

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 15 1965

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.053	.057	.061
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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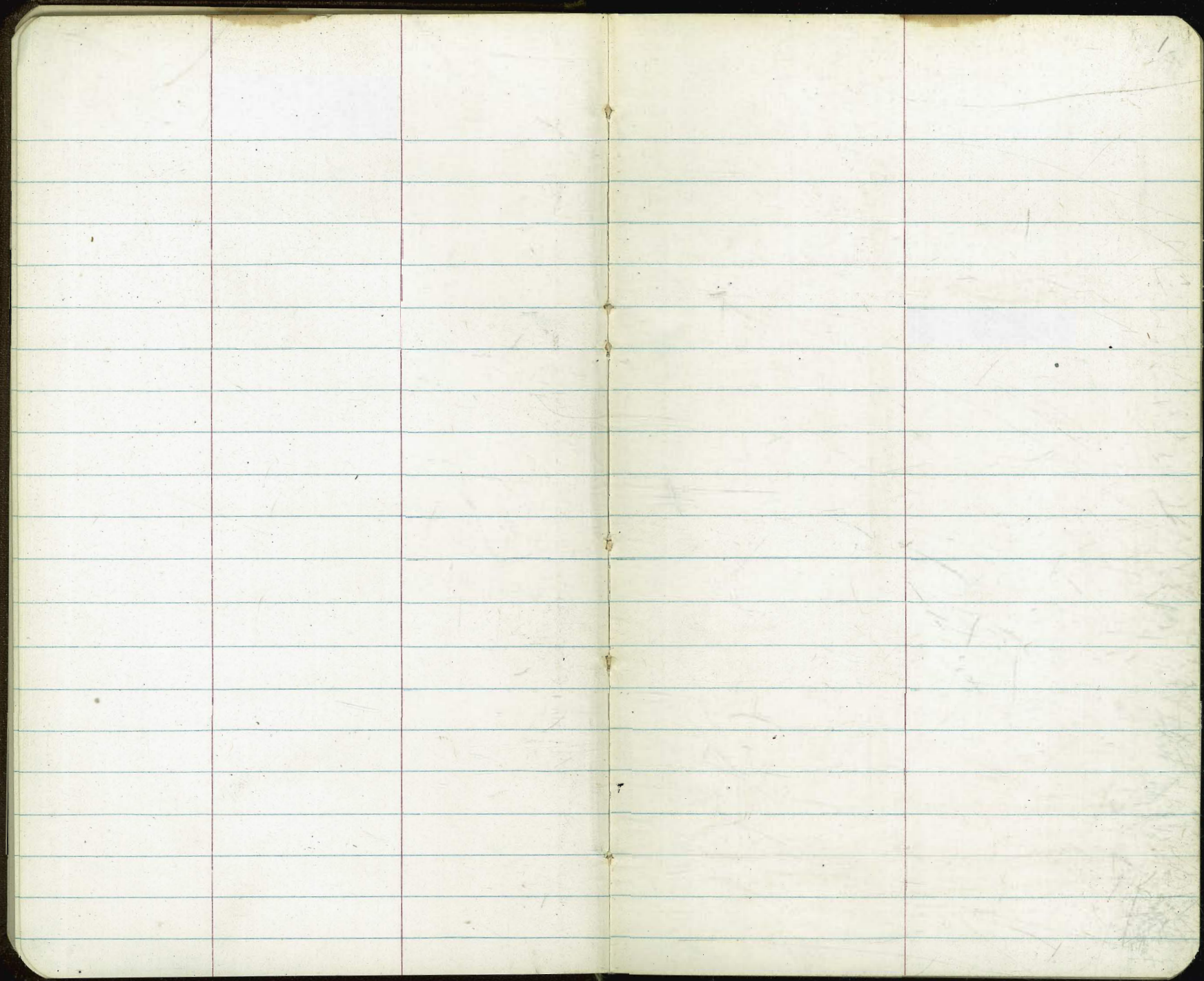
SEWER: GUY & CROWELL

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INDEX

Shuffleboard Court
Cor. Ebers + Santa Monica

Clark
Shepard
Moore
Bruncer
O'Neil

1-27-54
W.O.#20723

Grades for Hill Pt. A = 45.87

" " " " B = 45.95

" " " " C = 45.99

Grades for Hill Pt. D = 45.83

Grades for Courts = 46.00

#1 44.62 Rod
45.87 Grade
E 1.25

#5 46.20
45.87
C 0.33

#5 46.20
44.73
C 1.47 to Fl. of Drain

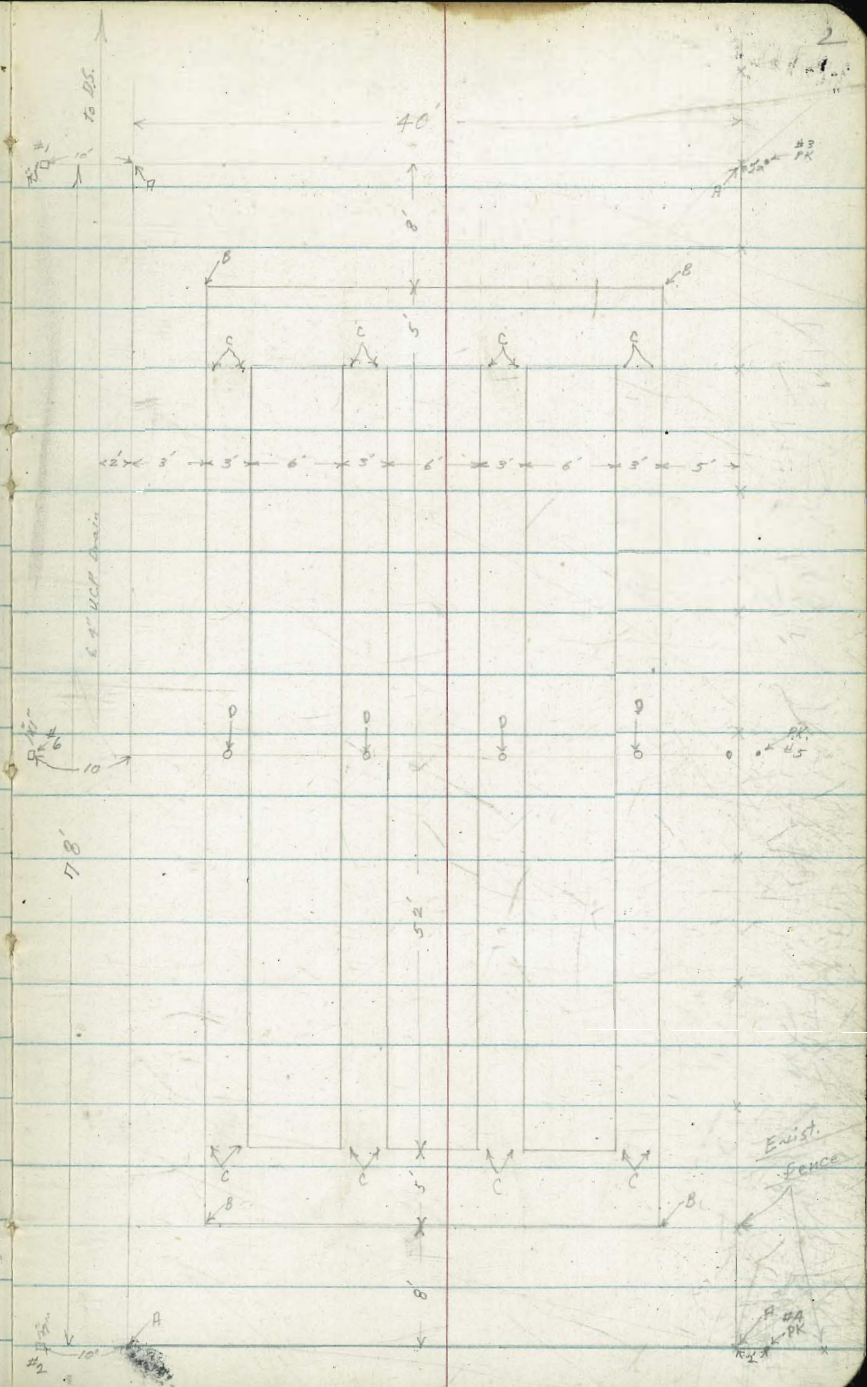
#2 46.71
45.87
C 0.84

#6 45.74
45.87
F 0.13

#1 45.74
44.34
C 1.40 to Fl. of Drain

#3 44.19
45.87
E 1.68

#4 46.51
45.87
C 0.64



Claw
Shepherd
Bruiser
Orrill

TMP'S "J" ST. #3rd WLY
to TOYNE (wily line)

INDEXED

REF: FB# 1638
FB# 2315-1
DYG: 19806-L
M.P.O. = 1844

TA	P.L.	CB.	£	CB.	P.L.	RT (WLY)	STA.	P.L.	CR	£	CB.	RT.	P.L.
							3+00	126.00 125.37	125.26 125.37		124.87 125.12		125.17 125.12
#2								Co.63	Fo.11		Fo.25		Co.05
ENO. CB							2+75	125.78	125.61 125.78		125.30 125.53		125.53
#1									Fo.17		Fo.23		
(N.E. Ret. Denay)							2+50	126.59 126.24	126.00 126.21		125.89 125.95		126.01 125.95
1+12.07 =	129.80 128.80	128.97 128.80		128.47 128.50	129.15 128.30			Co.38	Fo.21		Fo.06		Co.06
CB. BC RT only & E Line Denay)	C1.00	Co.17		Co.17	Co.85		2+25	126.62	126.44 126.62		125.84 126.36		126.36
0+83.04	131.23 129.90	129.85 129.90		129.47 129.25	129.90 129.25				Fo.18		Fo.52		
	C1.33	Fo.05		Co.22	Co.65		2+00	127.35 127.02	126.73 127.02		126.96 126.77		127.16 126.77
0+54.02	131.50 131.00	131.21 131.00		130.35 130.21	131.20 130.21			Co.33	Fo.29		Co.19		Co.39
	Co.50	Co.21		Co.14	Co.99		1+75	127.43	127.32 127.43		127.20 127.18		127.18
0+25	133.29 132.10	131.94 133.10		130.95 131.17	131.60 131.17				Fo.11		Co.02		
	C1.19	Fo.16		Fo.22	Co.43		#25 ENO. CB				127.14 127.55		127.14 (Denay)
0+15 = CB	133.61 132.50	132.28 132.50		131.22 131.50	131.64 131.50						Fo.41		
= EC LT & RT	C1.11	Fo.22		Fo.28	Co.14		#1				127.00 127.50		
0+00 = WLY	132.95	132.67 132.95		131.22 131.58			(N.W. Ret. Denay)				Fo.50		
Line #3rd ST.	133.27	Fo.28	chk	131.52 131.54									
							1+62.07 =	128.41 127.65	127.63 127.65		127.31 127.40		127.40
							CB. BC RT only	Co.76	Fo.02		Fo.09		Co.07
							= W. Line Denay						
B.M.	(D.K. F. Ret. Reg)			127.54 S.E. O.P.			1+37.07 LT only		128.18 128.22		Fo.04		
	Set B.M. on E.S. #469			(S.W. J + 43rd 133.33)									

"J" ST.

4

STA.	P.L.	CB	E	CR	P.L.	CHK
#2 CB. END				123.35 123.03 Co.30	W4 (Toyne)	133.32 = 133.33 (See T.B.M)
#1 N.W. Ret (Toyne)				122.92 123.10 Fo.18		
4448-07 C.B. BC RT. only (= W. Line Toyne)	123.62 123.06 Co.56	121.86 123.06 F1.20		123.34 123.00 Co.34	124.15 123.00 C1.15	
4428-07 LT. only	123.92 123.35 Co.57	122.48 123.35 Fo.87				
#2				124.18 123.18 C1.00	ELY (Toyne)	
#1 N.E. Ret. J + Toyne				123.68 123.28 Co.40		
3+98.07- C.B. DC RT. only (= E. Line Toyne)	124.18 123.75 Co.43	123.44 123.75 Fo.31		123.52 123.50 Co.02	124.39 123.50 Co.89	
3+75	124.12	124.09 124.12 Fo.03		123.82 123.88 Fo.06	123.88	
3+50	125.42 124.55 Co.87	124.48 124.55 Fo.07		124.18 124.30 Fo.12	124.78 124.30 Co.48	
3+25	124.96	125.07 124.96 Co.11		124.45 124.71 Fo.26	124.71	

INDEXED

Class
Shoemaker
Brumer
O'Connell
3-16-54
W.O. 32285

SEWER: ROANOKE, MORNING-SIDE

RACHAEL
T.B. = 31
REF: FB # 2107(?)
DWGS: 10968-L
10969-L
10970-L

STA.		Elev's.	STA.	Elev's.
			4+65	169.75 162.60 C 7.15
2+17.93	↑ 0.5%	161.12 152.49 C 8.63	4+30	167.73 160.68 C 7.05
1+89.37		161.54 152.84 C 9.20	3+95	166.50 158.75 C 7.75
	Δ = 76° 29' 40" LT.			
1+60.81 = M.H.	E Roanoke & S ELY E Rachael (stubs 3rd 5' x 10' 1/2)	162.13 152.20 C 9.93	3+60	164.48 156.83 C 7.65
1+28.64		164.05 150.69 C 13.36	3+26.50 = E.V.C. = B.Y.R.	162.78 154.99 C 7.79
0+96.48	↑ 4.7%	164.76 149.18 C 15.58	3+06.50	162.20 154.03 C 8.17
0+64.32		164.27 147.67 C 16.60	2+86.50	161.74 153.32 C 8.42
0+32.16		162.65 146.16 C 16.49	2+66.50	161.10 152.85 C 8.25
	(stubs S.B.T.E.)			
(EXIST) Rachael 0+00 = D.E. 176 E SLY Winchester		161.12 144.65 C 16.47	2+46.50 = B.V.C. = quit B.Y.R.	161.03 152.63 C 8.40
B.M.	(Dir. Elev. Rod)	147.04 = N.E.B.P.	Rachael & Winchester	

↑
5.5%

ROANOKE SEWER

STA.	Elev's.	STA.	Elev's.
(7+52 6" chimney RT)		(9+27 = 9" chimney RT)	193.95 181.65 C 12.30
7+37	193.64 176.83 C 16.81	9+26	
(7+26 24" box cradle)		(8+96 End cradle)	
7+02 (RT = 6" chimney)	189.77 175.01 C 14.76	8+91	198.18 181.51 C 16.67
6+67	184.59 173.19 C 11.40	(8+22 = 6" chimney RT)	
6+32	180.74 171.37 C 9.37	8+56	201.72 181.37 C 20.35
5+97	177.91 169.55 C 8.36	{CHK: 201.24 = 201.18 on E.H.O.B. EA 2107 29 61}	
5762	174.82 167.73 C 7.09	$\Delta = 12^{\circ} 32' 02" LT$	
5427.00	175.95 167.73 C 8.22	8+21.74 = M.H. #3 (E. HARKINS ST.) (grade 2' RT)	201.49 181.23 C 20.26
4+92.31 = M.H. #2	173.73 165.91 C 7.82	[Stubs set 503410' RT 2' on split.]	
	$\Delta = 7^{\circ} 28' 17" LT$ - (grade - etc) 171.66 164.10 C 7.56	8+07	200.41 180.46 C 19.95
	(Stubs 5' + 10' RT 20' on E.H.O.B.) 171.85 164.10 C 7.75	7+72	197.36 178.65 C 18.71

