.12	FO.04	FO.13	51.42 49.69 C 1.73
------	--------------------------	-------	-------	--------------------------

1+50

8.04 45.64 C 2.40	FO.20
-------------------------	-------

FO.06	C.11 45.64 C 0.47
-------	-------------------------

3+81	51.45 49.26 C 2.19	X	CO.04	51.25 49.03 C 2.22
------	--------------------------	---	-------	--------------------------

1+00

6.95 44.42 C 2.53	CO.05
-------------------------	-------

FO.11	45.45 44.26 C -1.19
-------	---------------------------

3+33	50.80 48.68 C 2.12	X	FO.04	51.27 48.37 C 2.90
------	--------------------------	---	-------	--------------------------

0+50

5.76 43.20 C 2.56	CO.02
-------------------------	-------

FO.20	3.99 42.88 C 1.11
-------	-------------------------

Ob. E.C. on Rt.

2+85	9.57 48.10 C 1.47	FO.01	47.71	50.29 47.71 C 2.56	Nail
------	-------------------------	-------	-------	--------------------------	------

Ob. E.C.
 0+125

4.89 42.30 C 2.59

1.86 41.84 CO.02	3.10 41.84 C 1.26
------------------------	-------------------------

Nly Chico

2+70	50.31 47.92 C 2.39	8.10 47.92 CO.18
------	--------------------------	------------------------

0+00

E Chico

.2+35 X on steps	49.25 47.40 C 1.85	7.77 47.40 CO.37
---------------------	--------------------------	------------------------

As per tie point
 0+00 = Nly. Fortuna

INDEXED
NER
DEC 15 1953

Kendall
7.00
27.06
F 0.06
6.55
E.C.
F 0.00
N.W. Ret
7.06
27.04
C 0.02
6.53
Prop
26.28
C 0.03
N.E. Ret
7.08
27.10
F 0.02
6.50
26.34
C 0.16
7.37
27.21
C 0.16
6.60
Prop
26.18
B.C.
C 0.42
Roosevelt

Roosevelt St
— E.C. —
7.27
27.19
C 0.08
5.97
26.18
F 0.21
N.W. Ret
7.31
27.10
C 0.21
6.02
26.35
F 0.33
F. Ret
6.80
27.08
F 0.28
5.64
26.54
F 0.83
6.46
B.C.
27.10
F 0.51
26.60
F 0.11
Kendall St

Kendall
5.25
25.54
F 0.29
5.10
25.59
F 0.49
5.34
25.65
F 0.31
5.28
25.80
F 0.52
25.90
B.C.
Laplaya Ave

INDEXED
NER
DEC 15 1953

Also SHASTA & Fortuna...
Kendall St
F 0.80
2.16
42.30
F 0.14
1.86
41.84
C 0.02
1.64
41.54
C 0.10
1.44
41.35
C 0.09
1.23
41.27
F 0.04
N.E. Ret
N.W. Ret
Prop
B.C.
FORTUNA

KENDALL
34.31
4.06
34.15
F 0.09
3.73
33.84
F 0.11
4.22
33.62
C 0.60
3.25
33.50
F 0.25
N.E. Ret
N.W. Ret
5.06
34.17
C 0.89
3.48
33.38
C 0.10
B.C.
FORTUNA

FORTUNA Ave.
— E.C. —
4.05
34.07
F 0.02
3.11
33.77
F 0.66
4.29
33.29
C 1.00
3.55
33.17
C 0.38
3.31
33.05
C 0.26
33.43
B.C.
32.94
KENDALL ST

Curb returns CHICO

CHICO.

Kendall St

IN

ROSEBURY ST

CHICO.

KENDALL ST.

8.26
38.60
F0.34

8.21
39.30
F0.09

8.31
38.79
F0.48

9.01
39.07
F0.06

8.38
38.85
F0.47

8.75
38.90
F0.15

8.19
38.76
F0.57

8.50
38.65
F0.15

8.07
38.59
F0.52

8.20
38.40
F0.20

Existing
at

Kendall St

CHICO ST.

SHASTA ST.

6.45
46.57
F0.14

7.34
47.71
F0.37

6.58
46.92
F0.34

7.56
47.56
grade

6.53
47.15
F0.62

7.28
47.37
F0.09

6.61
46.97
F0.36

6.93
47.22
F0.29

6.56
46.56
grade

6.53
47.02
F0.49

CHICO ST.

#5

#4

S.E. Ret.

S.W. Ret.

#3

#2

#1

#A

#1

#3

#4

N.E. Ret.

S.E. Ret.

#1

BC

Alley Returns CHICO

INDEXED
 DEC
 DEC

Kendall St

8.11
 36.16
 C19.5

6.06
 35.90
 C0.14

35.86

35.97

5.81
 36.02
 F0.21

8.10
 36.32
 C1.78

⑧

①

7.15
 35.69
 C1.46

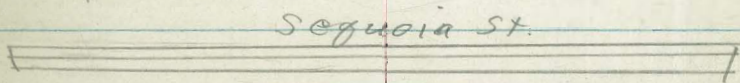
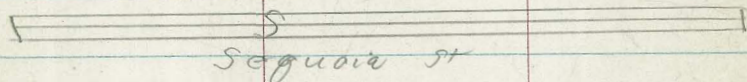
4.98
 35.41
 F0.43

35.39

35.56

5.05
 35.61
 F0.56

8.01
 35.91
 C-2.10



Sequoia St

Sequoia St.

7.00
 27.56
 F0.56

7.01
 27.30
 F0.29

7.01
 27.33
 F0.32

7.01
 27.26
 F0.25

7.75
 27.83
 F0.08

7.75
 27.76
 F0.01

8.18
 28.07
 C0.11

⑨

②

6.42 x in
 27.08 Conc.
 F0.66

6.41
 26.81
 F0.41

26.76

6.41
 26.70
 F0.29

7.05
 27.26
 F0.21

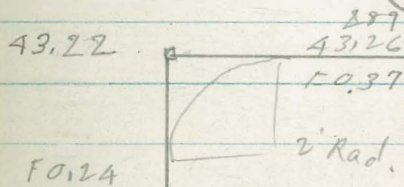
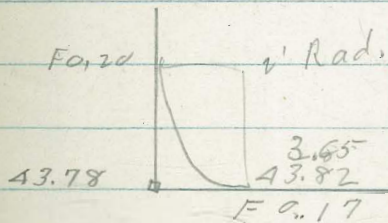
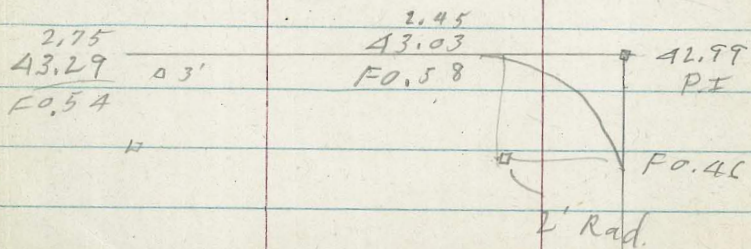
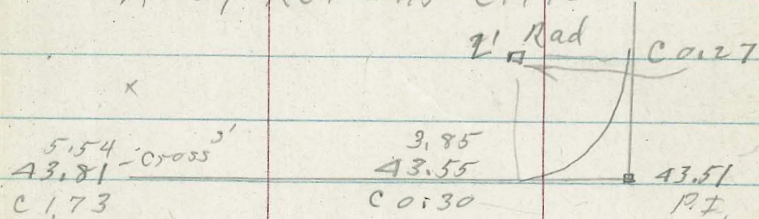
7.05
 27.20
 F0.15

7.64
 27.57
 C0.07

Lamont St

Lamont St

Alloy Returns CHICO



6.80
44.08
C 2.72

5.17
43.52
C 1.65

Brighton Ave.
Sewer west of Abbott

12-29-52

Sheet #8715L + #8716-L.

Existing M.H. 396 west of Abbott. = 0+00

stakes set 5' right (north) of \pm

B.M. = N.W. by B.P. Abbott & Brighton EL. = 10.15

3' back of ch.
(W) A+65 RT ch. EL. = 5.26
13.64
C 1.62

3' back of ch.
(W) A+80 Lt. ch. EL. = 2.29
13.67
F 1.38

0+79 End of pipe 2.94
-0.80
C-3.74

0+39 $\frac{5}{2}$ 3.28
-0.96
C-4.24

0+00 Exist. M.H. 4.00
-1.12
C 5.12

Sewer Laterals
Brighton Ave.

INDEXED
JAN 12 1954
JER

14

#1 - 4+70 Lt. = #1 3.62
+ 0.08
C 3.54

#2 - 4+55 RT. 4.57
+ 0.02
C 4.55

#3 - 3+85 RT. 4.52
- 0.09
C 4.61

#4 - 3+45 RT 7.76
+ 0.27
C 7.49

#5 - 3+41 Lt. 6.48
+ 0.32
C 6.16

#6 - 2+65 RT 7.22
1.09
C 6.13

#7 - 1+40 Lt. 8.80
2.65
C 6.21

Sewer Laterals - Cape May Ave

#8 - 0+55 RT. 9.34
4.76
C 4.58

Alley BIK 77 O.B.

N.W.B.P. Abbott &
Cape May EL = 8.89

1-2-53
C.H.S.

Set & grades. top of Pavc.

	LT	±	RT	
1+70 X-3'	9.99 9.23 C0.76	9.90 8.63 C1.33	X 13' Lt	9.32 D2 8.98 C0.34
1+35 X-2'	10.17 9.68 C0.49	10.1A 9.06 C1.08	X 12' Lt	9.73 D2 9.41 C0.32
1+00 E.V.C. X-2'	10.24 10.15 C0.09	10.20 9.48 C0.72	X 12' Lt	10.47 D-1 9.86 C0.61
0+80 X-2'	10.55 10.20 C0.35	10.51 9.66 C0.85	X 12' Lt	11.16 D-1 10.04 C1.12
0+60 N-0.60	11.40 10.13 C1.27	11.36 9.71 C1.65	N. 10.60 Lt	11.21 D-1 10.10 C1.11
0+40 N-0.65	11.44 10.04 C1.40	11.39 9.62 C1.77	N. 10.65 Lt	10.69 D-1 10.00 C0.69
0+20 N-0.70	11.24 9.81 C1.43	11.19 9.40 C1.79	N. 10.70 Lt	9.80 X1 9.80 X
Wly. Abbott 0+00 P.V.C.	9.57	9.22 X	N. 10.70 Lt	9.52

INDEXED
JER
JAN 12 1954

4+50 End pavc. station 12' Rt. 5.44

	LT	±		
End Pavc.	4.60	4.55	□ 12' Lt	5.48
4+50 D1	5.64	5.16	□ 12' Lt	5.53
	F1.04	F0.61		F0.05
□-2'	6.76	6.68	□ 12' Lt	6.20
4+15	6.09	5.60	□ 12' Lt	5.96
	C0.67	C1.08		C0.24
□-2'	6.00	5.97	□ 12' Lt	6.49
3+80	6.54	6.03	□ 12' Lt	6.39
	F0.54	F0.06		C-3.10
□-2'	6.21	6.18	□ 12' Lt	6.97
3+45	6.99	6.46	□ 12' Lt	6.82
	F0.78	F0.28		C0.15
□-2'	6.73	6.70	□ 12' Lt	7.92
3+10	7.44	6.90	□ 12' Lt	7.25
	F0.71	F0.20		C0.67
N. 2.60	8.28	8.24	N. 12.60 Lt	8.39
2+75	7.89	7.33	□ 12' Lt	7.68
	C0.39	C0.91		C0.71
□-2'	9.06	9.02	□ 12' Lt	9.66
2+40	8.34	7.76	□ 12' Lt	8.12
	C0.72	C1.26		C1.54
□-2'	9.59	9.50	□ 12' Lt	10.41
2+05	8.78	8.20	□ 12' Lt	8.55
	C0.81	C1.36		C1.86

Curb. Brighton Ave. 16

Sheet # 8715-L

0+00 = wly. line Abbott. N.W.B.P.
10.15

3+80

6.25
6.54
F0.29

3+60

7.07
6.67
C0.40

3+45

6.5 Ord.
6.8
F0.3

2+75 Ord.

7.7
7.7
F

2+40

9.63
8.18
C-1.45

1+70

9.95 8.94 walk
7.05 9.00
C0.90 F0.06

1+35

10.05
9.48
C0.57

1+00

10.08
9.91
C0.17

0+80

10.08
10.26
10.08
C 0.34

0+20

9.80
9.79
9.80
F0.01

(South)

North

10' Lt.

10' Rt.

Back of curb lines)
walls. (stakes 10'
= wly. face cut off
4+85 curb grade.

3.65

2.37

3.67

3.59

F0.02

F 1.22

□-3' back

□-3' Back

Lt.

Rt.

1
End. Cl.

2.89

1.84

4+85

3.67

3.59

F0.78

F 1.75

4+60

3.00

3.48

3.73

3.66

F0.73

F 0.18

4+40

4.08

3.77 Meet.

3.82

3.78

C0.26

4+37 = end Exist. Cl.

Sewer

12-8-53

Amalfi st + Brk. L.

1522D

1521-D

2+00

7.04%

8.67
84.24
C 4.43

1+50

5.16
80.72
C-4.44

1+45.31

Brk.

4.84
80.39
C 4.45

1+15.31

83.99
79.49
C 4.50

0+90.31

83.63
78.74

M.H.# 10
0+85.31

78.59

C 4.89

A 57-AALX

0+80.31

83.77
78.43
C-5.34

0+50

7.04%

4.57
77.53
C 7.04

M.H.# 9
0+00 A M.H.# 9

86.08
76.15
C-9.93

Existing stub

0+00

80.54 TP
79.62 TP

17

INDEXED
JER
JAN 12 1954

5+00

10.40
106.13
C 4.27

4+50

7.04%

12.65 Nail - 41 RT.
102.13 also = T.P.
C-10.52

4+26.81

108.08
100.27
C 7.81

Δ 70° 54' 45" RT.
4+21.81 M.H.# 17

99.87

4+16.81

7.04%
107.87
99.52
C-8.35

4+00

106.52
98.34
C-8.18

3+50

7.04%

102.61
94.82
C-7.79

3+00

8.07
91.29
C 6.78

2+50

93.21
87.77
C-5.44

Amalfi & BIK. L.
 pipe
 End of

8+76.86	5.92 141.24 C 4.68	
8+50	42.88 138.02 C 4.86	TP. 139.00
8+00 12%	7.28 132.02 C 5.26	
7+57.6	32.69 126.93 C 5.76	
Δ 12°-19'-30" Lt 7+52.60 M.H. #18	126.33	TP. 136.59
7+47.6	31.50 125.94 C 5.56	5' RT. 4.8
7+00	5' Lt. 7.62 122.13 C 5.49	127.63 122.13 C 5.50
6+50 %	22.94 118.13 C 4.81	12150 2.0
6+00	8.00 114.13 C 3.87	
5+50	3.90 110.13 C 3.77	

BIK. 69 & BIK C. La Jolla park 18
 Villa Franch. La Jolla pl.
 Continued page 26

2+50 12.44%	89.23	
2+44.09 BIK.	6.40 88.50 C 7.90	
2+39.09		
2+00	92.80 86.71 C 6.09	
1+50	90.92 84.68 C 6.24	
1+00 %	8.78 82.65 C 6.13	
0+50 %	8.06 80.62 C 5.44	6.16 80.62 C 5.84
0+05	84.56 78.80 C 5.70	Rostake.
Amalfi STI 0+00 = M.H. #10	3.92 78.59 C 5.33	on M.H. #10

INDEXED
 JAN 12 1954
 J. C. R.

