

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1, ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 15 1965

6-9

0.22  
7.65  
57

9377  
5245  
792  
396

7.67

524  
431  
93



DIRECTIONS FOR USE OF TABLE

TABLE NO. XIV

Distance of slope taken from side of shoulder  
states for any width roadway, slope 1 1/2 to 1

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IMPROVED TABLES  
AND  
INFORMATION

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cut table. If it does not make the right cut  
between curves.

TABLE NO. VIII

To find tangents and distances for curve of  
any other degree divide by degree of curve and  
add distance found in column of correspond-  
ing degree of curve with a distance may be found  
by dividing tangent for constant opposite 1 by  
given tangent (constant).

The distance from a point on the tangent to  
the curve is very nearly the extent of the tangent  
length divided by twice the radius.



490  
54  
436

TABLE IX  
MIDDLE ORDINATES OF RAILS  
Length of Rail (feet)

C o'	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE X  
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5 58	2-59	7.2
250	25	5 44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

13700

TABLE XI  
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL.

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XII  
MINUTES IN DECIMALS OF A DEGREE.

0'30"	.00833	10'30"	.17500	20'30"	.34167	30'30"	.50833	40'30"	.67500	50'30"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



Stown Pt. Sewer Replacement	Pump house to Pendleton	2-7
Bay Park Village Storm drain	(Morena - Milton Frankfort etc.)	8-18
Fairmount Sewer - Montezuma Slg.	to Burnham place.	38-41 19-26
" " Extension	To Hilldale Road	27-32
" " " west thru	Talmadge Park to Hart St. <sup>house</sup> pump	33-36
Aldino Drive Sewer Fairmount slg. to	Monroe	42-
ARCHER St. Sewer		46
Dawes St sewer		47
Cass St sewer		48
Van Nuys St sewer		49
Van Nuys Water line		49
Archer - Van Nuys - Agate	- Dawes Rough Grade Curbs	50-62 <sup>+68</sup>
" " " "	Water Services	63-67
Archer } Curb inlets +	culverts	67
Van Nuys }		
La Palma ch. stakes		75 <del>72</del>
La Jolla Mesa Dr. + } storm drain		76
Linde Rosa }		
check Sewer Alley BIK 24A Mission	Beach	78



Crown Point Sewer.

Replacement - Pumping plant to  
Pendelton St.

Sammermeyer Beqq altman.	1815-D 1816D	N.O. 20857 3-1A-52
2+90 M.H.#2	-1.43 -5.61 C-4.18	-1.28 -5.57 C-4.29
+75		
2+50	-1.30 -5.52 C-4.22	-1.38 -5.46 C-4.08
+25		
2+00	-1.24 -5.41 C-4.17	-1.46 -5.35 C-4.19
+75		
1+50	-1.21 -5.39 C-4.09	-1.06 -5.24 C-4.18
+25		
1+00	-0.92 -5.19 C-4.27	-1.02 -5.13 C-4.11
+75		
0+50	-0.90 -5.08 C-4.18	-0.86 -5.02 C-4.16
+25		
0+00 = M.H.#1	-0.63 -4.97 C-4.34	
7' west of Pendelton 7' S. of Alley B/K?		
Not shown on plan		

Rim existing M.H. = EL. to 0.73

EL. Rim Existing M.H. 5+75  
B.M. - 0.56

2

INDEXED

Law

MAR 25 1953 +75

6+50

0.12%

+25

6+00

-3.19	
-6.37	
-3.25	C-3.18
-6.34	
C-3.09	-2.83
	-6.31
-2.15	C-3.48
-6.28	
C-4.13	

Olney St.  
5+80 = M.H.#3

-2.05	
-6.25	
C-4.20	

5+50

+25

5+00

+75

4+50

+25

4+00

0.22%

+75

3+50

+25

3+00

-1.51	
-6.18	
C-4.67	-2.67
	-6.12
-2.63	C-3.45
-6.07	
C-3.44	-2.25
	-6.01
-1.95	C-3.70
-5.90	
C-4.01	1.87
	-5.90
-1.09	C-4.03
-5.85	
C-4.16	-1.55
	-5.79
-1.58	C-4.24
-5.74	
C-4.16	-1.59 T.P.
	-5.68
<del>-5.63</del>	C-4.09



M.H. 7' N. of 8+65<sup>2</sup> EL. = -0.185

	+75		-1.28 -6.85
10+50		-1.26 -6.82	C-5.57
	+25		-1.33 -6.79
10+00		-1.34 -6.76	C-5.46
	+75		-1.45 -6.73
9+50		-0.97 -6.70	C-5.28
	+25		-0.74 -6.67
9+00		0.83 -6.64	5.93
8+75			C-5.81
8+70 - M.H. # A		-0.45 -6.61	
	+7		C-6.16
8+50		+0.13 -6.58	+0.08 -6.58
	+25		C-6.71 -0.01 -6.55
8+00		-0.84 -6.52	C-6.54
	+75		-2.22 -6.49
7+50		-2.83 -6.46	C-4.27
	+25		-2.72 -6.43
7+00		-3.51 -6.40	C-3.71
			C-2.89

Ely rim exist M.H  
7' Lt. 11+45<sup>2</sup> = EL. = -0.68  
+ 7' ahead

3

14+00		-1.42 -7.24	
	+75		C-5.82 -1.82 -7.21
13+50		-1.52 -7.18	C-5.39
	+25		-1.32 -7.15
13+00		-1.34 -7.12	C-5.83
	+75		-1.76 -7.09
12+50		-2.90 -7.06	C-5.33
	+25		-2.35 -7.03
12+00		-2.35 -7.00	C-4.68
	+75		-2.64 -6.97
11+55.49		-2.28 -6.94	C-4.53
			C-4.66
Δ 74° 13' - 40" Lt. 11+45.49 M.H. # 5			-6.93
11+40.49		-1.84 -6.92	
	+25		-0.12 -6.90
11+00		-1.99 -6.88	C-6.78
			C-4.87



			-2.86
			-7.75
			C 4.87
	+25		
			-2.63
18+00			-7.72
			C-5.09
	+75		
			-2.49
17+50			-7.66
			C 5.17
	+25		
			-2.50
			-7.63
17+00			C 5.13
			-2.48
			-7.60
			C-5.12
	+75		
			-2.12
			-7.57
16+50			C 5.45
			-1.96
			-7.54
			C-5.58
	+25		
			-1.92
			-7.51
16+00			C-5.59
			-2.24
			-7.48
			C-5.24
	+75		
			-2.03
			-7.45
15+50			C-5.42
			-1.99
			-7.42
			C-5.43
			-1.97
15+30 = M.H.# 6			-7.39
			C-5.42
			-2.00
15+00			-7.36
			C 5.36
	+75		
			-1.73
			-7.33
14+50			C-5.60
			-1.40
			-7.30
			C-5.90
	+25		
			-1.43
			-7.27
14			C-5.84

			-0.09
			-8.20
			C 8.11
22+10			
			-0.14
			-8.19
			C-8.05
	+75		
			-0.39
			-8.17
			C-7.78
21+50			-0.42
			-8.14
			C-7.72
	+25		
			-0.73
			-8.11
21+00			C 7.38
			-0.76
			-8.08
			C 7.32
	+75		
			-0.78
			-8.05
20+50			C-7.27
			-0.69
			-8.02
			C 7.33
	+25		
			-0.65
			-7.99
20+00			C 7.34
			-0.85
			-7.96
			C-7.11
	+75		
			-1.40
			-7.93
19+50			C 6.53
			-1.37
			-7.90
			C-6.53
	+25		
			-1.91
			-7.87
19+00			C 5.96
			-2.22
			-7.84
			C-5.62
	+75		
			-2.35
			-7.81
18+50			C 5.56
			-2.06
			-7.78
			C-5.72
			-2.47
18+41 M.H.# 7			-7.76
			C-5.29
			B.M. on M.H. C'4
			EL = -0.26



25+25	-0.68 -8.59 C-771		+25	0.18 -9.06 C 9.24
25+00	-0.21 -8.56 C 8.35		29+00	0.58 -9.03 C-9.61
24+83.80 <sup>0.12%</sup>	-8.53		+75	-0.06 -9.00 C 8.94
24+78.80	South +0.83	North +0.60	28+50	-0.01 -8.97 C-8.96
24+66.52 137'-23'-15" Lt.	-8.52 C 9.35	-8.52 C-9.12	28+00 <sup>0.12%</sup>	+25 -0.35 -8.91 C 8.88
24+45	-0.67 -8.49 C 7.82	-0.97 -8.47 C 7.50	+75	-8.56 -0.28 -8.88 C 8.60
+25	-1.20 -8.44 C-7.24	-0.84 -8.41 C-7.57	27+50	-0.03 -8.85 C 8.82
24+00 <sup>0.13%</sup>	+75		27+45.87 M.H.# 11	-0.02 -8.84 C 8.82
23+50	-8.38		+25	-0.34 -8.80 C-8.48
+25	-1.52 -8.37 C-6.85		27+00	-0.34 -8.80 C-8.56
23+47.90 M.H.# 9		-1.64 -1.59 -8.34 -8.34 C-6.78 6.75	+75	-0.95 -8.74 C-7.97
+25	-1.91 -8.31 C 6.90	+2.38 -8.28 C 10.58	26+50	-0.95 -8.74 C-7.89
23+00	-2.34 -8.21 C-5.75		+25 <sup>0.12%</sup>	-0.80 -8.68 C-7.88
+75	+1.12 -8.25 C 9.37		26+00	-0.80 -8.68 C-7.88
22+50 <sup>0.12%</sup>		+0.80 -8.22 C-7.02	+75	-1.08 -8.62 C-7.54
+25			25+50	



+75		-0.24 -9.48 C-9.24	
32+50		-0.42 -9.45 C 9.03	
+25		-0.43 -9.42 C 8.99	
32+00		-0.31 -9.39 C 9.08	
+75	$\frac{1}{2}$	-0.71 -9.36 C 8.65	
31+50	$\frac{1}{2}$	-0.24 -9.33 C-9.09	
+25		+0.16 -9.30 C 9.46	
31+08.89		-9.28	
		South North	
31+03.89 M.H.#12	$\Delta 12^\circ - 40' H.$	+1.29 +1.46 -9.27 -9.27 C-10.56 C 10.73	
31 Ely. rim existing M.H.	El =	-0.30	
+75		0.13 -9.24 C 9.37	
30+50	$\frac{1}{2}$	0.24 -9.21 C 9.45	
+25	$\frac{1}{2}$	-0.09 -9.18 C 9.10	
30+00		-0.36 -9.15 C 8.79	
+75		-0.49 -9.12 C-8.63	
29+50		-0.33 -9.09 C-8.76	

35+00		-2.02 -9.95 C-7.73	-1.95 -9.72 C-7.77
+75		-1.76 -9.69 C-7.93	
34+50		-1.70 -9.68 C 7.98	El. wly Rim Exist M.H. -+0.25
34+42 <sup>03</sup>	$-90^\circ$ to Fwd targ.	-1.60 -9.67 C 8.07	
34+42.63	M.H.# 1A - $\Delta 62^\circ - 40' - 15'' N.$	+0.20 -9.62 C 9.82	+0.25 -9.59 C 9.84
34+35	$-90^\circ$ to back	+0.30 -9.56 C-9.92	-9.51 C 10.18
34+10		-9.51	
+75			
33+50	$\frac{1}{2}$		
+25	$\frac{1}{2}$		
33+10			
$\Delta 24^\circ - 16' L.$		+2.23 -9.51 C 11.74	
33+06 <sup>47</sup>	M.H.#13	+0.77 -9.50 C 10.27	
33+00			



B.M. on Mon. N.W. 1/4  
Crown Pt drive  
Q. Sequoia = 20.77

+75		-1.91	
		-10.19	
38+50		C-8.28	
		-1.91	
		-10.16	
+25		C-8.25	
		-2.04	
		-10.13	
38+00	0.1290	C-8.07	
		-1.88	
		-10.10	
+75		C-8.22	
		-1.73	
		-10.07	
37+49.82		C-8.14	
		-1.23	
		-10.03	
		C-8.80	

$\Delta 26^{\circ} 41' - 30''$  Lt.  
37+44.82 M.H. #15 B.M. on west rim  
El. +0.15 -10.03

37+39.82		-1.22	
		-10.02	
+27		C-8.80	
		-1.60	
		-10.01	
37+00		C-8.41	
		-1.89	
		-9.99	
+75		C-8.10	
		-2.54	
		-9.96	
36+50		C-7.42	
		-2.56	
		-9.93	
+25	0.1290	C-7.37	
		-2.67	
		-9.90	
36+00		C-7.23	
		-2.40	
		-9.87	
+75		C-7.47	
		-2.22	
		-9.74	
35+50		C-7.52	
		-2.21	
		-9.81	
		C-7.60	
+25		-1.80	
		-9.78	
		C-7.98	

Pump House  
40+34.89

40+18.89 M.H. #16

40+00

39+75

39+50

39+25

39+00

-0.03  
-17.00 - arrow on  
C 16.97 Pump House  
3' W. N.E. Cor.

-0.03  
-10.36 - 3' arrow on  
C 10.33 pump house  
10.33

-4.62  
-10.34  
C 14.96  
1.28  
+75 -10.30

-0.27  
-10.28  
C 11.58  
10' W. N.E. Cor.  
10.01  
-1.24  
+25 -10.25  
C 9.01

-1.86  
-10.22  
C-8.36 10' Lt.



Bay Park Village Storm Drain

INDEXED

8

*and*  
MAR 25 1953

5-27-52

(Milton Street)

N.O.  
20897

C.H.S.

Boggs

Oltman

Johns

sheets

9355-6-7-8+9 E

1+54.52<sup>#2</sup>

~~7.77~~ 7.75  
~~-2.07~~ -2.07  
C. 9.84 C. 9.82

B.M. = stall plug Fly end box

1+46.24<sup>#1</sup>

~~2.05~~ 6.39  
~~-2.12~~ -2.12  
C. 4.20 C. 8.51

culvert sta. 0+00 EL. = 2.70 (sheet 9355-L)

1+37.96 B.C.

3.99 ✓  
~~-2.17~~  
C. 6.16

1+35.96

-2.18

1+25

5.27 ✓  
~~-2.25~~  
C. 7.52

1+07.7 P.O.T.

7.79  
~~-2.36~~  
C. 10.15

0+75

7.50  
~~-2.57~~  
C. 10.07

0+50

1.71  
~~-2.73~~  
C. 4.44

0+18

3.82  
~~-2.94~~  
C. 6.26



Temp. B.M. - R.R. spike in pole # 415024H  
Lister - Merona EL. 210.27

9

4+50  
9.30  
-0.16  
C-9.46

3+98.31 C.D.#1  
8.92  
-0.49  
C-9.41

3+50  
8.03  
-0.80  
C-8.83

3+00  
7.90  
-1.12  
C-9.02

2+50  
0.6457  
T.P. 8.08  
-1.44  
C-9.52

2+00  
7.62  
-1.76  
C-9.38

1+71.09 = E.C.  
7.43  
-1.96  
C-9.39

1+62.80 #3  
~~7.61~~ 7.60  
~~-2.01~~ -2.01  
C-9.66 C-9.61

#2  
11.15  
2.04  
C-9.11

#1  
11.34  
1.98  
C-9.36

7+72.37 B.C.  
10.95  
1.93  
C-9.02

7+50  
12.24  
1.77  
C-10.47

7+00  
11.41  
1.45  
C-9.96

6+50  
11.51  
1.13  
C-10.38

6+00  
0.6457  
11.03  
0.81  
C-10.22

5+50  
10.08  
0.48  
C-9.60

5+00  
9.48  
+0.16  
C-9.32



13+00

9+50

2.657

16.04  
4.90  
C-11.14

9+00

14.50  
3.57  
C-10.93

8+75

13.79  
2.91  
C-10.88

8+50

10.80  
2.45  
C-8.35

8+25

10.93  
2.19  
C-8.74

start 45" pipe

8+09.37

8+07.37 C.O.#2

10.24  
2.15  
C-8.09

End 63" pipe

8+05.37 E.C.

