

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Hookwall at Dyka 7354

62339
78.67
4462

MICROFILMED

APR 15 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side of road
make for any width roadway, slope 1% to 1%
It is assumed that the road is 12 ft. wide

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent, External and Curve in
any other degree, divide by degree of curve and
add direction found in column of constants.
Degree of curve with a given arc or chord
by dividing tangent (or constant) by
the given tangent (or constant).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the degree.

3-4 Riley - N.E. from Pine
5-^(also 55) Napa - West of Riley
5. Linda Vista Rd. South of Napa
6-7 " " North + East " "
8 - Mollie St.
9 ^{Alley} BIK "D" Mollie East.
9 Lauretta - East of Mollie
10 - Napa - S.E. of Riley
10-12 Gains N.E. of Napa
13-14 AZUSA
15 - Alley BIK 6 Silver Terrace.
16-17 Lauretta Azusa to Brunner
17-20 Mildred - Azusa to Brunner
20-21 Colusa St + Alley BIK 12.
21-22 JOSEPHINE ST.
23-24 { BIK 387 J.P. Jones Sub
P.L. #1101
25-29 { Benicia +
Riley East of Benicia
27 Yuma - East of Benicia

East of Benicia
28 Gaines West " "
29-31 - ANDRADE ST
31-32 COLUSA - North of Andrade.
33-34 EUREKA " " "
34 - Yuma - West of Eureka
35-36 Fresno St
36-38 { Donahue St
Easement lots 14+15 BIK 2
38 Riley St. West of Donahue
39 " " East " "
40-42 Alley BIK 2-3+4 #11
42 Huememe St.
43-44 Easement BIKs 2-8+13
44-46 Lauretta - East of Brunner
{ Eureka North of Lauretta
46-47 { Alley BIK 14
48-49 Alley BIKs 6+7
49 Goshen (North of Alley BIK 6)
50 Goshen St. + Alley BIK 14

Cont. P. 2

- 51-54 Alleys BIK ¹⁵ 42 } Ocean Beach
- 55- Napa St. Sewer. - west of Greenwood
- 56-57 Beaumont. Colima to Midway
 & 60 (pave) Westbourne
- 58- Monte Vista to Belvedere
- 61- { Darnall school grounds
 R.P. for. A
- 62- Drain Sand Rock Grade
- 63-65 { Alley BIKs 5 + 24. Ocean Beach
 Guizot to Ebers
 Between Newport + Niagara.
- 66- Drain Lot. 13 Lomas De La Jolla #1
- 67-68 Alley BIK 9 - La Jolla Park
- 69- { Fergus St. also
 62nd st.
- 77- Drain. - Virginia Way.
- 78 Alley BIK 11 North Shore Highlands

Silver Terrace Sewer

INDEXED

Riley St. - N.E. from Pine

		9702-L			12.80
		9707-L	5+50	1.570	-0.62
		9712-L			C-13.42
2+80		11.86			13.05
		-1.56	5+19.7		-11.07
		C13.42 = C13.39			C14.12
2+40		11.70			
		-1.62	5+09.68 M.H.#1		-1.22
		C13.32 = 13.26			
2+00		11.25			12.73
		-1.68	4+99.7		-1.23
		C12.93 =			C13.96
1+60	Trace El.	10.60			12.68
		-1.74	4+80		-1.26
		C12.34 = C12.34			C13.94
1+20	Trace El.	9.35			12.42
		-1.80	4+40		-1.32
		C11.15			C13.74
0+80		8.30			12.10
		-1.86	4+00		-1.38
		C10.16			C13.48
0+40		7.93			12.03
		-1.92	3+60		-1.44
		C-9.85			C-13.47
0+00					11.99
Exist M.H.#5		8.76	3+20		-1.50
Pine St.		-1.98			C13.48
		10.74			plan grade from here on.

0+00 to 1+60 Set from Exist. M.H.
2+00 on Set from B.M.#1

0.1570

plan grade from here on.

Riley - East from Pine St.

4

9+00
0.49

11.70
4.21
C 7.49

8+59⁶⁸ M.H.#82

12.15
4.03
C 8.12

8+50

12.10
3.88
C 8.22

8+00

11.32
3.13
C 8.19

7+50¹¹

12.30
2.58
C 9.72

7+00

12.43
1.63
C 10.80

6+50

12.65
0.88
C 11.77

6+00

12.74
+ 0.13
C 12.61

plyg.

10+09⁶⁸

10.90
4.63
C 6.27

10+00

10.80
4.61
C 6.19

9+50

10.45
4.41
C 6.04

Napa St.
INDEVED

West of Riley

Linda Vista Rd.
South of Napa.
West

9707-L
9712-L

9707-L
9722-L

Linda Vista Rd.

3+30 M.H.#84

5.38

3+12.80

~~3+028~~
~~3+00~~

13.26
5.14
C8.12

2+50

13.25
4.03
C9.22

2+00

12.79
2.93
C9.86

2+45 M.H.#83

14.31
6.61
C7.70

1+50

12.73
1.93
C10.80

2+00

13.95
6.38
C7.57

1+00 $\frac{0}{2}$

12.64
+0.88
C11.76

1+50 $\frac{0.50}{0}$

13.85
6.13
C7.72

0+50

12.66
-0.17
C12.83

1+00

13.52
5.88
C7.64

0+10

12.87
-1.01
C13.88

out.
12.53

0+50

13.29
5.63
C7.65

0+00 = M.H.#1
Riley + Napa

-1.22

0+07 (on RT)

13.23
3.14
C7.82

Nail
13.23
7.27

0+00 = M.H.#84

5.38

INDEX DA VISTA RD.

JUN 25 East from Napa.

3+31.07	18.64 9.69 C-9.04	
M.H.# 85		
3+10 - P.O.T.	16.57 9.10 C-7.57	9.10
Δ 24°-09' H.		18.64 TIP.
3+00	16.60 8.98 C-7.62	
2+50	14.93 8.38 C-6.55	
2+00	14.52 7.78 C-6.74	TIP
1+50	14.15 7.18 C-6.97	
1+00	13.78 6.58 C-7.20	
0+50	13.48 5.98 C-7.50	
0+07 - Nail 7' H.	13.29 5.46 C-7.83	13.29
0+00 = M.H.# 84	5.38	

6

9707-L	
9708-L	
9722-L	
6+505	5.25 17.20 C-8.05
M.H.# 86 P.O.T	24.63
6+25 - P.O.T 6+27.48	16.66 7.97
6+00	24.00 16.03 C-7.97
5+50	22.76 14.86 C-7.90
5+00	21.41 13.66 C-7.75
4+50	20.14 T.P. 12.46 C-7.68
3+94.30 E.C	18.75 11.12 C-7.63
3+73.22	18.01 10.61 C-7.40
3+52.15 P.R.C.	17.46 10.11 C-7.35

Linda Vista
North + East from Napa.

9+45 $\frac{1}{11\%}$
33.58
24.94
C 8.64

$\Delta 51^\circ - 23' - 30''$ L

9+38⁰⁶ M.H.# 87 24.17

9+31¹
33.11
23.97
C 9.14

9+00
32.18
23.20
C 8.98

8+50
30.65
22.00
C 8.65

8+00 $\frac{2.4\%}{}$
29.20
20.80
C 8.40

7+50
27.87
19.60
C 8.27

7+00
26.57
18.40
C 8.17

6+24.71

11+63⁰⁶ - plug.

44.11
36.67
C 7.44

11+50

42.92
36.15
C 6.77

11+00

40.56
34.15
C 6.41

10+50 $\frac{0\%}{A}$

39.15
32.15
C 7.00

10+00

9+95⁰⁶

35.50
29.95
C 5.55

$\Delta 54^\circ$ RT

9+88⁰⁶ M.H.# 95

29.67

9+81⁰⁶

36.72
28.90
C 8.82

9+63⁰⁶ $\frac{11\%}{}$

35.01
26.92
C 8.15

INDEXED

Mollie St

Nail-Tip pole*

EL=33.70

8

9708-L

9712-L

Mollie St + Alloy-BLK "D"

2+00

1+50

32.05
25.17
C-6.88

1+00

0.4%

2.20
24.97
C-7.23

0+79.64

2.50
24.89
C-7.61

3+06.54 Plug

197
25.80
C-6.17

0+74.64 M.H.# 88

24.87

2+71.64

191
25.66
C-6.25

0+69.64

2+36.64

0.4%

177
25.52
C-6.25

0+37.3

0.4%

2+31.64 M.H.# 90

25.50

0+05

2+26.64

0.4%

2.00
25.48
C-6.52

0+00 M.H.# 87

24.57

2+00

0.4%

321.5
25.37
C-6.78

Linda Vista Rd.

INDEXED

Alley BIK "D." Addl
Mollie - East

Silver
to Terrace
9708-L
9712-L

3+50 ^{2.6%} Plug

40.90
34.24
C-6.66

P.O.T.
3+00 M.H.#89

39.10
32.92
C-6.18

2+50

7.63
31.62
C-6.01

2+00

6.22
30.32
C-5.90

1+50

35.00
29.02
C-5.98

1+00

2.6%

4.14
27.72
C-6.42

0+50

3.16
26.42
C-6.74

0+05

32.75
25.25
C-7.50

0+00 = M.H.#88
Mollie St.

25.12

INDEXED

Lauretta
East of Mollie

9708-L
9713-L

9

3+50 Plug

34.63
27.15
C-7.48

Set B.M.
Nail in
pole #5381
EL = 33.76
opposite
sta. #40

3+00 M.H.#91 P.O.T.

35.59
26.95
C-8.64

2+50

34.67
26.75
C-7.92

2+00

3.94
26.55
C-7.39

1+50

0.4%

33.13
26.35
C-6.78

1+00

2.65
26.15
C-6.50

0+50

2.30
25.95
C-6.35

0+05

32.25
25.77
C-6.48

0+00 = M.H.#90
Mollie St.

25.75

INDEXED

Alapa S.E. of Riley 9702-L

2+40

13.15
-0.86
C14.01

2+00

13.11
-0.92
C14.03

1+60

13.74
-0.98
C-14.72

1+20

12.90
-1.04
C13.94

0+80

12.80
-1.10
C13.90

0+40

12.47
-1.16
C13.63

0+10

12.73
-1.20
C13.93

0+00 M.H.#1

-1.22

Riley St.

INDEXED

Gaines - N.E. of Napa. 10

5+00

9.57
-0.47
C-10.04

4+60

9.93
-0.53
C10.46

4+20

9.66
-0.59
C-10.25

3+80

10.37
-0.65
C11.023+55²⁸10.81
-0.68
C11.49

Δ 90°-Lt

N.E. Mon
9.253+50²⁸ M.H.#2

-0.69

3+45³10.99
-0.70
C-11.69

3+20

11.32
-0.74
C12.07

2+80

12.79
-0.80
C13.59

Gains - East of Napa.

9705-L
9712-L

S.W.B.P. 62nd & Brook 717

11

Set. El. ~~245.14~~

7+00	10.80 4.75 C 6.05	
6+50	10.02 2.55 C 7.47	
5+98		
6+93	8.50 -0.48 C 8.02	+0.04 North East
5+93	8.50 -0.33 C 8.17	+0.04 North East
6+20		
5+83	8.75 -0.35 C 9.10	
5+40	9.26 -0.41 C 9.67	

10+00	0.48%	27.36 17.10 C 10.26
9+69	P.Oit. M.H.#41	25.55 16.95 C 8.60
9+50		24.24 16.05 C 8.19
9+00	4.6%	20.75 13.75 C 7.00
8+50		6.98 11.45 C 5.53
8+04.37		14.81 9.36 C 5.45
7+94.37	$\Delta 38^{\circ} 38' - 30''$ RT. M.H.#40	8.90
7+84.37		14.11 8.46 C 5.65
7+50	4.4%	12.33 6.95 C 5.38

22.817P

Gaines - East of Napa

12+50

31.78
25.52
C 6.4 C

12+00

0.4%

31.07
25.37
C 5.75

~~11+90.94~~

A.O.T.