↑
5-25

↑
10
10
10

ROANOKE SEWER

STA.		Elev's	STA.	Elev's
11+90	3.968	198.11 183.92 C 14.19	14+83	205.57 197.89 C 7.68
CHK: $\Delta = 9^{\circ} 50' 24''$ LT.	196.00 = 196.02	Hub DEANVILLE	14+48	202.47 195.91 C 6.56
11+53.99 = M.H. #4 - grade grade - (DEANVILLE ST)		196.67 182.57 C 14.10	14+13	199.78 195.93 C 5.85
(1999) [Stubs set 5.00' + 10' RT on split]		194.55 182.49 C 12.06	13+78	197.35 191.96 C 5.39
11+01		189.94 182.35 C 7.59	(2117) $\Delta = 80^{\circ} 31' 35''$ RT 13+43.03 = M.H. #5 (E.C.) Stubs set 5' 4 10' RT 90° to Fwd Tang.	195.86 189.98 C 5.88
(10+67 END CRADLE)			13+30	195.53 189.46 C 6.07
10+66		185.19 182.21 C 2.98		
	0.42		12+95	194.81 188.07 C 6.74
10+31		181.87 182.07 Fo. 20	12+60	195.53 186.69 C 8.84
9+96		183.13 181.93 C 1.20		
(9+77 - Bay cradle)			12+25	196.38 185.30 C 11.08
9+61		187.80 181.79 C 6.01		

ROANOKE SEWER

MORNINGSIDE [ROANOKE SEWER] 8
(Sly of Winchester)

STA.	Elev's.
chk	218.01 = 217.96 = N.W. B.P. Roanoke + Winchester
17+38.03 = D. END	219.78 211.16 C 8.62
17+03	218.75 209.41 C 9.34
16+68	216.98 207.66 C 9.32
16+33	215.28 205.91 C 9.37
15+98	213.50 204.16 9.34
15+63.03 = M.H. #6	211.59 202.41 C 9.18
15+53	210.87 201.84 C 9.03
15+18	207.95 199.87 C 8.08

STA.	Elev's.
2+48.4 = M.H. #7	209.43 201.67 F.L.W. C 7.76
2+45 (not set)	201.65
2+10	210.16 201.51 C 8.65
1+75	210.84 201.37 C 9.47
1+40	212.16 201.23 C 10.93
1+05	215.17 201.09 C 14.08
(0+90 END CRACK)	
0+70	218.00 200.95 C 17.05
(0+38.4 = 4' chimney LT.)	
0+35	219.12 200.81 C 18.31
(0+100 = END EXIST SERVICE Sly Winchester)	218.63 200.67 Elev. Eline C 17.96
B.M.	213.69 = N.W. B.P. MORNINGSIDE + WINCHESTER
B.M.	217.96 = N.W. B.P. WINCHESTER + ROO
B.M.	147.04 = N.E. B.P. WINCHESTER + RACHAEL

(Rachael END) Winchester

↑

↑

↑

(not in AT this note)

MORNINGSIDE, ROANOKE (Cont)

ROANOKE: W. LY & MORNINGSIDE 9

STA.

Elev.

STA.

Elev's

(For CLK. See Pg. 10)

1485 = D.END.

218.72
211.66
C 7.06

1475

218.31
210.12
C 8.19

1440

217.52
209.23
C 8.29

5748 →

3463.4 = D.END Morningside
5/4 of ROANOKE

209.34
202.13
C 6.21

1405

215.41
207.34
C 8.07

3453

↑
0.40

208.82
202.09
C 6.73

0470

213.44
205.45
C 7.99

3418

210.28
201.95
C 8.33

0435

211.30
203.56
C 7.74

2483

210.27
201.81
C 8.46

0400 = M.H. #7 E MORNINGSIDE
- 248.4 98

201.67 F line

(See Pg. 10)

B.M.

ROANOKE - ELY of MORNING SIDE

chk

213.69 = 213.68 - NWBP
MORNING SIDE of
N. Winchester

chk

1+20 = 0. END

205.65
202.15
C 3.50

1+05

0.48

205.63
202.09
C 3.54

0+70

207.10
201.95
C 5.15

0+35

208.35
201.81
C 6.54

0+00 = M.H. *7 E MORNING SIDE
(= 2+48.4 P 8)

201.67
(see P 8)

Clark
Shepherd
Stump
O'Neil
4-6-54
W.O. 32285

PARADISE HILLS UNIT #2 - WATER

ROANOKE: RACHAEL - ELY

R.F. T.B. #31
ANG: 10968-L & 10969-L & 10970-L

STA.	Elev's
2+20	166.79 163.50 C 3.29
1+80	164.45 161.75 C 2.70
1+40	162.35 160.00 C 2.35
0+80	160.50 158.5 F.L. C 2.00
0+40	160.34 158.15 C 2.19
0+13.65 = FINE-HYD. RT (sky)	159.97 CB Elev. 162.40 F 2.43
0+100 = Plug (end line) At Pt. Int. of Ely Line RACHAEL & Line 15' N 24' of SHY Line ROANOKE (= 2+20 ANG 10969-L)	161.00 157.8 F.L. Line C 3.20

STUBS sud 5' RT B
(upgrade)

B.M. Div. Elev. Res. 1470.4 = N.E.A.P

STA.	Elev's
6+60 = grid B.M.	202.22 190.60 C 11.62
6+05 = Fire Hyd. (RT) CB Elev. HOPKINS	198.68 194.20 C 4.48
6+00 = grid B.M.	198.40 190.00 C 8.40
5+50	193.26 185.79 C 7.47
5+00	186.79 181.56 C 5.23
4+40 grid B.M.	179.23 176.50 C 2.73
4+00 grid B.M.	176.33 173.60 C 2.73
3+50	173.76 170.78 C 2.98
3+00	170.90 167.96 C 2.94
2+68.38 = A.C. Δ = 33° 26' 30" NE WATER LINE R = 15.30' R.F. (L) = 1-12.43	168.51 166.19 C 2.32

Winchester + Rachael

WATER
ROANOKE - (Rachel Ely) (Cont)

STA.	Elev's
10+30	198.80 188.60 C 10.20
10+10 = FIRE-HYD. (RT) DRAINAGE	199.92 CB.EI. = 191.20 C 8.72
9+90	198.87 188.20 C 10.67
9+50	194.95 187.8 C 7.15
9+20	190.73 187.5 C 3.23
8+60	182.89 181.00 C 1.89
8+32	179.85 180.30 Fo. 45
8+04	183.76 181.00 C 2.76
7+60	171.67 182.00 C 3.67
7+00	200.80 190.20 C 10.60

STA.	Elev's
14+40	215.02 209.60 C 5.42
14+00.89 = FIRE HYD. (RT) E.C + 240' ±	212.62 CB.EI. = 198.20 C 14.42 212.62 208.20 C 4.42
13+90	212.61 206.31 C 6.30
13+40	208.00 203.04 C 4.96
12+90	216.30 199.77 C 6.53
12+40	200.82 196.50 C 4.32
12+00	197.89 194.30 C 3.59
11+60.97 = F.C.	195.89 192.68 C 3.21
11+20	195.08 191.00 C 4.08
10+80	195.56 190.00 C 5.56

CB grade on Plans Wrong!
See Profile sheets.
{ grade Used picked off Profile sheet approved by Inspector }

WATER: POANOKE - (RACHAEL ELY)

STA.	Notes	Elev's.	STA.	Elev's
18+75.22		209.81 204.83 C 4.98	CHK: 213.71 = 213.68	N.W.B.P. MORNINGSIDE & Winchester
18+80.89	= FIRE-HYD. (RT) (Line ahead is Ely & Morning-side)	20973 C.B. Elev. 207.30 C 2.43		
18+30.89	= L.L.T. 90° ± (Gate - raised)	(NO DATA GIVEN IN T.P. BOOK 31!) 209.01 203.50 C 5.51		
	[to S4 E Runike 10' Ely Morning-side]			
17+80		212.11 204.50 C 7.61		
			20+89.29 = CONNECT. I	219.66 212.00 C 7.66
17+20		216.52 210.88 C 6.52		
			20+60.59 Bck	219.70 212.50 C 7.20
16+80		218.10 212.00 C 6.10		
			20+20.59 2nd gate	218.40 212.50 C 5.90
16+20		219.01 213.80 C 5.21		
			19+63.89 2nd Bck	213.87 207.50 C 6.37
15+60		219.71 214.00 C 5.71		
			19+19.55	210.62 206.16 C 4.46
15+00		217.26 212.60 C 4.66		

Clark
5/20/54
INDEXED

W.O. 32197

STORM-DRAIN = STREAMVIEW DRIVE

544 1/2 ST NLY to Chollas Creek

Ref. Dwg. 9802 A-L

STA

Elev's

STA.		Elev's		
2+07.91		239.05 233.03 C 6.02		
1+89.91 = Gd Brk Bys		241.83 233.88 C 7.95		
1+40		240.72 236.59 C 4.13		
1+00		242.73 238.76 C 3.97		
0+66.91 = E.C		247.45 240.55 C 6.90		
0+49.46 = mid pt	stubs set 10' RT (grade only)	246.34 241.50 C 4.84	3+34.91 = END 60" Pipe	stubs set 15' RT 233.30 231.80 Fil Pipe C 1.50
0+32 = A.C		244.02 242.44 C 1.58	3+00	235.26 232.07 C 3.19
	$\hat{C} = 50^\circ$ RT. R = 40		2+69.91	235.74 232.32 C 3.42
0+00 = ELY F. EXIST. Box Culvert		chk 244.16 244.17	2+29.91 = E.V.C	237.77 232.64 C 5.13

B.M. DIR. Elev. AD'

258.51 B.P. NLY ISLAND STREAMVIEW W
4 544 1/2 ST.

Clark
5-14-54

STREAMVIEW DRAIN
54th ST Ely to Redwood Village #7

STA.	Elev's	STA.	Elev's
1141	256.31 253.20 C 3.11	4+40	268.21 266.15 C 2.06
1+17	255.36 252.16 C 3.20	4+00	266.46 264.42 C 2.04
0+93	254.05 251.12 C 2.93	3+60	265.10 262.69 C 2.41
0+69	253.05 250.08 C 2.97	3+20	263.06 260.96 C 2.10
		2+80	261.24 259.23 C 2.01
D+45 = B.C. 2 = 18' 49" 48" RT. R = 680' L = 192.19	252.94 249.04 C 3.90	2+42.45 = E.C.	259.69 257.58 C 2.11
D+106 = G. Channel #1 TYPE C	253.07 258.95 (Channel) F 5.88	Trade Section Tr. Hdwall 253.07 247.35 F.L. C 5.72	258.57 256.32 C 2.25
CHK. (EXIST. Hdwall) (0+00) ELY 2'ly END EXIST. 60" Pipe 54th ST + STREAMVIEW	247.13 - 247.11 = F.L. EX. Pipe 0+00	2+13	257.57 255.28 C 2.29
		1+89	256.91 254.24 C 2.67
		1+65	
B.M.	258.51 = B.P. N'ly - ISLAND	STREAMVIEW 54th	

STREAMVIEW DR. (cont)

STA.		Elev's	STA.	Elev's
7+47.64		284.52 277.73 C 6.79	11+00	285.77 283.37 C 2.40
7+07.64 6+9	(stubs set 8' RT E)	283.41 277.09 C 6.32	10+60	284.75 282.73 C 2.02
6+91.15 = B.C. $\Delta = 13^\circ 02' 11''$ LT E.R. 600 L = 136.49	(stubs set 10' + 18' RT E Box)	282.33 276.83 (see above)	10+20	284.18 282.09 C 2.09
Cleanout #2 type: (6+91.15)		282.33 285.70 TPA Box F. 337	9+80	283.69 281.45 C 2.24
6+16.49 = meet EXIST. 72' of 60" Cav. Pipe make connect	CHK'	273.75 273.77	9+40	283.08 280.91 C 2.27
6+08.49 = B.C. LT		275.57 273.41 C 2.16	9+00	282.75 280.17 C 2.58
5+60		272.81 271.35 C 1.46	8+60	284.42 279.53 C 4.89
5+20		271.42 269.62 C 1.80	8+27.64 = B.C.	285.31 279.01 C 6.30
4+80		269.85 267.89 C 1.96	7+87.64	284.83 278.37 C 6.46

STREAMVIEW LV (CONT.)

14+54.97 = B.C. Pipe
Δ = 14° 00' 10" RT.
ER = 500'

292.49
289.39
C 3.10

14+41.58 = END EXIST 60" Pipe

chk: 289.12
289.13 = F.L. EXIST

STA.
17+20

Elev's
297.16
295.96
C 1.20

13+64.58 = EXIST. 80' DE (MAKE CONNECT)
60" CON. PIPE

287.64 = chk:
287.66 = EXIST

Eq. (16+05.98 Ahead)
16+06.61 = B.C. STREAMVIEW DRIVE

16+40

295.90
293.98
C 1.92

13+20

289.12
286.92
C 2.20

15+77.17 = P.E.C. PIPE

295.20
292.41
C 2.79

12+80

288.94
286.28
C 2.66

15+50.97

294.75
291.76
C 2.99

12+36.19 = E.C.

288.33
285.56
C 2.77

15+26.97

294.76
291.17
C 3.59

12+18.69 = B.C.
Δ = 1° 00' 10" RT
R = 1000'
L = 17.50

288.17
285.27
C 2.90

15+02.97

295.80
290.58
C 5.22

11+80

287.10
284.65
C 2.45

14+78.97

293.58
289.98
C 3.60

11+40

286.21
284.01
C 2.20

STREAMVIEW DR. (CONT)

STA.	Elev's	
4-B.C StreamVIEW	306.13	
20+55.98 = B.C Pipe	304.25	304.55
$\Delta = 19^\circ 32' 35" \text{ LT.}$	C 1.88	304.25
$SR = 500$		C 0.30
$TAN = 103.42'$		
20+40	305.78	303.74
	303.86	303.86
	C 1.92	F 0.12
20+20	304.83	303.09
	302.87	302.87
	C 1.96	C 0.22
19+60	303.70	301.90
	301.89	301.89
	C 1.81	C 0.01
19+20	301.25	301.22
	300.90	300.90
	C 0.35	C 0.32
18+80		300.32
		299.91
		C 0.41
18+40		300.04
		298.92
		C 1.12
18+00		299.23
		297.93
		C 1.30
17+60		298.01
		296.95
		C 1.06

STA.	Elev's	
22+60.81 = E.C Pipe	311.35	309.58
	309.32	309.32
	C 2.03	C 0.26
22+47.98	310.92	309.32
	309.00	309.00
	C 1.92	C 0.32
22+23.98	310.46	308.46
	308.40	308.40
	C 2.06	C 0.06
21+99.98	309.88	307.90
	307.81	307.81
	C 2.07	C 0.09
21+75.98	309.33	307.15
	307.22	307.22
	C 2.11	F 0.07
21+51.98	308.59	306.67
	306.62	306.62
	C 1.97	C 0.05
21+27.98	307.91	306.32
	306.03	306.03
	C 1.88	C 0.29
21+03.98	307.19	305.72
	305.44	305.44
	C 1.75	C 0.28
20+79.98	306.52	305.12
	304.85	304.85
	C 1.67	C 0.27

Pipes out - Rise +

Stakes (unchanged) + Rise

STREAMVIEW DR. (CONT.)

