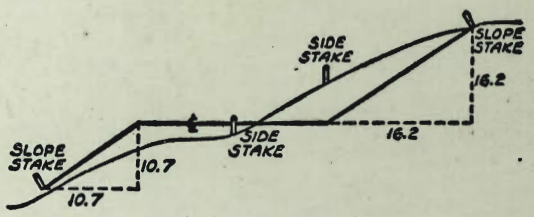
G-301



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

WO #'s in N 301	
31434	p9.8
32064	p9.11
32025	p9.17
[redacted]	p9.38
20839	p9.20
31992	p9.21
21053	p9.27
62283	p9.35
31735	p9.43
32024	p9.44
62316	p9.46

WO#	Bk. N 301
21001	p9.47
31945	p9.50
31795	p9.54
32141	p9.61
31837	p9.62
32210	p9.67
20009	p9.70
32139	p9.72

IMPROVED TABLES
AND
INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. VIII

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

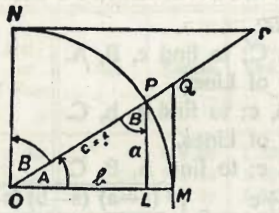


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \text{sos } B = LP$$

$$\text{sos } A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C^1}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

Page

Puterbaugh & T 1-2

Stake Sewer. Ventura Point ✓ 3-7

Stake Juan St & Sunset St Sewer 8-10, 20

Stake Drucker's Sub Sewer 11-16 19

Stake La Palma St Fanuelto Gresham 17-18

Stake Sewer La Dorna St. & Catoctin Dr. @ Montezuma 21-26

Stake Milton St - Mirena to Ilion 27-34

Hill St - Alexanderia Way 35-36

Hurlburt + Afton 37-42

Alley Blk 7 - City Hts Annex #2 43-

Alley Blk 40 Teralta 44-45

Golden Warehouse P1282 Sewer 46

Sewer P1282-283 Sherman Custer St. 47-49

Mead + El Cajon Texas

Alleys "T" Blks 103 & 104 University Hts. 50-53

Stake San Bernardo & La Paz Sts. 54-60

Stake Alley Blk 31 Ocean Beach 61-

Stake Francis St Ocean View to Webster St. 62-66

Stake Keats Sch. & Shafter 67-69

Stake Sewer Archer St. 70-

Stake Sewer 33rd & Nutmeg 71-

Stake Nashville & Lehigh St 72-

C. Allen
D. Smith
R. Taylor
R. Parks

INDEXED
DEC 8 1954

Lt. West

Stake Pringle to Mission

Puterbaugh St Hills Blvd. At = East

WO # 31710
10-8-52

C.

	rough	C6 grade	C6	gutter		gutter	C6	C6 grade	Rough
					℄				
1+50		225.31	5.25 built	224.21	225.66 s-33		225.68		226.43
1+40		226.25		225.85	226.51 6.18		226.45		227.20
1+20		227.40		227.00	227.24 7.41		227.76		228.51
1+00		228.05		227.65	228.51 8.18		228.64		229.39
0+95 (w) Pt									
0+80	27.98 F0.49	228.47	C-0.07 228.49	228.07	228.23 8.60		229.04		229.79
0+60	28.12 F0.48	228.60	F0.14 228.46	228.20	228.29 8.66		229.06		229.81
0+40	27.27 F1.06	228.33	F0.34 227.99	227.93	228.25 8.42		228.85		229.60
0+20	26.81 F0.77	227.59	F.0.27 227.32	227.19	228.24 7.91		228.56		229.31
0+00 My Pringle		226.30	6.29	225.75 exists	227.46 exists		228.17 8.21 exists		229.02
BM			225.29	SW 13' & 27' Puterbaugh & Pringle					

Lt = West

943 ℄ Int cb. ℄ drain (watch) use plan section end con 216.05

		cb grade	
942		217.30	F 0.99 216.31
942		217.57	F 0.85 216.72
943		218.12	F-1.25 216.87
829		218.95	F-1.80 217.15
829		219.82	F 0.43 219.39
PRC.	℄BK cb Face 20.24 F0.45	220.69	F-0.29 220.40
Mid Pt.		221.56	F 0.27 221.29
2709.05 24 Rad ⊙			
30.51 ↓ 1478.48	Turn around BC.	rough 21.25 F1.18	cb grade 222.43

cb	gutter
F 0.16 222.27	222.03

216.55 94t 217.30 cb F 0.75 trcb 216.55

217.44 NE Cor Apron = C 0.08

SE Cor = F 1.09

219.51 918 ℄

℄	gutter
222.77 244	222.28

nt = East

2.

	cb grade	cb ⊏
	217.63	C 0.32 217.95
	218.24	C 0.82 219.06
	219.12	C 1.79 220.91
Nail = 0.5 back	220.05	C 4.50 224.55
	220.22	C 2.93 223.85
SBK cb Face 23.90 ℄ 2.11	⊟ 2' back 221.79	C 1.34 223.13
	222.66	C 0.03 222.69

cb	cb grade	rough
F 0.03 223.50	223.53	

10-28-52 Stake Sanitary Sewer Mission Beach Pump Sta. #14 to Ventura pl
Allen Parks Taylor W.O. # 20479-

	ENIE.	stake - CUT
2+25	-9.32	0.99 - C-10.31
2+00	-9.43	+0.69 - C-10 1/2
1+75	-9.53	+0.23 - C 9.76
1+50	-9.24	+0.15 - C-9.39
1+25	-9.75	12 RT -0.90 - C-8.85
1+00	-9.86	(2' LT +0.74 - C-9.12) RT (-1.53 - C-8.33) LT
0+75	-9.97	12' LT -1.04 - C-8.93
0+50	-10.08	12' LT -0.88 - C-9.10
0+25	-10.19	12' LT -1.0 - C-9.09
MH#1 0+00	ON NOTE C-10.36 -10.30	STAKED 12' LT -1.08 - C-9.22

BM = stub at 0+00 FB. 2173 - P. 11 - EL = -1.51

First 100' staked ON LEFT 12'
Rest staked at 12'

	I.E.EL.	stake 12 RT
		stake
4+50	-8.38	3.62 - C-12.00
4+25	-8.48	3.85 - C 12.33

MH tied out on SPLIT OF L- ON South - ~~S 89° 18' - 120.24 - 24.05~~

MH#2 - L. ~~S 0° 30' E~~ S 0° 53'		
4+00	-8.58	343 C-12.01 ~~3.55 - C - 12.73~~
3+75	-8.67	3.65 - C - 12.32
3+50	-8.78	2.85 - C - 11.63
3+25	-8.89	2.67 - C - 11.56
3+00	-9.0	2.21 - C 11.21
2+75	-9.10	1.77 - C 10.87
2+50	-9.21	1.33 - C 10.54

	I.E. El.	12' Rt Stake
~~11+45~~ +50	~~-5.70~~ -5.68	2.18 - C 78 6
~~11+20~~ +25	~~-5.80~~ -5.78	2.05 - C 78 3
~~10+95~~ 11+00	~~-5.90~~ -5.88	1.97 - 78 5
~~10+70~~ +75	~~-6.00~~ -5.98	1.97 - C 79 5
~~10+45~~ +50	~~-6.10~~ -6.08	2.11 - C 8 1 9
~~10+20~~ +25	~~-6.20~~ -6.18	2.40 - C 8 5 8
~~9+95~~ 10+00	~~-6.30~~ -6.28	2.60 - C 8 8 8
~~9+70~~ +75	~~-6.40~~ -6.38	2.31 - C 8 6 9
~~9+45~~ +50	~~-6.50~~ -6.48	2.27 - C 8 7 5

	I.E. El.	12' Rt Staked
13+70	-4.80	2.02 - C - 6 8 2
13+45	-4.90	1.97 - C - 6.87
13+20	-5.00	2.01 - C - 7 0 1
12+95	-5.10	2.30 - C - 7 4 0
12+70	-5.20	2.36 - C - 7 5 2
12+45	-5.30	2.40 - C - 7 7 0
Tied 12+24 Rt (Sly.) MH # 4 - POT 12+20	-5.40	2.20 - C 7 6 9
~~11+95~~ 12+00	~~-5.60~~ -5.48	- 2.01 - C - 7 4 9
~~11+70~~ +72	~~-5.60~~ -5.58	- 2.20 - C 7 7 8

	I.E. EL.	12' Rt Stake
Tied out 120+24e Rt (WH)		
MH#5 - POT		
18+95	-3.90	1.96 - C 5 86
18+70	-4.00	1.89 - C 5 89
18+45	-4.10	2.01 - C 6 11
18+20	-4.20	2.15 - C 6 35
17+95	-4.30	2.24 - C 6 54
17+70	-4.40	2.20 - C 6 60
17+45	-4.50	2.17 - C 6 67
17+20	-4.60	2.06 - C 6 66
16+95 TP	-4.70	1.98 - C 6 68

	I.E. EL.	12' Rt. Stake
18+45	-2.90	2.75 - C 5 65
18+20	-3.00	2.22 - C 5 22
17+95	-3.10	2.07 - C 5 17
17+70	-3.20	2.25 - C 5 45
17+45	-3.30	2.09 - C 5 39
17+20	-3.40	1.83 - C 5 23
16+95	-3.50	1.85 - C 5 35
16+70	-3.60	1.84 - C 5 41
16+45	-3.70	1.89 - C 5 59
16+20	-3.80	1.89 - C 5 69

	I.E. EL.	12' Rt. Stake
Tied out 12°+24° R.& L.T. (3 Ly).		
MH #6 - EP		
19+65	-2.42	3.06. C5 48
19+45	-2.50	3.34 - C584
19+20	-2.60	3.23 - C583
18+95	-2.70	2.93 - C563
18+70	-2.80	2.75 - C555

D. Smith
C. Allen
R. Taylor
R. Parks

INDEXED
DEC 8 1954

Wo # 31434 8.

11/24/52

Ref Plan FB-2099 81	Grade	Stake Juan St Sewer Stake 8' Lt	Grade 66	Stake 8' Lt on diag 8 42
2+02 47 ahead = S MH #3				
2+11 47 Back L 89°58'30" Lt 29 02	0 23	4 91 C 4 68 on diag 11 42	MH #4 4+98 02 L 36°22' Rt 25 53	- 0 66	4 91 C 5 57
1+82 45	0 32	4 60 C 4 28	4+72 47	- 0 58	5 27 C 5 85
1+52 45	0 41	4 40 C 3 99	4+42 47	- 0 49	5 24 C 5 73
1+22 45	0 50	4 15 C 3 65	4+12 47	- 0 40	5 45 C 5 85
0+92 45 .003 rate	0 59	4 37 C 3 78 4' Lt	3+82 47 .003 rate	- 0 31	5 35 C 5 66
0+62 45	0 68	3 76 C 3 08	3+52 47	- 0 22	5 35 C 5 57
0+32 45	0 77	3 60 C 2 83 4' Lt	3+22 47	- 0 13	5 16 C 5 29
0+02 45 DE 8" plug	0 86	3 85 C 2 99	2+92 47	- 0 04	5 09 C 5 13
0+00			2+62 47	0 05	4 94 C 4 89
BM		BM #2 2099 45 4 54 NW 9X7 Hub Juan + Rosecrans	2+32 47	0 14	4 88 C 4 74

	Grade	Stake 8' Lt.
8+16.02 Make connection existing 8" V.C. sewer 18°	-1.61	4.22 C-5.83
7+98.02	-1.56	4.23 C-5.79
7+68.02	-1.47	3.90 C-5.37
7+38.02	-1.38	3.90 C-5.28
7+08.02	-1.29	3.97 C-5.26
6+78.02	-1.20	4.81 C-6.01
6+48.02 .003 rate	-1.11	5.51 C-6.62
6+18.02	-1.02	6.23 C-7.25
5+88.02	-0.93	5.41 C-6.34
5+58.02	-0.84	left out dog
5+28.02	-0.75	4.81 C-5.56

Sunset St Sewer	Grade	Stake 8' Lt.
seepage 20		
2+65	-0.96	6.50 C-7.46
2+35 .003 rate	-0.87	6.35 C-7.22
2+05	-0.78	5.67 C-6.45
1+75 MH #2 POT =S 2+67.45	-0.69	6.06 C-6.75
1+50	-0.62	5.73 C-6.35
1+20	-0.53	5.72 C-6.25
0+90 .003 rate	-0.44	5.73 C-6.17
0+60	-0.35	5.89 C-6.24
0+30	-0.26	5.75 C-6.01
0+00 =S 0+92.45 8" plug Of sewer	-0.17	5.50 C-5.67
BM	5.77	Q Hub Sunset + Int Gaines FB2099-47-57

Q 1

		Grade	Stake 8' Lt
1+50		-0.09	5.82 C-5.91
1+20		-0.21	5.81 C-6.02
0+90	.00 Grade	-0.33	5.90 C-6.23
0+60		-0.45	5.90 C-6.35
0+30		-0.57	5.94 C-6.51
1+75 = 5 0+00 Gaines	MH #2	-0.69	6.06 C-6.75
3+70	MH #1 Connect 8" VC sewer	-1.28	6.22 C-7.50
3+55		-1.23	6.07 C-7.86
3+25		-1.14	6.50 C-7.64
2+95	.003 Grade	-1.05	6.40 C-7.45

	Grade	Stake 8' Lt
8" Plug 2+55 DE sewer	0.33	6.42 C-6.29
2+40	0.27	6.65 C-6.38
2+10	0.15	6.64 C-6.49
1+80	0.03	6.14 C-6.4

D. Smith
C. Allen
R. Taylor
R Parks

INDEXED
JER
DEC 8 1954

Stake Druckers

Stakes 5' Rt

2+25		-9.01	0.20 / ~~0.22~~	C-9.30 / ~~C-9.12~~
			0.10	C-9.30
2+00		-9.20	~~-0.03~~	~~C-9.47~~
			0.15	~~C-9~~ C-9.45
1+75		~~-9.30~~	~~-0.13~~	~~C-9.17~~
			0.12	C-9.52
1+50		-9.40	~~-0.10~~	~~C-9.30~~
			0.16	C-9.66
1+25		-9.50	-0.13	~~C-9.37~~
			0.00	C-9.60
1+00		-9.60	~~-0.17~~	~~C-9.43~~
			-0.01	C-9.69
0+75	15' E D 0.06	C-9.76	-9.20	~~-0.30~~ ~~C-9.40~~
			-0.17	C-9.63
0+50	15' E 0.09	C-9.89	-9.80	~~-0.32~~ ~~C-9.48~~
			-0.15	C-9.75
0+25	15' E 0.08	C-9.72	-9.90	~~-0.23~~ ~~C-9.67~~
Jupiter St.	142 E			
0+06 MH #1	-0.01	C-9.99	-10.00	-0.30 C-9.70
BM				2.33

