

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 15 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side of shoulder
stake for any width roadway slope 1 to 1
If ground is nearly level the cut or fill is small

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find tangent and distance for curve of
any other degree divide by degree of curve and
add correction found in column of corrections
Degree of curve with a given L can be found
by dividing tangent (or distance) opposite L by
tangent (or distance) (or curve).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
multiplied by twice the degree.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.971	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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Clark
Shepherd
Bruner
ONEIL
W.O. 31861
4-3-53

TMP. BETA ST.

38' to 36' 1/4

Ref. DATA: T.P. 411 at 36' 1/4
FB. 2159-B from Δ between 36' 1/4 + 37' 1/4
to 38' 1/4.

LT		RT		STA	P.L.	CB	Σ	CB	P.L.
STA	P.L.	CB	Σ	CB	P.L.				
1718.11	8.41 8.21 Co.20	8.36 8.21 Co.15		8.36 8.23 Co.13	8.48 8.23 Co.25	3+25		7.99 7.68 Co.31	7.85 7.69 Co.16
0+98.11		8.48 8.43 Co.05		8.14 8.32 Fo.18		3+00	7.84 7.74 Co.10	7.87 7.74 Co.13	7.85 7.75 Co.10
0+78.1/2	9.56 8.60 B.V.C. Co.96	8.69 8.60 Co.09		8.43 8.42 Co.01	8.79 8.42 Co.37	2+75		8.01 7.80 Co.21	7.89 7.81 Co.08
0+49.05		8.93 8.89 Co.04		8.71 8.60 Co.11		2+50	7.94 7.86 Co.08	8.02 7.86 Co.16	7.99 7.88 Co.11
0+20 = CB	10.12 9.18 BC Co.94	9.38 7.18 Co.20		8.25 8.78 Fo.53	9.47 8.78 Co.69	2+25		8.13 7.92 Co.21	8.08 7.94 Co.14
# 1		7.72 9.30 Co.42		Knocked 8.12 out 8.80 Fo.68	7.80 8.80 Fo.00	2+00	8.09 7.99 Co.10	8.31 7.99 Co.32	7.69 8.00 Fo.31
# 2		9.58 7.38 Co.20		8.40 8.82 Fo.42		1+75		8.46 8.05 Co.41	8.43 8.03 Co.38
# 3 (S.W)	Knocked out	9.70 9.70 Co.30	9.37 9.40 Fo.03	8.69 8.85 Fo.76		158.11 E.V.C.	8.24 8.10 Co.14	8.41 8.10 Co.31	8.25 8.10 Co.15
(0+00 = N.W. Lwe 38' 1/4) (E.V.C.)						1438.11		8.41 8.15 Co.26	8.48 8.16 Co.32
B.M.	DIV. BAR RUN:			6.35 = chd N.W. Cottonwood Thro.		CB END			

STA.	P.L.	CB	♀	CB	P.L.
5+50	6.79 7.11	6.15 7.11 Fo.36		7.05 7.13 Fo.08	7.12 7.13 Fo.01
(5+40 Sew ^{#2} LT)	Fo.32 → 2.62 C4.17	FLP.L.	-6.79 -0.45 C7.24		
5+25		6.91 7.17 Fo.26		7.19 7.19 Grade	7.20 7.19 Co.01
(5+20.5 RT WATER)	7.10 7.19 Fo.09				
5+00	6.87 7.24 Fo.37	6.83 7.24 Fo.41		7.11 7.25 Fo.14	6.98 7.25 Fo.27
4+75		7.14 7.30 Fo.16		7.27 7.31 Fo.04	
(4+70 RT only WATER)				7.36 7.33 Co.03	
4+50	7.25 7.37 Fo.12	7.52 7.37 Co.15		7.30 7.38 Fo.08	7.65 7.38 Co.27
4+25		7.50 7.43 Co.07		7.54 7.44 Co.10	
4+00	7.91 7.49 Co.42	7.64 7.49 Co.15		7.66 7.50 Co.16	7.52 7.50 Co.02
3+75		7.80 7.55 Co.25		7.73 7.56 Co.17	
3+50	7.83 7.62 Co.21	7.84 7.62 Co.22		7.85 7.63 Co.22	8.15 7.63 Co.52

STA.	P.L.	CB	♀	CB	P.L.
# 4	7.18	7.38 7.18 Fo.20			6.85 7.18 Fo.33
# 3	7.15	6.95 7.15 Fo.20			6.92 7.12 Fo.20
# 2	7.10	6.78 7.10 Fo.32			7.00 7.10 Fo.10
# 1	7.01	6.68 7.01 Fo.33			7.05 7.05 Grade
(Co.00) = E.L.	6.77 7.03				7.10 7.08 Co.02
(Rough G. only)	374h Fo.26				
(5+90 Sew ^{#1} LT)	P.L. 2.50 F.L. C4.25	6.75 -0.75 F.L. C7.50			
(B. Returns)					
(R'y 374h Above)					
(5+83.88 RT)					
5+84	7.02	6.76 7.02 Fo.26			7.06 7.04 Co.02
= CB.AC					
5+75		6.80 7.05 Fo.25			7.06 7.07 Fo.01
(5+70 RT WATER)	6.97 7.06 Fo.09				7.09 7.08 Co.01

BETA ST.
37' th to 36' th

STA	P.L	CB	♀	CB	P.L	STA	P.L	CB	♀	CB	P.L
(0+55 RT only) water					6.35 6.36 T.C.B. CO.19						
0+50	6.95 6.37 CO.38	6.42 6.37 CO.05		6.70 6.37 CO.33	6.67 6.37 CO.30	2+75	5.83	5.81 5.83 FO.02		5.82 5.83 FO.01	
0+25	6.43	6.63 6.42 CO.21		7.02 6.42 CO.60		2+50	6.35 5.89 CO.46	6.10 5.89 CO.21		5.76 5.89 FO.13	6.30 5.89 CO.41
(0+00 = W'ly Line) 37' th	7.37 6.60 CO.77				7.28 6.60 CO.68	2+25 water on RT.	5.95	6.11 5.95 CO.16		6.16 5.95 CO.21	6.19 5.95 T.C.B. CO.24
0+15.18 LT 0+15.58 RT CB. B.C.		6.88 6.45 CO.43		6.97 6.45 CO.52		2+00	6.28 6.01 CO.27	6.71 6.01 CO.70		6.40 6.01 CO.39	6.27 6.01 CO.26
# 1		6.95 6.55 CO.40		6.58 6.52 CO.06		1+75 water on RT.	6.07	5.97 6.07 FO.10		5.97 6.07 FO.10	6.13 6.07 T.C.B. CO.06
# 2		7.00 6.63 CO.37		6.63 6.65 FO.02		1+50	6.60 6.13 CO.47	6.19 6.13 CO.06		6.35 6.13 CO.22	6.67 6.13 CO.54
# 3		7.13 6.70 CO.43		6.68 6.70 FO.02		1+25	6.19	6.29 6.19 CO.10		6.35 6.19 CO.16	
# 4		7.46 6.72 CO.74		7.04 6.76 CO.28		1+00	6.52 6.25 CO.27	6.41 6.25 CO.16		6.30 6.25 CO.05	6.29 6.25 CO.04
CB Ret's. W'ly 37' th						(0+95 RT only) water	0+75	6.58 6.31 CO.21		6.61 6.31 CO.30	6.45 6.26 T.C.B. CO.19
						(0+65 LT only) water	0+65	6.54 6.33 T.C.B. CO.21			

STA.	P.L.	CB	♀	CB	P.L.	STA.	P.L.	CB	♀	CB	P.L.
5+00	5.58 5.28	5.57 5.28		4.94 5.28	5.95 5.28						
(4+85 RT only) WATER	CO.30 5.57 5.33 TR. CA CO.25	CO.29		F0.34	CO.67						
4+75		5.26 5.34		5.55 5.34							
		F0.08		CO.21							
4+50	5.90 5.40	5.30 5.40		5.66 5.40	6.15 5.40	CHK:				6.38 - 6.35 = (See Gm) Pg 1	
(4+35 RT only) WATER	CO.50 5.46 5.23 TR. CA CO.03	F0.10		CO.26	CO.75						
4+25		5.48 5.46		5.86 5.46							
		CO.02		CO.10							
4+00	5.94 5.52	5.56 5.52		5.76 5.52	5.96 5.52						
(3+88 RT only) WATER	CO.42	CO.04		CO.24	CO.43						
3+75		5.67 5.58		5.72 5.58							
		CO.09		CO.14							
3+50	5.97 5.64	6.18 5.64		5.73 5.64	5.97 5.64	6+17.6 RT 6.16 RT Ely P.L. 364h 6+00	6.20 5.80 01.20	5.02 5.00 CO.02		5.60 5.00 CO.60	6.00 5.00 CO.00
1- (3+27.90 ON RT)	6.19	5.83		5.73	5.62			5.04 5.04 Grade		5.69 5.04 CO.65	
(3+27.51 ON RT)	5.69 CO.50	5.69 CO.14		5.70 CO.09	5.70 F0.08	6+15" (3+28 RT) WATER	5.46 5.09 TR. CA CO.02	5.15 5.10 CO.05		5.70 5.10 CO.60	5.04 5.07 CO.77
(3+05 RT only) WATER				5.87 5.76 TR. CA CO.11			5.83 5.16	5.45 5.16 CO.29		5.61 5.16 CO.45	6.06 5.16 CO.90
3+00	6.37 5.77	6.01 5.77		5.86 5.77	5.95 5.77	5+50 (3+28 RT only) WATER	5.83 5.16 CO.67	5.45 5.16 CO.29		5.61 5.16 CO.45	6.06 5.16 CO.90
	CO.60	CO.24		CO.09	CO.18		5.46 5.20 TR. CA CO.16				5.63 5.20 TR. CA CO.73
						5+25		5.54 5.27 CO.32		5.50 5.27 CO.28	

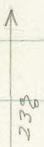
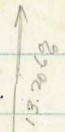
Clark
Shepherd
SPURER
O'Neil
6-5-53
W.D. 62328
STA.

SEWER - 65th - SLY IMPERIAL
to SHAUKES, thence WLY

65th - IMP. to SHAUKES
REF. DWG: 2194-D

INDEXED
DEC 6 1954

STA.	GRADE	STA.	GRADE
1+60	236.39 230.39 C 6.20	4+55	308.85 301.15 C 7.70
1+25	231.89 225.77 C 6.12	4+20	300.57 293.10 C 7.47
0+90	227.19 221.15 C 6.04	3+85	291.78 285.05 C 6.73
0+55 BKK, Grate	222.22 216.53 C 5.69	3+50 = GRADE BKK!	283.98 277.00 Fl. C 6.98
0+43	221.01 215.37 C 5.64	3+15	275.05 266.97 C 8.06
0+35	220.89 214.53 C 6.36	3+05 Sewer 1/2" 8" LT. 264.88 FLG "y"	270.58 264.86 FL C 5.78 265.35 256.99 C 8.36
0+25	220.75 214.01 C 6.74	2+80	254.66 246.99 C 7.67
0+15	220.92 213.81 C 7.11	2+10 = M.H. #1 = Grade BKK! Stubs set 5' 11" at 90° off F.V. TANG. 210 3/4" RT.	244.47 237.00 Fl. C 7.47
0+00 = M.H. IMPERIAL 4165 N 4/8 65th (DWG 1088-D)	213.75 F. LINE	1+95 1+76 LAT #7 RT.	241.30 235.01 C 6.29 239.04 233.34 Fl. P.L. C 5.70
B.M. NY. BRK. ROD.	223.64 T.P.F. HYD.	S.E. IMPERIAL + 65th	



6546 (CONT.)

CHK:

388.75 = 388.99 - Cur Man E 6544 Shales

STA.	GRADE	STA.	GRADE
6+95	341.33 335.30 C 6.03	(= 0+100 W/ly) 7+93.28 = M.H. #5	389.08 381.00 F.L. C 8.08
CHK	CON. MAN E 6544 L.V. M.H. ONE TO EAST	7+60	387.45 379.39 C 8.06
6+60 = M.H. #3	334.13 328.00 F.LINE C 6.13	9+25	385.78 377.70 C 8.08
6+40	332.17 325.95 C 6.22	9+13 = LAT #3	388.50 F.L. Prop 378.23 C 10.27
6+05	331.34 322.34 C 9.00	8+90 = M.H. #4	383.74 376.00 = F.L. C 7.74
5+70	326.79 318.72 C 8.07	8+70	382.59 371.83 C 10.76
5+35	322.59 315.11 C 7.48	8+46 = LAT #2	381.31 Ad 372.31 F.L. Prop C 9.00
5+00 = M.H. #2	318.24 311.50 = F.LINE C 6.74	8+35	374.91 367.52 C 10.39
4+90	316.85 309.20 C 7.65	8+00	367.11 357.21 C 9.90
		7+77 = LAT #1	358.87 349.91 C 8.96
		7+65	349.66 342.60 C 7.06
		7+30	

10.1875

^

10.3125

↑
6
6

↑

10.1875

↑

↑

↑

↑

65 1/2 H. (Cont.)
SHAULES - 65 1/2 ST. WLY 169'

CHK:	388.98 = 388.99	Common C	65 1/2 H + Shaules
LOT # 6	FLG 396.15	404.20 Bal F.M.H. 396.90 7.30	
1+69 = D.END.		403.74 395.90 C 7.84	
1+40		401.57 393.34 C 8.23	
1+25 LOT # 5 RT.	FLG 392.27	400.61 Bal FL.M.H. 393.02 C 7.59	
1+05	"Y"	398.70 390.26 C 8.44	
0+70		395.63 387.17 C 8.46	
0+35		392.12 384.09 C 8.03	
0+00 = M.H # 5 (E Shaules + ELY 21' LINE 65 1/2 H.)		381.00 (no P.H. 7)	
Sen/LOT # 4	FLG 387.30	390.65 FL.M.H. 388.11 C 5.54	
10+43.28 = D.END. 65 1/2 (5LY SHAULES)		391.71 384.00 FL C 7.71	
10+18.28		382.50	

8800
↑

Clark
S. Portland
O'Neil
6-24-53
W.O. 32031

IMPS - 504th ST. - ORANGE (S. LINE)

Sly 300 FT

REF: T.S. 3664
DWL: 10203-L
10202-L
10201-L

INDEXED
JER

JUL 13 1954

9

(E) LT.

