

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side of shoulder
stake for any width roadway slope 10 to 1
If ground is nearly level the cut or fill at any

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find tangent and external for curve of
any other degree divide by degree of curve and
add correction found in column of corrections.
Degree of curve which gives may be found
by dividing tangent (or external) by

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

Correct the above curve to wall
by dividing the tangent by wall

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.41	1.51
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.618	.707	.797	.887	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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Kearny Mesa Sewer Stakes

Plan- 2081-D - 4-7-53 7.0

Stakes 8' Lt.

	stake	F.L.	cut
0+00 = Conn.	82.34	74.85 ^{2.34}	7.49
+35	83.59	75.69 ^{3.59}	7.90
+70	84.97	76.53 ^{4.97}	8.44
1+05	85.89	77.37 ^{5.89}	8.52
+40	86.62	78.21 ^{6.62}	8.41
+75	87.24	79.05 ^{7.24}	8.19
2+10	88.62	79.89 ^{8.62}	8.73
+45	89.57	80.73 ^{9.57}	8.84
+80	90.38	81.57 ^{10.38}	8.81
3+23.29 = M.H. 1	91.07	82.61 ^{11.07}	8.46
0+35 T.P.	91.43	83.49 ^{11.43}	7.94
+70	93.11	84.37 ^{13.11}	8.74
1+05	94.28	85.25 ^{14.28}	9.03
+40	95.01	86.13 ^{15.01}	8.88
+75	95.52	87.01 ^{15.52}	8.51
2+10	95.67	87.89 ^{15.67}	7.78

300.29 = Pole Lt. 1+50 - M.H. 1+2

			cut
2+45	96.21	88.77 ^{96.21}	7.44
+80	97.14	89.65 ^{97.14}	7.49
3+15	98.05	90.53 ^{8.05}	7.52
+50.94 = M.H. 2	99.13	91.42 ^{9.13}	7.71
0+35	00.35	92.30 ^{00.35}	8.05
+70	01.12	93.18 ^{01.12}	7.94
1+05	01.97	94.06 ^{1.97}	7.91
+40	02.34	94.94 ^{2.34}	7.40
+75	03.42	95.82 ^{3.42}	7.60
2+10	03.65	96.70 ^{3.65}	6.95
+45	04.09	97.57 ^{4.09}	6.52
+80	04.73	98.45 ^{4.73}	6.28
3+15	05.73	99.33 ^{5.73}	6.40
+50	07.56	300.21 ^{7.56}	7.35
+85 - T.P.	08.44	01.09 ^{8.44}	7.35
4+20	09.44	01.96 ^{9.44}	7.48
+55	10.07	02.84 ^{10.07}	7.23
+95 = M.H. 3	11.34	03.84 ^{11.34}	7.50

B.M. = stab. - 4.4 + 55 324.57

66.37
6.50
59.87

2

0+00 = M.H. 3	03.84	cut.
+35	12.48 ^{2.48} 04.77	7.71
+70	13.50 ^{3.50} 05.69	7.81
1+05	14.22 ^{4.22} 06.62	7.60
+40	14.92 ^{4.92} 07.54	7.38
+75 - T.P.	16.40 ^{16.40} 08.47	7.93
2+10	17.87 ^{7.87} 09.39	8.48
+45	19.16 ^{9.16} 10.32	8.84
+80	19.88 ^{9.88} 11.24	8.64
3+15	20.36 ^{0.36} 12.17	8.19
+50	20.83 ^{0.83} 13.09	7.74
+85	21.08 ^{1.08} 14.02	7.06
4+20	21.69 ^{1.69} 14.94	6.75
+55	22.73 ^{2.73} 15.87	6.86
+90	23.41 ^{3.41} 16.79	6.62
5+15	23.74 ^{3.74} 17.45	6.29
+41.44 = M.H. 4	24.65 ^{4.65} 18.13	6.62
= for walls	39.47 ^{39.47} 28.35	11.12
0+32.04	53.40 ^{53.40} 38.57	14.83
+64.08	59.12 ^{59.12} 48.79	10.33

1+28.16 = M.H. 5	62.98	62.98	C 3.98
0+35	66.87	6.87	59.21
+70	68.98	8.98	59.42
1+05	70.26	70.26	59.63
+40 - T.P.	71.34	71.34	59.84
+75	72.75	72.75	60.05
2+10	72.40	72.40	60.26
+33.72 = Beg. Span	59.87	60.40	9.87
+83.72 = end "	60.64	60.70	9.87
3+18.72	75.00	75.00	60.91
+53.72	74.23	4.23	61.12
+88.22 = M.H. 6	73.87	73.87	61.33
0+35	73.12	73.12	61.54
+70	72.31	72.31	61.75
1+05	71.36	71.36	61.96
+40	70.75	0.75	62.17
+75	76.10	76.10	62.38
2+10	78.90	78.90	62.59
+45	70.85	70.85	62.80

2+80	73.18	63.01	10.17	2+45	83.87	83.87 67.18	16.69
3+15	76.13	63.22	12.91	+80	82.69	82.69 67.39	15.30
+52.84 = M.H. 7	79.02	63.45	15.57	3+15	77.58	77.58 67.60	19.98
0+35	81.43	63.66	17.77	+50	79.69	79.69 67.81	11.88
+70	83.73	63.87	19.86	+85	84.17	84.17 68.02	16.15
1+05	86.26	64.08	22.18	4+20	84.75	84.75 68.23	16.52
+40	87.43	64.29	23.14	+55	84.91	84.91 68.44	16.47
+75	87.58	64.50 ^{7.58}	23.08	+83.52 = M.H. 9	84.05	84.05 68.61	15.44
2+10	87.18	64.71 ^{87.18}	22.47				
+45	86.96	64.92 ^{86.96}	22.04	M.H. # 9	86.96	86.96 68.61	18.35
+80	86.40	65.13 ^{86.40}	21.27	0+45	83.55	83.55 69.06	14.49
3+15	86.07	65.34 ^{86.07}	20.73	1+73	82.48	82.48 70.34	12.14
+50	84.34	65.55 ^{84.34}	18.79				
+77 = M.H. 8	82.20	65.71 ^{82.20}	16.49	2+06.16 = M.H. 10	79.98	79.98 70.67	9.31
0+35	80.57	65.92 ^{80.57}	14.65				
+70	79.46	66.13 ^{79.46}	13.33				
1+05	80.45	66.34 ^{80.45}	14.11				
+40	80.69	66.55 ^{80.69}	14.14				
+75	81.72	66.76 ^{81.72}	14.96				
2+10	82.78	66.97 ^{82.78}	15.81				

$$\frac{86.1}{9.51}$$

$$\frac{12.68}{22.19}$$

$$\frac{8.65}{4.51}$$

				1+75	83.87	^{3.87} 73.26	10.61
			cut.	2+10	85.70	^{85.70} 73.39	12.31
0+00 = M.H. 10	79.86	^{9.86} 70.82	9.04	+45	86.22	^{86.22} 73.52	12.70
+35	79.62	^{9.62} 70.95	8.67	+80	85.75	^{85.75} 73.65	12.10
+70	78.60	^{8.60} 71.09	7.51	3+15	86.52	^{86.52} 73.79	12.73
1+05		71.22		+50	86.42	^{86.42} 73.92	12.50
+40	79.18	^{9.18} 71.35	7.83	+85	86.78	^{86.78} 74.05	12.73
+75	79.77	^{9.77} 71.48	8.29	4+20	87.43	^{87.43} 74.19	13.24
2+10	79.87	^{9.87} 71.62	8.25	+67 = M.H. 12	88.12	^{88.12} 74.37	13.75
+45	79.19	^{9.19} 71.75	7.44	0+35	88.44	^{88.44} 74.50	13.94
+80	79.17	^{9.17} 71.84	7.29	+70	87.22	^{87.22} 74.64	12.58
3+15	79.63	^{9.63} 72.02	7.61	1+05	87.27	^{87.27} 74.77	12.50
+50	79.17	^{9.17} 72.15	7.02	+40	87.04	^{87.04} 74.90	12.14
+85	80.20	^{0.20} 72.28	7.92	+75	87.24	^{87.24} 75.04	12.20
4+20	80.65	^{0.65} 72.42	8.23	2+10	87.77	^{87.77} 75.17	12.60
+67 = M.H. 11	81.70	^{1.70} 72.59	9.11	+45	87.62	^{87.62} 75.30	12.32
0+35	82.25	^{2.25} 72.72	9.53	+80	88.07	^{88.07} 75.43	12.64
+70	82.23	^{2.23} 72.86	9.37	3+15	88.63	^{88.63} 75.57	13.06
1+05	82.02	^{2.02} 72.99	9.03	+50	88.98	^{88.98} 75.70	13.28
+40 - T.P.	82.66	^{2.66} 73.12	9.54	+85	88.42	^{88.42} 75.83	12.59

4+20	88.37	⁸⁸³⁷ 75.97	12.40	1+75	90.73	⁹⁰⁷³ 78.29	12.44
+67 = M.H. 13	88.70	⁸⁸⁷⁰ 76.14	12.56	2+10	90.84	⁹⁰⁸⁴ 78.33	12.51
0+35	89.01	⁸⁹⁰¹ 76.27	12.74	+45	91.42	⁹¹⁴² 78.37	13.05
+70	89.55	⁸⁹⁵⁵ 76.41	13.14	+80	90.94	⁹⁰⁹⁴ 78.42	12.56
1+05	90.10	⁹⁰¹⁰ 76.54	13.56	3+15	91.49	⁹¹⁴⁹ 78.46	13.03
+40	90.28	⁹⁰²⁸ 76.67	13.61	+50	91.67	⁹¹⁶⁷ 78.50	13.17
+75 -	89.75	⁸⁹⁷⁵ 76.81	12.94	+85	92.36	⁹²³⁶ 78.54	13.82
2+10	89.70	⁸⁹⁷⁰ 76.94	12.76	4+20	92.46	⁹²⁴⁶ 78.58	13.89
+45	90.22	⁹⁰²² 77.07	13.15	+61 = M.H. 15	92.37	⁹²³⁷ 78.63	13.74
+80	92.41	⁹²⁴¹ 77.20	15.21	0+35	92.12	⁹²¹² 78.67	13.45
3+15	91.24	⁹¹²⁴ 77.34	13.90	+70	91.67	⁹¹⁶⁷ 78.71	12.96
+50	90.72	⁹⁰⁷² 77.47	13.25	1+05	91.38	⁹¹³⁸ 78.76	12.62
+85	90.55	⁹⁰⁵⁵ 77.60	12.95	+40	91.14	⁹¹¹⁴ 78.80	12.34
4+20	90.77	⁹⁰⁷⁷ 77.74	13.03	+75	92.49	⁹²⁴⁹ 78.84	13.65
+45	90.63	⁹⁰⁶³ 77.83	12.80	2+10	92.88	⁹²⁸⁸ 78.88	14.00
+70.42 = M.H. 14	90.50	⁹⁰⁵⁰ 77.93	12.57	+45	93.34	⁹³³⁴ 78.92	14.42
0+35	90.35	⁹⁰³⁵ 78.08	12.23	+80	93.47	⁹³⁴⁷ 78.97	14.50
+70	90.33	⁹⁰³³ 78.16	12.17	3+15	94.47	⁹⁴⁴⁷ 79.01	15.46
1+05	90.62	⁹⁰⁶² 78.21	12.41	= M.H. 16	79.04		
+40	90.65	⁹⁰⁶⁵ 78.25	12.40				

Cont. - P. 10

Beq. At Hwy. Crossing - M.H. 33 - etc.
See P. 17

6

out.		87.88		2+10	06.02	^{06.02} 89.29	16.73
M.H. 32 - in		^{05.58} 88.13	17.45	+45	07.32	^{07.32} 89.35	17.97
0+40		^{05.33} 88.20	^{17.13} 17.32	+80	09.38	^{09.38} 89.41	19.97
+88 } Tunnel		^{06.05} 06.28 88.29	^{17.76} 17.99	3+15	10.74	^{10.74} 89.48	21.26
1+15 } Tunnel		^{06.05} 06.11 88.34	^{17.71} 17.77	+50	12.32	^{12.32} 89.54	22.78
+63 } Tunnel		^{06.33} 88.42	17.91	+85	12.01	^{12.01} 89.60	22.41
+85		^{05.52} 88.46	17.06	4+20	09.84	^{09.84} 89.67	20.17
2+10	07.22	^{07.22} 88.51	18.74	+50 = M.H. 34	08.32	^{08.32} 89.72	18.60
+45		^{06.74} 88.57	18.17	0+35	07.32	^{07.32} 89.78	17.54
+80		^{07.91} 88.63	19.28	+70	06.49	^{06.49} 89.85	16.64
3+15	.74	^{08.74} 88.70	20.04	1+05	05.83	^{05.83} 89.91	15.92
+50	.02	^{09.02} 88.76	20.26	+40	04.81	^{04.81} 89.97	14.84
+85	.55	^{07.55} 88.82	19.73	+75	05.33	^{05.33} 90.04	15.29
4+10	.39	^{06.39} 88.87	17.52	2+10	05.65	^{05.65} 90.10	15.55
+32.93 = M.H. 33 93		^{05.93} 88.91	17.02	+45	06.05	^{06.05} 90.16	15.89
0+35		^{04.81} 88.97	15.84	+80	07.16	^{07.16} 90.22	16.94
+70		^{03.42} 89.04	14.38	3+15	08.36	^{08.36} 90.29	18.07
1+05		^{02.22} 89.10	13.12	+50	09.11	^{09.11} 90.35	18.76
+40		^{02.95} 89.16	13.79	+85	09.58	^{09.58} 90.41	19.17
+75		^{04.13} 89.23	14.90	4+20	10.92	^{10.92} 90.48	20.44

4+55	11.78	9 ^{11.74} 0.54	21.24
+90	12.45	9 ^{12.45} 0.60	21.85
5+25	12.13	9 ^{12.13} 0.67	21.46
+60	11.43	9 ^{11.43} 0.73	20.70
+95	09.96	9 ^{09.96} 0.79	19.17
6+15.97 = M.H.	09.26	9 ^{09.26} 0.84	18.42
<u>2-cuts</u>	09.29	9 ^{09.29} 1.04	18.25
at 90°	09.31	9 ^{09.31} 0.84	18.47
0+35	08.82	9 ^{08.82} 1.09	17.73
+70	08.21	9 ^{08.21} 1.14	17.07
1+05	07.01	9 ^{07.01} 1.20	15.81
+40	05.69	9 ^{05.69} 1.25	14.44
+75	05.29	9 ^{05.29} 1.30	13.99
2+10	06.47	9 ^{06.47} 1.35	15.12
+45°	07.57	9 ^{07.57} 1.40	16.17
+80	07.88	9 ^{07.88} 1.46	16.42
3+15	08.37	9 ^{08.37} 1.51	16.86
+50	08.78	9 ^{08.78} 1.56	17.22
+85	09.35	9 ^{09.35} 1.61	17.74
4+25	09.19	9 ^{09.19} 1.67	17.52

out.
35 on split

4+64.16 = M.H. 36	09.63	9 ^{09.63} 1.73	17.90
0+35	09.80	9 ^{09.80} 1.78	18.02
+70	10.64	9 ^{10.64} 1.83	18.81
1+05	10.71	9 ^{10.71} 1.89	18.82
+40	10.99	9 ^{10.99} 1.94	19.05
+75 T.P.	11.03	9 ^{11.03} 1.99	19.04
2+10	11.18	9 ^{11.18} 2.04	19.14
+45	10.95	9 ^{10.95} 2.09	18.86
+80	11.65	9 ^{11.65} 2.15	19.50
3+15	12.59	9 ^{12.59} 2.20	20.39
+50	13.15	9 ^{13.15} 2.25	20.90
+85	12.85	9 ^{12.85} 2.30	20.55
4+20	12.84	9 ^{12.84} 2.35	20.49
+55	13.38	9 ^{13.38} 2.41	20.97
4+80 = M.H. 37	13.47	9 ^{13.47} 2.45	21.02
0+35	14.18	9 ^{14.18} 2.50	21.68
+70	15.18	9 ^{15.18} 2.55	22.63
1+05	15.46	9 ^{15.46} 2.61	22.85
+40	13.02	9 ^{13.02} 2.66	20.36
+75	13.12	9 ^{13.12} 2.71	20.41

stakes 8' Lt.