Chisel □ end walk SW Cor Nashville + Midway

Sub Sewer

4+75	-8.10	0.10	C-8.20
4+50	-8.20	-0.16	C-8.04
4+25	-8.30	-0.06	C-8.24
= 0+00 Nashville St.			dias 707 1414
3+96 MH #2	-8.42	0.47	C-8.89
3+75	-8.50	-0.09	C-8.41
3+50	-8.60	0.03	C-8.63
3+25	-8.70	0.01	C-8.71
3+00	-8.80	-0.06	C-8.74
2+75	-8.90	-0.03	C-8.87
2+50	-9.00	0.02	C-9.02

WO # 32064
12-3-52
Stakes 5' Rt

31

7+25 MH #3	-7 10	-0 30	C-6 80	0+75	-8 12	0 38	C-8 50
7+00	-7 20	-0 13	C-7 07	0+50	-8 22	0 43	C-8 65
6+75	-7 30	-0 13	C 7 17	0+25	-8 32	0 44	C 8 76
6+50	-7 40	-0 02	C 7 38	Nashville 0+00 MH #2	-8 42	0 47	C-8 89
6+25	-7 50	0 02	C-7 52	8+75 DE Plug	-6 50	-0 08	C-6 42
6+00	-7 60	0 02	C-7 62	8+50	-6 60	-0 25	C-6 35
5+75	-7 70	-0 22	C 7 48	8+25	-6 70	-0 25	C-6 45
5+50	-7 80	-0 20	C-7 60	8+00	-6 80	-0 12	C-6 68
5+25	-7 90	-0 30	C-7 60	7+75	-6 90	-0 14	C-6 76
5+00	-8 00	0 05	C-8 05	7+50	-7 00	-0 10	C-6 90

		-0.53 C 6.59			-0.66 C 5.46
3+25	-7.12	-0.48 C 6.64	5+75	-6.12	-0.69 C 5.43
		-0.33 C 6.89			-0.72 C 5.50
3+00	-7.22	-0.22 C 7.00	5+50	-6.22	-0.77 C 5.45
		-0.20 C 7.12			-0.80 C 5.52
2+75	-7.32	-0.13 C 7.19	5+25	-6.32	-0.83 C 5.49
		7.07 diag 14.19			-0.83 C 5.59 diag 7.07 14.14
2+50 MH #5	-7.42	0.21 C 7.63	5+00 MH #8	-6.42	-0.95 C 5.47
2+25	-7.52	0.27 C 7.79	4+75	-6.52	-1.00 C 5.52
2+00	-7.62	0.24 C 7.86	4+50	-6.62	-0.76 C 5.86
1+75	-7.72	0.25 C 7.97	4+25	-6.72	-0.65 C 6.07 -0.67 C 6.05
1+50	-7.82	0.27 C 8.09	4+00	-6.82	-0.63 C 6.19 -0.65 C 6.17
1+25	-7.92	0.21 C 8.13	3+75	-6.92	-0.58 C 6.34 -0.59 C 6.33
1+00	-8.02	0.27 C 8.29	3+50	-7.02	-0.61 C 6.41 -0.58 C 6.44

		-0 12 C-5 09			1 35 C-5 47
8+25	-5 12	-0 27 C-5 05	10+75	-4 12	1 39 C-5 51
		-0 12 C5 10			1 04 C5 26
8+00	-5 22	-0 03 C-5 19	10+50 #MH9	-4 22	1 14 C-5 36
		0 54 C-5 86			1 05 C-5 37
7+75	-5 32	0 52 C-5 87	10+25	-4 32	1 02 C-5 34
		4 03 dup 707 1417 9 46			0 93 C-5 35
7+50 MH #10	-5 42	4 01 C-9 43	10+00	-4 42	0 98 C-5 40
		-0 16 C-5 36			0 94 C-5 46
7+25	-5 52	-0 17 C5 35	9+75	-4 52	0 97 C-5 49
		0 71 C-4 91			
7+00	-5 62	-0 79 C-4 83	9+50	-4 62	0 88 C-5 50
6+75	-5 72	-0 84 C-4 88 omited	9+25	-4 72	0 66 C-5 38
		-0 70 C-5 12			
6+50	-5 82	-0 68 C-5 14	9+00	-4 82	0 57 C-5 39
		-0 61 C-5 31			0 27 C-5 19
6+25	-5 92	-0 62 C-5 30	8+75	-4 92	0 30 C-5 22
		-0 57 C-5 45			0 14 C-5 16
6+00	-6 02	-0 60 C-5 42	8+50	-5 02	0 17 C-5 19

1+50	-6.82	0.07 C-6.89	4+05	-5.80 -0.10 C-5.70
1+25	-6.92	0.07 C-6.99	3+80	-5.90 -0.03 C-5.87
1+00	-7.02	0.07 C-7.09	3+55	-6.00 0.03 C-6.03
0+75	-7.12	0.11 C-7.23	3+30 MH#6	-6.10 0.09 C-6.19
0+50	-7.22	0.20 C-7.42	3+00	-6.22 0.14 C-6.36
0+25	-7.32	0.45 C-7.77	2+75	-6.32 0.14 C-6.46
MH#5 0+00 to North La Salle	-7.42	0.21 C-7.63	2+50	-6.42 0.09 C-6.51
11+45 DE	-3.84	2.89 C-6.73	2+25	-6.52 0.01 C-6.53
11+25	-3.92	2.59 C-6.51 ~~2.56 C-6.48~~	2+00	-6.62 0.03 C-6.65
11+00	-4.02	C-2.00 C-6.02 +.96 C-5.98	1+75	-6.72 0.06 C-6.78

1+50	-6 82	-0 15 C-6 67
1+25	-6 92	-0 24 C-6 68
1+00	-7 02	-0 15 C-6 87
0+75	-7 12	-0 16 C-6 96
0+50	-7 22	-0 17 C-7 05
0+25	-7 32	-0 74 C-6 58 -0 70 C-6 62
0+00 MH #6 LaSalle to South	-7 42	0 21 C-7 63
4+80 LaSalle to N. DE	-5 50	-0 28 C-5 22
4+55	-5 60	-0 36 C-5 24
4+30	-5 70	-0 20 C-5 50

Western St. on p 19 Cont.

3+95 to South DE LaSalle	-5 84	0 23 C-6 07
3+75	-5 92	0 24 C-6 16
3+50	-6 02	0 37 C-6 39
3+25	-6 12	0 35 C-6 47
3+00 MH # 4	-6 22	0 35 C-6 57
2+75	-6 32	0 28 C-6 60
2+50	-6 42	0 15 C-6 57
2+25	-6 53	-0 12 C-6 40
2+00	-6 62	-0 23 C-6 39
1+75	-6 72	-0 39 C-6 35 -0 16 C-6 56

D. Smith
C Allen
R. Taylor
R. Parks

Stake La Palma St.
Fanuel to Gresham

Wo # 32025 — 12-4-52 — 17

	Rough	C6 Grade	C6	E grade	C6	C6 grade	Rough
2+80	C0 20 8 04	7 84		7 43		7 03	7 37 C0 34
2+60	C0 40 7 98	7 58		7 17		6 76	6 64 F0 12
2+40 BVC	C0 71 8 16	7 45		7 03		6 61	6 25 F0 36
2+00	C1 07 8 40	7 33		6 90		6 47	5 95 F0 52
1+60	C1 42 8 62	7 20		6 76		6 22	5 52 F0 80
1+35 (W) Lt	C1 86 8 99	7 13					
1+30 (E) Lt (W) Rt	C 6 70 8 80	2 10				6 21	5 87 F0 34
1+25 (E) Rt						1 40	5 41 C 4 01
1+20	C1 50 8 58	7 08		6 62		6 17	5 60 F0 57
0+80	C1 20 8 15	6 95		6 48		6 02	5 74 F0 28
0+40	C1 22 8 05	6 83		6 34		5 87	Prop 5 84 F0 03
0+20.				6 27			
0+10				6 05			
0+00 Ely Fanuel		6 70 ✓		5 71		5 72 ✓	
BM			6 97	NE Lot Fanuel + La Palma			

	Rough	C6 grade	C6
5+00 Wly Gresham		17 88	
4+90			
4+75		16 46	
4+50	C1 02 16 07	15 05	
4+25		13 63	
4+00 E.V.C.	F6 22 12 09	12 22	
+85 (W) RT			
(E) RT			
3+80	C0 18 11 34	11 16	
3+60	C0 19 C0 27 10 42	10 23	
3+40	C0 25 9 68	9 43	
+35 (W) RT			
+30 (E) RT			
3+20	C0 25 9 02	8 77	
3+00	C0 26 8 50	8 24	

	E grade	C6	C6 grade	Rough
	17 34		17 26	
	16 99			
	16 10		15 83	
	14 62		14 39	19 10 C4 71
	13 14		12 95	
	11 66		11 51	14 39 C2 88
			10 70	13 95 C3 25
			5 40	13 20 C-7 80
	10 78		10 42	13 20 C2 78
	9 86		9 47	12 47 C-3 00
	9 04		8 66	10 97 C2 31
			8 51	10 80 C2 29
			5 30	10 53 C5 23
	8 37		7 98	9 49 C1 51
	7 84		7 44	8 27 C0 83

			3+95 DE to South	-4 84	-0 38 C-4 46
Western North 2+00 DE	-5 62	-1 12 4 50	3+75	-4 92	-0 40 C-4 52
1+75	-5 72	-1 24 C-4 48	3+50	-5 02	-0 50 C-4 52
1+50	-5 82	-1 12 C 4 70	3+25	5 12	-0 55 C-4 57
1+25	-5 92	-0 96 C-4 96	3+00 MH #7	-5 22	-0 65 C-4 57
			2+75	-5 32	-0 77 C-4 55
1+00.	-6 02	-0 85 C-5 17	2+50	-5 42	-0 71 C-4 71
			2+25	-5 52	-0 62 C-4 90
0+75	-6 12	-0 90 C-5 22	2+00	-5 62	-0 70 C 4 92
			1+75	-5 72	-0 55 C 5 17
0+50	-6 22	-1 11 C-5 14	1+50	-5 82	-0 31 C-5 51
			1+25	-5 92	-0 43 C-5 49
			1+00.	-6 02	-0 72 C-5 30
0+25	-6 32	-0 76 C-5 54	0+75	-6 12	-0 98 C-5 14
			0+50	-6 22	-0 74 C-5 48
Western to North 0+00 MH #8	-6 42	-0 95 C-5 47	0+25	-6 32	-1 03 C-5 49 5 29
			Western to South 0+00 MH #8	-6 42	-0 95 C-5 47

D. Smith
C. Allen
R. Taylor
R. Parks.

INI
JER
DEC 8 1954

Stake Rest of Sunset

		stakes 8' Lt
1+80	-2 44	4 64 C-7 08
1+50	-2 35	4 58 C-6 93
1+20	-2 26	4 91 C-7 17
0+90	-2 17	5 33 C-7 50
0+60	-2 08	5 30 C-7 38
0+30	-1 99	5 19 C-7 18
0+00 MH #1	-1 90	5 11 C 7 01
0-31 66	-1 80	4 75 C-6 55
0-63 33	-1 70	4 53 C-6 23
0-95 meet existing DE	-1 61	

St Sewer
Plan 9080-2

0+60	-1 72	5 12 C-6 84
0+30	-1 81	4 92 C-6 73
0+00 MH #1	-1 90	5 11 C 7 01
3+67 existing MH.	-3 00	6 06 C-9 06
3+60	-2 98	5 80 C-8 78
3+30	-2 89	4 79 C-7 68
3+00	-2 80	5 83 C-8 63
2+70	-2 71	5 64 C-8 35
2+40	-2 62	5 57 C-8 19
2+10	-2 53	5 04 C-7 57

W.O. #20839 20
12-17-52
Meet existing MH #1 10990

2+08	-1 28	
1+80	-1 37	5 83 C-7 20
1+50	-1 45	5 63 C 7 08
1+20	-1 54	6 50 C 8 04
0+90	-1 63	6 28 C-8 68
0+60	-1 72	6 06 C-8 46
0+30	-1 81	5 85 C-8 24
0+00 MH #1	-1 90	5 63 C-8 02
3+67 existing MH	-3 00	6 06 C-9 06
3+60	-2 98	5 80 C-8 78
3+30	-2 89	4 79 C-7 68
3+00	-2 80	5 83 C-8 63
2+70	-2 71	5 64 C-8 35
2+40	-2 62	5 57 C-8 19
2+10	-2 53	5 04 C-7 57

D. Smith
C Atten
M Taylor
R. Parks

INDEX
DEC 8 1954

Sewer Stakes

Catoctin Dr + La Dorna st

wo# 31972 21
12-19-52

	Grade	Stake 6' Ely	Montezuma Rd.		
+25'	431 32	43 25 C-12 43	19 +75'	432 32	47 69 C-15 37
+50	431 22	45 75 C-14 53	20+00	432 22	47 14 C-14 92
+75'	431 12	47 20 C-16 58	+25'	432 12	46 55 C-14 43
23+00	431 02	49 13 C-18 11	+50	432 02	45 49 C-13 47
+25'	430 92	50 05 C-19 13	+75'	431 92	44 01 C 12 09
+50	430 82	50 50 C-19 68	21+00	431 82	42 63 C-10 81
+75'	430 72	50 70 C-19 98	+25'	431 72	41 62 C-9 20
24+00	430 62	50 71 C-20 09	+50	431 62	41 24 C-9 62
24+25	430 52	50 71 C-20 19	+75'	431 52	41 40 C-9 88
Mly La Dorna 24+37 55	430 47	450 71 C-20 24	22+00 MH #9	431 42	42 19 C-10 77
B.M.		451 01 Top chent East.			