11+90.94

D.M.H.# 42

west
30.99
18.01
12.98

30.99
25.28 East
5.71

11+81

31.02
17.97
C 13.05

11+50

30.71
17.82
C 12.89

11+00

0.48%

29.58
17.58
C 12.00

10+50

29.01
17.34
C 11.67

end of line

14+20.94 M.H.# 31

32.04
26.20
C 5.84

14+00

32.91
26.12
C 6.79

13+50

0.4%

32.50
25.92
C 6.58

13+00

32.38
25.72
C 6.66

INDEXED AZUSA

Gaines to Mildred

9705-L

9708-L

9722-L

RM#2315C

13

8' RT

5+50

20.70

24.06

C 6.64

part

2+60 M.H.# 43

6.39

19.05

C 7.34

5+00

2.1%

9.82

23.91

C 6.81

2+50

26.25

19.01

C 7.24

4+86.23

9.50

22.72

C 6.78

2+00

26.43

18.81

C 7.62

4+86.23 M.H.#92 Alloy South 22.15 - 22.61 north

1+50

27.43

18.61

C 8.82

4+76.23

9.19

22.07

C 7.12

1+00

2.4%

28.95

18.41

C 10.54

4+50

9.07

21.71

C 7.36

0+50

30.30

18.21

C 12.09

4+00

1.4%

8.86

21.01

C 7.85

0+10

0+05

31.61

18.05

C 13.56

3+50

27.85

20.31

C 7.50

0+00 D.M.H.#42

18.01

3+00

26.98

19.61

C 7.37

Gaines

AZUSA

1A

8+00

43.23
36.30
C 6.93

7+50

9.02
33.30
C 5.72

7+00

6.03%

35.69
30.27
C 5.42

6+50

33.30
27.26
C 6.04

6+27.23

32.87
25.87
C 7.00

Mildred

9+30.23 - M.H.# 45 44.15

Lautetta St

6+22.23 - M.H.# 44 25.57

9+25.23

52.53
43.88
C 8.65

6+17.23

32.59
25.47
C 7.12

9+00

6.03%

50.05
42.32
C 7.73

6+00

2.1%

32.19
25.11
C 7.08

8+50

46.31
39.34
C 7.00

Alley BIK G
Silver Terrace
INDEXED

9705-L
9721-L

15-

2+50 29.09 40²³ C11¹⁴

2+00 ^{5%} 26.59 35²⁷ C9¹⁸

1+50 24.09 34²³ C10¹⁴

P.O.T.

1+39 M.H.#93 23.54 33³³ C9²⁹

1+00 23.15 31⁴¹ C8²⁶

End-line

4+24 = M.H.#94 37.79 47³⁶ C9⁵⁷

0+50 ^{5%} 22.65 26⁵⁸ C-3⁹³

4+00 36.59 46⁸¹ C10²²

0+05 3+50 34.09 45⁵⁰ C10²¹

0+00 = M.H.#92 22.15 26⁴⁷ C-4³²
AZUSA ST.

3+00 ^{5%} 31.59 43⁵⁰ C-11⁴¹

INDEXED

LAURETTA

Azusa to Brunner

9708-L

9709-L

9713-L

SRT182
725

16

SRT2+50
8.8%35.40
29.57

C-583

6+75

6235
53.22 C-913

6+25

6018
51.57 C-861

Δ 3°-03'-26" Lt.

2+25 MH#78

34.30
27.37

C-693

5+75

5846
49.92 C-818

2+00

33.14
27.17

C-597

5+25
3.3%5624
48.27 C-797

1+50

32.01
26.77

C-524

4+75

5460
46.62 C-7981+00
0.8%31.29
26.37

C-492

P.O.T.
4+25 M.H.#795298
44.97 C-801

0+50

31.46
25.97

C-549

4+00

5182
42.77 C-905

0+05

32.70
25.61

C-709

3+50
8.8%4824
38.37 C-987

0+00 = M.H.#44

32.57
25.57

C-700

3+00

4115
33.97 C-718

AZUSA ST.

End of Job.

10+85. M.H.#81 77.56
66.75 C-1080

10+50 75.61
65.60 C-109

10+00 72.38
63.95 C-843

9+50 69.31
62.30 C-701

9+00 67.93
60.65 C-728

8+50 67.18
59.00 C-818

8+00 66.05
57.35 C-820

P.O.T.
7+55- M.H.#80 64.83
55.86 C-897

7+25 63.97
54.87 C-90

Mildred - Azusa to Brunner 17

INDEXED

JUL 25 1951

P.O.T.

2+61.16 M.H.#46 4.00
48.59
C 5.41

2+50 T.P. 56.63
3.06
48.40 8' RT.
C 4.66

2+00 2.50
47.55
C 4.95

1+50 52.27
46.70
C 5.57

1+00 3.80
45.85
C-7.95

0+50 53.08
45.00
C 8.08

0+05 52.30
44.24
C 8.06

0+00 = M.H.#45 44.15
AZUSA ST.

3.3%

1.7%

Mildred

Nail in pole
PA898
EL. = 69.91

18

5+31.33

7.70
53.18
C- 4.52

5+11.16 ¹⁰/₁₁

1.7

4+91.16

65.45
52.50
C 12.95

Benecia st.

Δ 90°-15'-30" RT

4+86¹⁶ M.H.#47

5
52.11

4+81¹⁶

65.45
52.33
C- 13.12

4+50

64.64
51.80
C 12.84

4+00 ¹⁰/₁₁

1.7

65.05
50.96
C 14.11

3+50

61.02
50.10
C 10.92

3+00

56.17
49.25
C 6.92

6+45
6+50

1.5

6+38.8

J.P.O. T.M.M.

6+33.82 M.H.#49

6+28.82 64.99
54.92
6+28.8 C 10.07

6+00

5+

1.7

5+50

5+41.31

Δ 89°-28' Lt.
5+36.31 M.H.#48

69.10 69.09
56.46 55.99
C 12.64 C- 13.10

64.99 66.71
54.92 55.00
C 10.07 C 11.71

8.32
54.34
C 3.98

7.00
53.49
C 3.51

57.02
53.34
C- 3.68

5
53.26

Mildred

MILDRED

19

T.P. = 30' A.P. Nail to Mon.

96.87 = EL.
Colusa + Mildred

8+40

83.80
74.51
C 9.29

10+50

104.02
96.54
C-7.487+97 ⁸² 9.5%81.71
70.50
C-11.2110+04 ⁴⁰ 13.6%9.29
90.34
C-8.95

Josephine

Colusa St.

7+92 ⁸² M.H.#50

70.03

9+99 ⁴⁰ = M.H.#55

89.66

7+87 ⁸²~~81.09~~ 81.09
~~69.55~~ 69.55
C11.54 C11.549+94 ⁴⁰ 9.5%97.85
89.14
C8.71

7+75

68.33

9+52 ⁸² = End. C.I.5.90
85.23
C 0.677+15 ^{9.5%}
7+50~~78.50~~ 78.50
~~65.49~~ 65.49
C12.54 C-13.019+34 ⁸² = Pier2.79
83.52
F 0.73

7+25

63.58

Start o.I. Pipe

6+95
7+00~~76.47~~ 76.47
~~60.74~~ 60.74
C15.26 C-15.739+16 ⁸²4.15
81.81
C-2.346+70
6+75~~74.24~~ 74.24
~~58.36~~ 58.36
C-15.71 C15.88

8+80 9.5%

84.86
78.31
C-6.55

Mildred

30' R.P. Nail to \pm Mon. }
Colusa + Mildred } EL. = 96.87

Erid of line
12+8A⁴⁰ plug
22.32
114.97
C-7.35

12+50
21.60
114.20
C-7.46

12+00 ^{2.2%}
20.22
113.10
C-7.12

P.O.T.
11+66⁴⁰ M.H.# 56
7.86
112.37
C-5.49

11+50
6.92
110.14
C-6.78

11+00 ^{13.6%}
110.93
103.34
C-7.59

COLUSA St North from MILDRED ²⁰

INDEXED + ALLEY BLK 12 - Amended Map of Silver Terrace.

Sheet 9709-L

" 9719-L

Δ 90°-30' RT
1+35 = M.H.# 57
90.61

1+30
101.48
90.57
101.28
90.57
C 10.91
C 10.71
100.63 = T.P.

1+00
7.91
90.36
C-7.55

0+77 = pier
3.47
90.20
C 3.27

0+63 = pier
2.59
90.10
C 2.49

0+35
94.09
89.91
C 4.18

0+05 ^{0.7%}
97.80
89.70
C-8.10

0+00
89.66

M.H.# 55
Mildred St.

COLUSA North of Mildred
& ALLEY BIK 12.

End of line

4+20 plug

31:

3+90

T.P. 126.97

3+50

19%

T.P. 117.67

P.O.T.

3+10 = M.H.# 58

T.P. 108.90

2+60

2+20

1+80

6.5%

1+40

131.11
122.88
C-8.23

28.93
117.18
C 11.75

120.19
109.58
C-10.61

113.45
101.98
C 11.47

106.68
98.73
C-7.95

102.23
96.13
C 6.10

100.68
93.53
C 7.15

101.48
90.93
C 10.55

JOSEPHINE ST

21

INDEXED

9711L
9720L

2+50

2+25

2+00

1+75

1+50

1+00

0+50

0+05

0+00 = MH#50

Mildred St.

106.87
97.53
C-9.34

102.40
94.78
C 7.62

101.28
92.03
C 9.25

101.90
89.28
C 12.62

97.84
86.53
C 11.31

90.66
81.03
C 9.63

85.64
75.53
C 10.11

82.00
70.58
C 11.42

70.03

JOSEPHINE

5+49.49

9+08.71 M.H.#54
End of line

7.45
140.47
C 6.98

B.M. 22

Mon

10 feet

El: 147.92

9+00

7.52
140.21
C 7.31

5+00 $\frac{10}{11}$

37.96
125.03
C 12.93

132.63 T.P.

8+50

46.91
138.71
C 8.20

4+50

130.87
119.53
C - 11.34

124.02 T.P.

8+00

45.93
137.21
C 8.72

4+18.71

$\Delta 67^{\circ} 58'$ RA
4+13.71 M.H.#52

115.54

23.55
116.09
C 7.46

115.81 - T.P.

7+50

43.76
135.71
C 8.05

4+08.71

23.05
115.00
C 8.05

7+00

42.70
134.21
C 8.49

3+80

19.85
111.84
C 8.01

6+50 $\frac{10}{3}$

42.14
132.71
C 9.43

3+40 $\frac{11}{11}$

14.25
107.44
C 6.81

6+00

141.80
131.21
C 10.59

2+99.64

8.66
103.00
C 5.66

5+50

140.96
129.71
C 11.25

$\Delta 22^{\circ} 28' - 30''$ RA

2+94⁶⁴ M.H.# 51 102.44

P.O.T.

5+39.71 M.H.# 53

140.62
129.40
C 11.22

2+89⁶⁴

7.57
101.89
C 5.68

BIK 387- J P JONES SUB.

* P.L. 1101

9702-L

9703-L

9713-L

INDEXED

1111 95.00%
2+50 0.15%
0.

5.75
0.48
C 5.27

7+00

9.82
1.15
C 8.67

6+50

9.16
1.08
C 8.08

6+00

8.85
1.00
C 7.85

5+50

8.26
0.93
C 7.33

5+00

7.95
0.85
C 7.10

4+50

7.40
0.78
C 6.62

4+00

6.73
0.70
C 6.03

3+50

6.06
0.63
C 5.43

3+00

6.31
0.55
C 5.76

= 2+15.06 - Prelim $\frac{2160}{49}$

2+13.56 = M.H# A

4.89
0.43
C 4.46

Existing C.I.
Δ 492-06' Ltr

under Dyke
Existing C.I.