8

2+10 -T.P.	13.49 16.05	9 ^{13.49} 2.76	20.73 -	4+20	13.91	9 ^{13.91} 2.82	20.09
+45	13.70 17.00	9 ^{13.70} 2.81	20.89 -	+41.54 = M.H. 39	14.08	9 ^{14.08} 2.86	20.22
+80	14.18 17.50	9 ^{14.18} 2.87	21.31 -	0+35	14.59	9 ^{14.59} 2.91	20.68
3+15	14.89 17.25	9 ^{14.89} 2.92	21.97 -	+70	14.39	9 ^{14.39} 2.96	20.43
+50	14.69 17.13	9 ^{14.69} 2.97	21.72 -	1+08.82 = M.H. 40	14.14	9 ^{14.14} 4.02	20.12
+85	13.96 16.62	9 ^{13.96} 3.02	20.94 -	"	14.14	9 ^{14.14} 4.27	19.87
4+20	14.09	9 ^{14.09} 3.08	21.01 -	Req. "B" line at M.H. 40			
+55	15.45	9 ^{15.45} 3.14	22.31 -	0+00 = M.H. 40	14.13	9 ^{14.13} 4.44	19.69
+95 = M.H. 38	15.41	9 ^{15.41} 3.20	22.21	+35	13.97	9 ^{13.97} 4.72	19.25
0+35	15.81	9 ^{15.81} 3.25	22.56	+70	13.04	9 ^{13.04} 5.00	18.04
+70	15.06	9 ^{15.06} 3.30	21.76	1+05	12.10	9 ^{12.10} 5.28	16.82
1+05	15.11	9 ^{15.11} 3.36	21.75	+40	12.92	9 ^{12.92} 5.56	17.36
+40	15.41	9 ^{15.41} 3.41	22.00	+75 - T.P.	12.18	9 ^{12.18} 5.84	16.34
+75	15.47	9 ^{15.47} 3.46	22.01	2+10	11.91	9 ^{11.91} 6.12	15.79
2+10	14.95	9 ^{14.95} 3.51	21.44	+45	11.99	9 ^{11.99} 6.40	15.59
+45	14.38	9 ^{14.38} 3.56	20.82	+80	12.64	9 ^{12.64} 6.68	15.96
+80	14.42	9 ^{14.42} 3.62	20.80	3+15	12.53	9 ^{12.53} 6.96	15.57
3+15	14.01	9 ^{14.01} 3.67	20.34	+50	13.19	9 ^{13.19} 7.24	15.95
+50	14.34	9 ^{14.34} 3.72	20.62	+85	13.23	9 ^{13.23} 7.52	15.71
+85	14.26	9 ^{14.26} 3.77	20.49	4+20	13.33	9 ^{13.33} 7.80	15.53

415.35 = Pole

"B" Line

418.77 = Pole

stakes 8' Lt.

4+45	13.44	9 13.44 8.00	15.44
+70 = M.H. 55	13.73	9 13.73 8.20	15.53
0+35	12.99	9 12.99 8.48	14.51
+70	13.58	9 13.58 8.76	14.82
1+05	13.97	9 13.97 9.04	14.93
+40	14.48	9 14.48 9.32	15.16
+75	14.37	9 14.37 9.60	14.77
2+10	13.77	9 13.77 9.88	13.89
+45	14.77	40 14.77 0.16	14.61
+80 - T.P.	14.82	0 14.82 0.44	14.38
3+15	14.52	0 14.52 0.72	13.80
+50	14.82	0 14.82 1.00	13.82
+85	15.32	0 15.32 1.28	14.04
4+20	15.86	0 15.86 1.56	14.36
+45	16.12	0 16.12 1.76	14.36
+70 = M.H. 56	16.06	0 16.06 1.96	14.10
0+35	16.60	0 16.60 2.24	14.36
+70	16.72	0 16.72 2.52	14.20
1+05	17.34	0 17.34 2.80	14.54

1+40	17.45	17.45 03.08	14.37
+75	18.10	18.10 03.36	14.74
2+10	19.06	19.06 03.64	15.42
+45	19.26	19.26 03.92	15.34
+80	19.75	19.75 04.20	15.55
3+15	20.11	20.11 04.48	15.63
+50	20.47	20.47 04.76	15.71
+85	21.06	21.06 05.04	16.02
4+20	21.69	21.69 05.32	16.37
+60 = M.H. 57	21.86	21.86 05.64	16.22
= End.			

M.H. 16 - To 17 + N. ^{-s}	95.07	95.07 79.04	16.03	0+70	93.95	93.95 79.93	14.02
0+00 = M.H. 16 To -w	94.88	94.88 79.04	15.84	1+05	94.26	94.26 79.98	14.28
+35	94.80	94.80 79.08	15.72	+40	94.48	94.48 80.02	14.46
+70	94.85	94.85 79.12	15.73	+75	94.96	94.96 80.06	14.90
1+05	94.09	94.09 79.17	14.92	2+10	95.60	95.60 80.10	15.50
+40	93.05	93.05 79.21	13.84	+45	95.74	95.74 80.14	15.60
+75	93.28	93.28 79.25	14.03	+80	95.28	95.28 80.19	15.09
2+10	93.57	93.57 79.29	14.28	3+15	95.20	95.20 80.23	14.97
+45	94.08	94.08 79.33	14.75	+50	95.41	95.41 80.27	15.14
+80	94.35	94.35 79.38	14.97	+85	95.13	95.13 80.31	14.82
3+15	94.60	94.60 79.42	15.18	4+20	95.17	95.17 80.35	14.82
+50	94.04	94.04 79.46	14.58	+40 = M.H. 18	95.21	95.21 80.38	14.83
+85	93.58	93.58 79.50	14.08	0+35	95.61	95.61 80.42	15.19
4+20	93.63	93.63 79.54	14.09	+70	95.52	95.52 80.46	15.06
+55	93.85	93.85 79.59	14.26	1+05	95.60	95.60 80.51	15.09
+90	93.99	93.99 79.63	14.36	+40	96.08	96.08 80.55	15.53
5+25	94.05	94.05 79.67	14.38	+75	97.42	97.42 80.59	16.83
out. +45.89 = M.H. 17	94.08	94.08 79.70	14.38	2+10	98.87	98.87 80.63	18.24
in	94.08	94.08 79.85	14.23	+45	99.38	99.38 80.67	18.71
0+35	94.06	94.06 79.89	14.17	+80	98.98	98.98 80.72	18.26

3+15	98.10	^{98.10} 80.76	17.34
+50	98.65	^{98.65} 80.80	17.85
+85	98.72	^{98.72} 80.84	17.88
4+20	98.84	^{98.84} 80.88	17.96
+40 = M.H. 19	98.81	^{98.81} 80.91	17.90
0+35	99.06	^{99.06} 80.95	18.11
+70	99.32	^{99.32} 80.99	18.33
1+05	99.62	^{99.62} 81.04	18.58
+40	00.02	^{00.02} 81.08	18.94
+75	00.28	^{00.28} 81.12	19.16
2+10	00.42	^{00.42} 81.16	19.26
+45	00.57	^{00.57} 81.20	19.37
+80	01.00	^{01.00} 81.25	19.75
3+15	01.42	^{01.42} 81.29	20.13
+50	01.68	^{01.68} 81.33	20.35
+85	01.93	^{01.93} 81.37	20.56
4+20	01.89	^{01.89} 81.41	20.48
49.67 +267 = M.H. 20	02.37	^{02.37} 81.45	20.92
0+35	02.34	^{02.34} 81.49	20.85
+70	02.62	^{02.62} 81.53	21.09

1+05	02.95	^{02.95} 81.58	21.37
+40	03.42	^{03.42} 81.62	21.80
+75	03.44	^{03.44} 81.66	21.78
2+10	03.20	^{03.20} 81.70	21.50
+45	02.64	^{02.64} 81.74	20.90
+80	02.18	^{02.18} 81.79	20.39
3+15	01.87	^{01.87} 81.83	20.04
+50	01.75	^{01.75} 81.87	19.88
+85	01.80	^{01.80} 81.91	19.89
4+20	02.31	^{02.31} 81.95	20.36
out T.P. +40 = M.H. 21 in	02.61	^{02.61} 81.98	20.63
	02.63	^{02.63} 82.13	20.50
0+35	03.25	^{03.25} 82.17	21.08
+70	02.75	^{02.75} 82.21	20.54
1+05	01.63	^{01.63} 82.26	19.36
+40	00.85	^{00.85} 82.30	18.55
+75	00.02	^{00.02} 82.34	17.68
2+10	99.07	^{99.07} 82.38	16.69
+45	99.09	^{99.09} 82.42	16.67
+80	98.98	^{98.98} 82.47	16.51

3+15	99.78	99.28 82.51	16.77
+50	99.93	99.93 82.55	17.38
+85	99.99	99.99 82.59	17.40
4+20	00.48	00.48 82.63	17.85
+40 = M.H. 22	00.75	00.75 82.66	18.09
0+35	01.42	01.42 82.70	18.72
+70	02.07	02.07 82.74	19.33
1+05	02.68	02.68 82.79	19.89
+40	03.00	03.00 82.83	20.17
+75	03.12	03.12 82.87	20.25
2+10	02.46	02.46 82.91	19.55
+45	01.98	01.98 82.95	19.03
+80	01.60	01.60 83.00	18.60
3+15	01.38	01.38 83.04	18.34
+50	00.96	00.96 83.08	17.88
+85	99.98	99.98 83.12	16.86
4+20	98.81	98.81 83.16	15.65
+40.02 = M.H. 23	98.42	98.42 83.19	15.23

M.H. 40 + Cross Hwy. to M.H. 41

13

0 + 00 = M.H. 40

+35	13.97	13.97 94.35	19.62
+70	14.37	14.37 94.42	19.95
1 + 05	14.29	14.29 94.50	19.79
+40	14.19	14.19 94.58	19.61
+75	14.19	14.19 94.66	19.53
2 + 02.30	13.37	13.37 94.72	18.65
1			
+45.30	13.41	13.41 94.81	18.60
+69.30	13.44	13.44 94.86	18.58
3 + 12.30	13.11	13.11 94.95	18.16
3 + 47.80 - M.H. 41	11.53	11.53 95.03	16.50
0 + 00			
0 + 35	12.72	12.72 95.11	17.61
+70	12.22	12.22 95.18	17.04
1 + 05	11.55	11.55 95.26	16.29
+40	10.27	10.27 95.34	14.93

1 + 75 - T.P.

09.49	09.49	09.49 95.42	14.07
08.16	08.16	08.16 95.49	12.67
07.40	07.40	07.40 95.57	11.83
07.07	07.07	07.07 95.65	11.42
06.68	06.68	06.68 95.72	10.96
06.36	06.36	06.36 95.80	10.56
06.50	06.50	06.50 95.88	10.62
06.64	06.64	06.64 95.95	10.69
06.19	06.19	06.19 96.03	10.16
07.21	07.21	07.21 96.12	11.09
07.00	07.00	07.00 96.29	10.71
06.75	06.75	06.75 96.37	10.38
06.10	06.10	06.10 96.44	9.66
06.20	06.20	06.20 96.52	9.68
06.12	06.12	06.12 96.60	9.52
05.70	05.70	05.70 96.68	9.02
05.56	05.56	05.56 96.75	8.81
05.07	05.07	05.07 96.83	8.24
05.00	05.00	05.00 96.91	8.09
04.41	04.41	04.41 96.98	7.43

+55 out

+94.62 = M.H. 42

in

0 + 35

1 + 05

+40

+75 = T.P.

2 + 10

+45

+80

3 + 15

3+50	04.19	^{04.19} 97.06	7.13	0+35	01.52	^{01.52} 98.64	C 2.88
+85	04.01	^{04.01} 97.14	6.87	+70	01.39	^{01.39} 98.71	C 2.68
4+20	03.70	^{03.70} 97.22	6.48	1+00 = M.H. 44			
+60	03.58	^{03.58} 97.31	6.27	1+05	00.01	^{00.01} 98.79	C 1.22
5+00 = M.H. 43	02.86	^{02.86} 97.39	5.47	+20 = c I			
0+35	01.57	^{01.57} 97.47	4.10	+40	98.29	^{98.87} 29	F 0.58
+70	01.47	^{01.47} 97.54	3.93	+75	94.63	^{98.95} 463	F 4.32
1+05	01.24	^{01.24} 97.62	3.62	2+10	91.27	^{99.02} 1.27	F 7.75
+40 = T.P.	01.32	^{01.32} 97.70	3.62	+45	91.15	^{99.10} 1.15	F 7.95
+75	00.99	^{00.99} 97.78	3.21	+80	93.53	^{99.18} 3.53	F 5.65
2+10	00.53	^{00.53} 97.85	2.68	3+15	97.29	^{99.25} 2.29	F 1.96
+45	00.39	^{00.39} 97.93	2.46	+50 = End. C.I.	00.33	^{99.33} 2.33	C 1.00
+80	99.51	^{99.51} 98.00	C 1.51	+85	01.74	^{01.74} 99.41	C 2.33
3+15	98.09	^{98.09} 98.08	C 0.01	4+20 = M.H. 45	02.69	^{02.69} 99.49	C 3.20
+50	95.27	^{95.27} 98.16	F 2.89	Moved	See P. 18		
+85	94.15	^{94.15} 98.24	F 4.09	+ Bet. piers			
4+20	97.54	^{97.54} 98.31	F 0.77	1+44	98.38	^{98.88} 3.88	F 0.50
+55	00.07	^{00.07} 98.37	C 1.68	+80	93.99	^{98.96} 3.99	F 4.97
+90	01.07	^{01.07} 98.47	2.60	2+16	90.00	^{99.04} 6.00	F 9.04
5+31.34 = M.H. 44	01.43	^{01.43} 98.56	2.87	+52	91.13	^{99.11} 1.13	F 7.98
Moved.				+88	93.97	^{99.19} 3.97	F 5.22
				3+24	98.45	^{99.27} 8.45	F 0.82

				2+10	98.35	98.35 83.97	14.38
0+00 = M.H. 23	98.40	83.19	15.21	+45	99.14	99.14 84.01	15.13
+35	99.66	83.23	16.43	+80	99.54	99.54 84.06	15.48
+70	99.68	83.27	16.41	3+15	00.13	00.13 84.10	16.03
1+05	98.84	83.32	15.52	+50	01.00	01.00 84.14	16.86
+40	98.35	83.36	14.99	+85 = TP.	01.56	01.56 84.18	17.38
+75	98.25	83.40	14.85	4+20	02.27	02.27 84.22	18.05
2+10	97.07	83.44	13.63	+40 = M.H. 25	02.38	02.38 84.24	18.14
+45	95.88	83.48	12.40	0+35	02.35	02.35 84.28	18.09
+80	95.13	83.53	11.60	+70	02.33	02.33 84.32	18.03
3+15	94.89	83.57	11.32	1+05	02.47	02.47 84.37	18.12
+50	94.79	83.61	11.18	+40	02.62	02.62 84.41	18.23
+85	94.77	83.65	11.12	+75	02.85	02.85 84.45	18.42
4+20	95.81	83.69	12.12	2+10 Raised	02.60	02.60 84.49	19.13
+48 = M.H. 24	96.41	83.72	12.69	+45 .02	04.25	04.25 84.53	19.74
0+35	96.66	83.76	12.90	+80	05.04	05.04 84.58	20.48
+70	97.06	83.80	13.26	3+15	05.19	05.19 84.62	20.59
1+05	97.43	83.85	13.58	+50	05.07	05.07 84.66	20.43
+40	97.50	83.89	13.61	+85	04.81	04.83 84.70	20.13
+75	97.72	83.93	13.79	4+20	04.59	04.61 84.74	19.89

4+59.11 = M.H. 26	on Diag. 04.41	04.41	84.79	19.62
0+35	04.72	04.72	84.83	19.89
+70	04.70	04.70	84.87	19.83
1+05	05.03	05.03	84.92	20.11
+40	05.16	05.16	84.96	20.20
+75	05.29	05.29	85.00	20.29
2+10	05.52	05.52	85.04	20.48
+45	05.84	05.84	85.08	20.76
+80	05.87	05.87	85.13	20.74
3+15	05.97	05.97	85.17	20.80
+33.53 = M.H. 27	05.63	05.63	85.19	20.44
0+35	05.22	05.22	85.23	19.99
+70 = T.P.	04.75	04.75	85.27	19.48
-1+05	04.55	04.55	85.32	19.23
+45	03.78	03.78	85.36	18.42
+75	02.23	02.23	85.40	16.83
2+10	01.44	01.44	85.44	16.00
+45	00.60	00.60	85.48	15.12
+80	00.07	00.07	85.53	14.54
3+05	00.20	00.20	85.56	14.64

3+30 = M.H. 28	out. 99.92	99.92	385.59	14.33
in	397.70	85.74	13.96	Cut
0+35	398.49	85.78	12.71	
+70	397.75	85.82	12.13	
1+05	397.65	85.87	11.78	
+40	397.32	85.91	11.41	
+75	396.22	85.95	10.27	
2+10	394.58	85.99	8.59	
+45	392.93	86.03	6.90	
+80	391.69	86.08	5.61	
3+15	390.79	86.12	4.67	
+50	390.35	86.16	4.19	
+85	388.72	86.20	2.52	
4+20	389.14	86.24	2.90	
+55	390.38	86.29	4.09	
+90	390.71	86.33	4.38	
5+25	391.49	86.37	5.12	
+57.75 = M.H. 29	391.90	86.41	5.49	
0+35	392.76	86.45	6.31	
+70	393.44	86.49	6.95	

1+05	394.27	86.54	7.73
+40	394.53	86.58	7.75
+75	393.29	86.62	6.67
2+10 = Beg span	389.95	86.66	C-3.29
+45	383.24	86.70	F-3.46
+78 = end span			
+80	388.88	86.75	C-2.13
2+15	391.76	86.79	4.97
+50	392.64	86.83	5.81
+85	392.87	86.87	6.00
4+05 = M.H. 30	393.02	86.90	6.12
0+35	93.50	86.94	6.56
+70	94.42	86.98	7.44
1+05	94.42	87.03	7.39
+40	95.37	87.07	8.30
+75	95.71	87.11	8.60
2+10	96.50	87.15	9.35
+45	97.63	87.19	10.44
+80	98.12	87.24	10.88
3+15	99.36	87.28	12.08
+50	00.60	87.32	13.28