Make conn. existing

Start 400'

15+00		433 22	48 95 C 15 73 (corr C 15 70)	15+25	434 12	44 16 C 10 03
15+75		433 12	49 02 C 15 20 (corr C 15 86)	15+50	434 02	44 86 C 10 84
18+00		432 02	49 03 C 16 01	15+75	433 92	45 58 C 11 66
18+25		432 92	49 05 C 16 13	16+00	433 82	46 23 C 12 41
18+50	Do 4 mats	432 82	48 84 C 16 02	16+16 MH #7	433 76	46 56 C 12 80
18+75		432 72	48 66 C 15 94	16+25 Do 4 mats	433 72	46 79 C 13 07
19+00		432 62	48 54 C 15 92	16+50	433 62	47 41 C 13 79
19+68 • MH #8		432 59	48 52 C 15 93	16+75	433 52	48 04 C 14 52
19+25		432 52	48 40 C 15 88	17+00	433 42	48 39 C 14 97 (corr 14 92)
19+50		432 42	48 13 C 15 71	17+25	433 32	48 29 C 15 47 (corr C 15 45)

			0+50	437.38	47.38 C-10.00
			0+25	437.28	47.05 C-9.77
			0+00 W'ly on Montezuma = S		
12+75		435.31	45.00 C-9.69	10+34.53 MH #5	437.18
	.0078 mile				47.29 C-10.11
13+00		435.12	44.04 C-8.92	+50	437.07
					46.92 C-9.85
13+24 MH #6		434.92	42.70 C-7.78	+75	436.87
					46.37 C-9.50
+50		434.82	41.46 C-6.64	11+00	436.68
					46.17 C-9.49
+75		434.72	40.87 C-6.15	+25	436.48
					46.07 C-9.59
14+00		434.62	40.49 C-5.87	+50	436.29
					45.80 C-9.51
+25	.0047 mile	434.52	40.61 C-6.09	+75	436.09
					45.64 C-9.55
+50		434.42	41.28 C-6.86	12+00	435.90
					45.56 C-9.66
+75		434.32	42.23 C-7.91	+25	435.70
					45.44 C-9.74
15+00		434.22	43.24 C-9.02	12+50	435.51
					45.41 C-9.90

Plug DE 1+50 437.58 47.12 C-9.54

0+75 437.48 47.56 C-10.08

		5' West			5' West
7+50	438.60	49.18 C10.58	5+00 MH#2	439.60	53.01 C-13.41
+75	438.50	48.41 C9.91	+25	439.50	52.62 C-13.12
8+00	438.40	47.86 C9.46	+50	439.40	52.26 C-12.85
L. Lt 127°49'		47.42 C9.02 1st Estab			
8+16.22 MH#3	5+10' N of F. 438.34	47.43 C-9.09	+75	439.30	52.07 C-12.77
+25	438.30	47.54 C9.24	6+00	439.20	52.01 C12.81
+50	438.20	47.80 C-9.60	+25	439.10	51.73 C-12.63
+75	438.10	48.10 C10.00	+50	439.00	51.47 C-12.47
9+00	438.00	47.97 C-9.97	+75	438.90	51.11 C-12.21
9+25	437.90	47.93 C10.03	7+00	438.80	50.63 C-11.83
L. Rt 76°25'30"					
9+40.20 MH#4	437.84	47.99 C10.15	7+25	438.70	49.28 C-11.28
		5' North			

		5' west of		5' west of
			0-12 Plug DE. 442 67	56 65 C-13 98
2+50	441 10	54 36 C-13 26	0+00	442 60	56 53 C-13 93
+75	440 95	54 06 C-13 11	+25	442 45	56 39 C-13 94
3+00	440 80	53 79 C-12 99	+50	442 30	56 24 C-13 94
+25	440 65	53 62 C-12 97	+75	442 15	56 06 C-13 91
+50	440 50	53 47 C-12 97	1+00	442 00	55 82 C-13 82
+75	440 35	53 39 C-13 04	+25	441 85	55 55 C-13 70
4+00	440 20	53 34 C-13 14	1+50	441 70	55 24 C-13 54
+25	440 05	53 26 C-13 21	1+80 MH #1	441 52	54 96 C-13 44
+50	439 90	53 21 C-13 31	2+00	441 40	54 75 C-13 35
4+75	439 75	53 15 C-13 40	2+25	441 25	54 59 C-13 34

Apr 9 00

Apr 9 00

25

			4+84.73 existing Make con.	442.40	53.61 C-10.21
4+25		443.44	52.10 C-8.66	4+75	442.44	53.20 C-11.26
2+00		443.54	51.83 C-8.29	4+50	442.54	53.88 C-11.34
4+75		443.64	51.61 C-7.97	4+25	442.64	53.69 C-11.05
4+50		443.74	51.39 C-7.65	4+00	442.74	53.52 C-10.78
L.Lt 12°30'						
1+25 MH.#10		443.84	51.18 C-7.34	3+75	442.84	53.34 C-10.50
1+00		443.94	50.78 C-6.84	3+50	442.94	53.15 C-10.21
0+75		444.04	50.00 C-5.96	3+25	443.04	53.08 C-10.04
				L.Lt 15°00'		
0+50		444.14	49.49 C-5.35	3+00 MH#11	443.14	52.96 C-9.82
0+25		444.24	48.94 C-4.70	2+75	443.24	52.69 C-9.45
Catoctin Dr						
0+00 Plug DE		444.34	48.09 C-3.75	2+50	443.34	52.37 C-9.03
BM			447.25 SW 18" Montezuma & Catoctin Dr.			

Stake Milton St Lt=North — Morena to Milton, Rt=South — 7/12/53

	Rough	cut grade			cut grade	Rough
Chicago St 2+69.76 Wly	Co 2.21	20.11	19.30	19.95	19.60	21.23 C 1.63
2+40	C 1.19	19.60	18.41	19.03	18.67	20.10 C 1.43
2+10	C 1.14	18.66	17.52	18.18	17.74	19.43 C 1.69
1+80	C 1.17	17.79	16.62	17.21	16.82	18.65 C 1.83
1+50	C 1.43	17.16	15.73	16.30	15.90	17.73 C 1.83
1+20	C 1.42	16.25	14.83	15.39	14.98	17.04 CR.06
0+90	Co.88	14.82	13.94	14.48	14.06	16.28 CR.22
0+60	Fo.17	12.87	13.04	13.57	13.14	15.98 CR.84
0+40 ℄				12.97		
0+30	Fo.18	11.97	12.15		12.22	15.26 C 3.04
0+20 ℄				12.09		
Ely Morena 0+00	Fo.22	11.03	11.25	11.22	11.30	11.26 Fo.07
BM			42.03 SW BP Erie & Milton			

	Rough	Lt = North gutter grade	℄	Rt = South gutter grade	Rough
Denver St.					
2+69.76 wly	CO 40	31.20 . 30.80	31.30	30.80	31.18 CO 38
2+40	CO 45	30.20 29.75	30.24	29.77	30.13 CO 36
2+10	CO 31	29.01 28.70	29.23	28.75	29.26 CO 51
1+80	C-O 53	28.19 27.66	28.20	27.73	28.58 CO 85
1+50	C 101	27.63 26.62	27.14	26.21	28.15 C-1 44
1+20	CO. 69	26.24 25.57	26.13	25.68	27.37 C 69
0+90	C 102	25.55 24.53	25.10	24.66	26.18 C 52
0+60	C 110	24.58 23.49	24.06	23.64	25.59 C 75
0+30	C-1 27	23.71 22.44	23.03	22.62	24.27 C 60
0+00 Ely Chicago	C-1 58	22.98 21.40	22.00	21.60	23.36 C 76
0-40 ℄ Chicago			20.98	20.60	22.30 C 70

	Lt = North			Rt = South		
	Rough	gutter grade	℄	gutter grade	Rough
2469 76 Wly Erie to North	FO 1 40 90	41 00	41 07	39 88	40 74 CO 50
2459 76			40 78	40 19	
2440	FO 29 39 88	40 17	40 28	39 22	40 23 C1 01
2410	FO 24 38 90	39 14	39 36	38 41	39 91 C1 50
1480	CO 23 38 45	38 22	38 48	37 60	38 45 CO 85
1450	CO 22 37 52	37 30	37 60	36 79	37 83 C1 04
1420	CO 03 T 36 41	36 38	36 72	35 97	37 07 C1 10
0490	FO 14 35 32	35 46	35 84	35 15	36 01 CO 84
0460	CO 34 34 88	34 54	34 96	34 33	35 05 CO 72
0430	CO 95 34 57	33 62	34 08	33 51	34 41 CO 20
0400 Fly Denver	C1 51 34 21	32 70	33 20	32 70	33 74 C1 24
0-40 ℄ Denver			32 20	31 75	32 83 CO 78

	Lt = North			Lt = South		
	Rough	gutter grade	℄	gutter grade	Rough	
2+69.76 Frankfort Wly	FO 51.25	51.50	51.85	51.95		
2+40		50.49	50.82	50.20		
2+10	CO 3 49.45	49.42	49.78	49.17	50.46 C-1.29	
1+80	CO 37 48.73	48.36	48.74	48.15	49.56 C-1.41	
1+50	CO 22 48.02	47.30	47.70	47.12	48.26 C-1.64	
1+20	CO 57 46.81	46.24	46.66	46.10	47.39 C-1.69	
0+90	CO 25 46.13	45.18	45.62	45.07	46.22 C-1.65	
0+60	CO 66 44.78	44.12	44.58	44.05	45.47 C-1.42	
0+30	C/ 51 44.57	43.06	43.54	43.03	44.07 C-1.05	
0+10			42.85			
0+00 Ely Erie	C/ 50 43.50	42.00	42.47	42.00	42.77 C-0.77	
			41.79			
0+40 ℄ Erie						

		Lt = North		ℓ	Lt = South	Gutter grade	Rough
			Gutter grade				
1+85	C 1 12	63 02	61 90	62 70		62 10	63 78 C 1 68
1+65	C 1 35	61 45	60 10	60 70		60 30	63 12 C 2 82
1+45	C 1 28	59 88	58 60	59 15		58 70	61 90 C 3 20
				58 55			
1+25	C 1 54	58 24	57 40	57 95		57 50	60 58 C 3 08
1+05	C 1 56	58 06	56 50	57 00		56 50	59 40 C 2 90
0+85 BVC	C 0 97	56 82	55 85	56 30		55 75	58 12 C 2 37
0+65	C 0 84	56 13	55 29	55 72		55 15	57 34 C 2 19
0+45	C 0 62	55 36	54 74	55 15		54 55	56 40 C 1 85
0+25	C 0 22	55 11	54 19	54 57		53 95	55 20 C 1 25
0+00 Ely Frankfort	C 1 40	54 98	53 50	53 85		53 20	54 69 C 1 19
0-40	C 0 36	52 86	52 50	52 85		52 58	52

	Lt - North				Rt - South		
	Rough	Gutter grade			Gutter grade	Rough	
1+50	C2 00	101 80	99 80	100 35	100 30	100 53	C0 23
1+20	C1 26	96 45	95 19	95 69	95 69	95 47	FO 22
0+90	C1 29	91 87	90 58	91 03	91 08	90 78	FO 30
0+60	C1 38	87 35	85 97	86 39	86 47	86 29	FO 18
0+30	C0 74	82 10	81 36	81 71	81 86	82 35	C0 52
0+20				80 16			
0+00 Galveston Ely	C1 35	78 10	76 75	77 50	77 25	78 28	C1 53
0-40	C1 15	75 03	73 88	74 40			
2+69 62 Galveston Wly	FO 37	70 63	71 00	71 58	71 50	73 93	C2 43
2+49 6				69 74			
2+35	F-0 39	67 38	67 77	68 06	67 73	69 45	C1 72
2+05 E.V.C.	C0 50	64 50	64 00	64 20	64 40	65 24	C0 84

	Lt = North			Rt = South		
	Rough	Gutter grade			Gutter grade	Rough
1+20	CO 48	146 59	146 11	146 61	146 11	148 34 C2 23
1+60 BVC	CO 43	143 56	143 13	143 63	143 13	144 41 C1 28
0+66 6	FO 48	137 63	138 11	138 70	138 29	138 68 CO 39
0+33 3	F1 11	131 28	133 09	133 76	133 44	133 09 FO 35
0+00 Ely Hartford & N	CO 25	128 32	128 07	128 82	128 59	128 03 FO 56
0-40	C1 70	124 86	123 16	123 21	123 67	124 08 CO 44
2+69 62 Wly Hartford & N	C1 53	119 78	118 25	119 00	118 75	119 24 CO 34
2+40	C1 44	115 07	113 63	114 33	114 13	115 40 C1 27
2+10	C1 24	110 26	109 02	109 66	109 52	110 47 CO 25
1+80	C1 94	106 35	104 41	105 01	104 91	105 85 CO 94

Lt = North

Rt = South

	Rough	gutter grade			gutter grade	Rough
2+69.62 w/y Illion	CO 0.7 156.20	156.13	156.26		155.63	156.13 CO 0.56 CO 0.66
2+45	FO 0.22 155.39	155.61			155.36	156.17 CO 0.21
2+40			156.00			
2+20 EVC.	FO 0.12 154.97	155.09	155.59		155.09	155.60 CO 0.51
2+00	CO 0.24 154.47	154.23	154.73		154.23	153.78 CO 0.55
1+80	CO 0.47 153.57	152.90	153.40		152.90	155.01 CO 2.11
1+60	CO 0.83 151.93	151.10	151.60		151.10	153.28 CO 2.18
1+40	CO 0.46 149.30	148.84	149.34		148.84	151.32 CO 2.48

Stake Hill St

	Rough	Cl grade	
1+64 74 Brk	C2 74 72 14	269 40	9 56 CO 16
1+27 34 transition	Prop elv. 272 35	272 10	2 73 CO 63
0+90 Brk	F 180/180 1:1 to prop (variable slope)	274 80	5 12 CO 32
0+70 S RP -21	F 179/269 1½:1 to prop	275 98	6 30 CO 32
0+54 transition	Prop elv. 277 15		
0+50		277 16	7 70 CO 54
0+30	CO 41 78 74	278 34	8 74 CO 40
0+10	C-2 80 82 32	279 52	9 75 CO 23
0+00 Wly Line (Sunset Ridge)		279 99 V	
BM			279 26

F 82 19 7/24 E Pine Hill W Sunset Ridge

Alexandria Wly

3+82 74 Hand (=s 30)				
3+78 24 (=s 30)	@ prop 244 27	4 16 FO 11	244 03	D = CO 09 44 36 CO 33
Dry D				
3+57 74 (=s 30)	@ prop 246 69	7 38 CO 69	246 45	D = FI 3 45 40 F-1 05
3+53 74 BC 3+53 30 Hand (=s 30)		CO 69 7 22 CO 20 7 15	246 53 W 246 95	
3+39 74 Brk		CO 48 9 03	248 55	46 93 F-1 62
3+05 99		CO 60 3 34	252 24	52 68 FO 26
2+72 24		CO 60 7 53	256 93	59 37 C-1 44
2+38 49		CO 52 1 64	261 12	62 49 C-1 37
2+04 74 Brk		CO 26 5 56	265 30	66 21 CO 91
1+84 74		CO 23 7 84	267 61	68 21 CO 60