10.35  
2.14  
C-8.21

#3

10.85  
2.09  
C-8.76

14+00

T.P. 29.31  
16.82  
C-12.49

13+50

27.09  
15.50  
C-11.58

13+00

26.36  
14.17  
C-12.19

12+50

24.76  
12.95  
C-11.81

12+00

23.11  
11.52  
C-11.59  
T.P. Nail in pole  
#3999 El.=27.38

11+50

21.34  
10.20  
C-11.14

11+05

20.50  
8.87  
C-11.63

10+50

19.10  
7.67  
C-11.43

10+00

17.34  
6.27  
C-11.12



T.P. 37.14  
A3.32

18+00	3.5%	41.81 28.26 C 13.05
17+50		40.00 26.51 C- 13.49
17+25	E.V.C.	39.50 25.64 C- 13.86
17+00		37.97 24.84 C 13.13
16+75	P.V.C.	38.12 24.11 C 14.01
16+50		37.17 23.44 C 13.73
16+00		35.61 22.12 C- 13.49
15+50	2.65%	34.44 20.79 C 13.65
15+00		33.24 19.47 C- 13.77
14+50		31.04 18.14 C- 12.90

T.P. 51.15 West end S.W. Rot  
Top of Bl. Frankfurt & Milton 11

22+00		50.70 42.06 C 8.64
	5.1%	2.01 51.44 Top of Bl. C 0.57
		curb. Cr. 21+63.27 a- 10' North.
		C 2 #3 21+49.52 C- 12.83
		curb. Cr. 15' Type B-2. 21+47.27 a- 10' North
21+00		52.01 38.76 C- 13.25
20+50		48.37 37.01 C- 11.36
20+00		46.45 35.26 C- 11.19
19+50		45.32 33.51 C 11.81
19+00		43.90 31.76 C 12.14
18+50		42.51 30.01 C 12.50



24+01.42 #3 = E.C.  
58.60  
48.30  
C 10.30

23+92.67 #2  
58.60  
48.03  
C 10.57

23+83.91 #1  
58.80  
47.76  
C-11.04

23+75.15 = B.C.  
58.84  
47.49  
C-11.35

23+65.73 = E.C.  
59.20  
47.20  
C 12.00

23+58.23 = B.C.  
58.29  
46.97  
C-11.32

23+50  
57.87  
46.71  
C-11.16

23+00  
55.85  
45.16  
C 10.69

22+50  
3.11%  
T.P. 55.35  
43.61  
C-11.74

S.W.B.P.  
Frankfort  
+ M. 1/4" = 52.40

12

0+40 - Frankfort line (Page 17) =

cl. inlet # A, (15' - type 13-2)  
0+53.75  
East end  
2.25 west of 0+40,  
west end

135  
51.15 - top. cl.  
C 0.20  
131  
50.70 top. cl.  
C 0.61

E.C. = end of pipe  
24+47.93 = #3  
56.90  
49.75  
C-7.15

24+40.13 #2  
55.93  
49.51  
C-6.42

24+32.93 #1  
3.11%  
53.81  
49.28  
C-4.53

24+25.42 = B.C.  
53.60  
49.05  
C 4.55



Milton St. Drain  
Cont.

0+00 = 83<sup>5</sup> west of wly line

Alley BIK 87 - Map 909 (Sheet 9356-L)  
24" pipe

Stakes set 10' N. of 4

1+75

73.17  
62.82  
C 10.35

1+50

9 1/2%

70.45  
60.57  
C 9.88

1+00

65.77  
56.07  
C 9.70

0+62<sup>5</sup>

62.90  
52.70  
C 10.20

0+37<sup>5</sup>

61.56  
50.70  
C 10.86

0+12<sup>5</sup>

60.03  
48.95  
C 11.08

0+00

59.42  
48.20  
C 11.22

66.50 T.P.

84.80 T.P.

73.23 T.P.

101.83 T.P.

110.84 T.P.

C.O. 44

5+27.81

5+00

A+50

A+00

3+50

3+00

2+50

2+25

2+00

1/2 195 Lt. of 5+82.81 13  
E.L. = 129.76 FB 2180-19

23.52

112.55

C 10.97

120.56

108.46

C 12.10

112.71

101.11

C 11.70

104.62

93.76

C 10.86

76.35

86.41

C 9.94

88.08

79.06

C 9.02

80.25

71.71

C 8.54

77.48

68.39

C 9.09

T.P. 75.48

65.43

C 10.05

14.7%



Milton St

IP 48.95

9-16-52

Nail in pole # 4599 S.W. Illion + Milton 14

El. 157.62

8+00  
9 70

55.36  
135.30  
C 20.06

9+00

156.25  
136.21  
C-20.04

7+50

53.22  
134.85  
C 18.37

8+94<sup>50</sup> C.D.#5

156.64  
136.46  
C-20.48  
156.A9  
156.40  
Grade

7+25

51.15  
134.63  
C-16.52

8+93<sup>00</sup> #4  
E.C.

156.28  
136.15  
C-20.13

7+00

48.18  
133.71  
C-14.77

#4

6+75

43.89  
132.11  
C-11.78

8+75.31 #3

155.69  
135.78  
C 19.71

6+50

39.46  
129.81  
C-9.65

7.P.

8+57.63 #2 15' off

155.93  
135.82  
C 20.11

6+25

34.94  
126.83  
C-8.11

8+37.95 #1 10' off

155.71  
135.66  
C-20.05

6+00

130.95  
123.16  
C-7.79

8+22.27  
A-parts  
B.C. RX

55.65  
135.50  
C 20.15

5+50

25.32  
115.81  
C 9.51

14.78

5782.81 = Hub. 1



Milton St  
X Illion St.

9-16-52

11+40.17 C.I.#6  
14447  
138.37  
C-6.10

11+05.51 A  
E.C.  
14350  
138.07  
C-7.43

10+87.65 #3  
14291  
137.90  
C-5.01

10+69.78 #2  
↑  
Ch=2160  
141.72  
137.74  
C 3.98

10+51.91 #1  
↓ TP 143.49  
142.64  
137.58  
C 5.06

4 parts  
L1.  
10+34.04=B.C.  
147.28  
137.42  
C-9.86

10+00  
TP. 151.87  
148.82  
137.11  
C 11.71

9+50  
155.10  
136.66  
C-18.44

Illion + Milton

15

0+00 = 8+93- Milton St. Drain P.14  
18" pipe

C.I.#5  
0+81.18

156.86  
151.02  
C-5.84

0+50

156.54  
150.41  
C-6.13

0+31.42 #4  
E.C.

156.19  
150.02  
C-6.17

0+23.56 #3

~~149.87~~

0+15.71 #2

156.00  
149.72  
C 6.28

0+07.85 #1

~~149.56~~

4 parts

0+00 = B.C. RT

155.54  
149.40  
C 6.14

INDEXED  
flaw  
MAR 25 1953



Lister St Drain 7-7-52  
 Moreno to Chicago  
 L-9355

1955 T.P.

16

INDEXED

2 MAR 25 1953

stakes 18 L. dt

13.39  
 7.45  
 C-5.94

12.02 T.P.  
 6.15  
 C-5.87

1+50  
 11.03  
 4.85  
 C-6.18

1+00  
 10.03  
 3.55  
 C-6.48

0+87.5 Brk  
 7.84  
 3.23  
 C-6.61

0+62.5 Brk.  
 9.37  
 2.78  
 C-6.59

0+31.25  
 9.60  
 2.48  
 C-7.12

0+10  
 8.71  
 2.28  
 C-6.43

0+00 C.I.#1  
 2.18

west end  
 17.55  
 16.30 top of  
 C.I.#1  
 sly. side  
 Lister  
 C 11.25

East end  
 8.04  
 16.90 top of  
 C-1.14

16.51  
 16.05  
 Nly. side  
 Lister  
 C 0.46

17.49  
 16.62  
 C 0.87

B.M. on 103' R.P. Cross to sta. 3+21.77 El. = 22.58

3+57.77 C.I.#2

16.87  
 11.65  
 C-5.22

stakes 8' RL

FROM west  
 15.14  
 9.32  
 3+21.77 C.I.#1  
 C-6.82

17.62 to  
 11.00 North  
 C-6.62

16.14  
 15.14  
 7.30  
 3+20.02 F.C.  
 C-6.84

15.35  
 8.83  
 C-6.52  
 3+02.35

14.69  
 8.35  
 C-6.34  
 2+84.68 B.C.



FRANKFORT  
Drain

7-7-52

INDEXED  
MAR 25 1953

17

				6+00	55.75 47.24 C-8.51
2+00	(17.50 RT. on curb)	53.09 43.50 C-9.58		5+50	55.55 T.P. 46.84 C-8.71
1+50		52.66 43.00 C-9.66		5+00	55.09 46.44 C-8.65
1+15.94 #3 E.C.	10' RT. ↓	52.81 42.65 C-9.66	52.47 42.65 C-9.82 7.5 RT	4+72.50 = C.O. #6	55.04 46.22 C-8.82
0+92.37 #2	10' ↓	52.14 42.40 C-9.74		4+50	54.76 46.00 C-8.76
0+68.80 #1		51.59 42.15 C-9.44		4+00	54.88 45.50 C-9.38
0+45.23 = B.C. 10'	10' RT. ↓	51.23 41.90 C-9.33		3+50	54.37 45.00 C-9.37
0+40 = C.I. #4		51.00 41.40 C-9.60	Scoopage 12 for Cl. inlet	3+00	53.93 T.P. 44.50 C-9.43
0+00 = C.I. #3	↓	44.36 40.80 C-3.56		2+50	53.49 42.00 C-9.49



Cut on 0+10 1/2 → 6.74  
56.74  
0+02 = 50.10 0+10 = 50.22  
C. 6.64 C. 6.52

set stub at 1+05t } on 1/2  
cb. face = 20+00. set nail at 0+10 } (Assumed)

8+96.83 C.I. #7 49.60

5700  
5703 = BP, N. W. by el. orten + Frank fort.

#3  
8+95.08 E.C. 57.00  
49.60 1' RT  
C-7.40

8+76.05 #2 56.75  
49.45 5' RT  
C 7.30

8+57.02 #1 56.73  
49.30 7' RT  
C 7.43

(8+38)  
8+37.99 = B.C. 56.68  
49.14 7' RT  
C-7.54

8+00 56.54 T.P.  
48.84  
C-7.70

7+50 56.23  
48.44  
C-7.79

7+00 55.73  
48.04  
C-7.69

6+50 55.99  
47.64  
C-8.35



FAIRMOUNT SEWER.

Montezuma - Sly.

7-15-52

W.O. 20770

sheets 1770 D to 1777 D

FB. 1640

" 2040

" 2124

0+00 = Exist. M.H. Montezuma & Fairmount

2+50  $\frac{3.1\%}{3}$   
133.02  
124.53  
C-8.49

P.O.T.  
9+00 M.H.#1  
132.06  
122.98  
C-9.08

1+50  
131.23  
122.03  
C 9.20

1+00  
30.39  
121.08  
C-9.29

0+66  $\frac{1.9\%}{11}$   
29.94  
120.43  
C-9.51

0+40  
29.74  
119.94  
C-9.80

0+00  
29.39  
119.18  
C-10.21

B.M. = chiseled  $\square$  in head wall  
195 ft of. Sta. 0+44 - EL. = 128.99

19

6+50

6+00

$\Delta 0^{\circ} 39' 45''$  Lt.  
5+60.83 M.H.#2.

5+50

5+00

4+50

4+00  $\frac{0\%}{3}$

3+50

3+00

T.P.

44.60  
136.93  
C 7.67

43.53  
135.38  
C 8.15

42.34  
134.17  
C 8.17

41.00  
133.85  
C-8.15

40.34  
132.28  
C 8.06

38.99  
130.73  
C 8.26

37.45  
129.18  
C 8.27

35.89  
127.63  
C 8.26

T.R.

134.60  
126.08  
C 8.52

INDEXED

FILED  
MAR 25 1953



Fairmount

20

T.P. = P.K. Nail 14' Lt.

9+50	53.04 146.23 C-6.81	12+50	62.19 153.53 C-6.66
9+00 3.19%	T.P. <sup>v</sup> 51.11 144.68 C-6.43	12+00 3.19%	61.07 153.98 C-7.09
8+77.21	50.36 143.98 C-6.38	11+88.59	60.86 153.62 C-7.24
A 11°-52'-30" Lt. 8+72.21 M.H.#3	143.82	11+83.59 = M.H.#4	EL. 13' R.P. Nails = 160.66 153.47
8+67.21	50.08 143.66 C-6.42	11+78.59	60.64 153.31 C-7.33
8+50	49.42 143.13 C-6.29	11+50	TIP. 59.76 152.43 C-7.33-
8+00 3.19%	47.77 141.58 C-6.19	11+00 3.19%	58.22 150.88 C-7.34
7+50 3.19%	46.73 140.03 C-6.70	10+50 3.19%	56.89 149.33 C-7.56
7+00	45.81 138.48 C-7.33	10+00	54.94 147.78 C-7.16



## Fairmount

P.K. Nail 14' Lt. of 16+40 El: 176.20

P.O.C. 80-22-30"	175.73	
16+40 = M.H.#5	167.62	
80-00'	C-8.11	75.08
+25'		167.15
70-2A'	74.33	C-7.93
16+00	166.38	
60-48'	C-7.95	73.54
+75'		165.60
60-12'-30	72.55	C-7.94
15+50	164.33	
50-37'	C-7.72	71.50
+25'		164.05
50-01	70.53	C-7.45
15+00	163.28	
40-25'	C-7.25	9.65
+75'		162.50
30-49'	8.65	C-7.15
14+50	161.73	
30-1A'	C-6.92	167.64 TR
+25'		160.95
20-38'	6.71	C-6.69
14+00	160.18	
20-02'	C-6.53	65.58
+75'		159.40
10-26'	64.92	C-6.18
13+50	158.63	
00-50.28 +25'	C-6.29	64.12
00-12.467	63.43	157.85
13+00	157.08	C-6.27
	C-6.35	
	63.13	
12+89.9 = B.C.	156.77	
	C-6.30	

T.P. 185.33

21

	180-49'		92.12
	20 +75'		183.72
	180-13'	91.11	C-8.40
20+50		182.80	
	170-37'	C-8.31	9.91
	+25'		184.87
	170-01'	9.01	C-8.04
20+00		180.95	
	160-25'	C-8.06	7.99
	+75'		180.02
	150-52'-30	87.25	C-7.97
19+50		174.10	
	(150-13'	C-8.15	86.39
	+25'		178.17
	140-37	TR 85.39	C-8.22
19+00		177.25	
	130-59'	C-8.14	84.22
	+75'		176.32
	130-26'	83.21	C-7.90
18+50		175.40	
	120-48'-30	C-7.81	82.20
	+25'		174.47
	120-12'	81.21	C-7.73
18+00		173.55	
	110-36	C-7.66	80.15
	+75'		172.62
	110-00'	9.20	C-7.53
17+50		171.70	
	100-23'	C-7.50	8.37
	+25'		170.77
	90-48	77.66	C-7.60
17+00		169.85	
	90-12'	C-7.81	76.86
	+75'		168.92
	80-36	76.08	C-7.94
16+50		168.00	
		C-8.08	



Fairmount

Δ 5028' Lt. Cont P. 38  
 Δ 10° 20' 42" Lt.  
 27+82.22 M.H.# 8

2A+50  
 04.24  
 194.93  
 C 9.31

24+00  
 02.52  
 193.48  
 C. 9.04

23+50  
 200.90  
 192.03  
 C-8.87

23+00 2.9%  
 9.28  
 190.58  
 C-8.70

22+50  
 97.71  
 189.13  
 C-8.58

22+00  
 95.94  
 187.68  
 C-8.26

21+50  
 94.80  
 186.26  
 C-8.54

19° 51'  
 = Δ 10° 29' 30" RT. of tan 9  
 21+17.91 = E.C. = M.H.# 6  
 93.74  
 185.30  
 C 8.44

19° 25'  
 21+00  
 193.10 TIP  
 184.65  
 C-8.45

202.28 T.P.

27+77.22  
 13.19  
 200.56  
 C 12.63

27+50  
 12.23  
 200.23  
 C 12.00

27+00  
 210.69 TIP  
 199.63  
 C 11.06

26+50 1.2%  
 209.19  
 199.03  
 C 10.16

26+00  
 07.81  
 198.43  
 C-9.38

25+55  
 06.94  
 197.89  
 C-9.05

Δ 19° 22' Lt.  
 25+50 - M.H.# 7  
 197.83

25+45  
 06.63  
 197.68  
 C-8.95

25+00 2.9%  
 05.46  
 196.38  
 C 9.08



Fairmount

Station	Offsets	Notes
30+00	5'lt. 18.35 209.75 = Invert C 8.60	Note: Grade And Line Change from Station 27+82.22 to 35+93.02 See P-38 to Page 41
29+50	" 17.21 208.75 C 8.46	
29+00	" 16.22 207.75 C 8.47	
28+81.09	" 215.86 207.37 C 8.49	
28+76.09 M.H.# 9	" 1 207.274	
28+71.09	" 15.62 206.95 C 8.67	
28+50	" 15.35 205.40 C 9.95	
28+00	" 13.68 204.85 C 11.83	
27+87.22	" 213.59 200.97 C-12.62	

Station	Offsets	Notes
33+00	5'lt. 25.92 213.52 = Invert C 10.40	Note: Grade And Line Change from Station 27+82.22 to 35+93.02 See P-38 to Page 41
32+50	" 1.69% 214.72 Not set	
32+47.50	" 24.71 214.68 C 10.03	
32+42.50	" $\Delta 6^{\circ}-53'-08''$ RT = 32+42.50 A } M.H.# 10 32+42.91 B }	
32+37.81	" 24.45 214.51 C 9.94	
32+00	" 223.40 213.75 C 9.65	
31+50	" 222.02 T.P. 212.75 C 9.27	
31+00	" 2.0% 20.81 211.75 C 9.86	
30+50	" 19.51 210.75 C 8.76	



Fairmount

$\Delta 14^\circ - 47' - 30''$  Rt.  
35+95.92 = M.H.# 12

221.50

offsets

54 Adjusted to B.M.  
opp Page.

35+90.92

5'lt.