3+85 = T.P.	01.76	87.36	14.40
4+05 = M.H. 31	02.07	87.39	14.68
0+35	03.30	87.43	15.87
+70	03.00	87.47	15.53
1+05	02.81	87.52	15.29
+40	03.03	87.56	15.47
+75	03.39	87.60	15.79
2+10 =	03.76	87.64	16.12
+45	04.77	87.68	17.09
+80	05.01	87.73	17.28
3+15	04.11	87.77	16.34
+50	02.91	87.81	15.10
+85	03.99	87.85	16.14
4+11.95 = M.H. 32	05.56	87.88	17.68
in		88.13	

See P. 6

	Stake	Grade	Cut				
M.H. 45	02.69	99.49	C 3.20	2+15	10.85	10.85 01.00	9.85
0+35	03.85	99.57	4.28	+50	11.08	11.08 01.08	10.00
+70	04.66	99.64	5.02	+85	10.25	10.25 01.16	9.09
1+00 = M.H. 45 - New Loc.							
1+05	05.53	99.72	5.81	4+15 = M.H. 47	09.62	09.62 01.22	8.40
+40	06.56	99.80	6.76	in	09.62	09.62 01.38	8.24
+75	07.88	99.88	8.00	0+35	10.25	10.25 01.46	8.79
2+10	08.98	99.98	9.03	+70	10.37	10.37 01.53	8.84
+45	09.66	00.03	9.63	1+05	10.95	10.95 01.61	9.34
+80	10.39	00.11	10.28	+40	10.62	10.62 01.69	8.93
3+15	11.02	00.18	10.84	+75	10.34	10.34 01.77	8.57
+50	11.40	00.26	11.14	2+10	10.70	10.70 01.84	8.86
+72.04 = M.H. 46	11.20	00.31	10.89	+45	11.30	11.30 01.92	9.38
0+35	11.39	00.39	11.00	+80	10.95	10.95 02.00	8.95
+70 T.P.	11.28	00.46	10.82	3+15	11.05	11.05 02.07	8.98
1+05	11.04	00.54	10.50	+50	11.81	11.81 02.15	9.66
+40	11.40	00.62	10.78	+85	11.96	11.96 02.23	9.73
+75	10.72	00.70	10.02	4+10.16 = M.H. 48	12.19	12.19 02.29	9.90
2+10	10.79	00.77	10.02	0+35	11.29	11.29 02.37	8.92
+45	10.79	00.85	9.94	+70	11.58	11.58 02.44	9.14
+80	10.56	00.93	9.63	1+05	11.68	11.68 02.52	9.16

1+40	12.21	^{12.21} 02.60	9.61
+75	12.13	^{12.13} 02.68	9.45
2+10	13.25	^{13.25} 02.75	10.50
+45	14.00	^{14.00} 02.83	11.17
+80	14.13	^{14.13} 02.91	11.22
3+15	13.37	^{13.37} 02.98	10.39
+50	13.65	^{13.65} 03.60	10.05
+75.18 = M.H. 49	14.35	^{14.35} 03.11	11.24
0+35	14.43	^{14.43} 03.19	11.24
+70	13.80	^{13.80} 03.26	10.54
1+05	14.08	^{14.08} 03.34	10.74
+40	14.41	^{14.41} 03.42	10.99
+75	14.58	^{14.58} 03.50	11.08
2+10	14.76	^{14.76} 03.57	11.19
+45	15.50	^{15.50} 03.65	11.85
+80	15.55	^{15.55} 03.73	11.82
3+15	15.58	^{15.58} 03.80	11.78
+45.24 = M.H. 50	16.06	^{16.06} 03.87	12.19
0+35	16.49	^{16.49} 03.95	12.54
+70	16.70	^{16.70} 04.02	12.68

1+05	16.39	^{16.39} 04.10	12.29
+40	15.50	^{15.50} 04.18	11.32
+75	15.81	^{15.81} 04.26	11.55
2+10	15.62	^{15.62} 04.33	11.29
+45	16.83	^{16.83} 04.41	12.42
+80	16.94	^{16.94} 04.49	12.45
3+15	17.01	^{17.01} 04.56	12.45
+50 = M.H. 51	17.64	^{17.64} 04.64	13.00
0+35	18.17	^{18.17} 04.72	13.45
+70	18.77	^{18.77} 04.79	13.98
1+05	18.57	^{18.57} 04.87	13.70
+40	19.42	^{19.42} 04.95	14.47
+75	19.83	^{19.83} 05.03	14.80
2+15 = M.H. 52	20.02	^{20.02} 05.11	14.91
0+35	20.06	^{20.06} 05.19	14.87
+70	19.76	^{19.76} 05.26	14.50
1+05	20.71	^{20.71} 05.34	15.37
+40 ^{T.P.}	20.78	^{20.78} 05.42	15.36
+75	20.78	^{20.78} 05.50	15.28
2+10	20.85	^{20.85} 05.57	15.28

2+45	21.03	^{21.03} 05.65	15.38
+80	21.91	^{21.91} 05.73	16.18
3+15	22.30	^{22.30} 05.80	16.50
+50	22.48	^{22.48} 05.88	16.60
+85	21.34	^{21.34} 05.96	15.38
4+20	21.83	^{21.83} 06.03	15.80
+60 = M.H. 53	22.95	^{22.95} 06.12	16.83
0+35	22.98	^{22.98} 06.20	16.78
+70	22.93	^{22.93} 06.27	16.66
1+05	23.88	^{23.88} 06.35	17.53
+40	23.95	^{23.95} 06.43	17.52
+75	24.09	^{24.09} 06.51	17.58
2+10	23.62	^{23.62} 06.58	17.04
+45	23.27	^{23.27} 06.66	16.61
+80	24.14	^{24.14} 06.74	17.40
3+15	24.48	^{24.48} 06.81	17.67
+50	25.29	^{25.29} 06.89	18.40
+85	26.02	^{26.02} 06.97	19.05
4+20	26.59	^{26.59} 07.04	19.55
+42.04 = M.H. 54	27.17	^{27.17} 07.09	20.08

The End!

Begin Water Stakes.
INDEXED 2092-2098 - D

6-26-53

7.0

21

09.72
+ 1.16
10.88

				stake	Grade	Cut.
				8+50	26.3	6.3 20.8 5.5
				9~ = Brk	23.9	3.9 18.8 5.1
0+17.83 = 1/16 Bend.	19.3	13.3	6.0	+50	21.2	21.2 16.0 5.2
+50	20.7	14.7	6.0	10-	18.2	8.2 13.1 5.1
1~	22.8	17.0	5.8	+50	15.3	5.3 10.3 5.0
+50	25.1	19.2	5.9	+76.39 = Brk	13.9	3.9 08.8 5.1
2~	27.3	21.5	5.8	9+69.69 = ah.	13.5	3.5 408.8 4.7
+50	29.5	23.8	5.7	10~	13.9	03.5 08.5 4.8
3~	31.7	26.0	5.7	+50	17.3	17.3 08.5 8.8
+50	34.0	28.3	5.7	11~	18.6	8.6 08.3 10.3
4~ = Brk	36.2	30.5	5.7	+29.45 = 1/8 rt.	19.1	20.5 19.1 08.2 11.9
+50	38.2	31.3	6.9	+46.78 = 1/16	19.5	19.5 08.1 11.4
5~ = Brk	39.6	32.0	7.6	+90	17.3	17.3 08.0 9.3
+50	39.8	31.5	8.3	12+40 = Brk	14.0	14.0 07.8 6.2
6~ Brk	38.8	31.0	7.8	+90	10.7	10.7 05.6 5.1
+50	36.6	29.0	7.6	13+40.78 = 1/16	08.7	8.7 03.4 5.3
7~	34.0	26.9	7.1	+90	08.0	8.0 01.3 6.7
+50	31.5	24.9	6.6	14+40	05.9	05.9 99.1 6.8
8~	29.0	22.9	6.1	+90	03.4	03.4 97.0 6.4

	Stake	Grade	Cut				
15+40 = Brk.	00.6	90.6 94.8	C 5.8	24~	90.6	90.6 84.2	6.4
+90	00.2	90.2 94.7	C 5.5	+50	89.0	89.0 82.3	6.7
16+40 = Brk	00.7	90.7 94.6	6.1	+61.29 = 1/32	88.5	88.5 81.9	6.6
+62.68 = 1/16	01.0	91.0 94.6	6.4	25~ Brk.	86.4	86.4 80.4	6.0
17~	02.8	92.8 94.5	8.3	+40 = Brk	84.5	84.5 78.7	5.8
+50	04.9	94.9 94.5	10.4	26~ Brk.	79.8	79.8 79.4	10.4
18-	08.2	98.2 94.4	13.9	+20 = B.O. +30 Brk.	77.3	77.3 69.4	7.9
+47.27 = 1/8	10.0	910.0 94.4	15.6	+85	76.1	76.1 71.4	4.7
+57.95 = 1/16	09.2	909.2 94.4	14.8	Sewer 27+40 = Brk.	78.0	78.0 73.5	4.5
19~	06.0	906.0 94.3	11.7	Req. 8' Rt. +69.56 = 1/32	80.0	80.0 74.2	5.8
+50	02.3	902.3 94.3	8.0	28~	80.3	80.3 74.9	5.4
20~ Brk. = T.P.	99.91	999.91 94.2	5.7	+50	81.1	81.1 76.2	4.9
+50	97.8	97.8 92.5	5.3	29~ = Brk	82.2	82.2 77.4	4.8
21~	95.9	95.9 90.8	5.1	+50 8778	83.8	83.8 78.5	5.3
+44.89 = 1/32	94.6	94.6 89.4	5.2	30-	85.6	85.6 79.6	6.0
22~	93.3	93.3 88.9	4.4	+50	87.4	87.4 80.7	6.7
+50	92.5	92.5 88.5	4.0	31~	89.0	89.0 81.8	7.2
23~ Brk	93.6	93.6 88.0	5.6	+50	90.1	90.1 82.9	7.2
+50	92.1	92.1 86.1	6.0	32~	90.9	90.9 84.0	6.9

32+50		91.2	^{91.2} 85.1	6.1	+50	97.6	^{7.6} 92.7	4.9	
33~	Brk	91.4	^{91.4} 86.2	5.2	43~	Brk	98.1	^{8.1} 93.0	5.1
+50	91.57	91.6	^{91.6} 86.4	5.2	+50	98.4	^{8.4} 93.2	5.2	
34~		91.8	^{91.8} 86.5	5.3	44~	98.7	^{8.7} 93.5	5.2	
+50		91.8	^{91.8} 86.7	5.1	+50	98.9	^{8.9} 93.7	5.2	
35~		91.7	^{91.7} 86.9	4.8	45~	99.1	^{9.1} 93.9	5.2	
+50		91.9	^{91.9} 87.1	4.8	+50	99.3	^{9.3} 94.2	5.1	
36~	Brk	92.2	^{92.2} 87.2	5.0	46~	99.6	^{9.6} 94.4	5.2	
+50		92.7	^{92.7} 87.7	5.0	+50	99.8	^{9.8} 94.6	5.2	
37~		93.2	^{93.2} 88.1	5.1	47~	00.0	^{00.0} 94.9	5.1	
+50		94.0	^{94.0} 88.6	5.4	+50	00.2	^{00.2} 95.1	5.1	
38~		94.8	^{94.8} 89.1	5.7	48~	^{00.5} 00.5	^{00.5} 95.3	5.2	
+50		95.6	^{95.6} 89.6	6.0	+50	00.9	^{00.9} 95.6	5.3	
39~	Brk	96.2	^{96.2} 90.0	6.2	49~	= Brk	^{01.0} 95.8	5.2	
+50		96.32	^{6.3} 90.4	5.9					
40~		96.5	^{6.5} 90.9	5.6					
+50		96.7	^{6.7} 91.3	5.4					
41~	Brk	96.9	^{6.9} 91.7	5.2					
+50		97.2	^{7.2} 92.0	5.2					
42~		97.4	^{7.4} 92.4	5.0					

+39.1 = E.C.

Cont. on P. 27

Req. Water Stakes at 129+05-ahead.

24

		Ele.	cut.				
				138+50	16.5	^{16.5} 11.8	4.7
129+05		14.8 ^{14.8} 08.6	6.2	139~	17.0	^{2.0} 12.3	4.7
+50		14.1 ^{14.1} 08.3	5.8	+50	17.2	^{7.2} 12.9	4.3
130~	Brk	12.1 ^{12.1} 08.0	4.1	140~	17.9	^{7.9} 13.5	4.4
+50		12.1 ^{12.1} 07.7	4.4	+50	19.4	^{9.4} 14.1	5.3
131-	Brk	11.5 ^{11.5} 07.4	4.1	141~	19.7	^{9.7} 14.7	5.0
+50		11.8 ^{11.8} 07.6	4.2	+50	20.0	^{20.0} 15.3	4.7
132~		12.4 ^{12.4} 07.8	4.6	142~	20.6	^{20.6} 15.8	4.8
+50		13.0 ^{13.0} 08.0	5.0	+50	21.3	^{21.3} 16.4	4.9
133-		13.6 ^{13.6} 08.3	5.3	143-	22.3	^{22.3} 17.0	5.3
+50		13.0 ^{13.0} 08.5	4.5	+50	22.5	^{22.5} 17.6	4.9
134-		13.4 ^{13.4} 08.7	4.7	144-	23.2	^{23.2} 18.2	5.0
+50		14.1 ^{14.1} 08.9	5.2	+50	24.1	^{24.1} 18.8	5.3
135~		14.0 ^{14.0} 09.1	4.9	145~	24.8	^{24.8} 19.4	5.4
+50		14.5 ^{14.5} 09.3	5.2	+50	24.7	^{24.7} 19.9	4.8
136~		14.3 ^{14.3} 09.5	4.8	146~	Brk 25.1	^{25.1} 20.5	4.6
+50	14.59	14.6 ^{14.6} 09.8	4.8	+50	24.7	^{24.7} 20.0	4.7
137~	Brk	15.2 ^{15.2} 10.0	5.2	147-	25.0	^{25.0} 19.5	5.5
+50		15.8 ^{15.8} 10.6	5.2	+50	24.1 ^{4.15}	^{24.1} 19.0	5.1
138~		16.5 ^{16.5} 11.2	5.3	148~	Brk 24.4	^{24.4} 18.4	6.0

148+50	21.8	^{21.8} 17.7	4.1	158~	21.9	^{21.9} 17.4	4.5
149~	21.6	^{21.6} 17.0	4.6	+50	21.5	^{21.5} 17.5	4.0
+50	21.7	^{21.7} 16.3	5.4	159~	Brk 23.2	^{23.2} 17.6	5.6
150~	19.2	^{19.2} 15.5	3.7	+50	23.9	^{23.9} 18.5	5.4
+50	19.3	^{19.3} 14.8	4.5	160~	25.1	^{25.1} 19.4	5.7
+80= Brk	20.0	^{20.0} 14.4	5.6	+50	26.4	^{26.4} 20.3	6.1
151+30	19.3	^{19.3} 14.5	4.8	161~	Brk 27.9	^{27.9} 21.1	6.8
+80	19.7	^{19.7} 14.6	5.1	+40	27.6	^{27.6} 21.5	6.1
152+30	20.1	^{20.1} 14.7	5.4	^{26.93} 161+65.30= Tee	26.9	^{26.9} 21.8	5.1
+80 Brk	19.3	^{19.3} 14.8	4.5	162+00	27.4	^{27.4} 22.1	5.3
153+30	19.8	^{19.8} 15.2	4.6	162+27	27.5	^{27.5} 22.4	5.1
+80	21.4	^{21.4} 15.6	5.8	+50	29.3	^{29.3} 22.7	6.6
154+30	20.6	^{20.6} 16.0	4.6	163+0	29.8	^{29.8} 23.2	6.6
+80 Brk	21.1	^{21.1} 16.4	4.7	+50	30.5	^{30.5} 23.7	6.8
155~ Brk	21.1	^{21.1} 16.5	4.6	164+	30.4	^{30.4} 24.2	6.2
+50	21.6	^{21.6} 16.6	5.0	+50	29.3	^{29.3} 24.7	4.6
156~ 21.95	21.9	^{21.9} 16.8	5.1	+80	30.4	^{30.4} 25.0	5.4
+50	22.3	^{22.3} 16.9	5.4	165+20	30.5	^{30.5} 25.0	5.5
157~	22.4	^{22.4} 17.1	5.3	+70	31.7	^{31.7} 24.1	7.6
+50	22.5	^{22.5} 17.2	5.3	166+20	32.7	^{32.7} 23.3	9.4

166 + 75.47 = Ang. Pt.	32.7	^{32.7} 22.3	10.4
167 + 03.47	28.1	^{8.1} 21.8	6.3
167 + 46.47	28.2	^{8.2} 21.8	6.4
167 + 70.47	28.2	^{8.2} 21.8	6.4
168 + 13.47	28.1	^{8.1} 21.8	6.3
168 + 41.47 = end.	31.2	^{31.2} 21.8	9.4

