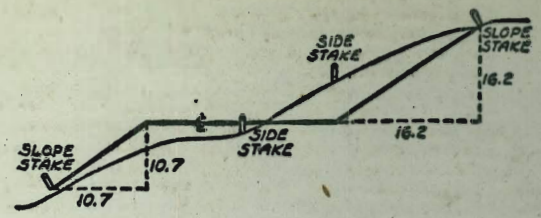


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

INDEX (Cont.)

INDEX (Cont.)

Clark
Shephard
Bruner
O'Neil

SUNNY SLOPE SEWER [ELENCANTO]
MADERA - HILGER - TARBOX - GIBSON - KLAUBER ETC.

MADERA (E HILGER Ely to D.END)

STA	Elev's
	284.63
2+45	276.30
	C 8.33
	283.51
2+10	275.53
	C 7.98
	282.50
1+75	274.76
	C 7.74
	281.45
1+40	273.99
	C 7.46
	280.36
1+05	Cl.'s set 6' Lt & 273.22
	C 7.14
0+70 ± = (END EXIST. 8" Sewer)	Beg NEW LINE 272.45
0+35	
	F.B. 2274/-3
	Clr: 278.10 = 278.10 = Rim EXIST MH
0+00 = EXIST M.H #8 (DWG #1767-D) E HILGER & MADERA	271.40
B.M. Dir. Elev. P.O:	294.80 = CON MON & Y E TARBOX

STA	Elev's
	289.26
5+65	281.38
	C 7.88
	289.15
5+30	280.89
	C 8.26
	289.05
4+95	280.40
	C 8.65
	288.90
4+60	279.91
	C 8.99
	288.73
4+25	279.42
	C 9.31
	288.35
3+90	278.93
	C 9.42
	287.81
3+55	278.44
	C 9.37
	286.93
3+20 = M.H #8 (6'+14' Lt &)	277.95
	C 8.98
	285.71
2+80	277.07
	C 8.64
HILGER	

MADERA (Cont.)

STA.	Elev's
8+85	297.13 290.02 C 7.11
8+50	295.93 288.94 C 6.99
8+15	294.75 287.85 C 6.90
7+80	293.52 286.77 C 6.75
7+45	292.33 285.68 C 6.65
7+10	291.21 284.60 C 6.61
6+75	290.26 283.51 C 6.75
6+40 = M.H #9 (cl-l- 6'4"14' Lt ℄)	289.70 282.43 C 7.27
6+00	289.41 281.87 C 7.54

11+00 = △ END	304.42 296.55 = F. line C 7.87
10+65	303.26 295.50 C 7.76
10+30	302.00 294.45 C 7.55
9+95	300.85 293.40 C 7.45
9+60 = M.H #10 (cl-l- 6'4"14' Lt ℄)	299.73 292.35 C 7.38
9+20	298.33 291.11 C 7.22

HILGER: (E MADERA N'ly to KLAUBER "M-17"

STA.	Elev's	
2+80		291.73 283.44 C 8.29
2+45		290.61 281.93 C 8.68
2+10		288.75 280.43 C 8.32
1+75		287.14 278.92 C 8.22
1+40	4.30 ↑	285.22 277.42 C 7.80
1+05		283.98 275.91 8.07
0+70		282.22 274.41 7.81
0+35	Stubs set 6' ↕ ℄	279.84 272.90 C 6.94
0+00 = EXIST M.H # 8 (DWG # 17675) E MADERA ℄ HILGER		271.40 = F. Line
B.M.	Dir. Elev. Rod:	294.80 = CON MON ℄ ℄ TAR BOX

STA.	Elev's	
5+75		306.68 296.95 C 9.73
5+40		304.90 295.31 C 9.59
5+05	4.20 ↑	303.11 293.66 C 9.45
4+70		301.16 292.02 C 9.14
4+35		299.32 290.37 C 8.95
4+00	E. HILGER - TAR BOX	297.74 288.73 C 8.41
CHK: 297.80 = 294.80 = CON MON		
3+68.8 = M.H # [[= 0+00 TAR BOX] see Pg 8] ETAR BOX		295.01 287.26 C 7.75
3+50		294.45 286.45 C 8.00
3+15		292.94 284.94 C 8.00
HILGER		

HILGER (CONT.)

STA.	Elev's
(8+49 = Chimney)	
8+45	320.86 309.11 C 11.75
8+10	319.20 307.64 C 11.56
7+75	317.22 306.17 C 11.05
CLK: 315.31 = 315.32 = CON. MON & HILGER & GIBSON	
7+39 = W.H #2 [=0+00 & GIBSON) See Pg. 11 Stubs set 10' & 15' LT &	314.84 304.66 C 10.18
7+15	314.28 303.53 C 10.75
6+80	312.56 301.89 C 10.67
6+45	311.25 300.24 C 11.01
6+10	309.11 298.60 C 10.51

STA.	Elev's
10+70	332.27 318.44 C 13.83
(10+49 = Chimney)	
10+35	330.86 317.04 C 13.82
10+09 = W.H #3 stubs 10' & 20' LT &	329.12 316.00 C 13.12
9+85	328.45 314.99 C 13.46
9+50	326.76 313.52 C 13.24
(9+49 = chimney)	
9+15	324.36 312.05 C 12.31
8+80	322.79 310.58 C 12.21

HILGERT (cont.)