Fortuna St. Curbs.
Nly. side east of Lamont.

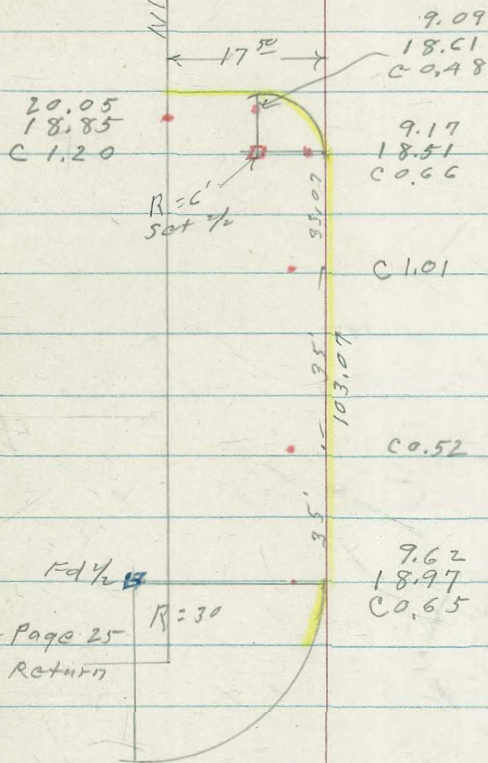
C.H.S.

stakes set 4' back of curb.

INDEXED
MAY 1958
JAN 1958

Nly. line Fortuna

19



LAMONT AVE.

Crown Pt. Drive to Pacific Beach Dr.

INDEXED
JER
JAN 12 1954

Rough curb curb Rough

10-27-52	WD. 31914	F.B. 2044-59	1 Roosevelt		change to curb	to water	Raised	
C.H.S.		Sheets			cover		to meet	
Beqq		9335-L			value		water gate	
Altman		9336-L	cb. B.C.	1.70				1.89
Johns.		9337-L	2+47.52	20.48	20.48	20.69		20.19
		EL. $\frac{1}{2}$ Rad. Sub.		C-1.22	C0.10			C 4.20
		EL. = 21.60	2+00	C 1.46				C 1.44
		↳ 21.84		1.74				C 1.00
				20.02	F0.04	grade		21.47
				C 1.72				19.77
				C 1.96				C 1.70
			1+50	1.16				C 1.60
				19.54	C0.03	F0.02		9.64
				C 1.62				19.33
				C 1.86				C0.31
			1+00	20.25				C0.55
				19.06	F0.01	grade		C0.45
				C-1.19				8.77
				C-1.43				18.89
			0+70	19.90				F0.12
				18.78	F0.02	C0.05		C0.12
				C-1.12				C0.07
				C 1.36				8.21
			cb. E.C. on Rt.					18.63
			0+45.46					F0.42
						18.41		F0.18
						C0.09		17.80
								18.41
								F0.61
								F0.37
			cb. E.C. on Lt.	9.32				
			0+41.20	18.50	F0.18			
				C 0.82				
				C 1.06				

Note.

Used Mon. Ely Lamont + wly

Pac. Beach Drive as 16.88 as shown

on plans. - should now be 17.12

Elevations as shown on
 rough grade stubs are: 0.24 low
 Rad. $\frac{1}{2}$
 EL. = ~~18.08~~
 ↳ 18.23

T.B.Ms have been corrected for Elev.wly Lamont. (2044-P.59)
0+00 = wly Crown Pt. Drive +

LAMONT
Roosevelt to Fortuna.
Rough. Curb Curb Rough
21.61
T.P.

3+00
0.65 20.26
C 0.39
C 0.63
0.40 20.26
C 0.14
0.20 20.20
X
21.37
20.20
C 1.17
C 1.41

2+50
1.35 20.71
C 0.64
C 0.88
0.73 20.71
C 0.02
20.60 20.58
C 0.02
1.80 20.58
C 1.22
C 1.46

2+00
2.42 21.16
C 1.26
C 1.50
1.12 21.16
F 0.04
1.10 20.96
C 0.14
2.10 20.96
C 1.20
C 1.44

1+50 E.V.C.
2.94 21.60
C 1.34
C 1.58
1.78 21.60
C 0.18
1.40 21.33
C 0.07
2.20 21.33
C 0.87
C 1.11

1+30
3.05 21.72
C 1.33
C 1.57
1.76 21.72
C 0.04
1.49 21.43
C 0.06
2.32 21.43
C 0.89
C 1.13

1+10
2.90 21.74
C 1.16
C 1.40
1.60 21.74
F 0.14
1.52 21.44
C 0.08
1.90 21.44
C 2.46
C 0.70

0+90 P.V.C.
2.88 21.64
C 1.24
C 1.48
1.71 21.64
C 0.07
1.42 21.34
C 0.08
1.88 21.34
C 0.54
C 0.78

0+51.25
2.96 21.36
C 1.60
C 1.84
1.48 21.36
C 0.12
1.12 21.17
F 0.05
1.50 21.06
C 0.44
C 0.68

0+12.5 O.E.C.
2.62 21.09
C 1.53
C 1.77
0.82 20.79
C 0.03
1.50 20.79
C 0.71
C 0.95

Roosevelt.
0+00 = Nly. line

21.64
EL. 1/2 Rad = 21.40

NE. 30' Rad Fortuna + 21
Lamont EL = 21.32
Rough Curb Curb Rough.

Sly. 600
Fortuna.
EL Rad cross
= ~~21.82~~ 21.82

O.B.C.
5+87⁵ TR. 21.70
21.45 9.07 8.95 9.62
18.94 18.94 18.56 18.56
C 2.51 C 0.13 C 0.39 C 1.06
C 2.75 C 1.30

5+35
20.90 9.22 8.99 8.93
19.12 19.13 18.84 18.84
C 1.78 C 0.09 C 0.15 C 0.09
C 2.02 C 0.35

4+85
20.25 9.30 9.18 9.90
19.30 19.31 19.10 19.10
C 1.95 F 0.01 C 0.08 C 0.80
C 2.19 C 1.04

4+35
9.90 9.57 9.37 9.40
19.48 19.49 19.36 19.36
C 0.42 C 0.08 C 0.01 C 0.04
C 0.66 C 0.28

3+85 E.V.C. X
9.68 9.66 9.67 9.75
19.67 19.67 19.62 19.62
C 0.01 F 0.01 C 0.05 C 0.13
C 0.25 C 0.37

3+65
9.90 9.89 9.75 20.22
19.76 19.76 19.74 19.74
C 0.14 C 0.13 C 0.05 C 0.48
C 0.38 C 0.72

3+45
20.10 9.08 9.86 1.00
19.89 19.89 19.87 19.87
C 0.21 C 0.19 F 0.01 C 1.13
C 0.45 C 1.37

3+25 P.V.C.
0.54 9.22 20.00 1.35
20.04 20.04 20.01 20.01
C 0.50 C 0.18 F 0.01 C 1.84
C 0.74 C 1.58

LAMONT

	Rough	Curb	Curb	Rough
#1 ^B				
E. Chico = 2337 produced to East.				23.95 23.61
#2 = P.R.C.				C 0.34 C 0.58
#1				
Sly. CHICO. 2+00 (Map)	5.05 23.70			2.77 23.22
on Lt. 1+82.24 = P.R.C.	C 1.35 C 1.59	23.55 - Rec.		F 0.45 F 0.21
1+62 ⁴⁶ = B.C.	4.77 23.21 C 1.56 C 1.80	3.19 23.21 F 0.02	22.76 22.72 C 0.04	2.57 22.72 F 0.15 C 0.09
1+12	4.20 22.13 C 2.07 C 2.31	C 0.12	1.88 21.66 C 0.22	2.00 3' 21.66 C 0.34 C 0.58
0+62	3.26 21.05 C 2.21 C 2.45	C 0.18	0.91 20.61 C 0.30	1.22 20.61 C 0.61 C 0.85
0+12 ^E of E.C.	22.90 19.97 C 2.73 C 3.17	20.11 19.97 C 0.14	9.81 19.56 C 0.25	0.95 19.56 C 1.39 C 1.63
0+00				
Nly. line FORTUNA =				

curbs - P-23

B.M. = 50' R.P. Cross to N.E. Prop + 7' 22
Mon. Chico + Lamont EL. = ~~23.03~~ 23.29

	Rough	Curb	Curb	Rough
1+85 E.V.C.	8.74 28.92 F 0.18 C 0.06	9.13 28.92 C 0.21	8.68 28.58 C 0.10	8.31 28.58 F 0.27 F 0.03
1+65 N.	8.66 28.29 C 0.34 C 0.61	8.49 28.29 C 0.20	8.12 27.87 C 0.25	7.97 27.87 C 0.10 C 0.34
1+45 N.	8.20 27.72 C 0.48 C 0.72	7.83 27.72 C 0.11	7.53 7.26 C 0.27	6.75 27.26 F 0.51 F 0.27
1+25 Nail	7.74 27.17 C 0.57 C 0.81	7.21 27.17 C 0.04	6.91 26.71 C 0.20	6.28 26.71 F 0.48 F 0.19
1+05 P.V.C.	7.03 26.74 C 0.29 C 0.53	6.80 26.74 C 0.06	6.30 26.24 C 0.06	5.93 26.24 F 0.31 F 0.07
0+69.9 on Rt	6.20 26.01 C 0.19 C 0.43	6.20 26.01 C 0.19	5.55 25.51 C 0.04	4.65 25.51 F 0.86 F 0.62
0+70.92 Lt.				
0+36.85				2' Back
#3B = E.C.	5.53 25.29 C 0.24 C 0.48	5.09 25.29 F 0.20	5.05 24.79 C 0.26	4.25 24.79 F 0.54 F 0.30
Mid. Curb	25.02			
#2 B.V.C.				
0+01 on Lt. Nly. CHICO. 0+00 =	5.08 24.50 C 0.58 C 0.82			4.25 24.00 C 0.25 C 0.49

P-23

Curb P-23

LAMONT

Elev. Curb - Reverse Curve

23

Lamont at chico

P-22-A

Left.

Right.

Changed
To Δ' offset.

N. E. LYT Lamont + P.B. Dr. =

35.07

0+36.85

E.C.

35.10 = bench mark

#5A

5.43

24.79

35.12 = (20.44 / 75)

25.129

C0.14

Def. = 9°-08'-07"

ch = 15.49

#4A

5.09

4.74

25.102

24.44

C0.07

C0.30

Def = 7°-23'

ch = 15.19

#3A

4.91

4.16

24.75

24.12

C 0.16

C0.04

Def = 5°-38'

ch = 16.59

#2A

3.73

23.79

F0.06

Def = 3°-45'-20"

ch = 16.59

#1A

3.80

23.60

C0.20

Def. 1°-52'-40"

ch = 16.59

#4

3.69

23.44

C0.25

Def 9°-08'-50"

ch = 16.35

P.R.C.

Pac. B. Dr. to East.

3+43.28

>

Pac. B. Dr. to west

330.27

End of Job.

3+21.71

33.46

Set for

2.61

33.43

Rake

33.51

α

10.90

2+76.2

176

2192

F0.16

1.52

31.92

F0.04

1.97

31.86

C0.11

0.75

31.86

F1.11

#3

3.64

23.30

C0.34

Def = 6°-52'

ch = 16.35

#2

3.25

23.22

C0.03

Def. 4°-34'-30"

ch = 16.35

2+30.6

1.71

N 0.02

C 1.29

1.44

30.42

C0.09

0.31

30.22

C0.09

9.42

30.22

F0.80

#1

(3' back)

ch = 19.75

23.55

2.89

22.96

F0.07

Def. 2°-14'-50"

Def. 2°-17'-0"

ch = 16.35

t.p. 29.67

1+62.4A = B.C. See page 22 Lt.

Rate 8.231

Curb Returns

Crown Pt. Dr. + Lamont

N.E. Return
 #3 EC. 10.20
 8.50
 18.41
 C 0.09
 #2 10.19
 8.34
 18.32
 C 0.02
 #1 11.02
 8.35
 18.23
 C 0.12
 #4 P.C.
 18.16
 B.C.

Lamont St.
 Lamont

E.C. 18.32
 18.50 on Lamont
 F 0.18

E.C. - 15.82
 18.05
 18.35
 F 0.30

E.C. - 31.65
 17.74
 18.19
 F 0.45

E.C. - 47.81
 18.03
 18.16
 F 0.13

0

S.W. Return

LAMONT

N.E. Ret.
 #3 EC. 11.78
 0.82
 20.99
 20.79
 F 0.17
 20.99
 #4 EC. 11.78
 0.80
 20.55
 20.70
 F 0.15
 20.70
 #1 EC. 13.07
 0.84
 20.80
 20.62
 C 0.04
 20.22
 #2 EC. 11.78
 0.74
 20.54
 C 0.12
 #1 EC. 11.78
 0.58
 20.58
 C 0.02
 1.00
 F 0.06
 B.C.

ROOSEVELT

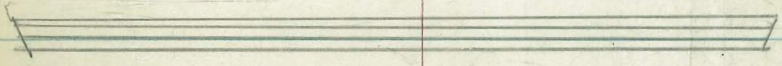
Curb Returns

Roosevelt + Lamont

S.E. Ret.
 #4 EC. 13.07
 1.11
 20.62
 C 0.49
 #3 EC. 11.78
 0.75
 20.59
 C 0.16
 #2 EC. 11.78
 0.74
 20.54
 C 0.20
 #1 EC. 11.78
 0.58
 20.48
 C 0.10
 B.C.

ROOSEVELT

LAMONT



S.W. Ret.
 #4 EC. 13.07
 1.11
 20.62
 C 0.49
 #3 EC. 11.78
 0.75
 20.59
 C 0.16
 #2 EC. 11.78
 0.74
 20.54
 C 0.20
 #1 EC. 11.78
 0.58
 20.48
 C 0.10
 B.C.