49~				59~	Brk	05.1	^{5.1} 99.9	5.2
+50	01.3	^{01.3} 96.1	5.2	+50		05.6	^{5.6} 400.7	4.9
50~	01.6	^{01.6} 96.3	5.3	60~		06.4	^{6.4} 01.4	5.0
+50	01.9	^{01.9} 96.6	5.3	+50		07.4	^{7.4} 02.2	5.2
51~	02.2	^{02.2} 96.9	5.3	61~	^{8.8} Brk	08.8	^{8.8} 03.0	5.8
+50	02.5	^{02.5} 97.1	5.4	+50		10.3	^{10.3} 03.8	6.5
52~	02.6	^{02.6} 97.4	5.2	62~		12.0	^{12.0} 04.5	7.5
+50	02.8	^{02.8} 97.7	5.1	+50		13.7	^{13.7} 05.3	8.4
53~	03.1	^{03.1} 97.9	5.2	63~		15.3	^{15.3} 06.0	9.3
+50	03.4	^{03.4} 98.2	5.2	+50		16.4	^{16.4} 06.8	9.6
54~ ^{3.8}	03.8	^{3.8} 98.4	5.4	64~		17.0	^{17.0} 07.5	9.5
+50	04.1	^{4.1} 98.7	5.4	+50		17.3	^{17.3} 08.3	9.0
55~	04.3	^{4.3} 99.0	5.3	65~	^{7.61} Brk	17.6	^{17.6} 09.0	8.6
+50	04.4	^{4.4} 99.2	5.2	+50		17.8	^{17.8} 09.2	8.6
56~ Brk	04.7	^{4.7} 99.5	5.2	66~		17.9	^{17.9} 09.3	8.6
+50	04.8	^{4.8} 99.6	5.2	+50		17.7	^{17.7} 09.5	8.2
57~	05.0	^{5.0} 99.6	5.4	67~		17.5	^{17.5} 09.7	7.8
+50	05.1	^{5.1} 99.7	5.4	+50		17.0	^{17.0} 09.8	7.2
58~	05.1	^{5.1} 99.8	5.3	68~		16.5	^{16.5} 10.0	6.5
+50	05.0	^{5.0} 99.8	5.2	+50		16.0	^{6.0} 10.2	5.8

69~	Brk.	15.7	10.3 ^{5.7}	5.4
+50		15.4	09.7 ^{5.4}	5.7
70~		15.0	09.1 ^{5.0}	5.9
+50		14.3	08.5 ^{14.3}	5.8
71~	Brk.	13.4	07.9 ^{13.4}	5.5
+50	238	12.4	07.0 ^{12.4}	5.4
72~		11.5	06.5 ^{11.5}	5.4
+50		10.7	05.2 ^{10.7}	5.5
73~		09.9	04.3 ^{9.9}	5.6
+50		08.9	03.4 ^{8.9}	5.5
74~		08.0	02.5 ^{8.0}	5.5
+50		07.0	01.6 ^{7.0}	5.4
75~		06.0	00.7 ^{6.0}	5.3
+50		05.3	99.8 ^{5.3}	5.5
76~	471 Brk.	04.8	98.9 ^{4.8}	5.9
+50		04.2	98.6 ^{4.2}	5.6
77~		03.7	98.3 ^{3.7}	5.4
+50		03.4	98.0 ^{3.4}	5.4
78~		03.2	97.6 ^{3.2}	5.6
+50		02.7	97.3 ^{2.7}	5.4

79~		02.2	97.0 ^{2.2}	5.2
+50		01.8	96.7 ^{1.8}	5.1
80~	Brk.	01.7	96.4 ^{1.7}	5.3
+50		01.6	96.0 ^{1.6}	5.6
81~		01.3	95.7 ^{1.3}	5.6
+50		00.9	95.3 ^{0.9}	5.6
82~		00.6	94.9 ^{0.6}	5.7
+50		00.4	94.5 ^{0.4}	5.9
83~	0.41	00.4	94.1 ^{0.4}	6.3
+51.5	Brk.	00.6	93.7 ^{0.6}	6.9
+70	Brk.	00.6	93.7 ^{0.6}	6.9
84~		00.7	94.3 ^{0.7}	6.4
+50		00.8	95.2 ^{0.8}	5.6
85~	Brk.	01.0	96.1 ^{1.0}	4.9
+50		01.3	96.3 ^{1.3}	5.0
86~		01.6	96.6 ^{1.6}	5.0
+50		01.9	96.8 ^{1.9}	5.1
87~		02.0	97.1 ^{2.0}	4.9
+50		02.3	97.3 ^{2.3}	5.0
88~		02.6	97.5 ^{2.6}	5.1

					Stake	Grade	cut.
88+50	02.8	97.8	5.0	97+00	- Brk 08.6	8.6 99.0	9.6
89~	03.0	98.0	5.0	+50	09.7	09.7 99.0	10.7
+50 3-15	03.1	98.3	4.8	98-	08.8	8.8 99.1	9.7
90~ Brk	03.4	98.4	4.9	+50	06.4	6.4 99.1	7.3
+50	03.6	98.5	5.1	99~	05.4	5.4 99.1	6.3
91~	04.1	98.6	5.5	+50	03.3	3.3 99.2	4.1
+50	04.4	98.6	5.8	100~	04.5	4.5 99.2	5.3
92-	04.7	98.6	6.1	+50	06.2	6.2 99.2	7.0
+50	05.0	98.7	6.3	01~	08.3	8.3 99.3	9.0
93~	05.1	98.7	6.4	+50	10.5	10.5 99.3	11.2
+50	05.3	98.7	6.6	02~	12.3	12.3 99.4	12.9
94+01 = 1/8 Bend. - 8' rt.	05.4	98.8	6.6	+50	11.8	11.8 99.4	12.4
	8' rt.			03~	08.4	8.4 99.4	9.0
94+21.90 = 1/16 Bend.	05.8	98.8	7.0	+50	07.6	7.6 99.5	8.1
94+44.63 } Tunnel	05.5	98.9	6.6	04~	06.0	6.0 99.5	6.5
+92.63 }	06.3	98.9	7.4	+50	05.2	5.2 99.5	5.7
95+19.63 } Tunnel	05.9	98.9	7.0	05~	05.5	5.5 99.6	5.9
+67.63 }	06.3	98.9	7.4	+50	07.2	7.2 99.6	7.6
96+00	06.2	98.9	7.3	06~ T.P. 8.98	09.0	9.0 99.6	9.4
+50	06.6	99.0	7.6	+50	09.7	9.7 99.7	10.0

107 ~	10.4	$\frac{10}{99.7}$	10.7
+50	11.9	$\frac{11.9}{99.7}$	12.2
108 ~	12.9	$\frac{12.9}{99.5}$	13.1
+50	11.8	$\frac{11.8}{99.5}$	12.0
09 ~	10.4	$\frac{10.4}{99.8}$	10.6
+23 = Cross	10.0	$\frac{10.0}{99.9}$	10.1
+50	09.5	$\frac{09.5}{99.9}$	9.6
10 ~	08.3	$\frac{08.3}{99.9}$	8.4
+50	07.5	$\frac{07.5}{99.9}$	7.6
11 ~	06.7	$\frac{06.7}{100.0}$	6.7
+50 = Brk	06.8	$\frac{06.8}{100.0}$	6.8
12 ~	07.9	$\frac{07.9}{100.5}$	7.4
+50	08.6	$\frac{08.6}{100.9}$	7.7
13 ~	09.3	$\frac{09.3}{101.4}$	7.9
+50	09.8	$\frac{09.8}{101.8}$	8.0
14 ~	10.1	$\frac{10.1}{102.3}$	7.8
+50	10.4	$\frac{10.4}{102.7}$	7.7
15 ~	10.8	$\frac{10.8}{103.2}$	7.6
+50	11.2	$\frac{11.2}{103.6}$	7.6
16 ~	11.5	$\frac{11.5}{104.1}$	7.4
+50	11.4	$\frac{11.4}{104.5}$	6.9

117 ~ Brk	12.2	$\frac{12.2}{122}$	7.2
+50	13.4	$\frac{13.4}{124}$	8.1
18 ~	13.8	$\frac{13.8}{124}$	8.3
+50	13.8	$\frac{13.8}{124}$	8.0
19 ~	14.0	$\frac{14.0}{124}$	8.0
+50	15.0	$\frac{15.0}{124}$	8.7
20 ~	15.0	$\frac{15.0}{124}$	8.5
+50	15.6	$\frac{15.6}{124}$	8.8
21 ~	15.9	$\frac{15.9}{124}$	8.9
+50	16.6	$\frac{16.6}{124}$	9.3
122 ~ ⁷¹⁰ Brk	17.1	$\frac{17.1}{124}$	9.6
+50	16.8	$\frac{16.8}{124}$	9.1
123 ~	16.1	$\frac{16.1}{124}$	8.3
+50	16.1	$\frac{16.1}{124}$	8.1
24 ~	15.7	$\frac{15.7}{124}$	7.5
+50	15.7	$\frac{15.7}{124}$	7.4
25 ~	15.3	$\frac{15.3}{124}$	6.8
+50	15.0	$\frac{15.0}{124}$	6.3
26 ~	14.7	$\frac{14.7}{124}$	5.9
+50	14.2	$\frac{14.2}{124}$	5.2

127 ~	14.4	0 ^{4.4} _{9.2}	5.2
+50	14.4	0 ^{4.4} _{9.3}	5.1
128 ~ Brk	14.3	0 ^{4.3} _{9.5}	4.8
+43.32 = $\frac{1}{8}$ Bend.	13.8	0 ^{3.8} _{9.3}	4.5
+80	14.6	0 ^{4.6} _{9.1}	5.5
129 + 20	14.9	0 ^{4.9} _{8.8}	6.1
+58.32 = $\frac{1}{4}$ Bend.	13.7	0 ^{3.7} _{8.6}	5.1

INDEX

Set Grades for 12" Drain + Stilling
 Tank. - Plan - 2099-D
 W.O. 32323 10-13-53 7.01

0+00 = \pm Box in Gutter	27.57	26.00	- C 1.57
P.K. - 10' front on Line ^{To top}	27.57	28.50	F 0.93
10' Lt. - 0+00	28.53	26.00	C 2.53
0+35	29.81	26.17	C 3.64
+70	30.87	26.34	C 4.53
1+05	30.86	26.51	C 4.35
+40	31.00	26.68	C 4.32
+75	30.81	26.85	C 3.96
2+10	30.07	27.02	C 3.05
+43.55	30.10	27.19	C 2.91
+56.95 = at Box		27.30	

1-13-54
INDEXED

7.0.

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Lt. ± Rt.

Sections in Wash by Balboa + Morena
to show water quantities at Peak of Storm.
0+00 = RR Rail in E of wash - about 25' E
of Edge of Pavc. by Underpass

Seems to be Confined in Sewer ditch
about 350' upstream from 0+88 - Main body of water

61.6	60.4	59.1	56.2	56.4	56.6		60.4
8	5	3.7	3.5		2.5		3.8 = Top
							= H.W.

0+88 - Last good Section - over banks ahead.

55.0	54.1	52.4	52.3	52.0	52.0	53.0	54.1	54.8
8	5.3	4	3	2.6		5	7.3	11 - Top
Top	H.W.							

0+75

55.7	54.2	53.8	53.3	52.3	51.4	51.3	53.3	53.8	54.7
13.5	11.5	10	7	4.2		0.8	3.5	5	8 = Top
Top		H.W.			wetted perimeter			H.W.	

0+50

55.4	53.1	52.0	50.4	50.6	52.2	52.5	53.7
7	5.5	4.7		2	4.3	12	16
Top	H.W.					approx. H.W. in Heavy Grass	

0+25

54.0	51.7	51.2	50.5	49.0	49.0	50.2	50.7	51.1	51.7	53.5
9	8	5	1		2.8	5	6	8	14.3	18.6
Top	H.W.								H.W.	Top

0+00

52.2	50.9	48.3	48.3	48.5	49.0	50.9	51.7
7.4	6	3		2	4.2	5.1	Est. High
Top of	H.W.						water Mark
Bank	Mark						Top of

B.M. = + on Rim of Sewer M.H.
± Balboa + Morena

52.56

Actual Elev. Shown. Section going upstream

INDEXED

 Sewer - wly. Muirlands -
 Plan - 2225 - D = 1-17-54
 W.O. 21075

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	Stake	Grade	cut.				
				1+45.15 = M.H. 4	97.51	7.51 92.35	5.16
0+00 = Exist M.H.	73.43	73.43 64.11	C 9.32	0+35	97.71	7.71 92.49	5.22
				+70	98.78	8.78 92.63	6.15
0+39.80 = M.H. 1	74.98	74.98 68.00	6.98	1+05	98.50	8.50 92.77	5.73
0+35	78.84	8.84 73.50	5.34	+40	96.81	6.81 92.91	3.90
+70	83.96	83.96 79.00	4.96	+62.62 = M.H. 5	96.13	6.13 93.00	3.13
1+05	89.54	9.54 84.50	5.04	0+35	96.95	6.95 95.24	1.71
+27.11 = M.H. 2	45 Rt. 10 Rt. 93.85 94.43	5.85 88.00	6.43	+75	99.28	9.28 97.80	1.48
0+35	97.20	7.20 88.42	8.78	1+05	03.74	3.74 99.72	4.02
+70	99.24	9.24 88.84	10.40	+40	06.89	6.89 01.96	4.93
1+05	00.52	00.52 89.26	11.26	+71.97 = M.H. 6	08.35	8.35 04.00	4.35
+40	02.18	2.18 89.68	12.50	0+35-36	12.79	12.78 05.15	7.63
+75	04.46	4.46 90.10	14.36	+70-27	14.60	14.60 06.30	8.30
2+10	02.50	2.50 90.52	11.98	1+05-3	16.11	16.11 07.45	8.66
+45	01.60	1.60 90.94	10.66	+40-45	18.67	18.67 08.60	10.07
2+80	00.52	00.52 91.36	9.16	+75-46	18.64	18.64 09.75	8.89
3+14.90 = M.H. 3	99.36	9.36 91.77	7.59	2+00-45	18.56	18.56 10.57	7.99
0+35	98.91	8.91 91.91	7.00	+25.38 = M.H. 7	18.93	18.93 11.40	7.53
+75	98.67	8.67 92.07	6.60	0+35	17.62	7.62 11.57	6.05
1+05	98.71	8.71 92.19	6.52	+70	15.64	5.64 11.75	3.89

1+05		14.36	⁴³⁶ 11.92	2.44	0+27	65.69	^{65.69} 58.65	7.04
+40		14.53	^{4.53} 12.10	2.43	+64.27	67.19	^{7.19} 61.27	5.92
+75		16.03	^{6.03} 12.27	3.76	1+01.54=P.C.C	69.86	^{9.86} 63.89	5.97
2+10		17.17	^{7.17} 12.45	4.72	+33.76	72.83	^{72.83} 66.15	6.68
+45-4'rt		15.64	^{5.64} 12.62	3.06	+65.98=M.H. 11	75.40	^{75.40} 68.40	7.00
+80		17.85	^{7.85} 12.80	5.05	0+32.22	78.21	^{8.21} 70.95	7.26
3+14.13=M.H.8		24.20	^{24.20} 12.97	11.23	+64.44=P.R.C.	80.12	^{80.12} 73.50	6.62
0+35		24.06	^{24.06} 15.60	8.46	+97.85	82.72	^{82.72} 76.14	6.58
+70		25.80	^{25.80} 18.23	7.57	1+31.26	85.53	^{85.53} 78.78	6.75
1+05-4'rt		27.79	^{7.79} 20.86	6.93	+64.67	87.96	^{7.96} 81.42	6.54
+40		29.71	^{9.71} 23.49	6.22	+84.67=M.H.12	89.45	^{9.45} 83.00	6.45
+75		31.86	^{31.86} 26.12	5.74	0+35	91.91	^{91.91} 84.63	7.28
2+09.8L=M.H.9	6.61 Diag.	36.28	^{36.28} 28.75	7.53	+70	94.01	^{94.01} 86.26	7.75
	4.84 ahead	37.18	^{37.18} 28.75	8.43	1+05	95.45	^{95.45} 87.89	7.56
0+35		44.08	^{44.08} 34.71	9.37	+40	96.78	^{96.78} 89.52	7.26
+70		51.40	^{51.40} 40.67	10.73	+75	98.03	^{8.03} 91.15	6.88
1+05		58.22	^{58.22} 46.63	11.59	2+10	98.93	^{8.93} 92.78	6.15
+39		63.93	^{63.93} 52.43	11.50	+45=P.C.	00.19	^{00.19} 94.42	5.77
+58.5		63.54	^{63.54} 55.75	7.79	+72.5	02.61	^{02.61} 95.71	6.90
+64.37=M.H.10		64.47	^{64.47} 56.75	7.72	3+00=M.H.13	04.75	^{04.75} 97.00	7.78

	stake						
0+34.92	08.46	^{8.46} 97.85	10.61	1+93.8 = M.H. 16	24.05	^{24.05} 04.97	19.08
+69.84	12.94	^{12.94} 98.70	14.24	0+30	24.16	^{24.16} 05.74	18.42
1+04.76	13.69	^{13.69} 99.55	14.14	+60	23.93	^{23.93} 06.51	17.42
1+39.68 - 4' Rt.	17.42	^{17.42} 00.40	17.42	+90	24.29	^{24.29} 07.27	17.02
1+74.60 - 4' Rt.	18.13	^{18.13} 01.25	16.88	1+20	23.92	^{23.92} 08.04	15.88
2+09.52	19.22	^{19.22} 02.10	17.12	+50	23.52	^{23.52} 08.80	14.72
2+51.87 M.H.#14	19.74	^{19.74} 03.13	16.61	+76 = M.H. 17	23.01	^{23.01} 09.46	13.55
0+35 - 4' Rt. Pin	20.70	^{20.70} 03.27	17.43	0+27	23.00	^{23.00} 09.57	13.43
+70 - 4' Rt Nail	21.84	^{21.84} 03.41	18.43	+54	22.69	^{22.69} 09.68	13.01
1+05	22.21	^{22.21} 03.55	18.66	+81	23.52	^{23.52} 09.79	13.73
+40	21.56	^{21.56} 03.69	17.87	1+08	23.21	^{23.21} 08.90	14.31
1+67.89 P.C.	21.97	^{21.97} 03.80	18.17	+35 = end.	22.52	^{22.52} 10.01	12.51
2+01.22	22.83	^{22.83} 03.93	18.90				
+34.55	22.14	^{22.14} 04.06	18.08				
2+67.89 = M.H. 15	22.63	^{22.63} 04.20	18.43				
0+35	22.83	^{22.83} 04.34	18.49				
+70	23.37	^{23.37} 04.48	18.89				
1+00	24.40	^{24.40} 04.60	19.80				
+30	24.38	^{24.38} 04.72	19.66				
+60	24.14	^{24.14} 04.84	19.30				

Beq. La Jolla Mesa Dr. + Line up side st.