WO 62283 35

1/23/53

	Cl grade	Rough
	FO 46 3 65	244 11
	CO 21 43 60	243 59

	Rough	c6 grade				c6 grade	Rough
6+09 74	C3 16 22 80	219 64	9 51 Fo 1 13				
5+82 3 4'Rad F.C.		222 98 L2 97 Fo 21 222 53	22 73 Co 2 20				
5+78 3	Co 08 Co 32 23 22	222 90	Fo 8 4 2 30	@ Prop 223 14			
5+54 3 Dry "B"	Fo 11 25 10			@ Prop 225 21			
5+31 3	D= F1 11 Fo 87 26 98	227 85	Co 45 8 54	@ Prop 228 09			
5127 34 4'Rad B.C.		227 93 W 8 46 Co 53 228 31	8 43 Co 12				
4+99 74	F-2 77 28 45	231 22	1 62 Co 40				
4+72 24	F-3 72 30 39	234 11	4 39 Co 28		6+66 3 2'Rad F.C.		
						Co 84 14 94	214 10 @ Prop
4+57 30 74 4'Rad. F.C.		236 13 F 5 80 Fo 33 235 63	5 82 Co 19		6+64 3		213 86
					Dry "A"		
4+53 30 74	D= F-1 72 Fo 93 35 12	236 05	Fo 28 6 01	@ Prop 236 29	6+56 3		
Dry "C"						Co 20 14 84	214 74 @ Prop
4+21 30 74	D= F-1 63 F-1 38 38 02	239 41	Fo 38 9 27	@ Prop 239 65	6+54 3 2'Rad B.C.	Co 11 14 69 Fo 2 14 71	214 58 W 214 78
4+17 30 74 4'Rad B.C.		239 49 W 9 83 Co 34 239 83	9 25 Co 12		6+37 24	Fo 48 6 27	216 75 22 86 C6 11
3+89 74 Brk	Co 52 43 30	242 28					

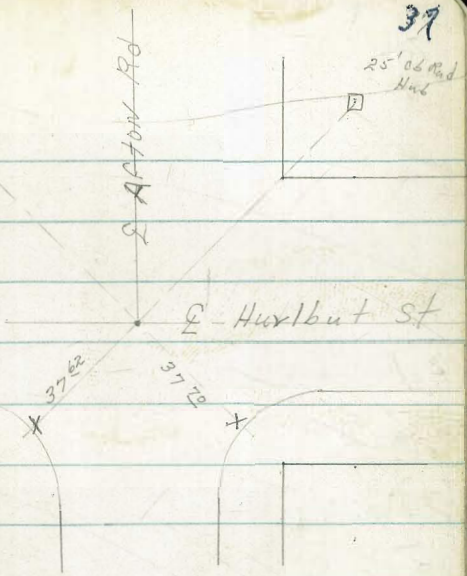
Rt = North

	Rough	Cb grade	Cb	Stake
Cl from BC Afton 0+00	Fo 48 94 60	395 08	94 59 Fo 49	Hurlbut St
0+45 5	Co 19 94 97	394 78	94 82 Co 04	
0+91	Co 15 94 63	394 48	94 37 Fo 11	
1+36 5	Fo 03 94 15	394 18	94 14 Fo 04	
1+82	Co 44 94 32	393 88	94 05 Co 17	
~~2+27 5~~	Cl 05 ~~94 63~~	~~393 58~~	93 31 Fo 27	
2+73	Cl 17 94 35	393 28	93 46 Co 18	
3+18 5	Co 30 93 28	392 98	93 18 Co 20	
3+64	Fo 16 92 52	392 68	92 45 Fo 23	
4+09 5	Co 11 92 49	392 38	92 24 Fo 17	
4+55	Co 20 92 28	392 08	91 84 Fo 24	

25'06 Rad Hub 1

INDEXED
JER
DEC 8 1954

37



EC. Afton	395 28	95 42	Co 14
3/4	395 23	95 19	Fo 04
1/2	395 18	94 87	Fo 28
1/4	395 13	94 60	Fo 53
BC Hurlbut	395 08	94 59	Fo 49

D. Smith
C. Allen
R. Parks
C. O'Miel

Lt = West

	Rough	Cb grade	Stake Aft on St. ℄
2+05		395 90	96 08 CO 18
1+85 EVC. East	F0 15 95 78	395 93	95 24 CO 01
1+65		395 92	95 90 F0 02
1+45 BVC. west	F0 39 95 47	395 86	95 23 CO 07
1+25		395 78	
1+05 BVC east	F0 13 95 57	395 70	95 82 CO 12
0+70	CO 27 95 83	395 56	95 80 C-O 24
0+35	CO 43 95 85	395 42	95 72 C-O 30
0+20			
0+00 Cb. Prop BC. Hurlbut	F0 68 94 60	395 28	95 42 CO 14
	11+51 50' RP to ℄ on Rt Ext Hub BM		397 82

	℄
	395 74
	395 81
	395 84
	395 83
	395 78
	395 71
	395 58
	395 44
	395 37
	395 20

INDEXED
YER
DEC 8 1954

Rt = East

WO 21 11/28/52 2086

	Cb grade	Rough
	396 02	96 20 CO 78
	396 10	
	396 13	96 59 CO 46
	396 12	
	396 06	95 97 F0 09
	395 92	95 99 CO 27
	395 78	95 72 F0 04
	395 64	94 98 F0 66
	395 77	F0 79

Lt = West

		Rough	C6 grade	
5+85		CO 22 94 24	394 02	94 05 CO 03
5+45		FO 37 93 86	394 22	93 93 FO 29
5+05		FO 63 93 79	394 42	94 27 FO 15
4+65		FO 43 94 19	394 62	94 68 CO 06
4+25		FO 48 94 34	394 82	95 00 CO 18
3+85		CO 04 95 06	395 02	95 29 CO 27
3+45		FO 18 95 04	395 22	95 41 CO 19
3+05		E 95 43	395 42	95 52 CO 10
2+65		CO 30 95 92	395 62	95 69 CO 07
2+25	EVC, west	FO 46 95 34	395 82	96 08 CO 26

℄

393 85
394 05
394 25
394 45
394 65
394 85
395 05
395 25
395 45
395 65

Rt = East

C6 grade	Rough
394 02	95 82 C-1 80
394 22	95 88 C-1 66
394 42	95 89 C-1 47
394 62	96 14 C-1 52
394 82	96 27 C-1 45
395 02	96 28 C-1 26
395 22	96 67 C-1 45
395 42	96 86 C-1 44
395 62	96 36 CO 74
395 82	97 26 C-1 44

Lt = West

	Rough	cb Grade	
9+05	CO^{80} 94^{48}	393^{68}	94^{04} CO^{36}
8+65	FO^{50} 92^{96}	393^{46}	93^{63} CO^{17}
8+25 E.V.C.	C1^{64} 94^{88}	393^{24}	93^{04} FO^{20}
8+05		393^{16}	92^{97} FO^{17}
7+85	CO^{24} 93^{36}	393^{12}	92^{93} FO^{19}
7+65		393^{15}	93^{14} FO^{01}
7+45 B.V.C.	FO^{92} 92^{30}	393^{22}	93^{30} CO^{08}
7+05	FO^{06} 93^{36}	393^{42}	93^{58} CO^{16}
6+65	CO^{13} 93^{75}	393^{62}	93^{82} CO^{20}
6+25	CO^{06} 93^{88}	393^{82}	94^{05} CO^{23}

Rt = East

4/0

2	cb grade	Rough
	393^{68}	94^{65} CO^{97}
	393^{46}	93^{28} C-0^{52}
393^{07}	393^{24}	94^{01} CO^{72}
392^{99}	393^{16}	
392^{95}	393^{12}	94^{13} C1^{01}
392^{98}	393^{15}	
393^{05}	393^{22}	94^{24} C1^{52}
393^{20}	393^{42}	94^{53} C1^{11}
393^{45}	393^{62}	95^{84} C2^{24}
393^{65}	393^{82}	95^{91} C2^{09}

Lt = West

	Rough	Cb Grade	
13+05	Co^{40} 96^{29}	395^{89}	95^{81} Fo^{08}
12+65	Co^{43} 96^{10}	395^{67}	95^{89} Co^{22}
12+25	Co^{61} 96^{06}	395^{45}	95^{68} Co^{23}
11+85	Co^{82} 96^{05}	395^{23}	95^{42} Co^{19}
11+49 22 obend Rt.			
11+45	Cl^{15} 96^{16}	395^{01}	95^{18} Co^{17}
11+05	Cl^{12} 95^{90}	394^{78}	95^{15} Co^{37}
10+65	Cl^{80} 95^{86}	394^{56}	94^{84} Co^{28}
10+25	Cl^{49} 95^{83}	394^{34}	94^{64} Co^{30}
9+85	Co^{23} 95^{05}	394^{12}	94^{39} Co^{27}
9+45	Co^{58} 94^{48}	393^{90}	94^{20} Co^{30}

Rt = East

	Cb Grade	Rough
Co^{16} 96^{05}	395^{89}	97^{38} Cl^{42}
Co^{02} 95^{69}	395^{67}	97^{22} Cl^{55}
Co^{01} 95^{46}	395^{45}	96^{24} Cl^{49}
Co^{27} 95^{50}	395^{23}	97^{32} Cr^{29}
Co^{26} 95^{29}	395^{03}	
	395^{01}	97^{10} Cr^{09}
	394^{78}	97^{37} Cr^{54}
	394^{56}	96^{69} Cr^{13}
	394^{34}	96^{48} Cr^{14}
	394^{12}	94^{78} Co^{66}
	393^{90}	94^{49} Co^{59}

	Rough	Lt = West		397 47 E Lidisk	Rt = East		Fl 4 42 Rough
EC.	Fr 0	396 97	96 40 Fo 57		Fl 22	96 44	397 66
3/4		397 05	96 53 Fo 52		Fo 42	97 14	397 56
Mid Pt.		397 12	96 96 Fo 16		Fo 14	97 31	397 45
1/4 [illegible]		397 20	97 15 Fo 05		Fo 16	97 19	397 35
15+51 25 C6 BC.	Fr 26	94 06	397 22	97 48 Co 26	Fo 18	97 07	397 25	96 22 Fl 03
15+45 25 Proj BC.	Fl 17	96 05	397 22	97 43 Co 21	Co 08	97 30	397 22	96 26 Fo 26
15+05	Co 06	97 05	396 99	96 78 Fo 21	Co 17	97 14	396 99	96 40 Fo 59
14+65	Co 32	97 09	396 77	97 02 Co 25	Co 38	97 15	396 77	97 51 Co 74
14+25	Co 59	97 14	396 55	96 82 Co 27	Co 22	96 77	396 55	97 49 Co 94
13+85	Co 47	96 89	396 33	96 40 Co 07	Fo 02	96 31	396 33	97 18 Co 85
13+45	Co 25	96 36	396 11	96 22 Co 11	Co 01	96 12	396 11	97 10 Co 98

Smith
Allen
Taylor
Parker
O'Neil

INDEXED
8 10EA
MER

stake Alley Blk 7 - city Hts Annex #2.

W.O. # 31735
1-28-53.

FB-1759-49 -

9676-L

BM = NW BP - Myrtle & Highland - El = 336.63
BM - S.W. 7' CT. Myrtle & Highland - El = 336.24
FB 1759-37

	Lt = West			Rt = east	
	stake			stake	
	FO 11		C	CO 35	
2+60	343.74	343.85	344.05	344.40	
	CO 01		C-4.67	Nail 0.8 bk.	
2+40	343.54	343.53	343.73	348.40	
TPLT	FO 03			CO 59	
2+00	342.83	342.86	343.06	343.65	
	FO-21			C-0.26	
1+60	341.99	342.20	342.40	342.66	
⊠ 1'bk	CO.56			C-0.52	
1+20	342.09	341.53	341.73	342.25	
	CO. 54			C 0.30	
0+80	341.41	340.87	341.07	341.37	
	CO-21			C 0.52	
0+60	340.68	340.47	340.69	341.19	
	CO. 32			CO 55	
0+40	340.29	339.97	340.17	340.72	
	CO. 71			C-1.22	
0+20	340.05	339.34	339.54	340.76	
Alyline Myrtle					
0+00		338.60	338.80		

	Lt = West		Rt = east	
		stake		stake
sly Dwight				
6+01.30	347.60		347.60	347.61
		CO 27		CO 80
5+60	347.33	347.60	347.20	348.00
OTO BK	CO	CO 51		C-0.54
5+20	347.06	347.57	346.80	347.34
	C	CO 19		CO 45
5+00	346.93	347.12	346.60	347.05
		CO 31		C 0 33
4+80	346.67	346.98	346.40	346.73
Nail 0.95 in Alley		C-0.88	'X' 3'bk	CO 49
4+40	346.13	347.01	346.00	346.49
		CO 05		C 0.97
4+00	345.60	345.65	345.60	346.57
	C	CO 34	C 1.50	C 1.50
3+60	345.07	345.41	345.20	346.70
	C 42	CO 49		C 0.77
3+40	344.82	345.31	345.00	345.77
	C	CO 05	C-1.88	
3+20	344.60	344.65	344.80	346.68
		CO 41		FO 07
3+00	344.38	344.79	344.58	344.51
⊠ 2'bk		CO.51	C 0.4	C 0 93
2+80	344.13	344.64	344.33	344.36

D. Smith
J. Rover
R. Taylor
C. Abell

Plan # 92932"

INDEXED
DEC. 8 1954

Stake Alley Blk 40 — Teralta

33rd St + Felton — Orange + El Cajon

W.O. # 32024 — 2/13/53 — 44

	Lt = West		Rt = East (3' BK unless specified)			Lt = West		Rt = East		
2+17	Co 44 73 32	372 88	372 88	74 20 C-1 32	5+07	Co 54 74 31	373 80	373 80	74 39 Co 59	1' BK
1+87 EVC.	Co 15 72 94	372 79	372 79	74 28 C-1 49	4+87 BVC.	Co 16 73 85	373 69	373 69	74 13 Co 44	
1+67	1' BK Fo 04 72 64	372 68	372 68	73 84 C-1 16	4+57	1' BK Co 73 60	373 60	373 60	73 75 Co 15	
1+47	0.12 IN Nail Co 48 72 86	372 47	372 47	73 53 C-1 06	4+27	Co 41 73 92	373 51	373 51	74 55 C-1 04	0.52 BK Nail
1+27	Co 10 72 27	372 17	372 17	73 29 C-1 12	3+97	Co 76 74 18	373 42	373 42	74 69 C-1 27	0.60 BK Nail
1+07 BVC.	Co 47 72 24	371 77	371 77	73 40 C-1 63	3+67	Co 31 73 44	373 33	373 33	74 63 C-1 30	1.02 BK Nail
0+77	0.06 IN Nail C-1 14 72 24	371 10	371 10	72 50 C-1 40	3+37	Co 28 73 52	373 24	373 24	74 27 C-1 03	
0+47	Co 21 70 64	370 43	370 43	72 01 C-1 58	3+07	Co 06 73 21	373 15	373 15	74 85 C-1 70	0.08 BK Nail
0+17 Brk	Co 49 70 24	369 75	369 75	71 25 C-1 50	2+77	Co 20 73 26	373 06	373 06	74 46 C-1 40	
0+00 Nly Orange Ave		369 39	369 66		2+47	Co 42 73 39	372 97	372 97	74 57 C-1 60	
BM			366 66	NWBP 33rd & Orange						

	Lt = West			Rt = East
6407 S/y El Cajon		374.88	375.02	
5787 B.K	0.02 iN Nail C.2.13 76.88	374.75	374.75	75.99 C.1.24 0.24 BK Nail
5757	1.04 BK Nail C1.26 75.64	374.28	374.38	75.31 C0.93 0.28 BK Nail
5727 Evc.	C0.61 74.61	374.60	374.80	74.66 C0.66

WO# 62316
3/11/53

Golden / Warehouse Sewer New St.

