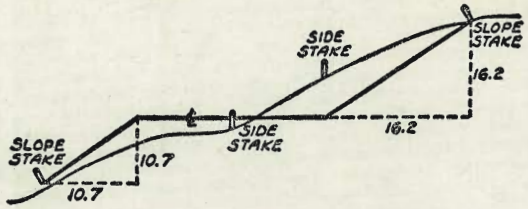
G-302



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

IMPROVED TABLES
AND
INFORMATION

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

2/28 - Gresham. 2 Hrs.

3/1 " 5 Hrs

INDEX - P-1

Index.

9+00	56.04 348.87 C 7.17	T.P.	12+50	8.93 351.77 C 7.16	
			12+42.38 = Prop. B.C.		
8+50	56.14 348.45 C 7.69		12+29.63 = Lug	8.74 351.60 7.14	
8+00	55.65 348.03 C 7.62		12+00	8.01 351.35 C. 6.66	
7+50	55.58 347.62 C 7.96		11+50	58.00 T.P. 350.93 C 7.07	
7+00	55.14 347.20 C 7.94	0.833 ℄	11+00	7.90 350.52 C. 7.38	
6+50	55.13 346.79 C 8.34		10+95.38 C.O.	7.88 350.50 C 7.38	7.88 356.50 C 13.8 to Finish Gr. grade Pave.
6+00	54.40 346.37 C 8.03	Pave Gr.	10+50	7.64 350.10 C. 7.54	
5+85.38 = C.O.	53.78 346.25 C 7.53	352.76	10+00	57.02 349.70 C 7.32	
5+50	53.68 345.97 C 7.71	T.P.	9+50	56.73 349.28 C. 7.45	

INDEXED
JUL 25 1955

		℄ Wellington	wlg. line Wellington
Stakes 10' Rt			
Storm Dr. Sta.	8+14.4 ~~8+17.38~~		
Sewer Lat. #2		4.93 345.95 C 8.98	5.25 348.00 C 7.25
Storm Dr. Sta.	4+08.4 ~~4+12.38~~		
Sewer Lat #1 =		5.19 343.44 C 7.75	5.12 344.20 C 7.72
13+42.13 = End.		6.32 352.55 C 7.77	
13+36.38 = Nlg Curb.		6.59 352.50 C 8.09	
13+00		9.93 352.18 C 7.75	

Curb Inlet - Nly. Side Tecolote 5 Road.
at Wellington
Stakes on ℄ line 17'w + 10'E. of ℄ C.I.

Wly end.		Ely end
0.20		0.58
360.06		360.09
C 0.14		E 0.49

18" Connection (9173-L)
Stakes on ℄ line - 9± off ℄ C.I.

Sly end.		Nly end
8.25		8.82
359.29		359.50
F 1.04		F 0.68

Nly end pipe EL. = 8.74 / 353.00 / C 5.74

Sly end pipe EL. =

4.4' - 18" pipe to north

Lug. Sta = 12+29.63

Tecolote Road Sewer
Sheet 9175-L

0+00 = Existing M.H. Wellington + Tecolote Road.

Stakes set 5' Rt. - running west.

3+00 =	62.75 352.58 10.17	
2+50	60.84 352.15 C-8.69	
2+00	61.07 351.72 C-9.35	
1+50	60.95 351.29 C 9.66	
1+00	60.85 350.86 C 9.99	
0+50	60.49 350.43 C 10.06	
0+00	9.89 350.00 C 9.89	

7+95 = stub end	63.11 355.77 C-7.34	
7+50	63.14 355.49 C 7.65	
7+00 = M.H. #2	63.21 355.18 C 8.03	
6+50	63.65 354.87 C-8.78	
6+00	63.60 354.56 C 9.04	
5+50	63.68 354.25 C 9.43	
5+00	63.89 353.94 C-9.95	
4+50	63.70 353.63 C 10.07	
4+00	63.68 353.32 C 10.36	
3+50 = M.H. #1	363.07 353.01 C-10.06	

Stake for paving

Alley Blk. 11 - La Jolla Strand,

C.H.S. 1-14-53

Boggs Oltman Powell — Sheet # 9242-L — W.O. 31346 — F.B. 2069 - P 41

0+00 = Wly. line La Jolla Blvd.

	Lt.	℄	Rt.	
2+10 75	X-2'	8.81		8.38	0.5 ◻
		68.35		68.35	
		C 0.46		C 0.03	
1+72 ℄	X 2'	9.83		9.72	X 2'
		69.82		69.82	
		C 0.01		F 0.10	T.P. 72.68
1+34 45	X-2'	70.97		1.41	◻-2'
		71.28		71.28	
		F 0.31		C 0.13	
0+96.3	X-2'	3.22		2.91	◻-2'
		72.75		72.75	
		C 0.47		C 0.16	
0+58 15	R 0.15 /'	4.99		4.26	◻-2'
		74.22		74.22	
		C 0.77		C 0.04	
0+20	◻-2'	6.39		5.81	◻-2'
		75.68		75.68	
		C 0.71		C 0.13	
0+00		76.45		76.35	

	Lt	℄	Rt.	52.76 T.P.
E.V.C.				
4+81 ℄	X 0.40	5.19		4.70	1.7 ~~Hub~~ X 0.35
		53.91		53.91	
		C 1.28		C 0.79	
4+61 ℄	X-0.50	8.21		9.59	
		56.45		56.45	N-0.80
		C 1.76		C 3.14	
4+41 ℄	X-0.60	60.45		60.48	
		58.48		58.48	N. 0.25
		C 1.97		C 2.00	
4+21 ℄	X-0.67	1.43		60.36	← T.P.
		60.01		60.01	N-2'
		C 1.42		C 0.35	
4+01 ℄ P.V.C.	X-0.85	2.58		1.24	N 2'
		61.03		61.03	
		C 1.55		C 0.21	
3+63 35	X-1.05	4.18		2.63	◻ 2'
		62.50		62.50	
		C 1.68		C 0.13	
3+25 ℄	X 1.20	6.17		5.60	
		63.96		63.96	N-0.22
		C 2.21		C 1.64	
2+87 05	◻-2'	5.56		5.15	
		65.42		65.42	N-0.19
		C 0.14		F 0.27	
T.P. 2+48 9	◻-2'	66.77		66.84	
		66.89		66.89	N. line
		F 0.12		F 0.05	

Alley Blk. 11.
La Jolla Strand.

D - 5' Rt. end of Lat.

6+17 Lt. = Sewer Lat #1.

B.M. = B.P. S.E. West Del Mar & Kalmar

5.09
EL. = 31.45
C 3.62
30.42

	Lt.	±	Rt.	
Del Mar. Ely. Line Vista				
6+41 E	31.51		31.51	
6+21 E Brk	5.97 34.31 C 1.66		5.86 34.31 C 1.55	D-0.50
38.74 T.R.				
5+86 E D 2'	40.32 39.21 C 1.11		40.30 39.21 C 1.09	X-2'
5+51 E D-2' T.R.	4 4.76 44.11 C 0.65		3.76 44.11 F 0.35	D-2'
5+16 E X-0.30	50.00 49.01 C 0.99		9.54 49.01 C 0.53	N-0.20

Storm Drain

Pacific Beach Dr. & Mission Blvd.

INDEXED

Sheet 10065-L

21" Conc. pipe along Mission Blvd.

1+21.16 = E.C.	-1.47 -4.35 C 2.88	
0+99.35 Mid Curve	-1.55 -4.45 C 2.90	
0+77.53 = B.C. Rx.	-1.67 -4.54 C 2.87	
Δ 45° Rx. 0+64.85 C.O.#	-1.78 -4.60 C 2.82	10' Sly. R.P. x
0+00 C.O.#	-4.65	

N.E. B.P. Pac. B. Dr. & Mission Blvd El = 1.739

S.W. Disk " " El = 1.61

2+50	-0.94 -3.75 C 2.81
2+25	-1.06 -3.86 C 2.80
2+00	-1.17 -3.97 C 2.80
1+75	-1.28 -4.08 C 2.80
1+50	-1.34 -4.19 C 2.85
1+75	-4.80

M.H. 57C't sly from P.B. Dr. ℄ 1.00

set Nails in poles

Elev. 10.0

M.H. 214'± sly from P.B. Dr. ℄ 1.00

Cont. on P. 12

4+75	+0.26 −2.76 N C 3,02		6+56.61 = end of pipe	−2.00
4+50	+0.07 □ −2.87 C 2.94		6+53.61 ℄ 3.E.C.	+0.97 X −2.101 C 2,98
4+25	−0.09 □ −2.98 C 2.89		6+36.15 ℄ 2	+0.91 X −2.07 C 2.98
4+00	−0.20 □ −3.09 C 2.89		6+18.70 ℄ 1	+0.87 □ −2.14 C 3.01
3+75	−0.50 N −3.20 C 2.70		6+01.25 B.C.	+0.95 □ −2.21 C 3,16
3+50	−0.53 −3,31 C 2.78		5+75	+0.72 □ −2,32 C 3.04
3+25	−0.55 −3,42 C 2,87		5+50	+0.63 □ −2,43 C 3,06
3+00	−0.66 −3,53 C 2,87		5+25	+0.46 * −2.54 C 3,00
2+75	−0,82 −3,64 C 2,82		5+00	+0.39 □ −2,65 C 3,04

P.B. Drive

18" Conc. pressure line from pump house Ely

Sheet 10065-L

		Cut from 8° Rt. Stub	Cuts from St. Y. disk M. Blvd. & P.B. Dr.
1+05 = Δ 5° Lt.			
1+00	▫	-1.28 -8.72 C 7.44	-1.61 -8.72 C 7.11
0+87.5	▫	-1.28 -8.95 C 7.67	-1.61 -8.95 C 7.34
0+62.5	▫	-1.43 -9.35 C 7.92	-1.61 -9.35 C 7.74
0+37.5		-1.38 -9.75 C 8.37	-1.61 -9.75 C 8.14
0+18.75		-1.40 -9.75 C 8.35	-1.61 -9.75 C 8.14
0+00 at pump house	⊕ on ℄	-1.09 -9.75 C 8.66	-1.61 -9.75 C 8.14

(1)

2+38.6 E.C.	-1.32 -4.65 C 3.33
2+31.2 B.C. ▫ 8° Rt.	-1.32 -4.67 C 3.35
2+25 ▫	-1.72 -4.70 C 2.98
2+12.5 ▫	-1.68 -4.80 C 3.12
2+00 ×	-2.18 -5.11 C 2.93
1+87.5 ×	-1.74 -5.41 C 3.67
1+75 N.	-1.41 -5.93 C 4.52
1+72.3 = Δ 5° Lt. N.	-1.37 6.05 C 4.68
~~1+62.5~~ *	-1.29 -6.55 C 5.26
1+61.3 = Δ N 5° Rt	
1+50	-1.15 -7.08 C 5.93
1+37.5	-1.14 -7.61 C 6.47
1+25	-1.19 -8.06 C 6.87
1+12.5	-1.24 -8.43 C 7.19

Drain Across Mission Blvd At Reed. Sheet 10065 L

0+583 = wly ob. Mission Blvd.

0+56.3	+0.76 −1.30 C 2.06	
0+37.6	+1.18 −1.36 C 2.54	
0+18.8	+1.18 −1.43 C 2.61	
= C.I. #1 0+00	+0.50 −1.50 C 2.00	

0-02 = Ely ob. Mission Blvd.

24" Collecting drain to Pump House

5 stations 22.54 each. 2.62 ft.

1+47.26 = C.O. #4		−0.81 −9.70 C 8.89
1+24.74		−0.59 −10.29 C 9.70
1+02.20		−0.30 −10.88 C 10.58
0+79.64		−0.29 −11.47 C 11.18
0+57.10	8' Lt	−0.43 −12.06 C 11.63
#3 = 0+34.56 = E.C.	8' Lt.	−0.24 −12.66 C 12.42
#2 0+23.04	8' Rt.	−1.09 −12.96 C 11.87
#1 0+11.52	8' Rt.	−1.09 −13.26 12.17
at pump house 0+00 = B.C.	8' Rt.	−1.09 −13.56 C 12.47

End. of pipe

3+00.26 = C.O. #2 — − 1.55 − 7.00 C-5.45 — 7' Rt. on ob.

2+80.26 — − 7.20

ob. inlet #3

2+60.26 = 8' Lt. — IN. — − 2.22 − 7.40 C-5.18 — − 2.22 8' Rt. − 8.60 out C-6.38

2+21.75 — (8' Lt.) — − 1.80 − 8.80 C 7.00

2 parts @ 21.75 each = 43.50

#3 = 2+16.76 = C.O. #3 — (6' Lt.) — − 1.66 − 9.00 C-7.34

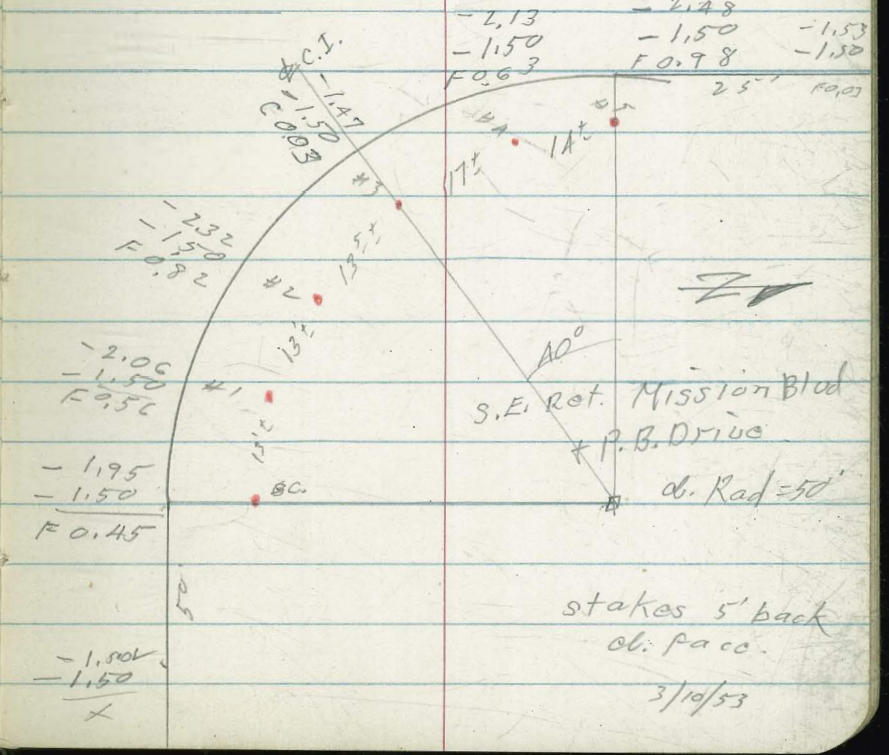
#2 = 1+93.60 — 8' Lt. — − 1.09 − 9.23 C-8.14

1+70.43 #1

3 parts @ 23.17 each = 69.51

− 0.82 − 9.46 C-8.64

− 1.50 − 1.50 X



INDEXED

Missouri St.

25 105A

From 580 East of Lamont to Lamont. Wly

0+00 = Ely line Acre Lot # 50

0+15 = start curb + Pavement.