~~34.79~~  
221.39 = Invert  
C 13.75

40+00

9.73  
243.57  
C-6.16

242.61 = Invert

T.P. 249.26

35+50

"

38.33  
220.94  
C 12.89

39+50

47.53  
241.38  
C-6.15

239.91

35+00 2.9%

"

31.61  
219.39  
C 12.32

39+00

46.59  
239.19  
C 6.40

237.31

34+50

"

30.67  
218.14  
C 12.53

38+50

49.53  
237.00  
C 6.53

234.71

N.G.

34+22.58

31.36  
217.51  
C 12.85

38+00

241.25 T.P.  
234.82  
C-6.43

232.11

$\Delta 23^\circ - 32' - 30''$  Rt.  
34+17.58 M.H.# 11

217.40

37+50

5.2%

9.18  
232.63  
C-6.55

229.51

34+12.58

30.07  
217.32  
C 12.75

37+00

6.96  
230.44  
C-6.52

226.91

34+00 1.6%

229.60 T.P.  
217.12  
C 12.48

36+50

35.33  
228.25  
C-7.08

224.31

CHK B.M. FB 2124  
26

33+50

27.67  
216.32  
C 11.19

36+00.92

34.70  
226.11  
C-8.59

34.70  
221.76  
C 12.94  
99

234.43 T.P.

234.48

0.05 diff  
Adjusted to B.M.

See Note: P. 23

Continued from P-40



Fairmount.

S.W.B.P. in culvert Head wall 25  
Van Dyke + Fairmount  $\frac{FB2124}{25}$  E.L. = 236.02

44+00  
7.90  
260.87  
C- 7.03

A7+50  
84.51  
276.15  
C- 8.46

266.26 T.P.

T.P. 283.50

43+50  
65.64  
258.72  
C- 6.92

A7+00  
82.23  
273.92  
C- 8.31

43+00  
63.20  
256.57  
C- 6.63

A6+50  
79.79  
271.70  
C 8.09

42+50  
60.90  
254.42  
C- 6.48

46+03.13  
77.55  
269.62  
C- 7.93

42+00  
8.90  
252.27  
C 6.63

$\Delta 4^{\circ}48'41''$   
A5+98.13 M.H.# 1A 269.40

T.P. 258.09

41+50  
56.71  
250.12  
C- 6.59

A5+93.13  
77.17  
269.17  
C 8.00

$\Delta 0^{\circ}43'30''$  Lt.  
41+30 = M.H.# 13  
T = 0.09  
55.96  
249.27  
C- 6.49

A5+50  
274.91  
267.32 T.P.  
C- 7.59

41+00  
54.27  
247.95  
C 6.32

A5+00  
72.34  
265.17  
C- 7.17

40+50  
52.01  
245.76  
C 6.25

A4+50  
9.90  
263.02  
C- 6.94



Fairmount.

51+50

98.54  
289.87  
C-8.67

51+00

265.0

99.33  
289.62  
C-9.71

50+51.22

300.21  
300.14 T.P.  
289.38

50+46.22 M.H. #15  
Δ 58°-44' Rt. M

C-10.83

Elev.  
289.36

50+41.22

99.85  
~~99.78~~  
289.12

C-10.66  
C 10.73

50+00

97.70  
287.27  
C 10.43

97.65  
287.27  
C-10.36  
Correct to  
B.M. on M.H.  
Stub.  $\frac{214}{31}$

49+50

74.93  
285.05  
C-7.88

T.P. 29259

49+00

1.45%

92.36  
282.82  
C-9.54

48+50

9.46  
280.60  
C-8.86

48+00

86.95  
278.37  
C-8.58

Existing M.H.

52+00

8.16  
290.13  
C 8.03



Sewer Extention  
Fairmount to Hilldale Road  
Pump house.

INDEXED  
law  
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54129

27

0+00 = 8+72.21 Fairmount line = M.H. #3

4+00 T.P. 62.36  
155.90  
C-6.46

1+10 46.42  
146.37  
C 0.05

3+50 61.33  
153.20  
C-8.13

5.49%

1+00 P.P. # 6

3+00 59.36  
150.50  
C-8.86

0+82 pier #5

2+85.56 58.21  
149.71  
C-8.50

0+64 pier #4

1.89%

A 12'-20' Lt  
2+80.56 M.H. # 16 = 149.44 ✓

0+46 pier #3

2+75.56 57.62  
149.35  
C-8.27

0+28 pier #2

2+50 55.09  
148.89  
C-6.20

0+10 pier #1

2+00 51.44  
147.99  
C-3.45

1.89%

0+00 M.H. #3 144.39

1+50 48.45  
147.09  
C 1.36



7+56.45  
181.38  
173.95  
C- 7.43

7+50  
180.96  
173.65  
C- 7.31

7+00  
78.56  
171.20  
C- 7.36

6+50  
A. 9%  
75.96  
168.75  
C- 7.21

6+00  
73.10  
166.30  
C- 6.80

5+50  
70.85  
163.85  
C- 7.00

P.O.T.  
5+20.56 M.H. 17  
7.49  
162.40  
C- 7.09

5+00  
8.30  
161.30  
C 7.00

4+50  
5.42  
64.91  
158.60  
C- 6.31

11+00

10+50

10+00

9+50

9+00

8+50

8+00

7+66.45

7+66.45 M.H. # 18 174.20 El. & stub = 183.31

8.90  
191.80  
C 7.10

75.81  
189.20  
C- 6.61

93.90  
186.60  
C 7.30

T.P. = 193.20

91.27  
184.00  
C 7.27

9.86  
181.40  
C- 8.46

88.52  
178.80  
C- 7.72

84.70  
176.20  
C- 8.70

T.P. 184.15

82.16  
174.46  
C- 7.70



Hilldale

29

14+00	12.55 205.75 C-6.80		17+00	25.50 219.25 C-6.25
13+50	10.97 203.50 C-7.47	T.P. 210.08	16+50	25.45 T.P. 217.00 C-6.45
13+00	8.64 201.25 C-7.39		16+00	21.40 214.75 C-6.65
12+50	206.15 199.00 C-7.15		15+50	19.22 212.50 C-6.72
12+00	03.65 196.75 C-6.90		15+23.12	18.54 211.30 C-7.24
11+67.85	202.30 195.30 C-7.00		$\Delta 14^{\circ}18'-30''$ L. 15+18.12 M.H. #20 211.06	
$\Delta 26^{\circ}49'-20''$ R. 11+62.85 M.H. #19	195.07		15+13.12	17.80 210.85 C-6.95
11+57.85	202.00 194.81 C-7.19		15+00	16.95 210.25 C-6.70
11+50	201.64 194.40 C-7.24		14+50	14.70 208.00 C-6.70

4.5%

4.5%

5.2%



20+44.8	50.09 241.80 C-8.29		23+57.28	9.59 260.63 C-8.96
20+00	47.80 238.39 C-9.50	T.P. 247.91	23+50	9.17 260.20 C-8.97
19+50 78.90	44.59 234.40 C 10.19		23+00	65.70 257.20 C-8.50
19+00	8.91 230.50 C-8.41	239.58 T.P.	22+50	61.83 254.20 C-7.63
18+50	34.45 226.60 C-7.85		22+00	8.92 251.20 C 7.72
18+36.91 Δ 790-26' RT.		32.14 225.58		
18+34.91: M.H. 21	225.18	C 6.56	21+50	56.04 248.20 C 7.84
				255.95 T.P.
18+26.91	32.11 224.96 C-7.15		21+00	53.18 245.20 C 7.78
18+00 A.596	30.56 223.75 C-6.81		20+54.8	50.79 242.48 C-8.31
17+50	8.14 221.50 C-6.64		Δ 230-254.15" LT. 20+49.80 M.H. #22	242.18



T.P. 234.55

Δ 37°-48' Lt.  
26+44.90 M.H.#24

279.57

29+00

31.80  
328.45  
C- 3.35

26+39.9

90.82  
279.25  
C- 11.57

28+75

23.91 T.P.  
320.57  
C- 3.34

287.93 T.P.

31.5%

26+00

86.58  
276.62  
C- 9.96

28+50

316.42 T.P.  
312.70  
C- 3.72

25+50

80.65  
273.32  
C- 7.33

T.P. 281.35

28+10

307.13 T.P.  
5.71  
300.10  
C- 5.61

25+00  $\frac{6.6}{10}$

77.75  
270.02  
C- 7.73

Δ 10°-35'-15" Lt.  
28+04.68 M.H.#25

298.42

24+50

75.07  
266.72  
C- 8.35

272.44 T.P.

28+00

304.25  
297.87  
C- 6.38

24+00

71.77  
263.42  
C- 8.35

27+50

98.75 T.P.  
291.97  
C- 6.78

$\frac{9.8}{11.1}$

23+67.28

70.15  
261.26  
C- 8.89

27+00

93.98  
286.07  
C- 7.91

Δ 15°-55'-30" Rt.  
23+62.28 M.H.#23

260.93

26+50

91.59  
280.17  
C- 11.42



1/2 0100 hub. on £ E1360.87

Exist. M.H.  
31470.92

60.63  
341.55  
C19.08

31450

60.27  
341.36  
C18.91

31400

58.71  
340.92  
C17.79

30450

88.80  
0

57.13  
340.48  
C16.65

30400

53.87  
340.04  
C-13.83

353.29

29450

46.80  
339.60  
C-7.10

T.P. 343.97

P.O.T.  
29435 M.H. #26

42.78  
339.47  
C-3.31

29425

31.59

40.05  
336.32  
C-3.73



Sewer Extension

From Fairmount to Hart St Pump  
House  
North of Aldine Drive.

0+00 = M.H. # 8 = sta. 27+82.22 Fairmount <sup>line</sup>

1+50 4.89  
202.18  
C-2.71

1+00 3.35  
201.68  
C-1.67

start v.c.  
0+50 End, C.I. 0.69  
201.18  
F 0.49

0+41 Pier #2

0+23 pier #1

0+1A

Fairmount to south  
Δ 74° 42' - 22" off  
0+00 = M.H. # 8 200.68

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A+50

19.66  
210.17  
C-9.49

A+00

15.87  
205.87  
C 10.00

3+65.55

9.91  
202.91  
C 7.00

8.91

= 3+60.55

Δ 22° - 23' - 30" RT.  
1+80.20 M.H. # 28 202.48V

1+75.12

8.43  
202.43  
C 6.00



			$\Delta 10^{\circ} 40' N$ , 10+31.20 M.H.# 31	244.82
7+50	8.43 230.66 C-7.77		10+26.2	51.73 244.57 C-7.16
7+00	38.05 227.96 C-10.09		10+00	50.66 243.26 C-7.40
6+50	34.79 225.26 C-9.53	TP 234.38	9+50	47.49 240.76 C-6.73
6+00	30.75 222.56 C 8.19		9+00	45.82 238.26 C-7.56
5+89	9.70 221.97 C-7.73		8+50	45.36 235.76 C-9.60
$\Delta 8^{\circ} 32' N$ , 5+84 = M.H.# 29	221.70 ✓		8+00	42.82 233.26 C-9.56
5+79	228.40 T.P. 221.27 C-7.13		7+78.56	41.37 232.19 C-9.18
5+50	24.92 T.P. 218.77 C-6.15		$\Delta 9^{\circ} 35' 30'' N$ , 7+73.56 M.H.# 30	231.94
5+00	21.10 214.47 C 6.63		7+68.56	41.15 231.66 C-9.49

514.96

5.96

T.P. 251.10

T.P. 243.80



13+09.33 $\frac{5.6\%}{5.15}$	65.71 258.76 C-6.95	17+00	97.94 287.60 C 10.34
$\Delta 15^\circ 47' - 30''$ Lt. 13+04.33 M.H.#32	258.48	16+50 $\frac{11.4\%}{11.4\%}$	94.90 281.90 C 13.00 T.P. 293.33
12+99.33	65.23 258.22 C 7.01	16+00	86.84 276.20 C-10.64 T.P. 284.42
12+50	62.47 255.76 C-6.71	P.O.T. 15+80 M.H.#33	83.10 273.92 C 9.18
12+00	9.71 253.26 C-6.45 T.P. 259.26	15+50	79.83 272.24 C-7.59
11+50	56.64 250.76 C-5.88	15+00	77.20 269.44 C-7.76 T.P. 276.00
11+00 $\frac{5.7\%}{5.7\%}$	55.13 248.26 C-6.87	14+50 $\frac{5.6\%}{5.6\%}$	72.78 266.64 C 6.14
10+50	53.55 245.76 C-7.79	14+00	70.84 263.84 C 7.00
10+36.2	52.16 245.07 C 7.09	13+50	67.89 T.P. 261.04 C 6.85



T.P. 307.12

12.76

3198.8

0.27

319.61

13.06

332.67

0.14

332.53

11.32

343.85

0.13

343.72

6.93

350.65

2.34

348.31

9.01

357.32

246

354.86 = Ctr. Ranjo (L+T. coveral)

354.44 - F.B. 1646.

+ 0.42

R59

T.P. 307.12

305.03

19+22.36 = M.H. 35

303.14

C 1.89

303.00

19+02

302.86

C 0.14

304125 T.P.

4.79

18+50

302.14

C-2.65

18+29.28

3.41

301.84

C 1.57

Δ 7°-44' 104RK

18+2A.28 M.H.#34 301.77

2.66

18+19.28

301.20

C 1.46

18+00

301.56

299.00

C 2.56

T.P.