ROOSEVELT

LAMONT

C. b. Returns

Lamont + Fortuna

A. E. Ret.

LAMONT	EC.	11.78	11.78	13.07
	7.81			
	19.56			
	C 0.25			
	9.33			
	19.30			
	C 0.03			
	9.15			
	19.11			
	C 0.04			
	9.58			
	19.00			
	C 0.58			
	9.62			
	18.97			
	C 0.5			

FORTUNA

N. W. Ret.

LAMONT	EC.	11.78	11.78	13.07
	9.11			
	19.97			
	C 0.14			
	9.02			
	19.83			
	C 0.19			
	9.19			
	19.93			
	C 0.26			
	9.43			
	20.26			
	C 0.17			

Note.

Stake complete return.
Mark End of Lamont Job +
start of Chico job.

S. W. Ret.

LAMONT	EC.	12.37	12.37	11.18	13.56
	3.39				
	23.55				
	F 0.16				
	3.54				
	23.66				
	F 0.02				
	3.71				
	23.74				
	F 0.03				
	3.89				
	23.92				
	F 0.03				
	4.22				
	24.27				
	C 0.05				

S. E. Ret.

LAMONT	EC.	13.07	11.78	11.78
	7.80			
	18.26			
	C 1.54			
	7.02			
	18.38			
	C 0.64			
	9.18			
	18.46			
	C 0.72			
	8.95			
	18.56			
	C 0.39			

S. W. Ret

FORTUNA	EC.	10.86	10.86	10.86
	4.91			
	24.75			
	C 0.16			
	4.80			
	24.52			
	C 0.28			
	4.70			
	24.38			
	C 0.32			
	4.51			
	24.30			
	C 0.21			
	4.63			
	24.51			
	C 0.32			
	4.77			
	24.37			
	C 0.40			

LAMONT

LAMONT.

N. W. Ret.

FORTUNA	EC.	10.86	10.86	10.86
	4.91			
	24.75			
	C 0.16			
	4.80			
	24.52			
	C 0.28			
	4.70			
	24.38			
	C 0.32			
	4.51			
	24.30			
	C 0.21			
	4.63			
	24.51			
	C 0.32			
	4.77			
	24.37			
	C 0.40			

CHICO ST

From Page 18
Bik. 69 + Bik c. La Jolla Park

INDEXED

26

JAN 12 1954

4+93.24	Brk	34.85 127.36 C-7.49	6+28.24 Brk	70.10 166.52 C-3.58
4+83.24	Brk	32.20 123.91 C-8.29	6+18.24 Brk	4.20 162.78 C-1.52
4+73.24	Brk	9.79 121.15 C-8.63	6+08.24 Brk	60.53 158.52 C-2.01
4+63.24	Brk	27.37 119.08 C-8.29	5+98.24 Brk	7.15 154.61 C-2.54
4+50		24.40 116.80 C-7.60	5+88.24 Brk	4.30 151.40 C-2.90
3+97.8		15.40 107.85 C-7.55	5+78.24 Brk	51.95 148.89 C-3.06
Δ 10 ⁰ -59	Lt.		5+68.24 Brk	50.43 147.08 C-3.05
3+92.80	M.H.#11	107.00		
3+87.8		13.10 106.38 C-6.72		
3+50		6.83 101.67 C-5.16	P.O.T. 5+23.24 M.H.#12	2.52 140.51 C-2.01
3+00		101.43 95.45 C-5.98	5+03.24 Brk	7.63 131.61 C-6.02

17.15%

12.44%

10'pt
10'pt

Bik. 69 + Bik. C.
La Jolla Park

7+50. A1

80.18
172.40
C-7.78

7+00.

9.83
171.91
C-7.92

6+63.2A

80.55
171.55
C 9.00

Δ 79.2A - 30" L+1
6+58.2A M.H.#13

80.60 90° to
171.50 Back
C 9.10 Tally.

6+48.2A BIK

80.53
170.88
C-9.65

6+38.2A BIK

77.84
169.22
C 8.62

Soledad Ave.

27

Δ 7° 43' RT
2+66.73 M.H.#15

INDEXED
JER
JAN 19 1911
188.60

2+61.73

~~83.94~~
188.27 188.27
C-5.65

2+50

E.C. 2+16 90 42
185.33
C 5.09

~~82.99~~ 294
187.52 187.52
C-5.46 C 5.42

2+00 1+83

(2% Curv) 1+83 8.31
183.22
B.C. C 5.09
1+50

~~89.84 TR~~
184.31
C 5.53

1+00

0+50

0+05

0+00 = M.H.#13

Line change
turned in to
office -
S.T. 37.0
 Δ 12°

~~576~~ C.09
181.11 181.11
C 4.59 C.4.98

~~82.86~~ 82.84
177.90 177.90
C-4.96 C 4.94

~~81.60~~ 81.95
174.70 174.70
C 6.90 C. 7.25

~~80.55~~
171.82 171.82
8.93

171.50

Δ 60-35' M.
5+50.11 = M.H. #16

210.99

5+45¹¹

6.52
210.60
C-5.92

215.09 T.R.

5+00

12.87
207.03
C-5.84

4+50

7.28 TR
203.08
C-4.20

4+00

203.61
199.13
C-4.48

3+50

200.45
195.18
C-5.27

98.70 T.P.

3+00

7.18
191.23
C-5.95

2+71.73

94.74
189.00
C-5.74

END of Pipe
6+50.11

22.77
217.69
C-5.08

6+00.11

9.83
214.33
C-5.50

5+55.11

9.09
211.32
C-5.77

Sewer

Torrey Pines

= 2+75.77 Ahead.

Δ 30-42 Lt. Also - B.C.

2+77.77 M.H.#8

2+66.77

2+50

2+00

1+50

1+00

0+50

0+2A BHK

Pump House
0+00

INDEXED

JER

RNER 500053
Fwd. Tang.

100.86 X
95.03 113'
C 5.83

100.43 X
94.70 115'
C 5.73

9.24 X
93.61 12.5'
C 5.63

5.76 X
90.36 16'
C 5.40

92.69
87.11
C 5.58

9.47
83.86
C 5.61

7.86
80.61
C 7.25

86.58
78.92
C 7.66

85.76
75.67
C 10.09

5+06.10

Δ 20°-23' RT.
5+01.10 M.H.#7

4+96.10

4+50

4+08.74 = E.C.#4

3+75.49 #3

3+42.30 #2

3+00

3+09.01 #1

4+Parts (33.24) each

T 66.02

R = 854.93

Δ 8°-54'-A on

A 124%

A 124%

111.73

106.33

C 5.40

106.00

111.55

105.77

C 5.78

109.99

103.83

C 6.16

9.38
102.08

C 7.30

107.91

100.32

C 7.59

107.13

98.56

C 8.57

100.01

96.80

C 9.21

17 curb
12³ R.P. cross
111.27

12³ R.P. cross
in diamond.
on curb
EL = 108.19

Torrey Road & Cowrie St

=
2 Δ 19°-05'-30" RX
7+8112 = M.H.#4 120.90

10+57.55 ^{9.20}
140.57
C-8.63

2 7+76.12
6.44
120.61
C-3.83

Δ 23°-27' RX
10+52.55 M.H.#5 140.17

2 7+50
23.80
119.15
C-4.65

10+47.55
47.92
137.80
C-8.12

2 7+00
21.54
116.35
C-5.19
117.86 T.P.

10+00
43.92
136.43
C-7.49

1 6+50
7.23
113.54
C-3.69
51.61%

9+50
40.26
132.88
C-7.38

1 6+00
3.83
110.74
C-3.09

9+00
37.46
129.33
C-8.13
7.10%

0 ~~5+65.33~~

8+50
32.82
125.78
C-7.04

Δ 107°-11' LF
0 5+60.33 = M.H.#3
13.21
108.51
C-4.70

8+00
8.58
122.23
C-6.35

P
0 5+55.33

7+86.12
7.50
121.25
C-6.25

Courie St.

INDEXED

JER
DEC 15 1953

123+175
13+00

13,30%

12+72.53

72.54
163.90
C-8.64

66.93
157.92
C 9.01

Δ 7°38' - 24" AX.

12+67.53 = M.H.# 157.26

12+62.53

55.47
156.88
C 8.59

12+50

63.95
155.88
C 8.07

12+00

58.97
151.91
C 7.06

11+50

7.95%

55.07
147.94
C 7.13

11+00

51.94
143.96
C-7.98

S. 66° 00' 00" W. 1/4 Sec. 14, T. 51. N.

End of pipe

13+67.53

9.79
170.56
C 9.23

13+50

Torrey Road

East of Cowrie St.

INDEXED

15 1953

DFC

2+53.38 #A = E.C.

22.44 51
118.110 RT
C 4.34

2+18.77 #3

20.40 51
116.79 RT
C 3.41

1+84.15 #2

A 21°
R 377.8
T = 70.02

1+49.53 #1

A Parts 34.62 each.

9.00
115.28 5' RT
C 3.52

7.92
114.17 6' RT
C 3.75

1+1A.91 = B.C.

6.68
112.86 C
C 3.82

1+00

6.15
112.29 C' RT
C 3.86

0+50

4.57
110.40 C
C 4.17

0+00 = M.H. #3

12.87
108.51 C
C 4.36

End. of Pipe

5+05.64

56.26
143.97
C 12.29

4+70

50.38
140.98
C 9.40

4+30

46.23
137.62
C 8.61

3+96.84

41.01
134.83
C 6.18

Δ 90° RT
3+91.84 = M.H. #1

~~41.01~~
~~134.83~~
~~C 6.60~~

3+86.84

41.01
133.59
C 7.42

3+50

34.34
127.53
C 6.81

3+09.34

26.47
120.83
C 5.64

Δ 112°-03' RT
3+04.34 = M.H. #2

120.01

2+99.34

25.50
119.84
C 5.66

3.78%
2

8.4%

16.46%

5' RT

Locust Street
Oliphant "
Newell "

Water line Oliphant

33

INDEXED
JER
DEC 15 1958

End.

2+10

41.20
35.47
C 5.73

1+00

17.20

1+90

5.76
31.00
C 4.76

0+90

8.55
14.92
C 3.53

1+70

9.84
26.52
C 3.32

0+80

15.40

1+60

0+70

7.19
13.60
C 3.58

1+50

4.68
22.67
C 2.01

0+60

17.10

1+40

0+40

13.80

1+30

22.36
19.45
C 2.91

0+25

4.72
11.35
C 3.37

1+20

0+00

2.99
10.00
C 2.99

1+10

20.16
16.87
C 3.29

Sewer Laterals

• Oliphant St.

o+o = wly. line Locust.

INDEXED
JER
DEC 15 1953

1+70 Lt. = #9

30.08
25.38
C 4.70

1+20 Rt. = #8

20.38
16.86
C 3.52

o+20 Lt #7

6.15
10.64
C 5.51

Sewer Laterals Newell St. 34

o+o = wly. Rose crans. (Lats 5+6)

& o+o = " Locust per Lats #1 to #4

Lt. #1
2+70 Rt. = #2

3.88
28.00
C 5.88

36.69
29.00
7.69

2+20 Rt. = #3

31.18
28.00
C 3.18

1+70 Rt. = #4

5.87
22.00
C 3.87

wly Locust = o+o

2+70 Rt. = #5

13.15
8.81
C 4.34

2+20 Rt. = #6

12.42
7.81
C 4.61

wly Rose crans = o+o

INDEXED
JER
DEC 15 1953

INDEXED
 1950
 DEC 15 1953

THOMAS Ave.

3/24/53
 W.O. 32073.

wly Jewell

5+80

C.76

43.30

35

C 3.46

7.95

44.30

C 3.65

to Jewell

5+40

Water line

Ely line Jewell

5+00

9.11

45.35

C 3.76

stakes 5' south.

N.W. B.P. Grand + Jewell EL. = 51.8A

4+60

51.15

47.10

C 4.05

1+40

7.20

52.70

C 4.50

4+20

3.40

48.80

C 4.60

1+00

7.00

52.40

C 4.60

3+80

5.45

50.55

C 4.90

0+60

6.06

52.00

C 4.06

3+40

7.10

51.90

C 5.20

0+30

5.41

51.65

C 3.76

3+00

7.80

52.50

C 5.30

wly. Kendall

0+00

4.43

51.30

C 3.13

2+60

7.90

52.80

C 5.10

0-40

3.58

50.40

C 3.18

2+20

7.80

52.90

C 4.90

0-80

52.92

49.50

C 3.42

1+80

7.58

52.90

C 4.68

Ely line

Kendall

INDEXED Water Laterals

DEC 15 1953 Thomas Ave 3/24/53

stubs 1' North of curb

" 5' RT to water service

" set to curb grade

B.M. = S.E. 30' Ob. Rad cross Jewell
to Thomas EL = 55.10

Fire Hydt. S.E. Cor. Jewell 49.85 Ob.
49.04 Grade

4+70

8.35
49.82
F0.97

4+10

1.76
51.92
F0.16

3+70

5.31
53.64
C1.67

1+95

8.42
56.35
C 2.07

Sewer Extension (6" pipe)
Collingwood Drive at Loring St.

C.H.S.
B999
Schelin

W.O. 20009
3-31-53

INDEXED
JER
JAN 12 1954

37

1+85 D.E.

42.09
236.35
C-5.74

1+50

41.04
236.00
C-5.04

1+25

40.53
235.75
C-4.78

1+00

9.83
235.50
C-4.33

0+75

9.62
235.25
C-4.37

0+50

9.77
235.00
C-4.77

0+25

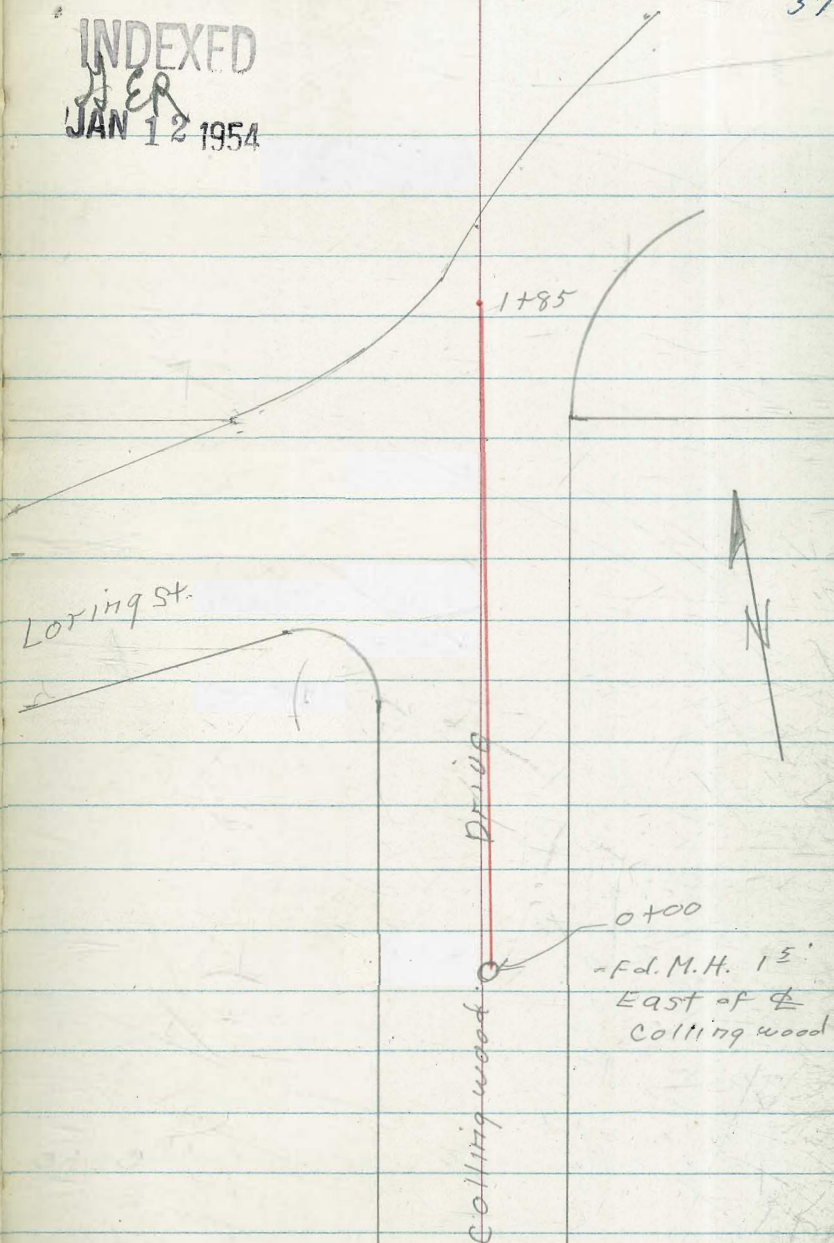
40.02
234.75
C-5.27

0+00 Exist. M.H. EL=234.23

40.42
234.50
C-5.92

B.M. = Existing M.H. I.E.