	Rough	Curb		Curb	Rough	
N. line	10.46	9.77		0.29	13.48	N. line
1+80	109.52	109.52		110.10	110.10	
	C 0.94	C 0.25		C 0.19	C 3.38	
		9.48		9.83		
1+60		108.95		109.46		
		C 0.53		C 0.37		
	9.73	8.95		8.94	11.44	
1+40	108.27	108.27		108.70	108.70	
	C 1.46	C 0.68		C 0.24	C 2.44	
		8.03		8.36		
1+20		107.50		107.82		
		C 0.53		C 0.54		
N. +0.2						
P.O.C.	8.37	6.89		6.79	8.14	
1+00	106.62	106.62		106.82	106.82	
	C 1.75	C 0.27		F 0.03	C 1.32	
N. -0.1	5.60	4.60		4.94	5.43	
0+60	104.78	104.78		104.83	104.80	
	C 0.82	F 0.18		C 0.11	C 0.63	
0+43.3	RX	—		3.60	- el. E.C.	
				103.92	10' Rad.	
				F 0.32		
		2.86		—		
0+20 Ct.		102.93				
		F 0.07				
	2.58	2.75			3.33	
0+15	102.82	102.82		102.52	102.52	
	F 0.24	F 0.07			C 0.81	

Missouri

	Rough	curb		Curb	Rough
A+95 Rt X 5+00 line	6.13 114.96 C-1.17	C0.74		C0.55	8.21 X-1 115.57 C 2.64
A+55 Rt □ 4+60 line	4.45 114.30 C0.15	C0.20		C0.04	6.44 □ 114.91 +d= C1.53
A+20 □ -d=	2.87 113.65 F0.78	F0.46		F0.11	5.00 □ 114.25 +d= C0.75
3+80 □ +d=	1.68 113.00 F1.32	F0.47		F0.04	4.64 X 113.60 -d= C1.04
3+40	09.30 112.34 F3.04	F0.20		C0.51	4.80 □ 112.94 Line C1.86
3+00	1.30 111.69 F0.39	C0.60		C0.76	4.43 112.29 C2.14
2+60 N line	2.48 111.03 C1.45	C0.22		C0.73	3.33 111.63 C1.70
2+20 Evc	10.99 110.38 C0.61	0.78 110.38 C0.40		2.51 110.98 C-1.53	3.11 110.98 C2.13
2+00		0.32 110.00 C0.32		1.25 110.59 C0.06	

Missouri

1C

	Rough	curb		Curb	Rough
0+80	9.75 118.12 C1.63	7.89 118.12 F0.23		9.30 119.12 C0.18	21.33 X-2 119.12 C-2.21
0+					
P.U.C. N-d= 0+40	8.80 117.19 C-1.61	7.18 117.19 F0.01		8.58 118.19 C0.39	21.23 118.19 C-3.04
N-d= 0+10	8.47 116.40 C2.07	6.31 116.40 F0.09		7.09 117.40 F0.31	28.16 117.40 C2.76
0+00	115.92				116.81
Wly. Lamont					

Lamont St

	Rough	curb		Curb	Rough
Ely. Lamont.					
5+80	116.29 ✓	116.29 C0.07		116.89	116.89 ✓
5+40	6.78 115.63 C1.15	C0.50		C0.29	9.02 116.23 C2.79

P.V.C. 3+00	8.41 119.00 F0.59	8.76 119.00 F0.24		0.14 120.00 C0.14	2.81 120.00 C 2.81
2+70	8.25 119.15 F0.90	8.90 119.15 F0.25		20.27 120.15 C0.12	2.47 120.15 C 2.32
E.V.C. X 2+40 -1'	18.56 119.30 F0.74	8.98 119.30 F0.32		20.42 120.30 C0.12	2.38 120.30 C 2.08
2+					
2+00	18.60 119.38 F0.78	9.01 119.38 F0.37		0.27 120.38 F0.11	2.34 120.38 C1.96
1+					
1+60	8.39 119.21 F0.82	8.90 119.21 F0.31		0.21 120.21 X	1.66 X 120.21 -1' C 1.45
1+					
1+20	8.28 118.78 F0.50	8.25 118.78 F0.53		9.74 119.78 F0.04	21.66 119.78 C 1.88
1+					

P.V.C. 5+00	4.97 115.22 F0.25	4.80 115.22 F0.42		6.27 116.22 C0.05	8.28 116.22 C 2.06
E.V.C. 4+60	4.96 116.35 F1.39	5.88 116.35 F0.47		7.55 117.35 C0.20	9.41 117.35 C 2.06
4+					
4+20	6.30 117.36 F1.06	6.96 117.36 F0.40		8.68 118.36 C0.32	21.29 N 118.36 C 2.93
4+					
3+80	7.19 118.14 F0.95	7.90 118.14 F0.24		9.49 119.14 C0.35	21.51 119.14 C 2.37
3+					
3+40	7.80 118.68 F0.88	8.30 118.68 F0.38		9.95 119.68 C0.27	21.82 119.68 C 2.14
3+					

Missouri

7+					
P.U.C.	8.09	7.58	8.28	9.11	
7+40	107.40	107.40	108.40	108.40	
	C 0.69	C 0.18	F 0.12	C 0.71	
				X-1'	
N-O$^{\frac{1}{2}}$	0.30	8.97	7.68	12.03	
7+00	108.74	108.74	109.74	109.74	
	C 1.56	C 0.23	F 0.06	C 2.29	
N-O$^{\frac{1}{2}}$	0.83	9.92	1.23	3.68	
6+60	110.08	110.08	111.08	111.08	
	C 0.75	F 0.16	C 0.15	C-2.60	
X-O$^{\frac{1}{2}}$	2.56	1.09	2.46	4.75	
6+20	111.42	111.42	112.42	112.42	
	C-1.14	F 0.33	C 0.04	C 2.33	
X-O$^{\frac{1}{2}}$					
E.U.C.	3.19	2.35	3.90	6.20	
5+80	112.76	112.76	113.76	113.76	
	C 0.43	F 0.41	C 0.14	C 2.44	
5+					
X-O$^{\frac{1}{2}}$	4.19	3.38	5.02	7.44	
5+40	114.05	114.05	115.05	115.05	
	C 0.14	F 0.67	F 0.03	C-2.39	
5+					

O.C.B.C.	Rough	C.C.		C.C.	Rough
10+70	1.13	1.12			3.41
	101.30	101.30		102.30	102.30
	F 0.17	F 0.18			C 1.14
	1.45	1.48		2.72	3.48
10+50	101.57	101.57		102.57	102.57
	F 0.12	F 0.09		C 0.15	C 0.91
	2.99	2.81	corrected to meet	3.51	4.47
10+00	102.25	102.25		103.25	103.25
	F 0.16	C 0.06		F 0.26	C 1.22
	2.60	2.76		4.31	5.54
9+50	102.93	102.93		103.93	103.93
	F 0.33	F 0.17		C 0.38	C 1.61
E.U.C.	3.29	3.40		4.60	6.72
9+00	103.62	103.62		104.62	104.62
	F 0.33	F 0.22		F 0.02	C 2.10
8+					
	3.81	4.34		5.21	6.46
8+60	104.27	104.27		105.27	105.27
	046	C 0.07		F 0.06	C 1.19
8+					
	4.81	4.83		5.91	7.04
8+20	105.12	105.12		106.12	106.12
	F 0.31	F 0.29		F 0.29	C 0.92
8+					
					□+3'
	6.98	6.23		7.22	8.01
7+80	106.17	106.17		107.17	107.17
	C 0.81	C 0.06		C 0.05	C 0.84

INDEXED JEWELL - St.

Rough Grade

N.E.B.P. Jewell + Chalcedony 113.28

		Lt. Rough	Rt Rough
Sly Missouri		0.53	1.14
2+70		100.23	100.47
		C 0.30	C 0.67
Sly. Missouri			
2+60		~~99.99~~	~~0.71 100.25~~
			~~C 0.46~~
2+50		9.60	0.71
		99.70	99.98
		F 0.10	C 0.73
(1+99) Rt		8.77	100.15
2+00 Lt.		98.40	98.73
		C 0.37	C 1.42
1+50	D-0.12	7.52	8.06
		97.10	97.47
		C 0.42	C 1.59
1+00		5.70	6.96
		95.80	96.22
		F 0.10	C 0.74
0+50		4.80	6.11
		94.50	94.96
		C 0.30	C 1.15
0+10	+0.1	3.97	5.68
		93.46	93.96
		C 0.51	C 1.72
Nly Diamond		3.44	3.73
0+00		93.31	93.72
		C 0.13	✓

Jewell.

S.W. 3' tie back Lt. T. 100.57
Missouri + Jewell

		Lt Rough	Rt. Rough
Sly Chalcedony			
2+70		110.65	111.39
2+60 B.C.		0.68	2.30
		110.20	110.85
		C 0.48	C 1.45
2+15		9.11	10.49
		108.45	109.02
		C 0.66	C 1.47
1+70 E.V.C.		7.84	9.05
		106.69	107.19
		C 1.15	C 1.86
1+30	T.P.	5.74	7.04
		105.23	105.73
		C 0.51	C 1.31
~~1+10~~		~~105.23~~	
0+90		3.49	5.42 N 0.4
		103.99	104.49 10
		F 0.50	C 0.93
0+50 P.V.C.		2.53	4.02
		102.94	103.44
		F 0.41	C 0.58
0+10 B.C.		1.98	3.54
		101.98	102.48
		✓	C 1.06
Nly. Missouri		1.84	3.35
0+00		101.78	102.27
		C 0.06	C 1.08

Jewell St. - Curbs

	Wly. Cb. ℄	Ely. Cb.			
			All of E.C. Pt. 1+35	—	~~105.90~~
2+60 B.C.	99.99 F0.63	100.25 F0.48	1+30	—	—
2+50	F0.60	F0.46	1+25.	~~105.05~~	~~105.55~~
2+00	F0.14	F0.25	All of B.C. 1+22.5	5.09 104.98 C0.11	5.55 105.48 C0.07
1+70	C0.02	F0.28			
1+47.5	F0.30	F0.44	1+10	4.74 104.58 C0.16	4.97 105.08 F0.11
1+22.5 Nail in pole →	C0.76	F0.20	0+90	4.14 103.99 C0.15	4.32 104.49 F0.17
1+00	F0.08	F0.27	0+70	3.61 103.44 C 0.17	3.66 103.94 F0.28
0+50	C0.15	F0.28	0+50	3.07 102.94 C0.13	3.10 103.44 F0.34
0+10 = E.C. = Nly Diamond 0+00	93.46 C0.54	93.96 F0.06	0+10 = E.C.	101.98	102.48
			Nly Missouri 0+00 =		

Jewell St.

Ch. B.C. 2+60	0.54 110.20 C0.34	0.80 110.85 F0.05
2+45 Rt.		9.95 110.11 F0.16
2+15 Lt	8.40 108.45 F0.05	
2+07½ Rt.		8.61 108.65 F0.04
1+70	6.81 106.69 C0.12	7.39 107.19 C0.20
1+50	~~105.94~~	6.56 106.44 C0.12
Alley E.C.Lt. 1+47½	6.14 105.85 C0.29	—
1+45	~~105.76~~	—
Alley E.C.Rt. 1+37½		6.10 106.00 C0.10

INDEX

Jewell St → Alley Returns

Jul 25

G=105.68 Chalcedony St. G=105.82

N. 0.5 in alley

6.94 6.14
106.18 105.81
C0.76 C0.33

6.10 8.37
105.95 106.32
C0.15 C2.05

10' wide

5.38 5.09
105.47 105.10
F0.09 F0.01

G=105.38

10' wide

5.55 6.49
105.60 105.97
F0.05 C0.52

G=105.62

Missouri St.

G=96.91

7.33 6.74
97.41 97.04
F0.08 F0.30

6.24 6.58
96.89 96.52
F0.65 C0.08

G=96.61

G=97.28

6.98 9.00
97.41 97.78
F0.43 C1.22

6.59 7.44
96.91 97.28
F0.32 C0.16

G=96.98

Diamond

Curb Returns
Jewell & Chalcedony

INDEXED

S.E. Rot.

S.W. Rot.

Exist 174 Pipe #1 dia.

111.39 — 110.85 — B.C.

110.65 — 110.20

Jewell & Diamond

3.90 / 93.96 / F 0.06
3.68 / 93.72 / F 0.04
3.81 / 93.65 / C 0.22
3.86 / 93.75 / C 0.11
4.06 / 93.90 / C 0.16
94.01

N.E. Rot.

Jewell — #5 E.C. — #4 — #3 — #2 — #1 — B.C. — Diamond

N.W. Rot.

Restaked - (P-24)

4.00 / 93.46 / C 0.54
3.84 / 93.31 / C 0.53
3.62 / 93.20 / C 0.42
3.32 / 93.10 / C 0.22
3.16 / 93.03 / C 0.13
3.06 / 93.00 / C 0.06

Curb Rot. Jewell & Missouri

22

INDEXED

2.00 / 102.48 / F 0.48
2.11 / 102.27 / F 0.16
1.78 / 102.10 / F 0.32
2.65 / 102.05 / C 0.60
2.64 / 102.14 / C 0.50
2.17 / 102.14 / C 0.03
2.38 / 102.30 / C 0.08
2.61 / 102.30 / C 0.31

174 32

N.E. Rot.

Jewell — #5 E.C. — #4 — #3 — #2 — #1 — B.C. — Missouri St.

N.W. Rot.

2.02 / 101.98 / C 0.04
1.70 / 101.78 / F 0.08
1.51 / 101.60 / F 0.09
0.88 / 101.46 / F 0.58
1.40 / 101.32 / C 0.08
1.19 / 101.19

0.12 / 101.30 / F 0.18
0.95 / 101.14 / F 0.19
0.85 / 100.92 / F 0.07
0.12 / 100.70 / F 0.58
9.84 / 100.47
F 0.63
9.77 / 100.25 / F 0.48

S.E. Rot.

Missouri — #5 E.C. — #4 — #3 — #2 — #1 — B.C. — Jewell St.

S.W. Rot.

100.26

0.61 / 100.40 / C 0.21
0.04 / 100.42 / F 0.38
7.85 / 100.38 / F 0.53
9.67 / 100.23
F 0.56
9.36 / 99.99 / F 0.63

INDEXED

Storm Drain
Missouri St.

0+00 = N.+S. ck. face East end of Imp. Sheet 91 A5-L
stakes 6' Lt of ℄

End of pipe

2+00 — 98.10 / 96.75 / C 1.35

1+50 — 101.35 / 97.25 / C 4.10

1+00 — 102.25 / 97.75 / C 4.50

0+50 — 103.02 / 98.25 / C 4.77

0+01 ℄ : start pipe — 103.50 / 98.75 / C 4.75

0+00 = face of N.+S. ck.

Missouri — (5) Lats.

	Lt.	Rt.
4+60 - #7 Rt		15.92 / 109.92 / C 6.00
3+20 - #1 Lt	12.10 / 106.02 / C 6.08	
2+30 #2 Lt	11.45 / 105.54 / C 5.91	
2+10 #4 Rt		113.12 / 105.79 / C 7.33
1+10 #5 Rt		10.11 / 102.32 / C 7.79
0+55 #3 Lt	105.24 / 99.55 / C 5.69	
0+05 #6 Rt		103.28 / 97.90 / C 5.38

INDEX Returns

Lamont & Missouri

Lamont

E.C.