STA.		Elev's
Set T.B.M. = Pk. nail P 76685 = 339.57		
21.74 Lt. E		
Δ = 28° 15' 22" RT.		
12+75.2 = M.H. Stake 10' via Lt. &		338.25
		326.65
		C 11.60
(12+65 Chimney)		
12+45		338.52
		325.44
		C 13.08
12+10		337.42
		324.04
		C 13.38
11+75		336.68
		322.64
		C 14.04
(11+60 Chimney)		~~322.67~~
11+40		335.17
		321.24
		C 13.93
11+05		333.93
		319.84
		C 14.09

STA.		Elev's
(15+65 = ℄ Chimney)		
15+55	(8' RT.)	361.84
		340.36
		C 21.48
15+20	(8' RT.)	359.36
		338.65
		C 20.71
14+85	(8' RT.)	356.59
		336.93
		C 19.66
(14+65 = ℄ Chimney)		
14+50	(8' RT.)	353.66
		335.22
		C 18.44
14+15	(10' RT.)	350.73
		333.50
		C 17.23
(13+90 = ℄ Chimney)		
13+80	(8' RT.)	346.44
		331.79
		C 14.65
13+45	(8' RT.)	343.72
		330.07
		C 13.65
13+10	(8' RT.)	342.60
(34.8)		328.36
		C 14.24

HILGER (CONT.)

STA.		Elev's
18+10		372.59 357.06 C 15.53
17+75		371.81 354.64 C 17.17
(17+65 = ℄ Chimney)		
17+40		370.73 352.23 C 18.50
17+05		368.76 349.81 C 18.95
16+70	↑ 26'	366.53 347.40 C 19.13
(16+65 = ℄ Chimney)		
16+35		364.96 344.98 C 19.98
(348')	(5 stubs 6'4")	
16+00.20 = M.H #5	(5 stubs 6'5o 2"℄)	362.94 342.57 C 20.37
15+90	(stub 8' ea)	364.19 342.08 C 22.11

STA.		Elev's
20+65		386.07 375.92 C 10.15
20+30		382.23 373.19 C 9.04
19+95	↑ 18'	378.77 370.46 C 8.31
19+60		377.08 367.73 C 9.35
(348')		
19+25.20 = ℄ M.H #6		375.15 365.00 C 10.15
19+15		375.17 367.30 C 10.87
18+80		374.48 361.89 C 12.59
(18+65 = ℄ Chimney)		
18+45		373.31 359.47 C 13.84

HILGER (Con't)

~~85°~~ 75° & E KLAUBER

Set T.B.M. on Sly 12' chx = 400.30
(Tie-Pt.)
(for & L+T.)

Chx: 400.41 = 400.34 = L+T & KLAUBER & HILGER

Stubs set (chx.) 6.94 418' LT on SPI. T.L.

22+51.90 = M.H. #7 E KLAUBER
(= 0+00 KLAUBER Sly HILGER & Nly HILGER See Pg. 23)

400.43
390.48
C 9.95

22+40

400.15
389.56
C 10.59

22+05

398.61
386.83
C 11.78

21+70

395.91
384.11
C 11.80

21+35

392.88
381.38
C 11.50

21+00

390.03
378.65
C 11.38

TARBOX: M.H.# 1 (EHILGER) to D.END

STA.	Elev's
2+80	308.86 298.34 C 10.52
2+45	308.29 296.95 C 11.34
2+10	307.60 295.56 C 12.04
1+75	306.70 294.18 C 12.52
1+40	305.41 292.80 C 12.61
1+05	303.93 291.41 C 12.52
0+70	301.60 290.03 C 11.57
0+35	298.65 288.64 C 10.01
0+00 = M.H.# 1 - E HILGER (= 3+68.8 HILGER see pg 3)	287.26 E. LINE
B.M. DIR. ELEV. ROD	294.80 = CON. MON. E HILGER & TARBOX

3.96 ROD

STA.	Elev's
5+60	311.14 304.48 C 6.66
5+25	310.96 303.96 C 7.00
4+90	310.63 303.43 C 7.20
4+55	310.40 302.91 C 7.49
4+20	310.18 302.38 C 7.80
3+85	309.97 301.86 C 8.11
(26.24) 3+58.76 = M.H.# 11	310.24 301.47 F.L. C 8.77
3+50	310.10 301.13 C 8.97
3+15	309.46 299.74 C 9.72

1.50 ROD

3.96 ROD

TARBOX (CONT.)