RT (WLY)

STA.	P.L.	CB	Z	CB	P.L.	STA.	P.L.	CB	Z	CB	P.L.
1+10 = Brk = B.V.C	323.69 322.60 C 1.09	322.61 322.60 C 0.01		322.94 323.11 F 0.17	322.98 323.11 F 0.13	2+65	318.30 315.76 C 2.54	315.50 315.76 F 0.26		315.52 315.55 F 0.03	317.62 315.55 C 2.07
0+83.75		322.23 322.25 F 0.02		323.12 322.85 C 0.27		2+45		317.29 317.54 F 0.25		317.30 317.43 F 0.13	
0+57.50	321.84 321.90 F 0.06	321.86 321.90 F 0.04		322.85 322.59 C 0.26	324.14 322.59 C 1.55	2+25	320.80 319.03 C 1.77	318.66 319.03 F 0.37		319.15 319.01 C 0.14	318.80 319.01 F 0.21
(Ch 15) 0+31.25		321.64 321.55 C 0.09		322.30 322.33 F 0.03		2+06 - W.M. RT.				320.31 170 ca.	
CB Bc 0+05	321.40 321.30 C 0.20	320.84 321.20 F 0.36		324.97 322.07 F 0.10	324.77 322.07 C 2.70	2+05		319.84 320.26 F 0.42		320.56 320.37 C 0.19	
(0+00 = S. LINE ORANGE)				321.52 321.73 321.98 F 0.25 F 0.46		1+85	322.20 321.20 C 1.00	320.92 321.84 321.20 321.64 F 0.23		321.57 321.38 C 0.19	320.78 321.38 F 0.60
" 1		320.68 321.06 F 0.38									
" 2		321.08 320.90 C 0.18		321.79 322.00 F 0.21		1+70		321.50 321.80 F 0.30		322.01 322.06 F 0.05	
" 3 =				321.88 322.23 322.16 C 0.07 F 0.28		1+50	322.84 322.43 C 0.41	322.23 322.43 F 0.20		322.64 322.77 F 0.13	321.85 322.77 F 0.92
(20' CB. RADII)						1+30		322.66 322.69 F 0.03		322.82 323.13 F 0.31	

B.M: 1st Elev. Rod. (see NEW B.M. Page 11) 320.87 = S.E. B.P. ORANGE + 504L

STA	P.L.	LT.	CB	E	CB	RT.	P.L.
CAK				320.85			320.87 (see B.M)

STA	P.L.	LT.	CB	E	CB	RT.	P.L.
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3+05 = END GRADING
 314.23
 311.87
 C 2.86

306.60
 311.02
 F 4.42

3+01 = FENCE
 FENCE ACROSS ROADWAY

3+00 = END CDS
 311.27
 311.81
 311.95
 1/2 PAY. & 5/8" FC
 OF WALLS ACROSS C&G. TT
 2+94 = W. M.A.T.
 312.65 M.C.A.

311.90
 311.64
 Co. 26
 311.64

2+85
 313.71
 313.35
 313.71
 F 0.36

313.35
 313.42
 F 0.07

2+80 = S. LOT
 1. LT. (PL)
 317.57
 309.46
 C 8.11

317.57
 306.68
 C 10.89
 RT. END MAIN

50' N ST. - N. LINE ORANGE
to S. LINE TROJAN

(only) LT.

STA.	P.L.	CB	E	CB	RT. (E.W.) P.L.
1+15	329.51 327.48 C203	327.36 327.78 Fo.12		326.38 326.58 Fo.20	327.52 326.58 C.94
0+87.5		326.19 326.43 Fo.24		325.36 325.53 Fo.17	
0+60.00	327.42 325.38 C2.04	325.09 325.38 Fo.29		324.25 324.48 Fo.23	326.07 324.48 C1.59
0+32.5	326.35 324.34 C2.01	324.10 324.34 Fo.24		323.05 323.44 Fo.39	325.78 323.44 C2.34
0+05 CA, BC	325.25 323.29 C2.06	322.91 323.29 Fo.38		321.93 322.39 Fo.46	322.90 322.39 C0.51
# 1		322.62 322.90 Fo.28		321.44 322.13 Fo.69	
# 2		322.92 322.93 Fo.01		322.14 321.94 C0.20	
# 3 -CA, E.C		323.44 323.16 C0.28	CHK:	321.73 <small>TR. DIST. CB.</small> 321.72	

Note: This B.M. transferred to new B.P.
 N.B. ORANGE + 50' N = 321.54
 (approx. 5' EAST EC)
 B.M. N.W. E.R.V. Rd.
 320.87 = S.E. B.P.
 ORANGE + 50' N

STA.	P.L.	LT.	CB	Q	CB	RT.	P.L.
3+10			338.49 338.51 Fo.02		337.47 337.61 Fo.14		
2+90	338.22 336.79 C1.43		336.56 336.79 Fo.23		335.58 335.89 Fo.31	333.90 335.89 F1.97	
2+70			334.85 335.22 Fo.37		334.09 334.32 Fo.23		
2+50	336.03 333.79 C 2.24		333.53 333.79 Fo.26		332.61 332.89 Fo.28	331.91 332.89 F1.08	
2+30			332.24 332.52 Fo.28		331.29 331.62 Fo.33		
2+10	333.89 331.39 C2.50		330.96 331.39 Fo.43		330.30 330.49 Fo.19	329.93 330.49 Fo.56	
1+90			329.95 330.41 Fo.46		329.31 329.51 Fo.20		
1+70 = B.V.C. (-WS LT.)	330.87 329.58 C1.29		329.14 329.58 Fo.44		328.40 328.68 Fo.28	329.24 328.68 C0.56	
1+42.5			328.92 328.53 Fo.21		327.21 327.63 Fo.42		

LT.		RT.	
STA	P.L	CR	E
4470		357.19 357.52 Fo.33	356.45 356.62 Fo.17
4450	357.74 357.63 C 3.11	354.43 354.63 Fo.20	353.73 353.73 GRADE F 4.02
4430		351.60 351.88 Fo.28	350.87 350.98 Fo.11
4410	352.35 349.29 C 3.06	349.13 349.29 Fo.16	348.23 348.39 Fo.16 344.92 348.39 F 3.47
3490		346.74 346.84 Fo.10	345.85 345.94 Fo.09
3470	348.00 344.54 C 3.46	344.65 344.54 C 0.11	343.42 343.64 Fo.22 341.77 343.64 F 1.87
3450		342.37 342.38 Fo.01	341.25 341.48 Fo.23
3445	V. Service RT.		
3430	344.20 340.37 C 3.83	340.23 340.37 Fo.14	339.29 339.47 Fo.18 337.04 339.47 F 2.43

LT.		RT.	
STA	P.L	CR	E
(Cont. next p.)			
5490	374.70	374.24 374.70 Fo.46	373.40 374.12 Fo.72 374.12
5472	V.S. - RT.		
5470	374.20 372.23 C 1.97	372.10 372.23 Fo.13	371.72 371.97 Fo.25 372.95 371.97 C 0.98
5450	= B/C	372.08 369.89 C 2.19	369.82 369.89 Fo.07 368.85 368.99 Fo.14 367.03 368.99 F 1.96
5420		365.45 365.23 C 0.22	364.17 364.33 Fo.16
5419	V.S. - RT.		
4490	= E.V.C	363.80 360.56 C 3.24	360.51 360.56 Fo.05 359.45 359.66 Fo.21 359.71 359.66 F 5.95

STA.	P.L.	CB.	Σ	CB.	P.L.	N. W	N. E	RET'S
CHK			320.85	320.87	(see B.M)	CB.		CB.
CHK			376.21	376.16	N.W. B.P. (Rough cross) 50% TROJAN	(N.W)		(N.E)
						CB. B.C. (50%+L)	375.75 meet	375.85 meet
						# 1	376.34 376.00 Co.34	375.48 375.80 Fo.32
						# 2	376.37 376.09 Co.28	375.51 375.77 Fo.26
						# 3 = E.C.	376.05	375.04 375.72 Fo.68
# 3		375.79	meet	374.00 375.22 F1.22				
# 2	375.31 375.75 Fo.44	375.66 376.75 Fo.09 KNECKED OUT		374.04 375.20 F1.16				
# 1	374.92 375.48 Fo.56	374.65 375.48 Fo.83		373.98 374.86 Fo.88	(S.E)			
5792 =	CB. B.C. (50%+L) 375.27 374.89 Co.38	374.21 374.89 Fo.68		373.53 374.30 Fo.77			373.78 374.30 Fo.52	

WINONA - W. Line
ORANGE - NLY 300

WINONA - W. Line				ORANGE - NLY 300			
STA	P.L.	CB	RT. (E.L.)	STA	P.L.	CB	RT. (E.L.)
1+20 = W.S. RT.							
1+00	337.22 336.40 C0.82	336.36 336.40 F0.04	336.05 336.30 F0.25	2+83.5 = END CB. ON RT. (Meet Ex. 1, T)			(meet) 360.13
0+80		334.94 334.80 C0.14	334.44 334.70 F0.26	2+66.66 =	358.04 357.47 C0.57	357.25 357.47 F0.22	356.97 357.53 F0.56
0+70 = W.S. RT.							
0+60 = B.Y.C.	335.57 335.87 333.40 C2.17 C2.17	333.40 333.40 GRADE	333.04 333.20 F0.16	2+43.33		353.58 353.93 F0.35	353.76 354.06 F0.30
0+32.5		331.67 331.75 F0.08	331.50 331.51 F0.01	2+20 = E.Y.C.	349.28 350.40 F0.12	350.08 350.40 F0.32	350.31 350.60 F0.29
(27.5)							351.00 350.60 C0.40
0+05 = CB B.C.	331.89 330.10 C1.79	329.84 330.10 F0.26	329.88 329.81 C0.07	2+00		347.09 347.60 F0.51	347.44 347.80 F0.36
W.P. Line ORANGE	# 1	329.62 329.80 F0.18	329.53 329.50 C0.03	1+80	344.65 344.80 F0.15	344.58 344.80 F0.22	344.80 345.00 F0.20
	# 2			1+60		341.98 342.30 F0.32	342.18 342.40 F0.22
	# 3			1+40	340.79 340.20 C0.59	339.97 340.20 F0.23	339.92 340.20 F0.28
				1+20		338.15 338.20 F0.05	337.94 338.10 F0.16
B.M.	DK. Elev. Rod:		332.95 = S.E. B. P 49424 ORANGE				

STA.	LT.	P.L.	CB	LT.	CB	RT.	P.L.
------	-----	------	----	-----	----	-----	------

CHK: 362.26 = 362.25 = TP CB 300 LT
 F. GRADE

CHK: 362.26 = 362.25 TACB 300 LT
 (ROUGH GRADES)

3100 = END CB LT. 362.25
 Limit of Grading.
 F. GRADE.

2490 = END	361.06	360.48	360.83	
	361.00	361.00	361.00	361.00
	0.06	0.52	0.17	

Clark
owner
Ore. L.
Pumil
9-8-53
W.D. 32055

IMP'S: Rose, STEWART, MILLAR,
HOBERT, 63rd et al

SEWER + WATER Lot's Rose ST.
MILLAR to 63rd

CHK

462.44 = 462.45 (See B.M.)

2455 = Sew. Lot ① LT. P.L. 465.73
E 458.65 465.73
C 6.73 C 7.08 455.80 P.L. 459.93

2430 = W.S. LT. 465.56
464.90 tp ca +
C 0.66

2422 = W.S. RT. 465.81
464.90 tp ca +
C 0.91

2415 = Sew. Lot ① LT. P.L. 466.29
E 459.00 466.29
C 7.29 C 7.64 455.60 P.L. 459.69

2405 = Sew. Lot ② RT. P.L. 465.84
E 455.60 465.84
C 10.24 C 6.69 P.L. 459.50
C 6.34 4455 = W.S. LT. 464.30
464.10 tp ca +
C 0.20

0480 = W.S. RT. 465.43
463.75 tp ca +
C 1.68

4440 = Sew. Lot ③ LT. P.L. 463.95
E 459.00 463.95
C 4.95 C 6.40

0465 = Sew. Lot ④ RT. P.L. 465.13
E 454.88 465.13
C 10.25 C 6.98 P.L. 458.50
C 6.63 2481 = W.S. RT. 465.17
464.70 tp ca +
C 0.47

0-01 = W.S. RT. 463.66
463.20 tp ca +
C 0.46

2468 = W.S. LT. 465.33
464.80 tp ca +
C 0.53

0-12 = Sew. Lot ② RT. P.L. 462.76
E 454.49 462.76
C 8.27 C 5.11 P.L. 458.00
C 4.76

0400 = E. line MILLAR. 2464 = Sew. Lot ⑥ RT. P.L. 465.35
E 455.87 465.35
C 9.48 6.20 P.L. 459.50
C 5.85

B.M.

5'4" x m.H. rim
462.45 = E MILLAR + STEWART (FB 2226-42)

B.M. Fr. fire 44. Rose + MILLAR
DIV. Elev. ROD

465.72
(Hyd. DINED)

SEWER & WATER LOTS MILLAR ST

ROSE to HOBBART.

STA.	CHK.	457.22 =	457.25 =	SLY X Rem MH HOBBART + MILLAR
4+15 = W.S.	RT.	457.22	457.25	460.49 + p CB ±
4+10 = W.S.	LT.	459.59 459.90 + p CB ± F. 31		
3+95 = Sew. LAT # 10	LT.	P.L. 460.13 C 5.13	460.13 E 454.60 C 5.53	460.13 E FL 457.43 C 12.70
3+88 = Sew. LAT # 9	RT.	E FL 460.41 C 13.11	460.41 E 453.00 C 7.41	P.L. 460.41 455.50 C 4.91
3+50 = W.S.	LT.	460.70 460.50 + p CB ± F. 0.20		
3+36 = Sew. LAT # 11	LT.	P.L. 461.08 455.00 C 6.18	461.08 E 454.60 C 6.48	(Joint chimney, EX)
1+22 = Sew. LAT # 8	RT.	E FL 462.94 453.55 9.39	462.94 E 456.85 C 6.09	P.L. 462.94 457.25 C 5.69
1+07 = W. Service	RT.		463.69 462.30 + p CB ± C 1.39	
0+00 = N. by Line ROSE				
B.M.	DIV. Elev. PO.		462.45 = SLY X Rem MH Stewart + Millar	

SEWER LOTS - STEWART ST.

MILLAR to 63' rd

(All LOTS connect to EXIST. 6" chimneys)
on E-Sewer

STA.	CHK.	457.28 =	457.25 =	SLY X Rem MH HOBBART + MILLAR
3+80 = W.S.	RT.	457.28	457.25	462.95 463.13 + p CB ± F. 18
3+65 = Sew. LAT # 16	RT.	463.21 E 457.50 5.71		P.L. 463.21 458.00 C 5.21
2+35 = Sew. LAT # 15	RT.	463.20 E 458.50 C 6.70		P.L. 463.20 457.00 C 6.20
2+20 = W.S.	RT.			463.18 462.48 + p CB ± C. 73
1+30 = W.S.	RT.			462.35 462.35 + p CB ± C. 10
1+15 = Sew. LAT # 14	RT.	463.24 E 456.50 C 6.74		P.L. 463.24 457.00 C 6.24
0+00 = E. Line MILLAR				
B.M.	DIV. Elev. PO.		462.45 = SLY X Rem MH Stewart + Millar	462.45

SEW. & WATER LAT'S - HOBART ST.
MILLAR to 63rd

18

2+24 = W.S. RT. 459.45 to cost

2+15 = Sew. LAT #13 RT. E 451.14 P.L. 454.00

1+80 = W. Service RT. 460.15 to cost

1+65 = Sew LAT #12 RT. E 450.79 P.L. 454.00

0+00 = E. Line MILLAR ST.

STEWART & CB GRADES

(WLY) MILLAR to 63' rd
RT.

(Sly RT)

RT.