#3 — 5.84 / 115.84 / Meet ac. — 116.94 / Meet ac.

#2 — 23 / 116.08 / C 0.15 — 7.09 / 116.93 / C 0.16

#1 — 25 / 116.27 / F 0.02 — 6.90 / 116.92 / F 0.02

BC — 31 / 116.27 / C 0.04 — 6.93 / 116.91 / C 0.02

Prop — 36 / 116.29 / C 0.07 — 6.94 / 116.89 / C 0.05

Missouri

S.E. Rot.

N.E. Rot.

Missouri

6.31 / 116.40 / F 0.09 — E.C. — 7.09 / 117.40 / F 0.31

#4 — 6.93 / 116.21 / F 0.18 — 6.95 / 117.08 / F 0.13

#3 — 5.96 / 116.10 / F 0.14 — 6.92 / 116.85 / C 0.07

S.W. Rot. — N.W. Rot.

#2 — 5.96 / 115.95 / C 0.11 — 6.94 / 116.75 / C 0.19

#1 — 5.96 / 115.71 / C 0.25 — 7.16 / 116.82 / C 0.34

B.C. — 5.52 / 115.48 / Meet — 7.10 / 117.10 / Meet

Lamont

Cl. for C.I. - Ely and Missouri

E.C.
#5 93.46

#4 2.74 / 93.31 / F 0.57

#3 3.07 / 93.20 / F 0.13

#2 2.74 / 93.10 / F 0.16

#1 2.65 / 93.03 / F 0.38

3.06 / 93.00 / C 0.06

Restake N.W. Rot. Diamond & Tacoma

B.C.

Missouri

16' — 10' — 2'

4.30 / 102.57 / C 1.73

3.53 / 102.50 / C 1.03

24

Gresham

Stakes - 32' off ℄

S.W. 3' Tie Back +7' Lft. } EL. = 25.25
Oliver + Gresham.

Chiseled □ S.W. Ret. } EL. = 31.51
Reed & Gresham

B.M. ≈ N.W.B.P. Gresham +	west	P.B. Dr. EL. = 21.19 East
	west	East
2+50 = Sly Oliver	24.74	24.46
2+45	5.71 24.68 C 1.03	5.58 24.40 C 1.18
2+00	4.79 24.04 C 0.75	4.63 23.90 C 0.73
1+50	4.80 23.33 C 1.47	4.42 23.35 C 1.07
1+00	3.65 22.62 C 1.03	3.93 22.80 C 1.13
0+50	3.02 21.91 C 1.11	4.45 22.25 C 2.20
0+00	21.20	21.70
Nly. P.B. Dr.		

Sly Reed	west	east
2+70	31.40	31.62
2+50	1.76 31.00 C 0.76	1.15 31.18 F 0.03
2+00	30.76 29.98 C 0.78	30.03 30.08 F 0.05
1+50	30.40 28.96 C 1.44	9.25 28.97 C 0.28
1+00	8.87 27.95 C 0.92	8.07 27.87 C 0.20
0+50	7.94 26.93 C 1.01	6.95 26.76 C 0.19
0+00	6.85 26.92 C 0.93	6.37 25.66 C 0.71
Nly. Oliver		

	Gresham	
Sly. Thomas		
2+70	36.30	36.50
2+50	6.45 36,00 C 0.45	6.35 36.19 C 0.16
2+00	5.83 35.26 0.57	5.80 35.41 C 0.39
1+50	5.20 34.52 C 0.68	5.25 34.63 C 0.62
1+00	4.61 33.78 C 0.83	4.70 33.85 C 0.95
0+50	3.96 33.04 C 0.92	3.92 33.07 C 0.85
Nly. Road.	3.42 32.30 C 1.12	3.00 32.29 C 0.71
0+00		

	Gresham	
	N.W chisel square	Thomas - EL. 37.17
Sly Grand.	3.50 42.00 C 1.50	3.15 43.00 C 0.15
2+70 C		
2+50	2.32 41.65 C 0.67	4 2.04 42.60 F 0.56
2+00	40.84 40.80 C 0.04	1.30 41.60 F 0.30
1+50	0.12 39.95 C 0.17	40.07 40.60 F 0.53
1+00	9.18 39.10 C 0.08	9.48 39.60 F 0.12
0+50	8.50 38.25 C 0.25	8.73 38.60 C 0.13
Nly Thomas		
0+00	37.40	37.60

Gresham
S.E. 7'L+t. Hornblend

	West	East
Sly Hornblend.	46.37	47.18
2+70		
2+50	6.18 46.12 C 0.06	7.90 46.95 C 0.95
2+00	5.66 45.50 C 0.16	7.19 46.36 C 0.83
1+50	4.54 44.87 F 0.33	6.35 45.77 C 0.58
1+00	4.28 44.25 C 0.03	5.38 45.18 C 0.20
0+50	4.16 43.62 C 0.54	4.85 44.59 C 0.26
Nly. Grand 0+00	4.40 43.00 C 1.40	4.75 44.00 C 0.75

EL. = 47.50
& Gresham

31' Ely. of Ely 7'L+t. R.P. to B.C. = x in Grand & Gresham

walk (N.E. Cor)
EL. = 46.68
Gresham St.

	West	East
Sly. Garnet		
2+70	2.28 52.25	53.20
2+50	2.20 51.88 C 0.32	52.80
2+18 = Exist el. on Rt.		52.19
2+00	1.21 50.98 C 0.23	52.19 51.84 C 0.35
1+50	0.40 50.07 C 0.33	1.94 50.88 C 1.06
1+00	9.28 49.17 C 0.11	51.00 49.92 C 1.08
0+50	8.45 48.26 C 0.19	50.41 48.96 C 1.45
Nly Hornblend 0+00	7.39 47.36 V	48.00

Gresham

Felspar- sly		
2+70	57.00	57.60
2+37½	5.80 56.35 F 0.45	7.43 57.00 C 0.43
2+05 Ev.C.	5.24 55.70 F 0.46	7.08 56.40 C 0.68
1+65	4.60 54.99 F 0.39	7.01 55.74 C 1.27
1+25	4.55 54.42 C 0.13	C.14 55.25 C 0.89
0+85 P.V.C.	3.80 54.00 F 0.20	5.94 54.89 C 1.05
0+42½	3.50 53.65 F 0.15	4.68 54.60 C 0.08
Nly Garnet 0+00	53.30	4.27 54.30

Gresham,

		28
3+10 ℄ Emerald	At. only	3.19 63.50 F 0.31
Sly Emerald 2+70	2.23 62.00 C 0.23	3.10 63.00 C 0.10
2+50	C 0.07	C 0.05
2+00	C 0.15	C 0.30
1+50	F 0.05	C 0.20
1+00	F 0.43	C 0.10
0+50	F 0.50	C 0.13
Nly Felspar 0+00 ch.E.C.	8.51 58.40 C 0.11	9.04 59.00 C 0.04

	Gresham		OLIVER AVE.
			1+60
Diamond Sty			
2+70	9.80	70.09	1+40
	69.50	70.00	
	C0.30	C0.04	
2+50	C0.42	C0.02	1+20
2+00	F0.25	F0.29	1+00
1+50	F0.18	F0.36	0+80
1+00	C0.05	C0.65	0+60
0+50	C0.08	C0.93	0+40 P.V.C.
			℄ E.C.
Emerald	3.27	5.32	0+10
Wly.	63.00	64.00	
0+00	C0.27	C1.32	Engraham
			wly
			0+00

Oliver

3+80

3+60

3+40

3+20

3+00

2+80

2+60 P.V.C.

2+30

2+00 E.V.C.

1+80

Oliver Ave.

N.W. 1" disk Haines & Oliver El = 42.68

1+00	39.99 39.79 C0.20	8.47 39.79 F1.32	9.69 40.29 F0.60	0.48 40.29 C0.19
0+80	0.68 40.45 C0.23	9.16 40.45 F1.29	1.01 40.95 C0.06	1.41 40.95 C0.46
0+60 P.V.C.	1.37 40.91 C0.46	40.00 40.91 F0.91	1.70 41.41 C0.29	1.72 41.41 C0.31
u. E.C. 0+10	2.54 41.81 C0.73	1.24 41.81 F0.57	1.17 42.31 F1.14	3.12 42.31 C0.81
Wly Haines 0+00				

5+00
Ely. Haines

u. B.C.
4+90

4+55

4+20 E.U.C.

4+00

Oliver Ave.

3+73

Rough

3+40	6.66 26.21 C0.45	6.86 26.21 C0.65	7.29 26.80 C0.49	6.98 26.80 C0.18
3+20	7.45 26.87 C0.58	7.57 26.87 C0.70	7.63 27.42 C0.21	7.53 27.42 C0.11
3+00	8.11 27.72 C0.39	8.37 27.72 C0.65	8.05 28.25 F0.20	8.27 28.25 C0.02
2+80	9.38 28.76 C0.62	9.23 28.76 C0.47	9.16 29.27 F0.11	9.28 29.27 C0.01
2+60 P.V.C.	0.10 30.00 C0.10	0.55 30.00 C0.55	0.14 30.50 F0.36	0.41 30.50 F0.09
2+10	3.79 33.33 C0.46	3.70 33.33 C0.37	3.83 33.83 x	4.00 33.83 C0.17
1+60 E.V.C.	6.30 36.66 F0.36	5.01 36.66 F1.65	6.46 37.16 F0.70	7.48 37.16 C0.32
1+40	8.04 37.89 C0.15	6.54 37.89 F1.35	7.70 38.39 F0.69	880 38.39 C0.41
1+20	8.95 38.94 C0.01	7.72 38.94 F1.22	9.49 39.44 C0.05	9.58 39.44 C0.14

Oliver Ave

31

Gresham Ely.

Rough

2.78

5+00				
C.B.C. 4+90	5.38 24.78 C0.60	5.08 24.78 C0.30	6.11 25.56 C0.55	6.28 25.56 C0.72
4+53 4	5.21 25.04 C0.17	5.42 25.04 C0.38	5.84 25.76 C0.08	6.03 25.76 C0.27
4+16 7 (34.7)	5.39 25.30 C0.09	5.61 25.30 C0.30	6.07 25.96 C0.11	6.18 25.96 C0.22
3+80 E.V.C.	5.92 25.57 C0.35	6.14 25.57 C0.57	6.30 26.17 C0.13	6.35 26.17 C0.18
3+60	6.35 25.76 C0.59	5.93 25.76 C0.17	6.35 26.38 F0.03	6.63 26.38 C0.25

INDEXED

Gresham
Curbs

	West	East	
oliver 2+50 = Sly			
℄ B.C. 2+40	4.46 24.60	5.52 24.32	
2+38 - R/R	F 0.14	C 1.20 C 1.28 - 2+38	
2+20	F 0.03	C 0.76	
1+80	F 0.43	C 0.03	
℄ B.C. 1+37 F 0.55	C 0.15	C 0.20	
℄ B.C. 1+13 F 0.65	F 0.70	C 1.12	
1+00	C 0.16	C 0.51	Grade Only No line
0+50	Grade	C 0.58	
℄ E.C. 0+10	21.30 Meet ℄	1.96 21.80 Meet ℄	
0+00 = Nly P.B. Drwg			

Gresham
curbs.

32

	West	East
Reed. 2+70 = Sly		
℄ B.C. 2+60	31.42 31.20 Meet	1.04 31.38 Meet
2+30	C 0.25	C 0.16
1+90	C 0.30	F 0.07
℄ E.C. 1+47	C 0.36	F 0.19
℄ B.C. 1+23	F 0.02	F 0.05
1+00	C 0.53	F 0.15
0+50	C 0.60	C 0.12
℄ E.C. 0+10	6.61 26.01 C 0.60	6.50 25.80 C 0.70
Oliver 0+00 = Nly		

Gresham - curbs.

	West		East	
Thomas. 2+70 = Sly.				
℄. B.C. 2+60	36.28 36.15 to Meet Exist		36,25 36.17	to meet exist ℄.
2+30	C0,02		F0.10	
1+90	C0,15		C0.27	
℄. E.C. 1+47	F0,24		C0,70	
℄. B.C 1+23	C0,20		F0.16	
1+00	C0,29		C0,51	
0+50	C0,63		C0,60	
℄. E.C. 0+10	32,45		32,45 C0.42	
0+00 = N.ly Reed				

Gresham - curbs.

	West		East	
Grand. 2+70 = Sly				
℄. B.C. 2+60	2,02 41,83 C0,19		42,80 F0,47	
2+30	C0,30		F0,35	
1+90	F0.11		F0,41	
℄. E.C. 1+49	F0,04		F0,35	
℄. B.C. 1+23	C0,47		F0,40	
1+00	C0,10		F0,28	
0+50	C0,16		F0,19	
℄. E.C. 0+10	7,70 37,57 C0,13		37,82 F0,30	
0+00 = Nly Thomas.				

Gresham curbs

Hornblend
2+70 = Sly

℄ B.C.		
2+60	6.20 46.29 F0.09	7.17 47.10 C0.07
2+30	C0.08 ~~F0.09~~	C0.18 ~~C0.05~~
1+90	C0.35 ~~F0.06~~	C0.21 ~~F0.13~~
℄ E.C.		
1+47	4.41 ~~44.46~~ ~~F0.70~~ F0.05	5.64 ~~F0.35~~ ~~45.48~~ C0.16
℄ B.C.		
1+23	C0.31 ~~F0.30~~	F0.06 ~~F0.59~~
1+00	C0.20 ~~F0.40~~	C0.06 ~~F0.45~~
0+50	C0.41 ~~F0.13~~	C0.01 ~~F0.49~~
0+10 = ℄ E.C.	43.13 ~~43.61~~ ~~C0.21~~	44.12 ~~44.60~~ ~~F0.30~~
~~Grand~~	C0.69	C0.19
0+00 = Nly		

Gresham - curbs

Garnet
2+70 = Sly — 2.28, 52.25, C0.03

℄ B.C. - Lt.
2+64 — grade

2+30 — grade

1+90 — F0.45, ~~C0.95~~

1+70 Rt.
℄ E.C.
1+47 — F0.08

℄ B.C.
1+23 — C0.07

1+00 — grade

0+50 — C0.11

℄ E.C.
0+10 — 7.00, 47.54, C0.06

0+00 = Nly
Hornblend

3.24
53.20
C0.04

—

Exist ℄ 0.12 High
Set stakes to Meet it

F

F0.07

F0.02

F0.33

F0.17

C0.18

8.30
48.19
C0.11

Gresham - curbs

52.66 = Nly 10' R.P.x to S. wly 7' Lft of Gresham Garnet

2+05 E.V.C.	5.42 55.70 F0.28	6.32 56.40 F0.08
1+85	5.15 55.33 F0.18	6.22 56.05 C0.17
1+65	4.94 54.99 F0.05	6.34 55.74 C.0.70
cl. E.C. 1+47	4.60 54.71 F0.11	5.54 55.50 C0.04
cl. B.C. 1+23	4.08 54.40 F0.32	5.07 55.23 F0.16
1+05	4.42 54.19 C0.23	5.13 55.05 C0.08
0+85 P.V.C.	4.17 54.00 C0.17	5.96 54.89 C0.07
0+39 5	3.75 53.68 C0.07	4.12 54.62 F0.50
0+06 cl. E.C.	3.55 53.35 C 0.20	3.98 54.34 F 0.3 6
0+00 = Nly. Garnet.		