EL = 234.23



INDEXED
JER
JAN 12 1954

Alloy BIK 2 }
" BIK 27 }

Ocean Beach
A-7-53
W.O. 31821

(BIK#2)

0+00 = Wly line Guizot

1+40 20.00 7.52
120.00 119.70
X F0.18

1+20 2.67 1.40
122.03 121.73
C 0.64 F0.33

1+00 4.61 3.88
124.36 124.06
C 0.25 F0.18

0+80 6.92 7.52 N-
127.15 126.85 0.55
F0.23 C0.67

0+60 X-1' 31.00 8.75 (X-
129.16 128.86 2.90)
C-1.84 F0.11

0+40 X-104' 3.75 0.36 N
130.83 130.53 -0.70
C 2.92 F0.17

0+20 X-1' 4.14 1.78
132.17 131.87
C 1.97 F0.09

0+00 133.18 132.79

Wly. Guizot

124.92 S.W. B.P. Cape May + Guizot 38

75.98 - S.W. B.P.

4+15 5.37 4.96
103.43 103.13 N-0.15
C-1.96 C 1.83

3+77^E 4.48 6.51 X-0.40
104.15 103.85
C 0.33 C 2.66

3+40 5.24 5.77
104.86 104.56 N-0.60
C 0.38 C 1.21

3+20 6.31 5.77
105.38 105.08 N-0.45
C-0.93 C-0.69

3+00 7.09 7.53
106.21 105.91 N-0.10
C-0.88 C-1.62

N-0.50 8.00 7.75
2+80 107.36 107.06
C 0.64 C 0.69

N-0.86 9.77 8.80
2+60 108.81 108.51
C 1.16 C 0.129

D-1' 0.14 10.34
2+40 110.56 110.26
F0.52 C 0.01

N. 41 in 6.02 16.14 N-0.04
1+90 115.28 114.98
C 0.74 C-1.16

Alley BIK 2 PB.

10231

Sewer Laterals BIK 2 OB 39
+27 OB

Ely Froude
6400

85.91 85.32

5+80

90.12 9.18 N
87.95 87.65 11nc
C 2.17 C 1.53

5+60

1.36 3.68 N.
90.50 90.20 -0.20
C 0.86 C 3.48 TN

5+35

4.72 4.71 N.
93.90 93.60 11nc
C 0.82 C 1.11

5+15 X-2

7.96 100.33 N-0.10
96.49 96.19
C 1.47 C 4.14

4+95 D-1

9.46 9.80
98.69 98.39
C 0.77 C 1.41

4+75 D-1

1.79 0.55 D-2
100.48 100.18
C 1.51 C 0.37

4+55

3.02 1.30
101.87 101.57
C 1.15 C 0.27

4+35

4.75 4.56 N
102.86 102.56 -0.20
C 1.89 C 2.00

Lats. BIK. 3.

5+80 RT=#5

42.70
37.00
C- 5.70

5+30 RT=#4

44.86
39.80
C- 5.06

3+80 RT=#3

51.89
46.47
C 5.42

Lats. BIK 2

5+55 RT=#2

91.97
86.60
C 5.37

5+45 Lt.=#1

91.68
87.56
C 4.12

				4+40	^D 2' 7.04 48.46 C 0.58	8.77 48.16 C 0.61	N-0.05'
2+40 P.V.C.	X 2' 2.44 62.46 F 0.02	2.70 62.16 C 0.54	^D 2'	4+20	^D 2' 50.02 49.41 C 0.61	9.40 49.11 C 0.35	N-1.10
1+95	^D 3' 8.10 67.46 C 0.64	7.12 67.16 F 0.04	^D 2'	4+00 P.V.C.	^D 2' 0.42 50.44 F 0.02	0.30 50.14 C 0.16	
1+50	^D 2' 2.37 72.46 F 0.09	1.73 72.16 F 0.43	^D 2'	3+60 E.V.C.	2.51 52.59 F 0.08	2.57 52.29 C 0.28	
1+05	N -0.165 7.50 77.46 C 0.04	77.16		3+40	^D 2' 4.05 53.75 C 0.30	3.86 53.45 C 0.41	^D 2'
0+60 E.V.C.	N -0.34 2.94 82.45 C 0.49	2.41 82.15 C 0.26		3+20	^D 1' 5.60 55.11 C 0.49	5.43 54.81 C 0.62	X-2'
0+40	N -0.30 5.75 84.17 C 1.58	4.75 83.87 C 0.88		3+00	^D 1' 7.34 56.66 C 0.68	6.66 56.36 C 0.66	^D 2'
0+20	N -0.20 0.56 84.89 C 1.67	5.37 84.59 C 0.78	N-0.20	2+80	^D 2' 8.56 58.40 C 0.16	8.38 58.10 C 0.29	H-2
wly. Froude 0+00 P.V.C.	N -0.20 0.56 84.62 C 1.71	84.32 C 1.71		2+60	^D 10' 60.47 60.33 C 0.34	0.57 60.03 C 0.54	^D 2'

Alley BIK, 27 Ocean Beach

41

Ely. line Ebers

Map. dist.

6+00 F.V.C.

40.90

40.79

	x	3.99	2.91 ^D
5+80	-0.18	42.36	42.13 ^L
		C 1.63	C 0.78

	x	5.12	3.72 ^D
5+60	-0.20	43.45	43.20 ^L
		C 1.67	C 0.52

	N	5.99	4.69 ^D
5+40	-1.33	44.43	44.17 ^L
		C 1.56	C 0.52

	x	6.00	5.05 ^D
5+20 P.V.C.	3'	45.30	45.00 ^L
		C 0.70	C 0.05

	N	7.18	6.05 ^D
4+80 F.V.C.	-0.20	46.80	46.50 ^L
		C 0.38	C 0.45

	N	8.14	7.40 ^D
4+60	0.00 in.	47.59	47.29 ^L
		C 0.55	C 0.11

OLIPHANT

Locust - west

4/15/53

INDEXED

DEC 15 1953

	So. cl.	No. cl.
1+70	9.22 29.92 F0.70	9.64 29.92 F0.28
1+50	5.40 26.07 F0.67	5.91 26.04 F0.13
1+30	2.16 22.85 F0.69	2.80 22.78 C0.02
1+10	9.74 20.27 F0.53	9.74 20.15 F0.21
0+90	7.89 18.32 F0.43	7.80 18.13 C0.33
0+70	6.61 17.00 F0.39	6.54 16.73 F0.19
0+25 = cl. E.C.	4.46 14.75 F0.29	4.04 14.28 F0.24
wly Locust Mid arc.	3.87 14.05 F0.18	3.33 13.60 F0.27
wly Locust 0+00-	3.48 13.50 Moot	2.91 12.92 Moot

	So. cl.	No. cl.
N.S. cl. Back of End of Job.		
2+08.37		
Ely. face N.S. cl.		
2+07.87	8.40 38.70 F0.30	8.45 38.70 F0.25
1+90	3.69 34.40 F0.71	2.95 34.40 F0.55

Locust St.
 oliphant to Newell.

INDEXED
 JER
 JAN 12 1954

Locust St.
 Newell to Macaulay

43

	Ely. ob.	wly. ob.
Ely. Newell 2+00	3.73 13.78	4.85 14.90
Mid Arc.	3.68 13.70 F0.102	4.46 14.80 F0.34
1+75 B.C.	3.57 13.62 F0.105	4.42 14.70 F0.28
1+25	3.36 13.30 F0.106	4.20 14.30 F0.10
0+75	2.85 12.98 F0.13	3.64 13.90 F0.26
0+25 E.C.	2.48 12.66 F0.18	3.14 13.50 F0.36
Mid Arc.	2.50 12.61 F0.11	3.22 13.42 F0.20
sty. oliphant 0+00	TJR 12.54 12.57 Meat	3.31 13.34 ✓

	Ely. ob.	wly. ob.
Ely. Locust. #3	6.95 17.00 F0.105	8.33 18.67 F0.34
Ely. Macaulay #2	7.01 17.05 F0.104	8.07 18.30 F0.23
#1	6.75 16.95 F0.119	7.87 18.00 F0.13
1+75 B.C.	6.60 16.80 F0.20	7.43 17.80 F0.37
1+25	4.76 15.97 F0.21	6.65 16.97 F0.32
0+75	4.83 15.14 F0.31	5.87 16.14 F0.27
0+25 E.C.	4.10 14.31 F0.21	4.96 15.31 F0.35
Mid arc.	3.93 14.12 F0.19	4.90 15.15 F0.25
sty. Newell 0+00	3.87 13.92 Meat	4.95 15.00 Meat

Storm Drain
Sly. End Cushman Pl.

INDEXED
DEC 15 1953
No. 20979
5-19-53

Ref. { sheet 9525-L
" 4552-B
F.B.# 1862-P59
" 2213-P-2

Elev. = 31.06
B.M. = Fly. step spike in pole # P.C. 4751
S.W. Cor. Cushman Pace + Cushman FB 1862
P60

storm drain stakes - 5' Rt. of \perp

2+50 } 6.04%
30.32
29.76
C 6.56
2+00 } 6.04%
34.24
26.74
C 7.50

1+77.40 = \perp Cushman Pl.

1+50 } 6.04%
9.21
23.72
C 5.49

1+00 } 6.04%
26.31
20.70
C 5.61

0+50
24.55
17.68
C 6.87

= Head wall
0+00 = wly end
6.66
14.66
C 2.00

ditch stakes - 10' Rt. of \perp

4+18
40.24
39.6
C 0.64

3+80 $\frac{7}{2}$
9.96
37.15
C 2.46

3+43 $\frac{4}{2}$ 90° to
Fwd. tang.
9.71
35.40
C 4.31

= Δ 25° Lt.
start ditch
3+43 $\frac{4}{2}$ = End Drain
90 to back tang.
40.38
35.40
C 4.98

3+00 } 6.04%
8.26
32.78
C 5.48

Pave THOMAS St.

Kendall to Jewell.

INDEXED
JER
DEC 15 1953

Lt-S

cb 3' BK

cb 3' BK

45

1st-N

C.H.S.
Begg
altmat

5/21/53

W.O.# 32073

Ref. sheet #9779-L

stakes set 5' back of prop. unless
Noted.

B.M. = N.W.B.P. Grand + Jewell EL=51.84

1+60	56 ⁵⁰	56 ⁶¹ C011	56 ³⁰ F010	56 ⁴⁰
1+40	6.71 56.39 C0.32	56 ⁵³ C014	56 ⁵⁴ C018	8.21 56.36 C1.85
1+20	56 ²⁴	56 ³⁸ C014	56 ⁴⁵ C021	56 ²⁴
1+00	7.20 56.10 C1.10	56 ²¹ C011	56 ¹¹ C011	7.95 56.10 C1.85
0+80	55 ⁹²	56 ²⁰ C028	56 ⁰⁵ C013	55 ⁹²
0+60	B.O.C. 3' in 6.25 55.75 C0.50	55 ⁹¹ C016	55 ⁶⁸ F027	7.52 55.75 C1.77
0+30	5' in 5.74 55.40 C0.34	55 ⁴⁴ 55 ⁴⁵ C013	55 ⁴⁴ 55 ³⁴ F010	6.72 55.42 C1.90
0+10	ab. B.C. 55.13	54 ⁸⁶ F027	54 ⁷² F041	55.13
0+00 wly. Kendal	5.23 55.05 C0.18	54 ⁸⁶ F019		5.25 55.09 C0.16

Thomas

4-5 C6

5631

C6

RT-N

3+60

55⁰²5539
C0375434
C030

5404

3+40

7.07
55.61
C-3.465585
C0245489
C0216.41
54.68
C 1.73

3+20

56⁰²5609
C0075533
C017

5516

E.V.C.
3+008.63
56.21
C-2.425646
C0255578
C0346.65
55.44
C 1.21E.V.C.
2+608.47
56.46
C 2.015673
C0275611
C02256.59
55.89
C 0.70

2+40

56⁵⁴5685
C0315642
C032

5610

2+20 x 0.2
Back8.19
56.60
C 1.595681
C0215654
C0307.79
56.24
C 1.55

2+00

56⁶¹5703
C0425649
C015

5634

1+80

8.63
56.57
C 2.065646
F0115652
C0128.36
56.40
C 1.96

Thomas

4-5 C6

C6

RT-N

46

Ely Jewell
5+00C6 B.C.
4+90

4944

4911
F0224792
F052

4844

4+53³³51⁰⁴5121
C0175002
F002

5004

4+16⁶⁶52⁶⁴5297
C0335176
C012

5164

Jewell
Ely. 1146
5+0052.46
49.07
C 3.397.26
48.10
F 0.84

4+60

5.16
50.79
C 4.377.67
49.82
F 2.15

4+20

6.88
52.51
C 4.374838
51.53
F 3.15E.V.C.
3+807.81
54.24
C 3.575447
C0235358
C0371.33
53.24
F 1.97omit
take above

INDEXED
DEC 15 1953

Curb Returns

Thomas & Jewell

C-1 46 4961 4810 Prop end

C-102 4934 4832 3/5

C-092 4962 4820 2/5

C-079 4986 4907 1/2

F-027 4912 4944 BC
H-190 Thomas

SE Ret.