STA.	Elev's
8+40	315.71 308.69 C 7.02
8+05	315.65 308.17 C 7.48
7+70	315.39 307.64 C 7.75
7+35	314.85 307.12 C 7.73
chk; T.B.M. {SPIKE Ble# 76623 8+60.21 RTE. - FB# 2274 -30} 317.07 = 317.10	
7+17.76 = M.H. # 13 = (0+00 EASEMENT Sewer Blk #6 See Pg. 14)	314.99 306.86 F.L. C 8.13
7+00	313.94 306.59 C 7.35
6+65	313.18 306.07 C 7.11
6+30	312.34 305.53 C 6.81
5+95	311.56 305.01 C 6.55

STA	Elev's
11+20	320.19 312.89 C 7.30
10+85	319.28 312.36 C 6.92
10+50	318.68 311.84 C 6.84
10+19.76 = M.H. # 14	318.95 311.38 F.L. C 7.57
9+80	316.83 310.79 C 6.04
9+45	316.32 310.27 C 6.05
9+10	315.89 309.74 C 6.15
8+75	315.70 309.22 C 6.48

TARBOX (Cont)

STA		Elev's
14+00	↑ 1.5%	325.90 317.09 C 8.81
13+65		325.87 316.56 C 9.31
13+30		325.29 316.04 C 9.25
13+19.76 = M.H #5		326.19 315.88 F.L C 10.31
12+95		324.57 315.51 C 9.06
12+60	↑ 1.5%	323.27 314.99 C 8.28
12+25		322.05 314.46 C 7.59
11+90		321.36 313.94 C 7.42
11+55		320.95 313.41 C 7.54

STA	Elev's
CHK:	329.15 = 329.12 = CON MEN SHIGERT ELEV. 694
14+59.76 = D.END	326.25 317.98 F.L C 8.27
14+35 ↑ 1.5%	325.85 317.61 C 8.24

GIBSON ST
M.H #2 (E HILGER) through MH #16 - #17
+ D.END E. GIBSON

STA.	Elev's	
2+80	352.50 337.42 C 15.08	
2+45	347.99 333.32 C 14.67	
2+10	343.12 329.23 C 13.89	
1+75	338.65 325.13 C 13.52	
1+40	334.09 321.04 C 13.05	
1+05	329.39 316.94 C 12.45	
0+70	324.87 312.85 C 12.02	
0+35	320.50 308.75 C 11.75	
0+00 = M.H #2 = E HILGER 1439 (see Pg 4)	304.66 = ELEV	
B.M.	DIST. ELEV. REM.	315.32 = CON NAIL E HILGER & GIBSON

11.76

(Hubs 6' Lt E)

STA.	Elev's
5+80	352.59 340.88 C 11.71
5+45	353.61 340.74 C 12.87
5+10	354.42 340.60 C 13.82
4+75	354.87 340.46 C 14.41
4+40	356.10 340.32 C 15.78
4+05	357.52 340.18 C 17.34
3+70	357.48 340.04 C 17.44
3+35	354.55 339.90 C 14.65
3+00 = M.H #16	354.27 339.76 = ELEV C 14.51

#16

GIBSON ST. (Cont'd)

Chs:		
	348.97	= 348.93 = Con. Mon & Gibson 4 Plover
		360.37
8+97.47 = D. END		353.67 = F. Line
		C 6.70
		359.10
8+80		351.97
		C 7.18
	↑ 10.6	355.55
8+45		348.42
		C 7.13
		352.61
8+10		344.92
(32.53)		C 7.69
		350.91
7+77.47 = M.H #42	(Stubs 10' 120° LT E M.H)	341.67 = F. Line
		C 9.24
		349.04
7+55		341.58
		C 7.46
		347.64
7+20		341.44
		C 6.20
	↑ 0.46	347.43
6+85		341.30
		C 6.13
		347.92
6+50		341.16
(32.53)		C 6.76
	(Stubs 10' 120° LT E M.H)	351.91
6+17.47 = M.H #17 & Plover		341.03 = F. Line
(=0+00 Plover see Pg. 17)		C 10.88

GIBSON ST. & (M.H #24 EASEMENT (186.60' ely & Zeller)) W'ly to D. END

Sta.		Elev's
		362.22
2+55		352.79
	↑ 9.0	C 9.43
		359.06
2+20		350.34
(33.40)		C 8.72
		354.60
1+86.60 = M.H #23 & Zeller	(Stubs M.H Set 10' 120° LT E)	348.00 see Pg. 20
(=0+00 N'ly Zeller Pg. 20)		6.60
		355.48
1+75		347.21
		C 8.27
		351.57
1+40		344.79
		C 6.78
		347.96
1+05		342.37
		C 5.59
	↑ 6.9	345.81
0+70		339.95
		C 5.86
		344.18
0+35		337.53
		C 6.65
M.H #24	(Stubs Set 6' RT E)	345.20
0+00 = E. EASEMENT	(Stubs M.H Set 10' 25° LT E)	335.11 E. Line
(EASEMENT - Pg 16)		C 10.09

B.M. Dirt Elev Rod: 355.37 = Con. Mon & Zeller & Gibson

GIBSON-EEASEMENT (Cont.) W'ly to D.END

B.K.:	355.40	355.37 = Con MON EZeller & GIBSON
5+11.60 = D.END		371.44 365.25 C 6.19
	↑ 1.5%	
4+80		371.99 364.98 C 7.21
4+45		371.82 364.25 C 7.57
(33.40)		
4+11.60 = M.H #22		370.95 363.75 C 7.20
3+95		370.30 362.59 C 7.71
	↑ 0%	
3+60		368.61 360.14 C 8.47
	↑ 1.0%	
3+25		366.85 357.69 C 9.16
2+90		364.96 355.24 C 9.72