1+04.9

8.94
0.23
C 8.71

0+55

9.22
0.14
C 9.08

0+10

8.70
0.06
C 8.64

= 0+00 M.H#3

0.04

± Gaines

5+93 01 ← From P-11-Left.

PL. 1101

24

10+50

11.55
1.68
C-9.87

10+00

11.10
1.60
C-9.50

9+50

10.51
1.53
C 8.98

9+00

10.83
1.45
C 9.38

8+50

10.39
1.38
C 9.01

8+00

10.16
1.30
C 8.86

7+50

9.94
1.23
C 8.71

P.O.T.

7+05126=M.H.#5

9.86
1.17
C 8.69

11+96.96 M.H.#6

1.90

11+87

10.45
1.89
C 8.56

11+50

10.46
1.83
C 8.63

11+00

11.43
1.75
C 9.68

0.15%

0.15%

BENICIA

* RILEY - East from Benecia

9704-L

Nail Pole 550R = 11.84

25

9705-L

9715-L

5+50

34.32

18.50

C 15.82 31.1679

5+00

28.39

15.20

C 13.19 22.3079

A+50

20.85

11.90

C 8.95

A+

A+00

12.94

8.60

C 4.34

3+

3+50

8.52

5.30

C 3.22

3+35.93

7.24

4.38

C 2.86

YUMA ST.

3+25.93 - M.H. #32

3.72

3+19.93

7.63

3.69

C 3.94

INDEXED

3+00

7.68

3.60

C 4.08

2+50

9.31

3.40

C 5.91

2+00

9.90

3.20

C 6.70

1+50

9.75

3.00

C 6.75

1+00

10.48

2.80

C 7.68

0+50

11.15

2.60

C 8.55

0+10

~~10.72~~ stub 10.97

~~2.44~~

2.44

C 8.28

C 8.53

0+00 = M.H. #6

10.14

2.40

ANDRADE ST.

BENEZIA

544

9715-L

26

811T

9+26.29

3%

42.10
35.03
C 7.07

7+00

20⁸² 25⁸² C4⁹³

Riley St.
Δ 90°-28' RT
9+21.29 = M.H.#38

1.95
34.88 Africa
C 7.07
34.88 42⁰² C-7¹⁴

6+75

20⁷⁹ 25⁸⁹ C5¹⁰

Riley St.
Δ 90°-28' RT

9+16.29 ~~M.H.#38~~

34.51 41⁸⁸ C-7³²

6+50

0.4%

20⁶⁹ 29⁵⁶ C8⁸⁷

9+00

33.33 42⁰¹ C-8 68

6+28.39

20⁶⁰ 33⁵⁴ C12⁹⁴

Gains to East

6+23.39 = M.H.#35

20.58

8+50

29.68 40²⁵ C10 52

6+18.39

0.4%

33.46
20.56
C 12.90

8+00

26.03 35³² C-9 39

5+88.67

34.07
20.44
C 13.63

7+50

22.38 28²⁷ C-5 89

Gains to West

5+78.67 = M.H.#34

20.40

P.O.T.
7+31.29 = M.H.#37

21⁰¹ 26⁸⁷ C-5 86

5+68.67

line to east
33.23 Gains
19.73 Turn east
15.50 Make 15⁵⁶

7+26.29

BM

33²⁰ E Gains RASPK
100 Benezia

INDEXED

7 st
East from Benecia9705-L
9714-LEnd of line
13+01.29 P149
5287
46128
C 6.5912+61129 9/10
3
51169
45108
C 6.60P.O.T.
12+21.29 M.H.#39
50184
43188
C-6.9612+00
10.27
43.24
C 7.0311+50
8.83
41.74
C 7.0911+00
7.28
40.24
C 7.0410+50 3/10
45.52
38.74
C-6.7810+00
14.09
37.25
C 6.849750
42.70
35.74
C 6.96YUMA
Benecia - East9704-L
9715-L

27

End of line
3+22-M.H.#33
11.10
5.01
C 6.093+00
10.55
4.92
C 5.632+50
9.86
4.72
C 5.142+00
9.00
4.52
C 4.481+50 9/10
8.21
4.32
C 3.891+00 0
8.02
4.12
C 3.900+50
8.00
3.92
C 4.080+10
8.01
3.76
C 4.250+00-M.H.#32
Benecia
3.72

INDEXED

III 25 105A

West GAINES
of Benicia9705-L
9712-L

End of line

1+20 Plug 5.04
20.88
C 4.160+80 5.95
20.72
C 5.230+40 0.4%
29.98
20.56
C 9.420+105 35.29
20.44
C 14.850+00 = M.H #34 3
20.40
GainesGaines
East of Benicia

5A 28

End of line

3+25 = M.H #36

34.50 41⁵⁰ C.7⁰⁰

3+00

34.00 41¹⁵ C.7¹²

2+50

33.00 40²⁸ C.7²⁸

2+00

32.00 39⁵¹ C.7⁵¹1+50⁰⁰
R31.00 38⁴⁶ C.7⁴⁶

1+00

30.00 37²¹ C.7²¹

0+50

29.00 36⁵¹ C.7⁵¹

0+05

28¹⁰ 34⁷⁴ C.6⁶⁴

0+00 = M.H #35

28.00

Gaines

INDEXED

ANDRADE ST.

B.M. 86 - 10.65

29

95.00 Bencia - East.

9704-L

9717-L

5+50

11.85

2.72

C 9.13

3+50

11.13
2.42
C 8.71

5+00

0.15%

11.85

2.65

C 9.20

3+00

11.00
2.35
C 8.654+87⁴

11.90

2.63

C 9.27

2+50

10.86
2.27
C 8.59

Δ 89°-58' Lt.

4+77⁴⁰ = M.H.# 8

12.05

2.62

C 9.43

2+00

11.23
1.70
C 9.034+72⁴

1+50

0.15%

10.39
2.12
C 8.274+64⁹

2.60

1+00

10.62
2.05
C 8.57

Δ 89°-58' RX

4+54.90 = M.H.# 7

Causa st

11.05

2.58

C 9.47

0+65

11.23
2.00
C 9.234+44⁹

11.21

2.56

C 8.65

0+10

10.72
1.92
C 8.80

4+00

0.15%

11.67

2.50

C 9.17

0+00

1.90

Bencia

Andrade

8+50

11.84
3.17
C 8.67

11+50

13.62
3.62
C 10.00

8+00

11.91
3.10
C 8.81

11+00

13.00
3.55
C 9.45

7+50

11.82
3.03
C 8.79

10+50

12.54
3.47
C 9.07

7+37.16

11.80
3.01
C 8.79

10+00

12.13
3.40
C 8.73

7+27.16 M.H.# 9 2.99

9+86.8

12.10
3.39
C 8.71

Donatue

Eureka St

7+17.16 - 11111 7

11.77
2.97
C 8.80

9+76.8 M.H.# 10

3.37

7+90

11.78
2.95
C 8.83

9+66.8

12.06
3.35
C 8.71

6+50

11.84
2.87
C 8.97

9+50

11.96
3.32
C 8.64

6+00

11.68
2.80
C 8.88

9+00

11.88
3.25
C 8.63

ANDRADE

INDEXED OLUSA ST. 9706-L
 " North of Andrade 9704-L
 9717-L

31

End of line
 13+31.8 P149

10.74
 3.90
 C 6.84

13+00
 12+96.8

14.10
 3.85
 C 10.25

12+56.8

13.93
 3.79
 C 10.14

12+21.8

13.43
 3.74
 C 9.69

Fresno

12+11.80 - M.H.# 11

3.72

13.35 T.P.

12+01.8

13.29
 3.70
 C 9.59

12+00

3.70

3+00

10.99
 4.28
 C 6.71

2+50

9.02
 4.08
 C 4.94

2+00

8.58
 3.88
 C 4.70

1+50

9.58
 3.68
 C 5.90

1+00

10.78
 3.48
 C 7.30

1+00 ± P.O.T.
 EL. = 10.79

0+50

10.70
 3.28
 C 7.48

0+10

11.13
 3.12
 C 8.01

0+00 = M.H.#7

3.08

0-22⁵ See page 29

Colusa st.

~~6+18⁴²~~

6+00

42.55
34.01
C 8.54

5+50

40.40
28.76
C 11.70

5+00

36.00
22.31
C 13.69

4+50

11.79%

28.44
16.46
C 11.98

4+00

21.68
10.61
C 11.07

3+50

~~4.76~~

Yuma St. west.

3+47⁵ = M.H. # 29
P.O.T.

14.60
4.47
C 10.13

~~3+42⁵~~

Colusa St

32

End of line

8+06⁴² plug

50.25
44.99
C 5.26

8+00

50.15
44.70
C 5.45

7+50

7.80
42.25
C 5.55

7+00

4.50%

5.52
40.20
C 5.32

6+50

43.52
37.95
C 5.57

~~6+28⁴²~~

Gainor St west

6+23⁴² = M.H. # 30
P.O.T.

43.15
36.75
C 6.40

INDEXED

North
III 25 1954

EUREKA ST
From Andrade

9704-L
9706-L
9716-L

6+50

6+00

5+50

5+00

M.H.# 17
4+90^E P.O.T.

4+50

4+00

3+50

3+00

2+58^E

Eureka

North of Andrade

47.78
36.26
C 11.52 ✓

43.92
34.61
C 9.31 ✓

43.13
32.96
C 10.17 ✓

41.91
31.31
C 10.50 ✓

41.52
31.00
C 10.52 ✓

39.18
26.62
C 12.56 ✓

31.35
21.22
C 10.13 ✓

22.47
15.82
C 6.65 ✓

16.34
10.42
C 5.92 ✓

12.58
5.94
C 6.64 ✓

33

Yuma St.

2+485 = M.H.# 16

4.86

2+38.5

11.91
4.82
C 7.09 ✓

2+00

10.03
4.67
C 5.36 ✓

1+50

10.19
4.47
C 5.72 ✓

1+00

11.13
4.27
C 6.86 ✓

0+50

11.70
4.07
C 7.63 ✓

0+10

12.07
3.91
C 8.16 ✓

0+00 = M.H.# 10

11.01
3.87
C 7.14 ✓

Andrade St.

3.3%

33287.18

24415.18

T.P. 14.88

Eureka
North of Andrade

YUMA
West of Eureka

34

970A-L
9716-L

INDEXED

JUL 25 1954

end of line

8+78 ⁵⁰ MM
1019
70.64
61.90
C 8.74

8+50
66.65
58.54
C 8.11

64.52 TIR

8+00
59.51
52.54
C 6.97

12 0/16
55.87 TR
7+50
33.81
46.54
C 7.27

7+00
51.21
40.54
C 10.67

M.H. # 18
6+70 = P.O.T.
49.43
36.94
C 12.49

0+85 plug

10.91
5.20
C 5.71

0+50

13.31
5.06
C 8.25

0+10

12.80
4.90
C 7.90

0+00 = M.H. # 16
Eureka St.

4.86

INDEXED

Fresno

9704-L
9706 L
9716-L

17.85 T.P.

1+85.61

14.10
5.71

C-8.39

Δ 4^o 45' 30" H.

1+80^o M.H.# 12

~~4.96~~

1+75.61

13.23
4.94
C8.29

1+50

10.74
4.84
C5.90

1+00

0.4%

13.29 T.P.

13.43
4.64
C8.79

0+50

13.51
4.44
C9.07

0+05

13.48
4.26
C-9.22

0+00 = M.H.# 11

4.24

Andrade st.

FRESNO

St.

35

6+00 58.90 T.P.

53.10
43.48
C9.62

P.O.T.

5+94^o M.H.# 14

53.06
42.64
C10.42

5+50

54.11
40.43
C13.68

5+00

51.16
37.93
C13.23

4+50

5%

48.24
35.43
C12.81

4+00

46.27
32.93
C13.34

P.O.T.