STA.

Elev's

STA.		Elev's		Elev's
25+68.83 = B.C. Pipe Δ = 1° 43' 07" RT. R = 600'		318.06 316.90 C 1.16	28+32.37 = N. LINE HUANES ³	322.45
25+34.42		317.50 316.18 C 1.32	28+00	324.18 321.76 C 2.42
25+00		315.45	27+60	323.93 320.92 C 3.01
(make correct - 48" RCP pipe) 24+84.36 = END EXIST. 60" C. PIPE		315.13	27+20	323.44 320.08 C 3.36
24+04.88 = EXIST 60" Pipe	AK: 318.80	EXIST 318.86 = TP Head VAN	26+80	322.50 319.24 C 3.26
24+00.83 = E. Cleavage #3	322.40	312.76 = FL Box	26+00	319.76 317.56 C 2.2
23+80	314.63 312.26 C 2.37	314.02 312.26 C 1.76	(29+25+86.65 ahead) 25+86.83 = B.C.	318.78 317.28 C 1.5
23+40	314.03 311.27 C 2.76	311.94 311.27 C 0.67	25+77.83 = mid-pt.	318.27 317.09 C 1.18
23+00	312.87 310.29 C 2.58	310.67 310.29 C 0.38		

STREAMVIEW DR. (CONT)

STA.	Elevs
30+41.40 (32' Arc's Def = 1° 31' 44" Ch = 31.99')	328.97 326.84 C 2.13
30+09.40 = D.C. ∠ = 35° 52' 05" R = 600'	328.10 326.17 C 1.93
30+00	
29+60	326.44 325.13 C 1.31
29+20 (stubs P' RT E)	326.32 324.29 C 2.03
28+80	325.37 323.45 C 1.92
(Stub 15' RT L Box) F.L. 18" AT INLET END	326.12 325.98 = F.L. 18" Pipes AT Box
28+57.37 = E CLEAROUT	329.45 331.99 TR. M.H. S F 2.54 CLEAROUT
28+40	329.45 322.98 = F.L. Box C 6.47 324.58 322.61 C 1.97

STA	Elev's
32+61.40	338.42 333.56 C 4.86
33+29.40	337.28 332.89 C 4.39
32+97.40	335.61 332.22 C 3.39
32+65.40	334.93 331.54 C 3.39
32+33.40	334.36 330.87 C 3.49
32+01.40	334.35 330.20 C 4.15
31+69.40	334.59 329.53 C 5.06
31+37.40	331.30 328.86 C 2.44
31+05.40	330.31 328.19 C 2.12
30+73.40	329.24 327.51 C 1.73

= 327.73 = 327.77 = 2x2 HUB = 1177.03
P.B. 2238 31

2 1/2' ↑

STREAMVIEW DRAIN (CONT.)

STA	Elev's	STA	Elev's
		39+29.62	359.38 353.59 C 5.79
36+52.73	346.73 343.70 C 3.03	38+97.62	359.66 352.44 C 7.22
36+20.73 (32' Arcs Ch F = 0° 55' 00" Cl = 32')	345.84 342.56 C 3.28	38+65.62 = B.C. LT. Δ = 13° R = 609.91'	358.52 351.30 C 7.22
35+88.73 = B.C. RT. Δ = 13° R = 1000'	345.98 341.42 C 4.56	38+40.62	356.94 350.41 C 6.53
35+60	345.40 340.40 C 5.00	38+15.62 = E.C.	357.56 349.52 C 8.04
35+20	345.20 338.97 C 6.23	(32' Arcs) 37+80.73	354.76 348.27 C 6.48
34+80	344.59 337.54 C 7.05	37+48.73	352.79 347.13 C 5.66
34+40	343.00 336.11 C 6.89	37+16.73	349.95 345.99 C 3.96
34+00	340.68 334.59 C 6.09	36+84.73	348.06 344.84 C 3.22
33+85.01 = E.C. = S CLEANOUT #5 TYPE B	340.15 340.39 TP M.H. FO.24 CLEANOUT 340.15 334.06 = F/LINE C 6.09		

3.57%

→ = grid Brk

STREAMVIEW DR. DRAIN (CONT)

CHK: EXIST 42" R.C.P. 357.61 = 357.69 - FB = 2238 - 34
(Redwood Village #7)
W/1/2"

40+91.87 = EXIST. TYPE F CEMENT
W/1/2" CEMENT. 358.10
↑

40+60.73 365.73
357.44
C 8.29

40+29 7' d BRK 362.30
356.78
C 5.52

40+04 = E.C. 363.76
356.16
C 7.60

39+93.62

39+79 = 6' d BRK 362.79
355.36
C 7.43

39+61.62 361.43
354.73
C 6.70

INDEXED

CLAIM SHEET
 O'NEIL
 6-22-54
 NO. 62384

REF: T.S. 144 - 145
 DWG: 5357-B

GUTTER & DRY GRADES: 2.87% +
 COMMERCIAL: SELBY CORNER - ELY
 EOV 100'

STA.	DRY. GUT.	Elev's Prop.
1400	67.07 66.41 C0.66	68.08 67.08 C1.00
0+75	66.89 66.32 C0.57	68.54 66.99 C1.53
0+50	66.81 66.23 C0.58	66.90
0+25	66.71 66.14 C0.57	68.53 66.81 C1.72
CHK. TP. CREC SELBY		
0+00 = Ely Line 2846	66.05	66.72
	(Stubs set 3' BK GUT Line)	(Gow Feet in FORM Bldg)
(Dir. Elev. Rod)		
B.M. S.W. BRASS Peg	2926 IMPERIAL	72.05

Ref: FB# 2217-.33

DWG: 109 57-L

(STAKED For Looking)

IND E V F N

IMP'S 35th-36th - WEBSTER - PARDEE

ST. 4 PARDEE PL. (STAKED For Looking ONLY)

6-23-54

W.D. 31769

36th ST: OCEAN VIEW - NLY.

STA.	LT (WLY)			RT (Ely)			STA.	PL	CB	E	CB	RT	PL
	P.L	CB	E	CB	P.L								
							1770	81.40 82.27 F0.87					88.02 83.49 C4.53
1+10	77.13				77.85								
							1+62 = Alley B.C. LT.	81.69	81.69				
0+90	75.73 74.93 C0.80				81.46 75.41 C6.05								
							Alley E.C.		81.56				
0+70	72.50				72.69								
							(1160) Alley AT P.L.		81.75				
0+50 = B.V.C.	72.43 69.80 C2.63				80.53 69.69 10.84								
							(1150) Alley AT P.L.		81.01				
0+25		66.30			65.75								
							(1150) Alley EC	80.80	80.84				81.89 ad.
0+10 (GUT MLY)		63.71 GUT			62.88 GUT								
							B.C. 1+48 = Alley R.T. LT.	80.64	80.64				
(0-07 = ERUB.E.C.)													
0+00 = N. line OCEAN VIEW		62.78 62.81			61.85 61.81		1+30	78.17 79.02 F0.85					83.88 80.01 C3.87
							1+20 = N.S. R.T.						83.41 Red 79.00 trace C4.41
B.M. DIKEY ROD.							6+24 = S.E. F.H. - TP.						
							36th OCEAN VIEW BVD.						

3644 - OCEAN-VIEW-N.Y. (CONT.)

STA.	P.L.	LT.	CB.	♀	CB.	RT.	P.L.	STA.	P.L.	LT.	CB.	♀	CB.	RT.	P.L.
3+30-	88.11					93.05		(4+39.53)							96.66
BVC	89.75					91.00		4+40	RT. only						93.45
	F1.64					C2.05									C3.21
	(IN)														
3+24-V.S.	89.49	LT.						4+10	RT. only						96.37
LT.															93.75
															C3.22
3+10	88.17					92.25		(3+89.53)							
	88.86					90.11		3+90	RT. only	90.15					92.88
	F0.69					C2.14				91.63	RT. only				
										F1.48					
2+85	87.77					89.02									
	(IN)														
2+78-V.S.	87.47	LT.						#3	(not set)						
LT.															
2+60	85.48					90.05		#2			91.22				
	86.68					87.93									
	F1.20					C2.12		#1			91.50				
2+35	85.59					86.84									
	(IN)														
2+32-V.S.	85.46	LT.						3+79.53	CB. R.C.	91.40					
LT.								(5 mi Franklin)	LT.						
								4-50th							
2+10-EVC	82.50					87.94				89.51					95.13
	84.50					85.75		3+70		91.16					92.41
	F2.00					C2.19				F1.65					C2.72
490	83.50					84.81		3+50		90.54					91.79

364h (CONT)

LT.				RT.				LT.				RT.					
STA.	P.L.	CB.	E.	CB.	P.L.	STA.	P.L.	CB.	E.	CB.	P.L.	STA.	P.L.	CB.	E.		
5449.05	91.70 93.33 F1.63				97.24 94.37 C2.87	# 1										94.25	
5429.05	93.12				94.34	6+67.05 = CB, B.C.											95.16 94.49 C0.76
(5+10 = W.S. LT.)	92.20 92.93 F0.73					N.W. Gilmore 1364h											
5+07.05 BVC RT.	92.12 92.92 F0.80				97.23 94.18 C3.05	6+57.05 = N.W. Gilmore											
4190	92.72				93.97	(5+95 = W.S. LT.) (IN)											
4165	92.47				96.45 93.71 C2.74	5499.05 LT = S.L. Gilmore ONLY											92.07 93.85 F1.78
E.C. Franklin # 3						*3 = E.C. Gilmore											
# 2	91.80					# 2											93.50
# 1	92.20					# 1											93.75
4449.53 = CB BC LT N.W. Franklin 1364h	90.91 92.30 F1.39					5489.05 = CB, B.C.											96.77 94.00 C2.77
						S.E. Gilmore 1364h											
						5469.05											93.54
						(5170 = W.S. RT.)											94.25
																	94.24 94.25 C3.04

Set
B.M. (OFF MON below)

94.71 - clx to step
3429' W 2y of
MON. ON N 2y 18'
LINE GILMORE

CHK:

93.47 = 93.51 = CON.
MON - N 2y 18' Gilmore
W 2y 17' 38 42
FB 2217-41

#2

94.00

Clark
Sho
B
O

INDEX

RIK II-CITY HTS
THORN to MYRTLE

REF: F.B.#1770
#2224
DNIG: 10865-L

7-23-54 (cut water line)
N.W. 31.310
(9-28-54 Staked Alley)

STA.	(W/L)	Grades 6" C.I. Water Line 5' Off Alley	(E/L) RT.	STA.	LT.	Grades 6" C.I. Water Line	RT.
1+50	331.61 331.14 C0.47	332.10 327.92 C4.18	331.79 331.34 C0.65	3+60	334.71 333.83 C0.88		334.45 334.03 C0.42
1+25	331.49 330.82 C0.67		331.14 331.02 C0.12	3+40 = B.V.C	333.91 333.55 C0.36	334.10 330.33 C3.77	334.59 333.75 C0.84
1+00 = F.V.C	330.67 330.51 C0.16	330.93 327.29 C3.64	330.84 330.71 C0.13	3+25	333.71 333.34 C0.37		334.02 333.54 C0.48
0+80	330.70 330.07 C0.63	330.36 326.85 C3.51	330.36 330.27 C0.09	3+00	333.56 333.03 C0.53	333.50 329.81 C3.69	333.62 333.23 C0.39
0+60	329.85 329.23 C0.62		329.75 329.09 329.73 F0.34 C0.32	2+75	333.33 332.71 C0.62		333.85 332.91 C0.94
0+40	329.51 328.03 C1.48	328.99 324.81 C4.18	329.10 328.23 C0.87	2+50	333.58 332.40 C1.18	333.04 329.18 C3.86	333.79 332.60 C1.19
0+20	328.15 326.43 C1.72		328.95 326.63 C2.32	2+25	332.91 332.08 C0.83		332.60 332.28 C0.32
0+00: N Line THORN	325.00 324.80 C0.20	most exist. 4" line 325.46 321.58 C3.88	325.99 325.00 C0.99	2+00	332.81 331.77 C1.04	332.60 328.55 C4.05	332.88 331.97 C0.91
Alley stubs set (7-28-54)		(Water stubs) section East Line alley					
B.M. Dr. Hwy Rod:			322.59 = N.W. B.P. HIGHLAND + THORN	1+75	332.22 331.45 C0.77		332.30 331.65 C0.65

ALLEY D.K. II (CONT.)

STA.	LT.	Grades Water Line	RT.	STA.	LT.	E	Grades Water Line	RT.
5+75	338.30 337.66 C0.64		338.13 337.86 C0.27					
5+50	337.65 337.21 C0.44	337.84 337.99 C3.85	337.65 337.41 C0.24					
5+25	337.00 336.72 C0.28		337.27 336.92 C0.35					
5+00	336.60 336.32 C0.28	337.09 333.10 C3.99	337.79 336.52 C1.27					
4+75	336.04 335.87 C0.17		336.55 336.07 C0.48					
4+50	335.77 335.41 C0.36	336.10 332.19 C3.91	336.77 335.61 C1.16					
4+25	335.65 334.97 C0.68		335.86 335.17 C0.69					
4+00	335.91 334.52 C1.39	334.93 331.30 C3.63	334.73 334.72 C0.01					
3+80 = F.V.C.	334.42 334.16 C0.26	334.50 330.94 C3.56	334.38 334.36 C0.02	6+00 (5+99.98)	338.10		338.80 meet 337.88 exist. C372.6' line	338.30
				5+80 2 only		337.97		

338.66 = 338.66 F.B. 1770
47-31
= 5' 4" CO END MY FILE +
ALBY

Clark
Shepherd

INDEXED

Imp's - COMMERCIAL ST. - 29th to 30th

W.O. 32319

HWG: 11021-L
REFS: FB# 2174-55
TS# 145

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	LT.	CB	E	CB	RT	GUTT. P.L. (R.Grade)	(Fin. Pav. Grades)
1+04.50				69.59 GUT 68.66 ca. 73	69.59 69.26 69.26	2+50							70.16 69.43 69.73	70.03
1+00	69.62 69.45 60.17	69.60 69.45 60.15 (0.08)				2+25							69.32	69.92
2+84.25 RT only				69.46 69.18										
0+75 LT only		69.59 69.39 60.20 (0.15)		60.28		2+00	70.60 69.68 60.92		69.97 69.68 60.29 (0.16)				70.07 69.20 60.81	69.80
0+64.85 RT only				69.23 69.09 60.14	69.49 69.09 60.40	1+75			69.82 69.62 60.20 (0.18)				69.09	69.69
0+50 LT only	70.10 69.33 60.77	69.43 69.33 60.10				1+50	70.64 69.56 61.08		69.75 69.56 60.19 (0.09)				69.79 68.97 60.82	69.57
0+44.85 RT only				69.11 69.00 60.11	70.59 69.00 61.59	1+25		69.50	69.67 69.50 60.17 (0.08)				68.86	69.46
0+25		69.17 69.27 60.10		68.86 68.91 60.05									70.44 69.64 60.80	70.44 69.60 60.84
0+00 = E. Line 27th	Meet EXIST. CA. 69.21	69.21		68.68 68.80 60.12	68.98 68.80 60.18	(1+08.50) CA. E.C. RT							69.59 69.38 60.21	
Note: Grades in (M) = ACTUAL grade to meet EXIST. CB'S, LT.														
B.M.						72.05 = S.W. B.P. IMPONAL + 29.46							69.58 69.30 60.28	

Notes: (Does not take plan)
OK 69.77?