4732 4662 F-020

4754 4712 F-042

4728 4727 F-001

4810 4781 F-029

4844 4722 F-052

NE Ret.

C-125 4875 4750 Prop end

C-066 4801 4735

C-020 4740 4720 Meet existing

4710
SW Ret

4671 4633 F-038

4676 4648 F-028

4627 4639 F-038

4671
NW Ret

Curb Returns

47

Thomas & Kendall

INDEXED
DEC 15 1953

G 5482 5482 add

C-019 5506 5487

C-015 5509 5494

C-020 5525 5505

F-027 5486 5513 EC
0-110 Thomas

SW Ret

5420 5438 F-052

5497 5437 F-060

5500 5420 F-020

5509 5445 F-064

5513 5472 F-041

NW Ret

C-011 5386 5375 Prop end 5390 5366 F-024

F-023 5360 5363 5392 5362 F-020

F-002 5340 5342 Meet existing 5385 5353 F-022

5319
SE Ret

5368
NE Ret

Muir + West Pt. Loma Blvd

Sewer

C-153
 CHS Ref 10603-L
 F.B. 2206-P30

B.M. = NEBR

2+04
 -0.08
 -3.00
 C 2.92
 Voltara + W. Pt.
 Loma Blvd.
 El. = 1.52

1+77
 0.09
 -3.10
 C 3.19

1+50
 0.06
 -3.21
 C 3.27

1+23
 0.10
 -3.32
 C 3.42

0+96
 0.30
 -3.43
 C 3.73
 90° to Fuel Tang

Δ 123° 27' RX.
 0+96¹ M.H. #1
 0.17
 -3.43
 C 3.60
 90° to back Tang

0+48⁰⁵
 0.95
 -3.62
 C 4.57

0+00
 1.65
 -3.81
 C 5.46
 Existing stub
 on Muir.

INDEXED
 JCR
 JAN 12 1954

End of line

3+66.1 M.H. #2
 0.58
 -2.35
 C 2.93

3+39
 0.46
 -2.46
 C 2.92

3+12
 0.57
 -2.57
 C 3.14

2+85
 0.37
 -2.67
 C 3.04

2+58
 0.26
 -2.78
 C 3.04

2+31
 0.13
 -2.89
 C 3.02

INDEXED
JER
JAN 12 1954

Storm Drain

Alley BIK-240-M.B.

6-2-53

w.o. 20996

C.H.S.

Beggs
Schelin

Sheet A590-B.

(Revised same.)

9¹/₂ ft. to line of face, of

M.B. storm drain - box culvert.

outlet,
for M.B. storm drain
south bulkhead wall
2401 = Nly face

- 0.29

- 4.20

C 3.91

49

on $\frac{1}{2}$
Nail

- 0.25

- 4.20

C 3.95

1+77.56 E.C.

- 1.05

- 4.10

C 3.05

1+65.75 Mid Curve

- 0.32

- 4.05

C 3.73

R = 30

1+54 = B.C. Lt. $\Delta = 45^\circ$

+ 0.05

- 4.00

C 4.05

1+25

- 0.15

- 3.88

C 3.73

1+00

+ 0.43

- 3.78

C 3.35

0+75

- 0.32

- 3.67

C 3.35

0+50

- 0.68

- 3.57

C 2.89

0+25

- 0.95

- 3.47

C 2.52

0+00 = Existing Stub

- 1.04

- 3.37

C 2.33

15th & Broadway
Curbs & Gutter

6-4-53
W.O.# 21069

Sheet 4808-B.

INDEXED
MER
JAN 12 10 51

Gutter 0+00 = 20' east of Ely line 15th St N.W. Ret.

Broadway
57.76 - Existing

780
5782
5782
E 0.102 - 9426

Mid
Curbs
57.89 - Existing
15.4

Wly end	pave plan Cr. 57.18		
1+25	57.18	57.15	Meet Existing
1+00		00.30	Nail 5' S. of \pm
0+75		00.52	
0+60 \pm 15 th		00.51	
0+50		00.53	
0+25		00.32	
0+00 =	plan Cr. pave 56.74	56.74	Meet Existing

Nly Gutter

Alley Blk 200
Pacific Beach

INDEXED

MER
JAN 12 1958

6-4-53

W.D. 32098

Sheet 9506

FB. 1753-P.7

0+00 = Wly. line Haines

B.M. = S.W. L&T Garnet + G rest hair

B.M. #2 = 10' R.P. to S.W. 4' L&T. + "

EL = 52.61

rest hair

EL = 52.66

Lt.		Rt.	
South	#	North	

1+20	X-1'	0.90 69.66 C 1.24	70.57 69.96 C 0.61	D-2'
------	------	-------------------------	--------------------------	------

1+00	X-1'	70.97 69.85 C 1.12	0.93 70.15 C 0.78	D-2'
------	------	--------------------------	-------------------------	------

0+80	X-1'	0.96 70.06 C 0.90	1.34 70.36 C 0.98	N. -0.20
------	------	-------------------------	-------------------------	-------------

0+60	D-2'	70.00 70.19 F 0.19	1.30 70.49 C 0.81	D-2'
------	------	--------------------------	-------------------------	------

0+40	D-2' P.V.C.	69.74 70.03 F 0.29	1.16 70.33 C 0.83	b.1'
------	-------------	--------------------------	-------------------------	------

0+00	N-2'	9.95 69.83 C 0.12	2.31 70.03 C 2.28	N. 1.83 IN
------	------	-------------------------	-------------------------	------------------

Lt. # Rt

3+00	D-2'	E.V.C. 4.10 64.37 F 0.27	4.82 64.67 C 0.15
------	------	-----------------------------------	-------------------------

2+80	N line	5.42 65.25 C 0.17	6.16 65.55 C 0.61	N-0.25
------	--------	-------------------------	-------------------------	--------

2+60	D-2'	6.22 66.06 C 0.16	6.45 66.36 C 0.09	D-2'
------	------	-------------------------	-------------------------	------

2+40	N-2'	6.40 66.80 F 0.40	7.75 67.10 C 0.65	X-2'
------	------	-------------------------	-------------------------	------

2+20	N-2'	6.88 67.47 F 0.59	8.32 67.77 C 0.55	X-2'
------	------	-------------------------	-------------------------	------

2+00	N-2'	7.37 68.06 F 0.69	8.68 68.36 C 0.32	N-0.15
------	------	-------------------------	-------------------------	--------

1+80	N-2'	8.00 68.58 F 0.58	9.65 68.88 C 0.77	N-0.15
------	------	-------------------------	-------------------------	--------

1+60	N-2'	8.54 69.02 F 0.48	0.15 69.32 C 0.83	N-0.15
------	------	-------------------------	-------------------------	--------

1+40	N-2'	8.67 69.38 F 0.71	70.10 69.68 C 0.42	D-2'
------	------	-------------------------	--------------------------	------

Restaked as shown
 To be torn out & put in to
 grade on sheet 9331-L

5+00 as per 9331-L
 Staked → 55165 55135 55185 } Note
 As built = 56.68 ← 57.04

	LT.	±	RT.	
Ely Gresham				ob
5+00	7.87		7.08	7.08
staked	55.65		55.85	55.87
	C 2.22		C 1.23	C 1.21
A+50 0-1'	8.22		9.12	N=0.02
	57.83		58.05	
	C 0.39		C 1.07	
A+00 0-2'	9.77		0.18	0-2'
	60.01		60.26	
	F 0.24		F 0.08	
3+50 0-2'	1.85		2.71	0-2'
	62.19		62.46	
	F 0.34		C 0.25	
			C 1.16	

A+60 57.8 B.L.

A+45 58.58
 Apron

A+45 Lt. = (S) #1

8.22
 51.30
 C 6.92

2+A5 Lt. = (S) #2

66.56
 56.00
 C 10.56

INDEXED

BER A Day BIK 17-0.B.

JAN 12 1951

6-9-53

CHS

Begg

oltman

Schelin

Sheet 101AC-L

F.B. 2220-P10

0+00 = Wly line Froude

	Lt.	±	Rt.		Lt.	±	Rt.
	South		North				
				A+25 0.2'	2.71 72.66 C0.05		3.06 72.96 C0.10
				start 1' Excep- tion on Rt. A+00 0-2	4.70 74.53 C0.17		4.83 74.83 X
				3+75 0-2'	6.52 76.55 F0.03		7.02 76.85 C0.17
1+75 0-2'	6.32 95.97 C0.35		6.65 96.27 C0.38				0-2'
				3+50 0-4'	80.43 78.73 C1.70		9.44 79.03 C0.41
1+50 0-2'	8.06 98.06 X		9.83 98.36 C1.47				N -0.12
				3+25 0-2'	0.84 81.06 F0.22		2.61 81.36 C1.25
1+25 0-2'	9.34 99.97 F0.63		1.65 100.27 C1.38				N -0.08
				3+00 0-2	4.32 83.54 C0.78		4.67 83.84 C0.83
1+00 0-2'	1.81 101.69 C0.12		2.66 101.99 C0.67				N -0.18
				2+62.5 0-2'	7.27 87.38 F0.11		7.68 87.68 X
0+75 N.0.05	3.24 103.72 C0.02		5.04 103.75 C1.29				0.2'
				2+25 0.2'	1.39 91.22 C0.17		1.27 91.52 F0.25
0+50 N 0.05	5.26 104.66 C0.60		5.86 104.66 C0.79				0-2'
0+25 N.-0.10	6.97 106.10 C0.87		8.40 106.40 C2.00				N 0.12
				2+00 0-2'	3.14 93.69 F0.55		4.10 93.99 C0.11
0+00	106.98		108.48				0-2'

53

Alley BIK. 17 - O. B.

	Lt.	Rt.	
Ely Ebers 6+00	59.29	9.90 59.90	
5+75 N. -0.128	3.83 62.26 C15.7	5.36 62.56 C28.0	X -0.15
End 1' Exception 5+50 X-0.121	5.31 64.54 C0.77	6.96 64.84 C2.12	X -2'-3'
5+25 0.2'	6.23 66.44 F0.21	8.26 66.74 C1.52	X- 2'
5+00 0-2'	67.65 67.97 F0.32	9.25 68.27 C0.98	0.3'
4+75 0-2'	9.54 69.38 C0.16	71.52 69.68 C1.84	N 0.90 in alley
4+50 X-0.52	1.99 70.94 C1.05	2.58 71.24 C1.34	N 1.05 in alley

INDEXED
JER
JAN 19 1951

Alley BIK 7-O.B

Guizot to Froude

Bet. Narraganset + Del Monte

6-10-53
W.D. 31951

sheet 10145L
F.B. 2260-P2

		Lt.	Rt.						
					4+00	02'	3.50 161.81 C 1.75	4.08 161.96 C 2.12	02'
					3+50	02'	71.27 169.96 C 1.31	71.42 169.96 C 1.46	02'
1+70	D-2	1.85 200.05 C 1.80	0.18 200.01 C 0.17	D-V	3+25	0-2'	4.70 174.07 C 0.63	6.32 174.07 C 2.25	01'
1+50	X-2'	3.39 202.13 C 1.26	2.49 202.05 C 0.44	02'	3+00	02'	80.56 178.40 C 2.16	80.24 178.40 C 1.84	02'
1+30	X-0.30 IN	5.81 203.79 C 2.02	3.80 203.68 C 0.12	0-2'	2+75	02'	4.52 182.95 C 1.57	4.28 182.95 C 1.33	01'
1+10	D 0.1714	6.95 205.05 C 1.90	4.95 204.90 C 0.05	02	2+50	0-2	6.29 187.71 F 1.42	8.60 187.71 F 0.11 C 0.89	X-2'
0+90	X-2'	7.07 205.89 C 1.18	5.66 205.71 F 0.05	X-2'	2+30	0-2'	2.83 191.41 C 1.42	1.94 191.40 C 0.54	X-2'
0+45	02	8.36 207.35 C 1.01	7.78 207.06 C 0.66	02	2+10	02'	5.11 194.70 C 0.41	7.60 194.68 C 2.92	X-3.50
0+00	wly line Guizot	208.80	208.41		1+90	N.O. 30	9.28 197.58 C 1.70	7.93 197.55 C 0.38	02'

Alley BIK7 O.B.

Sewer laterals
 0-5' Rt. of end of Lot.

56

Ely. Froude

6+00		133.43	133.88	
5+80	0-2'	9.50 136.48 C 3.02	9.69 136.78 C 2.91	0-2'
5+30	0-2'	5.60 143.98 C 1.62	8.05 144.28 C 3.77	0-2'
5+10	0-1'	7.22 146.67 C 0.55	7.50 146.97 C 0.53	0-2'
4+90	0-2'	8.68 148.72 C 0.04	9.01 149.02 C 0.59	N- 0.36
4+70	0-2'	1.03 150.82 C 0.21	1.01 151.12 C 0.11	0-2'
4+50	0-2'	4.84 153.66 C 1.18	4.35 153.96 C 0.39	0-2'

4+70 Lt. = #2
 50.19
 146.16
 C 4.03

4+45 Rt. = #3

56.20
 149.32
 C- 6.88

2+90 Lt. = #1
 80.83
 174.65
 C 6.18

Alley BIK, 12 Sunset Cliffs

Guizot to Novara streets
between Granger + Osprey, str.