17+50

99.63

293.30

C-5.73







Walker  
Hurdin  
Huffman  
Frasier  
Sparks  
9-3-52

FAIRMOUNT AVE. SEWER CONST. (Per Inst. Harvey Cole)

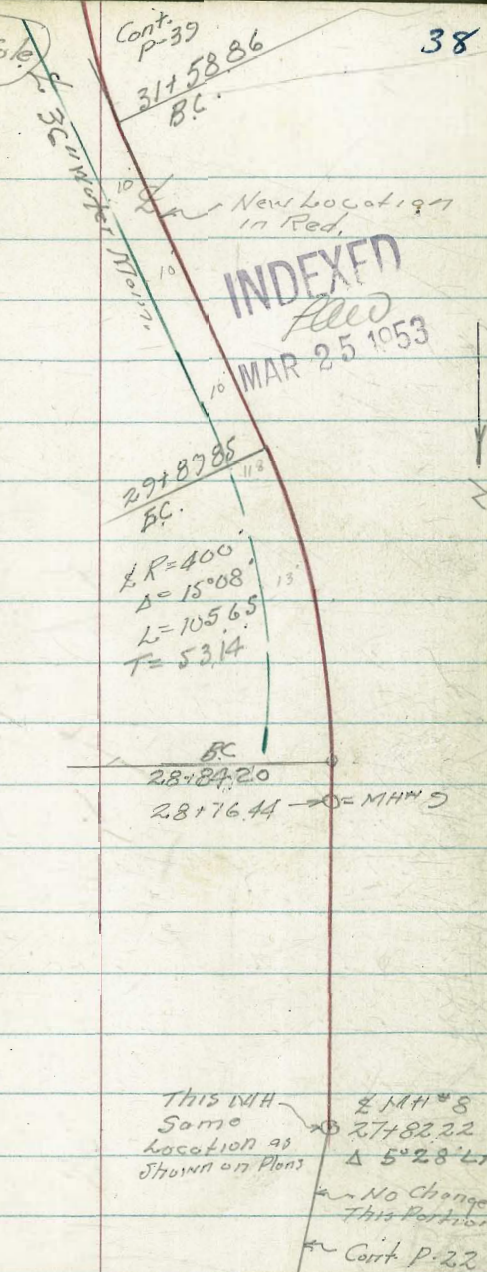
Alignment and Grade Change  
from 27+82.22 to 35+23.02

To Give Clearance  
Exist. 36" Water Main

Cont.  
P-39  
31+58.86  
B.C.

38

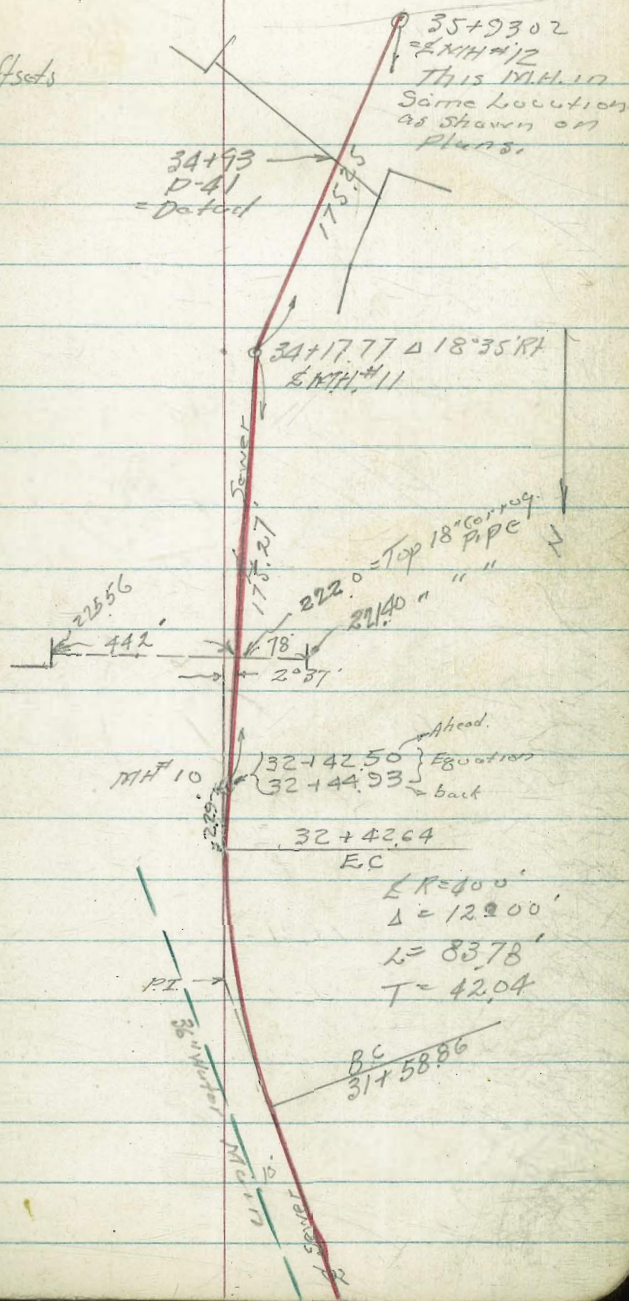
Station	Corit	Elev. stakes	Elev. Invert	Cuts	Offsets
31+20	P. 39	221.03	213.58	7.45	5' Lt.
30+80		219.90	212.55	7.35	"
30+40		219.11	211.52	7.59	"
30+00		218.71	210.50	8.21	"
29+89.85 = B.C.	7°34'	218.40	210.23	8.17	"
29+75	6°30.4	218.20	209.85	8.35	"
29+50	4°42.9'	217.88	209.21	8.67	"
29+25	2°55.4'	217.39	208.56	8.83	"
29+00	1°07.9'	216.87	207.92	8.95	"
28+84.20 = B.C.		216.35	207.51	8.84	"
28+76.44 = M.H. 9			207.31		
28+71.44		216.07	206.96	9.11	"
28+50		215.40	205.44	9.96	"
28+00		213.87	201.89	11.98	"
27+87.22		213.84	200.97	12.57	"
27+82.22 = M.H. # 8			200.62		
chk. stub 28+50' 5' Lt. P-23		215.36			
		215.86			





Fairmount Ave - Sewer Const.  
Alignment and Grade Change

	Filey. Station	Elev. Invert	Cuts	offsets
Cont. from P-40				
35+40	T.P. → 233.11	224.48	8.63'	
34+90		231.17	223.15	8.02'
34+50		230.22	222.08	8.14'
34+22.77		229.92	221.35	8.57'
Δ 18°35' RT				
34+17.77 = 2 M.H. #11		221.22		
34+12.77		229.50	221.10	8.40'
34+00		228.85	220.77	8.08'
33+60		227.54	219.75	7.79'
33+20		226.25	218.73	7.52'
32+80		225.22	217.71	7.51'
32+47.50		224.67	216.88	7.79'
32+42.50 Ahead (2 M.H. #10)				
32+44.93 = back (Elev. of 15M)		224.67	216.75	
32+42.64 = E.C. 6°00'		224.55	216.69	7.86'
32+25	4°44.3 TP →	224.17	216.24	7.93'
32+00	2°56.7	223.41	215.62	7.79'
31+75	1°09.4	222.65	214.98	7.67'
31+58.86 = B.C.		222.09	214.57	7.52'
Cont. from P-38				





Fairmount Ave Sewer Const.  
 Alignment and Grade Change

Continued on p. 24

FB2124-26 → 234.48  
 P-24 → 234.43  
 Chk L 3610092 P-24 234.44

35 + 23.02 = L MH#12 225.90  
 = Sta 35 + 20.92 (old Sta.)  
 35 + 88.02 234.80 225.76

2.67%

8.74

35 + 23.02  
 L MH#12

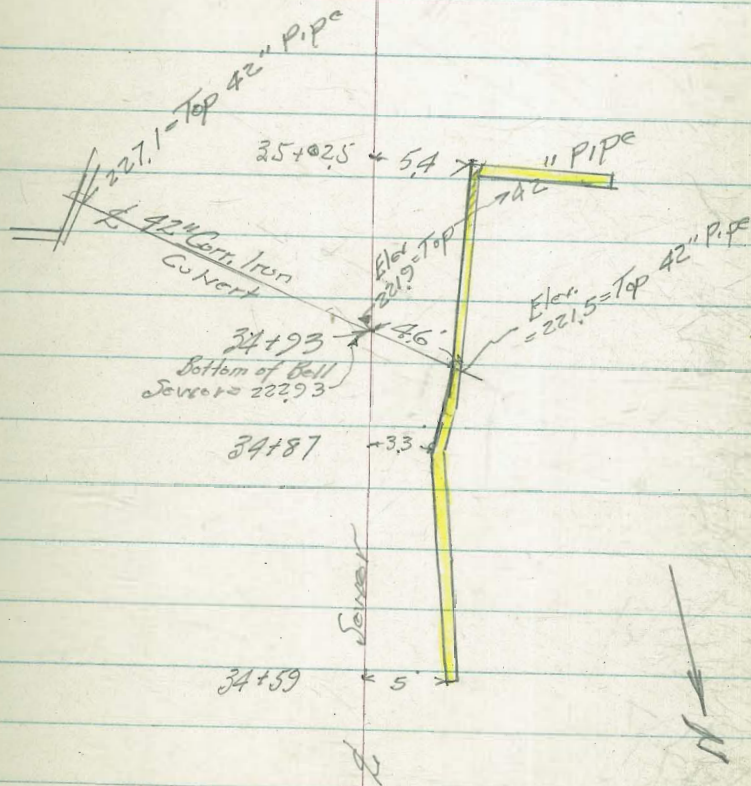


Fairmount Ave Sewer

Walker  
 Hardin  
 Huffman  
 Pesley  
 9-5-52

34+93

	Sewer	
	Invert	223.23
		- 3.0
	Sewer	
	Bottom Bell	222.93
	Top 42" Pipe	= 221.90
	Clearance	= 1.03





ALDINE DRIVE SEWER.

FAIRMOUNT TO MONROE.

9-12-52

Sheet 1777-D.

INDEXED  
Plan  
MAR 25 1953

2+00 40.00  
232.53  
C-7.47

1+50 8.50  
230.90  
C-7.60

1+00 37.37  
229.27  
C-8.10

0+75 36.85  
228.44  
C-8.41

3.27 1/2

0+50 36.30  
227.63  
C-8.67

0+25 35.46  
226.81  
C-8.65

0+05 34.65  
226.16  
C-8.49

=0+00 - M.H.#12 226.00

35+95.92 Fairmount 1140

B.M. - P-25 - E.L. = 236.02 = B.P. 77 42  
head wall

Δ 3° 04' Lt.  
5+20.62 = M.H.#37 244.92

250.99 TIP

5+15.62 52.22  
244.72  
C-7.50

5+00 51.60  
244.10  
C 7.50

4+50 9.63  
242.10  
C-7.53

4+00 7.55  
240.10  
C-7.45

1/2

3+50 45.44  
238.10  
C-7.34

3+00 43.47  
236.10  
C-7.37

P.O.T.  
2+60 = M.H.#36 41.90  
234.50  
C-7.40

2+50 241.57 TIP  
234.17  
C-7.40



## Aldine Drive

43

8+50	65.88 258.73 C-7.15	*P. 267.17	11+50	85.26 TIP, 277.42 C-7.84
P.O.T. 8+20 = M.H.#38	64.26 256.90 736		11+26.12	83.65 275.63 C 8.02
8+00	63.36 256.10 C-7.26		Δ 19°06' Lt. 11+21.12 = M.H.#39	83 275.26
7+50	61.08 254.10 C-6.98		11+16.12	82.80 274.96 7.84
7+00	259.13 = TIP. 252.10 C-7.03		11+00	81.55 273.98 C-7.57
6+50	7.08 250.10 C-6.98		10+50	7.57 270.93 C-6.66
6+00	55.12 248.10 C-7.02		10+00	74.15 267.88 C-6.27
5+50	53.45 246.10 C-7.35		9+50	71.23 264.83 C-6.40
5+2562	52.58 245.12 C-7.46		9+00	68.51 261.78 C 6.73

A/P

6.19%

T.P. 276.40



14+50  
307.49  
299.90  
C 7.58

14+00  $\frac{2}{1}$   
303.43  
296.15  
C 7.28

13+50  
9.75  
292.40  
C 7.35

13+19.32 #4 E.C.  
7.73  
290.10  
C 7.63

12+9A.60 #3  
96.04  
288.25  
C 7.79

12+69.87  $\frac{10}{1}$  #2  
94.23  
286.40  
C 7.83

12+45.14 #1  
92.15  
284.55  
C 7.60

A parts  
12+20.42 = B.C. Lt.  
90.25  
282.70  
C 7.55

12+00  
8.77  
281.17  
C 7.60

A 11° A8' Lt.  
16+85.47 M.H. # 41  
27.82  
319.94

16+80.47  
26.89  
319.52  
C 7.37

16+50  
23.61  
316.90  
C 6.71

16+00  
18.79  
312.60  
C 6.19

15+50  $\frac{8.6}{10}$   
14.76  
308.30  
C 6.46

15+00  
11.08  
304.00  
C 7.08

14+76.65  
9.40  
302.00  
C 7.40

A 23° 51' Rt  
14+71.65 M.H. # 40  
301.55

14+66.65  
8.85  
301.15  
C 7.70

303.22 T.P.

T.P. 62115

T.P. 312.05



Aldine Dr.

45

Existing M.H.	9.00
18+44.23	322.80
	C - 6.20

18+00	28.86
	322.00
	C 6.86

17+50	30.22
	321.10
	C - 9.12

17+00	8.55
	320.20
	C - 8.35

16+90.47	7.82
	320.03
	C - 7.79



ARCHER ST.  
SEWER

9-23-52

sheet 9144-L

" 9148L

Dawes - west. stakes 5' RT.

Main line Laterals

2+00 = D.E.

8.28 #1  
163.54  
C 4.74

1+50

169.25 F.P. #2  
162.79  
C 6.46

1+00

8.54 #3  
162.04  
C 6.50

0+50

6.80 #4  
161.29  
C 5.51

= 0+00

+ Dawes  
M.H. Ctr. Archer

5.88  
160.54  
C 5.34

See page 7

B.M. = S.W. 7' Mon. Dawes + Archer EL. = 164.30

INDEXED

MAR 25 1953

From Dawes east.

stakes 5' RT.

Main line Laterals  
see p. 47

1+48 1/2

6.79  
170.91  
C-5.88

1+10

73.97 T.P.  
169.11  
C 4.86

0+70

71.42  
167.23  
C 4.19

0+30 M.H. #1

9.33  
165.35  
C-3.98

0+00

7.97  
164.56  
C 3.41

~~0-111 Lat #5~~

+ Archer = 0-152 E  
M.H. Ctr. Dawes



Archer Sewer Laterals

Daws west 9-22/50  
9144L + 9143L

Stakes 5' RT of Lateral.

± Archer = 0+00

24' N. ± Archer  
0+24

2+00 #1

70.15  
164.32  
C 5.83

North  
1/4c. Archer  
0+35

71.33  
168.00  
C 9.33

1+50 #2

171.61  
163.57  
C 8.04

1+00 #3

70.87  
163.00  
C- 7.87

0+50 #4

69.18  
162.07  
C- 7.11

0+00 ± Daws

Daws East  
9144L + 9143L

Laterals staked 5' RT (East) of ±

Main line (± Archer) = 0+00

0+24  
24' N. ± Archer

1+18 #7

7.52  
171.50  
C 6.02

0+68 #6

8.55  
174.00  
C 4.55

0-127<sup>8</sup> Lat #5

TP  
67.42  
162.00  
C 5.42

0-152<sup>8</sup> ± Daws

8.60  
165.00  
C- 3.60



Cass St Sewer

So. of Van Nuys

INDEXED

MAR 25 1953

Stakes 5' Rt of  $\pm$

For location see sheet 9146-L

For profile see sheet 9148-L

B.M. = S.W. 7 Mon Cass  $\pm$  Van Nuys  $\pm$  E.L. = 168.60

1+97<sup>5</sup> = M.H.#2

165.25

1+92<sup>5</sup>

7685  
165.22  
C 111.63

1+50

169.59 T.P.  
164.92  
C 4.67

1+00

8.57  
164.57  
C 4.00

0+50

9.50  
164.22  
C 5.38

Exist 149 M.H.

0+00

70.81  
163.87

$\pm$  Cass  $\pm$   
 $\pm$  Alley BIK A

C 6.94

Van Nuys Sewer

East & west of Cass - sheet 9146-L

48

1+00 = D.E.