3+50^o M.H.# 13

43.87
30.46
C13.41

3+00

35.39 - T.P.
22.87
C12.52

2+50

15%

27.50
15.37
C12.13

T.P. 27.00

2+00

23.33
7.87
C15.46

Fresno

DONAHUE St.

36

+Easement lots 14+15 Blk 2. 9704-L
9706-L
9714-L

2+70

10.52
5.25
C5.27

end of line

8+79 1/2 plug

T.R. 74.99

98.33
85.39
C12.94

P.O.T.

2+48.5 M.H.# 20
Yuma St.

9.95
4.48
C5.47

8+50

17 1/2

85.75-T.R.

93.44
80.44
C13.00

2+00

9.12
4.29
C4.83

8+00

P.O.T.

7+8A 1/2 M.H.# 15

85.04
71.94
C13.10

1+50

9.86
4.09
C5.77

7+50

77.09 T.R.

82.39
69.24
C13.15

0+50

10.98
3.89
C7.09

7+00

14 1/2

67.96
57.48
C10.48

0+10

11.12
3.69
C7.43

6+50

60.72
50.48
C10.26

0+00 = M.H.# 9

Andrade St.

11.59
3.53
C8.06

3.49

INDEXED

JUL 25 1959

Donations

10' Lt. of \$

6+05

33.62
17.45
C 16.17

5+80

3.7%

33.22
16.82
C-16.40

5+65

24.31
15.90
C 8.415+36² prot.

M.H.# 21

22.00
14.85
C 7.21

5+00

20.17
13.53
C 6.64

4+50

17.35
11.73
C 5.62

4+00

3.6%

15.81
9.93
C 5.88

3+50

15.03
8.13
C 6.90

3+00

11.97
6.33
C 5.64

Donations

37

10' Lt. of \$

8+50

9.2%

33.75
27.77
C 5.98

8+36

32.82
26.48
C 6.348+25⁹⁹ M.H.# 22

25.56

8+16

31.98
24.22
C 7.76

8+00

31.07
24.63
C 6.44

7+50

3.7%

28.77
22.80
C 5.97

7+00

6.75
20.95
C 5.80

6+50

25.56
19.10
C 6.46

6+20

25.79
18.00
C 7.79

Easement
Lots 15 & 14 BIK 2

9714-L

RILEY ST
West of Donahue

38

9706-L
9714-L

Alley BIK #2

10+81⁰⁴ M.H.#24

44.85

10+71⁰⁴

51.56⁷⁸

52.01
44.22
C 8.37
6'2"

10+50 $\frac{0}{10}$

9.95
42.95
C 7.00
7'2"

End of line

10+00 $\frac{1}{9}$

47.25
39.90
C 7.35

1+60 Plug.

61.06
51.03
C 10.03

9+56²⁸

42.81
37.24
C 5.57

1+20

59.12
47.43
C 11.69

$\Delta 12^\circ - 12'$

9+46²⁸ M.H.#23

36.63

0+80 $\frac{9}{10}$

52.02
43.83
C 8.19

0+40

4.77
40.23
C 4.54

9+30²⁸

41.48
35.70
C 5.78

0+05

2.88
37.08
C 5.80

9+00 $\frac{9}{210}$

7.88
32.37
C 5.51

0+00 = M.H.#23

36.63

RILEY SPINEVERD

East of Donahue

9706-L

971A-L

3+00

82.47
71.98
C 10.49

2+50

14.7%

77.50
64.63
C 12.87

2+00

71.54
57.28
C 14.26

P.O.T.

1+75 = M.H.# 75

67.67
53.61
C 14.06

1+50

64.18
51.18
C 13.00

1+00

58.17
46.33
C 11.84

0+50

9.9%

9.80
41.48
C 8.32

0+05

42.83
37.11
C 5.72

M.H.# 23-

36.63

Donahue St.

Riley

East of Donahue

B.M. = 0+00 "L" line 39
2.49 = 1/2 Ctr. M.H.# 23
CC
EL. = 42.57

end of line

6+61 plug

103.73
98.20
C 5.53

6+50

104.13
98.09
C 6.04

6+00

106.32
97.59
C 8.73

5+50

1%

107.80
97.09
C 10.71

5+20

108.20
96.79

5+00

107.54
96.59
C 10.95

4+65 = M.H.# 76

P.O.T.

104.00
96.24
C 7.76

4+50

102.00
94.03
C 7.97

4+00

14.7%

94.99
86.68
C 8.31

3+50

88.50
79.33
C 9.17

Alley BIK 2

West of M.H.# 2A

Nail & Colusa Elev

9706-L

9718-L

62.99

Alley BIK 2

" " 3

" BIK 4

East of M.H.# 2A

40

70.55 T.P.

2+00

7.59
80.34
C 7.25

1+50

12%

82.83
74.34
C 8.49

1+00

75.37
68.34
C 7.03

End of line

1+60 plug

67.43
59.64
C 7.79

9' RT

RO.T.

0+95^{1/2} = M.H.# 70

74.34
67.74
C 6.60

1+20

69.09
59.48
C 9.61

0+55

44.0%

50.10

0+80

71.10
59.32
C 11.78

T.P.

0+50⁰² M.H.# 25

47.90

0+40

0.4%

72.82
59.16
C 13.66

7' RT

0+40⁰²

61.0%

54.29
47.29
C 7.00

10' Lt.

0+

65.17 T.P.

0+05

15.15

0+00

58.30
59.00
F 0.70

10' RT

0+00 = M.H.# 2A

58.23
44.85
C 13.38

10' Lt.

M.H.# 2A

2475.08

Alley BIK 2-3+4

Alley BIKs 2-3+4

41

6+00

13.07
110.36
C 12.71

P.O.T.
9+85¹¹ M.H.# 73

21.07
111.90
C 9.17

5+50

0.47

22.10
110.16
C 11.94

9+50

17.14
111.76
C 5.38

5+00

19.35
109.96
C 7.39

9+00

16.76
111.56
C 5.20

4+50

14.72
109.76
C 4.96

8+50

17.99
111.36
C 6.63

P.O.T.
4+45¹¹ M.H.# 71

14.11
109.74
C 4.37

8+00

21.69
111.16
C 10.53

4+00

10.04
104.34
C 5.70

7+50

20.32
110.96
C 9.36

3+50

12.20

104.00
98.34
C 5.66

P.O.T. Goshen St
7+25¹¹ M.H.# 72

17.21
110.86
C 8.35

3+00

97.51
92.34
C 5.17

7+00

20.59
110.76
C 7.83

2+50

92.30
86.34
C 5.96

6+50

22.53
110.56
C 11.97

Alley BIKs. 2-3+4

End of line

Huonette St.

12+2A.92 = M.H. #77 155.99

12+20

65.62
155.66
C 9.96

12+00

17%

64.56
154.10
C 10.46

11+50

939
150.22
C 9.17

M.H. # 74

11+25.11 P.O.T.

55.91
148.30
C 7.61

11+00

51.18
141.77
C 9.41

10+50

26%

39.34
128.77
C 10.57

10+00

24.94
115.77
C 9.17

Huonette St. 9710-L 42
9718-L

South of alley

1+10 = plug

63.43
156.43
C 7.00

0+75

65.80
156.28
C 9.52

0+40

0.4%

66.11
156.14
C 9.97

0+05

65.62
156.01
C 9.61

Alley BIK A

0+00 = M.H. #77

155.99

North of Alley

1+20 plug

77.85
167.99
C 9.86

1+00

74.55
165.99
C 8.56

0+50

1.0%

68.80
160.99
C 7.81

0+05

66.29
156.49
C 9.80

0+00 = M.H. # 77

155.99

Alley BIK. A

Easement BIKs 2-8+13

2+00	72.08 61.47 C 10.61	8' Lt.	4+60	93.13 82.88 C 10.25	7' Lt.
1+50	65.97 57.37 C 8.60	8' Lt.	$\Delta 11^\circ-37'-30''$ Lt. 4+52.84 M.H.# 28	82.20	
1+42.76	65.02 56.78 C 8.24	8' Lt.	4+45.12	72.25 81.55 C 10.70	8' Lt. 91.54 T.P.
$\Delta 36^\circ-47'-30''$ Rt. 1+34.76 = M.H.# 26	56.12		4+00	87.43 77.86 C-9.57	8' Lt.
1+24.76	61.39 55.51 C 5.88	10' Lt.	3+50	83.94 73.76 C 10.18	8' Lt. 82.77 T.P.
1+00	60.28 54.00 C 6.28	10' Lt.	3+10.32	80.60 70.52 C 10.08	8' Lt.
0+50	7.05 50.95 C 6.10	10' Lt.	$\Delta 10^\circ-05'-30''$ Lt. 3+02.32 = M.H.# 27	69.86	
0+10	54.29 48.51 C 5.78	10' Lt.	2+94.32	79.65 69.20 C 10.45	8' Lt.
0+00 = M.H.# 25 Alley BIK 2.	47.90		2+50	75.95 65.57 C 10.37	8' Lt.

Easements
Blks. #2-#8 + #13

LAURETTA 9709-L 44
East of Brunner 9710-L
9713-L

			1750	T.P. 9952	5.69 90.05 C 5.64
			1700	13%	89.40 83.55 C 5.85
			0+65		85.58 79.90 C 6.58
			0+55		85.06 77.60 C 7.46
6+60.8A p/49	111.38 101.96 C 9.42	7' L.	0+45		84.40 75.40 C 9.00
				T.P. 825A	
6+50	110.22 100.93 C 9.29	7' L.	0+35		80.45 72.30 C 8.15
		108.64 T.P.			
6+00	106.23 96.18 C 10.05	7' L.	0+25		75.57 68.20 C 7.37
5+50	101.00 91.43 C 10.23	7' L.	0+15.7		57.70
		100.64 - T.P.			
5+00	96.50 86.68 C 9.82	7' L.			
			0+00 = M.H.# 26		56.12
			South of Brunner		

INDEXED

Lauretta - East of Brunner

A+53.5 1954

30.85
125.39
C-5.46

P.O.T.

A+40.98 MH#60

30.28
125.01
C 5.27

4+00

27.61
120.22
C 7.39

T.P. 126.54

3+50

22.37
114.37
C 8.00

T.P. 117.25

3+00

15.82
108.52
C-7.30

11.7%

2+50

9.04
102.67
C 6.37

~~225.56~~

Eureka P.O.T.

220.56 M.H.#59

105.29
99.22
C 6.07

108.69
Nail in pole
#1099
S.E. Eureka
to Lauretta

~~215.56~~

T.P. 108.31

2+00

10.275
96.55
C 6.20

13%

Lauretta

East of Brunner

T.P. 146.25

8+50

44.51
139.69
C 4.82

8+00

41.71
136.94
C 4.77

P.O.T.

7+80.98 M.H.#61

41.20
135.89 ✓
C 5.31

7+50

41.80
134.89
C 6.91

7+00

40.62
133.29
C 7.33

B.H. - P.K.M.I.
Pole
#8.1978
E. 139.42

6+50

40.27
131.69
C 8.58

6+00

39.37
130.09
C 9.28

5+50

37.61
128.49
C 9.12

T.P. 135.52

5+00

34.60
126.89
C 7.71

5.5%

3.2%

Lauretta
East of Brunner

INDEXED Eureka

46

North of Lauretta 9709-L
Also Alley BIK 1A

2+50
7.54
120.90
C 6.64

2+00
23.90
117.40
C 6.56
122.40

1+50
20.61
113.90
C 6.71

172.55 T.P.
11+10.98 = p/29.
71.53
164.49
C 7.04

1+44.39
20.27
113.51
C 6.76

11+0.0
9.54
162.84
C 6.80

Alley BIK. 7 $\angle 75^{\circ} 13'$
1+39.39 - M.H.# 63
113.16

10+50
163.69 T.P.
60.98
155.34
C 5.64

1+34.39
9.46
112.66
C 6.80

P.O.T.
10+00 - M.H.# 62
154.81 T.P.
147.99
C 6.82

1+00
15.74
109.22
C 6.52
113.81

9+50
51.29
145.19
C 6.10

0+50
10.85
104.22
C 6.63

9+00
7.65
142.44
C 5.21

0+05
156.88
99.72
C 7.16

Lauretta St. ←
0+00 = M.H.# 59
99.22

Eureka
Alley BIK. 1A

Alley BIK. 1A

47

5+00
149.16^{TR}
52.45
142.48
C 7.97

4+50
12⁹⁰
44.93
136.48
C-8.45

4+23.49
139.77
133.30
C-6.47

Δ 750 13L 30" RT
4+18.49 = M.H. #68 132.70

4+13.49
9.19
132.34
C-6.84

4+00
8.03
131.40
C 6.63

3+50
11¹⁰
34.47
127.90
C 6.57

3+00
30.75
124.40
6.35

End of line.