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
		463.10		463.58		3+00	463.25	463.31		463.44	463.40
		461.81		462.03			462.71	462.71		462.87	462.87
0+75		C1.29		C1.53			C0.34	C0.60		C0.57	C0.53
						2+75		463.01		463.79	
								462.61		462.77	
0+50	463.08	463.06		463.49	463.49			C0.40		C1.02	
	461.71	461.71		461.94	461.94						
	C1.37	C1.35		C1.55	C1.55	2+50	462.96	462.90		463.04	462.81
							462.51	462.51		462.68	462.68
0+38	463.13	463.09		463.50	463.57		C0.45	C0.39		C0.36	C0.13
	461.65	461.65		461.90	461.90						
	C1.48	C1.44		C1.60	C1.67	2+25		463.06		463.12	
								462.41		462.58	
								C0.65		C0.54	
= 0+23		462.96		463.17		2+00	462.81	462.86		463.63	463.53
F.C. (on Stewart)		461.60		461.84			462.31	462.31		462.49	462.49
		C1.36		C1.33			C0.50	C0.55		C1.14	C1.04
# 3		463.14		463.11		1+75		462.90		463.54	
		461.56		461.80				462.21		462.70	
		C1.58		C1.31				C0.69		C1.14	
# 2		462.96		463.05		1+50	462.96	463.01		462.95	463.04
		461.52		461.75			462.11	462.11		462.31	462.31
		C1.44		C1.30			C0.85	C0.90		C0.64	C0.73
# 1		462.95		463.12		1+25		463.09		463.08	
		461.46		461.82				462.01		462.22	
		C1.49		C1.30				C1.08		C0.86	
BC (on Millar)		462.50		463.17		1+00	462.90	462.94		463.53	463.51
		461.39		461.88			461.91	461.91		462.12	462.12
		C1.11		C1.29			C0.99	C1.03		C1.41	C1.39
(also = E. Line Millar)	462.62										
	461.57										
	C1.05										

Set T.B.M. chx on drive 61' swly M.H. = 458.91

B.M. Dir. Elev. Rod:

457.33 = sly chx rim M.H. Millar Y. HOBART

4838 millar

CB GRADES - STEWART.

STA	4 ^T P.L.	CB.	E	CB	RT.	P.L.	STA	LT	P.L.	CB.	E	CB.	RT.	P.L.
5400	463.06 462.98 C 0.08	462.83 462.78 F 0.15		462.95 463.10 F 0.15	463.03 463.10 F 0.07		6+46.18 = CB. BC LT.			463.02 462.69 C 0.33				
4475		462.84 463.03 F 0.19		462.88 463.15 F 0.27	463.15		6+43.15 = CB. BC RT.					463.12 462.81 C 0.31		
4453 F.V.C	463.04 463.08 F 0.04	463.19 463.08 C 0.11		462.77 463.20 F 0.43	462.87 463.20 F 0.33		W. Line 63rd (P.L. 94.500)	462.91 462.68 C 0.23					462.90 462.80 C 0.10	
4433		463.02 463.09 F 0.07		462.85 463.21 F 0.36			6+31.18 = gr. BK (Beg. Cur. 9077) LT.			463.13 462.72 C 0.41				
4413	462.96 463.11 F 0.15	462.88 463.11 F 0.23		462.96 463.23 F 0.27	462.99 463.23 F 0.24		6+28.15 = gr. BK (Beg. Cur. 9077) RT.					483.30 462.84 C 0.46		
3493		462.77 463.08 F 0.31		462.91 463.20 F 0.29			6+25			462.98 462.75 C 0.25		462.85 (cut)		
3473 B.V.C	463.34 463.01 C 0.33	463.28 463.01 C 0.27		463.02 463.13 F 0.11	463.13		6+00	462.70 462.78 F 0.08	462.79 462.78 C 0.01			463.26 462.90 C 0.36	463.30 462.90 C 0.40	
3450	462.97 462.91 C 0.06	462.92 462.91 C 0.01		463.48 463.06 C 0.42	463.57 463.06 C 0.51		5+75			462.61 462.83 F 0.22		463.21 462.95 C 0.26		
3425		462.86 462.81 C 0.05		463.61 462.96 C 0.65			5+50	462.55 462.88 F 0.33	462.55 462.88 F 0.33			462.98 463.00 F 0.02	463.03 463.00 C 0.03	
							5+25			462.76 462.93 F 0.17		462.75 463.05 F 0.30		

STEWART ST. - C.B. GRADES

STA.	HT. P.L.	CB	Σ	RT. CB	P.L.
------	-------------	----	---	-----------	------

F.C. (on 63rd)	463.03			463.11	
	462.67			462.81	
	00.36			00.30	

mid. PT CB. Ref's:	462.68			463.07	
				462.80	
				00.29	

MILLAR ST. - G.B. GRADES

HOBART to Rose

(LH)
LT(RH)
RT

STA.	P.L.	CB.	±	CB.	P.L.	STA.	P.L.	CB.	±	CB.	P.L.
1+34.30 = BVC	461.94 460.96 C 0.98	462.01 460.96 C 1.05		459.61 460.56 F 0.95	460.91 460.56 C 0.35						
1+17.30		461.26 460.79 C 0.47		460.26 460.40 F 0.14		3+10.36 = END CON. POINT LT.	463.45 461.96 C 1.49	463.46 461.96 C 1.50		461.72 461.59 C 0.13	461.90 461.59 C 0.31
0+94.30	460.39 460.49 F 0.10	460.46 460.49 F 0.03		460.03 460.15 F 0.12	460.08 460.15 F 0.07	2+95.36 = CB (S-EAST) LT.		463.17 461.88 C 1.29		461.27 461.50 F 0.23	
0+74.30		460.02 460.06 F 0.04		458.92 459.80 F 0.88		2+72.36 = S. LINE STEWART RT ONLY				461.35 461.35 grade	461.34 461.35 F 0.01
0+54.30 = B.V.C.	460.16 459.52 C 0.64	460.08 459.52 C 0.56		459.06 459.35 F 0.29	459.07 459.35 F 0.28	2+52.36 RT only				462.00 461.24 C 0.76	461.27
0+27.15		459.30 458.77 C 0.53		458.55 458.68 F 0.13		2+32.36 = N. LINE STEWART (RT ONLY)				461.78 461.13 C 0.65	461.91 461.17 C 0.78
0+18.50 (and con.) QUIT.		459.25 458.50 C 0.75				2+09.36 = CB (N.EAST) LT.		462.50 461.39 C 1.11		461.82 461.00 C 0.82	461.00
0+03.5 = CB LT.		458.69 458.04 C 0.65				1+94.36 Beg. CON. POINT LT.		462.13 461.31 C 0.82		461.57 460.90 C 0.67	460.90
(0+00 = S. Line HOBART)	457.67 457.83 F 0.18			457.26 458.02 F 0.76	457.19 458.02 F 0.83	1+75	462.29 461.19 C 1.10	462.60 461.19 C 1.41		461.27 460.80 C 0.47	461.28 460.80 C 0.48
0-18 (RT. ONLY)				457.54 457.58 F 0.04		1+50		462.32 461.05 C 1.27		460.11 460.65 F 0.54	460.65

B.M.

Dir. Elev. Rod.

457.33 = SLY CK X ON

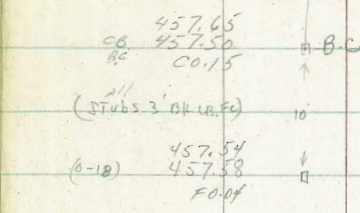
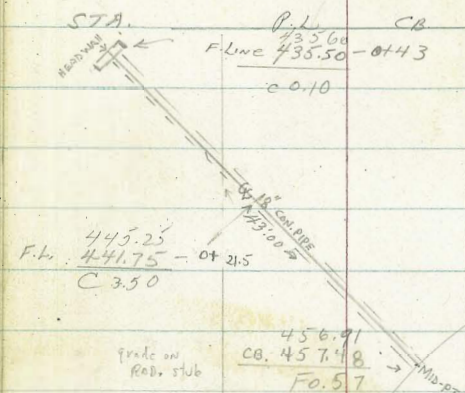
Rim M.H.
HOBART - MILLAR

MILLAR ST.

LT.				RT.				LT.				RT.				
STA.	P.L.	CB.	E.	CB.	P.L.	STA.	P.L.	CB.	E.	CB.	P.L.	STA.	P.L.	CB.	E.	
5+00 (RT. only)				462.75												
(4+84.30 = N. Line) Rose	463.47 462.85 C 0.54			462.68	462.55 462.68 F 0.17											
4+80.38 = CB Bc LT (N. EAST) RT.		463.86 462.93 C 0.93		462.36 = Rod 462.65 = gage F 0.29												
4+75	462.89	464.00 462.89 C 1.11		462.37 462.59 F 0.22		(5+18.70 = S. Line) Rose									462.96 462.87 C 0.09	
4+50	464.20 462.75 C 1.45	464.13 462.75 C 1.38		462.07 462.43 F 0.36	462.21 462.43 F 0.22											
4+25	462.61	463.92 462.61 C 1.31		462.39 462.28 C 0.11		F.C. (N. Rose) S. West.								462.11 462.89 F 0.88		
4+00	463.47 462.46 C 1.01	463.61 462.46 C 1.15		461.80 462.13 F 0.33	461.82 462.13 F 0.31	mid. PT.								462.02 462.90 F 0.88		
3+75	462.32	463.22 462.32 C 0.90		462.03 461.98 C 0.05	462.98	5+05.70 = CB Bc RT. (S. West)								461.86 462.81 F 0.95		
3+50	463.15 462.18 C 0.97	463.09 462.18 C 0.91		461.70 461.83 F 0.13	461.75 461.83 F 0.08	EC (Rose ST) N. EAST.								463.97 462.99 C 0.98		
3+25	462.05	463.54 462.05 C 1.49		461.99 461.60 C 0.31		mid. PT. (N. EAST.)								462.66		

HOBART ST. C.B. GRADES
MILLAR to 63' RD

LT.				RT.			
STA.	P.L.	CB	PL	STA.	P.L.	CB	PL
	F. Line 435.50	-0+43					
	c 0.10			0+75	458.07 458.35	458.94 458.43	
					Fo. 2p	458.51 458.49	
				0+50	455.10 458.12	457.98 458.26	459.84 458.26
					F 3.02	Fo. 14	C 1.76 458.29
					Stub (5' ex PL)		C 1.58
				0+25	457.64 457.87	459.22 458.09	
					Fo. 25	C 1.13	
				0+18.5		458.96 458.05	ok 458.05
						C 0.91	
				0+05 (LT only)	458.06 457.70		
					C 0.36		
				= 0+03.5		458.17 457.94	
						C 0.23	
				E.C. (on HOBART)			
				MID-PT.		458.44 457.96	
						C 0.48	
				CB BC (on MILLAR)		458.69 458.04	
						C 0.65	
				S.K. Reto			
				0+00 (LT only) ON CB GRADES	451.60 457.64	457.88 457.64	
					F 6.04	C 0.24	
					Stub (9' ex PL)		



N.W. Reto

0+40 LT only
(N.W. corner)
(rough grade)
Stub 29' ex PL

(0+00 - F.L. MILLAR)

(#4838 MILLAR)
SET T.B.M. = 458.91 on ch x in Drive 61' S'Wly M.H.

B.M. DIR. Elev. Rod: 457.33 = sly ch x Rim M.H. HOBART
9 MILLAR

Note: CB Grade based on sly line
HOBART opp. 10.00
ON 10' x 10' AS
Per office.

HOBART ST. CB GRADES

	P.L.	CB.	Q	CB.	P.L.		P.L.	CB.	Q	CB.	P.L.
# 3 EXIST CB (Pembroke)		460.10 meet									
# 2		460.26 459.99 C0.27				4+25				461.60 460.95 C0.65	
# 1 (N.W. Ret Pembroke)		461.42 459.88 C1.54				4+00				461.25 460.78 C0.47	461.23 460.78 C0.45
2+40 (2+35.9) CB, BC, LT.	461.31 459.78 C1.53	461.33 459.78 C1.55		460.63 459.53 C1.10 459.78 C0.85	459.53	3+75				461.36 460.61 C0.75	
2+25		461.17 459.68 C1.49		460.56 459.45 C1.13 459.66 C0.90		3+54.49 (app. CB) (Ec. LT.)				461.36 460.47 C0.89	etc
2+00	461.06 459.46 C1.60	461.07 459.46 C1.61		460.17 459.26 C0.91 459.46 C0.71	460.19 459.26 C0.93	3+50			461.11 460.44 C0.67		
1+75		461.01 459.24 C1.77		459.94 459.10 F0.86 459.27 F0.33		3+25			461.15 460.22 C0.93 460.29 C0.86		
1+50	460.13 459.02 C1.11	460.25 459.02 C1.23		457.96 458.94 F0.98 459.07 F1.11	457.19 458.94 F1.75	3+00			460.84 460.02 C0.82 460.14 C0.70	460.80 460.02 C0.78	
1+25		458.43 458.80 F0.37		456.80 458.77 F1.97 458.88 F2.08		2+75			460.65 459.81 C0.84 459.99 C0.66		
1+00	447.10 458.57 F11.47 STUB (17) BK (prop)	458.35 458.57 F0.22		458.17 458.60 F0.43 458.68 F0.51	457.55 458.60 F1.05	2+50 (CB'S ON RT. ONLY)			460.66 459.61 C1.05 459.84 C0.82	460.45 459.61 C1.84	

HOBART ST: CB. Grades

STA.	P.L.	CB.	±	CB.	P.L.	STA.	P.L.	CB.	±	CB.	P.L.
F.C. (on 63rd)				462.90 461.99 C 0.91							
# 2				462.85 461.96 C 0.89							
# 1				462.74 461.93 C 0.81							
5+62.92 = CB. BC RT. (S.W. Corner #08ART-63rd)				462.72 461.90 C 0.82							
5+50				462.94 461.81 C 1.13	462.89 461.81 C 1.08						
5+25				462.70 461.63 C 1.07							
5+00				462.50 461.47 C 1.03	462.56 461.47 C 1.09						
4+75				462.13 461.30 C 0.83							
4+50				462.13 461.13 C 1.00	461.92 461.13 C 0.79	W.L. 63rd				462.73 461.95 C 0.78	

ROSE ST. CB GRADES
MILLAR to 63rd

Ref: DWG: 10077-4
F.B: 2008.35
: 2226-33-61

STA.	(W) LT			RT (S'LY)		STA.	LT			RT		
	P.L.	CB	±	CB	P.L.		P.L.	CB	±	CB	P.L.	
						2175		465.06 464.72 C 0.34		465.11 464.75 C 0.36		
1400	465.10 463.95 C 1.15	465.42 463.95 C 1.47		455.58 464.09 C 1.49	465.63 464.09 1.54							
0+75		465.39 463.70 C 1.69		465.42 463.87 C 1.55		2150	464.82	465.48 464.82 C 0.66		465.41 464.84 C 0.57		
0+50	464.74 463.45 C 1.29	464.69 463.45 C 1.24		464.96 463.66 C 1.30	464.97 463.66 C 1.31	2+45 = E.V.C.	465.99 464.84 C 0.65	465.56 464.84 C 0.72		465.36 464.86 C 0.50	465.47 464.86 C 0.61	
0+25		464.51 463.20 C 1.31		463.80 463.44 C 0.36		2+25		465.87 464.90 C 0.97		465.76 464.90 C 0.86		
0+05	463.00	463.00		463.65 463.27 C 0.38	463.27	2+05	466.44 464.87 C 1.57	466.31 464.87 C 1.44		465.29 464.88 C 0.41	465.53 464.88 C 0.65	
0+04.33 = C.O.E.C. (N.E. Ret.)		463.97 462.99 C 0.98				1+85		466.03 464.78 C 1.25		466.03 464.80 C 1.23		
0+00				462.77 463.23 F 0.46	462.18 463.23 F 1.05	1+65 = B.V.C.	465.93 464.60 C 1.33	466.04 464.60 C 1.44		465.96 464.66 C 1.30	466.04 464.66 C 1.38	
0-27.73 R.F. = CB, E.C. (S. West Ret.)				462.11 462.99 F 0.88		1+50	465.95 464.45 C 1.50	466.15 464.45 C 1.70		465.52 464.53 C 0.99	465.94 464.53 C 1.41	
(0+00 = E.L. MILLAR)						1+25		465.84 464.20 C 1.64		465.93 464.31 C 1.62		
<p>458.91 = T.B.M. = S'WLY (# 4838 MILLAR) Chx on Drive - 61.00' From M.H. B.M. DIR. Elev. Ad: 457.33 sky chx on Rim M.H. HOBART & MILLAR</p>												