529.73 = Pole by MH 21

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Drop MH. 15	Same PK.	22.51	22.51 15.75	6.76	2+80	40.27	40.27 32.40	7.87
0+05		22.51	22.51 15.77	6.74	3+15	41.86	41.86 34.29	7.57
+35		23.22	23.22 15.90	7.32	+40 = MH.23	43.20	43.20 35.64	7.56
+70		23.83	23.83 16.05	7.78	0+35	45.33	45.33 37.39	7.94
1+05		24.39	24.39 16.20	8.19	+70	47.09	47.09 39.14	7.95
+41 = MH.20		25.06	25.06 16.34	8.72	1+05	48.91	8.91 40.89	8.02
0+35		25.69	25.69 16.48	9.21	+40	50.63	50.63 42.64	7.99
+70		26.24	26.24 16.62	9.62	+75	52.39	52.39 44.39	8.00
1+05		26.75	26.75 16.76	9.99	2+10	54.16	54.16 46.14	8.02
+40		27.25	27.25 16.90	10.35	+45	55.79	55.79 47.89	7.90
+75		27.56	27.56 17.04	10.52	+80	57.48	57.48 49.64	7.84
2+10		27.85	27.85 17.18	10.67	3+15	59.32	59.32 51.39	7.93
+35 = MH.21	45 ft = w.	28.14	28.14 17.28	10.86	+40 = M.H.24	60.70	60.70 52.64	8.06
0+35		30.59	30.59 19.17	11.42	= End.			
+70		31.73	31.73 21.06	10.67				
1+05		32.66	32.66 22.95	9.71				
+40		33.87	33.87 24.84	9.03				
+75		35.30	35.30 26.73	8.57				
2+10		37.01	37.01 28.62	8.39				
+45		38.54	38.54 30.51	8.03				

Deq. Inspiration Dr. Line.

4.5' rt.

Nov. 0-01.5

M.H. 14 =

0 + 35'

+70

1 + 05'

+32.96 = P.C.

+60.02

+87.08

2 + 14.13 = E.C.

+53.56 = P.C.

+76.77

3 + 00 = M.H. 18

0 + 31.11

+56.11

+81.11

1 + 06.11

+31.11

+56.11

+81.11

2 + 06.11

19.53

20.34

21.22

22.68

24.26

25.77

27.30

28.80

30.55

31.27

31.70

32.37

32.74

32.84

33.03

32.98

32.94

32.77

32.47

9.53

13.68

20.34

14.12

21.22

14.54

22.68

14.96

24.26

15.30

25.77

15.62

27.30

15.94

28.80

16.26

30.55

16.73

31.27

17.01

31.70

17.30

32.37

17.42

32.74

17.52

32.84

17.62

33.03

17.72

32.98

17.82

32.94

17.92

32.77

18.02

32.47

18.12

5.85

6.22

6.68

7.72

8.96

10.15

11.36

12.54

13.82

14.26

14.40

14.95

15.22

15.22

15.31

15.16

15.02

14.75

14.35

2 + 31.11

+56.11

+81.11

3 + 00 = M.H. 19

0 + 32.52

+65.05 = E.C.

+97.52

1 + 30 = Plug.

32.00

31.43

30.82

30.39

29.32

28.12

26.66

24.86

32.00

18.22

31.43

18.32

30.82

18.42

30.39

18.56

29.32

18.63

28.12

18.76

26.66

18.89

24.86

19.02

13.78

13.11

12.40

11.89

10.69

9.36

7.77

5.84

La Jolla Mesa Dr. - M.H. 21 to Conn.

39

0+00 = M.H. 21	28.14	28.14 17.28	10.86
+33	28.39	28.39 17.41	10.98
+66	28.61	28.61 17.54	11.07
+99	28.86	28.86 17.67	11.19
1+32	29.22	29.22 17.81	11.41
+65	29.70	29.70 17.94	11.76
+98	30.23	30.23 18.07	12.16
2+31	30.72	30.72 18.20	12.52
+64	31.19	31.19 18.34	12.85
+97	31.67	31.67 18.47	13.20
3+33 = M.H. 22	32.15	32.15 18.61	13.54
0+27	32.55	32.55 18.72	13.83
+54	32.99	32.99 18.83	14.16
+81 = Conn. to Exist. 8"	33.43	33.43 18.95	14.48

INDEXED

Rough Grade stakes - Mendocino St.
Plan - 2169-D - 4-12-54 - 70.
W.O. 32095

	West.		
N.L. Uoltare			
0+00 =	77.31	77.50	
+41.7	78.7	^{8.7} 74.0	C 4.7
+86.7	73.2	^{3.2} 70.2	C 3.0
+26.7 2 B.	73.1	^{73.1} 67.3	C 5.8
+66.7	68.8	^{8.8} 65.4	C 3.4
2+06.7	67.4	^{7.4} 64.6	C 2.8
2+46.7	66.8	^{6.8} 64.4	C 2.4
+89.07 = B.C.	68.5	^{8.5} 64.1	C 4.4
3+34.29	66.7	^{6.7} 63.7	C 3.0
+79.51	67.8	^{7.8} 63.4	C 4.4
4+24.73	70.7	^{70.7} 63.2	C 7.5
+69.95	70.4	^{70.4} 64.2	C 6.2
5+15.17 = E.C.	68.2	^{8.2} 65.4	C 2.8
+68.99 = End.	68.4	^{8.4} 66.50	C 1.9

40

66.43 = Pole - end.

	East.		
7636	75.28	75.5	
	70.7	^{70.7} 72.4	F 1.7
	69.1	^{9.1} 68.8	C 0.3
	64.4	^{64.4} 66.1	F 1.7
	61.4	^{61.4} 64.6	F 3.2
	59.8	^{59.8} 63.5	F 3.7
	60.4	^{60.4} 63.2	F 2.8
	61.4	^{61.4} 62.9	F 1.5
	61.8	^{61.8} 62.6	F 0.8
	62.4	^{62.4} 62.3	C 0.1
	61.1	^{61.1} 62.0	F 0.9
	61.8	^{61.8} 63.2	F 1.4
	62.1	^{62.1} 64.5	F 2.4
	64.1	^{64.1} 66.0	F 1.9

Venice St. - Muir to Voltaire - see P. 40
for w.o.

96.25 = \square on wall - w. 1+00

41

west

East

to w.			
0+00 = N.L. Muir	06.0	^{6.0} 04.5	C 1.5
+50	94.8	^{8.8} 97.8	C 1.0
1+00	92.6	^{2.4} 91.1	C 1.5
+50	87.9	^{2.9} 84.5	C 3.4
+79.65		^{5.5}	
+89.65 = S.L. Voltaire	85.6	80.5	C 5.1
		✓ 79.83	

99.6	^{0.5} 97.5	F 4.9
94.8	^{4.8} 97.7	F 2.9
87.4	^{7.4} 90.9	F 3.5
82.7	^{2.7} 84.0	F 1.3
	78.77	

Long Branch to Muir

0+00 = N.L. Long Branch	34.3	^{4.3} 32.5	C 1.8
+50	28.6	^{8.6} 26.8	C 1.8
1+00	22.8	^{2.8} 21.1	C 1.7
+50	17.3	^{7.3} 15.4	C 1.9
+95	12.2	^{2.2} 10.3	C 1.9
2+15 = S.L. Muir	09.7	^{9.7} 08.3	C 1.4

121.34 = Pole J.P. 2131 on Rt.

Brighton to Long Branch.

151.35 = S.W.B.P. - Venice + Brighton

42

12.71

West

East.

0+00 = N.L. Brighton

50.68

+20

52.8

^{2.8}
50.0

C 2.8

End. cb.

50.94

50.90

+60

51.8

^{51.8}
48.6

C 3.2

49.4

^{9.4}
49.0

C 0.4

1+00

50.3

^{50.3}
46.2

C 4.1

46.0

^{46.0}
46.3

F 0.3

+40

45.2

^{5.2}
43.1

C 2.1

1+20 = end

44.58

44.54

+80

40.7

^{40.7}
39.2

C 1.5

2+15 = S.L. Longbranch

36.2

^{6.2}
35.80

C 0.4

Pole - S.W. Longbranch

136.23

INDEX

	West.		East.	
0+00 = NL. Voltaire	77.30	77.50	75.28	75.47
+29.57	75.42	75.00 ^{.42}	Co.42	0+68.7
+59.14	71.97	72.50 ^{1.97}	F0.53	+34.7
+88.70	70.34	70.30 ^{.34}	Co.34	+60.7
1+08.7	68.33	68.50 ^{.33}	F0.17	+86.7
+28.7	67.49	67.20 ^{.49}	Co.29	1+06.7
+36.83 = RC. - cb.	67.48	66.71 ^{.48}	Co.77	+26.7
E.C. = Alley	67.48	66.57 ^{.48}	Co.91	+46.7
+12.49 = End. - S.	66.28	66.30 ^{.49}	F0.02	+66.7
End - N.	66.48	65.50 ^{.48}	Co.98	+86.7
E.C. = Alley	64.97	65.38 ^{.47}	F0.41	2+06.7
1+73.70 = RC. - cb.	64.97	65.22 ^{.47}	F0.25	+36.7
+88.7	64.65	64.90 ^{.465}	F0.25	+68.4 RC. - cb.
2+08.7	64.62	64.60 ^{.62}	Co.02	E.C. Alley
+35.5	64.55	64.45 ^{.55}	Co.12	6- End. - S.
+62.3	64.37	64.25 ^{.37}	Co.12	BC-2489.1
+89.1 = RC.	64.53	64.53 ^{.53}	Co.46	End - N
3+12.1	64.42	63.89 ^{.42}	Co.53	11.88
3+35.1	64.37	63.72 ^{.47}	Co.65	E.C. Alley
				1042'30"
				3+05.05 RC. - cb.
				4°25'45"
				+30.46

		West		East
^{6°25'30"} 3+58.1		63.77	⁷⁷ 63.55 C0.22	^{7°09} 3+55.87 62.26 62.41 F0.15
^{8°34'} 3+81.11 = PC.		63.86	⁸⁶ 63.38 C0.48	^{9°52'} +81.28 62.48 62.23 C0.25
EC Alley		63.86	⁸⁶ 63.44 C0.42	^{12°35'15"} 4+06.69 = PC 62.56 62.56 C0.51
+6 = End. - S.		64.80	^{4.80} 63.56 C1.24	^{1/2} 62.16 61.80 C0.36
End - N.		63.66	⁶⁶ 63.40 C0.26	End 61.39 61.37
^{15°12'} 4+52.22 Ang. II	.55 High	65.28	^{5.28} 63.48 C1.80	N Ret.
^{17°38'} +78.3	.44 Hi	65.43	^{5.43} 64.11 C1.32	End 62.71 62.70
^{20°04'} 5+04.4	.57 Hi	65.63	^{5.63} 64.73 C0.90	^{1/2} 62.84 63.51 F0.67
^{22°30'} +30.56 = EC		65.67	⁶⁷ 65.36 C0.31	PC - Ret 63.35 64.14 F0.79
+55.97		66.22	^{6.22} 65.93 C0.29	^{+15' 1°36'30"} = EC 64.22 64.48 F0.26
+81.38 = end.		66.52	^{6.52} 66.50 C0.02	25.41 65.48 65.24 C0.24
				End 65.72 66.00 F0.28
				^{5.77}

Curb Stakes - Venice St. - Voltaire to Brighton.
 W.O. 32095 - 5-3-53 7.0
 108.55 = B.M. Sw. Pole

INDEX

West.

East.

Ength.	06.34	06.31		06.60	06.45 ⁶⁰	C 0.15
1/3	06.34	05.84 ^{6.34}	C 0.50	06.12	06.00 ¹²	C 0.12
2/3	05.69	05.20 ^{5.69}	C 0.49	04.67	05.30 ^{4.67}	F 0.63
N.L. Muir tow. P.C. = 0+00 =	04.71	04.50 ⁷¹	C 0.21	04.22	04.50 ²²	F 0.28
+30	00.55	00.48 ⁵⁵	C 0.07	00.23	00.41 ²³	F 0.18
+60	96.80	96.47 ⁸⁰	C 0.33	96.02	96.32 ⁰²	F 0.30
+90	93.23	92.46 ^{3.23}	C 0.77	92.32	92.23 ³²	C 0.09
1+20	91.21	88.45 ^{91.21}	C 2.76	88.35	88.14 ³⁵	C 0.21
+50	88.14	84.44 ^{8.14}	C 3.70	84.17	84.05 ¹⁷	C 0.12
+79.65	85.71	80.49 ^{5.71}	C 5.22	80.00	80.00	G.
+89.65 = Meet.	79.90	79.83		78.86	78.77	

Long Branch to Muir.

End.	34.29	34.31		1+40	16.31	16.56 ³¹	F 0.25
1/3	34.04	33.70 ^{4.04}	C 0.34	+75	12.22	12.58 ²²	F 0.36
2/3	34.25	33.10 ^{4.25}	C 1.15	+95	10.04	10.30 ⁰⁴	F 0.26
N.L. Long branch P.C. = 0+00 =	33.47	32.50 ^{3.47}	C 0.97	2+15 = P.C. =	08.26	08.30 ²⁶	F 0.04
+35	29.52	28.52 ^{9.52}	C 1.00	1/3	07.99	07.76 ⁹⁹	C 0.23
+70	25.55	24.53 ^{5.55}	C 1.02	2/3	07.69	07.37 ⁶⁹	C 0.32
1+05	21.93	20.55 ^{1.93}	C 1.38	Meet.		107.38	

Brighton to Long branch.

151.35 = S.W. BP. Brighton + Venice

46.

136.25 = S.W. Pole Long branch.

West

East

0+00 = NL Brighton

50.68

51.50

+20

52.39

^{2.39}
50.00

C 2.39

50.95

50.90

+40

52.08

^{52.08}
49.35

C 2.73

49.91

50.00

F 0.09

+60

51.55

^{51.55}
48.60

C 2.95

48.64

48.95

F 0.31

+80

50.53

^{50.53}
47.57

C 2.96

46.44

47.70

F 1.26

1+00

49.45

^{9.45}
46.23

C 3.22

45.28

46.25

F 0.97

+20

46.71

^{46.71}
44.72

C 1.99

1+19.56 = Meet.

44.54

+40

44.48

^{4.48}
43.05

C 1.43

+65

42.78

^{2.78}
40.64

C 2.14

+90

39.99

^{9.99}
38.22

C 1.77

5L Long branch

2+15 = P.C.

35.77

35.80

F 0.03

1/3

35.49

⁴⁹
35.35

C 0.14

2/3

35.45

⁴⁵
35.20

C 0.25

Meet

41

35.41

Opal + Dawes

Sewer Stakes - N. Muirlands
 Plan - 2327-29-D - 4-28-54
 Book - 2275 w.o. 21152

7.0

284.19 = B.P. in S. cb. by M.H. 2
 316.85 = end cb. on S. By F.H.
 324.36 = D on W cb.