Staked S. N.

2+70	-0 46	6 16 C-6 62	6+00 MH #2	1 29	6 05 C-4 76
2+40	-0 91	6 39 C-7 30	5+70	1 17	6 07 C-4 90
2+10	-1 36	6 43 C-7 79	5+40	1 04	6 23 C-5 19
1+80	-1 81	6 12 C-7 93	5+10	0 91	6 49 C-5 58
1+50	-2 26	6 48 C-8 74	4+80	0 78	6 38 C-5 60
1+20	-2 71	7 39 C-10 10	4+50	0 65	6 40 C-5 95
0+90	-3 16	6 69 C-9 85	4+20	0 52	6 31 C-5 79
0+60	-3 61	6 98 C-10 39	+90	0 39	5 42 C-5 03
0+30	-4 06	7 50 C-11 56	+60	0 26	5 56 C-5 30
0+00 MH existing may be	-4 51	7 40 C-11 91	3+30	0 13	5 93 C-5 80
			3+00 MH #1	0-00	6 00 C-6 00

water elv. 14 60

water elv. 11 10

D.Smith
J.Rovers

Paces

Sewer 12" Stake

3+00 — -4 67 — 7 28 C-12 45

2+66 6 — -4 74 — 9 12 C-13 86

2+33 3 — -4 82 — 9 15 C-13 97

2+00 — -4 89 — 9 53 C-14 42

1+66 6 — -4 97 — 9 50 C-14 47

1+33 3 — -5 04 — 9 50 C-14 54

1+00 — -5 12 — 10 05 C-15 17

0+66 6 — -5 19 — 11 48 C-16 67

0+33 3 — -5 27 — 15 32 C-20 59

0+00 existing MH — -5 34 — rim 154

BM — 644 — Cor Mon E Sherman St S/y Anna st

.00226 rate.

Sewer 15" Sherman St & Custer St

Work 21001

3/25/53

6+40 80 — -3 89 — 7 39 C-11 28

6+10 80 — -3 96 — 6 92 C-10 88

5+80 80 — -4 03 — 6 84 C-10 87

5+50 80 — -4 10 — 6 89 C-11 09

5+20 80 — -4 17 — 6 66 C-10 83

4+90 80 — -4 24 — 6 52 C-10 76

.00226 rate

4+60 80 — -4 31 — 6 62 C-10 93

4+30 80 — -4 38 — 6 84 C-11 22

4+00 80 — -4 44 — 7 12 C-11 56

32 47 — 7 35 C-11 86 — FO 47 Top

3+68 23 MH #1 — -4 51 — 15 FT — 15 FT

34 80 — 10 FT — 10 FT

3+33 3 — -4 59 — 7 40 C-12 04

9+50 75		-3 26	7 31 C-10 67		
9+20 75		-3 41	7 48 C-10 89		
8+90 75		-3 45	7 62 C-11 07		
8+60 75		-3 50	7 71 C-11 21		
8+30 75		-3 55	7 47 C-11 02		
8+00 75 MH #3		-3 60	6 60 C-10 20		
			16.97 dia		
7+90 90		-3 62	6 87 C-10 49		
7+60 90	.017 rate	-3 67	6 85 C-10 52		
7+30 90		-3 72	7 23 C-10 95		
7+00 90		-3 77	7 52 C-11 29		
6+70 90 MH #2		-3 82	8 06 C-11 88		

12+67 71	-2 88	6 02	C-8 20
12+37 71	-2 92	6 48	C-9 40
12+07 71	-2 97	6 14	C-9 11
11+77 71	-3 01	7 99	C-11 70
11+47 71	-3 06	7 26	C-10 32
11+47 31 New MH #1 (10,623'-4")	-3 05	7 27	C-10 32
11+17 71	-3 10	7 24	C-10 34
10+87 71 MH #4	-3 15	6 21	C-9 86
		12.93 dia	
10+70 75	-3 17	7 00	C-10 17
10+40 75	-3 22	7 26	C-10 28
10+10 75	-3 26	7 34	C-10 60
9+80 75	-3 31	7 23	C-10 54

@ 90° to Main Stake 12+42

	L. 1°57 15" Rt				
16+50.55 Ely end existing pipe	-2.30	-2.20 ie existing			
+110' of existing pipe					
15+10.55 MH#5	-2.51	-2.51 ie existing			
14+77.71	-2.56	8.13 C-10.69	18+61.49 MH#6	22.54 -1.98	12.05 C-10.49
14+47.71	-2.61	7.16 C-9.77	18+30.55	22.59 -2.03	12.22 C-10.37
14+17.71	-2.65	6.75 C-9.40	18+00.55	22.63 -2.07	12.03 C-10.60
13+87.71	-2.70	6.84 C-9.54	17+70.55	22.68 -2.12	6.79 C-15.89
13+57.71	-2.74	6.49 C-9.23	17+40.55	22.72 -2.16	6.37 C-16.35
13+27.71	-2.79	6.42 C-9.21	17+10.55	22.77 -2.21	8.81 C-13.26
12+97.71	-2.83	6.15 C-8.98	16+80.55	22.81 -2.25	9.33 C-13.48

D. Smith
J. Norey
R. Parks
R. Taylor

Stake Alleys "T" University Hts. 1st Extn

B/K 104 3'BK Ft. West

INDEXED SER DEC 8 1954

WO # 31945 5.0
4/7/53
Ft = North 3'BK

2+60 E.V.C.	Co 11 2 46 332 35	332 05 1 11 F.O 94	0+80 Co 27 1 06 330 79	330 79 1 80 C 1 01
2+40	C O 79 3 57 332 78	332 48 1 59 F.O 89	0+60 F.O 50 1 58 332 08	332 08 2 15 C O 07
2+20	C O 65 3 72 333 09	332 77 2 34 F.O 43	0+40 2'BK F 1 14 2 57 333 71	333 71 3 03 F O 68 1'BK
2+00	C O 52 3 86 333 34	333 04 2 76 F.O 28	0+20 2'BK F 1 35 4 33 335 68	335 68 4 86 F O 80 0 43 BK
1+80 B.V.C.	C O 55 4 09 333 64	333 24 2 62 F O 62	0+00 W'ly Arizona 336 06	338 06
1+40	C O 54 4 42 333 88	333 58 4 03 C O 45	E & W Alley	
1+00	C O 29 4 51 334 22	333 92 4 43 C O 51	4+50 N'ly of E & W Alley C 1 18 9 51 328 31 33	328 04 06 8 20 C O 14
0+60	C O 68 5 24 334 56	334 26 4 23 C O 67	4+30 C O 74 9 48 328 74	328 44 8 42 F O 02
0+20 B.K	C 1 22 6 11 334 89	334 59 4 92 C O 33	3+87.5 C O 28 9 72 329 64	329 34 9 87 C O 53
0+00 S'ly Meade N & S Alley 20' wide	335 06	334 62	3+45 C O 54 1 08 330 54	330 54 9 44 F O 80
BM		331 41 S.E.B.P. Texas & Meade	3+02.5 F O 13 1 31 331 44	331 14 0 16 F O 98

			Stake Alleys Blk 103 University Hts
			0+72 8^{20} Co^{13}
			T+R2 Nly end Headwall 8^{21} ~~Co^{07}~~ 328^{07}
			327^{63} Co^{48} ic
			9^{81} Co^{41} $C1^{09}$
			0+74 8^{40} 328^{40} 327^{72} Co^{68} ic
3+00 Sly Texas	326^{13}	326^{13}	0+80 EVC Co^{27} 8^{57} 328^{25} 328^{45} 8^{40} Fo^{05}
2+65	Co^{54} 7^{14} 326^{60}	326^{60} 7^{28} Co^{68}	Co^{45} 9^{13} 0+60 B.K ~~Co^{39}~~ ~~9^{15}~~ 328^{68}
2+30	Co^{98} 8^{06} 327^{08}	327^{08} 7^{64} Co^{56}	0+60 328^{68} 328^{88} 9^{09} Co^{21}
1+95	Co^{74} 8^{30} 327^{56}	327^{56} 7^{21} Co^{15}	0+40 329^{39} 329^{57} 31^{24} $C1^{64}$
1+66 EVC	$C3^{24}$ 1^{28} 328^{04}	328^{04} 7^{98} Fo^{04}	~~Co^{55}~~ ~~Co^{41}~~ 0+36 30^{13} 329^{58} 329^{81} CR^{22} ic
1+40	$C3^{29}$ 1^{60} 328^{31}	328^{31} 9^{43} $C1^{10}$	0+20 Co^{29} 30^{65} 330^{36} 330^{51} 1^{96} $C1^{44}$
1+20	$C3^{07}$ 2^{07} 329^{00}	329^{00} 9^{83} Co^{83}	0+07 E $C3^{74}$ 1^{31} 328^{05} ic 331^{15} $C6^{16}$ rim E
1+00	CR^{13} 1^{80} 329^{77}	329^{77} 0^{57} Co^{80}	0+00 Sly Meade 331^{60} 331^{72}
			BM 325^{97} NEBP El Cajon Louisiana

	Lt = East	Rt = West	Lt = South	Rt = North
3+30 EVC.	4 BK Co^{26} 6^{32} 326^{07}	326^{30} 6^{44} Co^{14}		
3+70	4 BK Co^{47} 6^{63} 326^{16}	326^{41} 6^{44} Co^{03}	1+00 Fo^{33} 5^{04} 325^{27}	080 BK 325^{37} 6^{14} Co^{77}
2+90 BVC.	Co^{18} 6^{46} 326^{28}	326^{53} 7^{84} Cl^{31}	0+60 Fo^{96} 4^{29} 325^{25}	325^{25} 5^{30} Co^{06}
2+50	$C-O^{71}$ 7^{26} 326^{55}	102 BK 324^{78} 8^{23} Cl^{45}	0+20 Co^{62} 5^{25} 325^{13}	080 BK 325^{13} 5^{39} Co^{26}
2+10	Co^{51} 7^{32} 326^{81}	327^{03} 8^{48} Cl^{45}	0+00 Wly Texas 325^{10}	325^{20}
1+70 EVC.	Co^{31} 7^{39} 327^{08}	327^{28} 7^{77} Co^{49}	4+50 Nly E-Walley Fo^{07} 5^{42} 325^{49} 12 ent alley E	325^{69} 326^{37} Co^{92}
1+50	Co^{41} 7^{66} 327^{25}	327^{45} 8^{21} Co^{76}	4+43 BC Lt. 4+40 Co^{20} 5^{83} 325^{63}	325^{60} 25^{45} Fo^{04}
1+30 BVC.	Co^{36} 7^{86} 327^{50}	327^{20} 8^{45} Co^{75}	1 BK Co 05 4+30 5^{78} 325^{73}	325^{79} 6^{06} Co^{27}
1+02 end culvert	5^{11} Co 06 Co 19 7^{76} 327^{92}	Co 53 Co 40 327^{58} 18	3+96 Co^{37} 6^{71} 325^{84}	325^{96} 6^{48} Co^{52} 185 BK 17
1+05	Co^{28} 8^{15} 13 327^{87}	328^{07} 8^{58} Co^{51}	3+63 Co^{12} 6^{14} 325^{95}	326^{13} 7^{12} Co^{99} 176 BK

SR

	Lt: South	Rt: North
3400 Ely Louisiana	327^{33}	327^{40}
2780	$C\text{-}0^{63}$ 7^{56} 326^{93} 10BK	326^{98} 8^{22} $C1^{24}$ 14BK
2760	$C1^{04}$ 7^{57} 326^{53} 06BK	326^{57} 7^{59} $C1^{02}$ 22BK
2740	CO^{14} 6^{31} 326^{47}	326^{20} 6^{97} CO^{77} 17BK
2720	CO^{41} 6^{31} 325^{90}	325^{91} 6^{29} CO^{88} 12BK
2700	CO^{29} 6^{00} 325^{71}	325^{72} 6^{81} $C1^{09}$ 15BK
1780	CO^{35} 5^{96} 325^{61} 06BK	325^{61} 6^{39} CO^{74} 05BK
1760	CO^{19} 5^{44} 325^{55}	325^{56}
1740	CO^{36} 5^{85} 325^{49} 09BK	325^{49}