ROSE ST. C.D. GRADES

STA.	LT.				RT.				STA.	LT.				RT.
	P.L.	CA	E	CB	P.L.	CA	E	P.L.		P.L.	CA	E	CB	
5700	464.16 463.85 C0.31	463.35 463.85 F0.50		464.76 463.96 C0.80	464.97 463.96 C1.01									
4775		464.30 463.95 C0.35		464.74 464.05 C0.69					EC + 15 SLY ON 63rd = END CB + 90TT.				464.20 463.79 C0.41	
4750	464.50 464.07 C0.46	464.52 464.04 C0.48		464.88 464.14 C0.74	464.81 464.17 C0.67				EC (ON 63rd)				463.99 463.74 C0.25	
4725		464.34 464.14 C0.20		464.67 464.22 C0.45					Mid-pt. RT				464.14 463.73 C0.41	
4700	464.18 464.27 F0.06	464.17 464.24 F0.07		464.64 464.31 C0.33	464.81 464.31 C0.50				5+59.77 = CB EC RT. (S.W.L.) Ret.				463.49 463.74 F0.25	
3775		464.34 464.34 Grade		465.17 464.40 C0.77					W/LINE 63rd (Prop. L. grades)	463.95 463.53 C0.40			464.22 463.73 C0.49	
3750	464.51 464.73 C0.08	464.56 464.43 C0.13		464.59 464.50 C0.09	464.60 464.50 C0.10				5+51.38 = B.V.K. RT. (809 90TT.) ET	463.84 463.63 C0.21				
3725		464.68 464.53 C0.15		464.54 464.58 F0.04					5750	463.91 463.64 C0.27	463.89 463.64 C0.25		464.25 463.77 C0.48	
3700	464.91 464.63 C0.28	464.90 464.63 C0.27		465.12 464.66 C0.46	465.21 464.66 C0.55				5746 (5744.97) = B.V.K. RT. (809. 90TT.)				464.33 463.79 C0.54	
									5725		463.93 463.75 C0.18		463.82 463.86 F0.04	

W/LY LINE 63' rd : CB. GRADES
N. line Rose to STEWART

STA.	P.L.	CB.	E	CB.	P.L.	STA.	P.L.	CB.	E	CB.	P.L.
1+25		463.59 463.14 CO.45									
1+00		463.53 463.22 CO.31									
0+75		463.78 463.30 CO.48									
0+50	replaced 463.25 463.38 Fo. 13	463.50 463.38 CO.20									
0+25		463.89 463.46 CO.43									
0+19.92 = Brk (end con. gvt)		463.92 463.48 CO.44									
0+04.92 = C.B. EC on 63' rd (N.W. Ret)		463.89 463.53 CO.34									
0+00 = N. Line Rose											

(For STEWART to HOBART see Pg 31)

2+31.78 = E.C.
OF S.W. Ret
STEWART ST.

2+24.56 = F.C.

2+16.78 = Beg gvt.

2+14.36 =
mid-pt.
curve

2+04.16 = B.C.

2+00

1+75

-1+50

463.11
462.81
CO.30

463.09
462.83
CO.26

462.86
462.96
462.86
CO.10

463.21
462.89
CO.32

463.28
462.90
CO.38

463.49
462.98
CO.51

463.52
463.06
CO.46

TBM = 458.91 = ch x on drive - 61' S'ly M.H.
#4838 MILLAR
B.M. Dir. Elev. Pos. 457.33 = S'ly ch x
Rim M.H. HOBART
& MILLAR

WLY/63rd - GB. GRADES
N.L. STEWART TO HOBART

STA.	P.L.	CB.	Σ	CO.	P.L.	STA.	P.L.	CB.	Σ	CO.	P.L.
1+00	Rest 461.74 462.39 F. 65	^{100000 out} 462.47 462.39 CO. 08									
0+75		462.62 462.46 CO. 16									
0+50		462.62 462.54 CO. 08									
0+25		462.99 462.61 CO. 38									
0+18.72 = F.C.		462.87 462.63 CO. 24				2+30.96 = F.C. S.W. Rest HOBART.		462.90 461.79 CO. 77			
0+13.06 = mid pt		462.59 462.64 F. 03				2+25		462.83 462.81 CO. 82			
0+07.4 = B.C. (Curva H. B.S.)		462.99 462.66 CO. 33				2+00		462.64 462.89 CO. 55			
0+03.9 = F.C. (N.W. Rest Stewart + 63rd)		463.03 462.67 CO. 36				1+75		462.72 462.76 CO. 56			
0+00 = N. Line STEWART						1+50	Rest 462.46 462.24 CO. 22	Knocked out 462.78 462.04 CO. 04			
						1+25		462.53 462.31 CO. 22			

B.M.: (See Precod. Pg.)

Sly/CB. (1055')

CATOGTIN DR. (Choctaw to E.C. CATOGTIN)

(N41) LT.

(S41) RT.

STA

P.L.

CB

E

CB

P.L.

(EXIST)

(EXIST)

(Mount ex. CB)

1705.05 = E.C.
(CATOGTIN)

chk 462.91

462.92

mount

0+86.19 = mid-pt.

463.06

462.96

C0.10

0+67.34 = B.C.
(63rd)

463.13

463.00

C0.13

0+46.72

463.19

463.05

C0.14

0+26.11 = E.C.
(63rd)

463.33

463.11

C0.22

mid-pt.
0+13.05

463.46

463.27

C0.19

(N.E. RT.
Choctaw 463rd)

0+00 = B.C.

chk: 463.44

463.43

mount

(0+00 = B.C. Choctaw)

B.M.

Dir. Elev. Rod:

= T.B.M.

458.91 (see B.M. Pg 30)

Clark
Shepard
Brown
Civil
12-7-53
No. 62289

SEWER:
KEMPER ST. V PORTION OF
P.L. 242 (MIDWAY)

INDEXED
JUL 13 1954

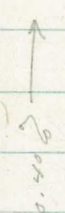
Ref F.B. # 2215-59

STA:

Elev. Fl. Line

DWG: 10108-L

STA.	Elev. Fl. Line			
1475	2.20 -2.15 C 4.35	3+75		2.64 -1.35 C 3.99
1450	2.23 -2.25 C 4.48	3+50		2.62 -1.45 C 4.07
1425	2.33 -2.35 C 4.68	3+25		2.34 -1.55 C 3.89
1400	2.45 -2.45 C 4.90	3+12.99 = M.H. #2 = 84'25" RT.	Stubs set 5.44' RT ON SPLIT	2.17 -1.62 EXIT C 3.79
0+75	2.56 -2.55 C 5.11	3+00		2.17 -1.65 C 3.82
0+50	2.64 -2.65 C 5.29	2+75		2.23 -1.75 C 3.98
0+25	2.70 Rd -2.75 SL C 5.45	2+50		2.22 -1.85 C 4.07
0+00 - EXIST. M.H. (approx. (Call No. 7611))	463' N'ELY OF MIDWAY DR. ON S'ELY LINE KEMPER ST.	(Meet.) -2.85 = F. Line 2+25		2.17 -1.95 C 4.12
		2+00		2.24 -2.05 C 4.29



(Stubs set 4' RT E)

B.M.

6.81 = N.W.B.P. TRAFFIC ISLAND MIDWAY DR
N.W. PT. LOMA BLVD.

KEMPER-MIDWAY SEWER (CONT.)

STA.	Elev.	FL. LINE	STA.	Elev.	FL. LINE
5+75	1.79 -0.55 C 2.34				
5+50	1.92 -0.65 C 2.57				
5+25	2.07 -0.75 C 2.82				
5+00	2.24 -0.85 C 3.09				
4+85.40 = M.H. #1 = P.O.T.	2.55 -0.91 = FL. LINE C 3.46				
4+75	2.50 -0.95 C 3.45				
4+50	2.48 -1.05 C 3.53	chk	(2x2 2172.41 FB# 2215.59)	2.38 = 2.38	
4+25	2.63 -1.15 C 3.78	6x10.40 = D. END (Plug)		1.90 -0.41 C 2.31	FL. LINE
4+00	2.59 -1.25 C 3.84	6+00		1.97 -0.45 C 2.42	

0.402
↑

Clark
Shepherd
Brunow
O'Neil
12-10-53
WFO.2111

STORM-DRAIN - 544L + PIVOTTE DR
TO 52nd ST & HANIMAN DR.
EASEMENT (Public RIGHTS OF WAY) WESTWOOD
HILLS #19 CLEARVIEW MANOR - Pg 38

INDEXED
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STA.		Elev's		STA	Elev's
					249.45 241.58 C 7.87
				2175	
CURB- INLET-GRADES	CB. 7.5'LT	258.40	258.38 TPCB	258.59	
	GUTT	257.57	257.55 GUTT	257.76 GUT	250.77 242.42 C 8.35
				2+55.45 = B.C Δ = 36° 52' 30" LT	
0+72.40 = G. INLET S. EAST. RT 544L + Pivotte	(= GFD B.P.K.)	259.32 250.36 = FL C 8.96		2+27.75	252.83 243.61 C 9.22
				2+00	255.27 244.80 C 10.47
0+50		258.00 250.83 C 7.17			
				1+04.84 = E.C	256.73 245.46 C 11.27
0+25		258.18 258.14 257.33 C 6.81 C 6.85	knocked out + replaced		
stubs set 5' RT & E				1+73.06 = B.C Δ = 15° LT	257.60 245.98 C 11.62
0+00.77 = CB. Fd INLET (N. E. RT 544L + Pivotte)	TPCB 7.5'LT	259.18 250.80	259.05 258.75 TPCB C 0.30	259.08 258.80 TPCB 7.5' RT C 0.28	1+50
	GUTT	259.18 257.97 C 1.21	259.05 257.92 GUTT C 1.13	259.08 257.97 GUTT C 1.11	
				1+25	258.03 248.06 C 9.97
OR CB. + (0+00 = G. Inlet N.E. CORN.) 544L + Pivotte		259.05 257.83 = FL C 7.22		1+00	257.85 249.15 C 8.70

B.M.

Dir. Elev. Rod.

258.08 = B.P. N. 1/4 END ISLAND
S. EAST. 544L + Pivotte

H 339 5

STORM DRAIN (cont.)

STA	Elev's	STA.	elev's
4+75	243.30 234.52 C 8.78	6+72.50 = E.C. (26.82)	237.45 228.59 C 8.86
4+58.18 = E.C.	243.59 235.03 C 8.56	6+45.68 (26.82)	238.51 229.40 C 9.11
4+50	243.76 235.27 C 8.49	6+20.68 (25") arcs	239.48 230.15 C 9.33
4+25	244.22 236.03 C 8.19	5+95.68 (18.11)	240.47 230.90 C 9.57
4+00	244.78 236.78 C 8.00	5+77.27 = B.C. $\Delta = 38^\circ 59' 30''$ RT.	241.13 231.45 C 9.68
3+75	245.46 237.53 C 7.93	5+68.87 = E.C.	241.43 231.70 C 9.73
3+53.21 = Cleanout #1 (= 0+00 ON EASEMENT LINE) Page 38	245.70 238.20 F.I. Box C 7.50	5+35.30	242.26 232.41 C 9.85
3+25	247.02 239.42 C 7.60	5+11.74 (22.36) arcs	242.60 233.12 C 9.48
3+00	248.11 240.50 C 7.61	4+98.18 = B.C. $\Delta = 90^\circ$	242.85 233.83 C 9.02

301.8

= 9' rd B.V.R.

453.2

STORM DRAIN (CONT)

STA.		Elev's	STA.	Elev's
8+42.50 = ξ Cleanout #2	= grid B'k	231.48 226.20 C 5.28	10+61.57 = B.C. $\Delta = 40^\circ$ RT.	226.86 222.54 C 4.32
8+25		231.98 226.32 C 5.66	11+31	227.14 222.77 C 4.37
8+00		232.84 226.49 C 6.35	10+00.54 = E.C.	227.46 223.00 C 4.46
7+75		233.76 226.66 C 7.10	= mid-pt. 9+86.58 (Line only)	
7+50	↑ C 6.88	234.63 226.83 C 7.80	= grid B'k 9+72.61 = B.C. $\Delta = 5^\circ$ Lt.	227.90 223.20 FL C 4.70
7+37.50 = Grid B'k	↑	235.09 226.91 FL C 8.18	9+50	228.20 223.72 C 4.48
7+25	↑ Nat. Curve	235.63 227.08 C 8.55	9+25	228.88 224.30 C 4.58
7+12.50 = Grid B'k	↓	235.99 227.38 FL C 8.61	9+00	227.87 229.57 227.90 C 1.67
7+00	↑ 3.01%	236.44 227.76 C 8.68	8+75	230.47 225.44 230.47 225.50 C 4.97

STORM-DRAIN (CONT.)

EASEMENT (Public-Rights-of-Way) WESTWOOD HILLS #1 & CLEARVIEW MANOR

STA	Elev's	STA	Elev's
		2+00	249.41 246.81 C 2.60
		1+83.06 = E.C	250.25 246.08 C 4.17
		1+55.20 = B.C A = 70° 56' 18" RT	251.91 244.88 C 6.93
		1+25	248.96 243.58 C 5.38
		1+00	247.77 242.50 C 5.27
		0+75 = grid mark	247.25 241.43 C 5.82
		0+50	246.58 240.82 C 5.76
		0+25	246.01 240.21 C 5.80
10+94.14 = Ely Edge inlet N.W. 1/4 ANIMIAN 4 52' rd	222.30 = F.L. Inlet	5 stubs 545' 4 E	245.70 239.60 = F.L. C 6.10 Nly Pipe
10+76.93 = E.C	226.72 222.43 C 4.29	0+00 = 3+53.21 SCOUROUT = 1 Drott Edr. Page 36	245.70 238.20 = F.L. C 7.50 Box

↑
43.0

↑
2.44 B

B.M. Div. Elev. Rod: (See pg 35)

STORM-DRAIN
(EASEMENT:) (CONT)

STA.