GIBSON-EEASEMENT - M.H #24 - E'ly to D.END

B.K.:	355.39	355.37 (See B.M.)
1+65 = D.END		358.02 350.58 F.Line C 7.44
1+40		354.60 348.23 C 6.37
1+05		350.46 344.95 C 5.51
	↑ 2.38%	
0+70		347.02 341.67 C 5.35
0+35		345.05 338.39 C 6.66
0+00 = M.H #24 EEASEMENT = (EASEMENT-Pg 16)		345.20 335.11 C 10.09
B.M. DIV. Elev. Rod:		355.37 = E Con MON Zeller & GIBSON

EASEMENT: M.H #13 - TARBOX to M.H #24
GIBSON - BLK 6 -

STA		Elev's:
2+20	1.5% ↑	328 39 322.53 C 5.86
(24.87)		
1+85.13 = L & R ∠ (∑ to EASEMENT)	70° = M.H # 38 (stubs set 11.31 & 20' ∥ ∑ ON SPLIT ∠)	327 59 322.00 - FL 5.59
1+75		321.18
1+40		323 81 318.31 C 4.70
1+05	2.81% ↑	320 97 315.44 C 5.53
0+70		318 74 312.58 C 6.16
0+35	(stubs set 8'LT & EASEMENT)	317.24 309.72 C 7.52
0+00 - M.H #13 ∑ TARBOX (See Pg 9)		317. 99 306. 86 = F. Line C 8.13
B.M. DIV. ELEV. ROD: (See Also Pg 9)		317.10 = SPIKE IN Pole # 76623 FB. 2274-30

STA		Elev's
		336.58 326.98 C 9.60
5+25	1.18% ↑	
(30.62)		
4+94.38 = M.H #39		335 23 326.67 FL C 8.59
4+65		333.85 326.20 C 7.65
4+30		332 37 325.67 C 6.70
3+95		331.10 325.15 C 5.95
3+60		330 00 324.62 C 5.38
3+25	1.5% ↑	329.85 324.10 C 5.75
2+90		329.57 323.59 C 5.98
2+55		329 07 323.06 C 6.01

EASEMENT BK -6- (CONT.)

STA.		Elev's
8+25		339.11 330.06 C 9.05
(326.2')	0+43	
7+94.38 = M.H #10	(Stubs set 8+20 Lt & Rt)	339.36 329.94 F.L. C 9.42
7+70		339.27 329.67 C 9.60
7+35		339.49 329.29 C 10.20
7+00	1+16	339.63 328.90 C 10.73
6+65		339.30 328.52 C 10.78
6+30		339.16 328.13 C 11.03
5+95		338.13 327.75 C 10.38
5+60		337.89 327.36 C 10.53

STA.		Elev's
(326.2')		
11+42.38 = M.H #11 = L.T. 90°	(Stubs set 11+18 20' Lt & on Spin ∠)	337.97 331.93 6.64
11+05		337.20 331.18 C 6.02
10+70		336.28 331.04 C 5.24
10+35		335.55 330.90 C 4.65
10+00	0+43	334.99 330.76 C 4.23
9+65		335.53 330.62 C 4.91
9+30		336.60 330.48 C 6.12
8+95		338.33 330.34 C 7.99
8+60		339.04 330.20 C 8.84

EASEMENT - BK. 6 - (CONT.)

STA.		Elevs
Ch'k'd.	329.12 =	329.12 = E Cor prop. / Tar Box ✓ Nl. 69+L
13+17.43 = M.H. # 24 E GIBSON (See Bks 12+13)		335.11 = F.L.
13+15 (not set)	2.16 BD	
12+80		342.93 334.29 C 8.64
12+45		341.24 333.54 C 7.70
12+10		339.66 332.78 C 6.88
11+75		338.92 332.03 C 6.89

PLOVER:
MH #17-E GIBSON N'LY to D.END

STA.		Elevs
		390.15
2+55	↑	380.86
	19.98	C 9.29
		384.39
2+20		373.89
		C 10.50
		378.75
1+85 = M.H #18	(stubs set 6' 4/5' LT E)	366.93
		C 11.82
		377.34
1+75		365.53
		C 11.81
		371.71
1+40		360.63
		C 11.08
	↑	366.69
1+05	14.86	355.73
		C 10.94
		360.65
0+70		350.83
		C 9.82
		355.05
0+35		345.93
		C 9.12
		351.91
0+00 = M.H #17		341.03 F line
(= 6+17.47 GIBSON See Pg 12)		C 10.88
B.M. Dit Elev Rod:		355.37 FE Common Zellen & GIBSON

STA.		Elev's
(5+59.26 = chimney)		
		436.50
5+55		420.78
		C 15.72
	↑	
	1.28	434.05
5+20		420.36
		C 13.69
		430.85
4+85		419.94
		C 10.91
(05 PM)	CLK & 427.34 = 427.37 = E Com. Mon △	
4+49.26 = M.H #19		426.97
△ = 18°54' Rt.	(stubs set 6.08' LT & 5' LT E)	419.52
		C 7.45
		424.22
4+30		415.68
		C 8.54
		418.44
3+95		408.72
	↑	C 9.72
	19.96	411.58
3+60		401.75
		C 9.83
		403.82
3+25		394.79
		C 9.03
		396.87
2+90		387.82
		C 9.05

PLOVER (Cont.)