C.H.S.
Boeg
oltman
Schelin
6-12-53
W.O.# 31842
FB 2148-40
Sheet 9790-L

0+00 = Ely line Guizot

1+60 0.2' 5.53 5.91 0.2' 125.95 125.95 0.2' F0.42 F0.04

124.90 T.P.
P.O.C.
1+40 0.2' 23.52 24.76 0.2' 124.30 124.30 0.2' F0.78 C0.46

0+90 0.2' 17.64 20.71 0.2' 120.40 120.40 0.2' F0.76 C0.31

T.P.
0+40 0.2' 115.98 596 0.2' 116.50 116.50 0.2' F0.52 F0.54

0+20 0.2' 4.03 4.80 0.2' 114.25 114.40 0.2' F0.21 C0.40

0+00 10.62 1.37 118.58 111.31 Meet Meet

T.P. Nail in 1/4 75H. of 1+90 = 130.39

57

INDEXED
JER
JAN 12 1954

5+70 0.2' 8.30 7.75 0.2' 167.35 167.35 C0.95 C0.38

4+70 0.2' 861.15 61.30 0.2' 161.47 161.47 F0.32 F0.17

T.P. 165.30
4+20 0.2' 4.81 5.27 0.2' 155.60 155.60 F0.79 F0.33

3+70 0.2' 50.84 50.25 0.2' 149.72 149.72 0.2' C-1.12 C0.53

7147.81
3+20 M.O.60 4.95 6.79 0.2' 143.85 143.85 0.2' C-1.10 C-2.94

T.P. 139.01
2+70 0.2' 7.97 8.34 0.2' 137.97 137.97 0.2' X C0.37

E.V.C.
2+20 W-0.50 6.21 1.80 0.2' 132.10 132.10 0.2' C.A.11 F0.30

2+00 0.2' 0.04 9.29 0.2' 129.85 129.85 0.2' C0.19 F0.56

1+80 0.2' 8.78 6.85 0.2' 127.80 127.80 0.2' C-0.98 F0.95

Alley BIK 12 - Sunset Cliffs

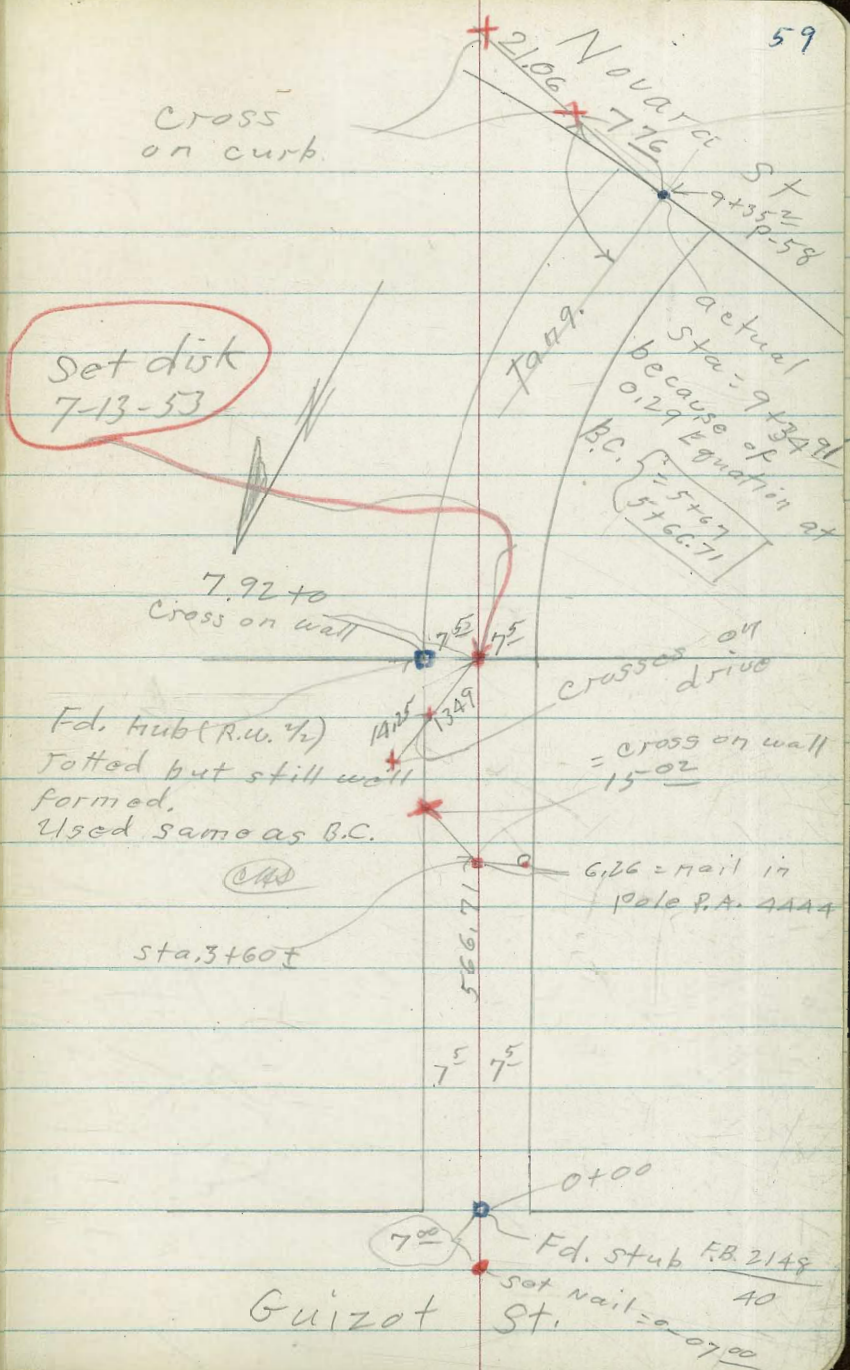
17°-08'-30" 7+60	Wall +3' BK	2.28 200.52	200.27 200.52	□ 2'	= Fd. Nail Novara Pauc. = NY. Cd 90			
Sewer # 11-19-76		C 1.76	F 0.25					
15°-22' 7+40	nail 2' BK	200.81 198.19	8.74 198.19	199.04 T.P. N-0.50	32°-42'-30" 9+35.2 0-2'	4.48 214.44	3.32 213.00	Curb
13°-35'-30" 7+20	X-1.55'	7.40 195.66	6.70 195.66	N-0.50	30°-15' 9+07.6	2.00 212.75	10.95 211.60	
		C 1.174	C 1.04		19.00 C 2.40	C 1.25	F 0.65	
11°-49' 7+00	N-1.70	5.26 192.93	3.57 192.93	0-2'	27°-48' x on Wall 0.50 BK 8+80 12.47	12.47 210.76	08.83 210.80	8.83 209.94
		C 2.33	C 0.64		N 209.94 C 2.43	C 1.71	F 1.41	F 1.11
10°-02.5" 6+80 P.V.C.	N-1.80	71.62 190.00	90.60 190.00	0-2'	26°-01'-30" 8+60 x wall 0.30 BK 9.30	9.30 209.30	208.50 209.17	7.50 208.73
		C 1.62	C 0.60	T.P. 189.71	N 209.73 C 0.57	Grade	F 1.67	F 1.23
6°-29.2" 6+40	X-1'	8.56 183.95	5.23 183.95	0-2'	24°-15' 8+40 + wall 0.50 m 6.95	6.85 207.84	5.17 207.84	5.37 207.52
		C 4.61	C 1.28		F 0.67	10.99	F 1.47	F 2.15
2°-56' 6+00	□ 2' BK	8.07 177.90	9.14 177.90	180.50 T.P. □ 2'	22°-28'-30" x Wall 35' Back 8+20	6.90 206.31	5.35 206.31	□ 2' BK
		C-1.07	C 1.24			C 0.59	F 0.96	
5+67 B.C.	x.40 BK	175.86 173.60	74.11 173.60	T.P. □-2'	20°-42' x on Wall 0.26 in 8+00	5.40 204.58	4.30 204.58	□ 2' out
		C 2.26	C 0.51			C 0.82	F 0.28	
5+40	0.2' 15"	71.70 169.70	70.92 169.70	□ 2'	18°-55' + on line 7+80	3.65 202.65	3.84 202.65	□ 2' out
		C 2.00	C 1.22			C 1.00	C 0.19	

5.50 on pipe
 = 5.190
 0.41

11.10 on pipe
 = 10.871
 0.229

Ties Alley BIK 12
Sunset Cliffs

Set B.M. on P.K. Nail 0-7' - Alley.	6.57	110.45		
T.P.	9.27	117.02	0.53	107.75
T.P.	4.17	108.28	6.10	104.11
T.P.	1.19	110.21	13.25	109.02
	2.10	122.27	-	120.17
				S.E.B.P. Guizot & Point Loma



Alley Bk. 12 Sunset Cliff
Sewer Laterals.

8+46 Rt #5
5.25
202.00
C-3.25

#A in

7+58-N #3
9.26
195.52
C-3.74

5+45 Rt #2
70.92
167.40
C 3.52

3+05 Rt #1 in at Sta. 3+53 (Met this)
Run from house is

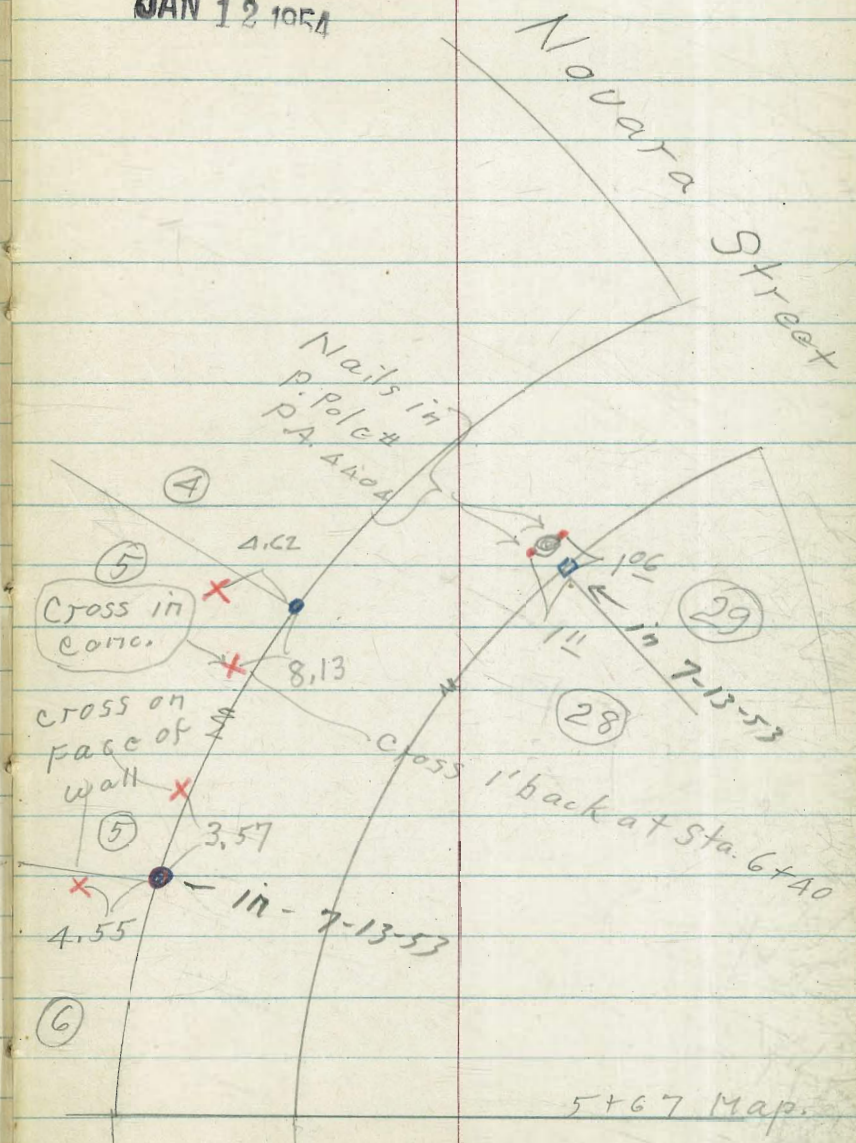
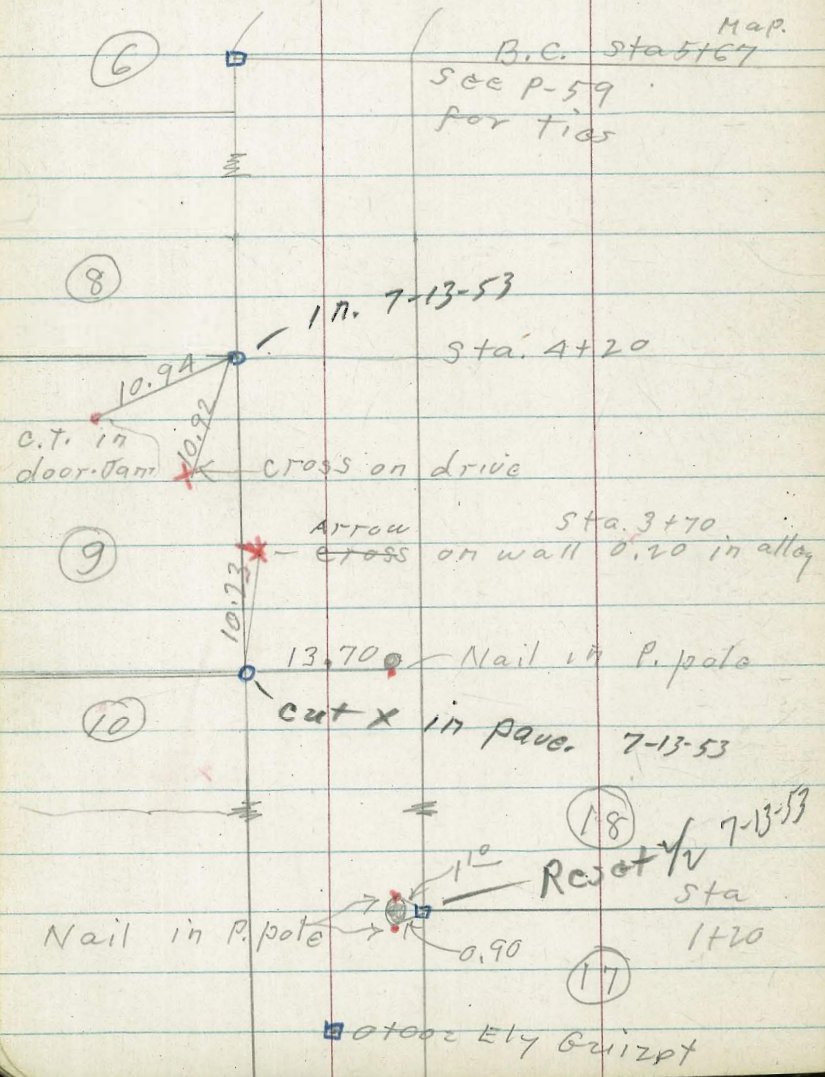
Ties to property pipes
Alley BIK. 12 - Sunset Cliffs

C.H.S.
Be99
oltman
Schelin

6/13/53

INDEXED
JER
JAN 12 1954

61



Por. Alley BIK 255 P.B.

INDEXED

C.H.S.
Begg
Oltman
Johns

JAN 19 1953

7-13-53
W.O. 20006

Profile # 773-A

sly side of alley
grade set at a point 75'
wly of Fannuel & also at a
point 114' wly of Fannuel st.

Sta 0+00 = wly line Fannuel

B.M. = N.W. 7' 1/4th Grand

& Fannuel (FB $\frac{2230}{14}$) EL. = 35.85

1+45 30.75
 30.62
 C 0.13

0+75 30.82
 30.83
 F 0.01

0+00

Alloy Blk. 158- P.B.

Cass
Ely line
5+00

Lt.

Rt.

63

7-23-53

W.O. 32089

B.M. = N.W.B.P. Diamond
+ Dawes E.L. 5212A
FB. 2194-P 16

Sheet
FB

7438-L
2194-P2

A+60 N-0.30

3.13
41.62
C 1.51

6.29
41.92
C 43.7

N-0.30

South

North

Lt.

Rt

A+15 D.V.

1.98
41.98
X

3.30
42.28
C 1.02

D 5'

INDEXED

NER

JAN 12 1954

3+95 D.V.

2.21
42.16
C 0.05

3.31
42.46
C 0.85

X-3'

1+39 X-2'

6.39
46.06
C 0.33

6.33
46.36
F 0.103
D.V.