Elev's

AK

252.25 = INVERT EX. Pipe

TP. Box = $\frac{259.60}{259.51}$
C 0.09

3 + 24.87 = E. CLEANOUT } $\frac{259.60}{252.20}$ FL Box 252.28 = EL Pipe NELY
C 7.40

3+00 $\frac{253.54}{251.13}$
C 2.41

2+75.21 = EC $\frac{250.94}{250.05}$
C 0.89

2+48.63 = B.C $\frac{249.10}{248.91}$
C 0.19
z = 67° 41' LT.

2+25 $\frac{248.53}{247.89}$
C 0.64

↑
3/8
↓

Clark
Shepherd
Brvier
Oweil
1-19-54
W/O. 20488

Storm-DRAIN - BLK 34
FAIRMOUNT ADDIT. LOTS 37438

P.O.F. DIVE. 5866-0
F.O. P 1720-35

INDEXED
JER
JUL 13 1954

40

CHK. F.LINE EXIST 36" Con. Pipe at 4846
(F.O. 1720-35-39) 331.89

0+79.41 = END CONST

331.66
327.30 = F.L.
C 2.36

0+55.41

332.01 | 332.01
328.99 | 328.81
C 3.20

0+31.41 = E.C.

13/8 →

330.61 | 330.61
328.68 | 328.33
C 2.28

0+15.70

(stubs set B.I.C.)

331.37 | 331.37
328.47 | 328.01
C 3.36

$\Delta = 20^\circ$
 $R = 90$

END
0+00 = EX Pipe (30" Con.)
(on curve)

{ to F. CURVE: $\Delta = 30^\circ$
 $R = 90$ }

328.26 = F.L., EXIST. (PLAN) : ACTUAL F.L. = 327.70 ! Grades changed to meet EXIST. F.L. LINE

B.M. DIR. EKV. RD.

332.95 = S.E. B.P.
ORANGE V 494 L

EXTENSION - STORM DRAIN

Clark
Shepherd
Bruner
Owens
1-27-54

W.D. 20556

LOT 21 - LEMON VILLA
(54 ST. W. UNIV. AVE.)

REF. F.B. 1697-30

DWG: 4496-B

STA:

Elev. F.I. LINE

CHK

325.15 = 325.15 = 2x2 (1400) F.B. 1697-31

1+06.24 - END CONST

326.17
323.2 F.I. LINE
C 2.97

0+86.24

324.59
322.1
C 2.49

0+66.24

323.69
321.00
C 2.69

0+46.24

(STUBS 6" 8" RIG)

322.92
319.90
C 3.02

0+26.24 - END EXIST. 18" CON. PIPE

chk: 318.81
318.80 - F.I. LINE EX. PIPE

B.M. (Dir. Elev. Rod)

310.02 = N.W. B.P.

54th & University

SEWER EXT. FROM 30.5' SLY OF NLY LINE
P.L. 1345 to 120.5' SLY, IN E 40%.

Clark
Shepherd
Survey
ONCE
2-2-54
MO. 20009

REF. T.S. 418

STA.

Elev's

INDEXED
JUL 13 1954

CHK:

32.87 = 32.87 = F.L. EX. M.H.

0+90.5 END CONST.



53.64
41.97 F.L. END
C 11.67

0+60

51.47
40.47
C 11.00

0+30

(Stubs set 5' RT G.)

48.57
38.97
C 9.60

0+00

CHK:
EXIST. D.END
(90' sly m.H.)



37.47 = F.L. EX. D.END

B.M. DIT. Elev. Rod:

32.87 = F.L. OF EXIST. M.H. 90' N'LY OF EXIST. D.END. (AT 0+00)

STORM-DRAIN EXT. SEA BREEZE
+ LAUDER (S.W. LAUDER)

Clark
Shepherd
Gruber
Owens
2-2-54
W.O. 21195

REF: 5142-B
No F.O'S

STA.

Elev. (F. Line)

INDEXED
JER
JUL 13 1954

Chk.

241.99 = 241.95 (See B.M.)

0+24 = END CONST. + FC. HEADWALL Elev. = 231.89
Elev. = 226.36 = F. Line 24" Con. Pipe
C 7.03 C 5.53

0+100 = END EX. 24" Pipe
E SEA BREEZE

chks: 225.31 Mt. F. line
225.28 = FL END EX. 24" Pipe Conc.

B.M. DIM. ELEV. POS:

241.95 = S.W. B.P. SEA BREEZE +
CUMBERLAND

Clark
Shepherd
Bryner
Dne.L
2-10-54
W.O. 21149

SEWER - 54th ST
KRENNING, S'ly 261+

REF: FB # 286-66
DWG: 2210-D

STA.

Elev's

STA.

Elev's - F.LINE

1+75

268.00
259.27
C 8.73

1+50

267.31
259.02
C 8.29

1+25

266.50
258.77
C 7.73

1+00

265.82
258.52
C 7.30

chk.

274.52 - 274.41 - LAD
E 54th + N 1/4
Line Olive
FB 286-67

0+75

265.02
258.27
C 6.75

2+60.90 = D. END

272.29
260.13 FL
C 12.16

0+50

264.32
258.02
C 6.30

2+56.90 = M.H #2

271.91
260.09 FL
C 11.82

0+25

(STUBS set 5' R.F.G.)

263.66
257.77
C 5.89

SEW. LAT #1 - BT.

2+40.90

LAT. Elev. 260.23
C 10.42

270.65
259.93 - 2' elev. error
C 10.72

LAT. 270.60
Elev. Prop. 260.43
C 10.22

- M.H #1

0+00

PT. INTERSECTION
E. EXIST 8" IC
SEWER - KRENNING ST.
W. LINE 20' E'ly of Proposed
W. LY - Prop. Line 54th St
(60' W'ly EXIST 54th ST)

263.26
257.52
C 5.74
(Approx)
F.LINE
MH #1

2+25

270.17
259.77
C 10.40

2+00

268.73
259.52
C 9.21

B.M. SW. Elev. Rod.

305.43 = Ch D N. CB.
Ret. Redwood & Chollas. STA. RD.

Clark
Shepherd
Bruner
O'Neil
2-22-54
W.O. 21149

IMP'S NLY 54th ST.
Sly of KRENNING ST.

NLY ISLAND - WLY 54th

REF. F. 2186-66
DNG: 2210-D

STA. P. GRADE Ely CB NLY CB R. GRADE

NLY CB Line 54th (Sly HAZELWOOD HTS #1)

(Cont. 946)

STA.	CO.	P.L.						
				1457.37 = B.C. wly.co			270.39 269.78 C 0.61	270.30 269.78 C 0.52
				1444.61	269.57 269.80 F 0.23	269.70 269.80 F 0.10	269.70 269.44 C 0.26	269.57 269.44 C 0.13
1450	271.03 270.84 C 0.19	271.89 270.84 C 1.05		1424.61	269.14 269.27 F 0.13	269.14 269.27 F 0.13	269.14 268.89 C 0.25	
				1404.61	268.15 268.75 F 0.60	268.27 268.75 F 0.48	268.27 268.35 F 0.08	268.15 268.35 F 0.20
1425	269.92 270.16 F 0.24			1484.61	268.25 268.30 F 0.05	268.25 268.30 F 0.05	268.25 267.81 C 0.44	
				1464.61	267.92 267.85 C 0.07	268.01 267.85 C 0.16	268.01 267.27 C 0.74	267.92 267.27 C 0.65
1400	269.29 269.49 F 0.20	268.85 269.49 F 0.64		1444.61	266.80 267.45 F 0.65	266.93 267.45 F 0.52	266.93 266.70 C 0.23	266.80 266.70 C 0.10
1475	267.97 268.80 F 0.83			1424.61	266.49 267.05 F 0.56	266.61 267.05 F 0.44	266.61 266.35 C 0.26	266.49 266.35 C 0.14
1450	267.86 268.12 F 0.26	267.35 268.12 F 0.77		1404.25 = 4.25' RABBT.	265.02 266.50 F 1.48	265.15 266.50 F 1.35	265.15 266.20 F 1.05	265.02 266.20 F 1.18
1425	267.22 267.44 F 0.22						265.15 266.25 F 1.10	
1400 = NLY LINE Sly Prop. Sly Line HAZELWOOD HTS UNIT #1		CHK: 266.78 266.77						

305.43 = Chk □ N. CB. bet. Redwood & Charles STA. Rd

NLY ISLAND

STA.	R. Grade	Ely CB	Wly CB	R. Grade
------	----------	--------	--------	----------

1475.28 =	271.02 270.58 CO. 44	271.15 270.58 CO. 57	271.15 270.40 CO. 75	271.02 270.40 CO. 62
mid pt Wly CB only			270.81 270.18 CO. 63	270.18

Sly ISLAND

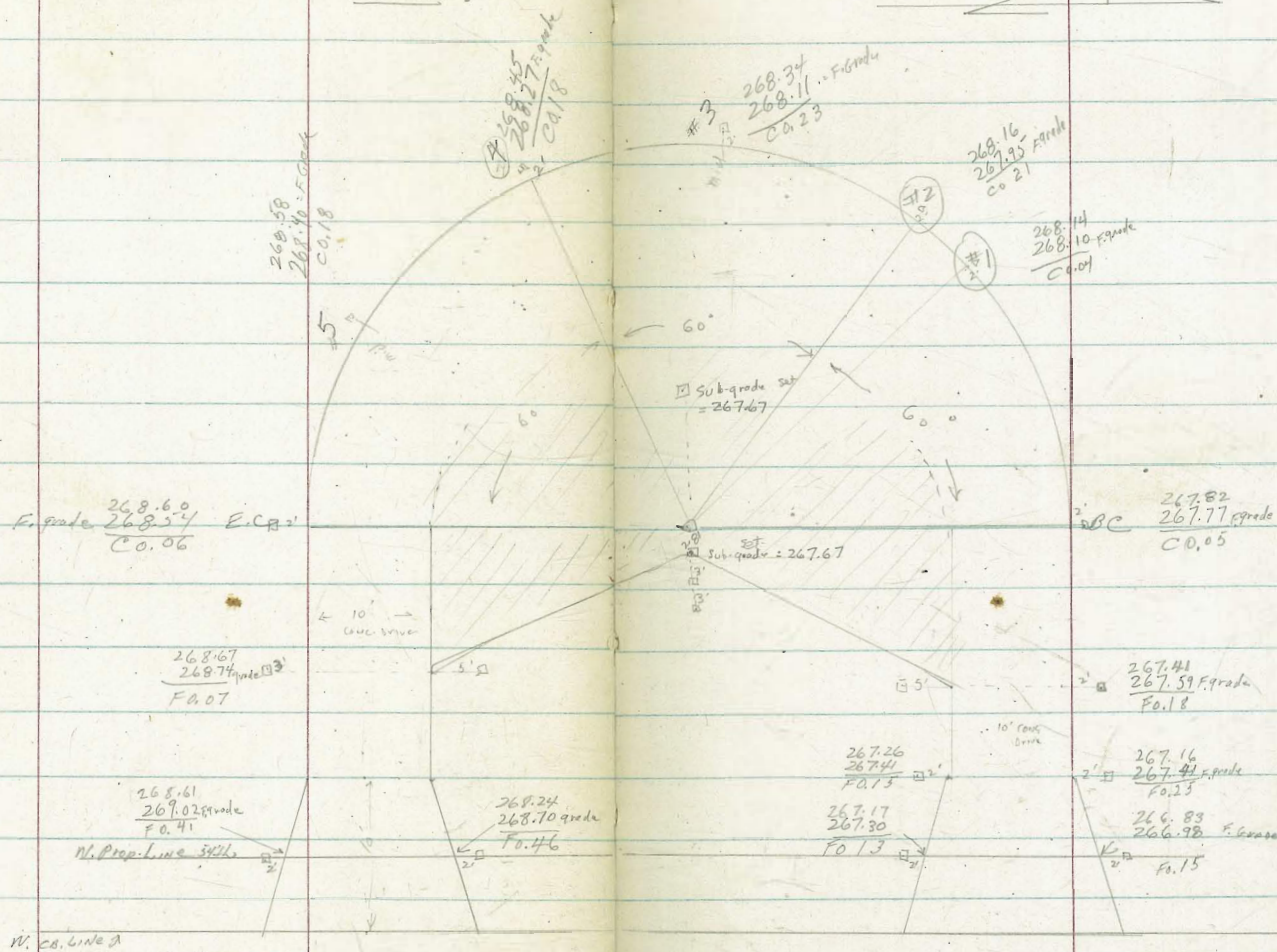
Ely CB	LINE	Wly Prop. Line (R. grades)
--------	------	----------------------------

2400 = END CB	278.19 278.02 CO. 17	277.67 278.02 FO. 35
1475	277.12 277.20 FO. 08	277.20
1450	276.51 276.38 CO. 13	276.17 276.38 FO. 21
1425	275.75 275.56 CO. 19	275.56
1400	274.95 274.74 CO. 21	275.85 274.74 CO. 11
0+77.11 = Wly Line olive - Proj	274.10 273.95 CO. 15 272.63 273.18 FO. 55	273.83 273.95 FO. 12
0+73.66 (end grade only)		272.99
0+25	272.39 272.47 FO. 08 272.09 272.04 CO. 05	273.15 272.04 CO. 11
0+10.25 = 10.25 RAD. PT. = CB BC Ely CB. - mid pt	272.04 272.90 CO. 14 272.88 271.88 CO. 00	271.90 = mid pt. 272.88 271.88 CO. 00
0+00 = NLY END OF Sly ISLAND = Sly Line City Prop. Projected		

54 1/2 ST. SWY KRANNING

PARKING AREA - CITY PROP.
(FIRE STATION)

47



Clark
Sheppard
Bruner
ONEIL

2-25-54
N.O. 32150

ALLEY BIK 2 - ALHAMBRA PK.

N+ SOUTH ALLEY

Ref: F.O. 2172-12 & 2228-12
DN: 16573-6

INDEXED
JUL 13 1954

STA.	(E.L.) LT.	(W.L.) RT.	STA.	LT.	RT.
2+10	381.12 380.12 C 1.00	381.37 379.88 C 1.49	(3+85 = E. E. Walky)		377.00 Set. m. 11 etc.
1+80	382.80 380.92 C 1.88	381.86 380.74 C 1.12	3+75 = N-Line EXN Alley	377.27	(See Pg 49) 377.27
1+50	383.37 381.73 C 1.64	382.92 381.59 C 1.33	mid-pt. Rd. Prop (to Road)	377.33	
1+20	383.71 382.55 C 1.16	384.03 382.44 C 1.59	3+65 = B.C. LT.	377.12 377.40 Fo. 28	376.25 377.10 Fo. 85 376.25 377.30 F 1.05
0+90	383.83 383.37 C 0.46	383.80 383.29 C 0.51	3+42.5	378.27 377.63 C 0.64	376.36 377.47 F 1.11
0+60	384.51 384.19 C 0.32	384.20 384.14 C 0.06	3+20 = E.V.C.	378.61 377.85 C 0.76	377.32 377.64 F 0.32
0+30	385.48 385.08 C 0.48	384.25 384.98 F 0.73	3+00	378.26 378.07 C 0.19	377.16 377.82 F 0.66
0+10	385.84 385.83	385.83 385.84	2+80	378.22 378.38 F 0.16	377.82 378.12 F 0.30
0+10 = S. Line MONROE: (Most EXIST. PAR.)			2+60	378.98 378.79 C 0.19	378.55 378.52 C 0.03
Note: Par. width = 17.50' (0.25' exception even. side only)			2+40 = B.V.C.	379.20 379.28 F 0.08	378.77 379.03 F 0.26
B.M. Dir. Elev. Rod.		374.58 = N.E.	7' x 4' Lit Fl. CH. STAN. 152 AND		

ALLEY BR 2 - ALHAMBRA PK.