6+98.49 plug

6+48.49

PRO.T.

5+98.49 M.H. #69

5+50

176.37
164.30
C 12.07

68.78
159.30
C 9.48

62.75
154.30
C-8.45

157.91^{TIP}
148.48
C 9.43

Alley Biks #647

9709-L
9710-L
9720-L

3+00 $\frac{5}{10}$

50.21
142.16
C 8.05

2+50

46.90
139.66
C 7.24

P.O.T.
2+00 = M.H.# 64

43.99
137.16
C 6.83

1+50

9.69
131.16
C 8.53

1+00

32.69
125.16
C 9.53

0+50 $\frac{12}{10}$

128.8472

27.43
119.16
C 8.27

0+05

119.90
113.76
C 6.14

0+00 = M.H.# 63

113.16

Eureka St.

Alley Biks #647

48

P.O.T.
6+32,71 = M.H.# 66

170.73
163.00
C-7.73

6+00

C.30
160.71
C 5.59

5+50

63.90
157.21
C 6.69

5+00 $\frac{7}{10}$

C 0.19
153.71
C-6.46

4+50

8.09
150.21
C-7.88

A+22.71

156.00
148.39
C 7.61

Gastien St.
A+22.71 = M.H.# 65

148.04

A+17.71

A+12 $\frac{7}{10}$

55.54
147.80
C 7.74

4+00

55.22
147.16
C-8.06

3+50 $\frac{5}{10}$

52.50
144.66
C-7.84

Alley BIK 6+7

INDEXED OSHEEN.

49

North of alley BIK 6
JUN 25 1954

End of line

Stub

8+57.71 = M.H.# 67

194.16
187.75
C-6A1

8+50

93.72
186.90
C 6.82

8+00

7.71
181.40
C 6.31

7+50 ^{do}
|||

83.27
175.90
C-7.37

7+00

8.44
170.40
C 8.04

6+50

71.96
164.90
C 7.06

end of line

0+70 stub

64.42
155.30
C 9.12

0+35 ^{do} stub

60.78
151.80
C-8.98

0+05 ^{do}

57.22
148.80
C 8.42

0+00 = M.H.#

1148.30

Alley BIK 6

Goshen St + Alley BIK 14
Silver terrace.

50

C.H.S.
Boyer
Oltman
Schelin

9-1-53
W.O.# 62342
Sheet #5044 B.

stakes 5' North of \pm

0+90-Plug

87.95
173.30
C 14.65

\pm Goshen

0+65 M.H.#1 P.O.T.

82.87
170.80
C 12.07

0+32 $\frac{E}{E}$

81.80
167.55
C 14.25

0+00 = Existing stub

Alley BIK 14

78.23
164.30
C 13.93

Alley BIK 15 + BIK 42 O.B.
Sewer Lats Alley BIK. 42.

Paving Grades
Alley BIK 15 - O.B.
Froude to Ebers - between {Bermuda
Pt Loma Ave

19.5' wide Pavement
outs to stakes are from edge of pave.

No Laterals in alley #15

B.M. = S.E.B.P. Ebers + Pt. Loma Ave. EL = 35.66

INDEXED
APR 29 1954

34.47 TIP
26.40 TP

1+80 X-0.65 2.74 3.90
62.06 62.36 X-0.55
C0.68 C1.54

1+40 0-2' 4.88 6.28 = edge Pava
64.86 65.16 N-line
C0.02 C1.12

1+00 0-V 7.70 9.55
67.65 67.95 N-0.06
C0.05 C1.60

A+45 Lt. = #1

21.14
16.47
C4.67

0+60 0-V 9.20 1.82
70.44 70.74 0-1'
C0.24 C1.08

1+99 Rt. = #3

30.80
25.35
C5.45

0+40 0-2' 1.80 4.70
71.71 72.01 X-0.80
C0.09 C2.69

1+96 Lt. = #2

30.32
25.19
C5.13

0+20 0-4 2.63 4.75
72.40 72.70 X0.80
C0.23 C2.05

0+00 72.53 73.17

38.75

0+00 = wly line Ebers

0+00 = wly line Froude

Blk. 15-O.B.

Alloy

Blk. 15-O.B.

52

4+80	D-2'	9.43 49.48 F0.05	50.1A 49.78 C0.36	D-2'
4+60	X-2'	0.38 50.47 F0.09	1.29 50.77 C0.52	X-2'
4+20	D-2'	2.14 52.01 C0.13	3.58 52.31 C1.27	D-2'
3+80	D-2'	3.39 53.55 F0.16	4.62 53.85 C0.77	D-2'
3+40	D-2'	4.85 55.09 F0.24	6.02 55.39 C0.63	D-2'
3+00	D-2'	6.58 56.63 F0.05	6.98 56.93 C0.05	D-2'
2+60	D-2'	8.54 58.18 C0.36	9.28 58.48 C0.80	D-2'
2+20	X-2'	0.70 59.73 C0.77	0.68 60.03 C0.65	D-2'
2+00	X-2'	1.10 60.70 C0.40	1.89 61.00 C0.89	D-2'

Ely Ebers

6+00		39.75	40.35
5+80	D-2'	2.56 41.40 C1.16	2.57 41.70 C0.87
5+40	D-2'	6.40 44.72 C1.68	6.71 45.02 C1.69
5+00	D-2'	8.59 48.04 C0.55	9.08 48.34 C0.74

48.33 TP.
56.99
62.12
69.55

Pave. Alley BIK. 42 - Ocean Beach.

Pave - 19.5' wide

outs to stakes are from edge of Pave.									
					4+40	D-2'	1.00 21.31 F0.31	1.50 21.61 F0.11	D-2'
2+60	N-0.35	8.06 27.20 C0.86	7.74 27.50 C0.24	D-2'	4+20	D-2'	1.21 21.65 F0.44	3.12 21.95 C1.17	X-2'
2+20	N-0.25	9.95 29.07 C0.88	9.41 29.37 C0.04	D-2'	4+00	D-2'	1.70 22.08 F0.38	3.15 22.38 C0.77	X-2'
1+80	D-2'	1.43 30.94 C0.49	1.50 31.24 C0.32	D-2'	3+80	D-0.40	2.44 22.58 F0.14	2.93 22.88 C0.05	D-2'
1+40	D-2'	3.12 32.81 C0.31	3.23 33.11 C0.12	D-2'	3+60	X-0.65	4.12 23.16 C0.96	3.42 23.46 F0.04	D-2'
1+00	D-2'	4.78 34.68 C0.10	4.96 34.98 F0.02	D-2'	3+40	X-2'	4.54 23.82 C0.72	4.12 24.12 X	D-2'
0+60	D-2'	6.18 36.55 F0.37	7.11 36.85 C0.26	N-1.25	3+20	X-2'	5.15 24.56 C0.59	5.92 24.86 C1.06	N-0.58
0+20	D-2'	8.24 38.40 F0.16	9.51 38.70 C0.81	N-0.55	3+00	X-2'	5.34 25.38 F0.04	5.79 25.68 C0.11	N-0.45
0+10	D-2'	8.60 38.72 F0.12	9.80 39.08 C0.72	N-0.50	P.O.C. 2+80	X-2'	6.07 26.27 F0.20	7.25 26.57 C0.68	N-0.35
wly. line Ebers 0+00		7.75 38.73	7.27 39.25						

Alloy BIK. 42-O.B.

54

Elg. Sunset Cliff Blvd 6+00	N-V	19.40	19.63	0.2
5+90	N-V'	20.10 19.88 0.22	0.50 20.17 0.33	0.2'
5+80	N-V'	0.80 20.10 x	0.49 20.40 0.09	0.2'
5+30	D-V'	0.78 20.47 0.31	0.46 20.77 0.31	0.2'
E.V.C. A+80	D-V'	1.19 20.85 0.34	0.73 21.15 0.42	0.2'
A+60	D-V'	1.31 21.04 0.27	0.87 21.34 0.47	0.2'

Napa St. Sewer
Linda Vista Rd. wly.

Sheet 4979-B
w.o. 62337

3+17 Plug 13.87
6.60
C-7.27

2+67 13.62
6.40
C 7.22

Δ 4°-09' 13.49
2+17 = M.H. 6.20
C 7.29

1+80 13.41
6.12
C 7.29

1+40 13.28
5.96
C 7.32

1+00 13.21
5.80
C 7.41

0+70 13.40
5.67
C 7.73

0+35 13.80
5.53
C. 8.27

0+07 13.34
5.41
C 7.93

El. 5.58
0+00 = Exist M.H. #84 Sheet 9709-L
 Δ 9°-18' Lt. Revised

INDEXED
MER
APR 29 1954

INDEXED

Rough Grade

Pave. Beaumont Ave
 10-15-53 Sheet # 106699
 W.O. 32036 F.B. 2127-P60

T.P. 94.38
 " 94.20
 T.P. 93.18

APR 29 1954

0+00 = Nly. line Colima
 5+90.3 = Sly line Midway

	Rough	Curb	curb	Rough		Rough	cb.	cb.	Rough		
					4+37 ^E	—	4.79 94.95	5.50 95.45	—		
							F 0.16	C 0.05			
					P.O.C. 4+17 ^E		3.97 94.76	4.83 94.76	5.41 95.26	95.26	
							F 0.79	C 0.07	C 0.15		
0+97 ^E N. 0.2 in	2.88 92.63 C 0.25	2.78 92.63 C 0.15	3.74 93.13 C 0.61	4.76 93.13 C 1.63	3+77 ^E		2.93 94.50 F 1.57	4.18 94.50 F 0.32	4.68 95.00 F 0.32	7.45 95.00 C 2.45	N. line
0+57 ^E Bk line	2.30 92.86 F 0.06	2.37 92.36 C 0.01	3.76 92.86 C 0.90	4.71 92.86 C 1.85	3+37 ^E		2.90 ^{T/B} 94.23 F 1.33	4.26 94.23 C 0.03	4.27 94.73 F 0.46	100.00 94.73 C 5.21	N 0.1 in
0+37 ^E N. -0.24	3.03 92.03 X	2.22 92.03 C 0.19	3.62 92.53 C 1.09	4.60 92.53 C 2.07	2+97 ^E		2.73 93.96 F 1.23	3.96 93.96 X	4.80 94.46 C 0.34	5.97 94.46 C 1.51	X line
U.E.C. on Lt. 0+17 ^E	1.70 91.70 X	1.70 91.70 X	64 92.20 C 0.44	92.20	2+57 ^E		2.60 93.70 F 1.10	3.20 93.70 F 0.50	4.34 94.20 C 0.14	8.15 94.20 C 3.95	X -0.09
0+00.	—				2+17 ^E		2.09 93.43 F 1.34	3.25 93.43 F 0.18	4.02 93.93 C 0.09	7.76 93.93 C 3.83	X -0.70
Exist cb. on Rt. 0-08.9	—			92.58	1+77 ^E		1.98 93.16 F 1.18	2.91 93.16 F 0.25	3.32 93.66 F 0.34	7.79 93.66 C 4.13	N 0.12
= Exist cb. on Rt. 0-17.7	—				N. 12 1+37 ^E in		2.44 92.90 F 0.46	2.82 92.90 F 0.08	3.29 93.40 F 0.11	7.13 93.40 C 3.73	N Line

Beaumont

B.M. = N.W. 5' x 7' Beaumont + Colima = EL = 9138

Rough ch. Rough Rough

EXIST ch. on Lt.