Req. GUTT. CB.
(For 100')

1+06.85
R. grade only - RT

COMMERCIAL ST. (CONT.)

STA.	P.L.	(N.Y.) LT.		E	CB	RT		STA.	P.L.	LT.		E	CA	RT	
		GUTT. (R.GRADES)	P.L. (FIN. BY GRADES)			GUTT. (R.GRADES)	P.L. (FIN. BY GRADES)			GUTT. (R.GRADES)	P.L. (FIN. BY GRADES)				
4+25		70.89 70.69 CO.20				G 70.24	70.84	6+25		71.28 71.59	mat DRIVE			G 71.08	71.68
4+00	71.06 70.58 CO.48	70.81 70.58 CO.23				G 70.14	70.74	6+00		72.40 71.47 CO.93				G 70.96	71.56 CO.94
3+90 = RT						G 71.05 70.10 CO.95	70.70	5+75						G 70.85	71.45
3+75		70.46 70.47 FO.01				G 70.02	70.62	5+50		71.71 71.25 CO.46				G 70.75	71.35 CO.83
3+50	70.68 70.36 CO.32	70.42 70.38 CO.04				G 70.69 69.90 CO.79	70.50	5+25		71.01 70.64 CO.37	DRIVE			G 70.65	71.25
3+25	Does NOT - (END EXIST CB, LT.) 4K 70.33(?) 70.25 CO. GUTT. (69.83)	69.75 (69.83)				G 69.79	70.39	5+00		71.69 71.03 CO.66				G 70.55	71.15 CO.68
3+00		GUTT. 69.63 (69.77)				G 70.68 69.67 CO.01	70.27	4+75						G 70.44	71.04
2+75		GUTT. 69.51 (69.61)				G 69.55	70.15	4+50		71.42 70.81 CO.61				G 70.34	70.94 CO.83

(349 END 10' DRIVE - LT.)

(299 Beg 10' DRIVE LT.)

(271 END 10' DRIVE LT.)

(6+00 Beg GUTT. CONT. LT.)

(5+30 END GUTT. CONT. LT.)

(5+05 Beg GUTT. CONT. LT.)

COMMERCIAL ST (CONT.)

STA.	P.L.	LT.	E	RT	RT	
CB E.C. RT				72.10	(GUTT. P.L. (R. Grabos))	
mid PT. RT.				72.14 72.05 C 009		
7124.96 = W. Line 30' to 40' = CB, BC RT (15' Rad.)	72.00	72.00	meet this grade	71.99 72.00 F 0101		72.00
7403.46 RT only				71.51 71.90 F 0.49		
7100 LT only	72.58 71.90 C 0.68	71.80 71.90 F 0.10				
6+81.96 = CB, BC RT only 7' Rad.				71.37 71.81 F 0.44	71.31	72.56 71.81 C 0.75
(6+75.4) 6+74.96 = E.C. (AT. PLANE) CB, RT ONLY		71.64 71.80 F 0.16		72.45 71.93 C 0.52	71.63	
6+61.96 = grid BRK GUTT. RT					71.23	71.83
6+50	72.11 71.70 C 0.41	71.72 71.70 C 0.02		72.46 71.18 C 1.28	71.78	71.79
6+37 = grid BRK set GUTT. LI		71.76 GUTT = 70.92 71.64 CD C 0.12				

= 71.77 = TO CB AT
Prop. N 44-30' 46"
Commercial
FB#2174-60

C.B. NWly 394h & Juniper

Ref: FB² 2270-1

DWG: 11183-L

0421.56 = C.B.A.C.

232.74
230.95
C 1.79

0416 BRK

232.30
230.80
C 1.50

0400 = Wly Line FAIRMOUNT

229.49
230.37
FO. 88

B.M.

234.44 = SPIKE IN
NWly Bk 394h
Juniper

C/avik
Shepherd
BRUNER
O'NEIL
9-1-54
W.O 32269

INDEXED

MP'S 44th ST: OLIVE SLY
362' F.I. D. END

Ref: F.B. 2108-61

SWG: 10932-L

		RT (W/L)				STA	PL	CB	E	CB	PL
STA	PL	CB	E	CB	PL						
						3100 =	286.77	288.31			
						F.I.C	287.74	287.74			
1+05	293.15 293.37 Fo.22	293.32 293.37 Fo.05		293.86 293.87 Fo.01	274.83 293.87 Co.96		Fo.97	Co.57		288.47 288.24 Co.23	289.67 288.24 C1.43
0+80	293.86	293.89 293.86 Co.03		294.33 294.36 Fo.03	294.36	2180	288.68	289.00 288.68 Co.32		289.34 289.18 Co.16	289.18
						(475 end walk RT)					
						2160	290.91 289.52 C1.39	289.98 289.52 Co.46		290.11 290.02 Co.09	293.33 290.02 C3.31
0+55	295.46 294.36 C1.10	294.49 294.36 Co.13		294.86 294.86 Grade	295.56 294.86 Co.70						
						2140	290.26	290.83 290.26 Co.57		290.80 290.76 Co.04	290.76
0+30	294.85	294.90 294.85 Co.05		295.36 295.35 Co.01	295.35	(2125 end walk RT)					
						2120	292.07 291.90 C1.17	291.24 290.90 Co.34		291.43 291.40 Co.03	294.29 291.40 C2.89
0+10 = CB, B.C	295.25	295.08 295.25 Fo.17		295.76 295.75 Co.01	295.75						
						2100	291.44	291.67 291.44 Co.23		291.94 291.94 GRADE	291.94
# 1 = mid-pt. (Δ = 35' 12" 39")		295.44 295.42 Co.02		295.98 295.85 Co.13							
						1180 = B.V.C	292.19 291.88 Co.31	291.90 291.88 Co.02		292.52 292.38 Co.14	294.44 292.38 C2.06
# 2 = CB END CB RETURNS R = 20' Δ = 66' 25" 18" - to CB END		296.66 295.60 C1.06		296.13 295.95 Co.18		1155	292.20 292.38 Fo.18	292.36 292.38 Fo.02		292.91 292.88 Co.03	294.58 292.88 C1.70
[C/O - S. Line Olive]	296.36 295.40 Co.96			296.17 295.80 Co.37		1130	292.87	292.89 292.87 Co.02		293.52 293.37 Co.15	293.37
B.M.				297.19 = S.F.B.P							

FAIRMOUNT & QUINCE

Clark
Shepherd
Grunen
8.7.54
W.O. 62366.

Imp's: Hilltop Dr. 47 1/2 ST.

HILLTOP DR. 47 1/2 ST ELY to WLY
Line LAT 27 (NLY - HILLTOP ONLY)

Ref: DWG'S: #2480-B
#2479-A
F.B'S: #2177-43
-56

36

INDEFINITE

	LT (NLY)	CA	CB	PL	STA	PL	CA	CB	PL
0+50	185.53 185.97 Fo.44	185.69 185.97 Fo.28			2+75	183.75	183.52 183.75 Fo.23		
0+30	(Slabs 2' x 6' Prop on R. side)	186.10	185.92 186.16 Fo.24		2+50	184.18 183.99 Co.19	183.79 183.99 Fo.20	183.99	
CB EC Hilltop Dr. = 0+22	185.42 186.25 Fo.83	185.93 186.25 Fo.32			2+25	184.24	183.98 184.24 Fo.22		
# 3		186.21 186.49 Fo.28			2+00	184.25 184.48 Fo.23	183.88 184.48 Fo.60	183.88 184.40 Fo.52	
# 2 mid-pt. Rd.	186.73	186.55 186.73 Fo.18			(1+87.70) Ely end drain	184.52	Meet		
# 1		186.72 186.97 Fo.25			(1+67.70) Wly end drain	184.60	Meet	EXIST. 184.60	
CB. BC. (on 47 1/2) (= 0+20, 47 1/2) By H	187.20	186.91 187.20 Fo.29			1+50	184.45 184.98 Fo.53	184.70 184.80 Fo.06		
(0+00) Ely line 47 1/2					1+25	185.23	184.93 185.10 Fo.17		
					1+00	185.21 185.47 Fo.26	185.33 185.40 Fo.07		
					(0+83) = 8.30 (Comp. Drive)				
					0+75	185.72	185.56 185.68 Fo.12		

B.M.

Dir. Ely Rd.

186.81 - Lat E 47 1/2 Hilltop

HILLTOP DR. (CONT.)

STA.	LT. (N4)		S
	P.L.	CB	
5100	183.32 181.52 C 1.80	181.86 181.52 C 0.34	
4775	181.77	182.83 181.77 C 1.06	
[4460.7 at calc. line for miller box (4452 approx. 2 meters)]	182.54 181.92 - 7ms C 0.62 184.37		
4450	182.02 C 2.35	182.02	
[442.4 Set still calc. line for meter box]	182.69 182.60 - 7ms C 0.59		
4425	182.27	182.73 182.27 C 0.46	
4400	184.85 182.51 C 2.34	182.84 182.51 C 0.33	
3775	182.76	182.98 182.76 C 0.22	
3750	183.91 183.01 C 0.90	183.14 183.01 C 0.13	
3725	183.25	183.45 183.25 C 0.20	
3700	183.95 183.50 C 0.45	183.46 183.50 F 0.04	

STA.	LT. (N4)		S
	P.L.	CB	
7100	179.38 179.55 F 0.17	179.46 179.55 F 0.09	
6775	179.80	179.63 179.80 F 0.17	
6750	179.78 180.04 F 0.26	180.04 180.04 G 1.14	
(6730.5 = 23' comm. dr.)			
6725	180.29	177.51 186.29 F 0.78	
6700	182.19 180.54 C 1.65	180.69 180.54 C 0.15	
5775	180.78	180.96 180.78 C 0.18	
5750	182.75 181.03 C 1.72	181.22 181.03 C 0.19	
5725	181.28	181.52 181.28 C 0.24	

HILLTOP DR. (CONT.)

STA	P.L	CB		STA	P.L	CB	
8+80	176.19	176.12 176.19 Fo.07		10+90	R. Grade ↑ (Stabs s' BK Prop) 171.87 167.60 C 4.29	167.61 167.60 Co.01	
8+60	177.27 176.80 Co.47	176.71 176.80 Fo.09		10+65	168.65	168.61 168.65 Fo.04	
(8+49.51 = 8.15 Comm. Dr. V.C.)							
8+40	177.36	177.23 177.36 Fo.13	177.23 176.78 (ST) Co.45	10+40	173.31 169.71 C 3.60	169.63 169.71 Fo.08	
8+39.5 = E Sidewalk Drain	177.40 177.16 FL Co.24	177.37 TPCB	176.79 GGT				
8+20	177.61 177.85 Fo.24	177.68 177.85 Fo.17	177.35 G	10+15	170.76	170.74 170.76 Fo.02	
8+00	178.28	178.17 178.28 Fo.11		9+90	175.17 171.82 C 3.35	171.82 171.82 Grade	
7+80	177.96 178.63 Fo.67	178.44 178.63 Fo.19		9+65	172.88	172.73 172.88 Fo.15	
7+60	178.93	178.82 178.73 Fo.11		9+40 = E.V.C.	176.36 173.94 C 2.42	173.66 173.94 Fo.28	
7+40 = B.V.C.	178.43 179.16 Fo.73	178.98 179.16 Fo.18		9+20	174.76	174.58 174.76 Fo.18	
7+25	179.30	179.13 179.30 Fo.17		9+00	176.90 175.50 C 1.40	175.33 175.50 Fo.17	

HILLTOP W. (CONC)

STORM-DRAIN - HILLTOP # 4746

(For Refs: See pg 36.)

STA	P.I.	C.B.	E	STA.	Elev's
(P. grade)		F. grade			
chk: 159.42 = 159.35 = TP (B. end)		chk: 159.40 = 159.35 = TP (B. end)			
ORIG. STA 12+84. FA # 2147.54					
				2+40	186.86 177.67 C 9.19
12+83.38 ± = dly line Lot 28	153.75 159.77 F 6.02	159.69 159.77 F 0.08		1+99.67 ± E TYPE-G - CLEAR CUT Δ = 90° RT	186.68 m.H 186.65 = T.P. Box C 0.03 186.68 177.26 = F. Line C 9.42
12+60	160.45	160.33 160.45 F 0.12		1+49.15	185.99 176.75 C 9.24
12+40 = B.P.C	166.05 161.25 C 4.80	161.25 161.25 Grade		1+08.15	185.61 176.35 C 9.26
12+15	162.30	162.21 162.30 F 0.09		0+68.15	185.20 175.94 C 9.26
11+90	167.37 163.36 C 4.01	163.21 163.36 F 0.15		0+28.15 = E.C.	184.74 175.54 C 9.20
11+65	164.42	164.43 164.42 C 0.01		0+16.23 = mid-pt. (Subst. at 16.79)	
11+40	169.91 165.48 C 4.43	165.44 165.48 F 0.04		0+04.92 = B.C. Δ = 15° RT R = 9' T = 11.98 E = 0.79	184.46 175.30 C 9.16
11+15	166.53	166.54 166.53 C 0.01		0+00 = Wly Adp. EXIST. Box - TYPE B-2 INLET - NLY CB. B'ING HILLTOP ELY # 12746	175.26 = F.L. Pipe at max 186.81 = L.S.F. 5474 Hilltop
				B.M. DIM. Elev. Rod:	

10/10

STORM DRAIN = Hill Top + 47.4h (Cont)

CHK:

186.85 = 186.81 = 56.8m 40

STA	EL'S
5+80	187.85 181.31 C 6.54
5+40	187.91 180.91 C 7.00
5+00	187.68 180.51 C 7.17
4+66.62 = S. TYPE G CLEANOUT 12" 15" Pipe FL AT 90° E (15" FL AT BOX)	<p>(15" on Hill Top) 187.58 m.H. 187.60 TP FO.02 Box 187.58 FL 180.18 m.H. C 7.40 Pipe</p> <p>187.58 FL 179.93 m.H. C 7.65 Pipe</p> <p>187.58 FL 180.18 m.H. C 7.40 Pipe</p> <p>187.58 FL 179.93 m.H. C 7.65 Pipe</p>
4+40	187.47 179.68 C 7.79
4+00	187.31 179.27 C 8.04
3+60	187.16 178.88 C 8.28
3+20	187.19 178.47 C 8.72
2+80	187.02 178.07 C 8.95