E + WEST ALLEY

STA	(WV) LT.	E	(SW) RT.	STA	LT.	RT.
1465	377.99 377.62 C 2.37		378.74 377.92 C 0.82			
1455	^{Prn} (10' RAD) = E.C. LT. B.V.C. LT. 377.88 377.27 Co. 61		376.66 377.67 F 1.01	2170.11	chk 385.01 N. LINE CROSS ON 384.99	chk: 385.04 385.02
1445	B.V.C K. Line		376.44 377.44 F 1.00	2160	385.23 384.65 Co. 58	385.10 384.89 Co. 21
1435	E.E. N+S ALLEY	375.85 377.00 F 1.15		2150	384.81 384.26 Co. 55	384.58 384.56 Co. 02
1425	W. Line N+S ALLEY O.D. LT.	377.58 377.27 Co. 31	375.18 377.48 F 2.22	2140	384.25 383.71 Co. 54	384.03 384.01 Co. 02
0492.5	375.54 377.21 F 1.67		374.53 377.37 F 2.81	2130	383.55 382.94 Co. 61	383.25 383.24 Co. 01
0460	377.10 377.15 Fo. 05	376.78	374.88 377.28 F 2.40	2107.50	382.51 380.95 C 1.56	381.84 381.25 Co. 59
0425	377.32 377.06 Co. 26	(L. and W. S. 21) 376.68	375.50 376.98 F 1.48 376.26 376.68 Fo. 42	1485	381.49 378.96 C 2.53	379.75 379.26 Co. 49
0400	(Beg. 6' CB on RT) E. Line 52' W	377.00	376.60 377.10 Fo. 41	1475	380.73 378.19 C 2.54	379.87 378.49 C 1.38

↑
V. LINE CB
At 0-09

B.M.

See B.M. Pg 48

Clark
Shepherd
Bruner
Oweil
2-25-54
W.O. 32150

IMPOS. ALLEY BIK - 7 ALHAMBRA FR.
N.H.S. ALLEY

REF: 2172-12
2228-12
DWG 10513-L

INDEXED
SER
JUL 13 1954

LT.

RT.

STA.	(W/O) LT.	Σ	RT. (E4)		LT.	RT.
2+00	387.89 388.16 Fo.27		388.39 388.16 Co.23	3170	388.66 387.53 Co.113	387.37 386.88 Co.49
1+80 = B.V.C	388.09 388.00 Co.09		388.15 388.00 Co.15	3+60 = B.V.C, RT only	388.14 387.66 Co.48	387.26 387.34 Fo.08
1+50	388.12 387.70 Co.42		388.36 387.70 Co.66	3+50 RT only		387.31 387.63 Fo.32
1+20	387.84 387.39 Co.45		388.18 387.39 Co.79	3+40 = B.V.C, RT only	388.28 387.77 Co.51	387.31 387.77 Fo.46
0+90	387.44 387.09 Co.35		387.58 387.09 Co.49	3+132	387.88 387.91 Fo.03	387.68 387.91 Fo.23
0+60	387.61 386.78 Co.83		387.89 386.78 Co.111	2+86.66	388.02 388.05 Fo.03	388.58 388.05 Co.53
0+40 Σ only - (not set)		(STB. drop Σ) 386.17				
0+30	386.57 386.47 Co.10		387.13 386.47 Co.66	2+60 = E.V.C	388.04 388.19 Fo.15	388.91 388.19 Co.72
0+20 Σ only		386.56 386.08 Co.48				
0+00 = N. LINE MONROE	chk: 386.16 386.15		chk: 386.19 386.17	2+40	388.13 388.24 Fo.11	388.03 388.24 Fo.21
Note: PAR-19.50 (0.25' EXCEPTION) E/W LINES				2+20	388.45 388.24 Co.21	387.71 388.24 Fo.53
B.M.			386.82 = S.W.B.P. E1 CAJON 51ST.			

86F: 5246-B

51A

ALLEY BIK 7 - (CONT.)
N+S

SEWER EXT. N+S ALLEY BIK 2 - ALHAMBRA PK

STA. LT. E RT.

STA. LT. E (Elev's) RT.

STA.	LT.	E	RT.
4106 ± = PL LT.	dx: 386.02 386.00		
4100	388.62 386.54 C 2.08		
3790	388.60 386.99 C 1.61		
3780 MT.	388.65		
3781 ± = PL RT.	387.31 C 1.34	dx: 386.23 386.25	

LAT 75 on LT.
382.54
376.46
C 6.08 PL

1+15 = D.END

381.21
375.96
C 5.25

1+10 = Sewer LT
#4 on RT.

375.83 E

0+95 = S. LAT #3
ON LT.

381.73
376.57
C 6.14 P.L.

383.30
376.03
C 7.27 P.L.

0+90

381.94
375.25
C 6.69

0+73 = Sewer LT #2
on RT.

374.76

381.42
374.96
C 6.46

0+60 = S. LAT #1 on LT.

380.62
374.38
C 6.04

379.58
374.38
C 5.20

0+30

stubs set 5' T.G.

378.92
373.51
C 5.41

EXIST.

0+00 = D.END

378.90

(110' NLY of NLY LINE
E-W ALLEY BIK 2)

372.64 = F.W. EX. DE
6.26 (AS PER PLAN)

MT. EXPOSED

B.M.

374.58 = NET 7' x 4'
LT EL. CANTON + 52nd

Clark
 Shephard
 Bruner
 Oneib
 2-25-54
 W.O. 2/1/90

STORM DRAIN BIR 52
 CARR'S Subdiv. (27th & MKT.)
 REF: DWG 5150-B
 F.B. 2237-43

STA. elev's

CHK F.L. EXIST 24" RCP 81'53 OFF 7 S LAND AVE = 102.92

(= 0+98.53 DWG)
 0+63.49 = END JOB
 107.21
 104.29
 C 2.92

0+45.49
 104.88
 104.54
 C 0.34

0+27.49 = EC
 105.08
 104.79
 C 0.29

0+13.74 - mid. pt.
 T=149'
 Δ=35°
 = B.C.
 107.97
 104.98
 C 2.99

0+00 = EXIST. 24" Con Pipe
 (= 1162.02 DWG)
 CHK 105.19
 105.17 F.L. EX.

B.M. Dkt. Elev. Rod. 143.11 = S.E.C.P. ISLAND 43746

Clark
Shepherd
Graney
Oneik
3-3-54
W.O. 21042

(8")
WATER-Line : HUGHES ST.
2278' WLY OF WLY LINE
REDWOOD VILLAGE #8

2100

471.34
465.74
C 5.60

1+75

471.64
465.78
C 3.86

1+50

471.63
465.83
C 5.80

1+25

471.57
465.87
C 5.70

1+00

471.30
465.92
C 5.38

0+75

471.00
465.96
C 5.04

0+50

470.87
466.08
C 4.79

0+25

470.70
466.05
C 4.65

#2278 - FND Job.

471.05
465.7
C 5.35

2+25

0+00 = RE. 20' NLY - SLY Line (MAKE CORRECT!) 466.10 (EXIST?)
HUGHES & WLY LINE
REDWOOD VILLAGE #8

Pipe Not Exposed
& No elev given on plans

Q.M. DIV. Elev. Rod.

470.64 = SPIKE Pole NLY Sub. Line - end HUGHES

Clark
Shepherd
Brown
O'Neil
3-17-54

IMP'S: HUGHES ST.
S'Wly REDWOOD VILLAGE #8

W.D. 21042

Ref: FB# 2139-36
DWG: 10306-L

STA	P.L.	CB	♀	CB	P.L.	STA	P.L.	CB	♀	CB	P.L.
1+04.09	470.59 470.74 Fo.15	471.00 470.74 Co.26		470.39 470.74 Fo.35	471.21 470.74 Co.47	2+40.17	469.93 470.07 Fo.14	470.77 470.07 Co.70		469.68 470.07 Fo.39	472.30 470.07 C 2.23
0+87.09	470.89 470.48 Co.41	470.98 470.48 Co.50		469.77 470.48 Fo.71	471.01 470.48 Co.53	2+26.59- BC	469.69 470.36 Fo.67	470.86 470.36 Co.50		469.97 470.36 Fo.39	472.44 470.36 C 2.08
0+64.09	470.11 470.14 Fo.03	470.78 470.14 Co.64		469.80 470.14 Fo.34	471.16 470.14 C 1.02	2+20.17	470.50	471.02 470.50 Co.52		470.15 470.50 Fo.35	470.50
0+44.09	469.72 (Not set)	469.85 469.72 Co.13		(Not set) 469.72 (Not)	470.82 469.72 C 1.10	2+00.17	469.70 470.81 F 1.11	471.30 470.81 Co.49		470.32 470.81 Fo.49	472.70 470.81 C 1.89
0+40.40 = Wly sub-line			469.62			1+80.17	470.99	471.41 470.99 Co.42		470.41 470.99 Fo.58	470.99
0+24.09	469.20 (Not set)	469.24 469.20 Co.04		470.62 469.20 C 1.42	470.32 469.20 C 1.12	1+70.17 = E.C	469.67 471.02 F 1.35	471.40 471.02 Co.38		470.49 471.02 Fo.53	472.60 471.02 C 1.58
0+04.09	468.60	468.68 468.60 Co.08		468.76 468.60 Co.16	468.60	1+60.17	469.68 471.06 F 1.38	471.41 471.06 Co.35		470.51 471.06 Fo.55	472.77 471.06 C 1.71
(E STATIONS)											
0+00 = BC	468.44 chks 468.46		468.46	Not	468.46	1+40.17	469.83 471.00 F 1.17	471.00		470.47 471.00 Fo.53	472.35 471.00 C 1.35
22.91 Ely 94 P. INT Wly Line Redwood Village #8 Wly Line HUGHES ST											
						1+24.09	470.28 470.90 Fo.62	470.90		470.47 470.90 Fo.43	471.45 470.90 Co.55

B.M. (Dr. Elev. Ref.)

470.64 = SPIKE IN N'ly Pole
(FB 2139.37) Wly Line R. Village #8
& Wly Line HUGHES
Set Bm chx 33 Ely/Wly Line Redwood Village #8 on Nly/Co.
HUGHES = 468.41.

HUGHES ST. (Drives)

STA.	P.L.	CB.	£	CB.	P.L.
S'ELY- DRIVEWAY LT.				N'WLY DRIVEWAY RT.	
o.B.B.C		471.51 470.98 C0.53		469.43 469.81 F0.38	ca. o.c
CB.E.C		471.51 471.02 C0.49		469.43 469.85 F0.42	Knocked-out CB.E.C
prop	469.88 471.18 F 1.30			470.85 470.01 C0.84	prop. 470.01
Prop	470.27 471.93 F0.76			470.22 469.57 C0.65	prop 469.57
CB.E.C		471.29 470.87 C0.42		469.87 469.41 C0.46	CB.E.C
CB.B.C		471.29 470.83 C0.46		469.87 469.37 C0.50	CB.B.C
CHK:					
	LT.			RT.	
2170.22 = END CONST.	470.07 469.20 C0.87	469.45 469.20 F0.25		468.72 469.20 F0.48	471.94 469.20 C 2.74
2160.17	470.13 469.51 C0.62	470.42 469.51 C0.91		469.00 469.51 F0.51	472.17 469.51 C 2.66

Knocked-out
 sub at 4 ft
 2' B.P. on line with Prop slab (2' run drive at Pitline)

468.98
469.41
F0.43
E.C

468.98
469.37
F0.39
CB.B.C N.W.L.Y

Clark
Sheppard
O'Neil
3-25-54
W.O. 32250

Temp's SANTA ISABEL
ENCINO to OLVERA

(W4) LT

REF: DWG: 10977-L : 10978-L
F.B. 2262-5

(E STATION NS)
STA

LT. (W4) E
P.L. CB

STA P.L. CB E

1245.57

192.35 188.66
188.92 188.92
C 3.43 F0.26

3+25.57

181.33
181.91
F0.58
182.15
181.91
C0.24

1425.57

193.26 190.39
190.15 190.15
C 3.11 C0.24

3+05.57

182.58
182.58
C0.01

1+10.07 = B.C.
Δ = 45° 24' 30" RT
E R = 175'

193.68 191.37
191.36 191.36
C 2.32 C0.01

190.67

2+85.57

183.34
183.42
F0.08
183.64
183.42
C0.22

1+05.57 - ARK

191.66 191.62
191.66 191.66
F0.04

2+71.75 = B.L. BE
(SIN ON FHE) RT

183.82
183.82
C0.03

0+75

194.83 194.19
194.14 194.14
C0.69 C0.05

2+48.76 = F.C.

184.90
184.48
C0.42
184.45
184.48
F0.03
184.04

0+50

196.38 196.01
196.17 196.17
C0.21 F0.16

2+25.57

182.54
183.42
C2.12
183.07
183.42
F0.35

6+25

198.27 197.85
198.20 198.20
C0.07 F0.35

2+02.49

189.35
186.39
C 2.96
185.50
186.39
F0.89

0+00 = S.W. by Prop. 200.19
LINE B.C.
ENCINO + SANTA
ISABEL

chk 200.19 (West)
200.23 200.23

1+79.41

190.58
187.37
C 3.21
186.53
187.37
F0.84

B.M.

DIT. Elev. Rod:

183.40 = N.W. B.P
SAN JACINTO + SAN BERN ARDO
PI

1+65.57

190.52
187.93
C 2.57
187.36
187.93
F0.59
187.35

SANTA ISABEL

LT. (wly)

PL PL B

(wly) LT.

STA P.L. CB E

4485.57 96'	167.81	167.79 167.81 Fo.02		6+85.57	163.08 156.60 C 6.48	156.49 156.60 156.71 156.87 Fo. 9.6 157.90 157.77 C 0.13	
4475.96 = B.C. $\Delta = 53^\circ 50' 30''$ ER = 85'	170.61 168.48 C 2.13	168.31 168.48 Fo. 17	4R 167.64 167.60				
4465.57 10.19'	169.25	169.25 169.22 169.25 Fo. 0.3		6+45.57 14.73	166.12 158.90 C 7.22	159.16 158.90 C 0.26	158.66
4445.57 20'	173.33 170.90 C 2.43	171.31 171.24 170.90 C 0.34 C 0.41		6+30.84	159.72		159.85 159.72 C 0.13
4425.57 30'	172.78	172.95 172.78 C 0.17	172.30	6+05.84	168.17 161.09 C 7.08		160.92 161.09 Fo 17
3495.57 20'	177.31 176.07 C 1.24	175.70 176.07 Fo. 37		5+80.84	162.47	2 dx plants	162.12 162.47 Fo. 35
3465.57 1382'	178.89 178.75 C 0.14	178.81 178.75 C 0.06		5+55.84 = E.C. 25.14	169.24 163.84 C 5.40	163.44 163.84 Fo. 40	163.23
3451.75 = PL & RT (S.M. OFFICE)	180.05	180.14 180.05 C 0.09	179.69	5+30.70 25.13	168.30 165.22 C 3.08	165.07 165.22 Fo. 15	
3445.57 6.18'	180.60	180.69 180.60 C 0.09		5+05.57 20'	168.46 166.60 C 1.86	166.64 166.60 C 0.04	165.83

(Wb) LT.