47

INDEXED

Conn.	242.94			0+90	89.78	89.78 83.34	6.44
0+00 = Sub. Line	53.13	53.13 49.51	9.62	1+20	91.72	91.72 85.32	6.40
+30	55.17	55.17 46.91	8.26	+50	93.70	93.70 87.30	6.40
+60	57.79	57.79 50.31	7.48	+80	95.65	95.65 89.28	6.37
0+90.69 = M.H. 1	59.75	59.75 53.80	5.95	2+10	97.61	97.61 91.26	6.35
1+25	62.12	62.12 56.51	5.61	+40	99.57	99.57 93.24	6.33
+50	63.97	63.97 58.46	5.51	+70	01.49	01.49 95.22	6.27
+75	65.84	65.84 60.41	5.43	3+00 = M.H. 3	03.36	03.36 97.20	6.16
2+02.78 = P.R.C.	68.06	68.06 62.58	5.48	0+20.83 = P.C.	04.57	04.57 97.64	6.93
+25	69.83	69.83 64.31	5.52	+50	06.19	06.19 98.29	7.90
+50	71.88	71.88 66.26	5.62	+80	07.82	07.82 98.96	8.86
+75	73.97	73.97 68.21	5.76	1+10	09.47	09.47 99.62	9.85
3+00	76.10	76.10 70.16	5.94	+40	11.09	11.09 00.29	10.80
+25	78.16	78.16 72.11	6.05	+70	12.70	12.70 00.95	11.75
+50	80.18	80.18 74.06	6.12	2+02.89 = P.R.C.	14.30	14.30 01.68	12.62
+75	82.16	82.16 76.01	6.15	+35	16.21	16.21 02.40	13.81
+92.87 = P.C. M.H. 2	83.49	83.49 77.40	6.09	+68 = E.C.	17.95	17.95 03.13	14.82
0+30	85.65	85.65 79.38	6.27	3+00	19.72	19.72 03.85	15.87
+60	87.77	87.77 81.36	6.41	+31.09 = M.H. 4	21.50	21.50 04.54	16.96
				0+35	23.22	23.22 04.64	18.58

0+70	25.27	04.75	20.52	2+95	50.90	50.90 45.25	5.65
1+05	27.65	^{27.65} 04.85	22.80	3+30.	52.63	52.63 47.36	5.27
+40	29.63	^{29.63} 04.96	24.67	+60 = M.H. 8	54.18	54.18 49.17	5.01
+75	31.10	^{31.10} 05.06	26.04	0+35	55.88	55.88 51.03	4.85
+95 = M.H. 5	31.99	^{31.99} 05.12	26.87	+70	57.61	57.61 52.89	4.72
Beg. Line up Muirlands Dr.				1+05	59.60	59.60 9.60	4.85
0+00 = M.H. 5		305.12		+30	60.90	60.90 56.08	4.82
+10	32.23	07.12	25.11	+55	62.38	62.38 57.41	4.97
+45	34.50	14.12	20.38	+80	63.69	63.69 58.74	4.95
+80	37.08	^{37.08} 21.12	15.96	2+05	65.11	5.11 60.07	5.04
1+08.15	38.93	26.75	12.18	+30	66.60	6.60 61.40	5.20
+30	40.27	31.12	9.15	+50	67.87	7.87 62.46	5.41
+40	40.95	32.92	8.03	+70	69.09	9.09 63.52	5.56
+50	41.69	34.52	7.17	+90	70.47	64.58	5.89
+60	42.27	35.92	6.35	+96.57 = Ang.	70.89	64.94	5.95
+70	42.91	37.12	5.79	3+25	72.94	66.48	6.46
+80	43.55	38.12	5.43	+53 = M.H. 9	74.79	74.79 68.00	6.79
+90	44.23	38.92	5.31	Beg. Line to S	76.43	8.43	8.43
2+25	46.53	41.03	5.50	0+00 = M.H. 9		68.00	
+60	48.79	43.14	5.65	+14.12	74.63	74.63 68.97	5.66

85.33 = □ on Cor. of Dr.

Beg. Line in Camino Del Cañon

49

0+29.24 75.01 75.01 69.94 5.07

+42.36 = P.R.C. 76.08 7.08 70.92 6.16

+75 77.97 7.97 73.17 4.80

1+00 79.34 9.34 74.89 4.45

+25 81.21 81.21 76.62 4.59

+50 83.10 83.10 78.34 4.76

+75 85.14 5.14 80.97 5.07

2+00 87.25 7.25 81.80 5.45

+15 = Plug. 88.54 8.54 82.84 5.70

Beg. Line up Muirlands Dr. from M.H. 9

0+00 = M.H. 9 68.00

+25 75.07 75.07 69.80 5.27

+50 = Ang. Pt. 76.37 6.37 71.60 4.77

+80 78.30 8.30 73.76 4.54

1+10 = Ang. Pt. 80.66 80.66 75.92 4.74

+45 83.50 83.50 78.44 5.06

+80 86.33 6.33 80.96 5.37

2+15 89.20 9.20 83.48 5.72

+52.51 = M.H. 10 92.23 92.23 86.18 6.05

Set B.M. = Rock above M.H. 10 = 394.55

0+00 = M.H. 5

+35 32.08 32.08 05.22 26.86

+70 27.24 27.24 05.33 21.91

1+05 26.73 26.73 05.43 21.30

+40 27.95 27.95 05.54 22.41

+75 27.64 27.64 05.64 22.00

2+10 25.61 25.61 05.75 19.86

+45 22.90 22.90 05.85 17.05

+76.20 = M.H. 6 22.19 22.19 05.95 16.24

0+30 21.19 21.19 06.04 15.15

+60 20.00 20.00 06.13 13.87

+90 18.47 18.47 06.22 12.25

1+20 17.21 17.21 06.31 10.90

+50.96 = P.C. 16.52 16.52 06.40 10.12

+72.79 17.16 17.16 06.46 10.70

+94.62 17.57 17.57 06.53 11.04

2+16.45 17.66 17.66 06.59 11.07

+38.29 = E.C. 17.28 17.28 06.66 10.62

= 15.51 15.51 06.72 9.87

+70 16.62 16.62 06.75 9.87

3+00	15.64	^{15.64} 06.84	8.80
+30	14.19	^{14.19} 06.93	7.26
+50 = M.H. 7	14.00	^{14.00} 07.00	7.00
0+35	13.64	^{13.64} 07.10	6.54
+68.4 = Plug.	19.55	^{19.55} 07.21	12.34

INDEXED

51
 Alley - Blk. 45 - Herberts sub.
 Plan - 10939-L - 5-17-54 - 70.
 0.25 excepted. on Sides w.o. 32307

377.57 = Pole at Int

51

E. + W. Alley

North

South

0+00 = E.L. 37^{1/2}

376.67

376.53

+20

77.35 ^{7.35} 76.43 C0.92

77.85 ^{7.85} 76.31 C1.54

+55

77.24 ^{7.24} 76.03 C1.21

76.76 ^{6.76} 75.93 C0.83

+90

76.44 ^{6.44} 75.63 C0.81

76.19 ^{6.19} 75.55 C0.64

1+18

75.94 ^{5.94} 75.31 C0.63

75.74 ^{7.74} 75.25 C0.49

+25 = W.L.N. Alley

75.82 ^{5.82} 75.23 C0.59

+40 = E.L.

75.90 ^{5.90} 75.06 C0.84

+47

75.72 ^{5.72} 74.98 C0.74

75.59 ^{5.59} 74.94 C0.65

+80

74.77 ^{7.77} 74.60 C0.17

74.72 ^{4.72} 74.58 C0.14

2+00

74.65 ^{4.65} 74.41 C0.24

74.48 ^{4.48} 74.40 C0.08

+20

74.48 ^{4.48} 74.27 C0.21

74.58 ^{4.58} 74.27 C0.31

+425

74.36 ^{4.36} 74.16 C0.20

74.75 ^{4.75} 74.15 C0.60

2+65 = W.L.M. = Clintock

^{74.35 top}
 74.05

^{74.35 top}
 74.03

N. + S. Alley

382.05 = Pole by Meade

52

West

East

	West	East
0 + 00 = N.L. E. + W. Alley	75.82 ⁸² 75.23 Co. 59	75.90 ⁹⁰ 75.06 Co. 84
+ 07	75.87 ⁸⁷ 75.48 Co. 39	75.82 ⁸² 75.33 Co. 49
+ 37	76.09 ⁰⁹ 75.69 Co. 40	75.87 ⁸⁷ 75.54 Co. 33
+ 67	77.03 ⁰³ 75.91 Co. 12	76.16 ¹⁶ 75.76 Co. 40
+ 97	77.03 ⁰³ 76.12 Co. 91	76.16 ¹⁶ 75.97 Co. 19
1 + 27	76.47 ⁴⁷ 76.34 Co. 13	76.48 ⁴⁸ 76.19 Co. 29
+ 57	77.17 ¹⁷ 76.55 Co. 62	76.51 ⁵¹ 76.41 Co. 10
+ 90	77.12 ¹² 76.80 Co. 32	76.75 ⁷⁵ 76.65 Co. 10
2 + 10	76.94 ⁹⁴ 77.00 Fo. 06	77.01 ⁰¹ 76.85 Co. 16
+ 30	77.69 ⁶⁹ 77.27 Co. 42	77.25 ²⁵ 77.12 Co. 13
+ 60 = T.P.	77.88 ⁸⁸ 77.74 Co. 14	77.45 ⁴⁵ 77.59 Fo. 14
+ 90	78.25 ²⁵ 78.21 Co. 04	78.31 ³¹ 78.06 Co. 25
3 + 20	78.87 ⁸⁷ 78.69 Co. 18	79.06 ⁰⁶ 78.53 Co. 53
+ 50	79.09 ⁰⁹ 79.16 Fo. 07	79.16 ¹⁶ 79.01 Co. 15
+ 70	79.65 ⁶⁵ 79.48 Co. 17	79.06 ⁰⁶ 79.27 Fo. 21
+ 90	80.44 ⁴⁴ 79.69 Co. 75	79.45 ⁴⁵ 79.40 Co. 05
4 + 10	80.65 ⁶⁵ 79.71 Co. 94	79.35 ³⁵ 79.40 Fo. 05
+ 30	80.01 ⁰¹ 79.54 Co. 47	79.52 ⁵² 79.15 Co. 37
+ 50.2 = S.L. Meade	79.17 ¹⁷ .13	78.76

INDEX

Stake Drain - Logan + Euclid
 5271-B. - Book 1879-P.60
 W.O. 3064 - 6-7-54 - 7.0.

NOV

= 0+39.25 on Plan.

5' x 6' Box Culvert. ^{= cut in wall}

0+00 = Disk at $\frac{1}{2}$ of Inlet 10.02 04.02 - C 6.00

+14.70 = Cross - 5' rt. 03.78 04.13 F 0.35

+50 - stake - 5' rt. 06.66 04.78 C 1.88

+85 " 08.75 05.43 C 3.32

1+20 " 12.62 06.08 C 6.54

+55' - 8' rt. 19.44 06.73 C 12.75

+90 - 7' rt. 20.51 07.38 C 13.13

2+25 - 5' rt. 17.53 08.03 C 9.50

+60 - 10' rt. 17.18 08.68 C 8.50

+95 - 10' rt = Cross 23.77 09.33 C 14.44

3+25 - 10' rt. 24.38 09.88 C 14.50

+49.63 = Cross on Wall ^{on $\frac{1}{2}$} 15.83 10.34 C 5.49

+51.87 = end 10.37

Not Staked

B.M. B.P. in Headwall -

111.32

53

INDEX
 Staken Sewer-
 2403-D
 W.O. 21087

E.S.D. Park + Rec Center.
 - 5-9-54 - 7.0.

369.26 = P.C. ct.

372.82 = Pole 54
 orange

			2+80	55.55	50.55	C 4.96
			2+15	55.25	50.75	C 4.52
0+00 = M.H. 13	48.15	48.15	+50	54.92	50.87	C 4.05
+35	45.97	42.57	+75	54.77	50.97	C 3.80
+70	48.34	42.37	+94.86 = M.H. 2	54.67	51.05	C 3.62
1+05	54.43	44.18	0+25	54.74	51.19	C 3.55
+40	60.00	44.98	+70	54.74	51.33	C 3.41
+75	64.41	45.79	1+05	55.09	51.47	C 3.62
2+10 - 8' Lt	69.04	46.59	+39.81	57.64	51.61	C 6.03
+45 - 5' Rt	70.28	47.40	+49.81	62.43	51.79	C 10.64
+80	70.33	48.20	+59.81	67.61	52.21	C 15.40
3+20.33 = st. b. to w.	67.75	49.12	+69.81	71.95	53.02	C 18.93
3+35.33 = M.H. 1	66.63	49.47	+79.81	71.80	54.06	C 17.74
0+35	64.59	49.61	+89.81	71.39	55.39	C 16.00
+70	56.77	49.75	+99.81	70.94	57.01	C 13.97
1+05	56.90	49.89	2+20	71.02	60.56	C 10.46
+40	56.69	50.03	+39.59 = Plug.	71.21	64.00	C 7.21
+75	56.31	50.17				
2+10	55.90	50.31				
+45	55.64	50.45				

Req. Lat. 4" to Rest Room.

0+00 = 3+20.33 on Mainline	67.75	67.75 55.76 C 11.99
+35	67.15	67.15 56.46 C 10.69
+70	65.95	65.95 57.16 C 8.79
1+05	64.72	64.72 57.86 C 6.86
+40	64.15	64.15 58.56 C 5.59
+62.2 plug.	63.85	63.85 59.00 C 4.85

Stake Sewer in Orange Ave
 Plan - 2547-D - W.O. 62380 - 6-18-54 - 70.

INDEXED

To E.

372.92 = Pole by M.H. 1

56

0+00 = M.H. 1	70.96	^{70.96} 364.00	C 6.96	0+35	71.65	^{71.65} 65.54	C 6.11
+35 - 4' t.	70.48	^{70.48} 64.35	C 6.13	+70	72.64	^{72.64} 67.08	C 5.56
+70	70.14	^{70.14} 64.70	C 5.44	1+05	73.71	^{73.71} 68.63	C 5.08
1+05	70.09	^{70.09} 65.05	C 5.04	+40	75.08	^{75.08} 70.17	C 4.91
+40	70.51	^{70.51} 65.40	C 5.11	+75	76.69	^{76.69} 71.72	C 4.97
+75	70.95	^{70.95} 65.75	C 5.20	2+10	78.79	^{78.79} 73.26	C 5.53
2+00 = M.H. 2	71.57	^{71.57} 66.00	C 5.57	+45	80.79	^{80.79} 74.81	C 5.98
0+35	73.15	^{73.15} 67.88	C 5.27	+80	82.30	^{82.30} 76.35	C 5.95
+70	75.45	^{75.45} 69.77	C 5.68	3+15	83.47	^{83.47} 77.90	C 5.57
1+05	77.85	^{77.85} 71.65	C 6.20	+40 = M.H. 4	84.26	^{84.26} 79.00	C 5.26
+40	80.31	^{80.31} 73.54	C 6.77				
+75	82.88	^{82.88} 75.42	C 7.46				
2+10	85.25	^{85.25} 77.31	C 7.94				
+35	86.81	^{86.81} 78.65	C 8.16				
+60 = M.H. #3	88.01	^{88.01} 80.00	C 8.01				

INDEXFD

Stake Curb + Pavc - Jelleff + Morena

Plan - 5373 - B. - W.O. 62386

7-1-54 7.0.

Curb Grades.

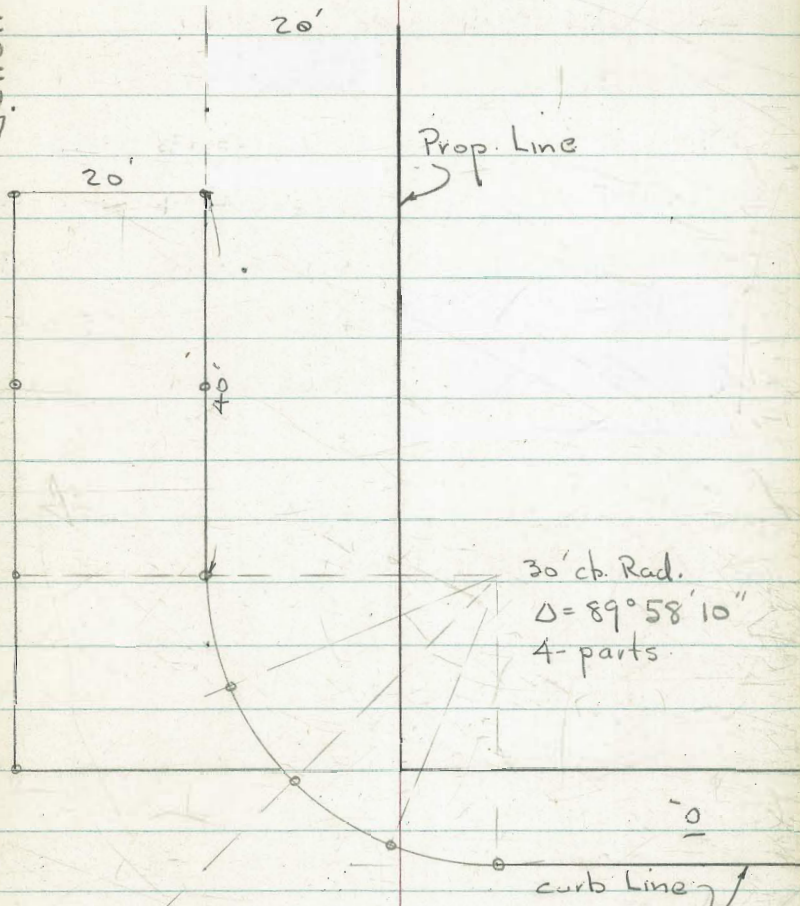
Grade

P.C. - on Morena	13.75	14.75 = F 1.00
1/4	14.74	14.88 F 0.14
1/2	15.19	15.12 C 0.07
3/4	15.52	15.47 C 0.05
E.C. = on Jelleff =	16.14	15.95 C 0.19
0+20	17.25	16.87 C 0.38
0+40 = end.	18.55	17.80 C 0.75

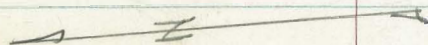
Pavc Grades.

E.L. Morena	15.41	15.20 C 0.21
opp. E.C.	16.60	16.20 C 0.40
0+20	17.64	17.12 C 0.52
0+40	18.61	18.05 C 0.56

Jelleff St.



Morena Blvd.



Stake cbs. - Thorn + Marlborough
 Plan - H212-L - 7-9-54 - 7.0.
 INDEXED 47

S.
 0+00 = W.L. Marlborough 301.10
 +35 - 3' Back 02.12 02.11 C 0.01
 +70 02.96 03.13 F 0.17
 1+05 03.96 04.14 F 0.18
 +38 = 2' Rad. 04.99 05.10 F 0.11
 To Alley 04.99 05.20 F 0.21
 PC. on Alley 04.99 05.44 C 1.22
 End at Prop. 2' Bk.