Gresham - Curbs

cl. E.C. on Lt. 1+47	C0.13	F0.61
cl. B.C. Lt. 1+23	F0.10	—
1+00	F0.18	F1.00
0+50	F0.26	F0.92
cl. E.C. 0+10	8.26 58.53 F0.27	8.13 59.15 F 1.02
Felspar 0+00 = Nly = S'ly Felspar 2+70		5.760
cl. B.C. 2+60	6.15 56.80 F 0 6 5	6.52 57.42 F 0.90
2+32 5	5.90 56.25 F0.35	6.54 56.91 F 0 3 7

Gresham - Curbs

B.C. on Lt.		
1+23	C1.08	→
1+00	F0.46	F1.02
0+50	F0.21	C0.22
= B.E.C.		
My Emerald	3.14	4.58
0+00 =	63.00	64.00
	C0.14	C0.58
3+10 on Rt.		F0.59
Emerald	2.17	2.81
2+70 = Sly	62.00	63.00
B.C.	C0.17	F0.19
~~B.C.~~		
~~2+60~~		
2+30	C0.02	F0.38
1+90	Grade	F0.31

Gresham - curbs.

Sly Diamond		
2+70 =		
B.C.	8.35	8.80
2+60	69.26	69.78
	F0.91	F0.98
2+30	F0.91	F1.51
1+90	F0.49	F1.36
B.E.C. on Lt.		
1+47	F0.38	F1.31

Gresham (alleys)

Reed Ave

BLK 288

29.20
C 3.92
Nail
29.84
C 0.36

28.80
C 0.43
28.81
F 0.19

8.64

8.65
28.85
F 0.20

9.21
29.21
Grade

BLK 287

28.79
C 0.66
28.41
F 0.13

28.39
F 0.34
28.37

8.26
28.41
F 0.15

8.70
28.77
F 0.07

Oliver Ave

BLK 301

23.49
C 0.44
23.13
C 0.13

23.09
23.25

3.47
23.29
C 0.18

4.02
23.65
C 0.37

BLK 302

23.20
C 0.06
22.84
F 0.79

22.80
4.17
23.05
C 1.12

4.15
23.09
C 1.06

3.92
23.45
C 0.47

Pacific Beach Dr.

GRESHAM. - (alleys)

GRAND AVE

BLK 254

0.08
40.26
F 0.18

9.85
39.90
F 0.05

39.86

40.50

40.54

0.31
40.90
F 0.59

BLK 253

9.60
39.92
F 0.32

9.94
39.56
C 0.38

8.45
39.52
F 1.07

40.10

40.14

0.25
40.50
F 0.25

THOMAS Ave

BLK 267

5.29
34.84
C 0.45

4.23
34.48
F 0.25

34.44

5.27
34.55
C 0.12

5.22
34.59
C 0.63

5.33
34.95
C 0.38

BLK 268

5.04
34.35
C 0.49

4.30
34.19
C 0.11

34.15

34.24

3.96
34.28
F 0.32

5.21
34.64
C 0.57

Reed Ave

Gresham – (alleys)

Garnet Ave.

X- grid in

50.01 X-grid

50.40 50.04 50.00 50.74 50.78 51.14 1.87

C0.39 F0.10 F0.04 C0.73

BLK 220

9.66

50.04 49.68 49.64 50.36 50.40 50.76 1.62

F0.38 F0.03 F0.43 C0.86

BLK 217

Hornblend Ave

1' Back

4.27 F4.44

4454 4446 4482 5.64 6.66

C0.23 F0.05 45.14 45.50 45.86

C0.14 C0.80

- 45.48

C0.16

BLK 233

4.42 4.78

4442 4431 4451 45.18 F0.10 C0.28

F X C0.27

BLK 234

44.27

C0.31

45.28

Grand Ave

10.08

9.72

Gresham – (alleys)

Emerald

Diamond

1.20 0.50

60.73 60.37 60.33

C0.47 C0.13

BLK 186

7.04 6.18

66.89 66.53 66.49

C0.15 F0.35

BLK F.

6.17 7.06

66.41 66.05 66.01

F0.24 C1.01

9.51 9.95

60.46 60.10 60.06

F0.92 F0.15

Emerald

Felspar

Felspar Ave.

Mid curve

55.57

57.08

4.42 4.60

54.09 54.73 54.69 55.47

C0.33 F0.13

BLK 199

5.54 7.68

55.51 55.87

C0.03 C1.21

Mid. curve

55.24

BLK 200

4.72 4.08

54.82 54.46 54.42 55.25

F0.10 F0.38

5.07 6.70

55.29 55.65

F0.21 C1.05

56.68

Garnet Ave.

INDEXED JUL 25 1954 Curb. Rot. Oliver + Gresham

Oliver Ave

25.25 E.C. 24.78

Prop.

25.10 #3 24.68

S.W. Rot. S.E. Rot.

25.02 Meet #2 24.58

4.78
24.80 #1 24.48
F 0.02

4.46
24.60 B.C. 24.32
F 0.14 2+40

Gresham

Gresham

6.61 #4 6.50
26.01 E.C. 25.80
C 0.60 C 0.70

6.17 6.20
25.91 #3 25.64
C 0.26 C 0.62

N.W. Rot. N.E. Rot.

5.88 C.37
25.96 #2 25.52
F 0.08 C 0.85

6.12
26.05 #1 25.49
C.463

Prop
E.C
2.56
6.11
26.14 E.C 25.56
C 0.55

Oliver Ave

INDEXED Curb. Rot. Reed + Gresham

Reed Ave.

Gresham

31.60 E.C. 32.00

Prop.

31.66 #3 31.11

S.W. Rot. S.E. Rot.

31.55 #2 31.76

31.40 #1 31.55

31.20 B.C. 31.04
31.38 Existing
F 0.34 Meet

Gresham

3.01 #5 E.C. 2.87
32.45 E.C. 32.45
C 0.56 C 0.42

2.68 #3 2.86
32.26 #4 32.25
C 0.42 C 0.61

N.W. Rot. N.E. Rot.

2.77 #2 2.87
32.20 #3 32.10
C 0.57 C 0.77

2.87
32.13 #2 32.10

#1 Prop

32.07 B.C. 32.21

Reed Ave

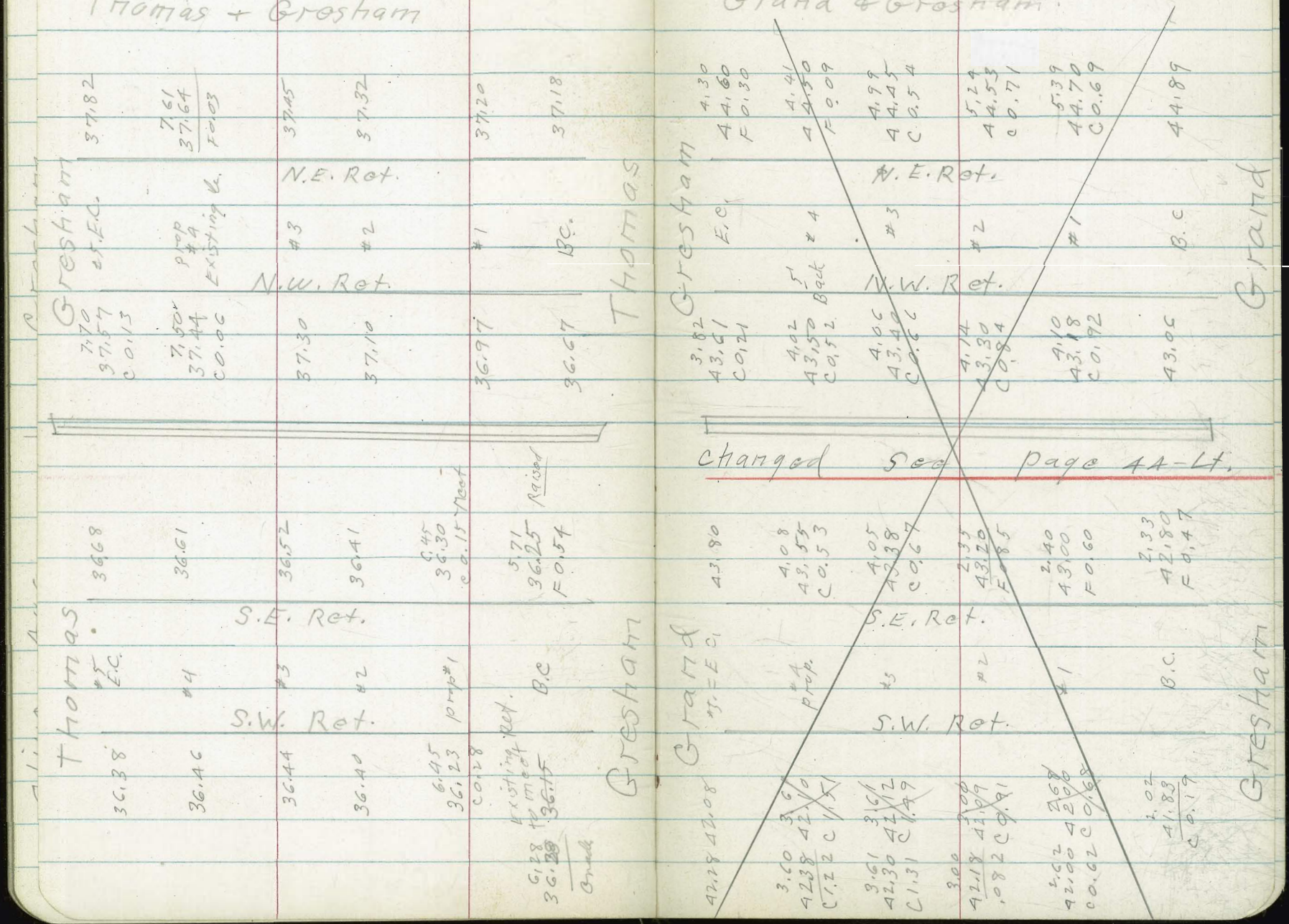
29

Curb. Rot.

Thomas + Grosham

Curb. Rot.

Grand & Grosham.



Changed See page 44-Lt.

Curb Rot.
Hornblend + Gresham

8.30
4.8.19
Co.11

8.01
8.00

Gresham

N.E. Rot.

prop

N.W. Rot.

7.60
4 7.54
Co.06

7.38
4 7.36

Hornblend

47.18

47.08

S.E. Rot.

Hornblend

prop.

S.W. Rot

46.37

46.27

Gresham

Curb. Rots
Garnet + Gresham

Gresham

N.E. Rot.

Garnet

N.W. Rot.

S.E. Rot.

Garnet

prop

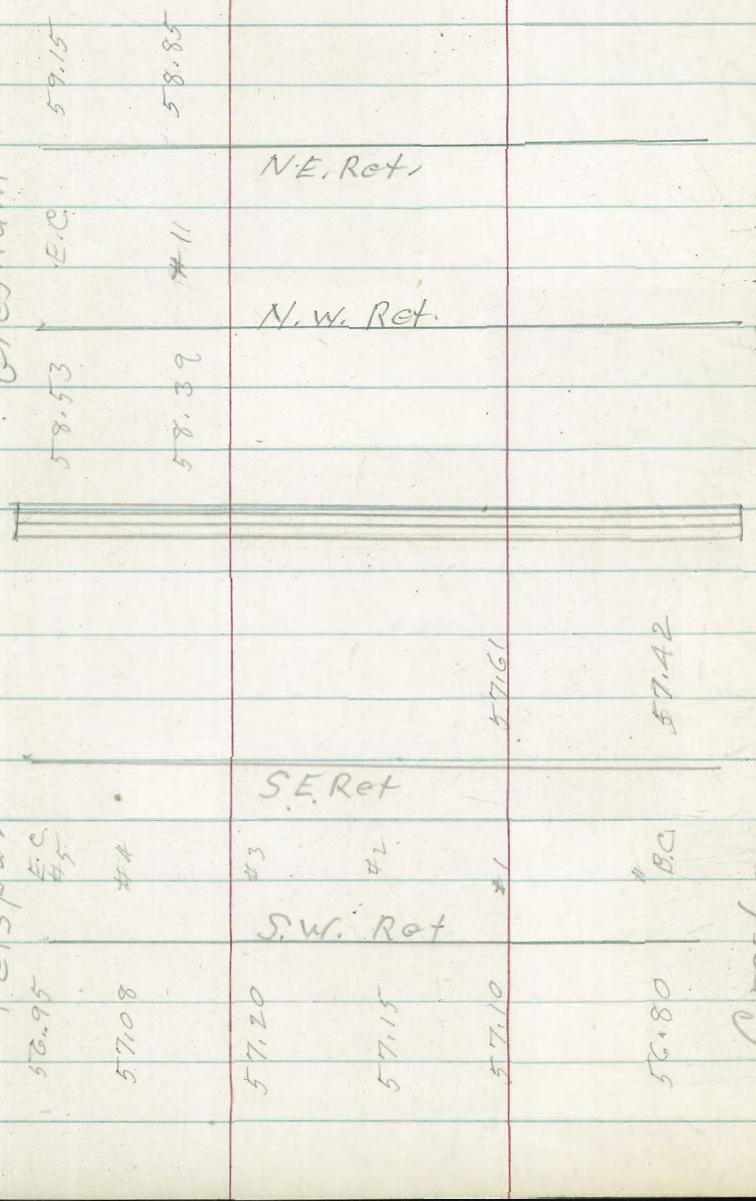
S.W. Rot

B.C.