P.L

CA

COTT.

C

= CB, EC, LT,
#3

151.54

150.97

II. 2

152.02
151.87
C.13152.02
151.27
C0.75

1

152.28
152.23
C0.05152.28
151.65
C0.637+52.64 = CB, BC
III. LT.
(over)154.10
152.63
C1.47152.96
152.63
C0.33152.96
152.13
C0.83

7+41.06

153.25

153.71
153.25
C0.467+33.38 = PL, BC, LT.
(over)

153.70

154.19
153.70
C0.49

7+24.48

= PL, BC, RT
(over)159.06
157.25
C4.81154.37
154.25
C0.12

154.68

7+05.02

155.32
155.42155.32
155.42
F0.10

Clark
Shepherd
Brumer
O'Neil
3-26-54
N.O. 21164

STORM DRAIN & CB INLET
"N'ELY" MKT & 47th
Ref: DWG: 10359 AA-L

STA

Elev's

[Meet Pst. Elev. TP. Cleanout]

0+37.5 S Type F. Cleanout (Meet F. Line)
+ S EXIST 36" R.C.P. - (EXIST. 36" Pipe with Box - Cleanout)
121.67
116.00 = F. Line 18" Pipe
C 5.67

0+18.5 (not set) 117.09

F. Line 18" Pipe & Inlet 122.11 (on Pst. MAIL 6.5 w/ly Cleanout)
118.17
C 3.94

GUTTER Elev (Grate) = 122.11 rd
121.17 curb
C 0.94

TP. CB Elev = (Meet) 122.00

EXIST.
0+00 = CB. E. N'Wly CB
Return - MARKET
+ 47th

B.M. DIV. Elev. Post: 122.15 TP CB BC
N 24 MKT 47th

Clark
Shepherd
Owner
Dweil
4-16-54
W.O. 20008

SEWER: Beverly
E. Geneva - NLY 1854

R.O.F. DWG: 1538-5
Profile DWG 1542-D

STA.
14.85 = DEND

Elev's:
259.90
251.04
C 8.86

14.75

259.67
251.00
C 8.67

14.50

259.26
250.90
C 8.36

14.25

258.94
250.80
C 8.14

14.00

258.76
250.70
C 8.06

04.75

↑
0.45

258.71
250.60
C 8.11

04.50

258.60
250.50
C 8.10

04.25

stubs set 5' RTG

258.91
250.40
C 8.51

0+00 = EXIST. M.H. E. Geneva & Beverly
(= M.H. #24 DWG 1538-D)

250.30

(meet)

= F. Line Elev

259.11
250.30 Ref grade
C 9.81

B.M.

250.30 = F. Line EXIST.

#24
M.H. E. Geneva & Beverly

Clay
Shepherd
Gruber
D'Neil
4-16-54
W.O. 62353

CB'S: LINDO PASEO - LOTS 11-12 - BIK 13
College PK #2

Ref: FB# 2152-63
DWG # 5189-B
MAP # 2218-2

ALLEY BIK I (College PK #2)

(WLY) 4T

PT (Ely)

INDEXED
JUL 13 1954

STA

elev's.

CHK

449.85 = 449.83 (See B.M.)

S

1+27.50 450.13 450.20 449.97 ENT 450.20
(= NLY Line Lot 12) 449.78 450.13
Co. 42 Co. 07

1+03.75 450.25 450.25 449.99 ENT 450.25
449.90 450.25
Co. 35 grade

0+80 450.37 450.22 449.90 ENT 450.22
= E.V.C. 450.02 450.22 450.37
Co. 20 450.12 F0.15
Co. 10

CB.EC
(= N. 10.5 SLY of N. Line Lindo Paseo
of on WLY Line Alley BIK I)

450.60
450.63
F0.03

0+60 450.44 450.14 449.98 ENT 450.14
450.09 450.14 450.44
Co. 05 F0.05 F0.30

0+36.5 = CB. B.C.
CB. R. 45'

450.45
450.63
F0.18

0+40 450.47 450.27 449.99 ENT 450.21
450.12 450.22 450.47
Co. 09 F0.01 F0.26

0+18.25

450.27
450.74
F0.44

(STUBS set 3' BK CAFE)

0+20 450.46 450.19 450.12 ENT 450.19
450.05 450.12 450.46
Co. 14 450.17 F0.27
Co. 02

0+00 = Pt. 7.5' Ely of Prolongation
of WLY Line Lot 11

450.77 chk.
450.78 (most EXIST)
CB

0+00 = N. Line
LINDO PASEO
Ely of Alley BIK I
0-05 4T only

450.47 450.40 450.12 ENT 450.40
450.00 450.12 ENT 450.40

B.M.

Dir. E/W Rd

449.83 = N.E. B.P
MONTZUMM +
College

450.38

INDEXED
JUL 13 1954

Ref: FB 2199-68

LT

Clark
Shepherd
Byrner
O'Neil
5-11-54
W.O. 32310

CB GRADES 68th ST
AMHERST TO EL CATON

STA.	Prop.	CB	E	RT (Ely)	Prop	CB	E	Prop
					2+50	455.49 455.80 F0.33		455.86 455.85 C0.01
1+25		453.28 453.30 F0.02		453.51 453.30 C0.21	2+25	455.21 455.30 F0.09		455.30 455.34 F0.04
1+00		452.84 452.80 C0.04		452.78 452.80 C0.18	2+00	454.87 454.80 C0.07		454.90 454.82 C0.08
0+75		452.36 452.30 C0.06		452.77 452.30 C0.47	1+72.07 Alley B.C.	454.16 454.24 F0.08		454.37 454.24 C0.13
0+50		451.79 451.80 F0.01		451.81 451.80 C0.01	1+70.07 Alley E.C.	454.16 454.24 F0.08		454.37 454.24 C0.13
0+25		451.63 451.30 C0.33		451.17 451.30 F0.13	Alley at Prop (Wly)	454.78 454.41 C0.37		454.42 454.41 C0.51
0+10 = C.B. B.C.		450.81 451.00 F0.19		450.98 451.00 F0.02	Alley at Prop (Sly)	453.88 454.01 F0.13		454.91 454.01 C0.90
# 1		451.07 450.76 C0.31		451.20 450.85 C0.35	Alley E.C. 1+50.07	453.86 453.84 C0.02		453.94 453.84 C0.10
W. Wly Ret.				Wly Ret				
(Case - N. Line) AMHERST					1+48.07 = Alley B.C.	453.86 453.76 C0.10		453.94 453.76 C0.18

NOTE: (Some grades set prior to this date by another party)

B.M. Div. Elev. Rod:

457.40 = S.W.B.P EL CATON + 68th

CB'S - 6876 :- AMHERST to EL. CAJON

INDEXED
 JER
 JUL 13 1954

STA.	PL	LT	CR	4	RT.	CR	P.L.
------	----	----	----	---	-----	----	------

chk:

457.39 = 457.40 (see 6876)

3+10.14 :- S. LINE
 EL CAJON

(met
 21157)

457.04 chk:
 457.00

chk: 457.09
 457.10 (met 21157)

3700

456.67
 456.80
 FO.13

456.73
 456.89
 FO.16

2175

456.03
 456.30
 FO.27

456.35
 456.37
 FO.02

Clark
Shepard
Bruner
Orwell
5-13-54
W.D. 32254.

SHAFTER ST.
BYRON to CARLETON

REF: F.B. # 2140-67
DWG: 10934-L
10935-L

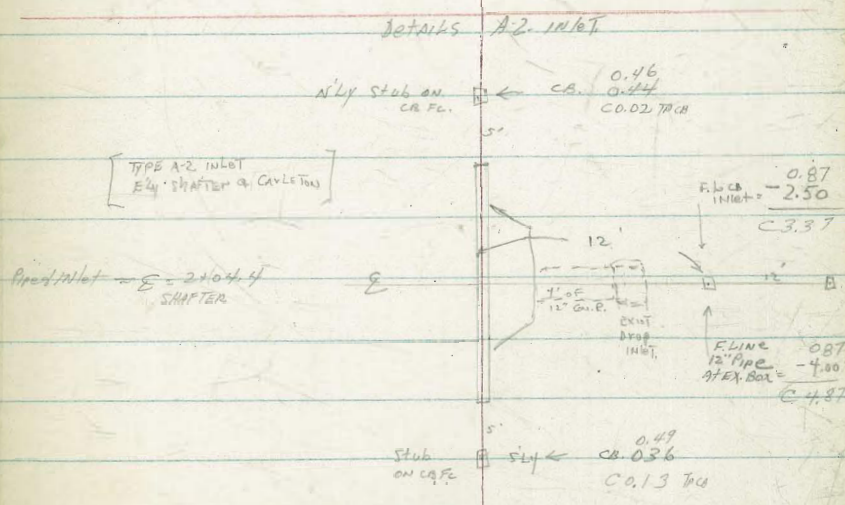
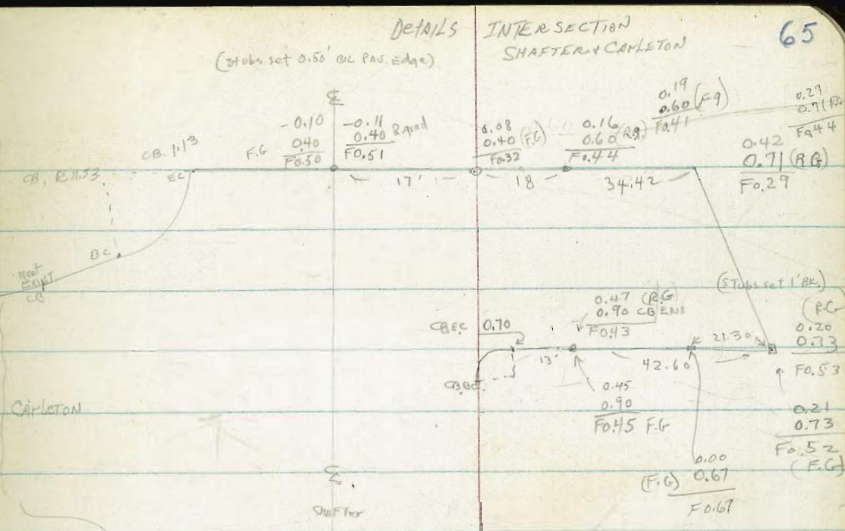
64

STA.	(W/2) LT.		E	RT (E/W)		STA.	P.L.	CB	E	CB	RT	AL
	P.L.	CB		CB	AL							
0+80 =	SEW. LATE #1 on LT	P.L. 2.10 -3.59 C 5.69	E 2.10 -4.08 E Saver	CB 6.18	AL	1488.9	RT only				0.46 0.40 Co.06	
0+75		2.02 1.43 Co.59	1.54 1.43 Co.11	1.00 0.73 Co.27	1.36 0.73 Co.63		(meet EXIST.) #2 BEG. CONC. GUTT. LT. Δ = 59° 27' 05" Dist. 27' 13' 32"			1.01		
0+50		1.50	1.51 1.50 Co.01	1.02 0.80 Co.22	0.80		#1 Δ = 27' 13' 32" Dist. 13' 36' 46"			1.05		
0+25 =	CB B.C.	2.04 1.57 Co.47	1.71 1.57 Co.14	0.90 0.87 Co.03	1.53 0.87 Co.66							
#1 Δ = 10°			1.65 1.60 Co.05	0.84 0.70 Fo.06		1475 =	CB B.C. LT.	1.13		0.88 1.13 Fo.25	0.58 0.43 Co.15	1.60 0.43 C.1.17
#2 Δ = 36°			1.76 1.61 Co.15	0.81 0.95 Fo.14								
#3 END CB. Δ = 45° 35' 05"			1.76 1.64 Co.12	1.03 0.97 Co.06		1450		1.21		1.17 1.21 Fo.04	0.79 0.51 Co.28	0.51
						1425		1.28		1.10 1.28 Fo.18	0.79 0.58 Co.21	1.25 0.58 Co.67
							CHK EXIST. MARK LT. Hrs.	1.41 - 1.43				
0+100 = N.Y. Line (BYRON)		1.40 1.65 Fo.25		0.56 0.75 Fo.37		1400		1.35		1.41 1.35 Co.06	1.00 0.65 Co.35	0.65
P.M.	DIR. E/for. RD:			6.33 = 7' C.T.	W/ly CORN.							SCOTT + CARLETON

SHAFTER ST. (Cont)

STA. (W/L) LT. CB. E CB. RT. ELY P.L.

CB.E.C + 55.60 = END PAV RT.			0.73	FIN. PAV
CB.E.C + 13 - END CB. ELY RT 90° TO BK TANG			0.45 0.90 Fo.45	0.90
CB.E.C.			0.48 0.70 Fo.22	0.47 0.70 Fo.23
2+44.5 - CB BC RT [R=5' Δ=90°]			0.41 0.60 Fo.19	0.60
2+19.9 RT only			0.54 0.52 Co.02	
2+09.90 RT only = NLY END INLET			0.44	
2+07.4 = S INLET 48" 12" R.C.P.				
1+98.9 RT only = SLY END A-2 INLET			0.36	



Clark

5-13-54
N.O. 32054

CARLETON ST.
SCOTT to SHAFER

INDEXED

JUL 13 1954
ET. (sev) AL

STA. AL CA E
CHK. To City of 2415 1.28 = 1.28

#2 = R.C. 1.13
0.80
1.13
F0.33

#2 = R.C.
A = 67° 09' 34"
R = 11.53
0.84
1.10
F0.26

#1 = END EX. (Buy STD. C.C.)
CB. LT.
Δ = 20° 50' 36"
WF = 10° 25' 18"
Ch = 1.08

2+75 = EX. CB, B, C LT. 1.80

2+45 = Sewer #2 on RT
Σ Sewer 1.79
3.54
C 5.33
- 1.79
- 3.25 PL
C 5.04

0+25 EXIST. 4.68 4.89 5.22 EXIST.

0+00 = ELEV. LINE SCOTT 5.03 met EXIST.

B.M. 214. Elev. Rod:

6.33 = 7' C.T. Willy Corry SCOTT & Carleton

Ref: F.B. 2140-67
10934-L
10935-L
DWG:

66

CHK

= 0.54 = Ch in
S.W. Corn. Conc. Slab
City Sewer Pump
Sta - Carleton & Shaft

3' Trench
(4' x 4' x 3')

Clark
Shepherd
Owens
5-18-54
W.O. 32170

IMP'S ALLEY BAK 119 UNIV. HTS
Howard Hwy to S.W. E & W ALLEY

Ref: F.B. 2293-1
DWG: 10971-L

STA.

LT.

RT.

STA.

(m) LT.

E

RT (E'ly)

1+75.04 = CLINE EAV.
Ally.

368.44
368.37
C 0.07

367.99

368.58
368.22
C 0.36

1+50

368.44
368.47
F 0.03

369.01
368.31
C 0.70

1+25

369.69
368.57
C 1.12

368.84
368.40
C 0.44

1+00

369.65
368.66
C 0.99

369.72
368.49
C 1.23

0+75

369.62
368.76
C 0.86

369.79
368.59
C 1.20

0+50

369.48
368.85
C 0.63

370.03
368.68
C 1.35

0+25

369.51
368.95
C 0.56

369.77
368.77
C 1.00

(FD 2293-2)

CH: T. B. M.