STA	EL'S
[4" of 15" Pipe on S. 51ST BOX - 64]	191.66 FL 15" Pipe 188.00 at inlet C 3.61
8+61.19 = Sky Box - ex. Type B.2 inlet (For inlet see pg 42)	191.66 188.20 = FL 15" Pipe at Pipe Line C 3.46
8+27.34 = EC	184.20
8+19.40 = mid-pt	189.86 183.82 C 6.04
8+11.46 = B.C. Δ = 10" RT R = 91' T = B =	189.20 183.63 C 5.57
7+85.87 = E TYPE G CLEANOUT 12" of 15" Pipe AT 90° E = 4' FL line 15" Pipe AT BOX =	189.03 m.H. 188.70 TP Box 189.03 183.34 FL C 5.69
7+40	189.03 186.40 C 2.63
7+00	189.99 187.20 C 2.79
6+60	188.63 182.91 C 5.72
6+20	188.50 182.51 C 5.99
6+20	188.25 182.12 C 6.13
6+20	187.96 181.71 C 6.25

Grade Only
191.61
188.00
C 3.61
(on 51st to 1st)

FL 15" Pipe
188.00 at inlet
C 3.61

FL 15" Pipe at Pipe Line
188.20 = FL 15" Pipe at Pipe Line
C 3.46

184.20

189.86
183.82
C 6.04

(15" on Hill Top) 187.58 m.H.
187.60 TP
FO.02 Box
187.58 FL
180.18 m.H.
C 7.40 Pipe
187.58 FL
179.93 m.H.
C 7.65 Pipe
187.58 FL
180.18 m.H.
C 7.40 Pipe
187.58 FL
179.93 m.H.
C 7.65 Pipe

189.03
186.40
C 2.63
189.99
187.20
C 2.79

CO. GRADES: 47-46 ST. - NLY Line Hilltop
 N'ly 823.69' (on 62y CO/47-46)

STA	RT. (Ely)		STA	RT. (Ely)	
	CB	P.L.		CB	P.L.
1+50	187.31 187.74 Fo.43	186.46 187.74 F1.28	3+50	188.08 188.75 Fo.35	187.31 188.43 F1.12
1+25	187.19 187.65 Fo.46	187.65	3+25	188.09 188.34 Fo.25	188.34
1+00	187.26 187.56 Fo.30	185.81 187.56 F1.75	3+00	187.95 188.25 Fo.30	187.29 188.25 Fo.96
0+75	187.33 187.48 Fo.15	187.48	2+75	188.14 188.14 Fo.03	188.17
0+50	187.20 187.39 Fo.19	185.80 187.39 F1.59	2+50	187.77 188.08 Fo.31	187.13 188.08 Fo.95
0+30	187.32 187.32 Fo.24	187.32	2+25	187.66 187.99 Fo.33	187.99
0+20 = CB & Prop B.C.	187.20	186.91 187.20 Fo.29	2+00	187.60 187.91 Fo.31	187.03 187.91 Fo.88
0+00 = NLY Line Hilltop (see 1936 for N'ly Rd)			(1+85 = E. 26' corner. done)		
			1+75	187.44 187.82 Fo.38	187.82
R.M. Dir. Elev. Rods:		186.81 = 1/2 to E 47-46 + Hilltop			

47.46 ST. (CONT.)

STA.	RT (Ely)		STA.	removed out	
	CB	P.L		CB	P.L
5750	189.10 189.12 F0.02	190.19 189.12 C1.05	6+75	190.44 191.60 F0.16	191.75 191.60 C0.15
5725	189.01 189.03 F0.02	189.03	6+72 = E 15' Comm. Drive)		
5700	188.66 188.74 F0.28	189.51 188.94 C0.57	6+60 = NY END 0-2 INLET	191.63 190.26 G C1.37	191.63 191.12 TPO C0.51
4475	187.99 188.86 F0.87	188.86	6+54 = E.V.C		190.84 190.93 TPO F0.07
4450	188.53 188.72 F0.24	189.04 188.77 C0.27	6+44 = SHY END Type B-2. ca 15' inlet.	191.49 189.80 G C1.69	191.49 190.60 TPO C0.89
4425	188.35 188.68 F0.33	188.68	6+34		190.47 190.34 C0.13
4400	188.36 188.68 F0.32	187.85 188.60 F0.75	6+14	189.58 189.78 F0.20	190.41 189.78 C0.63
(3+87 = E 26' Comm. Drive)			(6+06 = E 38' Comm. Drive)		
3475	188.18 188.67 F0.33	188.51	5+74	189.43 189.50 F0.07	190.30 189.50 C0.80
			5+74	189.18 189.23 F0.05	190.18 189.75 C0.75
			5+54 = B.V.C.		189.30 189.13 C0.17
					190.17 189.13 C1.04

49 1/2 ST. (CONT.)

STA.	RT. (E4)	CB	P.L.
chk: Sta 7400 & Nail 192.32 = 192.34 (BK 2147 P9.64)			
chk Sta 7400 & Nail 192.32 = 192.33 (" " " ") (CB grade)			
8+83.69 (END CONST)	198.05 198.28 F0.23	196.31 198.20 F1.97	
8+75	197.81 198.01 F0.20	198.01	
8+50	196.89 197.23 F0.24	192.84 197.23 F4.39	
8+25	196.22 196.45 F0.23	196.45	
8+00 = gid Brk	195.99 195.67 F0.28	192.58 195.67 F3.09	
7+75	194.61 194.85 F0.24	194.85	
7+50	193.74 194.03 F0.29	192.13 194.03 F1.90	
7+25	192.89 193.22 F0.33	193.22	
7+00	192.16 192.41 F0.25	191.60 192.41 F0.81	

Clark
Shepherd
Binner
Oneil

11-10-54
W.O. 62401

INDEXED

Loc. of Eler's Street LIGHTS
55' 1/2 ST N'LY OF N. Line
College Park LOT I BIK 17

REF: DWG: 11659-L
11655A-L

439.98 = 439.98 - (STG. B.M.)

(9+13.22 = F.C.)
E 554h

7+85 #5

434.64
434.93
Co. 29

6+10 #4

437.34
436.63
Co. 71

4+35 #3

438.76
438.52
Co. 24

(8+92.37 = F.C. 554h)
Δ = 85° 15' 50" 49"
ER = 350'

2+45 #2

439.25
438.53 ca
Co. 72

0+55 #1

438.78
437.58 elev ca
C/1.20

0+00 = N. line College Park

B.M.: DIKE by Rod.

439.98 = N.E. B. P
MANNY 1554h

Clark
Shepherd
Bruner
O'Neil
12-7-54
MO. 31119

CITY HTS SEWER: BIKS III-121-122
ET AL -

M.H. # 7 Ely to M.H. # 20, S/Ly
to M.H. # 19 - Ely to M.H. # 18 at ab. to D.H.
PILEY BK 138

Ref: F.B. 2278
DWG'S: 2291-D, 2292-D, 2293-D,
2294-D, 2295-D
DWG'S: 5076-B, 5077-B, 5078-B

245-88 = 245-87 - Hub [8+6897]
[82278-38]

STA

Eley's

STA:

Eley's:

2+45

INDEVED

231.28
225.96
C 5.32

4+20.07

252.84
238.92
C 13.92

2+10

231.17
225.82
C 5.35

4+08.07

252.22
237.82
C 14.40

1+75

232.14
225.68
C 6.46

3+96.07

251.39
236.01
C 15.38

1+40

235.05
225.54
C 9.51

3+84.07

249.22
233.69
C 15.53

1+05

238.05
225.40
C 12.65

3+72.07

246.77
230.66
C 16.11

0+70

239.60
225.26
C 14.34

3+58.57 = M.H. # 20

Δ = 90° 05' 30" RT.
stubs set 10' + 25' FT AT 45° ANGLE.
32' (replaced)

replaced stub 236.66
236.73
226.41 FL
C 10.32
C 10.25

0+35

241.34
225.12
C 16.22

3+50

240.11
226.38
C 13.73

0+00 = M.H. # 7

stubs set 10' + 20' RT Σ M.H.

238.54
224.98 = FL
C 13.56

3+15

230.84
226.24
C 4.60

2+80

231.60
226.10
C 5.50
232.36
226.10
C 6.26

B.M. Dir. Elev. Rod:

232.54 = [HUB 4100⁵³ F.B. 2278-62]

STUBS 6" RT E

STUBS 6" RT E

etc.

STUBS 6" RT E

M.H. #7 - 20 - 19 - 18 --- #4 - 10 D.E.

STA.	ELEV'S:
6+80	246.84 240.77 C 6.07
6+45	245.48 240.39 C 5.09
6+13.57 = M.H. #19 Δ = 90° 04' LT. Stubs set 10' + 20' RT at 90° BR TO RY.	244.48 240.04 = F.W. C 4.44
6+00	246.76 239.98 C 6.78
5+65	250.31 239.84 C 10.47
5+30	252.09 239.70 C 12.39
4+95	252.34 239.56 C 12.78
4+60	253.83 239.42 C 14.41
4+32.07 = F.V.C.	253.41 239.31 C 14.10

Stubs 6' RT
1.0' S

Stubs 6' RT

0.4' S

(51.48)

(20.93)

STA.	Elev's:	REMARKS
9+75	251.51 242.82 C 8.69	251.51 242.82 C 8.69
9+40		249.18 242.68 C 6.50
9+05	248.86 242.54 C 6.32	247.80 242.54 C 5.26
8+70	248.49 242.40 C 6.09	247.77 242.40 C 5.37
8+35	251.95 242.26 C 9.69	252.12 242.26 C 9.86
8+03.41 = M.H. #18 Δ = 30° 18' 15" LT. Stubs set 6.22 + 16.22 LT ON SPLIT A.		253.66 242.13 = F.L. C 11.53 C 11.48
7+85	249.68 241.93 C 7.75	254.59 241.93 C 12.66
7+50	256.11 241.54 C 14.57	252.96 241.54 C 11.32
7+15	254.33 241.16 C 13.17	252.28 241.16 C 11.12

Stubs 6' RT

0.4' S

Stubs 6' RT

1.0' S

Set TBM = NAIL IN B/L # PA 2881 = 249.53
- [OFF 2X2 HUB 8468.97 FB # 2278-4-56] = 245.87

M.H. # -20 -19 et al to #14 (CONT.)

STA.	ELEV'S:
12+70	276.70 269.23 C 7.47
12+35	274.74 265.48 C 9.26
12+00	271.21 261.73 C 9.48
11+65	267.42 257.97 C 9.45
11+30	263.00 254.21 C 8.79
10+95	259.03 250.46 C 8.57
10+60	254.35 246.71 C 7.64
10+25.54 = M.H. #17 Δ = STUBS SET 6.94 & 12.29 RT ON E. OF TANG.	251.80 243.02 = F.L. C 8.78
10+10	251.30 242.96 C 8.34

↑
10.722

0.406

Set T.B.M. ON 1x1 12.29 RT OF M.H. #17
ON E. OF TANG. = 251.41
[OFF 2x2 HUB 4+57, F.B. 2278-54]

47

STA.	ELEV'S:
15+75	293.76 285.27 C 8.49
15+40	293.03 284.29 C 8.74
15+05	292.14 283.31 C 8.83
14+70	291.24 282.33 C 8.91
14+35	290.27 281.35 C 8.92
14+00	288.84 280.37 C 8.47
13+65.04 = M.H. #16 P.O.T. STUBS SET 10' 42" LT	286.95 279.41 = F.L. C 7.54
13+40	283.82 276.73 C 7.09
13+05	281.05 272.98 C 8.07

↑
2.806

↑
10.722

M.H. #7 - 20-19 et al to #14 (Cont.)

STA

Elev's:

18+80 299.60
291.55
C 8.05

18+45 299.25
291.03
C 8.22

18+10 298.81
290.52
C 8.29

17+75 297.92
290.00
C 7.92

1.48%

17+40 297.12
289.49
C 7.63
(Set T.B.M. 291.38 Nail Pole #3947
At STA. 14+55 LT)

17+07.54 = M.H. #15
P.O.T.
Stubs set. 10' N 20' LT
296.48
289.00 = FL
C 7.48

16+80 295.83
288.22
C 7.61

19+77.54 = M.H. #14
P.O.T.
Stubs set 10' 20' (LX) S
300.03
293.00 FL
C 7.03

16+45 294.99
287.23
C 7.76

2.80%

19+50 300.08
292.59
C 7.49

16+10 294.21
286.26
C 7.95

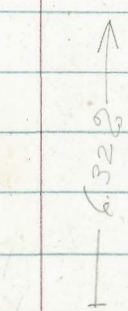
19+15 299.89
292.08
C 7.81

M.H. #7 n'ly to M.H. #6 - 5 - 7 etc
to M.H. #1 + D.END. T.HORN ST.

cdkt

256.41 = 256.45 + 22
HUB 0100
EQUICE VALLEY
BLK 140
[FA 2278-61] 99

STA.	Elev's:
1+90	250.87 242.34 C 8.53
1+55	248.12 240.13 C 7.99
1+20	244.97 237.92 C 7.05
0+85	241.62 235.71 C 5.91
0+48 = B.V.C	241.46 242.03 233.37 C 8.66 C 8.09
0+36	241.96 232.28 C 9.68
0+24	242.50 230.55 C 11.95
0+12	241.70 228.04 C 13.66
0+00 = M.H. #7 (see P. 45)	224.98
B.M. Div. Elev. Rod:	232.54 = [2X2 HUB #2278-62]



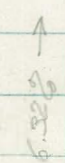
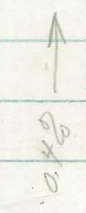
5465 87 6.0 207

(stubs set 6' RT)

(knocked out!)

STA.	Elev's:
4+85	265.25 250.70 C 14.55
4+50	264.31 250.56 C 13.75
4+15	262.18 250.42 C 11.76
3+80	260.37 250.28 C 10.09
3+45	258.53 250.14 C 8.39
3+11.05 = M.H. #6	255.97 250.00 = F.A. C 5.97
2+85.52 = mid PT	256.22 248.41 C 7.81
2+60 = B.C. LT	254.70 246.80 C 7.90
2+25	254.83 246.80 C 8.03
	252.75 244.57 C 8.18
	232.54 = [2X2 HUB #2278-62]

(LT 9 for stubs)



107. Def. = 10° 48'
C-ch = 51.5'
R = 131.43

knocked out

M.H. #7 x/4 to #6.5, etc to #1 +
D.END.