Gresham

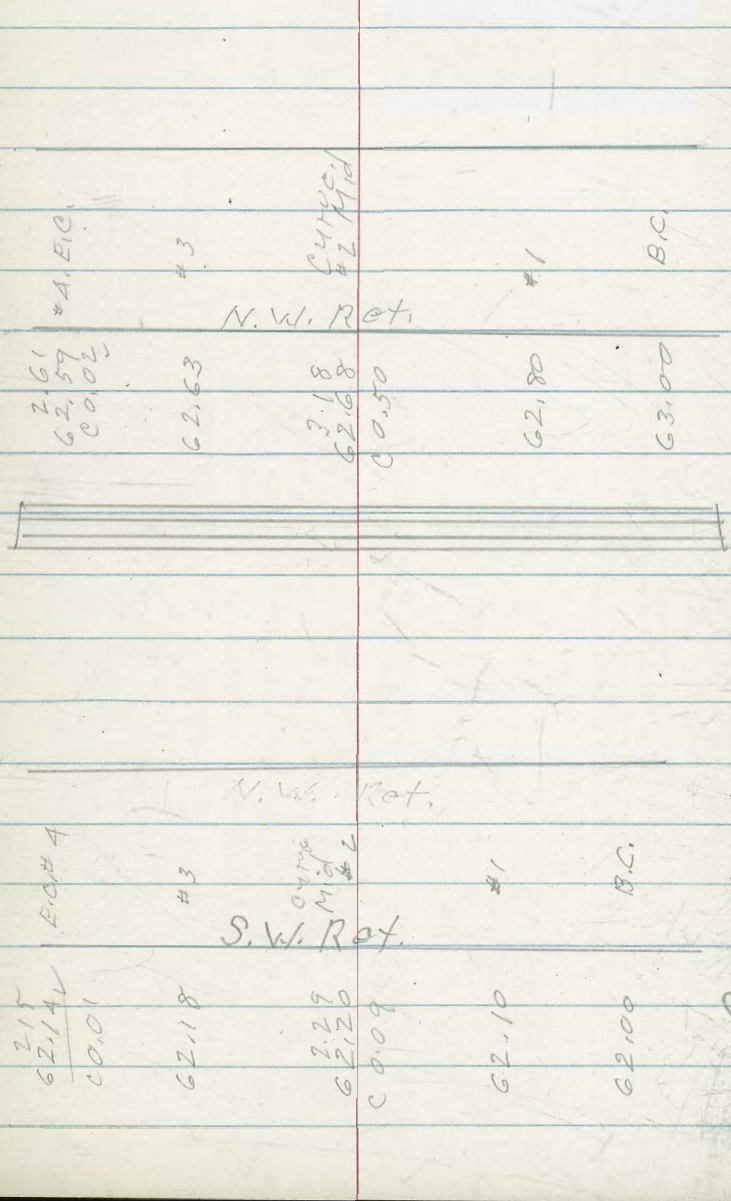
Curb. Rots

Felspar + Gresham



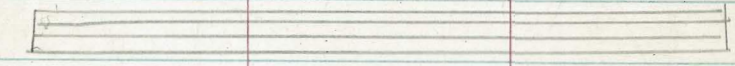
Curb. Rots

Emerald + Gresham



Curb. Rots.

Diamond



69.86

69.78

S.E. Rot.

Diamond

Asph.

BC

Graham

S.W. Rot.

69.34

69.26

Curb. Rot.

Oliver + Haines

INDEXED

Curb returns Grand + Gresham

Grand

42.08 #5 E.C. 43.61

3.62
42.10 #4 4.19
C 1.52 43.42
C 0.68

3.62 4.06
42.12 #3 43.28
C 1.50 C 0.78

3.00 2.35
42.09 #2 43.15
C 0.91 F 0.80

2.63 2.40
42.00 #1 43.00
C 0.63 F 0.60

2.33
41.83 B.C. 42,80
F 0.47

Gresham

Gresham

3.82
43.13 #5 E.C. 44.12
C 0.69 C 0.19

5' back.
4.04
43.10 #4 4.42
C 0.94 44.00
C 0.42

4.07 5.00
43.09 #3 44.03
C 0.98 C 0.97

4.15 5.25
43.08 #2 44.12
C 1.07 C 1.13

4.12 5.40
43.07 #1 44.25
C 1.05 C 1.15

5.97
43.06 B.C. 44.40
C 1.57

Grand

Ad East of E.C.
46.15
45.14
C 1.01

Grand

1.80
42.10 #4
F 0.30

1.34
42.12 #3
F 0.78

1.23
42.09 #2
F 0.86

1.71
42.00 #1
F 0.29

41.83 B.C.

Gresham

S.W. Quad. Nat. Rostate

Sat. 5-19-53

A4

c.H.

3-11-53

Alley Blk 246
Mission Beach
sheet 9686-L
F.B 2226- P-2

between Zanzibar ct. + York. ct.

		South	℄	North	
End. alley 0+53.33	X-6'	5.49 5.35 C0.14		5.26 5.35 F0.09	X-2'
0+40	X-2'	5.11 5.08 C0.03		5.27 5.08 C0.19	□-1'
0+20	□-1	5.17 4.50 C0.67		4.88 4.50 C0.38	T-0.27
Existing pave 0+00 wly line strand way		3.09		3.13	

Alley Blk. 243
Mission Beach

between
York ct. + Yarmouth ct.

Sheet 9686-L

3-11-53

6' Rt. of ℄ at 0+53.33 = (S) #18 — 4.90 / 1.00 / C 3.90

0+31.67 Rt. = (S) #17 — 5.18 / 1.00 = Prop. line I.E. / C 4.18

		South	℄	North	
west end Alley 0+53.33	□-2'	5.77 5.75 C0.02		5.30 5.75 F0.45	□-2'
0+40	□-0.2'	5.43 5.55 F0.12		5.52 5.55 F0.03	□-2'
0+20	T-0.13	6.67 4.80 C1.87		4.52 4.80 F0.28	□-2'
=Exist. pave 0+00 = wly. line strand way		3.35		3.33	

bet SURVEYED Alley Blk 244
York ct + Mission Beach 3/11/53
Yarmouth ct.
Sheet 9686-L

		North	℄	South	
1+90	D-1½'	-0.50 -0.45 F0.05		-0.59 -0.45 F0.14	T. line
1+45	X-2'	-0.47 -0.40 F0.07		-0.20 -0.40 C0.20	T-0.10
1+00	D-2'	-0.32 -0.36 C0.04		-0.32 -0.36 C0.04	↑-2'
0+80	D-0.1'	0.08 -0.18 C0.26		-0.05 -0.18 C0.13	D-2'
0+60	D-1'	0.77 0.31 C0.46		1.14 0.31 C0.83	
0+40	D-2'	1.56 1.12 C0.44		1.55 1.12 C0.43	T-0.10
0+20	D-2'	1.94 2.24 F0.30		2.67 2.24 C0.43	X-0.1'
Existing Pavc. 0+00 = Ely line Strand wky.		3.23		3.31	

Lt. = North.

2+70 Lt. = (S) #1 — 0.54 / -1.97 / C 1.43

1+65 Lt. = (S) #2 — 0.54 / -1.70 / C 1.16

0+15' Lt. = (S) #3 — 2.50 / -1.00 / C 3.50

	North	℄	South	
Mission Blvd. Wly. Ch. line 3+14.2		-0.85		
3+09.2	-0.55		-0.56	
Mission Blvd 3+04.3 wly. X-2'	-0.17 -0.57 C0.40		-0.10 -0.57 C0.47	T-0.30
2+80 E.V.C. D-1'	-0.60 -0.54 F0.06		-0.54 -0.54 X	T-0.10
2+35 D-0.3'	-0.31 -0.49 C0.18		-0.75 -0.49 F0.26	D-2

Alley Blk 242 M.B.

between Yarmouth ct. + Windimere Ct.

INDEXED

0+05 Rt.= (5) #16 I.E.= 3.94 / 0.00 / C 3.94

	Lt.= South	±	Rt.= North	
wly end alley				
0+53.33 N-3.84	5.43 / 4.95 / C 0.48		5.13 / 4.95 / C 0.18	X-1'
0+40 X-2'	5.02 / 4.80 / C 0.22		4.63 / 4.80 / F 0.17	D-2'
0+20 D-0.9'	4.35 / 4.35 / X		4.85 / 4.35 / C 0.50	□-1'
0+00 Exist. Pave. wly line Strand Way	3.68 ✓		3.69 ✓	

INDEXED

Alley Blk 241 Mission Beach

Between Yarmouth + Windimere	Lt. North	±	Rt. South	
2+50 T-0.10'	0.65 / -1.11		-1.19 / -1.11	□-2'
37'	C 1.76		F 0.08	
2+13 T.-1.87'	0.21 / -1.05		-0.79 / -1.05	□-line
36'	C 1.26		C 0.26	
1+77 T-1.80'	0.78 / -1.00		-0.05 / -1.00	T-on line
36'	C 1.78		C 0.95	
1+41 □-1'	-0.82 / -0.95		-1.08 / -0.95	N-1'
36	C 0.13		F 0.13	
1+05 N.-line	-0.97 / -0.90		-1.35 / -0.90	X-✓ 0.34 / -0.90
	F 0.07		C 0.55	C 0.56
0+85 N-2.40'	0.43 / -0.61		0.70 / -0.61	T-0.10'
	C 1.94		C 1.31	
0+65 X-line	0.31 / 0.21		0.26 / 0.21	□ 1'
	C 0.10		C 0.05	
0+20 N-1'	5.47 / 2.64		2.14 / 2.64	□-0.65'
	C 2.83		F 0.50	
0+00 = Exist Pave. Ely line Strand Way.	3.60 ✓		3.59 ✓	

Blk. 241 Cont.

2+46 Rt. = ⑤ # 4			−1.47 −1.93 C 0.46	
1+65 Rt. = ⑤ # 5		17	−1.77	
1+40 Rt. = ⑤ # 6		17	−1.72	
1+16 Rt. = ⑤ # 7			−0.61 −1.77 C 1.16	
Mission Blvd. 2+89 9 = wly. ℄	−0.76		−0.87	
	Lt. = North	℄	Rt. = South.	
2+84 9	−0.56 −0.58 —		+0.69 −0.69 C 0	
2+82 4	−0.40 −0.55 C 0.15		−0.33 −0.60 C 0.27	
wly. Mission Blvd. 2+79 9	−0.39 −0.65 C 0.26		−0.44 −0.60 C 0.16	−0.50 −0.60 C 0.10
2+65 X-0.40'	0.66 −1.00 C 1.66		−0.81 −1.00 C 0.19	−1.23 −1.00 F 0.23

Catch basin + Culvert
Alley Blk 241 + Mission Blvd.
Sheet 9687-L

Stakes 4' North (Rt.) of ℄.

		Restake
wly end culvert.		
0+85 = ℄ C.B.	−0.40 −2.40 C 2.00	−0.16 −2.40 C 2.24
		on wall
0+62	−0.70 −2.47 C 1.77	
0+46.5	−0.36 −2.52 C 2.16	
0+31	+0.43 −2.56 C 2.99	
0+15 5	−0.59 −2.60 C 2.01	
0+00 = ℄ C.B. (℄ y. ℄ line, Mission Blvd)	−1.09 −2.65 C 1.56	

Alley Blk 238 - Mission Beach

between Windimere & Whiting

		North	℄	South	
2+20	□-1'	-0.69 -0.96 C0.27		-0.16 -0.96 C0.80	□-1'
1+85	X-0.65'	0.18 -0.89 C0.71		1.48 -0.89 C-2.37	X-0.10'
1+50	□-2'	-0.59 -0.82 C0.23		-0.63 -0.82 C0.19	□ 2'
1+30	□-2'	-0.19 -0.69 C0.50		-0.38 -0.69 C0.31	□-2'
1+10	X-2'	-0.13 -0.37 C0.24		-0.27 -0.37 C0.10	□-2
0+90	□-1	0.87 0.12 C0.75		0.61 0.12 C0.49	□-1'
0+70 P.U.C.	□-2'	1.06 0.80 C0.26		1.14 +0.80 C0.34	X-2'
0+20	□-3'	2.82 2.73 C0.09		3.00 2.73 C0.27	□-2'
0+00 = Existing Pave = Ely Strand Way		3.18✓		3.13✓	

Blk 238 - Mission Blvd. 49

INDEXED

	℄ North	℄	Rt. - South	
wly. Blvd (℄) C.L. into Mission		-1.23		
2+48 = (℄)	-1.01		—	
2+42 (Rt.)	—		-0.75 -1.03 C0.28	top of
wly. Mission Blvd. 2+38 =	-0.29 -1.01 C0.72		-0.57 -0.99 C0.42	Pipe on line -0.65 -0.99 C0.34 from d.

Blk 238 Mission Beach
Sewer Laterals

1+95 Rt. = Ⓢ # 8	− 0.56 − 1.88 C 1.32
1+42 Rt. = Ⓢ # 9	− 0.65 − 1.65 C 1.00
1+40 Lt. = Ⓢ # 14	− 0.56 − 1.63 C 1.07
1+15 Rt. = Ⓢ # 10	− 0.35 − 1.50 C 1.15
0+70 Rt. = Ⓢ # 11	1.14 − 1.10 C 2.24
0+45 Lt. = Ⓢ # 15	1.86 − 1.00 C 2.86
0+44 Rt. = Ⓢ # 12	1.83 − 1.00 C 2.83
0+18 Rt. = Ⓢ # 13	3.30 − 0.50 C 3.80

INDEVER Alley Blk. 237
Mission Beach 5-7-53

Sheet 4910-B.

between Whiting & Windimere Cts.

B.M. = B.P. York Ct. + Sea Wall EL. = 7.08

	South	North
End of Alley	5.46	5.27
0+53.33	5.30	5.30
	Co.16	Fo.03
0+40	4.77	4.90
	5.00	5.00
	Fo.23	Fo.10
0+20	5.16	4.45
	4.35	4.35
	Co.81	Co.10
0+00	3.34	3.34

0+00 = Wly line 3 strand way

Grade for fill

Wawona Drive. 4-10-53

Stakes on Ely. Prop. line

Ely. line Wawona & Oliphant = 0+00

0+00 = 6+60 Bk $\frac{1803}{31}$

Exist. roadway Grd.

			86.4		2+00	77.35 87.75 F 10.40
			86.65 C 0.1		1+50	86.55
			87.1		1+00	90.00 85.35 F 4.65
Sta. 2+25±						
Nail in pole #		12.08	85.17	87.1	0+75	80.85 84.75 F 3.90
T.P.	1.10	97.25	1.47	96.15		
T.P.	13.01	97.62	1.2	84.61	87.1	0+50	81.15 84.15 F 3.00
T.P.	12.05	85.81	0.56	73.76		
0-00	2.62	74.32	—	71.70	88.0	0+00	1.95 82.75 F 1.00

N.W.B.P. Pac + Capistrano

INDEXED

Roosevelt

5/5/53

Haines to Riviera Dr.

VKL.O.32051

9338-L

	South Rough	South curb	North curbs	North Rough
1+84.4 Ch. B.C.	9.93 15.96 C 3.97	4.74 15.96 F 1.22	4.00 15.32 F 1.32	5.15 15.32 F 0.17
1+40 E.O.C.	4.74 T.P. 21.61 C 3.13	0.64 21.61 F 0.97	0.07 21.06 F 0.99	1.68 21.06 C 0.62
1+20	8.11 24.05 C 4.06	~~24.06~~	~~23.53~~	4.19 23.53 C 0.66
1+00	7.17 26.25 C 2.72	—	—	6.59 25.82 C 0.77
0+80	33.33 28.24 C 5.11	7.96 28.24 F 0.28	7.29 27.91 F 0.62	8.95 27.91 C 1.04
0+60 P.O.C.	5.36 30.00 C 5.36	29.93 30.00 F 0.07	9.44 29.72 F 0.28	32.20 29.72 C 2.48
0+31.25 33.00 T.P.	—	2.60 32.38 C 0.22	32.34 32.36 F 0.02	—
Ch. E.C. 0+02.5	7.15 34.75 C 2.40	34.75	35.00	6.34 35.06 C 1.34
0+00 Nly Haines	34.95			35.20

Haines

52

100' South of Roosevelt to Nly line Roosevelt.

0+00 = 100' south of Roosevelt.