71.75  
165.95  
C 5.80

0+50

74.94  
165.60  
C 9.34

0+05

78.23  
165.27  
C 12.96

0

0+00 =  $\pm$  Cass

165.25

2+40 M.H.#3

8.32  
174.85  
C 3.47

2+00

7.30  
173.25  
C 4.05

1+50

6.65  
171.25  
C 5.40

1+00

75.00  
169.25  
C 5.75

0+50

71.80  
167.25  
C 4.55

0+05

76.85  
165.45  
C 11.40

0+00 =  $\pm$  Cass

165.25

West of Cass

East of Cass



Van Nuys

19

Water line East of Cass (248' pipe.)

9-24-52

sheet 9146-L

stakes set 5' int. of  $\phi$ .

248 = End

9.54  
178.02  
C-1.52

2100

7.26  
176.10  
C-1.16

1450

176.48  
174.10  
C-2.38

1400

173.197R

174.14  
172.10  
C-2.04

0450

71.98  
170.10  
C-1.88

0400

69.85  
168.10  
C-1.75

0-15 = Ely line Cass



7453

ARCHER.

sheets

9142-L

9143-L

9144-L

ARCHER

East of Dawes.

INDEXED

50

MAR 25 1958

South

North

South

North

Rough

Curb

Curb

Rough

Rough

Curb

Curb

Rough

wly. Dawes

3+40<sup>8</sup>

4.90

164.90

grade

Page 51

164.90

2+20<sup>8</sup> Brk3.94  
164.925.41  
164.926.01  
165.9270.45  
165.92

F0.98

C0.49

C0.09

C.453

3+20<sup>8</sup>

4.48

164.43

164.43

2+00

4.33  
165.90

C0.16

F0.38

70.75  
166.90

F1.57

C3.85

3+00<sup>8</sup>

4.60

164.21

71.44

164.21

1+50

5.95  
168.25

C0.22

F0.21

71.70  
169.25

F2.30

C.2.45

2+80<sup>8</sup>

C0.39

7.23

1+00

68.90  
170.60C0.12  
~~F0.01~~

F0.15

Nail  
4.91  
171.60

F1.70

C.3.31

Ely. Dawes

2+60<sup>8</sup>

4.60

164.25

164.25

C0.35

0+50

71.62  
172.95C0.21  
C0.14

F0.15

7.61  
173.95

F1.33

C3.66

db. B.C. on H.

2+52<sup>8</sup>

2.80

163.75

4.98

163.75

4.40

164.55

9.16

164.55

F0.15

C.4.61

0+00

5.35  
175.308.40  
175.307.06  
176.3081.96  
176.30

C0.05

C0.70

C0.36

C5.66

Brk. 8

2+40<sup>8</sup>

3.55

164.11

5.03

164.11

5.01

165.11

9.76

165.11

Revol.

5.78

175.30

C0.43

F0.56

C0.92

F0.10

C.4.65

C0+00 = 260<sup>8</sup> East of Ely. line Dawes



# ARCHER

Dawes - west to end

51

	Rough	Curb	Curb	Rough
1+20	0.5 6.75 167.10 F 0.35	7.25 167.10 C 0.15	7.64 167.60 C 0.04	73.25 167.60 C 5.65
1+00	6.84 166.82 C 0.02	7.19 167.32 F 0.13		
0+80	6.89 166.47 C 0.42	6.80 166.47 C 0.33	6.99 166.97 C 0.02	73.05 166.97 C 6.08
0+60	6.39 166.06 C 0.33	6.52 166.56 F 0.04		
0+40	X 5.44 165.56 F 0.12	5.58 165.56 C 0.03	6.00 166.06 F 0.06	72.05 166.06 C 5.99
0+20	5.16 165.00 C 0.16	5.19 165.50 F 0.31		
Ch. E.C. on left 0+08	4.89 164.64 F 0.12	4.89 164.64 C 0.25		
wly line Dawes 0+00			72.16 164.90	
(3+40 <sup>2</sup> (P-59)) =			C 7.26	

	Rough	Curb	Curb	Rough
3+80	8.03 168.01 C 0.02	8.25 168.01 C 0.24	8.37 168.51 F 0.14	70.81 168.51 C 2.30
3+60	7.98 168.16 F 0.18	8.45 168.16 C 0.29	8.67 168.66 C 0.01	70.55 168.66 C 1.89
3+40	7.55 168.21 F 0.76	8.49 168.21 C 0.28	8.60 168.71 F 0.11	70.44 168.71 C 1.73
Brk 3+20	7.11 168.17 F 1.06	8.37 168.17 C 0.20	8.50 168.67 F 0.17	70.52 168.67 C 1.85
2+80	6.80 167.98 F 1.18	10.09 C 0.09	F 0.02	72.82 168.48 C 4.34
2+40	7.03 167.79 F 0.76	C 0.27	F 0.03	70.50 168.29 C 2.22
Map. Sta. 2+00	0.5 7.17 167.60 F 0.43	C 0.41	C 0.23	70.98 168.10 C 2.88
chain 383				
Brk 1+60	0.5 6.80 167.43 F 0.63	7.58 167.43 C 0.15	8.18 167.93 C 0.25	71.71 167.93 C 3.78
1+40	7.48 167.30	8.05 167.80 C 0.18		167.80



ARCHER

	Rough	Curb	Curb	Rough		Rough	Curb	Curb	Rough
0+20	62.59 162.55			C3.70 163.05	3+00	147.77	9.57 149.67	0.17 150.27	150.27
0+50	C0.04	C0.37	Grade	C0.85			F0.10	F0.10	
0+10 C.B.C.	2.98 163.07 F0.09	3.17 163.07 C0.10	3.83 163.57 C0.26	64.01 163.57 C4.44	2+80	50.26 150.47 F0.21	0.96 150.39 C0.07	0.95 150.98 F0.03	1.58 150.98 C0.60
Wly. line Cass. 0+00	163.43				2+60	151.25	1.38 151.19 C0.19	1.66 151.75 F0.09	151.75
Ely. Cass 5+00	165.14			165.76	2+40	2.98 152.08 C0.90	2.22 152.04 C0.18	2.31 152.58 F0.27	2.82 152.58 C0.24
C.B.C. 4+90	5.45 165.50 F0.05	5.34 165.50 F0.16	6.05 166.00 C0.05	9.85 166.00 C3.85	2+20	152.97	3.32 152.95 C0.37	3.26 153.47 F0.21	153.47
4+60	166.40	6.50 166.40 C0.10	6.80 166.90 F0.10	166.90	P.V.C. 2+00	4.31 153.91 C0.40	4.12 153.91 C0.21	4.30 154.41 F0.11	5.15 154.41 C0.74
4+40	C.90 166.95 F0.05	8.80 166.95 F0.15	7.16 166.95 C4.21	7.57 167.45 C0.12	1+55	5.40 156.07 F0.67			56.77 156.57 C0.120
4+20	7.14 167.40 F0.26	7.63 167.40 C0.23	7.98 167.90 C0.08	70.16 167.90 C-2.26	1+50	57.68 158.23 F0.55			57.90 158.73 F0.83
4+00	7.62 167.75 F0.13	9.82 167.75 C0.07	8.22 168.25 F0.03	70.51 168.25 C-2.26	1+00	60.51 160.39 C0.12	C0.15	F0.41	61.01 160.89 C0.12



ARCHER

	Rough	Curb	Curb	Rough		Rough	Curb	Curb	Rough
7+00	7.00 137.15 F0.15	grade	F0.05	39.24 137.65 C-1.59	11+19 = Wldy. line La Jolla Mesa Dr.				
6+50	8.80 138.72 C0.08	C0.36	F0.11	41.02 139.22 C-1.80	66, B.C. 10+91	4.35 124.86 F0.51	4.90 124.86 C0.04	125.47 F0.31	32.08 125.36 C-6.72
6+00	40.20 140.29 F0.09	C0.20	F0.05	2.60 140.79 C-1.81	10+50	6.25 126.15 C0.10	C0.15	F0.41	31.65 126.65 C-5.00
5+50	1.00 141.86 F0.86	C0.20	F0.35	3.58 142.36 C-1.22	10+00	6.93 127.72 F0.79	C0.14	F0.19	31.90 128.22 C-3.68
5+00	3.17 143.44 F0.27	F0.05	F0.35	4.71 143.94 C-0.77	9+52 on Lt. 9+50 on Rt	8.78 129.29 F0.51	C0.21	F0.12	32.97 129.79 C-3.18
4+50	5.19 145.01 C0.18	C0.05	F0.08	5.93 145.51 C0.42	9+00	29.93 130.86 F0.93	F0.37	C0.05	3.84 131.36 C-2.48
4+00	6.98 146.58 C0.40	F0.02	F0.30	8.00 147.08 C0.92	8+50	1.61 132.43 F0.82	F0.08	F0.20	5.53 132.93 C-2.60
3+50	8.31 148.16 C0.15	F0.15	F0.10	50.30 148.66 C-1.64	8+00	3.11 134.00 F0.89	C0.12	F0.19	7.10 134.50 C-2.60
E.V.C. 3+20	8.61 149.11 F0.50	148.98 Met. Curb.	9.36 149.61 F0.35	51.30 149.61 C-1.69	7+50	5.12 135.57 F0.45	C0.22	F0.27	7.43 136.07 C-1.36



ARCHER ST.

1.12.33

53

La Jolla Mesa Dr. - West

	Rough	Curb	Curb	Rough
3+00	4.46 115.29 F0.83	C0.05	F0.10	T.P. 118.13 115.79 C 2.34
2+50	6.15 116.76 F0.61	C0.15	F0.30	19.00 117.26 C-1.74
2+00	7.98 118.23 F0.25	C0.08	F0.38	20.81 118.73 C-2.08
1+50	20.50 119.70 C 0.80	C0.44	C0.07	2.63 120.20 C 2.43
1+00	1.08 121.17 F0.09	C0.38	C0.36	4.81 121.67 C-3.14
0+50	2.59 122.64 F0.05	C0.11	C0.17	6.22 123.14 C 3.08
Cl. E.C. 0+28	2.84 123.28 F0.44	3.23 123.28 F0.05		7.10 123.78 C-3.32

0+00 = Wly line La Jolla Mesa Dr.

	Rough	Curb	Curb	Rough
of Archer 4+79.9 = End.				See P-70
Cl. B.C. 4+62.9	1.04 110.50 C 0.54			4.14 111.00 C 3.14
4+50	11.04 110.88 C 0.16	Meat curb.	F0.34	4.21 111.38 C-2.83
4+00	1.74 112.35 F0.61	C0.05	F0.65	5.26 112.85 C-2.41
3+50	3.65 113.82 F0.17	C0.05	F0.20	7.07 114.32 C-2.75



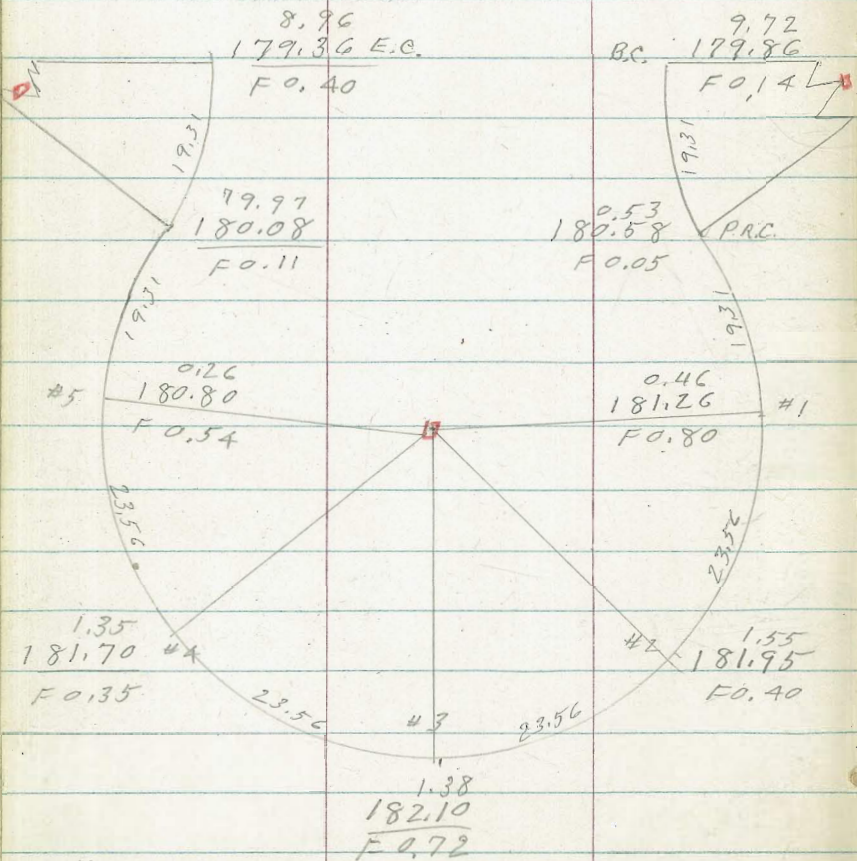
# Van Nuys

INDEXED  
MAR 27 1955

300' East of Cass to 480' West of La Jolla Mesa Drive

Banjo on east end

2+09. = Fly line Cass



	Rough	Curb	Curb	Rough
ob. B.C. on Rt. 2+01			1.82	
			171.82	
			Grade	
ob. B.C. on Lt. 1+99		1.48		
		171.40		
		C0.08		
		3.50	173.75	
		173.36	173.86	
		C0.14	F0.11	
		5.36	6.15	
		175.36	175.86	
		X	C0.29	
		177.48	7.81	
		177.38	177.86	
		C0.12	F0.05	
ob. E.C. 0+00		179.36	179.86	

For Rough grade see P 68-Lt.

For Rough Grade see P 68-Lt.



Van Mays

El. Curb Inlet & 164<sup>th</sup> 55  
Sta. 295 to 346 t

Rough Curb Curb Rough

Rough Curb Curb Rough

1+80 W-line	4.09 164.97 F0.88	5.15 164.97 C0.18	5.40 165.47 F0.07	7.45 165.47 C1.98
1+60	—	5.25 165.25 x	5.70 165.76 F0.06	—
1+40	3.94 165.62 F1.68	165.70 165.62 C0.08	<sup>P.</sup> 6.07 166.12 F0.05	7.81 166.12 C1.69
1+20	—	6.20 166.03 C0.17	6.51 166.53 F0.02	—
P.V.C. 1+00	D-1' 5.87 166.50 F0.63	6.72 166.50 C0.22	7.13 167.00 C0.13	9.65 167.00 C2.65
0+55	6.80 167.62 F0.82	8.10 167.62 C0.48	8.35 168.12 C0.23	72.55 168.12 C4.43
cl. B. on Lt. 0+10	67.77 168.75 F0.78	168.75		
cl. B. C. on Rt 0+08			169.30	75.65 169.30 C6.35
0+00 = Wly line Cass				

4+40	1.20 161.93 F0.73	2.08 161.93 C0.15	2.06 162.43 F0.37	6.18 162.43 C-3.75
4+20	—	2.52 162.48 C0.04	2.86 162.98 F0.12	—
X-5' 4+00	1.71 162.92 F1.21	2.92 162.92 Grade	3.48 163.42 C0.06	7.98 163.42 C4.56
3+80	—	3.30 163.25 C0.05	4.07 163.75 C0.32	—
P.V.C. 3+60	1.97 163.46 F1.49	3.36 163.46 F0.10	4.13 163.96 C0.17	7.48 163.96 C-3.52
3+20	2.80 163.77 F0.97	3.93 164.01 F0.08	4.36 164.27 C0.09	8.68 164.27 C-4.41
2+70	<u>E 164.10</u> <u>2+95, E.L. Curb Inlet</u> <u>Moat C.Z.</u> 3.33 164.15 F0.82	4.41 164.37 C0.09	4.36 164.65 F0.29	8.10 164.65 C-3.45
ENC. Vail 2+20 line	3.80 164.54 F0.74	5.11 164.54 C0.57	4.96 165.04 F0.08	7.24 165.04 C2.20
2+00	—	5.08 164.72 C-0.36	65.21 165.22 F0.01	TIP —



Van Noy's.

50

Fly line Buena Vista Tract.