301.82 - N.W. B.P. Marlborough + Thorn. 58

N.

301.70
 02.31 02.69 F 0.38
 03.22 03.68 F 0.46
 04.21 04.67 F 0.46
 05.11 05.60 F 0.49
 05.11 05.70 F 0.59
 07.89 05.94 C 1.95

INDEXED

Grades - Ogden St. - Landis to

Wightman - Plan - 10974-5-L

NOV. 1, 1956

NOV. 1, 1956 - 7-12-54

351.12 - Pole

59

0+00 = opp. N.E. Cor. Shiloh & Ogden. - Bothways

To W.

South

North

0+00		53.8					
+49.34	54.4	^{4.4} 53.4	C 1.0				
+58.70 = P.C. on N.				53.9	^{3.9} 53.8	C 0.1	
+89.34	53.8	^{3.8} 52.7	C 1.1	53.8	^{3.8} 53.2	C 0.6	
1+29.34	53.1	^{53.1} 51.5	C 1.6	53.7	^{3.7} 52.0	C 1.7	
+69.34	51.7	^{51.7} 49.8	C 1.9	53.3	^{3.3} 50.3	C 3.0	
+89.34	50.6	^{50.6} 48.8	C 1.8	52.8	^{52.8} 49.3	C 3.5	
2+29.34	49.3	^{49.3} 46.6	C 2.7	49.7	^{49.7} 47.1	C 2.6	
+63.78 = End on S.	46.6	^{46.6} 44.9	C 1.7				
+65.64 = " on N.				47.3	^{7.3} 45.3	C 2.0	

E. of Shiloh Rd.	North			South			
0+00 = N.E. Cr. = ^{0+055 = PC.}	54.8	^{4.8} 54.30	C 0.5	54.6	^{4.6} 53.8	C 0.8	
+50	55.4	^{5.4} 54.6	C 0.8	55.2	^{5.2} 54.1	C 1.1	
1+00	55.5	^{5.5} 55.0	C 0.5	55.0	^{5.0} 54.5	C 0.5	
+50	55.7	^{5.7} 55.3	C 0.4	55.6	^{5.6} 54.8	C 0.8	
+95.83	55.9	^{5.9} 55.6	C 0.3	56.0	^{6.0} 55.1	C 0.9	
2+35.83	56.7	^{6.7} 55.7	C 1.0	55.8	^{5.8} 55.2	C 0.6	
+75.69	56.0	^{6.0} 55.5	C 0.5	56.2	^{6.2} 55.0	C 1.2	
3+14.87 = PC. on N.	55.7	^{5.7} 55.3	C 0.4	56.2	^{6.2} 54.8	C 1.4	
0+00 = End of Pavc	Top 4.97 Cut 4.50	54.87		= PC. 3+36.21	54.7		
+45	56.1	54.50	C 1.6	+72.09	^{6.2} 54.6	C 1.6	
+93.86	56.1	54.0	C 2.1	4+07.97	56.1	54.2	C 1.9
1+26.95	55.7	53.5	C 2.2	4+43.51 = PC.	55.1	53.4	C 1.7
Turnaround: 1+63.57 = B.C.	54.6	52.6	C 2.0	+73.31 = PC	53.4	52.6	C 0.8
81.95 = PC	53.8	52.1	C 1.7	5+08.31 = end	50.6	51.7	F 1.1
2+16.95 end	49.4	51.7	F 2.3				

INDEXED

grades - Landis St. E. of 37th
 Plan - 10850-L - Orig. grades in another Book
 W.O. 32110 - 7-16-54 - 70.

on South Side - at Alley

P.C. - on Landis 27.55 ^{7.55} 26.69 C 0.86

4' Rad.
 E.C. - on Alley 27.55 ^{7.55} 26.53 C 1.02

end - at S.L. on W. - 2' Bk. 29.93 ^{9.93} 26.85 C 3.08

end - S.L. on E. - 2' Bk. 26.36 ^{6.36} 25.95 C 0.41

P.C. - on Alley 25.69 ^{5.69} 25.40 C 0.29

4' Rad.
 E.C. on Landis 25.69 ^{5.69} 24.93 C 0.76

+21 = end G cb. 22.65 22.93 F 0.28

+23.25 = P.C. 7.35 Rad. 22.44 22.68 F 0.24

E.C. 22.11 22.34 F 0.23

+1.5 = end cb. 22.05 ^{2.05} 21.74 C 0.31

7' from E
 +13.5 = end spillway 20.87 ^{20.87} 19.94 C 0.93

N. Side

End. spillway ^{Grade} 21.48 ^{21.48} 19.94 C 1.54

P.C. 1' Rad. 22.38 ^{2.38} 21.74 C 0.64

E.C. 22.38 ^{2.38} 22.04 C 0.34

+3.5 = Beg. G cb. 22.44 ^{2.44} 22.17 C 0.27

+33.34 = P.C. 2' Rad. 22.86 ^{2.86} 23.35 F 0.49

E.C. -

23.10 23.51 F 0.41

= E.L. of Alley Prod.

24.67

INDEXED

Dr Sewer - Lot 40 - La Mesa Colony
 Plan - 11611-L - 7-16-54 7.0

Set BM in Pole By Wash Room - Trailer Park
 400.08

62

W.O. 62371

on Exist 15" UC.

0+00 = M.H. 1

+37.40

+47.40

+57.40

+67.40

+77.40

+87.40

+97.40

+20

+50

+77.40

+87.40

+97.40

2+07.40

+17.40

+27.40

+37.40

+63.69

+89.98 = M.H. 2

96.78

98.73

99.24

00.11

01.54

02.96 3

05.42 4

08.78

16.25

24.71

30.40

33.05

35.01

36.97

38.47

39.71

41.16

40.47

40.94

6.78

8.73

99.24

00.11

01.54

02.96

05.42

08.78

16.25

24.71

30.40

33.05

35.01

36.97

38.47

39.71

41.16

40.47

40.94

31.65

C 5.24

C 4.34

C 3.94

C 3.62

C 3.59

C 3.28

C 3.72

C 4.79

C 6.77

C 7.95

C 6.99

C 7.40

C 7.50

C 8.00

C 8.41

C 8.96

C 10.10

C 9.12

C 9.29

0+00 = M.H. 2

+12.42

+22.42

+32.42

+42.42

+52.42

+77.42 = Plug.

40.52

41.43

42.00

41.68

42.02

46.73

56.78

40.52

31.65

41.43

31.80

42.00

32.33

41.68

33.73

42.02

35.99

46.73

39.12

56.78

48.00

C 9.87

C 9.63

C 9.67

= 7.95

C 6.03

C 7.61

C 8.78

INDEX Grades - Ogden St. - 351.09 = Pole
 W.D. 22182 - Plan 10974-5-L - 7-28-54 - 70

63

SWish¹ to w.³

South

North

0+00 = N.E. Cor.

53.50 53.76 F 0.26

Meet. 53.86 53.90 F 0.04

+29.34

53.11 53.55 F 0.44

P.C. 53.83 53.84 F 0.01

+49.34

53.09 53.39 F 0.30

+58.70 = P.C. 53.76 53.75 C 0.01

+69.34

52.69 53.10 F 0.41

53.57 53.60 F 0.03

+89.34

52.25 52.70 F 0.45

53.22 53.20 C 0.02

1+09.34

51.75 52.16 F 0.41

52.67 52.66 C 0.01

+29.34

51.25 51.51 F 0.26

52.00 52.01 F 0.01

+49.34

50.87 50.73 C 0.14

51.10 51.23 F 0.13

+69.34

49.64 49.83 F 0.19

50.29 50.33 F 0.04

+89.34

48.87 48.81 F 0.24

49.41 49.31 C 0.10

2+29.34

46.17 46.64 F 0.47

46.98 47.14 F 0.16

+49.34

45.25 45.62 F 0.37

2+53 = B.C. 45.60 45.77 F 0.17

+63.71 = end.

44.73 45.00 F 0.27

= E.C. 45.32 45.40 F 0.08

Lat. (A)

50.86 50.86
42.77 C 8.09

Lat. (B)

53.88 53.58
45.30 C 8.28

Lat. (C)

53.70
47.18 C 6.52

Shiloh to E.

North

354.94 = Pole

64

Mect.	54.19	54.22			S.
0 + 05.05 = PC	54.30	54.30	G.		
+35	54.94	54.50 ⁹⁴	C0.44	+35	53.72 54.00 F0.28
+70	54.96	54.75 ⁹⁶	C0.21		53.87 54.25 ⁸⁷ F0.38
1 + 05	55.24	54.99 ²⁴	C0.25		54.14 54.49 ¹⁴ F0.35
+40	55.42	55.24 ⁴²	C0.18		54.41 54.74 ⁴¹ F0.33
+75	55.44	55.49 ⁴⁴	F0.03		54.54 54.99 ⁵⁴ F0.45
+9583	55.53	55.63 ⁵³	F0.10		54.71 55.13 ⁷¹ F0.42
2 + 15.83	55.64	55.70 ⁶⁴	F0.06		54.75 55.20 ⁷⁵ F0.45
+35.83	55.67	55.67	G		54.93 55.17 ⁹³ F0.24
+75.35	55.43	55.47 ⁴³	F0.04	+70.83	54.86 55.02 ⁸⁶ F0.16
3 + 14.87 = PC	55.27	55.27	G	3 + 05.83	54.56 54.87 ⁵⁶ F0.31
Mid. Pt.	55.43	55.35 ⁴³	C0.08	3 + 36.15 = BC. Prop.	
Mect.	55.53	55.50 ⁵³		3 + 43.87 = BC. cb.	54.53 54.70 ⁵³ F0.17
Lat ②	55.38	49.80 ³⁸	C5.58	1/4	54.43 54.60 ⁴³ F0.17
				1/2	53.62 54.44 ⁶² F0.82
				3/4	53.61 54.02 ⁶¹ F0.41
Lat ①	54.84	50.69 ⁸⁴	C4.15	E.C.	53.44 53.40 ⁴⁴ C0.04

Wightman - Ogden - To E.

65

N.

0 + 00 = Exist. cb.	54.95	54. ⁹⁵ 87	C 0.08
+ 27.7	54.60	54. ⁷⁰ 70	F 0.10
+ 60.8	54.39	54.37	C 0.02
+ 93.9	54.00	54.04	F 0.04
1 + 27	53.57	53. ⁵⁷ 49	C 0.08
+ 63.57 = B.C.	53.24	52. ²⁴ 63	C 0.61
+ 94.1 = P.R.C.	53.46	52. ⁴⁶ 40	C 1.06
1	53.58	52. ⁵⁸ 11	C 1.47
12	51.85	51.90	F 0.05
3	51.57	51. ⁵⁷ 75	F 0.18
4 = 1' Rad. - Top cb.	51.38	51. ³⁸ 70	F 0.32
End. of spillway - N. = ± Grade	50.85	49. ⁸⁵ 00	C 1.85
End. . S.	50.39	49. ³⁹ 00	C 1.39
1' Rad. - Top	51.12	51. ¹² 70	F 0.58
1	51.54	51.91	F 0.35
2	52.44	52. ⁴⁴ 30	C 0.14
3	53.69	52. ⁶⁹ 70	C 0.99
4 = P.R.C.	53.14	53. ¹⁴ 03	C 0.11

INDEXED
Comb Stakes - NE. Cor. Jellet + Morena
w.O. 20007 - 8-6-54 - 7.0.

+ in Signal base - By R.R. BM = 12.79

Extist. cb = P.C. of 30 Rad. - on Morena

Meet. ✓ 15.97

1/4 15.30 15.98₃₀ F 0.68

1/2 15.59 15.87₈₄ F 0.28

3/4 16.00 15.98₂₀ C 0.02

E.C. = on Jellet. 16.25 16.36₂₅ F 0.11

+35 17.85 17.98₈₅ F 0.13

+70 19.31 19.60₃₁ F 0.29

= Prop. Cor. = Hub
at Alley - on S. side 21.90 21.20₉₀ C 0.70

INDEX

Alley - Block 1 - Montecello
Plan - 11150 - L - W.O. 32226 - 9-14-54 - 7.0.

382.05 = Pole - Alley + Monroe

67

N ^o	West.	East.
Oteo = N.L. Monroe	281.01	81.17
+10 - 2' B.	82.72 ⁷² 82.01 C 0.71	83.43 ^{3.43} 82.10 C 1.33
+20	83.20 ^{2.20} 82.73 C 0.47	83.91 ^{3.91} 82.77 C 1.14
+30	83.11 ^{3.11} 82.18 F 0.07	84.04 ^{4.04} 83.19 C 0.85
+40	83.01 ^{3.01} 83.35 F 0.34	84.42 ^{4.42} 83.35 C 1.07
+75	83.43 ^{4.43} 83.44 F 0.01	83.52 ^{5.2} 83.44 C 0.08
+110	83.34 ^{3.34} 83.53 F 0.19	84.10 ^{4.10} 83.53 C 0.57
+45 - 1.01 B.	83.93 ^{3.93} 83.62 C 0.31	84.07 ^{4.07} 83.62 C 0.45
+80	83.90 ^{9.0} 83.11 C 0.19	83.86 ^{8.6} 83.71 C 0.15
+90	83.88 ^{8.8} 83.76 C 0.12	84.19 ^{4.19} 83.76 C 0.43
2 + 00 - 1.75' B.	84.27 ^{4.27} 83.85 C 0.42	83.97 ^{9.7} 83.85 C 0.12
+35 - 1.68' B.	84.93 ^{9.3} 84.23 C 0.70	0.25 B. 84.63 ^{6.3} 84.23 C 0.40
+70 - 1.45' B.	85.01 ^{5.01} 84.61 C 0.40	84.94 ^{9.4} 84.61 C 0.33
3 + 05 .	85.52 ^{5.2} 85.00 C 0.52	3' B. 85.07 ^{5.07} 85.00 C 0.07
+40 - 1' B.	85.93 ^{9.3} 85.38 C 0.55	85.73 ^{7.3} 85.38 C 0.35
+75	86.54 ^{6.54} 85.76 C 0.78	0.65 B. 86.33 ^{6.33} 85.76 C 0.57
4 + 10 - 1.10' B.	87.96 ^{7.96} 86.14 C 1.82	0.60 B. 87.23 ^{7.23} 86.14 C 1.09
+45 - 0.50' B.	88.10 ^{8.10} 86.53 C 1.57	0.65 B. 87.32 ^{7.32} 86.53 C 0.79
+80 - 0.73' B.	87.33 ^{7.33} 86.91 C 0.42	-0.80' B. 87.52 ^{7.52} 86.91 C 0.61

		West		East
5+00 - 0.97' B.	87.84	^{7.84} 87.13	C 0.71	87.39
+20	87.41	⁴¹ 87.27	C 0.14	87.28
+40	87.79	⁷⁹ 87.30	C 0.49	87.46
+60	87.93	⁹³ 87.21	C 0.72	87.33
+80 - 1.88' B.	88.58	^{8.58} 87.02	C 1.56	87.57
6+05 - 0.28' B.	88.77	^{8.77} 86.72	C 2.05	86.88
+30 - 0.35' B.	88.73	^{8.73} 86.42	C 2.31	86.88
+50.70		86.20 ✓		86.17 ✓

-1.50 B

Round Grades - Webster St.
INDEXED
 To 36th - Plan - 10952-L

W.O. 31769 - 10-8-54 7.0.

SE. Pole 71.87 69
 Webster 35th

North

South

0+00 = W.L. Francis 47.0 ^{7.0} 45.7 C1.3

+50 = E.L. 52.1 ^{52.1} 49.4 C2.7

1 ~ 59.1 ^{9.1} 53.1 C6.0

+50 60.3 ^{60.3} 56.7 C3.6

2 ~ 62.4 ^{62.4} 60.3 C2.1

+50 65.3 ^{5.3} 62.9 C1.4

3 ~ 68.4 ^{8.4} 67.5 C0.9

+15 = P.C. 69.2 ^{9.2} 68.4 C0.8

35th

0+10 = P.C. 75.0 ^{5.0} 71.5 C3.5

+50 - on Line 77.1 ^{7.1} 74.7 C2.4

1+00 81.5 ^{8.5} 78.6 C2.9

+50 83.8 ^{3.8} 82.6 C1.2

+95 86.5 ^{6.5} 86.2 C0.3

2+35 88.8 88.9 F0.1

+75 91.2 ^{1.2} 91.0 C0.2

3+05 93.9 ^{3.9} 92.5 C1.4

+52.5 95.6 ^{5.6} 94.5 C1.1

53.2 52.5 C0.7
 56.9 56.1 C0.8
 61.1 59.7 C1.4
 63.3 62.3 G
 67.6 66.9 C0.7
 69.2 68.0 C1.2

73.4 71.00 C2.4
 78.3 74.2 C4.1
 84.0 78.1 C5.9
 86.6 82.1 C4.5
 88.1 85.7 C2.4
 89.9 88.8 C1.1

Pardee

= P.C. 93.3 92.0 C1.3
 95.3 94.0 C1.3

Webster - Cont.