STA.		Elev's
8+50	2.1%	431.58 425.46 C 6.19
8+15		431.95 424.44 C 7.51
(35.7')		
7+79.26 = M.H #20	(Stubs 6+15 LT ℄)	432.90 423.48 F.L. C 9.42
7+65		433.45 423.30 C 10.15
7+30		435.31 422.88 C 12.43
6+95	1.2%	437.29 422.46 C 14.83
(6+69.26 chimney)		
6+60		438.81 422.04 C 16.77
6+25		439.29 421.62 C 17.67
5+90		438.34 421.20 C 17.14

STA.		Elev's
11+55	0.4%	444.61 432.80 C 11.81
(85.7')		
11+19.26 = M.H #21	(Stubs set 6+15 LT ℄)	444.53 432.66 F.L. C 11.87
10+95		443.98 432.01 C 11.97
10+60		442.45 431.06 C 11.39
10+25		440.43 430.12 C 10.31
9+90	2.1%	437.87 429.17 C 8.70
9+55		435.28 428.23 C 7.05
9+20		433.15 427.28 C 5.87
8+85		431.97 426.34 C 5.63

PLOVER (Cont'd.)

STA.		Elev's	
Ck:		437.56 = 437.45	Lft. & Klauber & E. Plover
12+79.26 = J. END		441.63 433.30 F.L. C 8.33	
12+60		442.32 433.22 C 9.10	
12+25	1 0.40	443.45 433.68 C 1037	
11+90		444.15 432.94 C 11.21	

ZELLER : MH #23 E GIBSON KLAUBER to MH #34 E

(2+40 = chimney)

2+10 — 368.26 / 351.78 / C 16.48

1+75 — 367.07 / 351.15 / C 15.92

1+40 — 365.21 / 350.52 / C 14.69

(1+20 = chimney) ~~350.52~~

1.88

1+05 — 363.20 / 349.89 / C 13.31

0+70 — 360.65 / 349.26 / C 11.39

0+35 (stubs 6" ITE) — 358.04 / 348.63 / C 9.41

0+00 = M.H #23 E GIBSON — 354.60 / 348.00 = F.L. / C 6.60 (See Pg 12)

(= 486.60 on GIBSON-W'LY OF EASEMENT BK 6)

See Pg 12

B.M. — 355.37 = E CON MON. @ ZELLER

GIBSON

5+30 — 370.79 / 359.49 / C 11.30

2.74

4+95 — 370.74 / 358.53 / C 12.21

4+60 — 370.45 / 357.57 / C 12.88

(4+42.5 = chimney)

4+25 — 370.34 / 356.61 / C 13.73

3+90 — 370.18 / 355.65 / 14.53

3+55 — 369.40 / 354.69 / C 14.71

(32.49')

3+22.51 = M.H #12 — 368.77 / 353.80 = F.L. / C 14.97

3+15 — 368.73 / 353.67 / C 15.06

2+80 — 368.37 / 353.04 / C 15.33

2+45 — 368.53 / 352.41 / C 16.12

ZELLER (CONT.)

(8+42.5 = Chimney)		
		394.60
8+15		382.18
		C 12.42
		388.92
7+80		377.80
		C 11.12
	12.5' ↑	383.61
7+45		373.43
		C 10.18
		379.67
7+10		369.05
		C 10.62
		376.31
6+75		364.68
		C 11.63
		375.24
6+62.51 = M.H. #44		363.12
		C 12.12
		373.68
6+35		362.37
		C 11.31
	27.5' ↑	372.23
6+00		361.41
		C 10.82
		371.43
5+65		360.45
		C 10.98

	8.5' ↑ (Stubs set 8' LT & here on)	428.55
10+70		411.60
		C 16.95
(10+42.5 = Chimney)		
		423.10
10+35		408.49
		C 14.61
		419.26
10+02.51 = M.H. #43		405.60
		C 13.66
		417.89
9+90		404.05
		C 13.84
		414.12
9+55		399.68
		C 14.44
(9+42.5 = Chimney)	12.5' ↑	
		408.86
9+20		395.30
		C 13.56
		404.10
8+85		390.93
		C 13.17
		399.54
8+50		386.55
		C 12.99

ZELLER (CONT.)

chx. 437.17 = 437.17 = ℄ H T
KLAUBER & Zeller

12+22.51 = M.H 34 (Set chx's 7.04 VIS (Stub) 437.06
(0+00 KLAUBER SWly & NEly) 4 E 425.18 E line
(Sta 1+27) OF ZELLER C 11.88

12+10 (Set chx 6 LT ℄) 436.61
424.06
C 12.55

11+75 437.04
420.95
C 16.09

(11+42.5 = Chimney)

11+40 435.68
417.83
C 17.85

11+05 432.56
414.72
C 17.84

KLAUBER: ℄ HILGER S'WLY to pt 160' S'LY ℄ SEIDER

(31.20')

2+48.80 = M.H # 28 (clx's 6'+9' LT ℄)

2+45 (Not set)

2+10

1+75

1+40

1+05

0+70

0+35 (clx's set 6' LT ℄)

= M.H # 7

0+00 = ℄ HILGER x KLAUBER
(= 22+51.90 HILGER)
See Pg 7

BM.