Rough

Rough Curb Curb Rough

7+23 <sup>E</sup>	49.25 150.23 F 0.98	—	—	1.61 150.73 C 0.88
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7+19 <sup>E</sup>	—	0.48 150.38 C 0.10	0.93 150.88 C 0.05	—
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6+99 <sup>E</sup> P.V.C.	49.80 151.18 F 1.38	1.13 151.18 F 0.05	51.68 <sup>TR</sup> 151.68 Grade	3.34 151.68 C 1.66
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6+50	3.08 153.28 F 0.20	<sup>TR</sup> 153.62 153.28 C 0.34	3.60 153.78 F 0.18	6.30 153.78 C 2.52
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6+00	5.10 155.40 F 0.30	5.74 155.40 C 0.34	5.88 155.90 F 0.02	6.53 <sup>X</sup> 155.90 C 4.63
------	--------------------------	--------------------------	--------------------------	---------------------------------------

5+50	6.79 157.51 F 0.72	7.66 157.51 C 0.15	7.79 158.01 F 0.22	6.07 158.01 C 2.06
------	--------------------------	--------------------------	--------------------------	--------------------------

5+00 X-	8.70 159.62 F 0.92	9.59 159.62 F 0.03	160.02 <sup>TR</sup> 160.12 F 0.10	4.49 160.12 C 4.37
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E.V.C. 4+80	59.30 160.47 F 1.17	0.58 160.47 C 0.11	0.69 160.97 F 0.28	4.46 160.97 C 3.49
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4+60	—	<sup>TR</sup> 161.55 161.25 C 0.30	1.45 161.75 F 0.30	—
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P.V.C. 9+19 <sup>E</sup>	4.77 146.72 F 1.95	6.71 146.72 F 0.91	7.01 147.22 F 0.21	50.60 147.22 C 3.38
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8+89 <sup>E</sup>	5.10 146.95 F 1.85	7.11 146.95 C 0.16	7.34 147.45 F 0.11	50.16 147.45 C 2.71
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E.V.C. 8+59 <sup>E</sup>	5.15 147.18 F 2.03	<sup>TR</sup> 147.40 147.18 C 0.22	7.50 147.68 F 0.18	9.75 147.68 C 2.07
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8+39 <sup>E</sup>	—	7.48 147.37 C 0.11	7.54 147.87 F 0.33	—
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8+19 <sup>E</sup>	6.17 147.66 F 1.49	7.71 147.66 C 0.05	8.07 148.16 F 0.09	9.26 148.16 C 1.10
-------------------	--------------------------	--------------------------	--------------------------	--------------------------

7+99 <sup>E</sup>	—	8.20 148.03 C 0.20	8.27 148.53 F 0.26	—
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7+79 <sup>E</sup> X	7.05 148.49 F 1.44	8.68 148.49 C 0.19	8.67 148.99 F 0.32	50.20 148.99 C 1.21
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7+59 <sup>E</sup>	—	8.95 149.03 F 0.08	9.28 149.53 F 0.25	—
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7+39 <sup>E</sup>	8.46 149.66 F 1.20	9.62 149.66 F 0.04	0.32 150.16 C 0.16	1.57 150.16 C 1.41
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Van Nuys  
 Rough cb. cb. Rough

10+91<sup>E</sup> = B.C.  
 2.76 1.60 9.00  
 141.50 141.50 142.40 142.40  
 C-1.26 C 0.10 C-6.60

10+79<sup>E</sup>  
 3.03 2.25 2.78 9.75  
 142.10 142.10 142.60 142.60  
 C 0.93 C 0.15 C 0.18 C-7.15

10+59<sup>E</sup>  
 — 3.41 3.31 —  
 143.05 143.55  
 C 0.36 F 0.24

10+39<sup>E</sup>  
 4.05 4.01 4.24 50.47  
 143.89 143.89 144.39 144.39  
 C 0.16 C 0.12 F 0.15 C-6.08

10+19<sup>E</sup>  
 — 4.58 4.66 —  
 144.62 145.12  
 F 0.04 F 0.46

9+99<sup>E</sup>  
 4.98 5.05 5.39 51.17  
 145.26 145.26 145.76 145.76  
 F 0.28 F 0.21 F 0.37 C-5.41

9+79<sup>E</sup>  
 — 5.51 5.95 —  
 145.78 146.28  
 F 0.27 F 0.33

9+59<sup>E</sup>  
 4.92 6.10 6.60 50.68  
 146.20 146.20 146.70 146.70  
 F 1.32 F 0.10 F 0.10 C 3.78

9+39<sup>E</sup>  
 — 6.48 46.80<sup>T.P.</sup> —  
 146.51 147.01  
 F 0.03 F 0.21

VAN Nuys 57  
 Rough cb. cb. Rough

1+50  
 4.19 40.50  
 135.15 F 0.12 F 0.54 135.65  
 F 0.96 C-4.85

T.P. 13622

1+00  
 35.79 41.61  
 137.06 F 0.10 F 0.20 137.56  
 F 1.27 C-4.05

0+50  
 8.38 43.85  
 138.98 C 0.14 C 0.02 139.48  
 F 0.60 C-4.37

Bk.  
 0+38  
 8.52 9.39 9.77 43.95  
 139.43 139.43 139.93 139.93  
 F 0.91 F 0.04 F 0.16 C-4.02

0+28 = F.C.  
 8.65 43.93  
 139.68 140.45  
 F 1.03 C-3.48

Mesa Dr.  
 Wly, La Jolla  
 0+00

La Jolla Mesa Dr.

Ely La Jolla Mesa Dr.  
 11+19.52



INDEXED

MAR 25 1953  
Van Nuys  
West end  
4+798

4+748  
2' Rad. End  
cl. at alley

cl. Rough  
3.84  
122.90  
C 0.14  
C 1.26  
123.00  
4.71  
123.07  
C 3.26  
C 1.64

4+772 on Rt.

4+67.8 B.C.

2.93  
123.15  
F 0.22

on 171 Rad Hub.

4+70  
~~4+548~~

F 0.16

4+46.8

3.03  
123.77  
F 0.74

6.83  
124.27  
C 2.56

4+00

5.30  
125.57  
F 0.27

C 0.53

C 0.06

29.12  
126.07  
C 3.05

3+50

7.15  
127.49  
F 0.34

C 0.27

C 0.30

31.57  
127.99  
C 3.58

T.R. 127.17

3+00

8.71  
129.40  
F 0.69

Grade

C 0.20

33.63  
129.90  
C 3.73

2+50

30.00  
131.32  
F 1.32

C 0.50

C 0.02

5.08  
131.82  
C 3.26

2+00

31.00  
133.23  
F 2.23

C 0.24

F 0.55

5.88  
133.73  
C 2.15

INDEXED

MAR 25 1953  
AGATE St.

58

Rough cl. cl. Rough  
3.90 5.12 5.75 7.62  
155.18 155.18 155.68 155.68  
F 1.29 F 0.06 C 0.07 C 1.94

2+79

2+59

2+19

1+79

1+39

0+99

0+59

E.C.

0+08

Wly Dawes

0+00

Dawes

3.91 4.95 5.60 7.47  
155.10 155.10 155.60 155.60  
F 1.19 F 0.15 X C 1.87

3.70 5.20 5.38 7.25  
154.86 154.86 155.36 155.36  
F 1.16 C 0.34 C 0.02 C 1.89

3.66 4.39 4.98 6.81  
154.44 154.44 154.94 154.94  
F 0.78 F 0.05 C 0.04 C 1.87

2.99 3.27 4.62 6.77  
153.86 153.86 154.36 154.36  
F 0.87 F 0.59 C 0.26 C 2.41

2.19 3.45 3.85 6.39  
153.12 153.12 153.62 153.62  
F 0.93 C 0.33 C 0.23 C 2.77

50.44 2.51 3.08 5.30  
152.20 152.20 152.70 152.70  
F 1.76 C 0.31 C 0.38 C 2.60

4.03 1.75 4.42  
150.90 150.90 151.40 151.40  
F 0.87 C 0.35 C 3.02



AGATE

	Rough	cb.	cb.	Rough
Cass. St.				
Ely Cass 4+99				
4+89 B.C.	2.68 153.38 F 0.70	3.87 153.38 C 0.49	3.99 153.88 C 0.11	7.10 153.88 C 3.28
4+79	2.84 <del>153.58</del> F 0.74	4.00 153.58 C 0.42	4.23 154.08 C 0.15	7.40 <del>154.08</del> C 3.32
4+39	3.27 154.28 F 1.01	4.75 154.28 C 0.47	4.95 154.78 C 0.17	7.71 154.78 C 2.93
3+99	3.95 154.80 F 0.85	5.25 154.80 C 0.45	5.53 155.30 C 0.23	8.45 155.30 C 3.15
3+59	3.92 155.12 F 1.20	5.40 155.12 C 0.28	5.82 155.62 C 0.20	8.13 155.62 C 2.51
3+19	4.14 155.24 F 1.10	5.31 155.24 C 0.07	5.92 155.74 C 0.18	7.78 155.74 C 2.04

5150  
1471847R

AGATE

	Rough	cb.	cb.	Rough
3+00	2.62 142.39 C 0.23	C 0.45	C 0.04	3.80 142.89 C 0.91
2+52 ONLY 2+50 ONLY	4.74 144.04 C 0.70	C 0.75	C 0.12	6.72 144.54 C 2.18
2+00	6.26 145.70 C 0.56	C 0.80	C 0.21	7.80 146.20 C 1.60
1+50	7.66 147.35 C 0.31	C 0.78	C 0.28	50.87 147.85 C 3.02
1+00	9.30 149.01 C 0.29	C 0.50	F 0.04	52.50 149.51 C 2.99
0+50	49.94 150.66 F 0.72	grade	F 0.23	3.61 151.16 C 2.45
E.C. 0+10	50.84 152.00 F 1.16	1.78	2.18 152.50 F 0.31	4.29 152.50 C 1.79
Cass Wty 0+00				

766 59



Agate

AGATE

	Rough	Cl.	Cl.	Rough
P.V.C. 7+29	8.25 128.19 C 0.06	8.58 128.19 C 0.39	8.97 128.69 C 0.28	30.63 128.69 C 1.94
7+00	8.65 9.78 129.15 C 0.62 F 0.50	C 0.33	C 0.26	31.58 129.65 C 1.93
6+50	27.75 27.75 130.80 F 3.05	F 0.15	F 0.06	32.65 131.30 C 1.35
6+00	28.73 132.46 F 3.73	F 0.18	C 0.40	31.00 132.96 F 1.96
5+50	30.96 134.11 F 3.15	C 0.10	C 0.13	27.85 134.61 F 6.76
5+00	3.54 135.77 F 2.23	C 0.05	F 0.13	29.86 136.27 F 6.41
4+50	4.26 137.42 F 3.16	C 0.09	F 0.23	7.20 137.92 F 0.72
4+00	7.18 139.08 F 1.90	F 0.10	F 0.24	9.26 139.58 F 0.32
3+50	0.31 140.73 F 0.42	C 0.31	C 0.12	2.50 141.23 C 1.27

	Rough	Cl.	Cl.	Rough
9+57 <sup>8</sup>	9.84 119.36			21.44 119.86
9+50	C 0.48	C 0.18	F 0.97	C 1.58
9+13 <sup>4</sup>	1.68 121.18 C 0.50			3.38 121.68 C 1.70
(5+44.4) 9+00		F 0.03	F 0.33	
E.V.C. 8+69	4.57 123.00 C 1.57	3.24 123.00 C 0.24	3.42 123.50 F 0.08	6.50 123.50 C 3.00
8+49	4.74 123.81 C 0.93	4.19 123.81 C 0.38	4.25 124.31 F 0.11	6.74 124.31 C 2.43
8+29	4.78 124.60 C 0.38	4.93 124.60 C 0.33	4.89 125.10 F 0.22	8.20 125.10 C 3.10
8+09	6.54 125.36 C 1.18	5.58 125.36 C 0.22	5.49 125.86 F 0.37	8.45 125.86 C 2.59
7+89	6.66 126.10 C 0.56	5.28 126.10 C 0.18	6.65 126.60 C 0.05	8.60 126.60 C 2.00
7+69	6.66 126.82 F 0.16	7.09 126.82 C 0.27	7.44 127.32 C 0.12	30.10 127.32 C 2.78
7+49	7.50 127.52 F 0.02	7.91 127.52 C 0.39	8.11 128.02 C 0.07	30.63 128.02 C 2.61



114-86

AGATE

Rough    el.    el.    Rough

0+50  
 1.40  
 111.45    Co.17  
 F0.05  
 3.22  
 111.95  
 C 1.27

See  
 p. 79

E.C.  
 0+28  
 1.97  
 112.14    2.26  
 F 0.17    Co.12  
 2.01  
 112.64    3.78  
 F 0.63    Co.14

= 0400  
 wly. line

La Jolla  
 Mesa Dr.

Mesa Dr.  
 Ely. La Jolla  
 11+19

B.C. on Lt.  
 11+04  
 5.16  
 5.28  
 113.37    4.05  
 C 1.91    Co.68

B.C. on Rt.  
 10+91  
 113.90    Co.76  
 +50    Co.58

10+46E  
 6.98  
 115.72    9.41  
 C-1.26    116.22  
 C 3.19

10+02E  
 8.10  
 117.54    20.85  
 Co.56    118.04  
 10+00    Co.1A    F0.20    C 2.81

Agate  
 End of

A+80 = wly  
 Alley.

B.C.  
 A+58

A+50

A+00

3+50

3+00

2+50

2+00

1+50

1+00

AGATE  
 Rough    el.    el.    Rough

on Rad.  
 8.69  
 98.69    8.82  
 98.69    Co.13    99.19

8.70  
 98.74    Co.15  
 F0.20

M.  
 135  
 100.50    Co.25  
 C 0.85

2.21  
 102.07    Co.35  
 Co.14

3.26  
 103.63    Co.06  
 F0.37

5.09  
 105.20    Co.10  
 F0.11

6.45  
 106.76    Co.15  
 F0.31

8.07  
 108.33    Co.15  
 F0.26

7.73  
 109.89    Co.21  
 F0.16

G1  
 Rough

on Rad.  
 100.80  
 99.19  
 C 1.61

101.26  
 99.44  
 C 1.82

3.30  
 101.00  
 C 2.30

4.65  
 102.57  
 C 2.08

6.19  
 104.13  
 C 2.06

7.54  
 105.70  
 C 1.84

9.94  
 107.26  
 C 2.68

11.31 x  
 108.83  
 C 2.48

2.00  
 110.39  
 C 1.61

see page 79

3.13%



Bl. BC. on rd  
3 + 2.46

DAWES  
Rough

Bl.

Rough  
9.61  
149.71

Archer,  
sly. Vine  
2+65

Rough

Bl.

Bl.

Rough

62

B.C. on Lt.  
2+99

50.16  
149.24  
C 0.92

FO.10

B.C.  
2+52

4.36  
163.01

2.54  
162.51

2+60

9.33  
147.85  
C-1.48

FO.03

FO.24

8.50  
147.71  
C 0.79

2+40

4.00  
162.50  
C 1.50

2.26  
162.02  
C 0.24

2+20

7.95  
146.33  
C-1.62

CO.17

CO.08

7.24  
146.19  
C-1.05

2+30

2.36  
160.75  
C 1.61

CO.08

FO.03

59.69  
160.35  
FO.66

1+80

6.91  
144.81  
C 2.10

CO.25

CO.30

5.91  
144.67  
C 1.24

1+90

CO.33  
159.00  
C 1.33

CO.07

CO.15

8.53  
158.68  
FO.15

1+42

Ally. of  
B.C.

5.53  
143.24  
C 2.29

CO.41

CO.18

4.32  
143.25  
C 1.14

1+44

7.98  
157.25  
C 0.73

FO.15

CO.5A

6.95  
157.01  
FO.06

1+21

~~CO.18~~

Bl. Sta. 1+21  
1+20

1+00

4.36  
141.86  
C-2.50

FO.19

FO.14

3.16  
141.87  
C 1.29

0+80

7.00  
155.50  
C 1.50

FO.03

CO.27

5.10  
155.34  
FO.24

0+60

2.21  
140.48  
C-1.73

CO.02

CO.02

2.14  
140.48  
C 1.66

0+40

5.20  
153.75  
C 1.45

CO.15

CO.45

4.17  
153.67  
C 0.50

E.C.