STA.	Elev's:
7+65	263.13 251.82 C 11.31
7+30	262.08 251.68 C 10.40
6+95	258.67 251.54 C 7.13
6+60	257.43 251.40 C 6.03
6+25	260.55 251.26 C 9.29
5+90 (not set)	
5+86.05 = M.H. #5 $\Delta = 22^{\circ} 05' RT$ Stubs Set 10' x 20' LT. 9. At 90° BK TANG.	258.60 256.10 = F.L. C 7.50
5+55	261.83 250.98 C 10.85
5+20	264.40 250.84 C 13.56

Stubs 6/RT

0.45
↑

0.45
↑

knocked out
by Contractor

STA.	Elev's:
10+60	265.39 256.41 C 8.98
10+25	265.78 255.12 C 10.66
9+90	265.13 253.83 C 11.30
9+56.05 = M.H. #4 $\Delta = 111^{\circ} 38' 30'' LT$ Stubs Set 10' x 20' RT 9 (N/4) At 90° FV. TANG.	265.94 252.58 = F.L. C 13.36
9+40	258.67 252.52 C 6.15
9+05	260.52 252.38 C 8.14
8+70	261.92 252.24 C 9.68
8+35	262.82 252.10 C 10.72
8+00	263.95 251.96 C 11.89

3.69
↑

0.45
↑
Stubs 6/RT

knocked out
by Contractor

MN #7 nly to #6 - 5 etc to #1
D. END. - TYPICAL ST.

STA.	Elev's:
13+68.55 = MN #2 ROT. Stubs set - 10' x 20' RT	293.09 285.00 C 8.09
13+40	290.66 282.15 C 8.51
13+05	287.32 278.65 C 8.67
12+70	284.15 275.15 C 9.00
12+35	282.18 271.65 C 10.53
12+00	275.79 268.15 C 7.64
11+65	272.04 264.65 C 7.39
11+30	267.76 261.15 C 6.61
10+96.05 = MN #3 Δ = 90° Stubs set 8' x 20' OK. MN ON SPLIT L (to RT)	265.98 257.75 = F.L. C 8.23

100' ←

Stubs 6' RT

100' ←

80' ←

STA.	Elev's:
16+90	300.96 288.11 C 12.85
16+45	301.15 287.76 C 13.39
16+10	300.58 287.41 C 13.17
15+75	300.03 287.16 C 12.87
15+40	299.38 286.71 C 12.67
15+05	298.44 286.36 C 12.08
14+70	297.43 286.01 C 11.42
14+35	296.35 285.66 C 10.69
14+00	294.97 285.31 C 9.66

Stubs 6' RT

80' ←

M.H. #7 N by to M.H. #6-5, #4 etc. to #1 & D.END

CHK'S

CHK'S

305.73 = 305.72 = S.W. CORN
M.H. 39'4" x 4'
TWOEN

19+65.92 = D.END.

292.90
290.10 = F.L.
C 2.80

18+75

294.08
289.85
C 4.23

18+40

294.81
289.57
C 5.24

18+05

296.29
289.29
C 7.00

17+70.92 = M.H. #1

$\Delta = 39^\circ$ RT
Stubs 10' x 20' RT
I 4. BK 1/4"

299.18
289.02 = F.L.
C 8.16

17+50

298.10
288.81
C 9.29

17+15

299.44
288.46
C 10.98

Stubs 6' x 2'
38.0

100.0

EXIST. M.H. & OLIVE (DWG: 449-D) + WABASH AVE
N.E. to M.H. #7

52

REF: F.B. #2278-5
DWG. 11258-L
MO 21169

INDEFINITE

STA
note (M.H. moved) SLY 3.5' FROM M.H. #1
OF PLAN
H. COLE

Elev's

1789.46
~~1792.96~~ = M.H. #2
Stubs Set 10' x 20' RT

180.12
169.96 = F.L.
C 10.16

1471.96

176.85
169.24
C 7.61

1150.96 = M.H. #3
Stubs set 10' x 20' RT
 $\Delta = 58^\circ 51'$ LT

175.94
168.40
C 7.54

1140

175.05
167.98
C 7.07

1105

174.91
166.69
C 8.22

0+70

174.50
165.39
C 9.11

0+35

171.61
164.10
C 7.51

D.P.O. = EXIST. M.H. 15' River
& Olive + WABASH AVE

162.14 = F.L.

169.69
162.80 = F.L.
C 6.89

B.M. DIR. Elev. Rod:

169.69. Run EXIST. point
Olive + WABASH

EXIST M.H. ϕ Olive & WABASH AVE N.E.V. to
M.H. #7 (cont.)

M.H. #20 (RILEY BRK 143) N.V. to
M.H. #8 (RILEY BRK 111)

CHK: 231.71 = 231.70 = T.B.M. 64
OF M.H. #7 - 1.0 FT. - 1.0 FT.

3+23.05 = M.H. #7 See pg 45
New Ref: Stubs set 10' 4' 20' LT
(cut on Pgs 45 from stub set at 10' RT - M.H. on Ely 7000)

3+00 238.14
224.41
C 13.73

2+75 236.24
223.78
C 12.46

2+43.58 = M.H. #1
2' - 20' 25' LT
Stubs set 10' 4' 32' RT

2+23.96 = ϕ Anchor WALL
Stubs set 10' 4' 20' RT

CHK 175.36 = 175.37 on HUB
(483.14 FB 2278)

2+00.96 (8' ahead of L) (stub 8' RT E)
192.53
182.72
C 9.81

1+92.96 = ϕ Anchor WALL
 ϕ PIPE
Stubs 10' LT + 10 RT ϕ
181.43
170.08 = F-Line
11.35

0+80.85 = E.V.C

0+74.85

0+68.85

0+56.85

0+44.85

0+32.85

0+20.85

0+08.85

0+00 = B.V.C
= M.H. #20
J = 3+58.57
See Pg 45

B.M. Dir. Elev. Rod:

257.16
245.31
11.85

256.88
245.10
C 11.78

256.19
244.73
C 11.46

255.36
243.25
C 12.11

253.60
241.04
C 12.56

250.24
238.08
C 12.16

244.75
234.38
C 10.37

238.41
229.94
C 8.47

226.41 = F.L.

245.87 - 222 HUB. 9+68.97
FB 2278 - 56.4

Stubs set 6' RT

M.H. #20 N'ly (Cont.)

STA. 3+09.85 = M.H. #19
 (93) Stubs set P.O.T. 10' + 20' RT.
 2+86.85
 (93)
 2+63.85 = Grid Bmk
 12
 2+51.85 = Grid Bmk
 2+40
 2+05
 1+70
 1+35
 1+00

Sta 6 RT

8.618 ↑
↓
↑
1.522 ↓

Elev's: 265.58
 252.52
 C 13.06
 264.05
 250.52
 C 13.53
 262.49
 248.52
 C 13.97
 261.73
 247.91
 C 13.82
 261.12
 247.73
 C 13.39
 258.48
 247.19
 C 11.29
 257.80
 246.66
 C 11.14
 257.59
 246.13
 11.46
 257.30
 245.60
 11.70

STA. 6+15.35 = M.H. #12
 P.O.T.
 Stubs set
 5+85
 5+50
 5+15
 4+80
 4+45
 4+10
 3+75
 3+40

10.50 ↑

Elev's: 390.78
 284.60
~~C 5.98~~
 C 6.18
 289.45
 281.41
 C 8.04
 286.47
 277.74
 C 8.73
 283.03
 274.06
 C 8.97
 278.47
 270.39
 C 8.08
 275.12
 266.71
 C 8.41
 272.93
 263.04
 C 9.89
 268.52
 259.36
 C 9.16
 264.01
 255.69
 C 8.32

STA.	Elev's	STA.	Elev's
9+30	290.95 286.60 C 4.35	12+35	303.83 291.56 12.27
8+95	294.51 286.38 C 8.13	12+00	303.37 290.91 12.46
8+60	296.11 286.16 C 9.95	11+65	302.53 290.26 C 12.27
8+25	297.10 285.94 C 11.16	11+30	301.56 289.61 C 11.95
7+90	297.25 285.71 C 11.54	10+95	300.27 288.95 C 11.32
7+55	296.47 285.49 C 10.98	10+60	298.43 288.30 C 10.13
7+20	295.30 285.27 C 10.03	10+25	296.41 287.65 C 8.76
6+85	293.70 285.04 C 8.66	9+90.01 = M.H. #11 P.O.T. Stubs set 10' 4 1/2 RT.	295.84 287.00 = P.L. C 8.84
6+50	292.75 284.82 C 7.93	9+65	292.53 286.84 C 5.69

← 0.6490

← 1.860

← 0.6510

M.H. #20 - NLY - (cont.)

STA.	Elev's
15+35	307.67 293.56 C14.11
15+00	307.58 293.42 C14.16
14+65	306.93 293.28 C13.65
14+30	306.58 293.14 C13.44
13+95	306.22 293.00 C13.22
13+60	305.63 292.86 C12.77
13+25	305.03 292.72 C12.31
12+90.01 = M.H. #10 P.O.T. Stubs set 10' @ 20' RT	304.31 292.58 = FL C11.73
12+70	304.10 292.21 C11.89

Stubs 6' RT

C 14.11

C 14.11

STA.	Elev's
18+15	302.32 302.77 294.68 294.68 C7.64 C8.09
17+80	303.68 304.02 294.54 294.54 C9.14 C9.48
17+45	304.87 305.11 294.40 294.40 C10.47 C10.71
17+10	305.79 305.82 294.26 294.26 C11.53 C11.56
16+75	306.57 306.79 294.12 294.12 C12.45 C12.67
16+40	306.80 306.96 293.98 293.98 C12.82 C12.98
16+05	307.29 307.29 306.96 306.96 293.84 293.84 C13.12 C13.45
15+90.01 = M.H. #9 P.O.T. Stubs set 10' @ 20' RT	307.94 307.94 307.28 307.28 293.78 = FL 293.78 = FL C13.56 C13.56 C14.16 C14.16
15+70	307.64 307.64 293.70 293.70 C13.94 C13.94

Stubs 6' RT

C 14.11

C 14.11

CONTRACTOR

by

Knocked

out

included - out

M.H. #20-Nly

CHK	305.76	= 305.72 = SW. CONC. MONUMENT 394 ¹ / ₂ THORN
-----	--------	---

(=END LINE) 18+93.93 = M.H. #8 PO.T. Stubs set 10' + 20' RT & L.	299.22 295.00 4.22	299.26 295.00 = P.L. C 4.26
---	--------------------------	-----------------------------------

18+05	299.95 294.96 C 4.99	299.94 294.96 C 4.98
-------	----------------------------	----------------------------

18+50	301.18 294.82 C 6.36	301.30 294.82 C 6.48
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Stubs set 6.5

0.48

Knocked out by Contractor

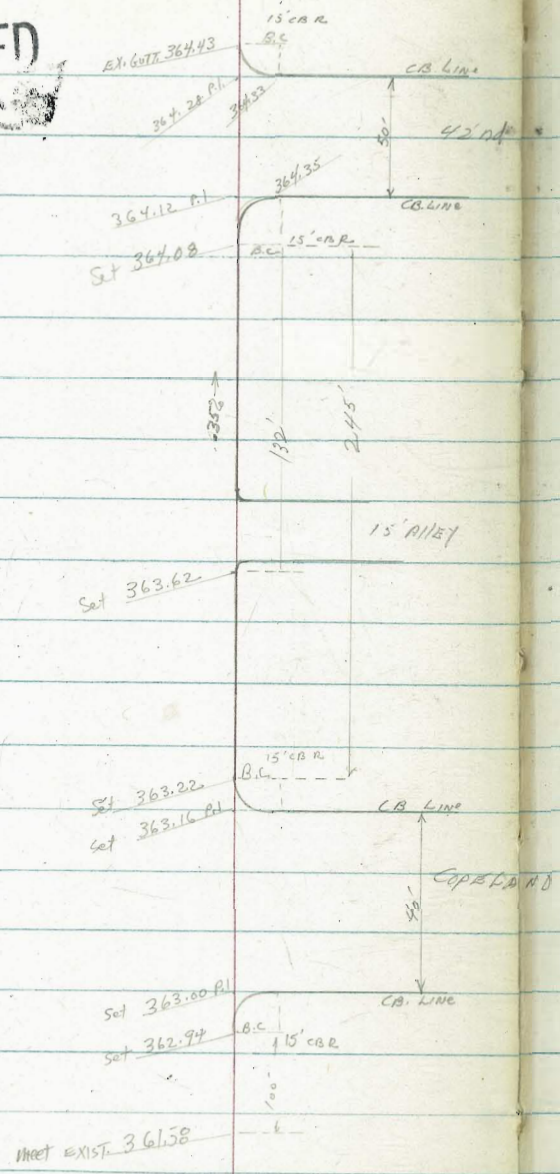
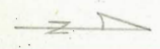
Clark
Shepherd
Stump
Over

GUTT GRADES: MEADE; 42nd to Copeland.

2-2-55
W.O. 20008

INDEXED

Note: No Ref. Dike's
Grades established in Field
by order of Office



B.M.

366.07 = N.W.P.P
MEADE + MARLBOROUGH

Clark
Shepherd
Bruner
O'Neil

ALLEY BIR 3 - LA MESA COLONY

68th to 67th

3-1-55
W.O. 31040ReF: F.B.#1840-27
DWG: #11603-L

STA.	LT	E	RT	STA.	LT	E	RT
	INDEXED			3+30 = W.S. IN RT.			454.08 453.04 = Tp. Pav. C 1.04 to tp. Pav.
1+50	452.77 453.54 F0.77		453.95 453.74 C 0.21	3+25	453.33 452.86 C 0.47		454.59 453.06 C 1.52
1+25	453.57 453.63 F0.06		454.59 453.83 C 0.76	3+05 = Sew. LAT #2 on LT.	452.6 447.9 at Prop C 4.7	452.60 447.00 on 440.18 main 5.6 C 1.242	
1+00	454.02 453.73 C 0.29		454.15 453.93 C 0.22	3+00	452.64 453.96 F1.32		454.26 453.16 C 1.10
0+75	453.74 453.82 F0.08		454.42 454.02 C 0.40	2+75	452.55 453.06 F0.51		453.89 453.26 F0.17
0+50	453.85 453.92 F0.07		454.71 454.12 C 0.59	2+50	452.43 453.15 F0.72		453.41 453.35 C 0.06
0+30 = 2nd Brk	454.46 454.00 C 0.46		455.02 454.20 C 0.82	2+25	452.31 453.25 F0.94		453.40 453.45 F0.05
0+15	454.59 453.90 C 0.69		455.01 454.10 C 0.91	2+00	452.42 453.34 F0.92		454.31 453.54 C 0.77
0+00 = Wly Line 68th	453.79 453.80		453.98 454.00	1+75	452.70 453.44 F0.74		454.05 453.64 C 0.41
B.M. D.V. ELEV. ROD:			453.70 = S.W. B.P. 67th + EL CAJON				

STA	LT.	E	RT.	STA.	LT.	E	RT.
5+00 = grid Bk	452.16 451.70 C 0.46		452.54 451.90 C 0.64	chk.		453.70 = 453.70 = STV B.M.	
4+75	453.37 451.95 C 1.42		452.83 452.15 C 0.68	6+43.04 (6+41.92) = E Line map 67th b.T.	450.97 451.04 F 0.07	450.97 450.80 C 0.17	
4+50	453.28 452.20 C 1.08		453.69 452.40 C 1.29	6+41.06 (6+39.9) = F.L. line map 67th E			
4+35	453.17 452.35 C 0.82		454.16 452.55 C 1.61	6+39.08 E Line (6+37.98) = 67th map on RT.		451.81 451.34 C 0.47	
4+20 = grid Bk	453.57 452.50 C 1.07		454.15 452.70 C 1.45	6+25	450.85 451.12 F 0.27	452.32 451.39 C 0.93	
4+00	453.60 452.58 C 1.02		454.30 452.70 C 1.52	6+00	451.66 451.24 C 0.42	452.36 451.50 C 0.86	
3+75	453.65 452.68 C 0.97		454.26 452.87 C 1.39	5+75	451.55 451.35 C 0.20	452.04 451.60 C 0.44	
3+55 = Sew LAT. #1 on RT.	main 440.00 454.30 447.00 Bk C 7.3		454.30 447.90 at prop C 6.40	5+50	450.87 451.47 F 0.60	451.60 451.70 F 0.10	
3+50	453.47 452.77 C 0.70		454.20 452.97 C 1.23	5+25	450.83 451.58 F 0.75	452.50 451.80 C 0.70	

Clark
Overt
Kathy
3-15-55
W.O. 20638

IMP'S: E. TECOLOTE ROAD
From PT. 764.73' W'LY OF W. Line
WELLINGTON ST, to PT. 700' W'LY
Hence.