6+08' 98.105 ✓
98.00

5+90.3

ch. B.C. on Rt.

5+72' 9' 5' 6.01 8.02 8.71
98.10 98.10 98.60 98.60
F2.09 F0.08 C0.11

5+35.25

4.69 6.98 7.54 9.14
97.10 97.10 97.60 97.60
F2.41 F0.12 F0.06 C1.54

E.O.C.
A+97.5

4.40 5.50 6.19
96.10 96.10 96.60 96.60
F1.70 F0.60 F0.41

A+77.5

5.57 5.81
95.62 96.12
F0.05 F0.31

A+57.6

4.00 5.35 5.64 6.91
95.23 95.23 95.73 95.73
F1.23 C0.12 F0.09 C1.18

Also see
page 59

Beaumont

91.70
91.70

X

- Exist ch.

Wly. Ret.

91.56

Colima

Midway

Ely. Ret.

99.4
98.95

B.C.

8.71
98.60
20.91

Beaumont

Pave.
 Monte Vista INDEXED
 Westbourne to Belvedere.
 10/15/53 sheet 10318-L
 C.H.S. F.B. 2188-19
 W.O. 31029

2+10 sly line Belvedere

1+95

1+85

1+65

1+45

1+25

Raked.
5 Sta.

0+00 = Nly. line Westbourne

58

Plan cb.	Exist. cb. as built	G.	G.	Exist cb. as built	Plan cb.
-------------	---------------------------	----	----	-----------------------------	-------------

		pave Exist	pave. Exist.		
59.60	59.5A	59.04	59.25	59.98	59.96
60.23	60.10	59.60	60.11	60.60	60.62
61.01	60.86	60.36	60.88	61.38	61.44
61.64	61.75	61.15	61.62	62.16 62.12	62.12 62.17
62.18	62.18	61.68	62.15	62.64	62.65
62.59	62.50	62.00	62.50	63.00	63.07
64.73	64.70	64.23 Exist pave			

1854
Stakes set 2' Back of
limit of grading - Beaumont St.
See page 56 for Reg. cut +
Fill stakes

59

3+50

5.81
94.80
C 1.01

3 ~

4.82
94.50
C 0.32

2+50

5.20 T.R.
94.15
C 1.05

2 ~

4.06
93.81
C 0.25

5+73

98.60

1+50

3.75
93.55
C 0.20

5+40

8.22
97.75
C 0.47

1 ~

3.75
93.15
C 0.60

5 ~

7.34
96.68
C 0.66

0+50

3.36
92.70
C 0.76

4+50

5.38
95.55
F 0.17

0+00

4 ~

5.79
95.10
C 0.69

0-08

Beaumont + INDEXED
 Colima to Midway ^{July 25 1954}
 & Grades - Sub grade

4+17[±]94.49[✓]

4+07

3+57

3+07

2+57

2+07

1+57

1+07[±]0+57[±]92.09[✓]0+37[±]91.86[✓]0+17[±]91.43[✓]

Col. Nly. Colima
 0+00

91.74[✓] Exist PaveExist Pave
5+90[±]98.10[✓]Ab. B.C. on Rt.
5+72[±]97.83[✓]

5+

Rake.

x

4+97[±]95.83[✓]4+77[±]95.35[✓]4+57[±]44.96[✓]4+37[±]94.68[✓]

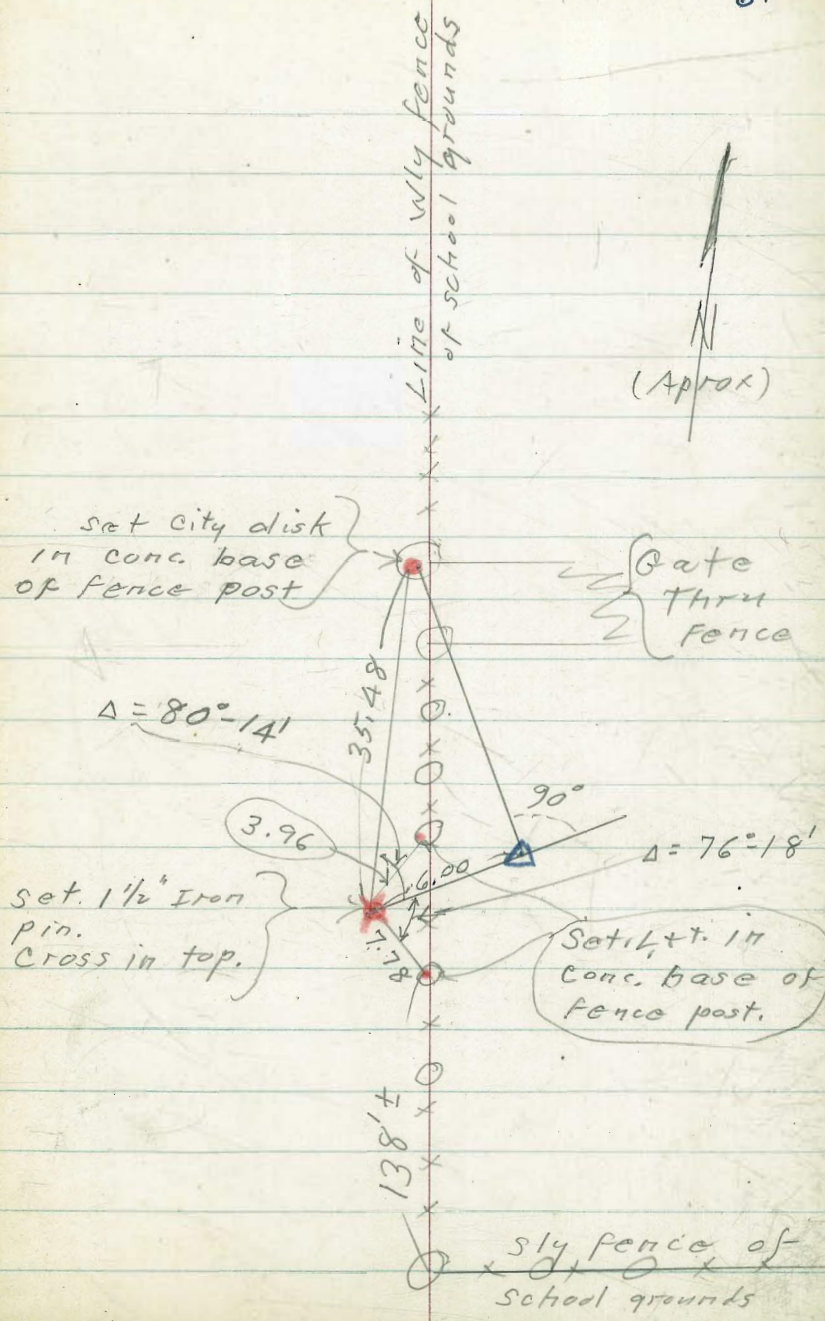
Ref. for Δ in
Darnall School Grounds
(Hughes St. in Redwood)

C.H.S.
Begg &
Ottmar
Schelin

11-13-53
N.O. 20006

Δ denotes existing triangulation point
~~o x o x o x o~~ denotes chain link &
pipe post fence set in conc.

INDEXED
JER
APR 29 1954



32' ^{of.} Storm Drain
Sand Rock Grade w.o. 21183

C.H.S.
Begg
Oltman
Schielin

Sheet 10911-L

3+92.92 (Sheet 10911-L) 20+00

B.M. = Nail in pole 35' rt

of 3+60 - EL. = 94.10 (FB 2245-P14)

INDEXED

62

Stakes 12' rt. of ±

I.E.
0+32

97.50
87.40
C 10.10

88.2
wash

I.E.
0+00

93.70
84.42
C 9.28

wash
85.3

spillway
0+00

93.70
82.42
C 11.28

INDEXED

Alley BIK 5 O.B.
Guizot to Frande
Between 1954 Niagara + Newport Street 10510-L

11-20-53

C.H.S.
Bozz
Rorer
Taylor

2+00 0 3'

p.o.c.
1+80 0 1'

Sewer laterals

1+50 0 3'

5+44 RT. = # 6

A+45 Lt. = # 1

3+95 Lt. = # 2

3+45 RT. = # 5

1+95 Lt. = # 3

1+55 RT. # 4

32.30
124.78
C 8.524.23
139.08
C 5.15144.33
144.A.17
148.17
C 6.0071.85
164.43
C 7.422.93
166.40
C 6.43
283
164.40
C 8.43

Alley BIK. 5 O.B.

63

Lt. =
S. wly.Rt. =
N. Ely.2.66
167.10
C 3.563.32
170.41
C 2.914.34
172.36
C -1.98E.V.C.
1+20 N. 1' 5.40
174.31
C 1.091+00 N-110 6.63
175.40
C 1.230+80 0 2' 7.14
176.10
C 1.040+60 0 2' 8.82
176.40
C 2.420+40 0 2' 9.55
176.30
C 3.25p.o.c.
0+00 wly. Guizot 176.189.43 0
168.80 1'
C 0.630.16 0
170.11 2'
C 0.051.75 0
172.06 3'
C 0.314.08 0
174.01 3'
C 0.075.10 0
175.10 3'
X6.28 0
175.80 3'
C 0.486.74 0
176.10 3'
C 0.647.81 0
176.00 3'
C 1.81

175.40

Eliz. Grande
G+00

Alley BIK 5- O.B.

Alley BIK, 24 - O.B. 64

5+80 RR

5+60 D-2'

E.V.C.

5+20 DA

5+00 D-2'

P.O.C.
4+80 X 2'

4+32 D-2'

3+84

3+36 N,
0.40 in

2+88 X-0.50

E.V.C.
2+40 B-2'

2+20 D-2'

121124

30.68

127.95

C 2.73

8.15

134.65

C 3.50

8.05

137.90

C 0.15

1.96

140.40

C 1.56

7.08

145.46

C 1.62

1.42

150.52

C 0.90

6.26

155.58

C 0.68

4.04

160.64

C 3.40

71.04

165.70

C 5.34

71.66

167.60

C 4.06

119.77

8.98

127.06

C 1.82

5.68

134.35

C 1.33

6.75

137.60

F 0.85

0.21

140.10

C 0.11

145.16

150.22

C 0.03

4.28

155.28

F 1.00

1.67

160.34

C 1.33

8.70

165.40

C 3.30

9.25

167.30

C 1.95

-0.72

N-1³⁰

-0.57

D-2'

D-2'

N

0.62

X-2'

X-2'

N

-0.64

N

-0.45

N

0.54

Froude to Ebars

Between Niagara & Newport, Street 10511-L

C.H.S.

Beqq

Roxor

Taylor

P.O.C.

1+40 D-2'

E.V.C.

1+10 D-2'

0+90 D-2'

0+70 D-2'

0+50 D-1'

0+30 X-2'

0+10 N-0.17

0+00

wly. Froude

11-20-53

102.01

99.50

C 2.51

4.43

102.50

C 1.93

5.49

104.72

C 0.77

8.63

107.38

C 1.25

2.86

110.48

C 2.38

3.62

114.02

F 0.40

9.88

117.57

C 2.29

9.45

119.47

100.53

99.20

C 1.33

2.60

102.20

C 0.40

5.19

104.42

C 0.77

6.21

107.08

F 0.87

1.00

110.18

C 0.82

3.94

113.72

C 0.22

7.19

117.29

F 0.10

7.97

117.95

N

-0.62

N-

0.98

N

-0.95

D-2'

D-1'

D-1'

D-1'

Alley BIK 24-O.B.

Alley BIK 24-O.B.