402.09
393.71
C 8.38

393.66

401.62
393.21
C 8.41

401.20
392.75
C 8.45

400.84
392.30
C 8.54

400.47
391.84
C 8.63

399.94
391.39
C 8.55

399.82
390.93
C 8.89

390.48 = F.Line
See Pg 7

400.34 = L.T. ℄
HILGER & KLAUBER

1.30

5+75 (Not Set)

5+40

5+05

4+70

4+35

4+00

(33.3')

3+66.70 = M.H # 27 (clx's 6.47' + 10' LT ℄ ℄ on SPLIT ℄)

3+50

3+15

2+80

4.75

1.30

412.08
403.38
C 8.70

410.30
401.73
C 8.57

408.55
400.09
C 8.46

406.88
398.44
C 8.44

405.31
396.80
C 8.51

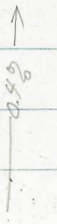
403.34
395.24
C 8.10

403.97
395.00
C 8.97

403.12
394.55
C 8.57

402.51
394.10
C 8.41

KLAUBER (S'WLY OF KILGER - Cont'd)



8+15 (26.5 Rt)

425.90
415.17
C 10.73

7+88.49 = M.H #25 (Ch's 6' Lt of Ø Line)

424.69
415.06
C 9.63

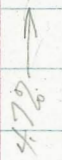
7+85 (not set)

d.k.

424.75 = 424.79 = HT of Elect @ KLAUBER

7+50

422.73
413.25
C 9.48



7+15

420.96
411.61
* C 9.35

9+48.49 = D.END @ KLAUBER

429.34
415.70
C 13.64

6+80

419.19
409.96
C 9.23

9+20

429.00
415.59
C 13.41

6+45

417.40
408.32
C 9.08

8+85

428.24
415.45
C 12.79

6+10 (8.30)

415.56
406.67
C 8.89

8+50

427.19
415.31
C 11.88

5+76.70 = M.H #26 (Ch's 6+9 Rt of Ø)

413.92
405.11
C 8.81

KLAUBER: E HILGER (M.H #7) N 61° W to D.END.
(330' ±W OF E Plotter)

0+00 = E HILGER + KLAUBER (See Pgs 7+23) = M.H #7		390.48
		See Pg. 7 22+51.90 HILGER
0+35		400.76 391.32 C 9.44
0+70		401.29 392.16 C 9.13
1+05		402.23 393.00 C 9.23
1+40		403.78 393.84 C 9.94
1+70 = M.H #29	(chi's 6'x9'LT E)	405.63 394.56 C 11.07
2+05		408.26 397.81 C 10.45
2+40		411.49 401.07 C 10.42
2+75		414.68 404.32 C 10.36
B.M.	Dir. Elev. Rod:	400.34 = L+T E HILGER + KLAUBER

3+10 = M.H #30	(chi's 6'x9'LT E)	418.00 407.58 C 10.42
3+45		421.15 409.26 C 11.89
3+80		424.08 410.94 C 13.14
4+15		426.67 412.62 C 14.05
4+50 (4+35 = CHIMNEY)		428.72 414.30 C 14.42
4+85		430.60 415.98 C 14.62
5+20		432.27 417.66 C 14.61
5+53 = CHIMNEY)		433.56 419.34 C 14.22
5+90		434.93 421.02 C 13.91

KLAUBER: EHLLER N'LY (M.H #7) (Cont.)

8+60		445.29 436.45 C8.84
8+25		444.38 434.35 C10.03
7+90		443.30 432.25 C11.05
7+55		441.87 430.15 C11.72
7+20		440.42 428.05 C12.37
(6+93.74=Chimney)		
6+85		438.80 425.95 C12.85
(31.26')		
6+53.74 = M.H #31 (dw's 6+9 LT&)		437.41 424.08 C13.33
6+25		436.28 422.70 C13.58

CLK: 437.99 = 437.45 = Lt. ℄ Paver & KLAUBER

9+83.74 = D. END		447.76 441.45 F.L C6.31
9+53.74		447.14 440.46 C6.68
9+23.74		446.57 439.47 C7.10
8+93.74 = M.H #32 (dw's 6+9 LT&)		445.99 438.48 F.L C7.51

(M.H #34)

KLAUBER & ZELLER S'WLY to.

D.END

2+70 = M.H # 33	(CLX & SIGHTING)	446.89 437.89 = FS LINE C 9.00
2+45		443.94 436.69 C 9.25
2+10		444.34 435.05 C 9.29
1+75		442.57 433.40 C 9.17
1+40		440.86 431.76 C 9.10
1+05		439.13 430.11 C 9.02
0+70		437.35 428.47 C 8.88
0+35		436.36 426.82 C 9.54
		437.06 425.18 C 11.88 See Pg. 22 12+22.51 ZELLER
& KLAUBER & ZELLER = 0+00 = M.H # 34 = M.H # 34 (See Pg 22. (=12+22.51 ZELLER)		
B.M.		437.17 = Lt. C & ZELLER & KLAUBER

CHK:

437.17 = 437.17 = Lt. C. & ZELLER & KLAUBER

3+70 = D.END	448.63 442.00 = FS C 6.63
3+40	448.55 440.77 C 7.78
3+05	447.96 439.33 C 8.62

(M.H #34)