REF: DWG: 5566-B
9174-L
FB. 2136

INDEXED

STA.	LT.		RT (N'LY)		STA.	LT.		RT (N'LY)		
	CB	E	CB	Prop.		Prop	CB	E	CB	Prop.
1453.7=END CB AT PROP.	361.73				4+50		360.47 357.10 C 3.37			360.29 357.10 C 3.19
1450 RT ONLY (1448=FC.DV)				361.72 361.54 C 0.18	4+40=FC		360.47 357.40 C 3.07			360.18 357.40 C 2.78
1436=EDN. ST (1424=FC.DV)					4+00		360.90 358.50 C 2.40			360.20 358.50 C 1.70
1418.3=END CA AT AMP.	361.93				3+60		361.23 359.42 C 1.81			360.57 359.42 C 1.15
1404=BC DR LT.	362.20 361.82 C 0.38				3+20		361.60 360.14 C 1.46			360.85 360.14 C 0.71
1400	361.84			361.84 361.84 grade	2+80		361.69 360.66 C 1.03			360.76 360.66 C 0.10
0+50	362.86 362.14 C 0.72			362.51 362.14 C 0.37	2+40=B.V.C.		362.00 361.00 C 1.00			361.21 361.00 C 0.20
0+00=PT. 764.73 W'LY OF W. Line WELLINGTON ST (=10+84.73 DWG. 9174-L)	362.41 362.44 EAST CA TR. (PLAN)			dx 362.41 (PLAN) EAST TO CA = 362.44	2+00		361.77 361.24 C 0.53			361.39 361.24 C 0.15
(Stubs set on Prop. Lines) grades to tp. CB's					1468=BC DR. LT.		361.80 361.44 C 0.36			

Set T.B.M. chd w'ly end s'ly CB
dwg: 9174-L (10+84.73) PLAN: Elev = 362.41
(2000 CONST)

Note: See Pg 62 For Bench Levels;
B.M.: DIR. Elev. ROD

356.61 = LT DISC. RE
ELUNDA VISTA RD + S.L.
32
RL 1203

E. T. CO. L. O. T. E (CONT.)

STA	LT PROP	CR	E	RT(NLY) CR PROP	LT	E	RT
Beg 20' wide grading strip = END grading road.							
7+00	355.76 349.61 C 6.15			353.37 349.61 C 3.76			
6+50	355.68 351.10 C 4.58			354.29 351.10 C 3.19			
6+08 = B.C. Dr. LT.	357.11 352.37 C 4.74						
6+00 RT only				355.70 352.60 C 3.10			
5+93.7 = END CR RT PROP (5+88 = E.C. Dr.)	352.92						
5+76 = EDIVE CR (5+64 = E.C. Dr. LT.)							
5+58.3 = END CR PROP.	357.06						
5+50 RT only				359.31 354.10 C 5.21	8+50		352.36 348.11 C 4.25
5+44 = B.C. Dr. LT.	359.09 354.29 C 4.80				8+00		354.61 348.61 C 6.00
5+20	360.05 355.60 C 4.45			360.05 355.60 C 4.45	7+50		356.84 349.11 C 7.83

(grading for drainage only
 on 1/2 grade from 7+00)

BENCH LEVELS FOR E. TECOLOTE RD
See pg 60

CHK:		8.09	356.59	= 356.61	= STG. B.M.
T.P.	1.69	364.68	5.46	362.99	
T.P.	3.57	368.45	1.54	364.88	
T.P.	2.75	366.42	5.06	363.67	
T.P.	6.32	368.73	6.15	362.41	= Ch. \square TP Swily CR-End E. TECOLOTE RD - 10184.73 DWG. 9174-L
T.P.	4.34	368.56	3.61	364.22	
T.P.	6.67	367.83	5.53	361.14	
T.P.	1.80	366.67	3.59	364.87	
T.P.	5.38	368.46	1.51	363.08	
B.M.	7.98	364.59		356.61	= Elev. L ^x Disc ELINDA VISTA RD \square S.L.P. 1203

Clare
Shepherd
Crew

IMP'S Alley BR 88 - OCEAN BEACH EXT. #2

Ref: 2313-12
DWG: 11044-L

3-22-55
V.O. 32256

IND. PIPING - From EXIST. 60" Pipe 22.5' SLY & ELY
of NWLY Line BACON to pt. 250' NWLY of
NWLY Line BACON (in ALLEY)

STA.

STA.

1464.5 = E Support Wall

1450 INDEXED

4.37
-1.93
C 6.30

1425

4.31
-2.13
C 6.44

1417.5 = E Support Wall

1400

4.95
-2.32
C 7.27

0496.5 = E Support Wall

0475

4.97
-2.52
C 7.49

2472.5 = E TYPE D" Catch Basin

3.56
2.25 = TP GRATE
C 1.31

3.56
-1.00 = FL
C 4.56

0452.5 = E Support Wall

0450

5.37
-2.71
C 8.08

2450

3.50
-1.17
C 4.67

0425

5.20
-2.90
C 8.10

2425

3.68
-1.35
C 5.03

2423.5 = E Support Wall

0400 = EXIST 60" Pipe
22.5' SLY of NWLY Line
BACON & 4' NWLY of E ALLEY

F.L. 12' or 12" =
Pipe C 7.87

5.10 = F.L. 12' or
EXIST 60" Pipe
(over walls
54' 10" RT)

2400

3.88
-1.54
C 5.42

B.M. No. Elev. Pvc

4.47 = N.W. L&T
BRIGHTON & BACON

1475

4.41
-1.74
C 6.15

Sheds set 5' N of E drain
at 1785

ALLEY PAV. & Sew. LAT.
GRADES - BLK. 88 (CONT.)

STA.	LT.	RT.
1430	3.27 3.25 C0.02	3.41 3.25 C0.16
1405	3.35 3.31 C0.04	3.51 3.31 C0.20
0+80	3.38 3.38 grade	3.68 3.38 C0.30
0+70 = E.V.C.	3.64 3.41 C0.23	4.21 3.41 C0.80
0+50	3.65 3.88 F0.23	4.21 3.88 C0.33
0+30	4.90 5.08 F0.18	6.81 5.08 C1.73
0+20	5.55 5.84 F0.29	6.70 5.86 C0.84
0+10	6.25 6.52 F0.27	7.48 6.60 C0.88
= B.V.C.	chk: 6.88	chk: 6.99
0+00 = S Ely Line ABBOTT	6.91 FIRST	7.02 FIRST

B.M. (See pg 63)

STA.	LT.	RT.
3+50 (Inlet)	3.54 2.71 C0.83	3.53 2.71 C0.82
3+30 = B.V.C	Knobbed out 3.70 3.62 2.72 2.72 C0.78 C0.90	3.37 2.72 C0.65
3+30 = Sew. LAT #2 - LT.	-2.79 Prop. C0.09	-3.79 C6.89
3+05	3.40 2.78 C0.62	4.03 2.78 C1.25
2+90 = Sew. LAT #3 - LT.	3.38 -2.2 Prop. C5.58	-3.38 -3.38 C6.68
2+80	3.35 2.95 C0.50	4.40 2.85 C1.55
2+55	4.05 2.92 C1.13	3.34 2.92 C0.42
2+30	3.56 2.98 C0.58	3.47 2.98 C0.49
2+10 = Sew. LAT #4 RT.	-2.0 Prop.	4.07 -3.68 C7.67
2+05	3.26 3.05 C0.21	3.57 3.05 C0.52
1+80	3.65 3.12 C0.53	3.89 3.12 C0.77
1+55	3.71 3.18 C0.53	4.09 3.18 C0.91

ALLEY BK 88 (CONT.)

STA	LT.	RT.
5740	5.25 5.11 Co.14	5.05 5.09 Fo.04
5720	5.37 5.02 Co.35	5.12 5.00 Co.12
5700	4.37 4.83 Fo.46	4.39 4.81 Fo.42
4780 = B.V.C.	4.47 4.52 Fo.05	4.20 4.52 Fo.32
4755	4.33 4.08 Co.25	4.40 4.08 Co.32
4730	4.18 3.65 Co.53	3.76 3.40 3.65 3.65 Co.11 Fo.25
4710 = E.V.C.	4.10 3.30 Co.80	4.44 3.30 Co.14
3790	3.74 2.99 Co.75	3.65 2.99 Co.66
3770	3.69 2.80 Co.89	3.46 2.80 Co.66

~~4.65~~ ^{knocked out}
4.28
Co.57

(OFFSHOULDER)
3.69
2.75
Co.124

STA	LT.	RT.
CHK:		4.47 = 4.47 = STG B.M
670032 = Ninety Line BACON	4.96 4.98 EXIST	4.89 4.89 EXIST
5780.16	5.73 5.04 Co.67	4.96 4.96 grade
5770 = Sew LAT #1 - LT.	5.34 5.30 Prop. 5.34 5.48 Co.30	5.34 -0.2 G 5.54
5760 = E.V.C.		5.00 5.00 Fo.06

INDEVER / ALLEY BIK 76 / OCEAN BEACH

STA.

LT.

LT.

RT

RT

RT

STA.	(N.Y.) LT.	RT	STA.	LT.	LT.	RT	RT
1+60 = E.V.C.	10.08 9.93 Co.15	10.69 9.84 Co.85	3+75	6.18	7.67 6.25 F 1.58	6.18	5.59 6.25 Fo.66
1+40	11.22 10.40 Co.82	10.69 10.26 Co.43	3+50	6.26	5.38 6.32 Fo.94	6.26	6.32 6.32 Grade
1+20	11.24 10.72 Co.52	10.54 10.56 Fo.02	3+40 = E.V.C.	6.29	6.64 6.35 Co.29	6.29	6.01 6.35 Fo.34
1+00	11.67 10.90 Co.77	10.95 10.72 Co.23	3+20	6.77 6.41 Co.36		6.23 6.40 Fo.17	
0+80	12.16 10.93 Co.1.23	11.29 10.76 Co.53	3+00	7.18 6.64 Co.54		6.93 6.63 Co.30	
0+60	12.18 10.81 Co.1.37	11.08 10.66 Co.42	2+80	7.61 6.99 Co.62		7.12 6.95 Co.17	
0+40	11.46 10.55 Co.91	10.81 10.44 Co.37	2+60 = B.V.C.	8.22 7.45 Co.77		7.48 7.39 Co.09	
0+20	10.80 10.14 Co.66	10.49 10.08 Co.40	2+35	8.65 8.07 Co.58		9.49 8.00 Co.49	
0+00 = ABBOTT ST = B.V.C.	9.58	9.60 9.60	2+10	8.81 8.69 Co.12		9.83 8.62 Co.1.21	
B.M.	DIV. Elev. Rod:	10.13 = N.W. B.P.	1+85	9.14 9.31 Fo.17		10.42 9.23 Co.1.19	

No. made, changed as per plan to get the new set of pipes.

E 1080
9.7
Co.109

Chk: 9.60 Meet
9.60

10.13 = N.W. B.P.
ABBOTT & BRINGTON

ALLEY BIK 76 - (Cont.)

STA.	LT.	RT.
6+00.30 = NWly Bacon	5.46	5.37
	6.81 5.54 1.27	6.62 5.30 1.32
	6.81 5.64 C1.17	6.62 5.64 C0.98
5+80		6.62 5.54 1.08
5+65	5.59	5.59
	6.65 5.68 C0.97	6.95 5.68 C1.27
5+50	5.64	5.64
	7.13 5.72 C1.41	7.21 5.72 C1.49
5+25	5.71	5.71
	7.38 5.80 C1.58	7.80 5.80 C2.00
5+00	5.79	5.79
	7.04 5.87 C1.17	7.25 5.87 C1.38
4+75	5.87	5.87
	6.77 5.95 C0.82	6.32 5.95 C0.37
4+50	5.95	5.95
	6.10 6.02 C0.08	6.15 6.02 C0.13
4+25	6.03	6.03
	6.46 6.10 C0.36	6.30 6.10 C0.20
4+00	6.10	6.10
	5.62 6.17 F0.55	6.53 6.17 C0.36

Clark
Shepherd
Bruner
D'Neil
3-25-55
W.O. 20638 on DWG: 2723-D
20608 on 10 sheet

E. TECOLOTE - WATER MAIN

{ Beg. PT (0+00) = EXIST B'T 764.73' }
W/Ly OF W. LINE WELLINGTON ST.

Ref: DWG: 2723-D
5566-B

68

INDEXED

(1+96.5)
1+94.5 = \angle 4' x 5' x 18" Box
(\angle LT = 2' 16" to meet
EXIST 3" stub)
(Set stub 10' wly)
361.36
358.60
C 2.76

(1+92.5)
1+92 = FUT Prop. CB Line
Set stub 7.5' wly CB AC = stub
on CB Line
361.20
361.44
361.15
361.36 = \angle CB 12' S wly
of CB AC
Set stub 12.5'
wly CB AC
F.O. 24
F.O. 21

(1+770.5)
1+68 = \angle LT 90°
(Note: Box moved 2.5' wly
to avoid driveway CB Ret.
marker CPA 4470.5
(See DWG 5566-B))
(Stub's set 5' 110' RT E)
(to \angle meter box)
361.62
357.60
C 4.02

1+26
361.81
357.82
C 3.99

(2+95.5)
2+93

(meet EXIST stub
S'wly Bldg.)

359.20 +

0+84
362.17
358.05
C 4.12

0+42
362.38
358.27
C 4.11

(2+46.25)
2+43.75

361.32
358.90
C 2.42

(13' main)
0+00 = EXIST B'T 764.73' W/Ly OF
W. LINE WELLINGTON
(Stub's set 5' RT E (N'ly))
358.50 (meet)

(2+00.5)
1+98 = Sky line Tecolote

\rightarrow B.M
362.41 = \angle S'wly
(See pg. 62)

CB END E. TECOLOTE RD.