D. Smith
J. Rorer
R. Taylor

Lt = South

Stake San Bernardo & La Paz Terrace

wo # 31795

Rt = North

54

	Rough Stake	C6 grade	C6			C6	C6 grade	Rough Stake
1+75 24		179 00		178 90				
1768 34 ACLT	Co 27 79 37	179 10	79 28 Co 18		SURVEYED DEC 8 1954	Co 08 79 28	179 70	79 53 Co 56
1+50	Co 25 79 11	179 37	79 54 Co 17	179 27		Fo 19 79 27	179 46	79 74 Co 28
1+25	Fo 11 79 81	179 68	79 87 Co 19	179 65		Fo 42 79 50	179 92	80 12 Co 20
1+00	Fo 42 79 97	179 99	79 97 Fo 02	180 02		Fo 41 79 98	180 39	80 30 Fo 09
0+75	Fo 39 79 97	180 38	80 35 Co 05	180 40		Fo 36 80 51	180 86	81 20 Co 34
0+50	Fo 45 80 87	180 61	80 75 Co 14	180 77		Fo 34 80 98	181 32	81 20 Co 38
0+25	Fi 01 80 77	180 92	81 32 Co 40	181 15		Fo 18 81 60	181 28	82 51 Co 73
0+00	Fo 26 80 97	181 23	81 16 Fo 07	181 52		exists ✓ end	182 23	
0-05				181 59				
0-10 74		181 08	existing ✓ end					
BM			183 40	NWBP San Bernardo San Jacinto				

	Lt. South				Rt. North			
	Rough Subbase	C6 grade	C6	℄	C6	C6 grade	Rough Subbase	
4+21 91 6°26.75	FO 34 74 02	174 36	74 38 CO 02	174 27	CO 06 74 42	174 36	69 38 F-4 98	
3+96 91 5°33.03	FO 21 74 19	174 90	74 69 FO 21	174 80	G 74 90	174 90	70 64 F-4 26	
3+71 91 4°39.32	FO 73 74 21	175 44	75 32 FO 12	175 33	FO 10 75 34	175 44	72 63 F-2 29	
3+46 91 3°45.60	FO 82 75 16	175 98	76 24 CO 26	175 87	FO 09 75 89	175 98	74 90 F-1 08	
25								
Brk 3+21 91 2°51.89	FO 25 76 26	176 51	76 35 FO 16	176 41	FO 12 76 39	176 51	76 69 CO 18	
20								
3+01 91 2°08.92	FO 14 76 39	176 93	76 97 CO 04	176 83	FO 23 76 70	176 93	77 66 C-0 33	
2+81 91 1°25.94	FO 30 77 06	177 36	77 36 G	177 26	CO 14 77 45	177 31	78 17 CO 86	
2+69 91 C6 FC 24	FO 72 77 03	177 75	77 83 CO 08					
2+61 91 0°42.97				177 57	CO 32 77 99	177 67	78 82 C-1 15	
30								
2+41 91 P.C.C. 0°00				177 90	CO 43 78 43	178 00	79 17 C-1 17	
33 39								
2+08 57				178 40	CO 42 78 92	178 50	79 39 CO 89	
13 33								

	Rough S/BK	C6 grade	C6	E	C6	C6 grade	Rough S/BK
EVC, 6+40	C2 73 65 72	163 04	64 20 C1 16	162 94	F0 07 62 97	163 04	59 89 F3 15
6+20	C5 94 71 45	165 57	66 23 C0 72	165 41	C0 09 65 60	165 51	62 77 F2 74
6+60	C6 32 73 93	167 61	67 89 C0 28	167 51	C0 15 67 76	167 61	63 59 F4 02
5+80	C1 74 71 03	169 33	69 38 C0 05	169 23	C0 14 69 47	169 33	65 50 F3 83
5+60	C5 54 76 23	170 69	70 36 F0 33	170 57	C0 11 70 80	170 69	67 14 F3 55
5+40	C5 25 76 92	171 67	71 37 F0 30	171 57	C0 09 71 86	171 67	67 46 F4 21
20							
BVC, 5+20	C3 16 75 44	172 28	72 27 F0 01	172 18	C0 37 72 65	172 28	67 31 F4 97
23 09							
4+96 91	C3 55 76 32	172 77	72 94 C0 17	172 68	C0 12 72 89	172 77	67 23 F5 54
4+71 91	C2 02 75 32	173 30	73 40 C0 10	173 21	C0 08 73 38	173 30	68 06 F5 24
4+46 91	F0 13 73 70	173 83	73 95 C0 12	173 74	F0 04 73 78	173 83	69 16 F4 67

C6 Rad = 30'

SW Return

C6 grade

EC San Bernardo 91° 08'		177 75	77 83 Co 08
5/6	75° 56' 30"	177 90	78 24 Co 34
2/3	60° 45'	177 95	78 29 Co 34
1/2	45° 34'	Fo 03 77 87	77 90 78 16 Co 26
1/3	30° 22' 30"	177 71	77 21 C
1/6	15° 11	177 45	77 88 Co 43
BC La Paz		177 06	77 77 Co 71

	Rough 5'/K	C6 grade	C6
		154 27 +56 05	meet existing end 154 27
Pavedge 7+03 77			
N wly Prop 6+93 12	C5 15 63°	156 21 +57 85	56 29 Co 08
6+60	C2 97 63 77	160 50 +60 80	61 88 C1 38

C6 Rad = 30' SE Return

C6 grade

EC San Bernardo 92° 22' 30"		179 10	79 28 Co 18
5/6	76° 59'	179 00	79 32 Co 32
2/3	61° 35'	178 80	79 36 Co 56
1/2	46° 11'	Co 5 79 88	178 55 79 22 Co 67
1/3	30° 48'		178 20 79 07 Co 87
1/6	15 24'		177 85 78 49 Co 64
BC La Paz			177 39 78 11 Co 72

	C6	C6 grade	Rough 5'/K
E-54			
156 35			
		155 91 meet existing end +56 82	
157 30	Co 02 56 20	156 18	53 25 F3 43
160 65	Co 30 60 62	160 32 +60 70	57 05 F3 65

Lt=West

La Paz

		Rough 5 BK	C6 grade	C6
2+47 74	16°18.11	C1 65 57 70	156 05	55 73 FO 32
2+22 74	14°29.32	C1 64 56 78	155 14	53 16 CO 02
1+97 74	12°40.53	C1 47 55 40	154 23	54 45 CO 22
1+72 74	10°51.74	C2 34 55 66	153 32	54 08 CO 76
1+47 74	9°03.95	C1 88 54 29	152 41	52 64 CO 23
Ork E.V.C. 1+22 74	7°15.16	C.O 87 52 37	151 50	51 00 FO 50
0+97 74	5°26.37	C2 04 52 67	150 63	50 49 FO 14
0+72 74	3°37.58	C2 00 51 85	149 85	50 22 CO 37
0+47 74	1°48.79	C2 63 52 04	149 41	49 89 CO 48
25 BC. 0+22 74	0°00'	C2 36 51 45	149 09	49 33 CO 24
0+00			148 83	existing ent

St

2 - 54	
156 21	
155 31	
154 41	
153 51	
152 61	
151 71	
150 83	
150 01	
149 42	
148 94	
148 80	

Rt=East

58

C6	C6 grade	Rough 5 BK
FO 43 56 01	156 44	57 59 C1 15
CO 50 56 06	155 56	57 31 C1 75
CO 28 54 96	154 67	56 72 C2 05
FO 13 53 65	153 78	55 40 C1 62
CO 15 53 04	152 89	54 31 C1 42
CO 12 52 12	152 00	52 98 CO 88
CO 06 51 18	151 12	6 BK 51 40 CO 48
CO 55 50 20	150.25	52 62 C2 37
FO 21 49 30	149 51	49 29 FO 22
CO 31 49 18	148 87	49 40 CO 23
existing ent	148 47	

	Lt. West					Rt. East			
	Rough 5'10K	C6 grade	C6			C6	C6 grade	Rough 5'10K	
E.V.C. 4+75 7°27.62	CO 41	66 27	165 66	65 24 CO 28	℄ -54 165 75	CO 19	66 11	165 92	65 88 FO 54
4+50 5°11.15	CO 21	65 17	164 26	64 39 CO 13	164 35	CO 17	64 69	164 52	64 72 CO 20
4+25 2°54.67	C1 09	64 05	162 96	62 74 FO 22	163 05	FO 22	63 00	163 22	63 20 FO 02
C=24 99									
4+00 0°38.20			161 78	61 29 FO 49	161 87	FO 08	61 96	162 04	
7 04									
B.C. 3+92 96 0°00' 10'BK	C2 44	63 91	161 47	60 05 F1 42	161 56	CO 02	61 75	161 73	62 23 CO 80 10'BK
17 96									
3+75	C1 58	62 31	160 73	60 80 CO 07	160 82	CO 24	61 23	160 99	61 81 CO 82
E.V.C. 3+50	C2 44	62 21	159 77	59 41 FO 36	159 86	C0 12	60 15	160 03	60 88 CO 85
27 25									
3+22 77	C2 68	61 46	158 78	58 58 FO 20	158 90	CO 47	59 57	159 10	60 70 C1 60
27 24									
E.C. 2+95 52 19°47.00	C3 45	61 25	157 80	57 64 FO 16	157 94	CO 31	58 48	158 17	59 80 C1 63
22 28									
2+72 74 18°06.90	C4 18	61 14	156 96	56 34 FO 62	157 11	CO 44	57 80	157 36	59 17 C1 81

Lt = West

	Rough 5'BK	C6 grad.	C6
C6 BC Lt. 6+71.84	FC 15 76 91	177 06	77 77 Co 21
C6 BC Lt. 6+70.67			
6+42.66	Co 05 75 41	175 36	76 10 Co 74
27.86			
EC. 6+14.80 20° 10.50	F1 57 72 14	173 71	74 25 Co 54
14.80			
6+00 18° 50.00	F0 93 71 24	172 84	73 50 C-0 46
5+75 16° 33.52	F0 12 71 30	171 42	71 89 Co 47
5+50 14° 17.06	Co 47 70 47	170 00	70 40 Co 40
5+25 12° 00.57	Co 18 68 74	168 56	68 76 Co 20
5+00 9° 44.01	Co 09 67 21	167 12	67 21 F0 11

Rt = East

	C6	C6 grade	Rough 5'BK
E-54			
176 95			
	Co 75 78 11	177 39	78 68 C1 29
175 39	Co 94 76 69	175 75	77 14 C1 39
173 94	Co 59 74 70	174 11	75 19 C1 08
173 05	Co 81 74 03	173 22	74 67 C1 45
171 59	Co 20 72 46	171 76	72 93 C1 47
170 13	F0 18 70 82	170 30	69 68 F0 62
168 67	F0 12 68 73	168 84	68 00 F0 84
167 21	Co 25 67 63	167 38	67 21 F0 17

D. Smith
J. Hoover
R. Taylor
J. Schlein

INDEXED
YER
DEC 8
1954

WO 77 32141 61

Stake Alley Blk 31

Ocean Beach

	Lt = NEly 3' Blk	Rt = SWly 3' Blk	NWly Ebers 6+00	✓ exists	✓ 6/30/53 exists
2+52	CO 63 34 58 33 95	33 95 34 38 CO 43	5+80	F1 15 44 60 45 75	45 74 46 63 CO 29
			5+60	F1 18 44 54 45 73	45 73 46 01 CO 28
2+20 Brk	FO 02 32 68 32 70	32 70 32 81 CO 11	5+40 BVC	F1 01 44 21 45 22	45 22 45 98 CO 76
1+80	FO 17 31 58 31 75	31 75 31 66 FO 09	5+08	FO 32 43 65 43 97	43 97 43 43 FO 54
1+60	C 30 80 30 80	30 80 31 41 CO 61	4+76	CO 04 42 76 42 72	42 72 43 13 CO 41
1+30	CO 13 29 28 29 85	29 85 29 86 CO 01	4+44	FO 08 41 38 41 46	41 46 41 68 CO 22
1+10 ⓢ 21	CS 32 29 52 24 20 1e			1' Blk	
1+00	CO 34 29 24 28 90	28 90 29 15 CO 25	4+12	CO 14 40 35 40 21	40 21 40 71 CO 50
0+70	CO 23 28 18 27 95	27 95 28 64 CO 69	3+80	1' Blk CO 98 39 94 38 96	38 96 38 77 FO 19
0+40 Brk	CO 42 27 42 27 00	27 00 27 55 CO 53	3+48	CO 25 37 95 37 70	37 70 37 92 CO 22
0+20	2' Blk CO 57 26 71 26 14	26 03 26 78 CO 75	3+16	0.08 Blk CO 02 38 42 36 45	36 45 36 92 CO 47
S. Ely Sunset Cliff. 0+00	✓ exists 25 28	25 06 ✓ exists	2+84	CO 77 35 87 35 20	35 20 35 22 CO 02 2' Blk
BM	25 03	Zone SWBP Sunset Cliffs 24 03 NWBP Saratoga — Santa Monica			

Lt = Wly. Stake — Francis St. — Rt = Ely — WO# 31837 — 62

Curb Stakes Sept 30-63 H.S. Sisson Gerber — Ocean View to Webster — Chipman Parker Kelley

		Rough 5'10K	CG grade	CG			Offsets Back Face CG	CG grade	Rough 5'10K
2+00			61.10	3.84 / 3.96 / F0.12		61.25	3.24 / 3.29 / C0.05	61.60	
1+80		C1.77 62.67	60.90	3.01 / 2.98 / C0.01		61.02	2.57 / 2.57 / C0.02	61.35	64.79 C3.44
1+60			60.35	3.59 / 3.38 / C0.21		60.45	3.19 / 3.13 / C0.06	60.75	
1+40		C-2.76 62.11	59.35	4.59 / 4.23 / C0.36		59.52	4.04 / 4.07 / F0.03	59.90	63.87 C3.97
TP		5.61	53.94	0.96	58.33				
1+20			58.15	1.14 / 0.96 / C0.18		58.32	0.59 / 0.82 / F0.23	58.70	
1+00		C-4.48 61.18	56.50	2.79 / 2.84 / F0.05		56.70	2.19 / 2.85 / F0.66	57.10	62.67 C5.57
0+80			54.70	4.59 / 4.96 / F0.37		54.80	4.19 / 4.81 / F0.62	55.10	
0+60 BVC		C-7.72 60.12	52.40	6.89 / 7.82 / F0.93		52.60	6.39 / 6.70 / F0.31	53.00	56.03 0.01
0+30	0.01K	C2.50 51.25	48.75	10.54 / 11.29 / F0.75		49.03	9.84 / 10.20 / F0.36	49.45	57.19 C7.74
0+00			45.10	14.19 / 14.23 on CG		45.47		46.10	13.19 / 13.20 on CG
BM Fd Curb Stakes		18.21	59.29	1.08	Lt 7.47 Ft Ocean View & Francis				
BM				58.78	SW 13' Mon. Franklin & Francis				