65

1954

3+70	D-2'	1.66 81.24 C0.42	0.42 80.94 F0.52	D .5				
P.O.C. 3+50	D-2'	4.06 82.75 C1.31	2.39 82.45 F0.06	D 2'	Ely. Ebers. 6+00		48.55	48.25
3+17 ^E	D-2'	6.19 85.19 C1.00	3.85 84.89 F1.04	D 2'	5+45 N-0.33	60.26 57.67 C2.59	8.56 57.37 C1.19	N .84
2+85	X-2'	8.76 87.63 C1.13	5.35 87.33 F1.98	D 3'	A+90 D-2'	8.73 66.79 C1.94	7.07 66.49 C0.58	N 0.48
2+52 ^E	X-2'	89.91 90.07 F0.16	6.97 89.77 F2.80	D 4'	A+70 D-0.5	71.40 69.83 C1.57	70.04 69.53 C0.51	N 0.55
E.O.C. 2+20	D-2'	3.76 92.50 C1.26	0.87 92.20 F1.33	D 2'	A+50 P.K.-3'	5.96 72.75 C3.21	3.98 72.45 C1.53	N 1'
2+00	D-2'	5.95 94.06 C1.89	2.64 93.76 F1.12	D-2'	A+30 D-2'	7.32 75.30 C2.02	4.43 75.00 F0.57	D 2'
1+80	D-1'	8.08 95.75 C2.33	6.94 95.45 C1.49	N- 0.56	A+10 X-2'	8.18 77.55 C0.63	7.21 77.25 F0.04	D 2'
1+60	D-2'	100.45 97.56 C2.89	8.87 97.26 C1.61	N- 0.55	3+90 X-2'	8.80 79.50 F0.70	9.13 79.20 F0.07	D- 0.5

Storm Drain - Lot #13

155158 B.M.

Lomas De La Jolla - Unit #1

164.25 T.P.

173.21 T.P.

C.H.S.
Begg
oltman
Schelin

INDVTR
JER
APR 29 1954 sheet

11-30-53

w.o.#21191

51A3-B.

0+00 = N. Fly. line Linda Rosa. Ave.

0+80

71.45
164.54
C 6.91

N. 5.35 W.

0+70

71.28
163.46
C 7.82

N. 6.47 W.

End of pipe
2+00^s

8.60
173.23
C 5.37

0.10'

0+39

12.67

6.85
159.55
C 7.30

0.10'

1+70

7.22
171.07
C 6.15

0.10'

0+08

9.45
155.65
C 3.80

0.10' W.

1+30

74.07
168.25
C 5.82

N. 6.58 W.

0+00

5.58
155.35
C 0.23

on disk 5' W.

0+90

71.90
165.43
C 6.47

N. 5.82 W.

INDEXED

JER

APR 29 1954

Alley Bk. 9. La Jolla Park

North of Pearl

11-30-53

Between Eads + Fay W.O.# 31880

5+00 D.V.

C.28

86.11

C0.17

7.93

86.41

C1.52

N-010

C.H.S.

Begg

oltman

Schelin

Sheet 10573-L

Improvement - 19' wide

A+80 X-1.45

7.25

86.40

C0.85

8.17

86.70

C1.47

N-015

1+80 D-V

8.53

97.24

C1.29

8.28

97.54

C0.74

D.V.

A+60 X-1'

7.28

86.92

C0.36

8.40

87.22

C1.18

Grade only

N.012

1+30 N.1.20

100.60

99.16

C1.44

100.15

99.46

C0.69

X-2'

A+20 D.V.

8.14

88.17

F0.03

9.66

88.47

C1.19

N-037

0+80 D-V

0.74

101.07

F0.33

2.79

101.37

C1.42

X-1.23

A+00 D.V.

9.09

88.83

C0.26

9.52

89.13

C0.39

D-0143

0+60 D.V.

1.62

101.78

F0.16

2.82

102.07

C0.75

X-1.28

3+80 N
1.95

90.09

89.56

C0.53

1.39

89.86

C1.52

N.036

0+40 X-1.60

3.87

102.36

C1.51

5.30

102.64

C2.66

X-1.30

3+30 D.V.

1.81

91.48

C0.33

1.52

91.78

F0.26

D-1

0+20 D-60

3.16

102.83

C0.33

3.82

103.08

C0.74

X-1.29

2+80 X-V

4.62

93.40

C1.22

4.51

93.70

C0.81

D-V

0+00 = Nly.

103.17

103.38

2+30 D.V.

6.33

95.32

C1.01

7.64

95.62

C2.02

D-V

line Pearl.

Alley Blk. 9 La Jolla Park.

68

1+90 Lt. ^{7.54}
92.00
C 5.54

= (5) #1

7+33 N. ^{4.44}
0122 IN 84.26 N 1.182
C 0.18 84.56
C 0.69

7+23 D.V. ^{2.80}
84.13 N. 1.123
F 1.33 F 0.10

7+03 X.V. ^{1.93}
84.19 D. 0.115
F 2.26 F 0.50

6+60 D.V. ^{2.76}
84.60
F 1.84 3.96
84.90
F 0.94

6+20 D.V. ^{4.25}
84.98 D. 0.03
F 0.73 4.48
85.28
F 0.180

5+80 N. 1.14 ^{6.80}
85.36 D. 0.2
C 1.44 5.61
85.66
F 0.05

5+40 D.V. ^{5.84}
85.74 N 0.122
C 0.10 86.04
C 0.82 IN

0138

INTERVEN
 Sewer Services
 APR 29 1954

Sewer Laterals } Fergus st
 Sewer Services } 62nd st.

Fergus + 2 }
 M.H. RIM - & AKINS } EL = 180.24

0+00 is 52.85' North of N14.
 line AKINS. (& stationing) ^{see} below.

(Kenny Atwell
 Foreman for
 Daley Corp.)

Fergus st

Lt.

Rt

8+43⁸ (18) Lt. ^{3 2.66} 227.50
 C 5.16

— 5+

~~4+35~~

4+09 (W) Lt.

^{4.66}
 204.54
 C 0.12

—

~~8+57~~

8+31 (W) Rt.

^{2.48}
 232.00
 C 0.48

3+93⁸ (22) Lt.

^{20 4.07}
 199.49
 C 4.58

— 4

8+15⁸ (21) Rt.

^{3 1.3 C}
 226.00
 C 5.36

~~3+85~~

3+59 (W) Lt.

^{2.69}
 202.07
 C 0.62

—

~~6+35~~

6+09 (W) Lt.

^{19.23}
 218.95
 C 0.28

~~3+69~~

3+45 (W) Rt.

^{2.31}
 201.95
 C 0.36

5+93⁸ (19) Lt. ^{9.70} 212.00
 C 7.70

— 6

3+43⁸ (23) Lt.

^{202.09}
 198.05
 C 4.04

— 4

~~5+85~~

5+59 (W) Lt. ^{15.82} 215.20
 C 0.62

3+32
 3+29⁸ (25) Rt.

^{202.10}
 197.40
 C 4.70

5+43⁸ (20) Lt. ^{15.68} 209.00
 C 6.68

— 5+

0-52.85 = N14 line AKINS for (S)

0-26.67 = " " " for (W)

From AKINS to Brooklyn st.

12-4-53

9922-L

F.B. 2217-9

9923-L

" 2220-2

9924-L

9925-L

S.W.B.R. Fergus + Brooklyn 242.79

Fergus St.

Note 0100 for sewer

laterals = 52.85 N. of N. line Akins

0100 for balance of job

= 26.67 - North of Nly
line Akins

10435 10409 (W) Lt.	2.16 241.53 C 0.63	—
9+93 ⁸ (16) Lt.	40.99 235.00 C 5.99	— C
9+85 9+59 (W) Lt.	39.22 238.85 C 0.57	—
9+43 ⁸ (17) Lt.	7.91 233.00 C 4.91	— S
8+85 8+59 (W) Lt.	3.41 233.49 F 0.08	—

C2nd Akins to Brooklyn 70
Sewer laterals + Water Service.

INDEXED

A+98 Lt. = (W)	12.10 209.86 C 2.24	—
A+89 Lt. = (S) # 11	12.13 204.00 C 8.13	—
2+82 Lt. = (W)	91.01 192.49 F 1.48	—
2+76 Lt. = (S) # 12	90.67 185.00 C 5.67	—
2+18 Lt. = (S) # 13	8.34 184.00 C 4.34	—
2+07 Rt. = (W)	—	88.81 190.43 F 1.62
1+92 Rt (S) # 15	—	7.91 181.80 C 6.11
0+20 ⁶ Lt. (W)	86.77 190.91 F 4.14	—

0+00⁶ = (E Sta.) Nly line Akinson west

⑤ + ⑥ - 62nd st.

6+60 Lt. ⑥
5.37
222.77
C 2.60

6+50 Rt. ⑥
—
21.98
222.07
F 0.09

6+45 Lt. ⑤ #5
23.96
217.79
C 6.17

6+40 Rt. ⑤ ⑩
—
20.94
217.35
F 3.59

6+06 Lt. ⑥
20.08
218.72
C 1.36

5+91 Lt. ⑤ #6
9.42
213.03
C 6.39

5+49⁵⁰ Rt. ⑥
—
13.70
214.14
F 0.44

5+39⁴⁰ Rt. ⑤ #9
—
13.07
208.52
C 4.55

62nd st

71

9+70 Rt. = ⑥
—
9.36
241.06
F 1.70

9+60 Rt. = ⑤ #7
—
9.14
234.00
C 5.14

8+80 Rt. = ⑤ #8
—
4.96
230.00
C 4.96

8+22 Lt. = ⑥
30.51
232.55
F 2.04

8+07 Lt. = ⑤ #2
9.33
226.30
C 3.03

7+68 Lt. ⑥
31.08
229.51
C 1.57

7+53 Lt. = ⑤ #3
30.31
224.00
C 6.31

6+99 Lt. = ⑤ #4
8.42
221.70
C 6.72

Fergus St.
Akins to Brook 47

12/9/53

72

	Rough	el.	el.	Rough	A+00	Rough 3.53 202.73 C0.80	3.15 202.73 C0.42	3.01 203.22 F0.21	3.12 203.22 F0.10
					3+80	-	2.15 201.85 C0.30	2.13 202.35 F0.22	-
1+40	-	2.42 191.59 C0.83	1.81 192.09 F0.28	-	3+60 P.O.C.	1.39 201.07 C0.32	1.32 201.07 C0.25	1.38 201.57 F0.19	1.83 201.57 C0.26
1+20	2.41 190.23 C2.18	0.75 190.23 C0.52	0.52 190.73 F0.21	1.13 190.73 C0.40	3+20	200.73 199.62 C1.11	200.03 199.62 C0.41	0.06 200.12 F0.06	0.91 200.12 C0.79
1+00	-	9.05 188.80 C0.25	9.25 189.30 F0.05	-	2+80	9.60 198.16 C1.44	8.59 198.16 C0.43	8.66 198.66 X	9.74 198.66 C1.08
0+80	8.68 187.45 C1.23	7.64 187.45 C0.19	7.98 187.95 C0.03	90.41 187.95 C2.46	2+40 E.V.C.	8.81 196.70 C2.11	6.81 196.70 C0.11	7.06 197.20 F0.14	8.33 197.20 C1.13
0+60	-	6.07 186.27 F0.20	6.95 186.77 C0.18	-	2+20	-	5.81 195.91 F0.10	6.23 196.41 F0.18	-
0+40	2.44 185.26 F2.82	5.26 185.26 X	5.60 185.76 F0.16	A.02 185.76 F1.74	2+00	7.59 195.00 C2.59	4.95 195.00 F0.05	5.31 195.50 F0.19	7.77 195.50 C2.27
start obs. 0+26.18	1.70 184.70 F3.00	4.41 184.70 F0.29	4.41 185.20 F0.79	3.07 5.20 F2.13	1+80	-	4.50 193.98 C0.52	4.39 194.48 F0.09	-
0+00 = 2667 N. of N. line Akins.	183.71			184.21	1+60	5.65 192.84 C2.81	3.22 192.84 C0.38	3.34 193.34 X	4.74 193.34 C1.40