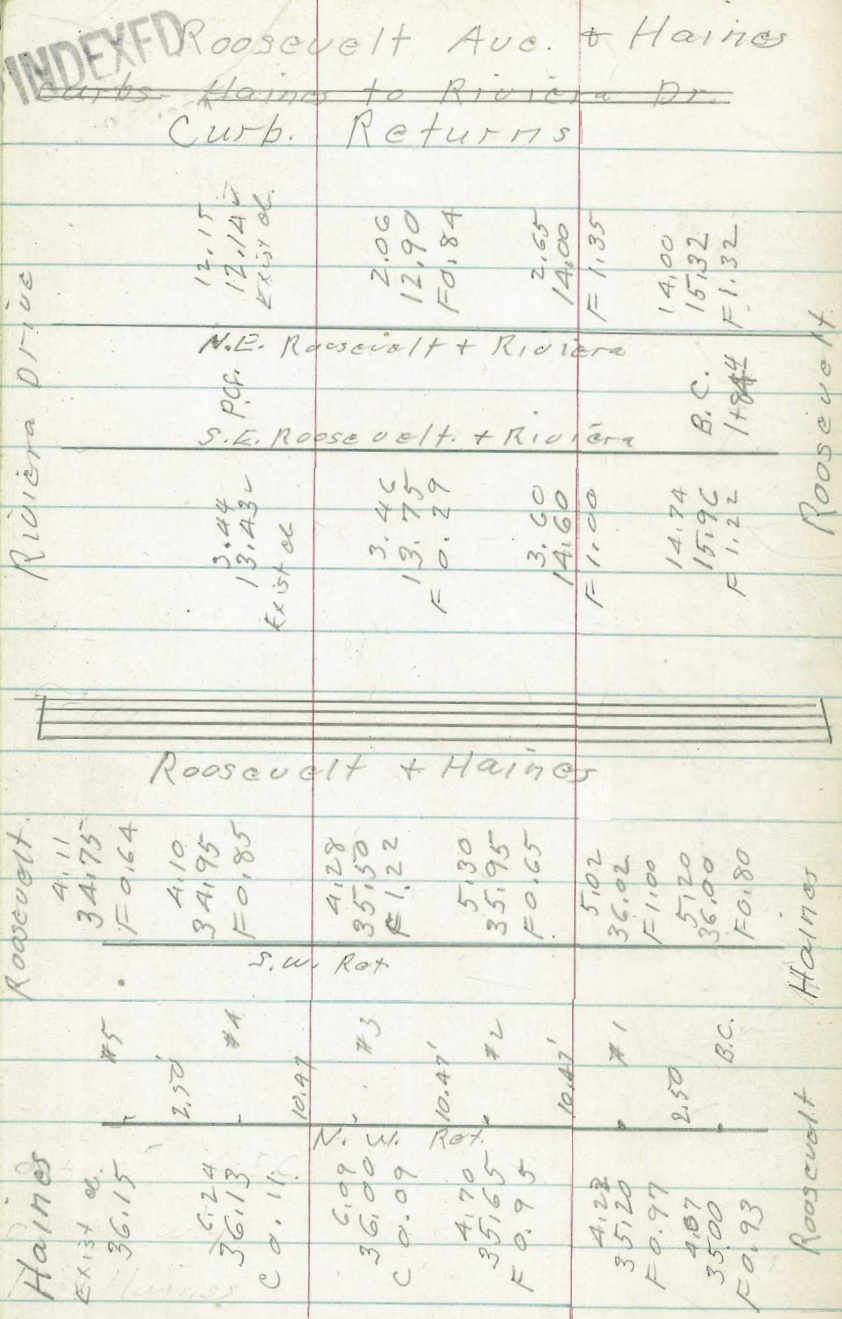
	Rough west			Rough East
36.34 = N.W.	3'x8' disk Roosevelt + Haines			
		ob.	ob.	
Nly Roosevelt 1+75	6.17 36.15		6.74 36.72	36.72
1+37.5			5.70 36.72 F 1.02	40.39 36.72 C 3.67
Sly. Roosevelt 1+00	36.00			36.72
Ch. B.C. on Lt. 0+97.5	7.27 36.00 C 1.27	5.20 36.00 F 0.80	6.11 36.72 F 0.61	41.07 36.72 C 4.35
Ch. Sta = 0+48.75 0+50 = Rough Ch. Sta.	6.60 35.30 C 1.30	4.97 35.27 F 0.30	4.97 36.01 F 1.04	9.32 36.03 C 3.29
0+00	6.57 34.55 C 2.02	4.48 34.55 F 0.09	4.52 35.30 F 0.78	8.52 35.30 C 3.22

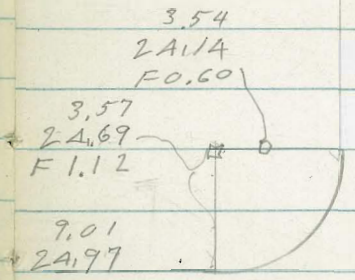
INDEXED

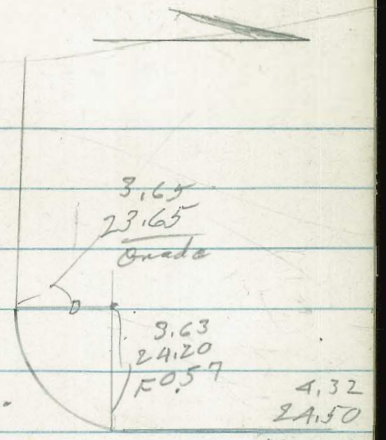
Roosevelt Ave. + Haines

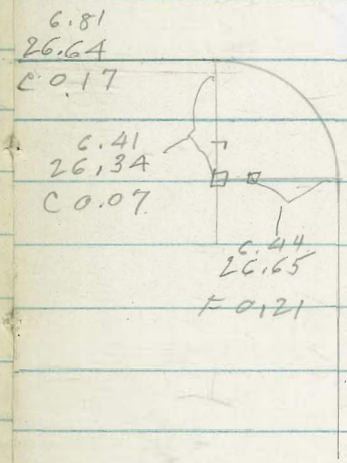
~~Curbs Haines to Riviera Dr~~

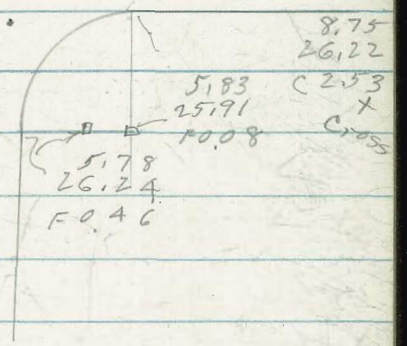
Curb Returns











Jennings St. Bangor West

6/16/53

sheet #10846-L

	Rough Cr.		530	Rough Cr.
1+40.73				
wly. Jennings Pl. 1+40.73			5.30 262.39 C 2.91	6.33 262.39
1+20.73			6.33 265.07 C 1.20	6.71 265.07
Ely Jennings Pl. 0+90.73 On	Mon. 267.30	66.66 7.30 FO.64	7.75 7.15 C0.60	7.75 267.15
0+60.73	269.52	70.06 9.06 C1.00	8.88 9.02 F0.14	8.88 269.48
0+40.73 X-5'	70.47 269.77 C0.70	70.46 9.44 C1.02	9.37 9.40 X	9.37 269.73
0+20.73	70.63 269.41 C 1.22	70.63 9.36 C 1.27	9.82 9.32 C0.50	9.82 269.37 C0.45
Wly Bangor 0+00	268.77		8.73 V	268.73

Jennings St.

prop. Cor. 3+34.25	4.28 269.6 F 3.32
2+94.25	6.06 269.40 F 3.34
2+54.25	8.08 269.26 F 1.18
2+14.25	7.79 269.42 C 0.67
1+74.25	70.63 268.98 C 1.65
1+34.25	70.26 268.84 C 1.42
0+94.25	70.20 268.30 C 1.90
0+54.25 1.77'	9.43 267.57 C 1.86
ob. E.C. 0+00	7.34 266.60 C0.74
0-05.73 = Sly Jennings	

Place 54

Place - South

9.84 258.6 C 1.24

2+03.38 = ob. B.C. (P-55)

1+87.28	268.58
1+67.28	268.49
1+47.28	70.06 268.30 C 1.76
1+07.28	70.04 268.00 C 2.04
0+87.28	7.97 267.60 C 2.37
0+67.28	9.86 267.20 C 2.66
0+47.28	9.57 266.56 C 3.01
0+27.28	8.27 265.94 C 2.33
0+00 = ob. Rgt. E.C.	6.43 265.10 C 1.33

Tie Points - P.B. Drive. 55

'INDEXED'

Mid curve → 9.24 / 268.7 / C 0.54

#C Ely. wly. P.R.C. 8.20 / 268.79 / F 0.59

23.56

#5 5.24 / 268.90 / F 3.64

23.56

#4 ℄ 5.58 / 269.10 / F 3.52

23.56

#3 ℄ 5.05 / 269.35 / F 4.30

23.56

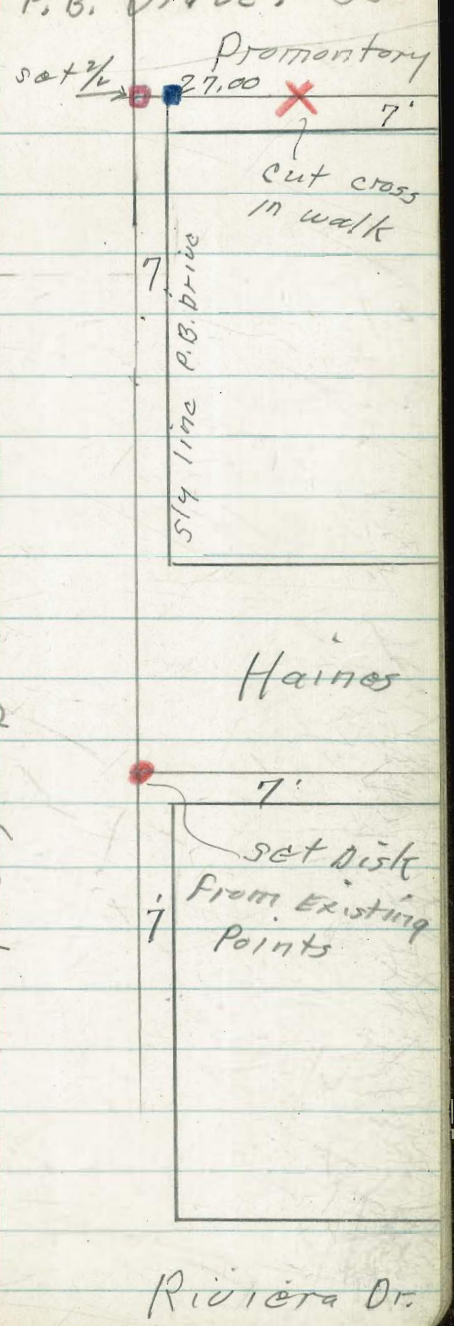
#2 5.01 / 269.52 / F 4.51

27.92

Ely. = #1 6.06 / 269.40 / F 3.34

Ch.

Nly. and wly side Cul-de-sac - = B.C. = #1



Pac. Beach Dr.

Riviera Dr. to Jewell 10055L 10056L 10057L

Storm Drain

Drain 7' North of ℄ P.B. Drive			3+00	54.86 35.80 C19.06
stakes 10' Rt. of ℄				
Stake for curve - Def = 5° - ch 17.61			2+50	52.11 35.52 C 16.59
Rad = 101'. 5 parts (#6 = E.C.) = 0+00				
			2+00	50.97 T.P. 35.24 C15.73
Tang. = 0+00 on				
#6 = E.C.	34.54 29.15 C 5.39	T.P.	1+50	49.30 34.96 Nail C 14.34
#5 = (0-15.88)	33.12 27.82 C 5.30		1+00	45.34 34.68 C10.66
	8.37 %			43.34 T.P.
#4 = (0-31.76)	31.70 26.49 C 5.21		0+67 0.56 %	42.16 34.50 C 7.66
#3 = (0-47.64)	30.63 25.16 C 5.47		0+65.5 = ℄ C.O.	
#2 = (0-63.52)	9.41 23.83 C 5.58		0+64	41.81 34.50 C 7.31
#1 = Exist C.O. = 0-79.40	28.51 22.50 C 6.01	x	0+32	8.15 31.83 C 6.32

Curve Δ-50° R-91' L:79.40 Sheet 10055-7L

P.B. Drain

End of pipe To North 0+11.16
E 45.78
38.19
C 7.59

stakes 10' East of ℄

0+25.16
End pipe to So
45.10
37.74
C 7.36

0+00 = ℄ C.O.	45.80 37.50 C 8.30	
5+99 = ℄ C.O.		
End. of pipe 5+97.5	45.58 37.50 C 8.08	
5+50	46.16 37.20 C 8.96	
5+00	47.20 36.92 C10.28	
4+50	48.75 36.64 C-12.11	
4+00	51.15 36.36 C 14.79	
3+50	53.66 36.08 C17.58	

B.M.#1 = 46.21
Lot.

Paci Beach Dr.
Rough grade
Jewel to Riviera Dr.

57

Set B.M. SE. Jewell & P.B. Drive
El. = 45.97

stakes 5' back of line

3+50	41.7 Rt	6.14 46.34 F 0.20	
3 ~	41.5 Rt.	5.80 46.15 F 0.35	
2+50	41.2 Rt	5.85 45.96 F 0.11	
2 ~	41 Rt	5.29 45.77 F 0.48	
1+50	40.7 Rt	5.31 45.57 F 0.26	
1 ~	40.5 Rt	6.29 45.38 C 0.91	N.-2.60
0+50	40.2 Rt	4.71 45.19 F 0.48	"X"
0+00 wly. line Jewell To North.		45.00	

1,100 to 5+00

P. B. Drive
Rough grade

				5,80		7,48
			1+35 N on line	A2.83		A3.26
				C.2.97		C4.22
0+22.5 Lt				5,38		7,36
			1+15 0-2'	A2.72		43.10
				C2.66		C4.26
0+20 Rt				5,68		7,49
			0+95 X-1'	A2.85		A3.15
Ingraham				C-2.83		C4.34
0+00				5,60		7,70
			0+75 0-1'	A3.19		A3.41
				C-2.41		C 4.29
				5,97		7,05
to North.			0+55 0 on line	A3.76		A3.89 X-5'
Ingraham				C-2.21		C3.16
Ely line						
5+00	42.5 Rt	6,75	0+22.5 Lt. 0-1'	6.02		4 —
		46.44		A5.11		
		C0.31		C0.91		
4+80	42.4 Rt	C.91	0+20 Rt	—		7,05
		46.54				A5.30
		C0.37				C1,75
4+40	42.2 Rt	7,00	To So			
		46.62	wly. Ingraham			
		C0.38	0+00 =	46.13		
4+00	42' Rt	6,54				
		46.54				
		X	0-05.7			46.50

P.B. Dr.
Rough Gr.