	Rough s'tion	C6 grade	24 - Wly C6	-054 £	Rt - Ely C6	C6 grade	Rough s'tion
0+40	C0 50 58 55	58 05	5.89 5.53 C0.36	58 22	5.36 5.13 C0.23	58 58	62 09 C3 51
0+10 EC Ely.		58 39	5.55 5.17 C0.11	58 54	Pl 59.58 4.36 4.08 C0.28	½ 59.30 4.64 4.44 C0.20	½ 59.03 4.91 5.12 Fo.21	58 89 5.05 5.02 Co.03	61 97 C3 08
0+00 Wly Prop	C0 09 58 59	58 50 out		58 65				59 00 out	
1+25 ± St. to East	C0 07 58 83	58 75	5.19 5.08 C0.11	58 90					
3+89 19 Sly P.L.	C0 25 59 35	59 00 out		59 15				59 50 out	
3+79 19 EC Ely		59.12	4.82 4.46 C0.36		Pl 59.80 4.14 3.15 C0.99	½ 59.65 4.32 3.82 C0.37	½ 59.60 4.34 4.19 Fo.15	59 62 4.03 4.57 Fo.26	62 19 C2 57
3+40	C0 13 59 73	59 59	4.35 4.13 C0.22	59 74			3.85 4.25 Fo.40	60 09	62 40 C2 31
3+00	C0 08 60 14	60 06	3.88 3.91 Fo.03	60 21			3.38 3.75 Fo.37	60 56	62 51 C1 95
2+60	C1 23 61 76	60 53	3.41 3.55 Fo.14	60 68			3.91 3.03 Fo.12	61 03	63 6 C2 6
2+20 EVC	C1 46 62 44	61 00	2.91 3.03 Fo.09	61 15			3.44 3.43 C0.01	61 50	65 44 C3 94
		6394							

		Rough	C6 grade	C6		Rt=Bly C6	C6 grade	Rough
~~3+80~~								
3+00		3.94 F16 @ 24 ② -06	56 00.	3.68 4.28 F0.60.	56 20.	3.08 3.96 F0.38.	56 60.	47 F87 @ 13 ⑤ +10
~~2+80~~	2+70 culvert ℄ 15"	C2 29	45 49	5 Staked	43 30 ic		45 00 ic Staked	55' out ℄ 47 05 C2 05
2+60		4.46 F96 @ 14 ⑤ +01	56 20.	3.48 3.71 F0.23.	56 40.	3.88 3.28 F0.38.	56 80	46 F102 @ 16 ⑤ -03
2+20		F1 @ 15 55 -06 ⑤	56 40.	3.28 3.42 F0.21.	56 60.	3.68 2.84 C0.06.	57 00.	53 F 42 @ 6 -03 ⑤
TP		4.39 C0 89	59.68	6.05 7.44 7.42 C0.02.	57.29			
2+00	0.19 IN	57 39	56 50.		56 70.	6.84 6.65 C0.19.	57 10	55 68 F1 42
~~1+80~~								
1+60 ~~1+58~~	3 IBK	C0 38 57 08	56 70	7.34 7.15 C0.09	56 90.	6.64 6.71 F0.10.	57 30.	58 89 C1 59
1+20		F1 37 55 78	57 15	6.79 6.86 F0.07.	57 35.	6.22 6.38 F0.06.	57 72.	60 38 CR 66
0+80		C0 23 57 83	57 60	6.34 6.09 C0.25.	57 78.	5.74 5.96 C0.03.	58 15.	62 14 C3 99
			63.94					

	Lt. Wly				Rt. Ely		
	Rough	C&grade	CS	℄	CS	C&grade	Rough
2+20	C-2.24 54.92	52.68	7.00 / 6.91 / C0.09	52.85	6.45 / 6.51 / F0.06	53.23	61.35 C-8.12
2+00	C-3.09 56.21	53.62	6.06 / 6.01 / C0.05	53.80	5.50 / 5.48 / C0.02	54.18	61.10 C-6.98
1+80	C-2.64 56.96	54.32	5.36 / 5.32 / C0.04	54.01	4.77 / 4.95 / F0.18	54.91	61.15 C-6.24
1+60	C-2.30 57.08	54.78	4.90 / 4.94 / F0.04	54.98	4.30 / 4.16 / F0.14	55.38	62.03 C-6.65
1+40 B.V.C.	C-1.80 56.80	55.00	4.88 / 4.80 / C0.08	55.20	4.08 / 3.91 / C0.17	55.60	62.64 C-7.04
1+10	F0.30 54.85	55.15	4.53 / 4.49 / C0.04	55.35	3.93 / 3.70 / C0.23	55.75	62.04 C-6.29
0+80	F-1.60 53.70	55.30	4.38 / 4.22 / C0.16	55.50	3.78 / 3.80 / C0.18	55.90	58.67 C-2.74
0+40	F1.75 53.75	55.50	4.18 / 4.21 / F0.03	55.70	3.58 / 3.72 / F0.14	56.10	59.49 C-3.39
0+00 3+59.20 P.I. Line	F5.07 50.63	55.70	3.98 / 4.02 / F0.04	55.90	3.88 / 4.01 / F0.13	56.30	54.55 F1.75
3+40	F11.4 Ⓒ 17.1 44.2 Ⓢ -0.2	55.80 / 59.68	3.88 / 4.16 / F0.28	56.00	3.28 / 3.70 / F0.42	56.40	52.0 F 4.40 CS +0.2 Ⓢ

Lt. Wly

Rt. Ely

	Rough	C6 grade	C6			C2	C6 grade	Rough
10+53.48 on Hab+D.T. & Project N.L. Webster's B.M.			295	47.88	(47.78)			
2+99 97 Sly Prop		47 00			47 00		48 00	
		3.08. 3.67 F 0.59.	3.70. 4.01 F 0.31.	3.90. 4.25 F 0.35.				
2+89 97 BC.	C0 38 48 15	47 77.	47 15	46.95	47 80.	S.L. Webster 18.55 2.60. 2.55 C0.54.	18.30 2.65. 1.92 C0.73.	48 40. 2.45. 2.20 C0.25. 50 64 C2 26
TP	3.67	50.85	13.50	47.18				
2+80	C2 26 50 80	48 54	11.14. 11.23 F 0.09.		48 72.		10.68. 10.57 C0.11.	49 00. 51 24 C2 24
2+60	C3 85 53 93	50 08.	9.60. 9.79 F 0.19.		50 22.		9.11. 9.34 F 0.23.	50 57. 53 34 C2 77
2+40	C2 47 53 97	51 50.	8.18. 8.46 F 0.28.		51 66.		7.66. 7.95 F 0.29.	52 02. 57 38 C5 36
		5.78						

WO# 32210, 67
7/30/53

Stake Keats

	Star Rough	Ht. My C6 grade	C6	
2+25	1.14 C0.57	0.57	0.58 C0.01	-.63/100
2+00	0.44 F0.11	0.60	0.45 F0.15	-.61/100
1+75	-0.53 F.1.47	0.62	0.43 F0.19	-.59/100
1+50	-0.85 F.1.50	0.65	0.44 F0.21	-.57/100
1+25	-0.80 F.1.47	0.67	0.29 F0.38	-.56/100
1+00	-0.80 F.1.50	0.70	0.26 F0.44	-.54/100
0+75	-1.05 F.1.77	0.72	0.43 F0.29	-.53/100
0+50	-0.71 F.1.46	0.75	0.56 F0.19	-.51/100
0+25 C6 BC. 43 Rad. ON Prop	0.14 F0.63	0.77	0.43 F0.34	-.50/100
0+00 Fly Scott	0.11 F0.11	0.82		
BM			-2.44	Int Mon Keats & Shafter

Scott to Shafter

	Ht = 5'	C6	C6 grade	Star Rough
	-.042			
0.37	-.63/100	0.00 F0.57	0.57	1.12 C0.55
0.41	-.61/100	0.15 F0.45	0.60	0.37 F0.18
0.46	-.59/100	0.09 F0.53	0.62	-.013 F0.75
0.50	-.57/100	0.01 F0.64	0.65	-.020 F.0.85
0.54	-.56/100	-.023 F0.90	0.67	.013 F.0.80
0.59	-.54/100	-.001 F0.71	0.70	.06 F0.1
0.63	-.53/100	0.02 F0.70	0.72	0.45 F0.27
0.67	-.51/100	0.21 F0.54	0.75	.052 F.0.23
0.71	-.50/100	0.28 F0.49	0.77	0.53 F.0.24
0.79			0.82	0.83 C0.1

Lt = N/y

	Rough	Cbgrade	C6
NE Ret Keats + Scott			
Prop	0 89	0 22	F0 67
2/3	0 84	0 39	F0 45
1/3	0 79	0 44	F0 35
Keats BC	0 77	0 43	F0 34
NW Ret Keats + Scott			
	1 17 N Prop	0 85	F0 32
	1 12 S Prop	1 95	C0 83
Prop		0 55	1 01 C0 46
2/3		0 50	0 51 C0 01
1/3		0 50	0 32 F0 18
BC (16° 09)		0 52	0 34 F0 18
3+00 W/o Shafter	1 1 C0 6	0 52	
2+75 43' Rad CL BC		0 52	0 34 F0 18
2+50	0 51 F0 04	0 55	0 51 F0 04

Rt = S/y

	C6	Cbgrade	Rough
E -0 42			
SE Ret Keats + Scott			
S/y EC, Scott	0 97	0 52	F0 45
3/4	0 90	0 55	F0 35
1/2	0 84	0 66	F0 18
1/4	0 80	0 24	F0 56
BC, Keats	0 77	0 28	F0 49
Prop		0 55	1 01 C0 46
2/3		0 51	C0 01
1/3		0 32	F0 18
BC,		0 34	F0 18
0 00			
0 29			
0 33			
SW Ret Keats + Scott			
EC, Scott	1 22	0 73	F0 47
3/4	1 16	0 75	F0 41
1/2	1 09	0 62	F0 47
1/4	1 09	0 69	F0 40
BC, Keats	1 10	0 49	F0 61
Rx (0+50)	1 62 +25 = 3	0 97	F0 86
Prop	1 40	C0 93	0 47
2/3	0 29 F0 30	0 49	
1/3	-0 24 F0 76	0 52	
BC,	0 20 F0 32	0 52	
		0 47	1 52 C1 05
	0 20 F0 32	0 52	
	0 03 F0 52	0 55	1 03 C0 48

Scott St

	Lt = Ely	℄	Rt = Wly
		CS grade	CS grade
Meet 1+08		1.16	1.37
0+80	0.86 FO 2.1	1.17	1.41 1.21 FO 0.20
0+60	0.84 FO 1.8	1.12	1.37 0.70 FO 0.67
EC. 0+25	0.52 FO 4.5	0.97	1.22 0.73 FO 0.49
E Shafter 3+35 Plug			-3.28 -0.86 C-2.42
3+00			-3.42 -0.67 C-2.75
E SH #1 2+75		1.35 C4.21	-3.52 -0.38 C-3.14 ic 0.29 top F 0.67 rim
2+62 Lt Lt	-2.86	0.08 C-2.94	
2+50			-3.62 -0.53 C-3.09
2+25			-3.72 -0.72 C-3.00
2+15 Rt Lt	-3.06	1.09 C-3.15 1.28 C-4.37	

5th Lt

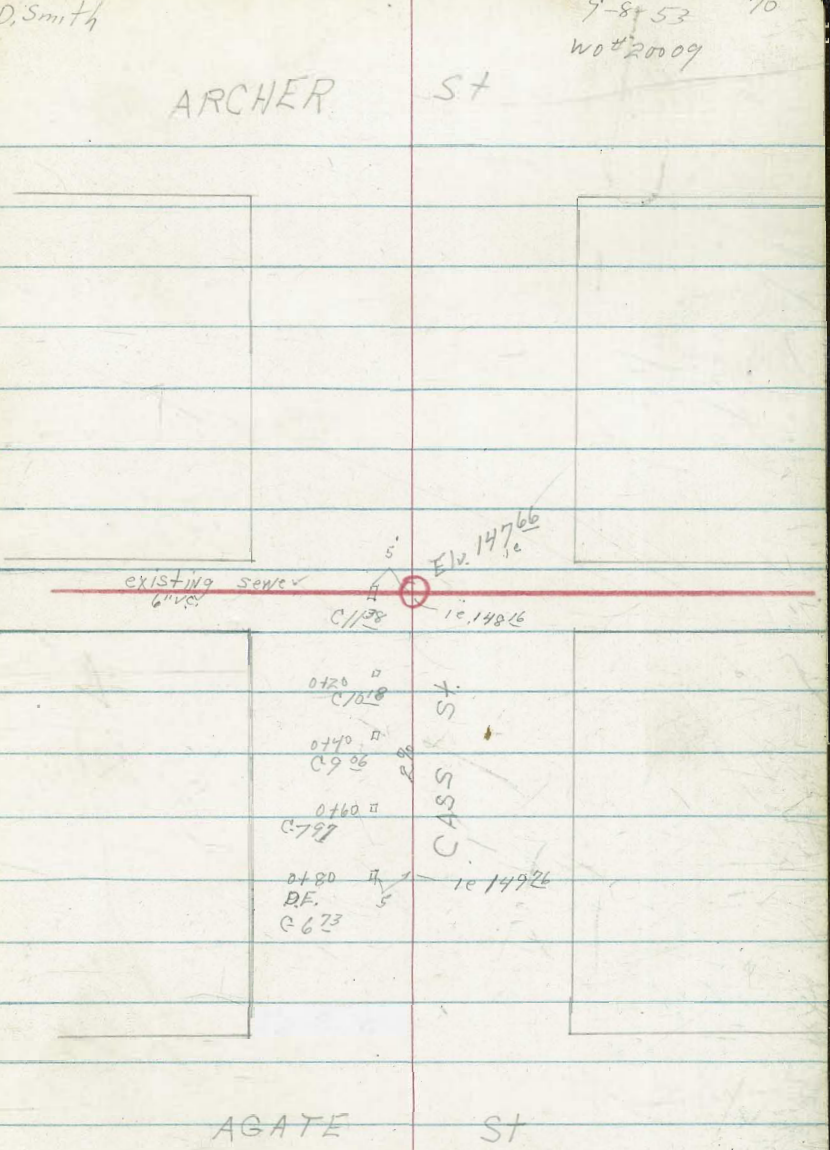
2+00	-3.82	-0.49 C-3.33
1+75	-3.92	-0.55 C-3.37
1+65 Rt & Lt (3)(7)	-3.26	-0.50 C-2.76 -0.07 C-3.19
1+50	-4.02	-0.58 C-3.44
1+25	-4.12	-0.75 C-3.37
1+15 Rt & Lt (2)(6)	-3.16	-0.20 C-2.26 -0.09 C-3.07
1+00	-4.22	-0.50 C-3.72
0+75	-4.32	-0.60 C-3.72
0+65 Lt O	-3.36	-0.83 C-2.53
0+50	-4.42	-0.48 C-3.94
0+25	-4.52	-0.50 C-4.02
0+00	-4.62	-0.49 C-4.13
0-35 Make corn & Scott	-4.76	✓