Fergus					Fergus				
Rough		Rough			Rough		Rough		73
				9+00	3.61 234.29 F0.68	Co.10	Co.139	6.05 234.29 C1.76	
6+20	-	7.83 217.86 F0.103	7.94 217.98 F0.104	8+50	1.30 231.61 F0.31	F0.17	C0.12	1.97 231.61 Co.36	
6+00 P.O.C.	7.64 216.34 C1.30	6.41 216.34 Co.07	6.48 216.50 F0.02	7.75 M 216.50 C1.25	8+00	9.09 228.93 Co.15	Co.04	Co.20	32.50 N 228.93 C3.57
5+65	4.34 213.64 Co.70	4.05 213.64 Co.01	3.96 213.87 Co.09	3.78 213.87 F0.09	E.V.C. 7+60	8.09 226.79 C1.30	7.05 226.79 Co.26	7.02 226.79 Co.23	8.40 226.79 C1.61
5+20 E.V.C.	4.50 210.16 Co.34	4.37 210.16 Co.21	4.60 210.50 Co.10	1.74 + 210.50 C1.44 LITE	7+40	-	5.93 225.68 Co.25	5.63 225.68 F0.05	-
5+00	-	8.79 208.69 Co.110	9.34 209.05 Co.129	-	7+20	6.44 224.52 C1.92	4.59 224.52 Co.07	4.48 224.54 F0.06	5.64 224.54 C1.10
4+80	8.68 207.30 C1.38	7.49 207.30 Co.19	7.79 207.69 Co.10	8.05 207.69 Co.36	7+00	-	3.17 223.31 F0.14	3.43 223.32 Co.11	-
4+60	-	5.86 206.01 F0.15	6.35 206.43 F0.08	-	6+80	3.64 222.04 C1.60	1.85 222.04 F0.19	1.85 222.07 F0.22	3.72 222.07 C1.65
4+40	4.30 204.82 F0.52	5.03 204.82 Co.21	5.05 205.27 F0.22	6.06 205.27 Co.73	6+60	-	0.76 220.70 Co.06	0.31 220.76 F0.45	-
4+20	-	4.02 203.73 Co.29	3.88 204.20 F0.32	-	6+40	2.004 219.31 Co.73	9.42 219.31 Co.11	9.13 219.40 F0.27	9.38 219.40 F0.02

Fergus

62nd

7A

0+01^E = N.W. Prop. Atkins + 62
 0+06^L = N.W. Prop. Atkins + 62nd

S.W. B.P. Fergus + Brooklyn Eb = 242.82

	Rough	cl	cl	Rough
set, 1+60	190.10	190.10	0.57 190.10	190.10
start cl. on top			Co.47	
1+58.31			0.73 190.10	1158.31
			Co.53	
1+30			9.99	
cl. on Lt.		→	190.10	
1+12.96 = end			F0.11	
1+00	87.20 190.10	7.91 190.10	190.10	190.10
0+83 ^{06 End}	F 2.90	F0.19	9.95 190.27	0+83 ⁰⁶
			F0.32	87.80
0+50	86.70 190.60	0.19 190.60	190.60	190.89
	F 3.90	F0.41	Co.16	F3.09
0+22.14 ^{cl.} EC.			1.57 191.32	
			Co.25	
0+10 ⁵ RT			7.59 191.50	
			F3.91	
0+06 ^L				
0+10 ²⁶ cl. EC.			0.79 191.02	
0+01 ^E	85.80 191.10	F0.23		
	F5.30			
start curbs			0.78 191.10	1.69 191.50
			F0.32	Co.19

	Rough		Rough
Brooklyn 3 rd 10+65 sly. line	243.00		3.31 243.30
10+55 cl. B.C.	242.60	2.67 242.60 Co.07	2.60 242.60 X
10+30	0.80 241.26 F0.46	Co.28	4.08 241.26 C2.82
10+00	9.17 239.65 F0.48	Co.10	41.12 X 239.65 C1.47
9+50	6.62 236.97 F0.35	X	8.09 236.97 C1.12

6279

6279

75

4+50

9.07	CO.17	CO.10	8.53
205.91			205.91
C 3.16			C 2.62

7+10

7.06	6.12	6.07	8.74
226.12	226.12	226.15	226.15
C-274	X	F0.08	C 2.59

4+00

4.87	grade	CO.31	2.70
201.80			201.80
C 3.07			C 0.70

6+90

4.90	4.73
224.83	224.86
C 0.07	F 0.13

3+50

200.02	CO.15	CO.15	8.73
197.68			197.68
C 2.34			C 1.07

6+70

5.87	3.39	3.33	3.84
223.48	223.48	223.49	223.49
C 2.39	F 0.09	F 0.16	C 0.35

3+10 Euc.

3.61	4.11	4.03	1.90
194.39	194.39	194.39	194.39
F 0.78	F 0.28	F 0.36	F 2.47

6+50

2.01	1.98
222.07	222.07
F 0.06	F 0.09

2+90

1.73	2.96	2.72	0.70
192.93	192.93	192.93	192.93
F 1.20	C 0.03	F 0.21	F 2.23

6+30

1.97	0.53	0.47	0.58
220.58	220.58	220.58	220.58
C 1.39	F 0.05	F 0.11	X

2+70

1.33	1.93	1.80	89.71
191.83	191.83	191.83	191.83
F 0.50	C 0.10	F 0.03	F 2.06

6+10

8.74	8.95
219.04	219.04
F 0.30	F 0.09

2+50

88.10	1.23	1.15	89.22
191.10	191.10	191.10	191.10
F 3.00	C 0.13	C 0.05	F 1.88

5+90 PUC

9.25	7.13	7.44	6.60
217.42	217.42	217.42	217.42
C 1.83	F 0.29	C 0.02	F 0.82

2+30 PUC.

87.71	0.80	0.79	83.4
190.74	190.74	190.74	190.74
F 3.03	C 0.06	C 0.05	F 2.40

5+50

6.33	F 0.02	C 0.15	3.85
214.14			214.14
C 2.19			F 0.29

1+95

86.85	0.37	0.49	87.26
190.42	190.42	190.42	190.42
F 3.57	F 0.05	C 0.07	F 3.18

5+00 N.

2.91	F 0.06	F 0.05	0.38
210.03			210.03
C 2.88			C 0.35

Cb. on left

1+83.29 = start

0.21
190.31
F 0.10

Sly. Braklyn ✓

10+30

244.30

244.48 ✓

M.H. on 62nd

6+83

~~A.50
224.78
C 0.12~~224.38 ✓
Grade10+20 ^{d.} B.C.^{3.92}
243.70^{3.22}
243.70^{3.40}
243.90^{A.20}
243.90

6+80=M.H.

C 0.22

F 0.48

F 0.50

C 0.30

10+00

^{2.44}
242.57

F 0.45

F 0.10

^{3.35}
242.76

6+77

F 0.13

C 0.59

~~A.60
223.97
C 0.23~~223.97 ✓
Grade

9+50

^{8.15}
239.76

F 0.95

F 0.22

^{9.10}
239.92

F 1.61

F 0.82

9+00

^{5.60}
236.95

F 0.24

F 0.20

^{6.38}
237.08

F 1.35

F 0.70

8+50

^{9.25}
234.13

F 0.13

F 0.10

^{6.77}
234.24

F 4.88

C 2.53

8+00

^{9.00}
231.31

F 0.10

grade

^{3.76}
231.40

F 2.31

C 2.36

7+50 E.V.C.

^{9.60}
228.50^{8.60}
228.50^{8.41}
228.56^{31.92}
228.56

C 1.10

C 0.10

F 0.15

C 3.30

7+30

^{7.39}
227.34

C 0.05

^{7.24}
227.39

F 0.15

Virginia Way
Storm Drain

12-29-53

W.O. 21139

INDEXED

JER

JUL 30 1954 sheet 5099-B.

FB. 222-36

stakes 5' Lt. of ~~to~~

0+00 = Existing pipe at

N. Ely and Virginia Way.

Existing 18"

0+92

148.95

146.54

C 2.41

0+58.6

134.92

134.73

C 0.19

0+39.1

127.86

120.70

C 7.16

0+35.7

22.94

118.66

C 4.28

0+31.9

21.89

117.24

C 4.65

0+28

20.81

116.50

C 4.31

Existing 24"

0+00

113.70

111.17

111.37

C 5.80

Alley BIK. 11.

North Shore Highlands

Fanuel to Events

between Law + Beryl

0.25' exception on south

0.50' " " North

stakes set in relation to

edge of Pav. (not Prop. line)

0+00 = wly line Fanuel.

2+00 #2 100.10
99.69
C 0.41

1+60 x 4.07
p.25' 100.73
C 3.3, 4

E.O.C. N 2.38
1+20 0.40 101.77
C 0.61

1+00 N 2.54
0.25 102.17
C 0.37

0+80 N 1.95
~~1.85~~ 102.39
F 0.44

0+60 N 2.02
1.80 102.40
F 0.38

0+40 #4 2.35
102.24
C 0.11

0+20 #2 2.91
101.96
C 0.95

P.O.C. ✓
0+00 101.46 ✓

102.49

78

1.43 N
99.99 0.04 in
C 1.44

2.28 N
101.03 0.26
C 1.25

2.57
102.07 D 2
C 0.50

3.04
102.47 D 2
C 0.57

4.90 N
102.69 1.40
C 2.21

4.89 N
102.70 1.50
C 2.19

3.49 D
102.54 1.25
C 0.95

3.36 D 1.50
102.26
C 1.10

102.02 ✓

477

A+70	N 1.08	7.30 95.17 C 2.13	8.00 95.47 C 2.53	□ 1.68
A+50	N 1.37	8.18 96.52 C 1.66	7.86 96.82 C 1.04	□ 1'
A+30	N 2.05	8.31 97.01 C 1.30	8.76 97.31 C 1.45	N 1.58
A+20	N 2.10	8.28 97.05 C 1.23	8.35 97.35 C 1.00	□ 2'
3+80	N 0.85	8.05 97.25 C 0.80	8.20 97.55 C 0.65	□ 2'
3+40	N 0.102	8.15 97.57 C 0.58	8.91 97.87 C 1.04	□ 0.50
3+00	0.1	7.93 97.94 C 0.01	0.01 98.24 C 1.77	N 0.15
2+80	0.2	7.90 98.15 C 0.25	9.28 98.45 C 0.83	X 2'
2+40	0.2	7.08 98.79 C 0.29	0.75 99.09 C 1.66	N 0.02

98.82

79

□-3' NT.

0+39³ Lt. = (5) #1

102.96
94.88

C 8.08

Ely. Events

4+99² 92.91 93.20

4777

4770

4750

4730

4720

3780

3740

3700

2780

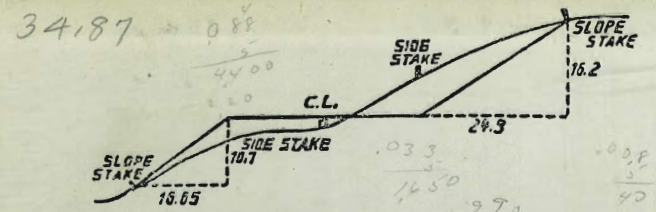
2740

313

313

2443

32.01 79.83 28.14 1161
 TR 1354
 91.255
 A 13.71 12.67 3516C
 294.64 447
 119.07 16.20
 116378 8.41
 576 10.79 317
 975
 69.48 - E Colma 033 33
 54.642 Ramicia 45 31
 2805 RR spike 145 97 42.81
 1485 1155 41.48
 1.33
 799.60 5733 111
 22.42 248 67 18
 5507
 935
 2.50 17.8 11
 8685
 2+40 79.83
 2+80
 2+40



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY
 HOLYOKE MASSACHUSETTS
 NEW YORK CHICAGO BOSTON SAN FRANCISCO