3+75 X-2

2.95
42.39
C 0.56

3.42
42.69
C 0.73

X-3'

0+90 D.V.

6.95
46.83
C 0.12

7.38
47.13
C 0.25
D.V.

3+55 X-1'

3.06
42.66
C 0.40

3.61
42.96
C 0.65

X-3'

0+40 E.V.C. X-2'

7.74
47.61
C 0.13

8.48
47.91
C 0.57
X-2'

3+35 P.V.
P.V.

3.66
42.98
C 0.67

4.00
43.28
C 0.72

X-3

0+30 X-2'

7.86
47.75
C 0.11

8.51
48.05
C 0.46
X-2

2+86 D-V

4.05
43.75
C 0.30

5.15
44.05
C 1.10

D-2'

0+20 X-1'

7.89
47.88
C 0.01

8.67
48.08
C 0.59
X-2

2+37 N-0.07

6.82
44.52
C 2.30

5.66
44.82
C 0.84

X-2

0+10 X-1'

7.92
47.87
C 0.05

8.80
48.17
C 0.63
X-2

1+88 D-0.7

5.70
45.29
C 0.41

5.90
45.59
C 0.31

D-2'

0+01 = why
line Dawes

47.85

48.15

Sewer Laterals

Alley BIK 158 P.B.

0+00 = Wly line Dan

stubs 5' Rt. & Lateral. (on Prop.)

INDEXED
JAN 12 1954

3+90 Rt. #5 40.01

3+85 Lt. #6 42.74
37.20 39.78
C 5.54

3+40 Rt. #7 40.79

3+35 Lt. #8 43.37
38.37 40.57
C 5.00

2+90 Rt. #9 44.88 41.88
39.88 41.58
C 5.00 C 3.30

2+85 Lt. #10 44.03
39.03 41.35
C 5.00

2+15 Lt. #11 5.09 45.09
42.45 40.09
C 2.64 C 5.00

Alley BIK. 157 P.B.

Sheet 9438-L

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INDEXED
JAN 12 1954

2+00 12 1954

2+20 0-v

1+80 0-v

1+40 Btk 0-v

1+20 Btk 0-v

1+00 Btk 0-v

0+60 0-v

0+20 x-v

Wly. line Cass
0+00

Lt. South

7.50
36.98
C 0.52

8.02
37.41
C 0.61

7.96
37.85
C 0.11

8.41
38.29
C 0.12

8.79
38.52
C 0.27

9.16
38.79
C 0.37

9.49
39.36
C 0.13

0.40
39.94
C 0.40

40.38

Rt. North

7.82
37.28
C 0.54

8.32
37.71
C 0.61

9.36
38.15
C 1.21

8.67
38.59
C 0.08

8.78
38.82
C 0.16

7.44
39.09
C 0.32

40.60
39.66
C 0.94

3.92
40.24
C 3.68

40.76

x-4'

0-2'

N. 0.70

0-v

0-v

0-4'

x-2'

N-1'

Alley BIK. 15/7 Pacific Beach

Alley BIK 156 Pacific Beach 65

Sewer - Laterals

Bayard
Fly line
5+00

30.2
33.03

33.42

4+80 X-3'

4.60
34.45
C0.15

5.32
34.77
C0.55

4+60 X-3'

4.64
34.95
F0.31

5.97
35.25
C0.72

4+40 D-2'

5.10
35.05
C0.05

5.66
35.35
C0.31

P.U.C.
4+20 B-K D-2'

5.98
35.24
C0.74

5.85
35.54
C0.131

3+80 D-2'

5.72
35.67
C0.05

6.41
35.97
C0.44

3+40 D-2'

6.30
36.11
C0.19

7.50
36.41
C1.09

3+00 D-2'

6.39
36.54
F0.15

10.21
36.84
C3.37

4+90 RA #1

9.97
23.92
C-5.85

4+30 Lt #2

24.43

2+90 Lt #3

26.13

0+10 RA #4

28.46

Alley BIK 156

Pacific Beach

0+00 = wly line Bayard

Rod elevations on this page are 0.10 Low.

Cuts + Fills O.K.

INDEXED

JER
JAN 12 1954
2+40

Sheet # 9A37-L

		Lt.	Rt.		Lt.	Rt.
	0-2	1.25 31.48	1.89 31.78	0-2		
		FO.23 FO.13	CO.11 CO.21		Mission Blvd	28.50
	0-2'	1.54 31.94	2.65 32.24	0-2'	Ely line	
		FO.40 FO.30	CO.41 CO.51		5+00	
	T.P. 0-2'	32.77 32.40	3.26 32.70	0-2'	A+80 BIK ↓ online	9.28 28.73
		CO.37 CO.47	CO.56 CO.66			9.56 29.03
	0-2	3.12 32.86	3.52 33.16	0-2'	A+40 N-2'	9.38 29.19
		CO.26 CO.36	CO.36 CO.46			9.45 29.49
	0-2'	3.20 33.32	3.60 33.62	0-2'	A+00 0-2 ³⁵	9.83 29.65
		FO.12 FO.02	FO.02 CO.08			0.92 29.95
	0+40 BIK X-2	3.75 33.77	4.32 34.07	X-2'	3+60 T.P. D-2 ²⁰	9.18 29.75
		FO.02 CO.08	CO.25 CO.35			0.75 30.11
	0+20 BIK X-2'	3.71 33.62	4.30 33.92	0-1'	3+20 0-1 ¹⁸	0.28 30.57
		CO.09 CO.19	CO.38 CO.48			1.13 30.87
	0+00 wly Bayard	32.61	33.01		2+80 X-2.07	1.00 31.02
						1.39 31.32
						CO.26 CO.36
						CO.19 FO.19
						CO.44 FO.26
						CO.34 CO.44
						CO.26 CO.36
						CO.07 CO.17
						CO.07 CO.17

Alley Bk. 75-OB.
Bacon to Abbott Between

Cape May
+
Saratoga

UNCOVERED
SER
JAN 19 1954

Lt. =
50

Rt. = No

67

Sheet 9509-L

		Lt. = 50	Rt. = No				
				3+80 #2'	1.65 10.98 E0.67	1.14 11.18 F0.04	□ 2'
1+10	□ 2'	10.12 12.36 F2.24	3.67 N 12.53 -12'	3+40 #2'	0.96 11.34 F0.38	1.28 11.54 F0.26	□ 2'
1+00 P.V.C.	□ 2'	9.48 11.64 F2.16	3.21 N 11.87 -120	3+00 #2'	11.34 11.70 F0.36	11.72 11.90 F0.18	□ 2'
0+70 ENC.	□ 2'	9.44 9.16 C0.28	13.24 # 9.29 -2'	2+60 #2'	3.24 12.06 C1.18	2.74 12.26 C0.48	□ 2'
0+60	□ 2'	8.10 8.42 F0.31	11.87 # 8.53 2'	2+20 #2'	TIP 13.64 12.42 C1.22	3.08 12.62 C0.46	□ 2'
0+50	□ 2'	8.21 7.88 C0.33	8.90 # 7.97 2'	1+80 #2'	3.47 12.78 C0.69	3.50 12.98 C0.52	□ 2'
0+40	X 2'	7.36 7.52 F0.16	8.02 # 7.58 1'	1+40 EX.C.	2.11 13.12 F1.01	3.86 13.32 C0.54	□ 2'
0+30 P.V.C.	X 2'	7.35 7.35 X	8.10 # 7.39 2'	1+30 #2'	11.21 13.09 F1.88	3.65 13.30 C0.35	□ 2'
0+00 wly line Bacon		7.13	7.08	1+20 #2'	10.56 12.84 F2.28	3.78 13.04 C0.74	N -125

BIK 75-0.B.

L₁-2₁R₁
=N₁

Abbott.

Ely line

6+00

7.17

7.17

7.17

X

5+90

N₁-2.83

9.50

7.94

C 1.56

8.45

8.05

C 0.40

X

1'

5+80

D 2'

8.42

8.46

F 0.04

8.68

8.64

C 0.04

X

1'

5+70 P.O.C.

D 2'

9.02

8.75

C 0.27

8.89

8.95

F 0.06

X

1'

5+35

D 2'

9.37

9.32

C 0.05

10.11

9.52

C 0.59

X

-0.13

5+00 Brk

D 2'

9.97

9.90

C 0.07

10.76

10.10

C 0.66

N

-0.26

4+60

D 2'

10.50

10.26

C 0.24

11.34

10.46

C 0.88

N

-0.25

4+20

D 2'

0.63

10.42

C 0.01

1.60

10.82

C 0.78

X

2'

Storm Drain
Linda Rosa + Forward

7-28-53

C.H.S.
Begg
Oltman

W.O. 21103

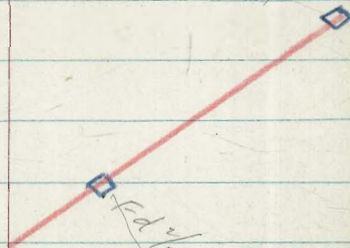
INDEXED
JAN 12 1954

Prop. pipe Ties.

69

Fd. 2" pipe

Fd. $\frac{1}{2}$ "
Sta 2+10.94



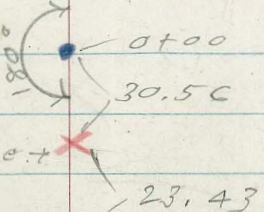
Fd. $\frac{1}{2}$ " Sta 1+15.75

Δ 58°29'18"
R = 45
+25.19
L 45.98

Fd. disk FB2210
1" pipe

cut cross in Pavet

cut cross on ab.



Storm Drain
Forward + Linda Rosa

70

1+00.43
19°29'-46" Ob
80.26
175.60
C 4.66

0+85.12
92°22'-53" Ob
Chord - 15122
78.85
174.15
C 4.70

B.C.
0+69.81
4.35
172.70
C. 165

0+41.81
4.31
170.04
C 4.27

0+13.81
71.36
167.38
C 3.98

0+05.81
9.09
166.86
C 2.23

Head wall
0-02.19
7.27
166.57
C 0.70

End

Head wall
2+20.94
6.25
183.96
C 2.29

1+92.3
4.53
182.27
C 2.31

1+63.65
4.18
180.47
C 3.71

1+35
81.03
178.72
C. 2.31

1+25
80.47
177.94
C-2.53

1+15.75 E.C.
29°-14'-39" Ob
79.78
177.06
C 2.72

Alley BIK 45 O.B.

Water line in N. Ely - S. wly. Alley 7/31/53

0+00 = Nly. line Pescadero

stakes 4' East of E Pipe (or

9' East of E Alley) sheet #10147-L

1+05 7.83
24.11
C-3.72

1+40 7.69
24.40
C 3.29

0+90 Lk 8.71
28.36
C-3.35

0+70 9.52
25.93
C-3.59

0+50 30.19 * on drive
26.91 a' off
C-3.28

0+30 31.37
28.30
C-3.07

0+00 4.01
30.97
C-3.04

INDEXED
JER
JAN 12 1954

71

sly. orchard

3+00 7.25
34.17
C 3.08

2+80 5.37
31.39
C 3.98

2+50 30.64
27.47
C 3.17

2+35 8.96
26.06
C 2.90

2+20 8.37
25.06
C 3.31

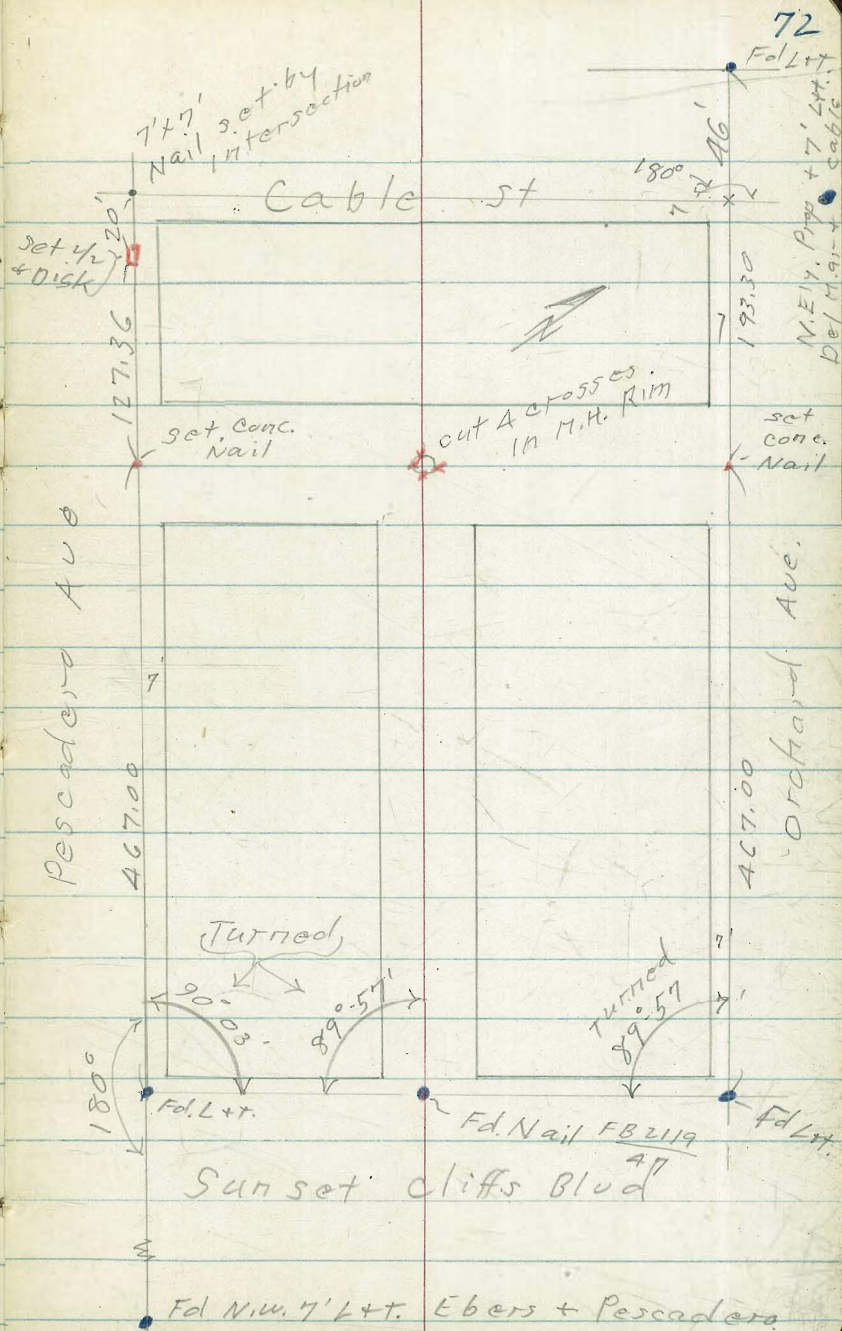
2+05 8.19
24.50
C 3.69

Ties to alley
Blk 45-0.13.