Clark
Shepherd
Brunner
DINEL

SEWER IN P.L. 1203
(NATIONAL GUARD ARMORY)-EAST.
-TECOLOTE RD-

Ref: FB 2152-68-76
DWG: 2724-D (amended)

3-24-55

W.O. 20638 on DWG: 2724D

20608 on W.O. 5/20/55

STA.

Elevs,

STA

5+25

Elevs 345.62
338.90
C 6.72

2+45

INDEXED

295.76
289.21
C 6.55

4+90

346.43
338.76
C 7.67

2+10

293.59
287.42
C 6.17

4+55

↑
4.5

346.47
338.62
C 7.85

1+75

291.53
285.62
C 5.91

4+20 = M.H. #3

Stubs set 10' + 20' RT E.M.H.

344.51
338.48 FL.
C 6.09

1+40

289.22
283.84
C 5.38

3+90 (int. set)

(Stubs S. RT.)

1+05

286.96
282.05
C 4.91

3+80 = E CUT-OFF WALL

330.41
322.43
C 7.98

0+70

↑
5.10

283.82
280.27
C 3.55

3+60 = grad B.V.

↑
4.0

322.84
314.40 FL.
C 8.44

(0+60) = END CONC. ENCASE.

0+35

281.64
278.48
C 3.16

3+40 (also CUT-OFF WALL)

315.71
309.52
C 6.19

(0+20) Box CONC. ENCASMENT.

= M.H. #1 TYPE 'B'

0+00 = PT. 145' N.W. 1/4 EXIST. M.H. #8

286.26
276.38 FL.
C 9.88 EXIST. SEWER

286.26
276.70 = F.L. 8"
C 9.56 Sewer AT. M.H.

3+00 (also CUT-OFF WALL)

↑
2.40

303.47
299.76
C 3.71

EXIST. M.H. #8 ON EXIST. SEWER 145' N.W. 1/4 OF (STUBS SET 8.09' + 20' RT E)

B.M. (INT. Elev. Rod)

280.81 = INV. grade EXIST. M.H. #8 DWG: 1876-D

2+60 = M.H. #2

Stubs Set 10' + 20' RTE M.H.

296.75
290.00 = F.Line
C 6.75

STA	Elev's	STA	Elev's
8+40	352.83 340.16 C 12.67	11+20	351.27 341.27 C 10.00
8+05	351.27 340.02 C 11.25	10+85	351.47 341.13 C 10.34
7+70	351.50 339.88 C 11.62	10+50	351.93 340.99 C 10.94
7+35	349.86 339.74 C 10.12	10+15	353.26 340.85 C 12.41
7+00	349.91 339.60 C 10.31	9+80	353.34 340.71 C 12.63
6+65	349.82 339.46 C 10.36	9+45	353.67 340.57 C 13.10
6+30	349.30 339.32 C 9.98	9+10	354.05 340.43 C 13.62
5+95	348.33 339.18 C 9.15	8+75	353.38 340.29 C 13.09
5+60	346.91 339.04 C 7.87		353.05 340.25 F.L C 12.80

(E) 8+66.57 = LRT. 3008' 40"
8+62.23 = M.H. "A"

CHK

Set T.B.M. on 2x260' w/ly of 2x2 8+66.57
(Elev. of 2x2 at 8+73.29) F.B. 2/152

} = 355.66 = T.B.M.

STA.	Elev's
14+35	354.39 342.52 C 11.87
14+00	353.63 342.38 C 11.25
13+65	353.30 342.24 C 11.06
13+30	352.72 342.10 C 10.62
12+95	352.45 341.96 C 10.49
12+60	351.66 341.82 C 9.84
12+25	351.33 341.68 C 9.65
12+04.57 = M.H #5 (Stubs set 5' 10" RT) M.H	351.31 341.60 = F. Line C 9.71
11+90	351.61 341.55 C 10.06
11+55	351.22 341.41 C 9.81

400

STA.	Elev's
chk:	355.67 = 355.66 (See Pg 70)
10 ± Beyond Box	
16+30 = CLEAN-OUT	356.74 349.30 = F.L. C 13.44
16+10	356.87 349.22 C 13.65
15+75	356.02 343.08 C 12.94
[6" Sew = 85° 51' RT]	
15+50 = M.H #6 = 0+00 ELY 6" SEWER (Pg 72) Stubs set 5' 10" RT ON 6" Sew.	<div style="display: flex; align-items: center;"> <div style="margin-right: 10px;"> <p>(Holding 0.30' Above EL → M.H.)</p> </div> <div> <p>356.09 343.78 = F.L. 6" Sew C 12.81 ELY</p> </div> </div>
15+40	356.02 342.94 C 13.08
15+05	355.48 342.80 C 12.68
14+70	355.13 342.66 C 12.47

400

6" Sewer ELY M.H. #6 (=15+50)
Pg 71

STA.	Elev's	STA.	Elev's
2+45	356.13 347.95 C 8.18	CHK	353.34 = 353.35 = INV. 6" C.I. Sewer AT 3+51.25
2+10	356.02 349.28 C 8.74		
1+75	356.10 346.61 C 9.49	0+65.75 = Connect. with EXIST 4" C.I.	357.30 355.02 C 2.28
1+72.5 = Connect. with 4" Sewer N'ly (= 0+00 ON LAT. N'LY)	355.80 346.29 = F.L. C 9.51 4" (Stubs 5' L' RT)	0+32.87 (stubs set 5' RT)	356.47 350.65 C 5.82
1+40 (Not set)	345.94	0+00 = (1+42.5) (ON 6" ELY)	355.80 346.29 C 9.51
1+05 (stubs set 5' RT.)	356.55 345.28 C 11.27		
0+70	357.31 344.61 C 12.70	Connect. with EXIST 6" C.I. Pipe with Vert. Riser & Cleanout	
0+35	356.60 343.94 C 12.66	3+51.25 3+47.4 (as per Plan) 2724-D	354.26 350.00 F.L. C 4.26
0+00 = M.H. #6 (=15+50) (8" Sew. Pg 71)	Knocked-out F.L. M.H. #6 356.09 342.98 C 13.11	3+15	356.49 349.30 C 7.19
set grade only stub	356.06 342.98 C 13.08 M.H.	2+80	356.01 348.62 C 7.39
	356.09 343.28 = F.L. 6" Sewer ELY C 12.81		
	356.06 343.28 C 12.78 F.L. 6"		

Clark
Shepherd
Briner
O'Neil
4-26-58
W.O. 21300

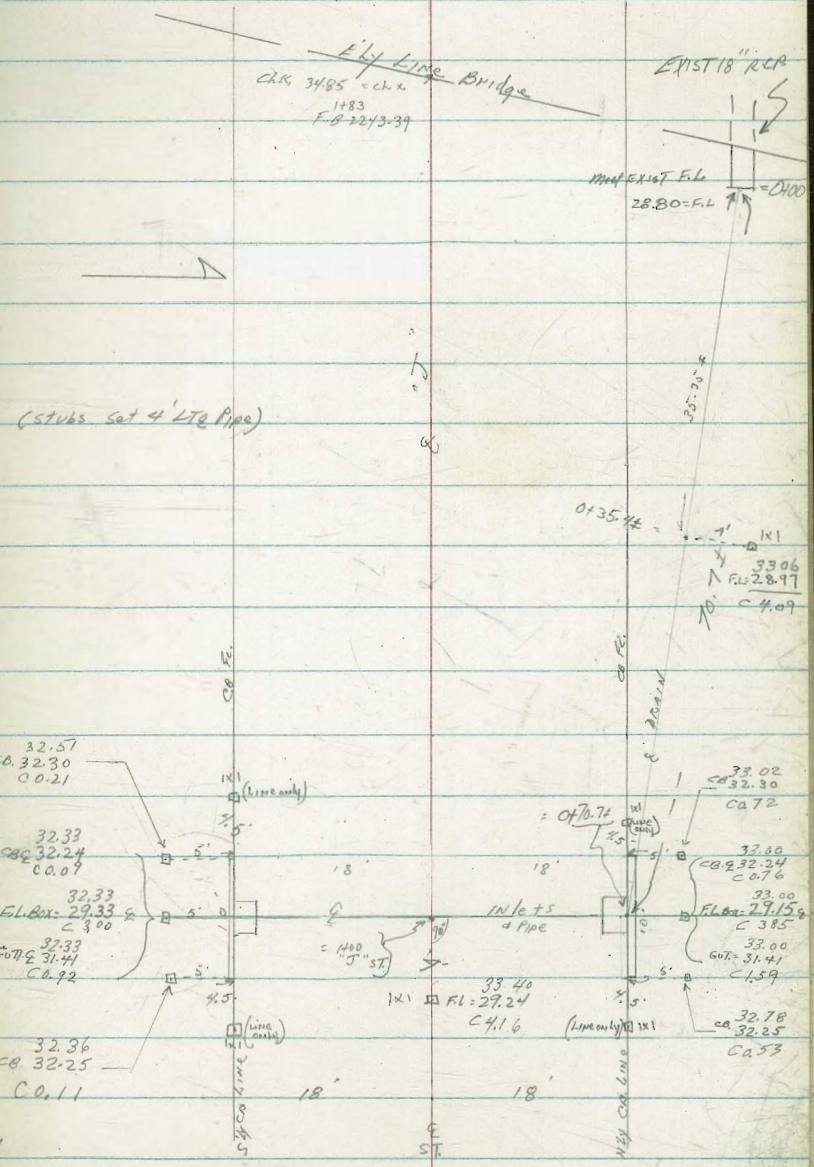
C.B.

INLETS & STORM DRAIN
33rd, ELY OF J
ST. GRADES - ROUGH GRADE
Ref: DWG: 5614-B
F.B. 2243-38

INLETS & STORM DRAIN

INDEXED

STA.	LT.	RT.
	meet bridge 35.61	35.59 meet EXIST bridge
1+30	32.97 33.03 Co.06	33.96 33.08 Co.88
1+10	32.79 32.37 Co.72	33.12 32.38 Co.74
1+00	32.24 (see opp pg)	32.24
0+90	32.65 32.26 Co.39	32.84 32.26 Co.58
0+50	33.00 32.59 Co.41	32.70 32.59 Co.11
0+10	33.12 32.92 Co.20	33.37 32.92 Co.45
0+00 = ELY Line McLAR	Meet EXIST grid	Meet EXIST grid
		32.51 = S.W. Cor. Med 34 1/4 of J



INDEXED
CLARK
S.H. [unclear]
BROWN
CWEIL
8-24-55
W.O. 2/10/7

EXTEND STORM DRAIN
VOLTAIRE & WASHINGTON
(B.K. 38 - WESTERN ADD.)

74
REF: F.B. 2210-42
F.B. 2365-17
DWS: 5738-B

STA.		Elev's.
CHK:		48.27 = 48.27 = INV. CL. END EXIST. 30" PIPE
5+46.38 = F.C.	CURTAIN WALL	43.02 39.30 C 3.72
5+14.38	(Sat. stub 5' RT 2)	44.44 41.93 C 2.51
4+82.38		45.72 44.55 C 1.17
4+50.38 = B.V.		46.85 47.17 F 0.32
4+42.38 = B.V.		47.26 47.73 F 0.47
4+34.38 = E.C.		47.88 48.12 F 0.24
4+30.54 = END EXIST. 30" CON. PIPE		48.27 CHK: 48.27 F.LINE
B.M. (Dir. Elev. P.O.D.)		96.35 = S.E.B.P. VOLTAIRE & POINSETTIA

Clark
Shepherd
Bruner
9-16-55
W.O. 62435

SEWER: GUY ST:
EXIST. M.H. #1 - DWG: 4476-L
& Crowell & Guy to PT. INT. BY
LINE GUY + PT. 10' S of NLY Line
LOT 8 - MIDDLETOWN ADD:

REF: F.B. # 1361
DWG: 5751-B
T.P.S. # 430

75

STA.

Elev's:

INDEXED

1+42
193.49
188.00 - Plug
C 5.47

1+25
195.97
187.87
C 8.10

1+00
198.78
187.70
C 11.08

0+75
201.06
187.52
C 13.54

0+50
200.91
187.35
C 13.56

(Stubs set 5' out)

0+25
196.18
187.17
C 9.01

0+00 = EXIST. M.H. #1 meet - 187.00 = I.E. (As per DWG: 4478-L)

Set T.B. Men S. W. Y. B. P. Crowell = 193.49 = B.M. for Sewer Line

B.M. Div. E. P. R. Add: (No recorded elev in our T.D. Book) 97.11 = S.E. B.P. Co. Lumbria & Clark Meters

Note: { F. Line M.H. #1 = 187.34 USING B.M.
As noted. Since F. Line grade Proposed
Sewer is established at .76; elev OFF
F. Line M.H. used AS B.M. AT 187.00
(RELATIVE)

Clark
Garber
Bruyer
Pullen

GRADES: GUY ST. - CROWELL (N'WLY)

(LINE) to 175' N'WLY

(NO CAS)

9-29-55

N.O. 62435

REF: DWG 15751-B
T.P.S 480

76

STA	LT.	RT (N'WLY)	STA.	LT.	RT (N'WLY)
1+10	185.40 187.99 F 2.57	193.23 188.47 C 4.76			
0+90	188.25 190.48 F 2.23	196.86 190.98 C 5.88			
0+70	190.73 192.54 F 1.81	200.04 193.04 C 7.00			
0+50	192.53 194.14 F 1.61	202.57 194.64 C 7.93			
0+30	194.62 195.28 F 0.66	204.82 195.78 C 9.04			grade stakes set 1' Bk Prop. line - Guy
0+20 <u>L. Only</u>	195.36 195.74 F 0.38				
0+10	195.38 195.90 F 0.52	204.83 196.71 C 8.12			
0+00 = N'Wly Line CROWELL	(meet EXIST PRT) 195.71	197.32	1+75 = End grading	173.00 177.80 F 4.80	182.14 178.30 C 3.84
B.M. Dir. Elev. Rod:	97.11 = S.E.B.P.	Chalmers & Columbia	1+30	182.19 185.00 F 2.81	190.58 185.50 C 5.08

Hatch
Pope
Garber
Pullen

Stake Curbs
9th & Ast.

10-7-55
W.O. 20008

77

INDEXED

Grade

P.R.'s set 5' out inst

S.E. P.C. on 9th 82.97 82.57 F040

$\frac{2}{3}$ 83.35 82.84 F051

$\frac{1}{3}$ 83.40 83.10 F030

S.E. P.C. on Ast. 83.06 - Meet.

B.M. = N.W. 7' LYT. 9th & Ast. 89.14

Hatch
Pope
Garber
Pullen

INDEX

P.K. 5

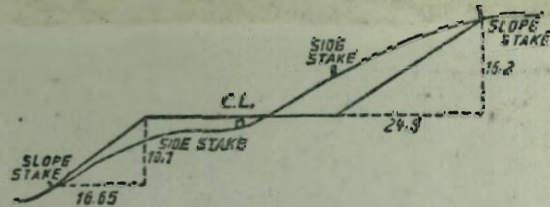
S.E. P.

2/3

1/3

S.E. 1

B.M.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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