		South	North
0+64	N. 31	2.29	4.22
		51.02	51.15
		C 1.27	C 2.7
0+20	D 2	9.31	5313
		48.94	49.50
		C 0.37	C 3.63
0+00		48.00	51.95
			48.73 X-5'
wly Promontory Dr.			C 3.12
Ely Prom. Dr.		6.25	51.81
2+15		45.50	46.00
		C 0.75	C-5.81
1+95	D-2	6.16	9.71
		44.50	45.00
		C 1.66	C 4.71
1+75	N-0.30	6.28	8.09
		43.72	44.21
		C 2.56	C-3.88

P.B. Dr. - Rough grade

27' Mon. R.P. Cross EL: 46.65
Promontory Dr. + P.B. Dr.

		S.	N.
To South.			
Ely Hainas			
2+15		51.08	
1+94	D 5	5.54	
		52.18	51.87
		C 3.36	
1+64	D 5'	5.39	6.50
		52.60	53.00
		C 2.79	C 3.50
1+44		4.95	6.25
		52.78	53.36
		C 2.17	C 2.89
1+24		4.53	6.17
		52.71	53.37
		C 1.82	C 2.80
1+04		3.17	5.66
		52.40	53.01
		C 0.77	C 2.65
0+84	D-2	2.64	4.94
		51.83	52.33
		C 0.81	C 2.61

P.B. Dr. Rough Gr.

T.P. 27.64 Cross R.P. Nail Hammer
EL. = 5.135

stakes

Ely. Riviera Dr.
℄ 2+15

℄ 2+05	0-5	3.25 31.10 C 2.15	
1+72	0-4'	5.00 33.75 C 1.25	
1+39	N. 0.7 in	7.65 36.39 C 1.26	
0+94	N. -5'	A 1.93 40.62 C 1.31	
0+49		8.84 44.85 C 3.99	
0+04	0 min	~~49.09~~	
0+00		52.08 49.44 C 2.64	

Haines to So.
N/y line

P.B. Drive Sewer

0-107.5 = n/y line Jewel - to south

Sheet # 1005 G-L

Sta 1+37.5

Sewer Lat # 1

7.50
41.72
C- 5.78

5.78
42.2
1.5 %

M.H. # 1

3+00		C.07 41.45 C 4.62
2+50		5.91 41.10 C- 4.81
2+00	T.P.	5.60 40.75 C 4.85
1+50		5.40 40.40 C 5.00
1+00		5.20 40.05 C 5.15
0+50		5.02 39.70 C 5.32
0+00 M.H. #2		5.09 39.35 C 5.72

Curbs Pac. Beach Dr.
~~E of~~ Riviera Dr. to Jewell

INDEXED

Promontory to Haines

	South	North
1+17 Lt. ch. E.C.	2.25 52.63 F 0.38	
1+04.32 Rt	~~52.40~~	2.79 53.01 F 0.22
ch. B.C. 0+98 Lt.	1.65 52.24 F 0.59	
0+84.32	2.08 51.83 C 0.25	2.38 52.33 C 0.05
0+64.32 Lt. P.U.C	1.46 51.02 C 0.44	
0+52.16 Rt		1.06 50.92 C 0.14
0+32.16 Lt.	9.78 49.51 C 0.27	
0+20		9.69 49.50 C 0.19
Wly. Promontory 0+00	48.00	8.82 48.73 C 0.09

61

#3 B.C. Pac. Bch. Dr.

#2

#1 S.W. Rit. Promontory

Ext'd of B.C. Pac. Dr.

7.90
48.12
F 0.22

7.52
47.63
F 0.11

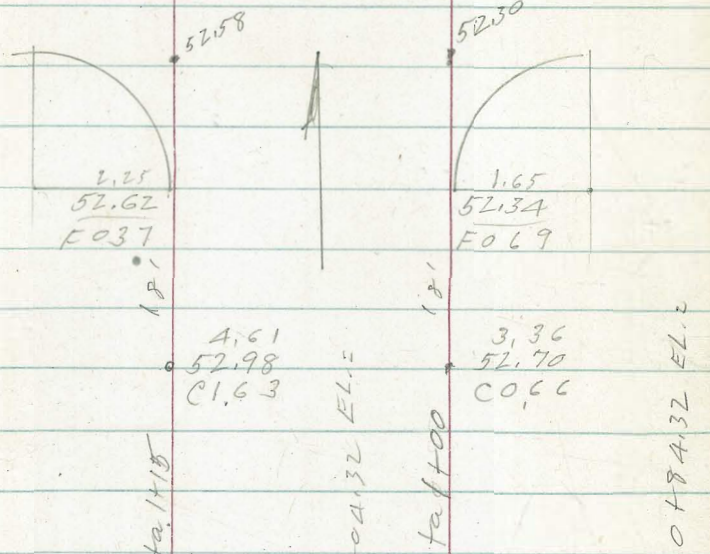
7.27
47.20
C 0.07

6.85
46.86

Ely. Haines 2+15	51.17	51.81	51.88 (2+07)
1+94.32 Exist. ch.	51.87	51.95	1.97 51.87
1+84.32	52.18	~~52.08~~	2.53 52.40 C 0.15
1+64.32	52.60 (plus grade)	52.39 52.45 F 0.06	3.05 53.00 C 0.05
1+44.32	52.78 (plus grade)	52.48 2.68 F 0.20	3.30 53.36 F 0.06
1+24.32		52.35 52.71 F 0.36	3.27 53.37 F 0.10

Alley Rel. Blk 2

between Promontory + Hainis



Alley Blk. 1

Riviera Dr. on Rx Exist. ℄

2+15	30.30	
℄ B.C. Rt. 2+02.3	0.84 31.32 F0.48	
1+50	F1.08	
1+17 ℄ Lt. ℄ E.C.	F0.77	
0+98 ℄ Lt. ℄ B.C.	F0.45	
0+50	F0.75	
Exist. ℄ 0+04.9	49.09	
0+00 Wly Hainis		

Assume El. 10+00

9 of 4p @ 0.06

F1.01

1.61
10.65
C0.96

Assume El. 10+00

9.75
10.00
F0.25

10.38
10.00
C0.38

Alley ℄ end set from take stake on P.I.

P.B. Drive

Curb inlets between stakes 5' Back of cb Faces

& Promontory Ingraham

Grade raised on crests of E.G.

Promontory Dr. E.L. -5+14.4 cb.

S.Ely Rd Promontory + P.B.

P.B. Dr.

B.C.

Chord - 845

cb. Ingraham to Promontory

Left back

1+

1+25 43.14 — 3.90 43.45 cb 0.45

1+15 43.12 — 3.64 43.60 C 0.04

0+98 5.00 43.22

0+95 ~~43.25~~ — 3.44 43.55 F 0.11

0+75 3.80 43.49 C 0.31 — 3.82 43.71 C 0.11

0+55 4.39 43.96 C 0.43 — 4.46 44.09 C 0.37

0+35 4.72 44.65 C 0.07 — 5.00 44.68 C 0.32

B.C.H. 5 0+22 4.86 45.11 F 0.25

0+17.5± B.C.R.X. — 45.30

0+00 = Nly Production Wly line Ingraham

Curbs

w/y. Promontory
2+90 = 0+00 P-61
8.31
48.73
F 0.42

2+70
7.64
48.16
F 0.52

2+55
7.15
47.70
F 0.55

2+35
6.59
46.98
F 0.39

2+15
5.93
46.40
F 0.17

2+12.5 B.C. 4
4.85
45.38
F 0.53

1+95
4.34
44.60
F 0.26
4.97
45.20
F 0.23

1+75
4.00
43.92
C 0.08
4.20
44.51
F 0.31

1+55
3.63
43.47
C 0.16
4.58
44.04
C 0.54

1+35
43.23
3.94
43.76
C 0.18

N.E. Cb. Ret. Ingraham & P.B. Dr.

Ingraham #5 = E.C.
46.43

	#4	#3	#2	#1	B.C.
	6.56	6.74	6.20	5.75	5.87
	46.38	46.32	46.32	46.40	46.47
	C 0.18	C 0.42	F 0.12	F 0.65	F 0.62
					P.B. Dr.

N.W. cl. Ret. Ingraham + P.B. Dr.

P.B. Dr.	#5 = E.C.	#4	#3	#2	#1	B.C.	Ingraham
	5.53	5.51	5.65	5.82	5.97	46.11	
	45.30	45.51	45.68	45.83	46.00		
	C 0.23	X	F 0.03	F 0.01	F 0.03		

Chord = 8.45
S.W. Ret Ingraham + P.B. Dr.

P.B. Dr.	#5	#4	#3	#2	#1	B.C.	Ingraham
4.86		5.20	5.44	5.62	5.38	46.39	
45.11		45.50	45.78	45.95	46.00		
F 0.25		F 0.30	F 0.34	F 0.33	F 0.62		

Cl. N'ly Side P.B. D'r
Jewell to Ingraham
0+00 = W'ly line Jewell

			E.C.C.	
2+50		F0.39	4+90	46.49
				5.95
2+00		F0.32	4+80	46.54
				F0.59
				6.08
1+50		F0.43	4+60	46.60
				F0.52
				6.19
1+00	Rake	F0.16	4+40	46.62
				F0.43
0+80				6.22
#3 = E.C.		F0.23	4+20	46.60
				F0.38
				6.12
#2		F0.24	4+00 P.V.C.	46.54
				F0.42
#1		C0.20	3+50	F0.44
= Existing CL		45.08		
0+00 P.O.C.		45.00	3+00	F0.39
		Meat		

Curb Stakes

Morenci

Littlefield to Tonopah 9/30/53

W.O. 32175

10166-7 L

10071 -L

10072 -L

10073 -L

10074 -L

	7.38	6.65
1+50	57.69	56.92
	FO.31	FO.27
	8.79	7.98
1+13 E.V.C.	58.76	57.98
	Co.03	X
	9.19	8.31
0+93	59.30	58.45
	FO.11	FO.14
	9.87	8.55
0+73	59.78	58.77
	Co.09	FO.22
	0.25	8.78
0+53	60.17	58.91
	Co.08	FO.13
	0.58	8.81
0+33	60.50	58.88
	Co.08	FO.07
also P.V.C.		
0+13=E.C.	60.68	58.78

0+00 = Sly line Littlefield

P.V.C.	7.47	7.79
0+70	47.86	47.54
	FO 39	Co.25
	8.53	8.62
0+41.5	48.93	48.53
	FO.40	Co.09
	9.71	9.30
0+13 = E.C.	50.00	49.53
	FO.29	FO.23

0+00 = Sly. line Ashor

3+75 = Nly. line Ashor.

	1.52	1.13
3+62 B.C.	51.58	50.88
	FO.06	Co.25
	1.81	1.47
3+50	51.93	51.22
	FO.12	Co.25
	3.75	2.98
3+00	53.37	52.64
	Co.38	Co.34
	5.00	4.46
2+50	54.81	54.07
	Co.19	Co.39
	6.20	5.57
2+00	56.25	55.50
	FO.05	Co.07

45.72

	East	Lt	west = Rt	
3+90 ± = B.C.	4.82 43.00		5.83 43.50	4.48
3+58 Lt. 42.93	C 1.82	3.58 43.32	C 2.33	43.74
3+57 Rt ~ 42.78 Top pipe	3.38	C 0.26	4.82	C 0.74
3+40	43.50	3.54	43.87	
3+30 Lt 42.60	F 0.12	C 0.95		4.33
3+06 Rt 42.55		3.48 43.60		44.13
2+90	4.14 44.00	F 0.09	4.31 44.25	C 0.20
Top Lat = 42.33	C 0.14	4.07 4.04 44.19	C 0.06	
2+71 Lt.				
2+40	4.35 44.50	F 0.15	4.65 44.62	
	F 0.15		C 0.03	
1+90 E.V.C.	4.89 45.00		4.87 45.00	
	F 0.11		F 0.13	
1+70	4.92 45.25		5.11 45.21	
	F 0.33		F 0.10	
1+50	5.34 45.59		5.43 45.52	
	F 0.25		F 0.09	
1+30	5.95 46.02		6.03 45.95	
	F 0.07		C 0.08	
1+10	6.22 46.54		6.45 46.37	
	F 0.32		C 0.08	
0+90	7.16 47.16		6.96 46.90	
	X		C 0.06	

Moreno

9.53
49.53

#3 E.C.

50.01

9.24
49.68
F 0.44

S.W. Rot.

#2

0.10
50.21
F 0.11

8.96
49.56
F 0.60

#1

0.20
50.42
F 0.22

8.56
49.30
F 0.74

B.C.

9.32
50.60
F 0.28

Ashton

Ashton

9.00
49.90
F 0.90

E.C. #3

1.25
51.27
F 0.02

0.60
50.24
C 0.36

N.W. Rot

#3 1

N.E. Rot. #2

1.24
51.26
X

0.77
50.58
C 0.22

#4

1.64
51.33
C 0.31

#3 B.C.

51.58

50.88

Moreno

Moreno

8.93
58.78
C 0.15

E.C.

0.27
60.68
F 0.41

8.85
58.66
C 0.19

7.01
58.58

S.W. Rot.

C 0.43

S.E. Rot

1.34
60.82
C 0.52

2.31
60.89
C 1.42

Little Field

Tonopah

Exist ch.
0 + 86.57
1.00
40.98
C 0.02 - Meet ch.

0 + 76.57
1.60
41.63
F 0.03

0 + 66.57
2.30
41.94
C 0.36

0 + 39.78
2.66
42.28
C 0.38

0 + 13 = E.C.
2.76
42.62
C 0.14

4.57
43.44
C 1.13

4.39
43.41
C 0.92

43.56

N. w. Rot.

Tonopark
#3
E.C.
2.76
42.62

N. E. Rot.
#2
2.91
42.75
C 0.16

#1
3.39
42.90
C 0.19

43.00 B.C.

Moreno

Armada terrace

INDEXED

Drain - Talbot to Bessemer.

Cuts on top of ℄ 2.5 East of ℄ drain.

0+55 = bottom of Conduit Telephone 37.35

0.5 East of ℄ = Top. bell EL. 35.87

0+52.5 Top of 4" Lat. EL. 35.77

3+75.5 = Ctr. C.I. 3.55 47.44 C 6.11

3+68 Pipe End of 53.05 47.44 C 5.61

3+46 3+52 B.C. & 3- 51.26 46.60 C 4.66

3+42 Brk. 51.02 46.45 C 4.57

cont. on left page.

2+93 6"10 8.52 43.51 C 5.01

2+44 Brk. 5.62 40.57 C 5.05

2+24 Brk. 44.76 39.74 C 5.02

1+83 2"10 43.92 38.92 C 5.00

1+42 Brk. 43.14 38.10 C 5.04

1+00 42.25 37.00 C 5.25

0+50 2"10 40.94 35.70 C 5.24

0+16 = E.C. 40.68 34.82 C 5.86

0+00 start pipe 40.00 34.40 C 5.60

0+00 = = I.E. existing C.I.

Diamond St.

Ingraham to Haines

Curb grades W.O. 31913

B.M. = L+T & Diamond } Ely. Ingraham } El. = 83.59

Page-74- Jewell St Returns

Ingraham

E.C. #4 3.10 / 83.00 / C0.10

3.41 / 83.15 / C0.26 #3

S.E. Return. #2

3.95 / 83.30 / C0.65

4.07 / 82.45 / C0.62 #1

4.17 / 83.63 / C0.54 B.C.