INDEXED
JAN 19 1954

Alley set on map distance
as per sketch.

This meets existing curbs
and private improvements
better than apportionment
of $\left\{ \begin{array}{l} 0.36 \\ 0.30 \end{array} \right\}$ (see sketch)
coverage in block
would meet the improvements



				South	North	73	
NWly + S. Ely Alley, BIK 450 B.				Cross Alley			
0+00 wly line Sunset Cliff Blvd.				Ely line 4+50	7.81	7.91	- 0.10 Ely
				2 Both ways	27.60	27.40	X 20 North
Sheet 10147-L					Co. 21	C2.51	
				A+30	7.65	7.77	X 28 in
				2	28.05	27.75	
					FO 40	C2.02	
					28.41	30.02	
				Tip	28.57	28.25	X - 0.17 in
1+60	0.17	1.59	31.47	0.29	4+00	0.132	
		Co. 12	Co. 21				
1+40	0.176	1.43	31.10	0.24	3+60	0.134	
		Co. 33	X				X + 0.09 in
1+20	0.178	0.68	30.57	0.22	3+20	0.144	
		Co. 11	Co. 11				0.256
1+00	0.182	30.12 ^{TR}	30.09	0.19	2+80	0.153	
		Co. 03	Co. 18				0.250
0+80	0.185	9.84	29.52	X 1.66	2+40	0.152	
		Co. 32	Co. 62		E.V.C.		0.248
0+60	0.188	9.14	29.22	0.12	2+20	0.160	
		8.94	29.22				0.240
		FO. 08	FO. 28				
0+40	P.V.C. -1.92	9.10	28.83	0.08	2+00	0.167	
		Co. 27	Co. 12				0.233
0+00		28.60	28.60		1+80	0.168	
wly. line							0.232
Sunset Cliff							
Blvd							

N.Ely.-S.Wly. Alley BIK 45- O.B.
 0+00 = Nly line Pescadero Ave.

Sheet 10147-L

B.M. Pole # PA.4872
 Nail Elev. = 28.80

74

1+75	x-4'	7.66 27.31 C0.35	8.58 27.31 C1.27	x-21					
1+60	x-2'	7.87 27.36 C0.51	9.91 27.40 C2.51	x-0.121 2' back	orchard sly line 3+00	37.29	37.37	# 1'	
1+40	x-2'	8.05 27.64 C0.41	7.81 27.60 C0.21	# 21 Both ways	2+80	a-2'	5.88 34.59 C1.27	6.09 34.59 C1.45	x-0.18
0+90	E.V.C. x-2'	8.99 28.56 C0.42	8.87 28.56 C0.31	D-2'	2+65	D-2'	3.35 32.53 C0.82	3.74 32.53 C1.21	x-0.18
0+70	x-2'	0.102 29.13 C0.87	9.50 29.13 C0.37	D-2'	2+50	D-2'	0.58 30.67 F0.09	1.43 30.67 C0.76	x-0.120
						T.P. 30.67			
0+50	x-2'	0.40 30.11 C0.29	0.26 30.11 C0.15	x-2'	2+35	x-2'	9.05 29.26 F0.21	8.85 29.26 F0.41	D 2'
0+30	x-3'	0.77 31.50 F0.73	1.76 31.50 C0.26	x-0.48	2+20	x-2'	8.14 28.26 F0.12	9.17 28.26 C0.91	x-0.30
0+10	P.V.C. x-0.55	4.98 33.30 C1.68	3.75 33.30 C0.45	x-0.59	2+05	x-2'	7.94 27.70 C0.24	8.26 27.70 C0.56	D-1'
0+00		4.24 34.28	34.17		1+90	x-2'	7.95 27.43 C0.52	7.85 27.43 C0.42	x-0.50

Storm Drain

Blk. 45 Ocean Beach
Sheet 10147-L

75

1122
1194
1466

1+23.47

1+19.86

1+16 Brk

0+88

Exist pipe
0+60 = End

Exist. pipe
0+12 = Meet

Catch Basin
0+03 = 4 PRY.

0+00 = E Alley

1+46.85 End of pipe

1+42.91

1+39.16

1+35.70

1+32.65

1+29.93

1+26.87

27.66
~~33.45~~
33.11
18.66
18.45
8.86
9.59
C 9.6

Sewer BIK I - Plumosa Manor

C.H.S.
Beqq
Oltmann
Schelin

INDEXED
ER
JAN 12 1954

8-14-53
W.O.# 21079

B.M. = $\frac{1}{2}$ - 0+00 $\frac{FB204}{35}$ EL = 135.16

136.05 = d. end on Rt.

0.40%

2+00
36.26
124.50
C 11.76

1+50
37.77
124.30
C 13.47

1+00
41.81
124.10
C 17.71

$\Delta 71^{\circ}44'$ Rt
M.H.#3
0+78
42.52
124.01
C 18.51

0+39
37.63
123.86
C 13.77

M.H.#4
0+00
31.94
123.70
C 8.24

on Nly. 15' line Elliot
3' Tie back from alley 136.27

End of line 34.98
125.86 on M.H. west rim
M.H.#1 C 9.12
5+41

5+00
35.03
125.70
C 9.33

4+50
33.68
125.50
C 8.18

4+00
34.33
125.30
C 9.03

3+50
35.02
125.10
C 9.92

M.H.#2
3+21 P.O.T.
35.90
124.98
C 10.92

3+00
35.93
124.90
C 11.03

2+50
35.38
124.70
C 10.68

Pacific Beach Storm Drain
Gresham to Riviera Dr. 9-11-53

C.H.S.
Beeg
Altman
Scholin

INDEXED
SER
JAN 12 1954

w.o.
21041

B.M. 2 S. Ely 7' Lt. P.B. Dr. + Riviera Pl.
Crosses 12' Lt. of ϕ

2.400
1.450
1.400
0.450
0.400 start pipe
0.402 = ϕ Type F, C.O.
0.402 = ϕ Nly + Sly 36" drain - on Gresham

26.23
19.11
C 7.12
25.07
17.62
C 7.45
3.94
16.14
C 7.80
22.75
14.65
C 8.10
21.18
13.17
C 8.01

3 + 17¹⁴ Type G Ctr. C.O.
3 + 14.14 End of pipe
2 + 91.40^{#5} F.C.
2 + 75.52^{#4}
2 + 59.64^{#3}
2 + 43.76^{#2}
2 + 27.88^{#1}
2 + 12 = B.C.

28.51
8.51
22.50
C 6.01
7.58
21.83
C 5.75
7.01
21.35
C 5.66
6.85
20.88
C 5.97
6.68
20.41
C 6.27
26.90
19.94
C 6.96
6.53
19.47
C 7.06

Reed Ave.

9-18-53

Check grades Nly side Reed
From Cass to Dawes.

#10346-L

INDEXED
HER

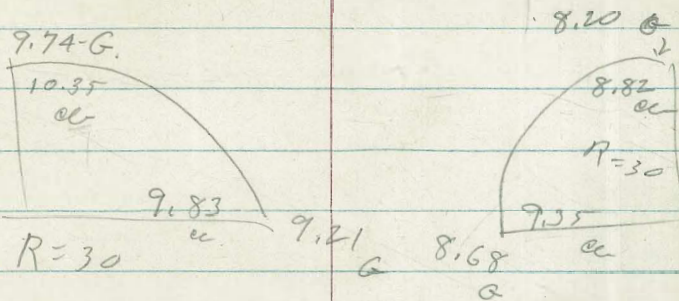
DEC 15 1953
Wly. Dawes

EXIST ch. A+90	Mark at Stakes	Nly. ch Grade	Elev Stake	Cut or Fill
5	CO.10	10.47	9.83	CO.05
4+50	CO.02	10.35	10.18	CO.19
4	FO.84	10.20	9.21	FO.99
3+50	FO.31	10.05	9.55	FO.50
3	CO.17	9.90	9.95	CO.05
1+50	CO.91	9.75	10.50	CO.75
2	CO.63	9.60	11.11	CO.51
1+40	CO.51	9.42	10.05	CO.63
1	FO.07	9.30	9.30	Grd
0+40	CO.41	9.12	9.45	CO.33
Ely Cass 0+00		9.00	9.00	

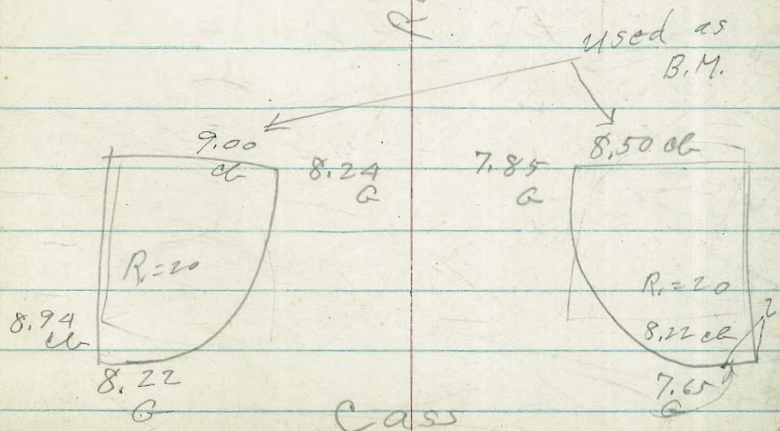
Ely. line Cass must be met
for drainage, therefore used
curbs as B.M.

78

Dawes



Reed



Cass

Cl. stakes Reed
Cass to Dawes

INDEXED
JER
17-01-53-53

W.O. 32237

Used N.E. cl. Ret. Cass + Reed as

B.M. - E.L. = 9.00 sheet 10346-L

This is 0.14 low in relation to

B.M. shown on plan but grade
is slight (0.16%) + existing cl.
+ gutter has to be met.

(See - P. 78)

1+00 Rate C0.30

0+50 C0.09

0+06 = E.C. 8.31
9.00
F0.69

0+00 9.00
Meet cl.

5+00 Meet cl.

B.C. 9.97

4+90 9.83

C0.14 - This Fits Pave.

A+50 C0.25

A+00 F0.30

3+50 F0.02

3+00 C0.05

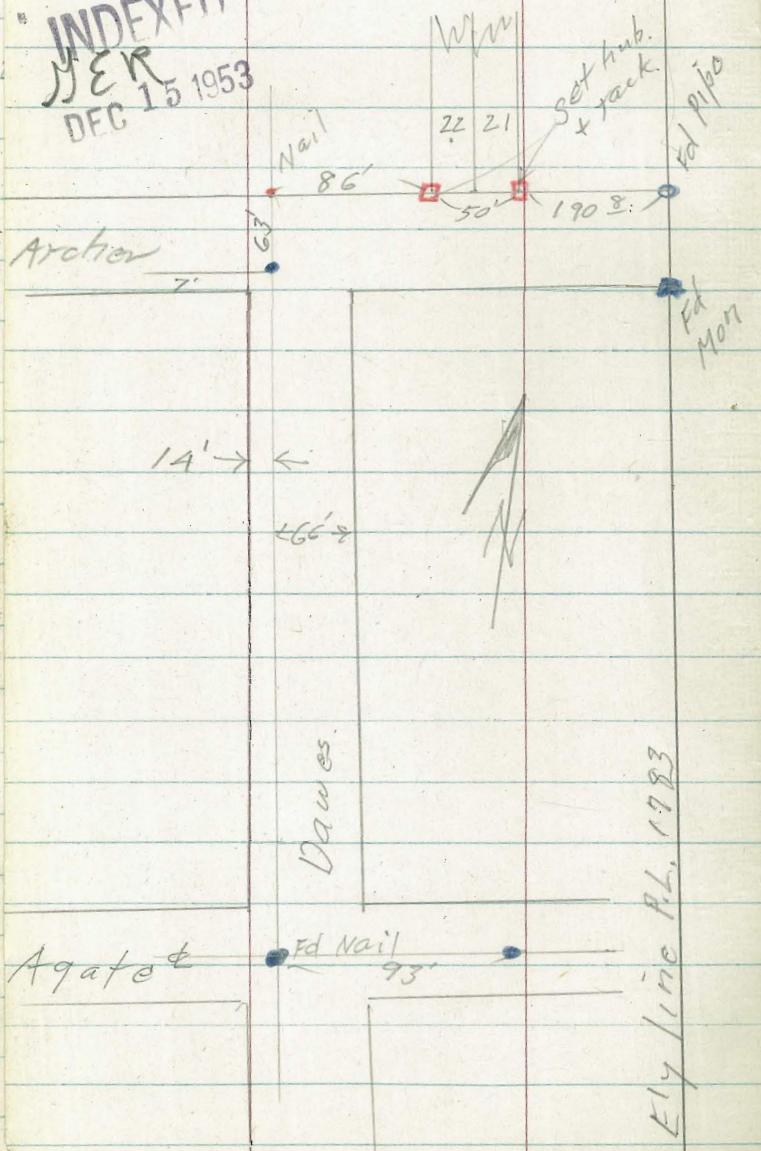
2+50 Rate C0.02

2+00 C0.24

1+50 C0.47

Restake sly line
 Lots 21-22 BIK. 10 Monte Villa
 Tract.

INDEXED
 MER
 DEC 15 1953



257

16.

0	.35
1	.85
2	.35
3	.85
4	.35
5	.85
6	.35
7	.85
8	.35
9	.85
10	.35
11	.85
12	.35
13	.85
14	.35
15	.85
16	.35
17	.85
18	.35
19	.85
20	.35
21	.85
22	.35
23	.85
24	.35
25	.85
26	.35
27	.85
28	.35
29	.85
30	.35
31	.85
32	.35
33	.85
34	.35
35	.85
36	.35
37	.85
38	.35
39	.85
40	.35
41	.85
42	.35
43	.85
44	.35
45	.85
46	.35
47	.85
48	.35
49	.85
50	.35

16A108 35 10.40 PL. 17998
 70
 50
 28
 78
 22

22
 25.47
 13
 21.60

82.4
 76.2
 159.6
 340.8
 150
 190.8
 30.9
 190.8

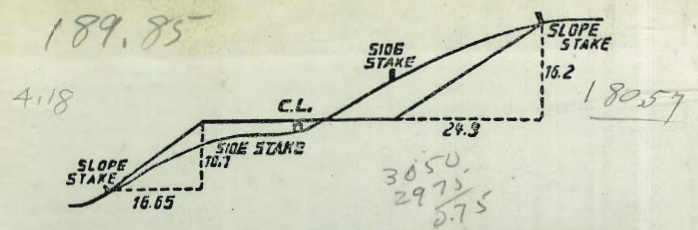
0100
 45.65
 81.71
 0

23.15
 9.14
 32.29

14633 Chics - Souths 46
 28.14
 27.65
 49
 9.43
 150
 1956
 160
 21.17

69.2
 25.8
 93.0
 12.5
 107.5

21.15
 162
 1856
 130
 706
 72.70
 3 436
 145



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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