0+175

0.98  
139.01  
1.97

40.72  
138.91  
C 1.81

E.C. on Lt.

0+08

4.30  
152.35  
C 1.95

0+00

N.Y.

Tyguoise

40.72  
137.00  
C 1.72

0+00 = N.Y.  
line Agate

0-065

B.C. on rd

2.44  
151.50  
C 0.94

2.73  
151.21

C 1.52

Grade  
only

INDEXED  
MAR 25 1953



ARCHER.

Water Services

Service Pipe Lt. or Rt. of L	Lt.	Rt.
Service Pipe 41.75	7.56	—
3+30	168.19	—
	F 0.63	—
1+80	70.01	—
	168.01	—
	C 2.00	—
1+30	71.16	—
	167.70	—
	C 3.46	—
0+80	71.45	—
	166.97	—
	C 4.48	—
0+30	7.45	—
	165.45	—
	C 3.70	—
Wly Dawos 0+00 =		—
Ely. Dawos 2+60	7.05	—
	164.55	—
	C 2.50	—
0+60	4.30	—
	173.44	—
	C 0.86	—
0+158	8.25	—
	175.55	—
	C 2.70	—
0+00		—
Ely end Monte Villa Tract.		—

Risers - 232 off L

Archer

Water Services

63

Lt.	Rt.
6+89	8.95
	138.00
	C 0.95
6+74	8.10
	137.98
	C 0.12
6+49	140.19 <sup>TIP</sup>
	139.27
	C 0.92
6+09	1.14
	140.53
	C 0.61
3+99	TIP 147.30
	146.63
	C 0.67
3+64	49.20
	148.23
	C 0.97
2+80	43.28
	150.48
	F 7.20
2+20	3.60
	153.47
	C 0.13
1+20 RT	8.40
	158.27
	C 0.13
0+00 = wly. line Cass	

INDEXED

MAR 25 1958

RISERS 257 OFF L



Archer st.  
Water Services  
Lt.

VAN NUYS  
Water Services

64

Rt.

Next Page

INDEXED  
MAR 25 1958

2+85  
1+30  
Risers 237 off

5.43  
115.73  
F 0.30

in

0+00 = Wly Cass

Lt. Rt.

3+00 = Fly Cass

2+55

173.93  
173.22  
C 0.71

0+00 = Wly La Jolla Mesa Drive

10+04

7.07  
127.61  
F 0.54

1+95

5.78  
175.62

1+80

72.74  
175.80  
C 2.06

1+45

7.28  
177.62  
F 0.34

9+49

28.68  
129.34  
F 0.66

1+30

5.16  
177.80  
F 2.64

8+84

30.07  
131.38  
F 1.31

change  
to 0+44  
0+45

9.30  
181.72  
F 2.42

7+39

5.83  
135.94  
F 0.11

0+00 =

Ely line Monte Villa Tract.

**NOTE**  
Stake Riser  
337 off & to  
keep box in  
street + out  
of walk



Van Nuys  
Water Services

6+89

Lt. RT.  
3.07  
152.14  
C 0.93

5+39

159.67  
158.47  
C 1.20

4+39

162.55 in place

3+49

Risers 23.7 off

F 162.82  
163.54  
0.72

3+29

168.96  
164.21  
C 2.75

2+80

166.40  
164.59  
C 1.81

2+30

165.74  
164.97  
C 0.77

0+65

70.05  
167.95  
C 2.10

0+20

9.09  
168.50  
C 0.59

0+00 = Wly line Cass

Van Nuys  
Water Services

Lt. RT.

4+79 = Wly Alley. + End of Van Nuys

3+94  
3+90

Risers 22.7 off

6.42  
125.80  
C 0.62

3+45

128.17 IN

0+00 = Wly. La Jolla Mesa Dr.

11+194 = Ely La Jolla Mesa Dr.

8+39

Lt. RT.  
146.31  
147.37  
F 1.06



AGATE ST.  
Water Services

Risers  
1975 off £

	Lt.	RT.	
4+99	2.52 135.82 F 0.30	—	
3+49	0.30 140.78 F 0.48	—	
3+05	2.57 142.24 C 0.33	—	
2+05	6.50 145.55 C-0.97	—	
1+20	—	50.21 148.86 C 1.35	
0+30	—	1.90 151.84 C 0.06	
0+00 = Wly line Cass			
5+00 = Ely line Cass			
3+70	—	155.56	2 Meters IN
0+00 = Wly line Dawes			

Agate ST  
Water Services

66

INDEXED

11+19 = Ely La Tolla Mesa Dr.

	Lt.	RT.	
10+49	7.25 115.62 C 1.63	—	
9+49	120.78 = T.P. 119.72 C-1.06	—	
8+99	2.68 121.77 C 0.91	—	
7+24	128.98 <sup>T.P.</sup> 128.39 C 0.59	—	
6+74	31.44 130.04 C-1.40	—	
6+24	28.29 131.69 F 3.40	—	
5+64	0.82 133.67 F 2.85	—	
5+34	31.85 134.66 F-2.81	—	

MAR 25 1953

Risers 1975 off £



AGATE ST.  
Water Services

10-17-52 67  
Curb Inlet & Culvert # 2. (9145-L)

West end of Van Nuys  
Stakes 8' back of cb

End of pipe		Top of cb	I.E. Pipe	
4+81.8				21.64
				112.70
				C-8.94
		Restake 10-20-52		
West end. curb inlet	23.03	<del>22.91</del>	<del>22.91</del>	23.03
4+62.8	123.15	<del>122.15</del>	<del>116.50</del>	116.50
	F 0.12	<del>F 9.24</del>	<del>C 6.41</del>	C-6.53
Ely. end of Inlet	3.65	<del>3.36</del>		
4+51.8	123.57	<del>123.57</del>		
	C 0.08	<del>F 9.21</del>		

Restake 10/20/52  
curb stakes 6' back

Culvert #1 + cb. Inlet

West end Archer (9142-L)

4+62.9	<del>12.80</del>	10.90
West end of cb. Inlet	<del>110.50</del>	110.50
	C 9.30	C 0.40
4+51.9	<del>11.35</del>	11.33
East end of cb. Inlet	<del>110.82</del>	110.82
	C-0.53	C 0.51

Stakes 5' Ely of #

Culvert - 4 parts

N. Face box	0+18	0+36	0+54	0+72
0+00	#19	#2	#3 (1/2)	#4 = stub end
B.C.				
11.45	11.35	11.51	11.85	10.94
104.25	104.07	103.88	103.69	103.50
C 7.20	C-7.28	C 7.63	C 8.16	C 7.44

4+80 = Alloy - west end Agate

Lt. Rt.

3+45

3.19  
102.22  
C-0.97

1+95

7.38  
106.92  
C 0.46

1+30

9.42  
108.95  
C 0.47

0+00 = Wly. line La Tolla Mesa Drive

Rise 19.75 off #



Van Nuys - Rough  
East of Cass Grade

Continued - P 55

2+92 cl.B.C. Rt

79.97  
171.82  
C-8.15

2+90 cl.B.C. Lt. 9.90  
171.40  
F 1.50

2+50 70.10  
172.98  
F 2.88

2+00 1.25  
174.98  
F 3.73

1+50 3.92  
176.98  
F 3.06

TR. 12437

1+00 6.58  
178.98  
F 2.40

0+50 80.24  
180.98  
F 0.74

300' East of Cass 91.04  
Ely End Oak 182.98  
0+00 C-8.06

3.80  
183.48  
C 0.32

Curb Returns

Van Nuys + La Jolla Mesa Dr.

INDEXED

68

MAR 25 1953

#3 N.Wly. Ret.

#1 Prop.

#1

B.C.

Van Nuys

0.26  
140.45  
F 0.17

0.64  
141.12  
F 0.48

1.11  
141.81  
F 0.70

1.57  
142.70  
F 0.91

3.57  
142.50  
C 1.07

#3 S.Wly Ret.

9.66  
139.68  
F 0.02

9.59  
139.65  
F 0.06

9.63  
139.40  
C 0.23

8.81  
138.91  
F 0.10

#1 Prop.

B.C.

La Jolla Mesa Dr.

E.C.

#3 Prop.

N.Ely. Ret.

#1

B.C.

3.47  
143.05  
C 0.42

2.37  
142.50  
F 0.13

2.23  
142.35  
F 0.12

2.54  
142.40  
C 0.14

La Jolla Mesa Drive

E.C.

#3 Prop.

S.Ely. Ret.

#1

B.C.

42.66  
139.50  
C 3.16

0.34  
140.20  
C 0.14

0.92  
140.85  
C 0.07

1.60  
141.50  
C 0.19

X on wall 150' back

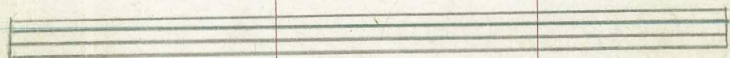
Van Nuys



Curb Returns  
Van Nuys + Cass.

INDEXED  
MAR 25 1953

Van Nuys	Van Nuys	Van Nuys	Van Nuys	Van Nuys	Van Nuys
9.26 168.75 C 0.51	9.42 169.30 C 0.12	9.35 169.04 C 0.31	9.88 169.95 F 0.07	9.53 171.25 F 0.72	7.08 173.05 F 1.97
#A E.C.	#1 E.C. = 0108	#2 S.Wly. Ret	#3 N.Wly. Van Nuys + Cass	#4 N.Wly. Van Nuys + Cass	#5 P.L. MAR 25 1953
169.27 F 0.27	169.11 F 0.11	169.27 F 0.27	169.95 F 0.07	171.25 F 0.72	173.05 F 1.97



Cass St.	Cass St.	Cass St.	Cass St.	Cass St.	Cass St.
9.08 170.15 F 1.07	9.30 173.50 F 1.20	9.84 170.52 F 0.68	9.58 172.25 F 0.67	1.73 171.75 F 0.02	1.70 171.70 F 0.00
#3 S. Ely. Ret.	#4 N. Ely. Ret.	#2 S. Ely. Ret.	#1 S. Ely. Ret.	#1 S. Ely. Ret.	#1 S. Ely. Ret.
170.15 F 1.07	173.50 F 1.20	170.52 F 0.68	172.25 F 0.67	171.75 F 0.02	171.70 F 0.00

Cass - St.  
Van Nuys

Curb. Ret. 69  
Alley west of La Jolla Mesa Dr.  
& Van Nuys

Alley	Alley	Alley	Alley	Alley	Alley
2.52 122.70 C 0.81	2.57 122.40 C 0.11	3.15 123.15 F 0.01	13.55 13.55 C 0.11	13.55 13.55 C 0.11	13.55 13.55 C 0.11
E.C. = End of C.C.	S.E. Ret. Mid. Curb.	B.O. = Sta. A + 62.8	13.55	13.55	13.55
122.70 C 0.81	122.40 C 0.11	123.15 F 0.01	13.55 13.55	13.55 13.55	13.55 13.55

ARCHER ST  
+ DAWES  
INDEXED  
MAR 25 1953

Dawes	Dawes	Dawes	Dawes	Dawes	Dawes
2.50 162.51 F 0.01	2.92 162.85 C 0.07	3.36 163.15 C 0.21	3.92 163.45 C 0.47	4.98 163.75 C 1.23	4.98 163.75 C 1.23
#5 E.C.	#4 S. Ely. Ret.	#3 S. Ely. Ret.	#2 S. Ely. Ret.	#1 S. Ely. Ret.	#1 S. Ely. Ret.
162.51 F 0.01	162.85 C 0.07	163.15 C 0.21	163.45 C 0.47	163.75 C 1.23	163.75 C 1.23

Archer	Archer	Archer	Archer	Archer	Archer
4.89 164.64 C 0.25	4.62 164.28 C 0.34	4.00 163.90 C 0.10	3.25 163.47 F 0.22	2.70 163.01 F 0.31	2.70 163.01 F 0.31
#4 E.C.	#4 S.Wly. Ret.	#3 S.Wly. Ret.	#2 S.Wly. Ret.	#1 S.Wly. Ret.	#1 S.Wly. Ret.
164.64 C 0.25	164.28 C 0.34	163.90 C 0.10	163.47 F 0.22	163.01 F 0.31	163.01 F 0.31

Archer  
Dawes



Curb Returns  
Archer + Cass

ARCHER ST.	3.83 163.57 C 0.26	#4 E.C.	10:20	N.W. Ret.	10:41	#1 Cross	B.C.
	4.16 164.06 C 0.10	#4					
	5.21 164.55 C 0.66	#4					
	5.68 164.97 C 0.71	#1					
ARCHER ST.	3.17 163.07 C 0.10	#4 E.C.		S.W. Ret.			B.C.
	3.46 163.43 C 0.09	#4					
	3.45 163.55 F 0.13	#2					
	3.28 163.55 F 0.27	#1					
ARCHER ST.	7.45 165.67 C 1.78	#4		N.E. Ret.			B.C.
	6.67 165.62 C 1.05	#2					
	5.85 165.74 C 0.11	#2					
	6.05 166.00 C 0.05	#1					

ARCHER ST.

CASS ST.

INDEXED

ARCHER + L. J. Mesa Drive  
Curb Returns

ARCHER	3.57 123.78 F 0.11	#4 E.C.	11:22	S.W. Ret.	11:23	#3	
	3.43 123.48 F 0.05	#3					
	3.47 123.39 C 0.10	#2					
	3.25 123.04 C 0.21	#1					
ARCHER	8.19 124.87 F 0.71	#3		N.W. Ret.			B.C.
	6.65 125.50 C 1.15	#2					
	5.37 165.50 F 0.16	#1					
	5.37 165.50 F 0.16	#1					
ARCHER	3.83 163.57 C 0.26	#4 E.C.	10:41	N.E. Ret.	10:41	#3	
	4.95 125.75 F 0.80	#2					
	4.90 125.52 F 0.62	#2					
	5.16 125.47 F 0.31	#1					
ARCHER	3.17 163.07 C 0.10	#4 E.C.	10:47	S.E. Ret.	10:47	#3	
	3.85 124.02 F 0.17	#3					
	4.55 124.43 C 0.12	#2					
	4.90 124.86 C 0.104	#1					

La Jolla Mesa Drive

ARCHER ST.

Cross  
in  
walk

Tanwalk

B.C.

La Jolla Mesa Drive



Curb Returns

Archer + Alley at wly. end  
Archer

INDEXED  
MAR 20 1953

Alley -  
Mail 2' outside  
Face. cbr. ac  
#2 E.C.  
9.11  
109.71  
F 0.60

N. Fly. Ret.  
1.71  
110.87  
C 0.84

S Fly Ret.  
9.82  
110.11  
F 0.29

Archer  
0.18  
110.50  
F 0.22

Mid  
Curb  
0.10  
110.72  
F 0.02

BC.  
0.41  
111.06  
F 0.59

DAWES + TURQUOISE

INDEXED  
MAR 25 1953

Dawes  
#2 E.C.  
9.06  
138.91  
C 0.15

N. Fly. Ret.  
8.78  
138.59  
C 0.19

N. Fly. Ret.  
138.32

Turquoise  
EXIST  
OC.  
138.43

INDEXED

Curb Returns

MAR 25 1953

DAWES + AGATE

151.50 - Prop.  
2.15  
151.21 #4  
C 0.94

Dawes.  
BC 2.55  
152.35  
C 0.31

N. Fly. Ret.  
2.18  
151.93  
C 0.25

N. Fly. Ret.  
1.67  
151.60  
C 0.07

N. Fly. Ret.  
1.40  
151.40  
9 grade

N. Fly. Ret.  
1.51  
151.33  
5. Face

N. Fly. Ret.  
1.75  
151.40  
C 0.35

Agate  
150.80  
150.75 #4  
Meat d.

0.26 #3  
150.44  
F 0.18

9.88 #2  
150.10  
F 0.22

9.55 #1  
149.71  
F 0.16

Agate  
PL.  
#1  
150.90 E.C.  
C 0.61

1.12  
150.67  
C 0.45

0.42  
150.34  
C 0.08

9.93  
149.99  
F 0.06

0.16  
149.61 #2  
C 0.55

8.98  
149.24  
F 0.26

Dawes St.