Diamond

Ingraham

4.70 / 84.40 / C0.30

N. E. Ret. -

4.76 / 84.20 / C0.76

4.15 / 83.98 / C0.17

4.05 / 84.00 / C0.05

4.3 / 84.12 / C0.31

Diamond

Diamond

4.91 / 82.30 / C0.61 #4 E.C.

N. W. #3 Ret.

3.07 / 82.45 / C0.62

3.05 / 82.60 / C0.45 #2

2.50 / 82.80 / F0.30 2.28 / 82.80 / C0.45 #1

3.44 / 83.00 / C0.44 B.C.

Ingraham

2+80	8.90 / 78.15 / C0.75
2+40 E.O.C.	9.05 / 78.32 / C0.73
2+20	8.80 / 78.45 / C0.35
2+00	8.88 / 78.66 / C0.22
1+80	8.91 / 78.94 / F0.03
1+60 P.O.C.	79.43 / 79.30 / C0.13
1+10	0.55 / 80.30 / C0.25
0+60	1.64 / 81.30 / C0.34
0+10 E.C.	2.91 / 82.30 / C0.61
Ingraham	

Diamond St. curbs — — Lamont to Jewell ~~Kendall~~ 71

107.51 T.P.

		3 — F 0.50	C 0.20 ~~F 0.32~~
Haines		2+~~45~~ 2+50 F 0.46	C 0.08 ~~F 0.56~~
5+00 Existing ℄	7.14 77.16		
		1+95 ~~2+~~ F 0.29	C 0.09 ~~F 0.68~~
4+90 Ch. B.C.	7.08 77.21 F 0.13	1+50 F 0.01	C 0.29 ~~F 0.60~~
4+45	7.74 77.41 C 0.33	1 — F 0.28	C 0.71 ~~F 0.32~~
4+00	8.02 77.61 C 0.41	0+70 C 0.23	C 1.23 ~~C 0.12~~
3+60	7.67 77.79 F 0.12	BM 0+40 6.89 106.13 C 0.76	7.45 106.55 C.34 C 0.90
3+20	8.28 77.97 C 0.31	w/y Lamont 0+00 106.15	C.95 106.87

Diamond St

6+70	F0.09	F0.04
6+30 Brk	3.06 103.20 F0.14	3.18 103.50 F0.32
wly Kendall 5+80	3.77 103.80 F0.03	4.63 104.30 C0.33
5+40	103.60 104.00 F0.40	4.20 104.52 F0.32
Ely. Kendall 5+00	3.86 104.20 F0.34	4.38 104.75 F0.17
4+50	C 1.09	C 1.84 ~~C 1.70~~
4 —	C0.37	C1.54 ~~C 1.30~~
3+50	C0.32	C0.87 ~~C 0.47~~

Ely. Jewell St.

10+80		
℄ B.C. 10+70	2.96 93.52 F0.56	
10+40	F0.17	
9+90	F0.46	
9+40	F0.69	
8+90	F0.58	
8+40	F0.56	
Brk 7+90	99.05 99.70 F0.65	Exist. ℄. 0.24 ✓ 100.23
7+50	F0.31	F0.16
7+10	F0.66	C0.07

95.10

Diamond St. cls.

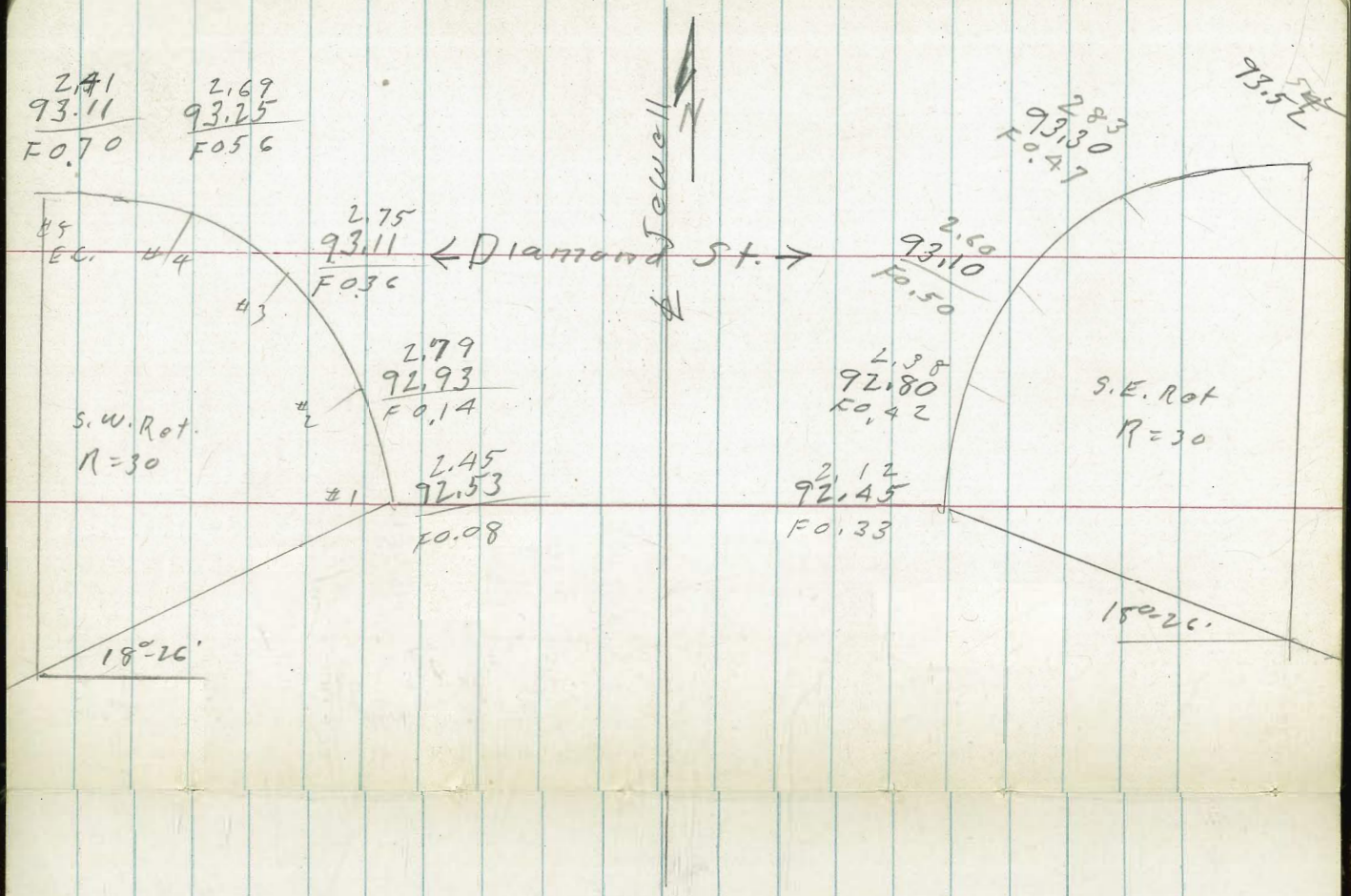
Jewell to Ingraham

		S curbs	N curbs
3+~~50~~ +48		C0.04	C0,32
3+00		F0.20	C0.20
2+50 Rake clg.		F0,14	C0.05
2+00		C0.11	C0.07
1+50		F0.04	C0.36
1+00		F0.60	C0.31
0+60. on Rk. Brk	F0.60	F0.65	2.45 92.45
E.C. 0+10	93,11	93.11	93.24
			93,40
0+00 = Wly Jewell			

X-t Diamond + Ely. 7' Jewell El.: 93,11

	S cl.	N cl.
Wly Ingraham 5+10 =		
C.B.C. 5+10	83.63	84.12
Brk on Rt. 4+80	C0.32	4.63 84.46 C0.17
4+50	C0.05	C0.92
4+00	Grade	C1,30

on ck.ed


2.41
93.11
F0.70
2.69
93.25
F05 6
2.75
93.11
F0.3c
← Diamond St. →
Jewell
2.83
93,30
F0.47
93.5
2.60
93,10
F0,50
2,38
92,80
F0,42
2,12
92,45
F0,33
2,79
92,93
F0,14
2,45
92.53
F0.08
#5
E.C.
#4
#3
#2
#1
S.W. Rot.
R=30
S.E. Rot
R=30
18°-26'
15°-26'

Anna Ave west of Sherman

Curb. stakes 1-22-54

Sheet #10624-L

stakes on edge of Pave. = 3' back of curb line

B.M.= disk & Anna at & Sherman

N.ly. Side Anna. Ave. El.=

	~~ch. Grade~~	Edge of Pave		Curb Gr.	Edge of pave
3 ~~	~~11.43~~	11.59 11.13 C 0.46			
2+50	~~11.00~~	10.90 10.70 C 0.20	#3 & Banjo	3.12 13.02 C 0.10	
2 ~~	~~10.57~~	10.44 10.27 C 0.17	#2	3.51 12.86 C 0.65	
1+50	~~10.14~~	10.14 9.84 C 0.30	#1	3.45 12.65 C 0.80	
1 ~~	~~9.71~~	9.70 9.41 C 0.29	ch. B.C. 4+19.14	3.52 12.45 C 1.07	
0+50	~~9.28~~	9.99 8.98 C 1.01	A ~~	~~12.29~~	3.32 11.99 C 1.33
0+00=E.C.	9.11 8.85 C 0.26 Top of Ch.		3+50	~~11.86~~	1.81 11.56 C 0.25

INDEXED

Alley Blk 58
H.M. Higgins Add.

C.H.S.

10-23-53
W.O. 31797

B.M. = N.W. B.P. 27th + B. = EL. = 196.97

			T.P.				
1+00 N-0.60	9.72 208.80 C 0.92	8.70 208.80 F 0.10	D-2'	99.18 T.P. 200.51 T.P.		210.78 T.P. 202.05	
0+80	9.02 208.55 C 0.47 C 0.55	8.47 208.55 F 0.08	X-4' Grade	2+80 D-2'	9.65 201.05 F 1.40	0.57 201.05 F 0.48	D-2'
0+70 N-0.50	8.77 208.30 C 0.47 C 0.57	8.15 208.30 F 0.15	X-2' F 0.05	2+60 D-2'	4.09 202.80 C 1.29	2.76 202.80 F 0.04	D-1'
0+60 N-0.50	8.60 207.75 C 0.85	7.63 207.75 F 0.12	D-1.8	2+40 D-2'	5.92 204.20 C 1.72	3.94 204.20 F 0.26	D-1'
0+50 D -0.80	8.30 206.85 C 1.45	6.89 206.85 C 0.04	D-2'	2+20 D-2'	5.43 205.40 C 0.03	5.85 205.40 C 0.45	X-2'
0+40	7.02 205.30 C 1.72	6.23 205.30 C 0.93	D -1.40	2+00 D-2'	7.33 206.50 C 0.83	6.40 206.50 F 0.04	D 2'
0+00 D-2'	197.20	197.30		1+80 D 2'	8.30 207.40 C 0.90	7.64 207.40 C 0.24	D-2'
Ely line 27th				1+60 N-2'	8.92 208.10 C 0.82	8.59 208.10 C 0.49	D-1
				1+40 N-2'	9.07 208.50 C 0.57	9.35 208.50 C 0.85	N-1.90
				1+20 N-2'	9.13 208.75 C 0.38	9.10 208.75 C 0.35	D-2'

3+41 = Elg. face cut off wall

3+40 D-2'	2.24 191.00 C 1.24		4.75 191.00 C 3.75	N-1 60
3+20 D-2'	5.77 195.00 C 0.77	TIR	6.97 195.00 C 1.97	N-1 41
3+00 D-2'	8.45 198.40 C 0.05		9.92 198.40 C 1.52	X-2'

INDEXED
MYER
APR 29 1954

Alley # 88
E.W. Morse's Sub.
West of 30th
Between B. + C. Sts.

10.12
14.75
10-26-53
WO. 31682
L-10305

P.O.C. 2+00	N-0.25	3.73 213.34 C 0.39		3.91 213.34 C 0.57	□-2'				
1+70	X-2'	4.07 213.89 C 0.18		4.76 213.89 C 0.87	□-2'				
E.U.C. 1+40	X-2'	4.44 214.44 X		5.44 214.44 C 1.00	X-3'				
1+20	N.-0.35	5.13 214.53 C 0.09		4.87 214.53 C 0.34	□-2'				
1 ~	N. 0.04 IN.	5.28 213.92 C 1.36		4.58 213.92 C 0.66	□-2'				
P.O.C. 0+80	N.-0.06	3.45 212.61 C 0.84		2.77 212.61 C 0.16	N-0.17				
0+50.	X-2'	0.40 210.12 C 0.28		10.08 210.12 F 0.04	□-1'				
0+20	X -2.19	17.99 207.63 C 4.36		9.03 207.63 C 1.40	□-2'				
wly. 30th 0+00 =		206.03		207.20					

FB 2221-P1

2+95 Rt. = (S) #1

220.32 NEB.P.
30th + B.

79

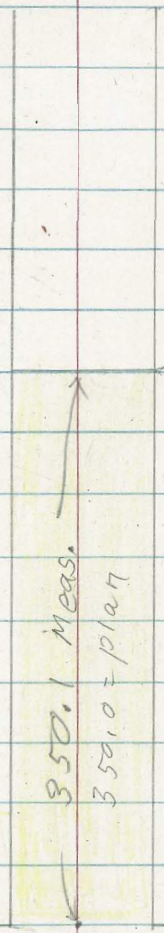
9.12
203.60 — □ 5' Rt.
C 5.52

End of Job 3+50	□-2'	2.33 203.41 F 1.08		4.10 203.41 C 0.69	□-2'				
3+40	□-2'	3.09 204.47 F 1.38		5.07 204.47 C 0.60	□-2'				
3+20	□-2'	6.29 206.32 F 0.04		8.73 206.32 C 2.41	X-0.53				
3+00	N-0.55	8.06 208.40 F 0.34		8.78 208.40 C 0.38	N-0.32				
2+80	N-0.45	10.17 210.00 C 0.17		9.85 210.00 F 0.15	□-2'				
2+60	N-0.45	2.07 211.13 C 0.94		1.84 211.13 C 0.71	□-2'				
2+40	N-0.50	3.03 212.01 C 1.02		2.32 212.01 C 0.31	□-2'				
2+20	N-0.35	3.33 212.79 C 0.54		3.62 212.79 C 0.83	X-2'				

Pavement - As built.
Alley 88
E.W. Morse Add. 1/15/54

C.H.S.
P. Smith
Begg
Shelin
Pullen

sheet 10305-L



P.O.C 2+0

1+7

E.O.C 1+A

1+20 End Conc. Pave

1 ~

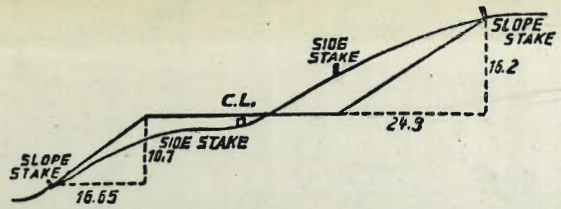
P.O.C 0+8

0+3

0+2

wly. 0+0

Wly line 30th



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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