367.71 - 367.70 = N.W. 7' C.T.
30' 4" + HOWARD

0+00 = N. Line HOWARD

369.04

368.65

369.21
368.86
C 0.35

(Stubs set in REF. to
edge Pav. INTAL)

Note: 0.35 Exception 27' 0" RT
on Pav. - 19.50' to WITH Pav.

B.M. D.V. Elev. Rods.

367.47 = S.F.B. P. HOWARD AVE.
40410 ST.

C/ark
 3/11/54
 5-30-54

CB GRADES Lot #18
 SIERRA VISTA TRACT - MAP #1295
 ON S24 - SAN MIGUEL AVE

Ref: MAP #1295
 Profile sheet #2941

INDEXED
 HER
 JUL 14 1954

STA.	CR. Elev's (S/L)	EX. GUT PAVE.
chk	61.92 = 61.90 = CB on N1/4 San Miguel AT B.C. (+26)	
0+65	66.09 65.99 C0.10	65.32
0+38	65.12 65.26 F0.14	64.56
0+41.50	63.15 63.53 F0.38	62.88
0+25 = B.C. LT. San Miguel	61.71 61.80 F0.09	61.07
0+125 = mid-pt.	59.74 60.11 F0.37	59.44
0+00 = N.E. by Corn Lot 18 Proj. face line of San Miguel	58.41 58.49 F0.08	57.82
B.171	86.15 = N.E. B.P. FRANKLIN + CUYAMACA	

not shown
for EUTZ

Clark
Shepherd
Brunner
Omes
5-24-54
W.O. 21121

REPLACEMENT SEWER
COMMERCIAL ST.
HENSLEY TO 29th

Ref: DWG 2209-D (ALIGNMENT OF SEWER)
Noted 5' NELY AS PER
(No F. Lines)
AL. SAUTIER

Note:

69

STA.	Elev's.	STA.	Elev's
1+50	66.10 60.81 C 5.29	3+75.97 = M.H. #2 NOT. (= Grade over)	67.20 61.37 = F. Line C 5.83
1+25	66.29 60.75 C 5.54	3+50	67.12 61.31 5.81
1+00	66.28 60.69 C 5.59	3+25	67.04 61.25 C 5.79
0+75	66.16 60.62 C 5.54	3+00	66.95 61.19 C 5.76
0+50	65.95 60.56 C 5.39	2+75	66.75 61.12 5.63
0+25	65.86 60.50 C 5.36	2+50	66.50 61.06 C 5.44
0+00 = M.H. #1 Δ = 72 15' LT	65.56 60.44 = F. Line C 5.12	2+25	66.63 61.00 5.63
0-21 = EXIST. M.H. (connect.) HENSLEY	66.30 60.37 = F. Line 12" C 5.93	2+00	67.05 60.94 C 6.11
		1+75	66.18 60.87 C 5.31
B.M. Dir. Elev. Rod:	72.05 = S.W.B.P.	29th & IMPERIAL	

0.25%

0.42%

Stubs at 10' intervals

(Stubs set 5' intervals)

Stubs at 10' intervals

Pipe connect.

JENNER - Commercial ST. (Cont.)

STA.	Elev's.
6000	6839 62.31 6.08
5975	6825 62.21 6.04
5950	6814 62.10 6.04
5925	6802 62.00 6.02
5900	6783 61.89 5.94
4975	6774 61.79 5.95
4950	6776 61.68 6.08
4925	6758 61.58 6.00
4900	6745 61.47 5.98

0.422 ↑

STA.	Elev's
7172.94 = EX. M.H. 2946 ST	63.21 EX. M.H. 63.22 F. LINE
7151.94 = M.H. #3 Δ = 72° 15' LT	68.92 62.95 F.L. 5.97
7125	68.52 62.84 5.68
7100	68.43 62.73 5.70
6975	68.55 62.63 5.92
6950	68.62 62.52 6.10
6925	68.56 62.42 6.14

0.422 ↑

Clark
Shepherd
Brimer
O'Neil
5-25-54
W.O. 3224

IMP'S ALLEY BIK 3 Normal H'TS
ARTHUR to MOUNTAIN VIEW DRIVE

Ref: F.B. 2129
DWG: 11050-L

INDEXED
M & R
DFC 6 1954

STA	LT	RT	STA	RT
1470	397.66 396.88 Co.18	396.97 396.18 Co.09	3450	396.10 396.02 Co.08
1420 = B.V.C	397.36 397.14 Co.22	397.23 397.06 Co.17	3425	396.02 396.12 Co.13
1400	398.55 397.48 Co.07	397.30 397.28 Co.02	3400	396.03 396.21 Co.18
0+80 = E.V.C	398.43 397.82 Co.61	397.86 397.50 Co.30	2175	396.37 396.31 Co.06
0+60	398.20 397.89 Co.31	397.56 397.49 Co.07	2150	396.48 396.41 Co.07
0+40	397.84 397.41 Co.43	397.53 397.03 Co.50	2125	396.10 396.50 Co.40
0+20	397.32 396.39 Co.93	397.22 396.39 Co.83	2100	396.66 396.60 Co.06
0+00 = N.W. LANE ARTHUR	395.34 394.81 Co.53	395.08 394.81 Co.27	1475	396.96 396.70 Co.26
1460 E.V.C	395.11	394.74 Co.42		396.93 396.75 Co.18

Note: Revised Elevation (E.V.C)
 After S.D. & F. Professional
 Study of existing fences and lots

Note: TOTAL AV. WIDTH = 14.50'
 0.25' EXCEPTION ELY N.W. ALIMS
 ALLEY

B.M. DIV. Elev. Rod:

395.11 = N.W. B.P.
 ARTHUR HAWLEY B.M.

ALLEY BK 3 (Cont.)

	LT.		RT.		LT.	RT.
6+00	396.75 395.05 C 1.70		395.67 395.30 C 0.37			
5+75	396.09 395.15 C 0.94		395.89 395.38 C 0.51	395.93 395.38 C 0.55		
5+50	395.85 395.24 C 0.61		395.71 395.47 C 0.24			chk: 394.86 (9-24-54) chk: 394.87 394.87 - EXIST.
5+25	396.02 315.34 C 0.68		395.54 395.55 Fo. 01	395.42 395.55 Fo. 13	7+17.5: CB. END RT.	
5+00	395.85 395.44 C 0.41	395.75 395.44 C 0.31		396.02 395.64 C 0.38	7+15.12: P.L.-F. ALLEY	394.41 - EXIST. PAV.
4+75	395.64 395.53 C 0.11		395.50 395.72 Fo. 22	395.60 395.72 Fo. 12	7+12.96 = CB. END L.P.	chk: 394.51 394.50 - EXIST.
4+50	396.22 395.63 C 0.59		395.77 395.81 Fo. 04		7+00: BAK	396.32 394.66 C 1.67
4+25	396.16 395.73 C 0.43	396.10 395.73 C 0.37		396.33 395.89 C 0.44	6+75	396.32 394.66 C 1.66
4+00	396.60 395.82 C 0.78	396.55 395.82 C 0.73	396.97 395.98 C 0.99	397.10 395.98 C 1.12	6+50	395.32 394.66 C 0.66
3+75	396.60 395.92 C 0.68	396.56 395.92 C 0.64	396.32 396.06 C 0.26	396.38 396.06 C 0.32	6+25	395.91 394.85 C 1.06
						396.28 394.76 C 1.52
						395.19 395.05 C 0.14
						395.21 395.05 C 0.16
						395.33 395.14 C 0.19
						395.28 395.14 C 0.24
						395.64 395.22 C 0.42

Clark
Shepherd
Brunner
Omell
6-7-54
W.O. 31954

INDEXED
SEP
JUL
1954

TMP'S ALLEY BK 50 - OCEAN BEACH
CABLE ST. to SUNSET CLIFFS BLD.

Ref: F.B. # 2266-37
DWG: 11127-L

Note: { 0.25' PATI EXCEPTION } 73
H + RT
Tot. Pav. Width L = 19.50'

STA.	LT.	E	RT.
1+45			28.21 28.45 FO. 24
		E	29.77 28.75 C 1.22
	3+60		29.77 29.42 Co. 35
1+20			28.56 28.35 Co. 21
		E	29.72 28.65 C 1.07
	3+40		29.85 29.24 Co. 61
0+95			28.51 28.25 Co. 26
		E	29.05 28.55 Co. 50
	3+20 = B.V.C.		29.75 29.13 Co. 62
0+70			28.31 28.16 Co. 15
		E	28.76 28.46 Co. 30
	2+95		30.60 29.03 C 1.57
0+45 = E.V.C.			28.00 28.06 FO. 06.
		E	28.63 28.36 Co. 27
	2+70		29.80 28.93 Co. 87
0+40			27.94 27.78 FO. 04
		E	28.61 28.28 Co. 33
	2+45		30.85 28.84 C 2.01
0+30			27.67 27.49 Co. 18
		E	28.52 27.76 Co. 76
	2+20		28.93 28.74 Co. 19
0+20			27.18 26.55 Co. 63
		E	28.01 26.76 C 1.25
	1+95		28.80 28.64 Co. 16
0+15 = B.V.C.			26.84 25.91 Co. 93
		E	26.98 26.08 Co. 90
0+00 = Fly Line Cable			23.82 23.88
		E	23.84 23.86
B.M. Del. Monte			25.11 = S.E. B.P. DEL MONTE + CABLE

4854
Cable Spine Pile 2+75-RT
29.97 = 29.78

STA.	LT	E	RT	STA.	LT	E	RT
5100	32.25 31.59 C0.66		32.07 31.89 C0.20				
4475	32.52 31.18 C1.34		31.76 31.48 C0.28				
4150	31.28 30.77 C0.51		31.80 31.07 C0.73				
4+37.5 = Sew. LAT #2 LT.	FL Pop 30.99 25.56 C5.43	30.99 24.96 C6.03		CHK: 33.03 = 33.03 = TP CB-END			5+99.97 LT F.B. 2266-46
4+25	30.74 30.36 C0.38		31.55 30.66 C0.89				
4+14 = Sew. LAT #3 RT. (Already in)		24.67E	25.47 FL Pop	5+99.97 = W by Line Sunset Cliffs Bldg.	CHK: 32.93 32.93	CHK: 33.00 32.98	
4+12.5 = Sew. LAT #1 LT.	FL Pop 30.53 25.15 C5.38	30.53 24.66 C5.87		5+80 = B/K	34.23 32.90 C1.33		33.50 33.20 C0.30
4400 = F.V.C	30.40 29.95 C0.45		30.36 30.25 C0.11	5+75	36.23 32.81 C3.42		33.20 33.11 C0.09
3180	29.85 29.65 C0.20		29.95 29.95 C0.00	5+50	32.99 32.40 C0.59		32.91 32.70 C0.21
				5+25	32.33 31.99 C0.34		32.33 32.29 C0.04

Clark
Brewer
O'Neil
6-18-54
No. 31649

IMPS WUNDERLIN AVE: 63rd-60th

SEWER & WATER SERVICES

Ref: F.B. 2316
DWG'S: 11024-L
11025-L

75

STA.	(Sly) LT.	RT (Nly)	STA.	LT.	RT.
			14+46 = W.S. LT.		
3+60 = W.S. LT.			13+76 = W.S. LT.		
3+55 = Sew # 8 RT.		272.8 276.00	12+71 = W.S. LT.		
2+80 = Sew # 5 LT.	274.1 273.5		11+80 = Sew # 4 RT.		269.0 271.2
2+60 = W.S. LT.			10+66		
1+80 = Sew # 7 RT.		274.5 275.8	10+88 = Sew # 1 LT. 278.4 277.8		
1+61 = W.S. RT.			(CHANGED TO meet EXIST. FACILITIES)		
0+80 = Sew # 6 LT.	280.7 280.1		10+40 = Sew # 2 LT. 281.9 281.3		
0+60 = W.S. LT.			(NOT STAKED - prop. OWNER does NOT WANT)		
0+00 = Wly Line 63rd			10+30 W.S. LT.		
			7+80 = Sew # 3 RT.		284.0 287.3
			5+50 = Sew # 9 RT.		285.5 286.8
			4+40 = W.S. RT.		

B.M.

274.34 = C.T. @ WUNDERLIN
Wly 10' time 63rd

W 031979
10-7-54

PAY GRADES - Ellison Pl. N. Mt. View Ely.

INDEXED
JER
DEC 7 1954

77

Gutt.
L+

Gutt.
L+

R+
Gutt.

2+29

387.65

2+27

387.31

2+26

387.55

2+10

389.80

389.52

C&G in
Raked Crows Feet

C&G in
Raked Crows Feet

2+46

387.50 stub. 4' BM Edge Ave
287.45 on Prop. Line
00.05

2+42

287.31

CK 388.75
0-05 = Nly Line Mt View 388.75

CK 388.28
388.28

0-16 = Nly Line Mt View
0+00 = NW Cor Ellison + Mt View Dr.
BM Direct Elev. Rd

389.57 = NW B.P.
Ellison Pl. + N. Mt. View

Clarks
Shepherd
0 Mail
6-21-54
W.O. 2mb

477' SIDEWALK (6') N'LY OF ALLEY
BK'1 - W'ly. Side TPA AVE between UPAS
& BROOKES

78

1475

7.37
7.38
FO.01

3+50

6.40
6.32
CO.08

1450

7.63
7.76
FO.13

3+40 Meet EX. Cross walk

6.35 EXIST

1425

8.20
8.14
CO.06

3+25

6.22
6.40
FO.13

1400

8.61
8.52
CO.09

3+00

6.35
6.45
FO.10

0+80 Meet EXIST. Cross-walk

8.81 EXIST

2+75

6.30
6.50
FO.20

0+75

9.10
8.89
CO.21

2+50

6.52
6.55
FO.03

0+50

9.60
9.26
CO.34

2+25

6.64
6.70
FO.06

0+25

9.97
9.63
CO.94

2+00

6.93
6.98
FO.05

0+00 = N'ly Line Alley

2+05 Meet EX. Cross-walk

6.87 EXIST

B.M. assumed elev. TP. CB. at int. of Front edge WALK (13.5' BK W'ly CB 7th) = 10.00
N'ly line Alley

Clark
Shepherd
O'Neil
6-21-54
W.O. 20

1475

1450

1425

4477- EXIST 6' N/S. WALL

4.65 EXIST

1400

4475

4.91
4.62
CO.24

0480 M

4450

5.43
5.38
CO.05

0475

4425

5.94
5.85
CO.09

0450

4415 Int EXIST. Cross WALL

5.98 EXIST

0425

4400

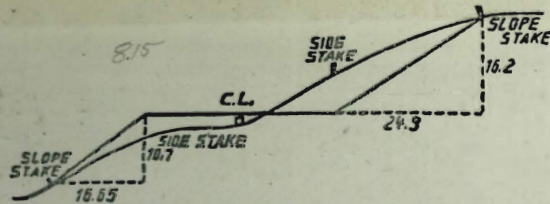
6.10
6.08
CO.02

0400=M

3475

6.27
6.20
CO.07

B.M



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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