Proposed Sewer 80' S/y Alley
Cass Btwn Archer & Agate

D. Smith

9-8-53
Wo # 20009

70

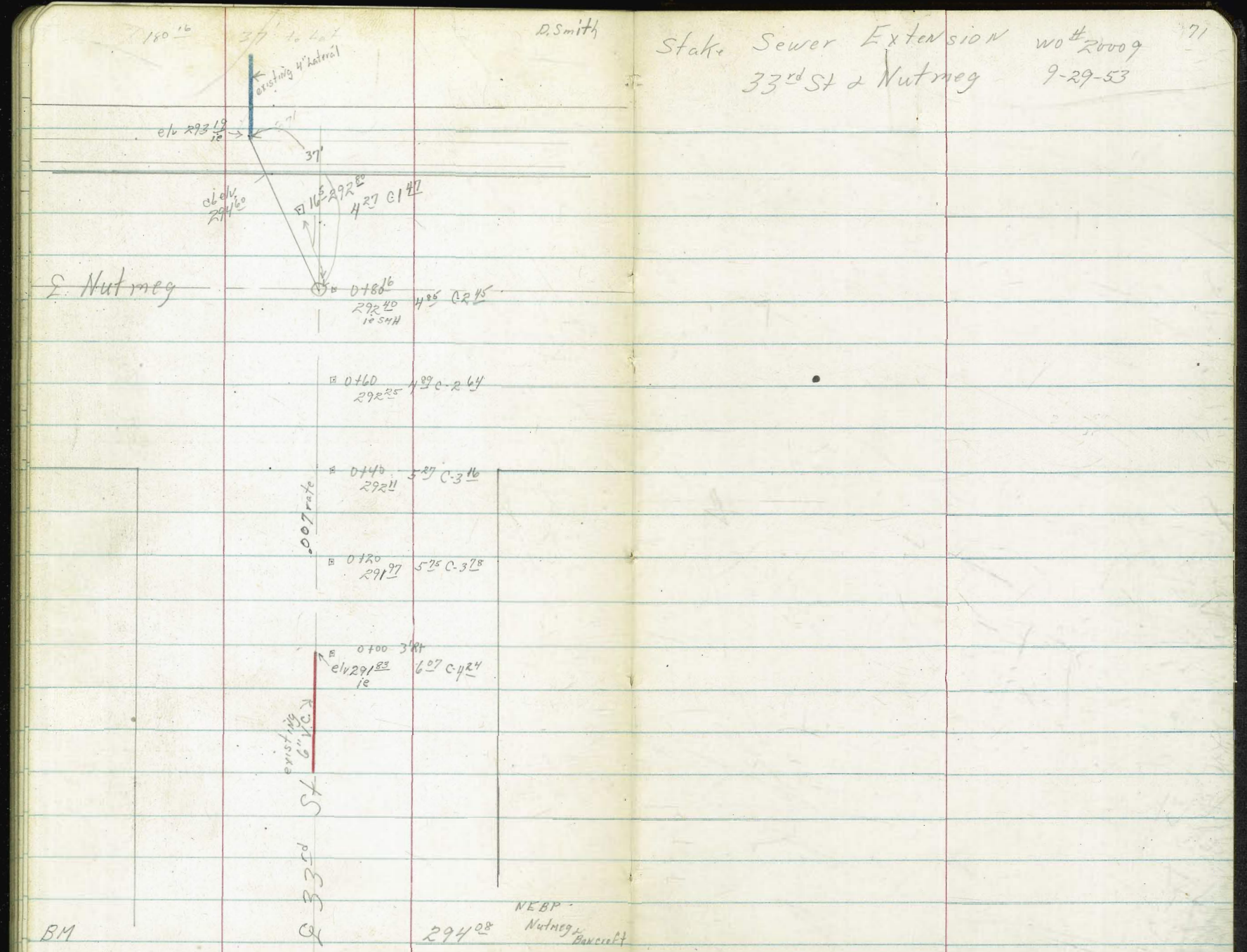


159.54 148.16 C 11.38
158.74 148.56 C 10.18
158.02 148.96 C 9.06
157.33 149.36 C 7.97
156.69 149.76 C 6.73

D. Smith

Stake Sewer Extension W.O. # 20009

33rd St & Nutmeg 9-29-53



Wo# 32139

D. Smith
J. Rorer
R. Taylor
B. Rish

Stake Nashville St 2/9/54
50' by Morena Blvd to Tonopah

	Rough	C6 Grade	C6		C6	C6 Grade	Rough
					Sky		
1+34.94 4' Alley Rad. EC.		7.42	6.85	F0.57	F0.11	7.54	7.65
BC.		7.49	6.85	F0.64	F0.18	7.54	7.72
Prop Ely		7.55	6.98	F0.57 24/100	19/100 F0.14	7.04	7.78
Prop Wly		7.51	7.28	F0.23 2/10	15/100 F1.26	6.18	7.74
EC		7.45	7.28	F0.17	F0.16	7.52	7.68
1+11.94 4' Alley Rad. EC.		7.36	7.28	F0.08	F0.07	7.52	7.59
1+08	Co.60 7.95	7.35	7.17	F0.18	Co.09	7.67	7.58	6.62 F0.96
0+73	Co.43 7.68	7.25	7.21	F0.04	Co.15	7.63	7.48	7.30 F0.18
0+38 Brk	Co.53 7.69	7.16	6.92 F0.24	67/100	50/100 Co.06	7.45	7.39	6.72 F0.67
0+08 Prop BC								
0+07.5 BC. C6. Δ = 32°14'	Co.35 7.31	6.96	6.57 F0.39	55/1000	5/10 F0.14	7.17	7.31	6.67 F0.64
0+00 Δ = 57°46'		6.91	6.77 F0.14	58/100	5/10 F0.40	7.09	7.40	
End C6. Now.		6.89 ✓		51/100	5/10 F0.59	6.87	7.46	
BM			7.06	P.K. Morena Blvd. Ex. 3 Marks 46.5 left of Tan.				

72
5.104

	Rough	C6 Grade	C6 NH	Sky C6	C6 grade	Rough
4+93	$C0^{53}$ 8^{92}	8^{39}	8^{54} $C0^{15}$	$C0^{03}$ 8^{65}	8^{62}	7^{57} $F1^{05}$
4+58	$C0^{32}$ 8^{62}	8^{30}	8^{13} $F0^{17}$	$F0^{23}$ 8^{30}	8^{53}	7^{49} $F1^{04}$
4+23	$C0^{35}$ 8^{55}	8^{20}	8^{29} $C0^{09}$	$F0^{04}$ 8^{39}	8^{43}	7^{55} $F0^{88}$
3+88	$C0^{05}$ 8^{16}	8^{11}	7^{86} $F0^{25}$	$C0^{18}$ 8^{52}	8^{34}	7^{55} $F0^{79}$
3+53	$F0^{05}$ 7^{96}	8^{01}	8^{20} $C0^{19}$	$C0^{07}$ 8^{31}	8^{24}	6^{64} $F1^{60}$
3+18	$F0^{14}$ 7^{78}	7^{92}	8^{00} $C0^{28}$	$F0^{16}$ 7^{99}	8^{15}	6^{47} $F1^{68}$
2+83	$F0^{10}$ 7^{72}	7^{82}	7^{84} $C0^{02}$	$C0^{05}$ 8^{10}	8^{05}	6^{65} $F1^{40}$
2+48	$F0^{07}$ 7^{66}	7^{73}	7^{82} $C0^{09}$	$F0^{07}$ 7^{87}	7^{96}	6^{31} $F1^{65}$
2+13	G 7^{63}	7^{63}	7^{66} $C0^{03}$	$C0^{05}$ 7^{91}	7^{86}	6^{78} $F1^{08}$
1+78	$F0^{27}$ 7^{27}	7^{54}	7^{41} $F0^{13}$	$F0^{05}$ 7^{72}	7^{77}	6^{64} $F1^{13}$
1+43	$F0^{32}$ 7^{12}	7^{44}	7^{09} $F0^{35}$	$F0^{10}$ 7^{57}	7^{67}	6^{64} $F1^{03}$

N'ly

S'ly

	Rough	C6 grade	C6			C6	C6 grade	Rough
Tonopah E.C.		$8\frac{78}{}$	$7\frac{21}{}$ $FO\frac{87}{}$ $CO\frac{13}{}$	$\frac{E3}{100}$		$FO\frac{34}{}$ $8\frac{36}{}$	$8\frac{70}{}$	
$8\frac{44}{}$ $\Delta = 32°\ 14'$		$8\frac{60}{}$	$7\frac{88}{}$ $FO\frac{72}{}$ $CO\frac{28}{}$	$\frac{6}{10}$		$FO\frac{65}{}$ $8\frac{05}{}$	$8\frac{70}{}$	
$6\frac{68}{}$ $\Delta = 57°\ 46'$		$8\frac{51}{}$	$8\frac{54}{}$ $CO\frac{03}{}$	$\frac{62}{100}$		$FO\frac{42}{}$ $8\frac{28}{}$	$8\frac{70}{}$	
$8\frac{44}{}$ $\Delta = 90°$								
C6 $5722\frac{93}{}$ B.C.	$CO\frac{54}{}$ $9\frac{01}{}$	$8\frac{47}{}$	$8\frac{49}{}$ G	$\frac{67}{100}$		$FO\frac{42}{}$ $8\frac{28}{}$	$8\frac{70}{}$	$8\frac{24}{}$ $FO\frac{46}{}$

S ½

	Slope Rough	Cb grade	Cb
3+96 end	C1 04 8 53	7 49	11 03 C3 54
3+68	C3 12 10 69	7 57	8 22 C0 65
3+33	C1 36 9 04	7 68	7 83 C0 85
2+98	F0 17 7 61	7 78	7 87 C0 99
2+63	F0 28 7 61	7 89	7 98 C0 99
2+28	F0 02 7 97	7 99	8 08 C0 09

N ½

Cb	Cb grade	Slope Rough
C0 30 7 79	7 49	8 26 C0 77
C0 16 7 73	7 57	8 25 C0 68
C0 12 7 80	7 68	8 47 C0 78
C0 05 7 83	7 78	8 14 C0 36
G 7 89	7 89	7 59 F0 30
F0 13 7 86	7 99	7 21 F0 28

Stake Water Main 6"CI
Lehigh St

1+93	4 99	7 34 C-2 40
1+58	5 04	7 40 C-2 36
1+23	5 15	7 45 C-2 30
1+00	5 21	7 44 C-2 23
0+88	~~5 25~~	
0+68	5 38	7 63 C-2 25
0+48	5 64	
0+28	6 04	7 95 C-1 91
0+13 & Fire Hyd		FO 68 8 87 9 55 10 base Stock.
0+08	6 34	8 19 C-1 85
0+00 w/y Tarapah		
0-20 make connection		

4+00	4 31	7 89 C-3 58
3+68	4 41	7 72 C-3 31
3+33	4 52	7 60 C-3 08
2+98	4 63	7 57 C-2 95
2+63	4 73	7 50 C-2 77
2+28	4 83	7 40 C-2 57

WO# 21109 Stake

D Smith
J Rorg
B Fish
R Taylor

Storm Drain
18" RCP
San Elijo & Jennings

Stakes 5 Lt

4/15/54

1+59.29 BC,

43.09

8.68 C-5.59

INDEXED
DER
DEC 7 1954

1+30

44.95

9.59 C-4.64

1+00

46.87
1.92

0.97 C-4.10

0+85.38 EC,

47.83

1.59 C-3.76

0+75.08 BC

48.47

2.19 C-3.72

0+50

50.07

4.02 C-3.95

0+25

51.67

5.68 C-4.01

0+00

53.27
1.6

6.19 C-2.92

56.32
Grade

6.19 FO 1.3

57.07
CS

BC CS

1/3

2/3 Evl

57.11 — 6.19 FO.92

57.27 — 6.11 FI.16

57.48 — 7.04 FO.44

57.70 — 7.29 CO.29

BM

596.5 — SW BP San Elijo & Kellogg

3+14.03 EBox INT EBroadway

3+05.57 EC,

2+96.23

2+87.20

2+79.06

2+70.23 BC

2+50 Evl,

2+40 Brks

2+30 BVC

1+93.55

1+81.77 BC

1+68.53 EC

Stakes 5 Lt

78

35.30 8.01 C-2.71

35.44 8.43 C-2.99

35.80
33

8.84 C-3.04

36.13
37

9.52 C-3.39

36.45 0.14 C-3.69

3 Brk

36.72
33

0.27 C-4.05

37.53
41

2.36 C-4.83

37.98 2.87 C-4.89

38.55 3.53 C-4.98

40.90 5.60 C-4.70

2 Lt

41.67 5.99 C-4.32

2 Lt

42.51 7.27 C-4.76

WO #

D Smith
J Rorg
B Kish
R Taylor

1+59

1+30

1+00

0+85

0+75

0+50

0+25

0+00

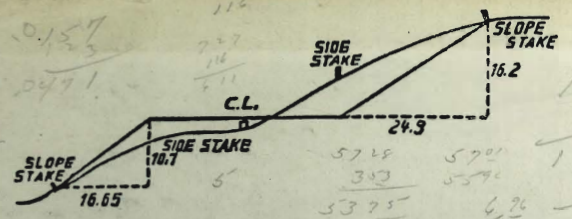
BC

1/3

2/3 Ev

BM

575
4 1/2
-1 37
11 1/2



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
HOLYOKE MASSACHUSETTS
NEW YORK CHICAGO BOSTON SAN FRANCISCO