		North	
4+00	98.7	96.6 ^{8.7}	c2.1
+40	00.4	97.8 ^{0.4}	c2.6
+80	00.4	98.1 ^{0.4}	c2.3
5+00	99.9	97.8 ^{9.9}	c2.1
+29 - PC	99.2	97.0 ^{9.2}	c2.2

96.93 = S.E. Pole - 36th

70

		South	
1 Bk	96.4	96.1 ^{6.4}	c0.3
Line	97.8	97.4 ^{7.8}	c0.4
	98.1	97.8 ^{8.1}	c0.3
1 Bk	98.4	97.6 ^{8.4}	c0.8
	97.8	97.8 ^{7.8}	c0.8

Rough Grades - 36th
INDEXED - R.P. Cross at 90°

walk - 86.73
 Cor. Walk at Franklin
 96.45

97.33 = Pole - Gilmore 71

		West.			East.	
0+00 = N.L. Ocean View	62.77	62.8		cb =	61.88	61.8
+50	72.5	72.5 69.8	C 2.7		80.6	80.6 69.7
+90	75.1	74.9 5.1	C 0.2		82.3	82.3 75.4
1+22.95 = R.P. Cross						
1+30	77.7	79.0 7.7	F 1.3		84.7	84.7 80.0
+70	81.3	82.3 1.3	F 1.0		88.3	88.3 83.5
2+10	82.3	84.5 2.3	F 2.2	1-Bk.	88.4	88.4 85.8
+50	84.0	86.3 4.0	F 2.3		90.0	90.0 87.5
+90	86.1	88.0 6.1	F 1.9		91.3	91.3 89.3
3+30	88.3	89.8 4.3	F 1.5		93.2	93.2 91.0
+70	88.6	91.2 8.6	F 2.6		95.3	95.3 92.4
+90 = S.L. Franklin						
	89.3	91.6 89.3	F 2.3	4+10	96.6	96.6 93.2
+40 = N.L.	89.7	92.2 9.7	F 2.5	=	96.9	96.9 93.5
+75	91.3	92.6 9.3	F 1.3		96.9	96.9 93.8
5+10	✓91.8	92.9 9.8	F 1.1		97.3	97.3 94.2
+50	✓91.5	93.3 9.5	F 1.8		97.4	97.4 94.4
6+00 = S.L. Gilmore	92.1	92.5 9.5	F 1.8 F 1.4		94.8	94.8 91.8
0+00 = N.L. Gilmore	93.5	94.7 9.5	F 1.2			4.8
+40	95.4	96.1 9.5	C 0.5		94.3	94.3 94.3
					95.2	95.2 94.5

36+4 Cont.

	West			
0+80	97.6	98.1	95.5	C2.6 C2.1
1+20	99.2	99.7	95.9	C2.8 C3.3
+62	98.6	99.1	96.4	C2.7 C2.2
2+02	97.2	97.7	96.8	C0.4 C0.4
+42	97.2	97.7	97.0	C0.7 C0.2
+82	97.9	98.4	97.0	C1.4 C0.9
3+222	98.2	98.7	96.9	C1.8 C1.3
+62	98.0	98.0	96.8	C1.2 C1.2 ✓
4+02	✓97.5		96.6	C0.9
+32 = P.C.	97.8		96.6	C1.2
5+12 = P.C.	98.9		95.5	C3.4
+37	98.0		94.5	C3.5
+68.7 = 5+95.6 = P.C.	97.0		93.3	C3.7
6+09.3 = S.L. Durant	91.0		91.4	F0.4

96.94 = Pole Webster

72

	East			
	95.7	96.1	94.8	C1.3 C0.9
	96.4	96.8	95.1	C1.7 C1.3
	96.3	96.7	95.4	C1.3 C0.9
	95.3	95.8	95.8	G. F0.5
	95.9	96.4	96.0	C0.1 F0.1
	96.0	96.4	96.0	C0.4 CT
	95.6	96.0	95.9	C0.1 F0.3
	95.8	96.2	95.7	C0.5 C0.1
	✓96.3		95.6	C0.7
= S.L. Webster +42	✓96.2		95.4	C0.8
5+02 = N.L.	96.9		95.1	C1.8
	95.8		94.4	C1.4
PC	95.3		93.8	C1.5
cb =	93.72			

INDEXED

Rough Grades

NOV 1 1956

0+00 = N.L. View Ocean

ch. 65.86 66.00

+10

75.0 75.0
66.3 C 8.7

+65

74.9 4.9
71.0 C 3.9

1+05

74.7 4.7
73.6 C 1.1

+45

74.2 74.2 G

+95

74.0 4.0
73.9 C 0.1

2+45

73.7 3.7
73.5 C 0.2

+95

73.7 3.7
73.2 C 0.5

3+45

72.8 72.8 G

+80 = P.C.

72.9 2.9
72.6 C 0.3

Franklin

0+10 = P.C.

73.4 3.4
72.6 C 0.8

+45

73.8 3.8
72.7 C 1.1

+65

73.9 3.9
72.7 C 1.2

1+05

72.9 2.9
72.4 C 0.5

+55

72.3 2.3
72.2 C 0.1

2+05

72.6 2.6
71.9 C 0.7

+55

71.6 71.7 F 0.1

3+05

71.8 1.8
71.4 C 0.4

73.07 = S.W. Pole - Franklin.

73

Fast.

65.86 66.00

77.7 77.7
66.5 C 11.277.1 7.1
71.4 C 5.776.3 6.3
74.0 C 2.375.4 5.4
74.7 C 0.775.4 5.4
74.4 C 1.075.8 5.8
74.0 C 1.875.6 5.6
73.7 C 1.974.4 4.4
73.3 C 1.174.4 4.4
73.1 C 1.375.5 5.5
73.1 C 2.475.4 5.4
73.3 C 2.175.5 5.5
73.3 C 2.275.1 5.1
73.1 C 2.073.7 3.7
72.9 C 0.873.8 3.8
72.6 C 1.273.9 3.9
72.4 C 1.572.8 2.8
72.2 C 0.6

35⁴
Cont.

	West.		
3+55	72.5	71.1 ^{2.3}	C 1.2
4+05	72.3	70.9 ^{2.3}	C 1.4
+55	71.0	70.6 ^{1.0}	C 0.4
5+05	70.2	70.4	F 0.2
+55	70.2	70.1 ^{0.2}	C 0.1
+95	69.7	69.8	F 0.1
6+35	69.9	69.3 ^{0.9}	C 0.6
+50 = P.C.	69.8	69.1 ^{0.8}	C 0.7

Webster.

0+10 = P.C.	69.3	69.1 ^{0.3}	C 0.2
+55.18	69.3	69.6	F 0.3
1+00.35 = P.C.	69.9	70.0	F 0.1

Durant.

0+13.6 = P.C.	70.8	69.6 ^{20.8}	C 1.2
+60	69.7	67.7 ^{9.7}	C 2.0
1+00	66.3	66.0 ^{6.3}	C 0.3
+40 = P.C. on W.	66.5	64.3 ^{6.5}	C 2.2
+80 = P.C. on E.	65.6	62.7 ^{5.6}	C 2.9
2+20 = End of Grading in E	65.5	62.4 ^{5.5}	C 3.1

71.87 = Pole - Webster

74

70.63 = Pole - N. of Durant.

		East.	
73.4	72.4 ^{3.4}	C 1.4	
73.7	71.8 ^{3.7}	C 1.9	
72.3	71.6 ^{2.3}	C 0.7	
72.2	71.4 ^{2.2}	C 0.8	
72.5	71.2 ^{2.5}	C 1.3	
73.5	70.9 ^{3.5}	C 2.6	
73.4	70.4 ^{3.4}	C 3.0	
73.5	70.2 ^{3.5}	C 3.3	

74.6	70.1 ^{4.6}	C 4.5
73.5	70.6 ^{3.5}	C 2.9
74.9	71.0 ^{4.9}	C 3.9

75.2	70.6 ^{5.2}	C 4.6
74.6	68.7 ^{4.6}	C 5.9
73.8	67.0 ^{3.8}	C 6.8
73.9	65.3 ^{3.9}	C 8.6
73.1	63.6 ^{3.1}	C 9.5
69.7	62.4 ^{9.7}	C 7.3

INDEXED

Grades - Pardee

68.45 = Pole - Alley.

73.50 = Pole - Franklin

75

East End of Alley

West.

East.

N.		68.5	^{8.5} 67.5	C1.0	S.	68.2	^{8.2} 67.3	C0.9
0+00 = S.L. Pardee	Place	68.2	68.2	G		68.0	^{8.0} 67.5	C0.5
0+10		68.9	68.0	C0.9				
+16						68.5	^{68.5} 67.7	C0.8
0+50		69.5	^{9.5} 68.5	C0.7		69.1	^{9.1} 68.5	C0.6
1+00		70.3	^{10.3} 69.9	C0.4		70.9	^{10.9} 69.8	C1.1
+50		71.7	^{1.7} 70.9	C0.8		72.1	^{2.1} 71.1	C1.0
2+00		72.8	^{2.8} 72.0	C0.8		73.2	^{3.2} 72.3	C0.9
+40 = S.L. Franklin		73.0	^{3.0} 72.9	C0.1		74.1	^{4.1} 73.4	C0.7
0+00 = N.L.		74.7	^{4.7} 74.0	C0.7		75.7	^{5.7} 74.6	C1.1
+50		76.4	^{6.4} 75.5	C0.9		77.3	^{7.3} 75.9	C1.4
1+00		78.3	^{8.3} 76.9	C1.4		78.9	^{8.9} 77.4	C1.5
+50.		79.9	^{9.9} 78.4	C1.5		80.4	^{80.4} 78.9	C1.5
2+00		80.5	^{80.5} 79.9	C0.6		81.8	^{1.8} 80.4	C1.4
+50		81.3	81.3	G.		84.4	^{4.4} 81.8	C2.6
3+00		82.5	82.5	F0.3		86.3	^{6.3} 83.3	C3.0
+40		84.1	^{4.1} 83.9	C0.2	3.0.	87.2	^{7.2} 84.4	C2.8
+80		84.7	84.8	F0.1		87.6	^{7.6} 85.3	C2.3

Pardee

S. w. Pole - webster
89.62

step = 92.01 76

West.

East.

4+20	84.8	85.7 _{4.8}	F 0.9	88.3	86.2 _{8.3}	C 2.1
+50	85.1	86.3 _{5.1}	F 1.2	87.5	86.8 _{7.5}	C 0.7
5+00	86.0	87.3 _{6.0}	F 1.3	89.4	87.8 _{9.4}	C 1.6
+50	88.2	88.3	F 0.1	91.1	88.8 _{9.1}	C 2.3
6+00	89.6	89.3	C 0.3	91.9	89.8 _{1.9}	C 2.1
+50 = P.C.	90.0	90.3	F 0.3	93.1	90.8 _{3.1}	C 2.3

Stake Culverts - 53rd + Imperial
 Plan - H263-L - w.o. 32107 - 10-19-54 7.0

INDEXED

Req. 18" pipe at S.E. Inlet.			
Top of cb	55.05	54.69	C 0.36
I.E. pipe at Box	55.05	51.00	C 4.05
o + 43.21 = Box at S.W. Inlet.			
Top cb.	56.34	55.08	C 1.26
I.E. of Box = Pipes	56.34	49.00	C 7.34
o + 00 = Edge of Box			
o + 13 = BRK.	56.17	48.87	C 7.30
+ 23	55.42	48.50	C 6.92
+ 55.80	55.04	46.20	C 8.84
Inlet at 2E.			
S. end - Top cb.	55.02	54.73	C 0.29
N. end.	54.82	54.74	C 0.08
Inlet at S.W.			
S. end	56.26	55.12	C 1.14
N. end	56.32	55.06	C 1.26

BM. = 156.03 = S.E. Pole

77

Boxes on Santa Margarita

N. Side 10' opening

from PC. - 4.27	69.95	71.41	F 1.46
= E 9.77	69.96	71.35	F 1.39
- 6' B. 15.27	69.97	71.36	F 1.39

old

S. side

from PC. 13.83	72.29	72.11	C 0.18
= E 18.83	71.76	72.13	F 0.37
7' B. 23.83	71.78	72.14	F 0.36

N.

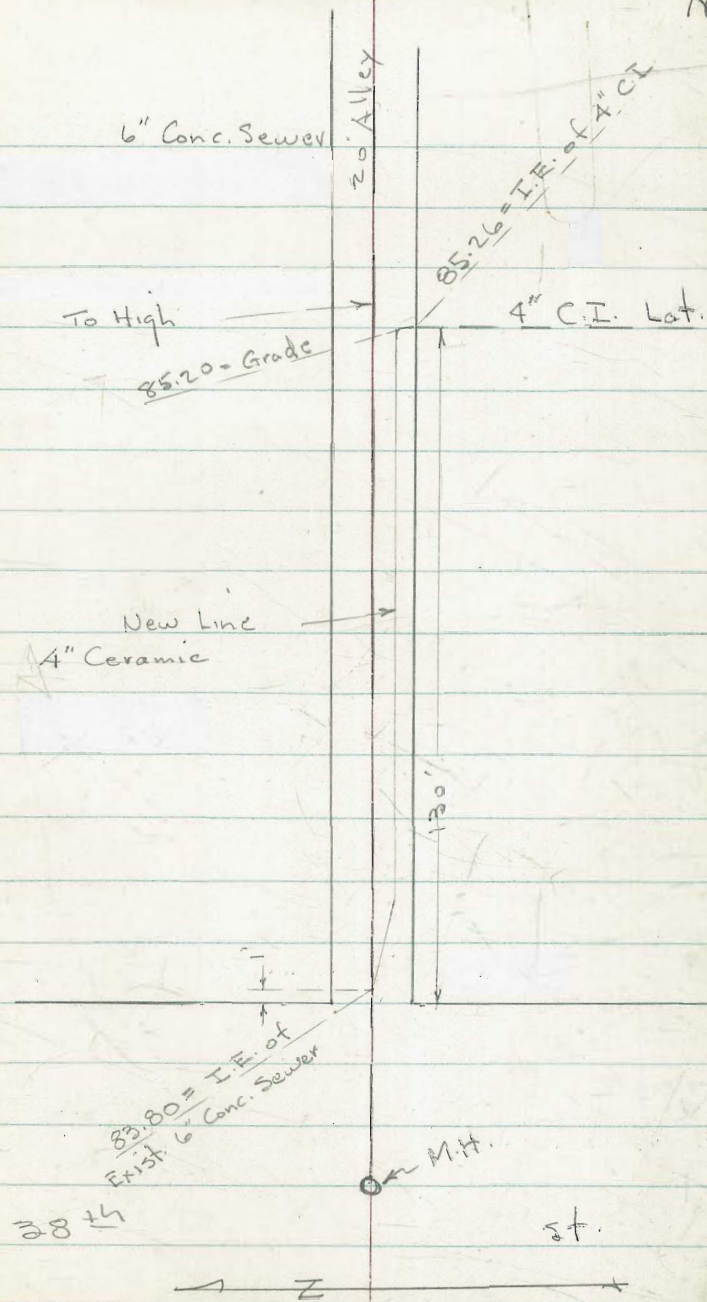
New ↘

4.27	69.96	70.91	F 0.95
9.77	69.97	70.85	F 0.88
15.27	69.98	70.87	F 0.89
S. side			
E - only	71.77	71.85	F 0.08

Stake Sewer in Alley for Sewer Dept.
 W.O. 20009 - 12-22-54 7.0.

0+00 = Conn.	86.93	83.80 ^{5 93}	C 3.13
+25'	89.46	84.07 ^{9 46}	C 5.39
+50	91.65	84.34 ^{9 65}	C 7.31
+75	93.05	84.61 ^{3 05}	C 8.44
1+00	93.68	84.88 ^{3 68}	C 8.80
+29 = Elbow	93.45	85.20 ^{3 45}	C 8.25

Ocean View 3



Stake ~~INDEXED~~ - Redwood St. + Lynn St.
 Plan 5532-B - 4-22-55 70.
 N 1 193 M = \pm inlet 394.70
 stakes - 5' Rt.

to Inlet.

0 to 00 = Conn

+04.5 = B.C.

+12.18 = Mid.

+19.86 = E.C.

+27.72

+35.68

22

+57.68 - 2.10 Rt.

31 +88.68 - 2.15 Rt. nail

27.20

+15.88 = End.

95.02	95.02	6.72
95.32	88.30	6.18
95.82	95.32	5.25
96.37	89.14	4.36
96.99	95.82	3.51
97.36	96.37	3.11
98.37	92.01	C 3.90
98.81	96.99	C 4.03
98.48	97.36	C 3.43
	94.25	
	94.47	
	94.78	
	95.05	

Water Tank.

79

431.00 = Top of Conc.

1 = Axis	27.17	31.00	F 3.83
2	26.65	31.00	F 4.35
3	26.84	31.00	F 4.16
4	26.46	31.00	F 4.54
5	26.62	31.00	F 4.38
6	26.73	31.00	F 4.27
7	27.31	31.00	F 3.69
8	27.22	31.00	F 3.78
9	26.86	31.00	F 4.14
10	27.31	31.00	F 3.69

See Profile 3156
w.o. ~~240.07~~ - 5-13-55 70.

cb. at Winchester -

Subline Grade

66.08

+ 14.6 - w. = stake 3' bk. 66.01

65.81 C 0.20

+ 93.65 = PC.

64.30

89° 05' RT

7.14
2

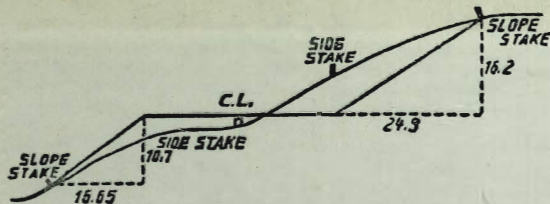
9.31
7.14
2.17
27
3
81

04 048

588

9.31
1.81
48.50

1938



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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