KLAUBER: E ZELLER N'ELY

to 69+7h

(2+88.15 = E chimney)			
2+70	0.4 ↑	455.36 442.69 C 12.67	
(31.85')			
2+38.15 = M.H # 35		453.68 442.56 = FL C 11.12	
2+10		452.10 440.51 C 11.59	
1+75		449.83 437.95 C 11.88	
1+40		447.15 435.40 C 11.75	
1+05		444.42 432.84 C 11.58	
	1.3 ↑		
0+70		441.67 430.29 C 11.38	
0+35		439.03 427.73 C 11.30	
= M.H # 34			
0+00 = E KLAUBER & Zeller		437.06 425.18 C 11.88	
= (12+22.51 ZELLER See Pg 22		See Pg 22	
B.M.		437.17 = L+Tc E ZELLER & KLAUBER	

6+15			457.85 447.10 C 10.75
			460.12
5+80			446.19 C 13.93
(5+58.5 = END CONC. CRADLE)	2.0 ↑		
5+45			461.69 445.28 C 16.41
5+10			462.59 444.37 C 18.22
(31.85')			
4+78.15 = M.H # 36	(CLR'S 1ST 8.48 RTV 8.48 LT & ON SPLIT ∠)		462.76 443.54 = FL C 19.22
= (0+00 PERKINS DRIVE) See Pg 29.			
4+45			462.41 443.40 C 19.01
4+10	0.4 ↑		461.57 443.26 C 18.31
3+75			460.28 443.12 C 17.16
(3+43.15 = E chimney)			
3+40			458.73 442.97 C 15.76
(3+18.15 Bag Conc. Cradle)			
3+05			457.06 442.83 C 14.23

KLAUBER (Concl.)

Set T.B.M

Chk: 462.83 =

6+88.15 = D.END

6+50

46373 = P.K.NAIL 30' S'Ly OF ℄ KLAUBER AT POT L+Tk. 7807' W'Ly OF ℄ KLAUBER & PIERINO

462.79 = L+Tc. ℄ KLAUBER & PIERINO

455.46
449.00 ±FL
C 6.46

455.63
448.01
C 7.62

PIERINO DRIVE

℄ KLAUBER, M.H.T 36, N'Ly to D.END

STA	Elev's
2+50 = ℄ M.H.T 37	454.85 444.54 C 10.31
2+45	455.23 444.52 C 10.71
2+10	456.94 444.38 C 12.56
(1+80 = END Con. cradle)	
1+75 (Also ℄ Chimney)	458.50 444.24 C 14.26
1+40	460.03 444.10 C 15.93
(1+25 = ℄ chimney)	
1+05	461.70 443.96 C 17.74
0+70	461.98 443.82 C 18.16
0+35	462.42 443.68 C 18.74
= M.H.T 36. (Bay Con. cradle)	
0+00 = ℄ PIERINO DR. & KLAUBER	443.54
= (4478.15 KLAUBER) See Pg 28	See Pg 28
B.M.	462.79: L+Tc. ℄ KLAUBER & PIERINO

0+48

PIERINO DR. (CONT.)

dik:

462.78 = 462.79 (See B.M.)

3+65 = D.END

450.75
445.00 = F.L.
C 5.75

3+50

451.15
444.94
C 6.21

D. 4%

3+15

452.22
444.80
C 7.42

2+80

453.57
444.66
C 8.91

clark
Shephard
Bruner
O'Neil

10-11-54
NO. 32415

Imp's. Alley Blk 102 - Central Park

30'4L / 30 31.3 T.

Ref: FB # 2264-31
Dwg: 11325-L

PAV. EXCEPTIONS = 0.25' & 2.0' Sidewalks

STA.	LT.	RT.
1+50	74.36 74.27 C0.09	74.44 74.47 F0.03
1+25	74.09 74.05 C0.04	74.37 74.25 C0.12
1+00 = E.V.C	74.14 73.83 C0.31	74.02 74.03 F0.01
0+98.3+ = (E.M.H. Begin Conc. Sourkencase)		
0+80	74.01 73.59 C0.42	73.85 73.79 C0.06
0+60	73.08 73.25 F0.17	73.49 73.45 C0.04
0+40	72.94 72.79 C0.15	73.34 72.98 C0.36
(0+25 = L. Paving)		
0+20	72.85 72.22 C0.63	73.34 72.40 C0.94
= B.V.C.		
0+00 = E. Line 30'4L	71.53 Meet Exist.	Meet Exist. 71.70
B.M. Dk. Elev. Rod:		73.98 = S.E. B.P. 30'4L & "L" St.

STA	LT.	RT.
3+50	76.98 76.03 C0.95	77.00 76.23 C0.77
3+25	76.16 75.81 C0.35	77.09 76.01 C1.08
3+00	76.98 75.59 C1.39	76.02 75.79 C0.23
(2+98.3 End Sourkencase)		
2+75	75.82 75.37 C0.45	75.72 75.57 C0.15
2+50	75.56 75.15 C0.41	75.65 75.35 C0.30
2+25	75.36 74.93 C0.43	75.37 75.13 C0.24
2+05 = Sew Lat. ⊼ /- Lt.	74.81 72.75 Rep. C2.06	74.81 72.55 Rep. C2.26
2+00	74.90 74.71 C0.19	75.15 74.91 C0.24
1+75	74.67 74.49 C0.18	74.88 74.69 C0.19