Gas Co Vault  
Dawes - + Alloy BIK. #11

Dawes	45	8.55 7.75 CO.80	8.47 7.84 CO.63
Alloy		7.61 7.09 CO.52	7.81 7.17 CO.64
Wily. Liro			

INDEXED  
MAR 25 1953

Cb. Returns  
Cass + Agate

Cass St. E.C.	#5	2.46 152.00 CO.46	2.94 152.43 CO.51	#3	S. Ely. Ret.	#2	#1	B.C.	Agate
	#4	3.33 152.82 CO.51	3.77 153.89 FO.12						
	#1	3.74 153.11 CO.63	3.86 153.80 CO.06						
	#4	3.87 153.38 CO.49	3.99 153.88 CO.11						
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Agate St. E.G. P1/4

S.Wly. Ret. E.C.

N.Wly. Ret

La Jolla Mesa Dr.

#5	2.26 112.14 C 0.12	12.01 112.64 F 0.63
#4	2.13 112.30 F 0.17	2.30 #1 112.96 F 0.66
#3	2.30 112.28 C 0.02	2.50 #2 113.28 F 0.78
#2	2.46 112.10 C 0.30	2.80 #3 113.61 F 0.75
#1	2.30 111.83 C 0.47	3.49 #4 113.93 F 0.44

La Jolla Mesa Dr. E.G. P1/4

S.Ely Ret. #1

N.Ely. Ret #2

Agate + La Jolla Mesa Dr. Curb. Returns

3.69 112.33 C 1.36	3.85 #4 112.47 C 1.37	13.59 #4 114.49 F 0.90
4.14 112.68 C 1.45	3.59 #3 114.28 F 0.69	3.67 #2 114.15 F 0.48
4.02 #2 112.90 C 1.12	3.99 #1 114.18 F 0.19	3.99 #1 114.18 F 0.19
4.05 113.37 C 0.68	4.20 114.20 C 0.21	4.20 114.20 C 0.21

La Jolla Mesa Dr.

AGATE

INDEXED  
MAR 25 1953

Agate + Alley on West end 73  
Cb. Returns

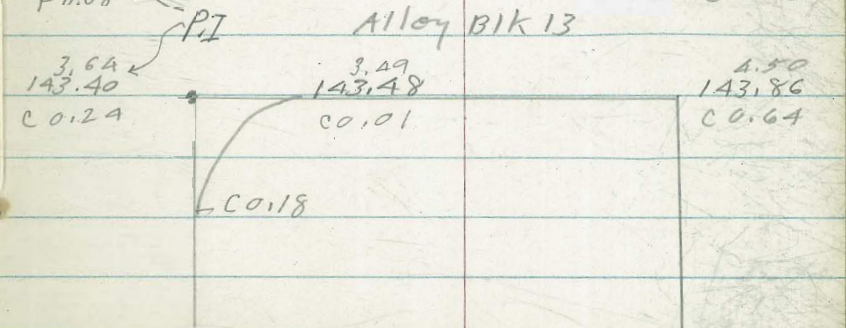
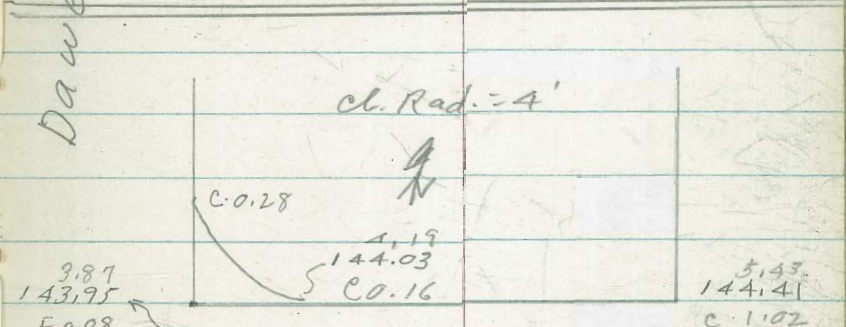
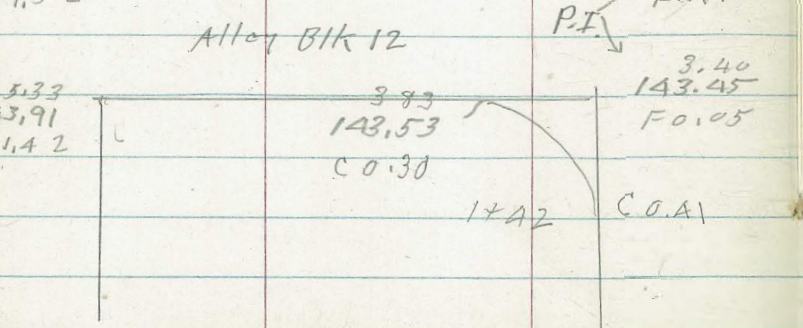
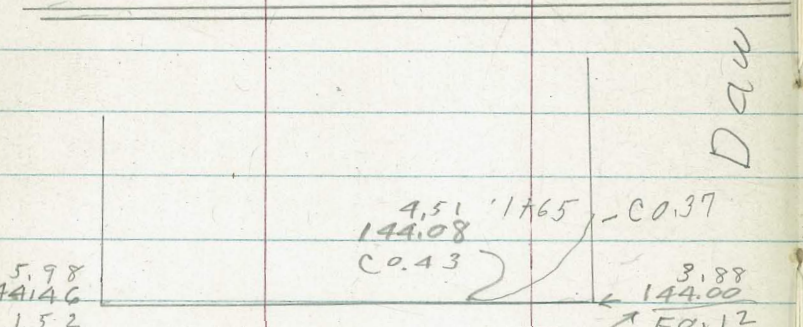
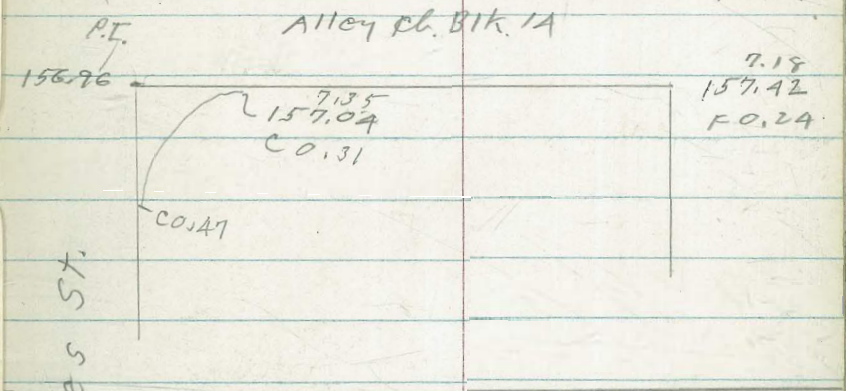
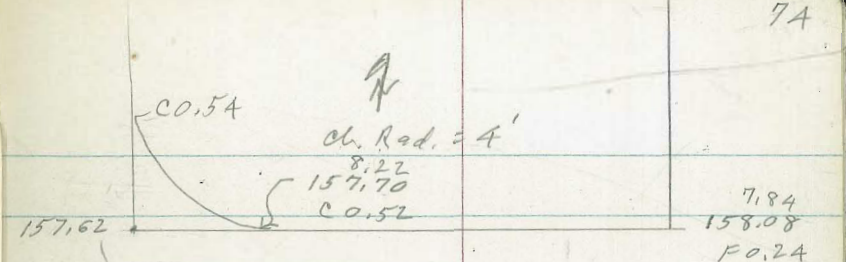
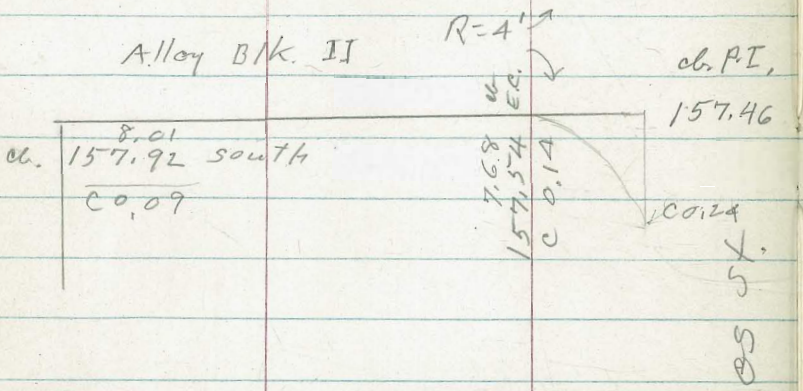
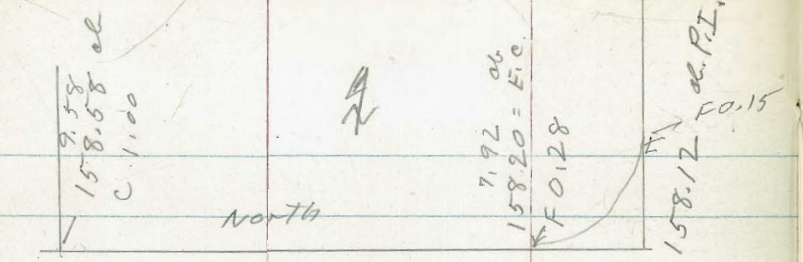
Alley

N.Ely Ret.

#4 E.C. 7.64 97.80 F 0.16	#3 8.25 97.98 C 0.27	#2 8.38 98.19 C 0.19	#1 8.65 98.43 C 0.22
100.21 #4 99.24 C 0.97	8.97 #3 99.00 F 0.03	8.77 #2 98.90 F 0.13	8.96 #1 99.00 F 0.04
8.82 98.69 C 0.13	9.11 99.19 F 0.08	9.11 99.19 F 0.08	9.11 99.19 F 0.08

AGATE





Dawes St.

7.84  
158.08  
C 0.24

7.18  
157.42  
C 0.24

5.45  
144.41  
C 1.02

4.50  
143.86  
C 0.64



INDEXED

MAR 25 1953

La Palma Curbs  
Stakes 3' back

Sheet 9511-L

1-30-53

NO 32025

South

North

2+00	7.30 17.44 FO.14	8.28 8.24 CO.04
1+80	7.92 17.98 FO.06	8.95 8.77 CO.18
1+60	8.78 18.66 CO.12	7.51 7.43 CO.08
1+40	10.41 9.47 CO.64	10.25 10.23 CO.02
1+20	1.40 10.42 CO.98	1.37 11.16 CO.21
1+00 P.V.C.	2.11 11.51 CO.60	2.54 12.22 CO.32
0+50	4.92 14.38 CO.54	5.00 15.05 CO.01
w/ly Grestom 0+00	17.26 ✓	17.88 ✓

B.M. = NE 7' L + T. La Palma  
+ Fomuel - EL. = 6.97.

75

South

North

Ely. Fomuel 5+00	5.72 ✓	6.70 ✓
A+60	6.00 5.87 CO.13	6.83 <del>6.88</del> 6.83 <del>C X 5</del>
A+20	6.20 6.02 CO.18	6.95 <del>7.00</del> 6.95 <del>C X 5</del>
3+80	6.11 6.17 FO.06	7.00 <del>7.05</del> 7.08 FO.08
3+40	5.90 6.32 FO.42	7.06 7.20 FO.14
3+00 Nail 117 pole	7.83 6.47 C 1.36	7.00 7.33 FO.33
2+60 E.V.C.	6.61 6.61 +	7.20 <del>7.26</del> 7.45 FO.25
2+40	6.96 6.76 CO.20	7.50 7.58 FO.08
2+20	7.12 7.03 CO.09	7.81 <del>7.84</del> 7.84 FO.03



La Jolla Mesa Dr. + Linda Rosa,

76

Storm Drain

C.H.S.  
Boyer  
oltman

2-25-53  
W.O. 20977

Sheet 4704 B,

Stakes - 10' Rt. of  $\neq$

INDEXED

MAR 25 1953

End. of pipe  
1+32

81.06  
168.20  
C 12.86

0+98

77.23  
166.41  
C 10.82

0+64 Bk

175.96 TP  
164.62  
C 11.34

0+32

9.51  
163.21  
C 6.30

End existing 54"  
0+00

70.03  
161.80  
C-8.23  
out of headwall

1+32

9°-40'



0+00 EL: 161.47

Existing IE

Existing 54"



Sewer Dawes St.

N.I.S. of Reed

Sheet 4789-B.

2-26-53

C.H.S

Begg

Altman

W.O. 62307

East

0+00 = ~~E~~ Alley Blk 2. Produced. to

B.M. = S.E. 7<sup>th</sup> Man. Dawes + Thomas EL = 1484

1+96

9.60

3.87

C 5.73

1+90

9.50

3.71

C 5.79

1+50

8.88

3.43

C 5.45

1+00

0.7%

8.11

3.08

C 5.03

0+50

7.07

2.73

C 4.34

0+00

6.00

2.38

Existing M.H.

C 3.62

Existing M.H.

3+50

12.32

7.34

C 4.98

3+00

11.38

6.21

C 5.17

2+50

2.25%

10.54

5.09

C 5.45

INDEXED

MAR 25 1953



Levels on Existing 6" Sewer

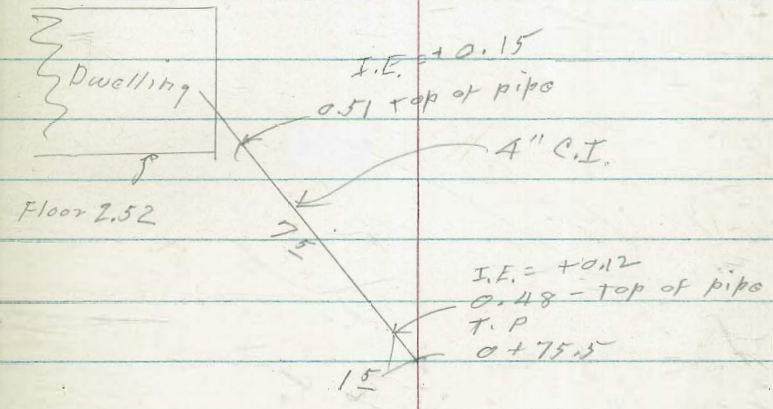
Alley BIK 244 M. B.

INDEXED  
Law  
MAR 25 1953

C.H. Schimmermayer  
Boyg.  
Altman  
Schelin

3-25-53  
W.O. # 31824

	Top of pipe.	I.E. pipe.
1+50	0.78	+0.22
1+25	0.70	+0.14
1+00	0.66	+0.10
0+75 <sup>5</sup>	0.63	+0.05
0+68.7	0.55	-0.01
0+63	0.56	0.00*
0+55	0.54	-0.02
0+28	0.54	-0.02
0+00 = M.H.	0.00 F.L.	1.99 West rim



0+00



N/4 Agate - La Jolla  
Mesa

west

79

= 0428 - page 61  
E.C. = A+30

3+90 F0.63

3+50 F0.47

+15 F0.29

2+80 C0.103

2+45 F0.24

2+10 C0.104

1+75 C0.01

1+40 F0.03

1+05 F0.01

0+70 F0.29

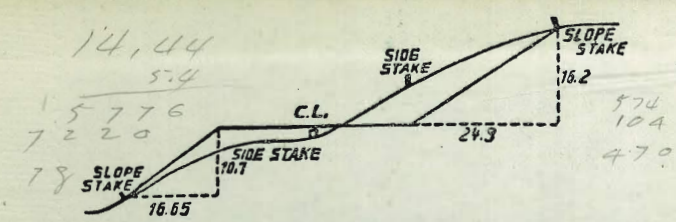
0+35 C0.06

Run by F.O. on this sta  
stationing 0+00 = ely end  
alley return. Agate + west  
end of job.



12.93 -0.27 20.56  
 831 11.65  
 1.28  
 462 11499 18 50 4  
 122.40 18 22 4  
 184  
 12056 1007

45.44  
 108  
 4436 256  
 18  
 10562 19 49  
 30 1026  
 3 56  
 6.5 7.60 100.6  
 4.9 6.14 20.6  
 59.5 4.4 5.4 4.9  
 260 2.34  
 71.85 10 8.24  
 0.48 5.35  
 145.93 8.84  
 137.52 14  
 37  
 146.91



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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