STA.	LT.	RT.
5+40	77.63 77.22 C0.41	77.50 77.40 C0.10
5+20 = grd BRK	77.56 77.18 C0.38	77.73 77.38 C0.35
5+00 = grd BRK	77.38 77.12 C0.26	77.42 77.32 C0.10
4+80	77.31 77.03 C0.28	77.33 77.23 C0.10
4+60 = grd BRK	77.22 76.94 C0.28	77.07 77.14 F0.07
4+40	78.20 76.79 C1.41	77.20 76.99 C0.21
4+20 = grd BRK	77.62 76.65 C0.97	76.90 76.85 C0.05
Chk. T.B.M. (NAIL IN Pole # JPA3061) (F.B.# 2264-40	77.29 = 77.30	
4+00	76.81 76.47 C0.34	76.89 76.67 C0.22
3+75	76.46 76.25 C0.21	76.40 76.45 F0.05

STA.	LT.	RT.
Chk: P.K. NAIL Pole # 925581-H 5+82 LT F.B. 2264-43		78.19 = 78.20
Chk:		(grade - new - CB 76.51 SE. BP 31'57½")
6+00.58 = W. Line 77.28 31'ST.		77.19
5+80.29 (5+75.58 = L. Prop. edge)	77.91 77.27 C0.64	78.13 77.29 C0.84
5+60 = grd brk	77.66 77.26 C0.40	77.29 77.39 C0.10

Clark
Shepinard
Bruner
O'Neil
1-12-55
W.O. 31527

EASEMENT - LOTS 1-24 - VICTORY MANOR; MARKET ST. - PITTA ST. - "J" ST. SEWERS

"J" ST. - E'LY - EASEMENTS LOTS 1-24 - VICTORY MANOR - (M.H. #10 - E'LY to M.H. #4 N'LY to M.H. #2 - PITTA ST.)

Ref: F.B. #1660
DWG: 1439-D
" 1440-D

STA.		Elevs
5+70		126.19 119.86 C 6.33
5+35		125.62 119.11 C 6.51
5+00		124.84 118.35 C 6.49
4+65		123.79 117.60 C 6.19
4+30		122.93 116.84 C 6.09
3+95		122.48 116.09 C 6.39
3+60 = M.H. #9 = P.O.T. Stubs set 10'+25' RT	TO M.H. 12+00 C. 1.51	125.51 115.33 - F.L. C 10.18
3+50		121.25 115.15 C 6.10
3+15		120.92 114.55 C 6.37
2+80		120.41 113.93 C 6.48
2+45		120.05 113.32 C 6.73
2+10		119.51 112.69 C 6.82
1+75		119.06 112.08 C 6.98
1+40		117.78 111.46 C 6.32
1+05		116.97 110.85 C 6.12
0+70		116.30 110.23 C 6.07
0+35		116.01 109.62 C 6.39
0+00 = M.H. #10 = PT 52' N'LY OF EXIST M.H. #5 - DWG. #1004D AT 90° (7' N'LY OF S.D. EXIST.) Stubs set 10 & 25' RT	119.51 TO M.H. 117.00 RIM C. 2.51	119.51 109.00 - F.L. C 10.51
B.M. Dir. Elev. Rod		119.76 = Rim M.H. S'LY R.R. + E'LY OF 59th

1.76 ↑

1.76 ↑

EASEMENT (CONT.)

STA.		Elev's	STA.	Elev's
7+90		131.62 125.01 C 6.61	11+05	139.65 133.63 C 6.02
7+73 = END ENCASE—			10+70	138.37 132.66 C 5.71
7+55	2.74%	131.22 124.05 C 7.17	10+35	137.42 131.70 C 5.72
7+43 = Beg. CONC ENCASE—		~~124.05~~	10+00	135.79 130.74 C 5.05
7+23 = M.H. #8 = P.O.T. Stubs set 10'4 25 RT	132.77 TP M.H. 132.00 C 0.77	132.77 123.17 = F. Line C 9.60	9+65	134.63 129.79 C 4.84
7+10		131.00 122.89 C 8.11	9+30	133.54 128.83 C 4.71
6+75	3.16%	129.75 122.13 C 7.62	8+95	133.02 127.88 C 5.14
6+40		128.78 121.37 C 7.41	8+60	133.13 126.92 C 6.21
6+05		127.56 120.62 C 6.94	8+25	133.07 125.96 C 7.11

2.74%

EASEMENT (CONT.)

STA.	Elev's
14+10	148.11 143.44 C 4.67
13+75	148.20 142.30 C 5.90
13+40	148.35 141.15 C 7.20
13+05	146.92 140.00 C 6.92
12+70	144.55 138.86 C 5.69
12+35	143.24 137.72 C 5.52
12+00	142.04 136.58 C 5.46
11+65	141.11 135.44 C 5.67
CHK! 18181 = 18186 = S.E.B.P. MKT VPITTA	
11+33 = M.H. # 7 (Truly S.D.N.E.R.R.) Rim = 142.00 F 1.08 Δ = 1° 03' 30" LT Stubs set - 10'+20' RT	140.92 134.40 = F.L. C 6.52

3.268

STA.	Elev's
17+05	158.64 152.77 C 5.87
16+70	157.20 151.68 C 5.52
16+35	156.92 150.58 C 6.14
16+00	155.54 149.48 C 6.06
15+65	155.20 148.38 C 6.82
15+30	155.12 147.28 C 7.84
14+95	153.78 146.18 C 7.60
14+59.28 = M.H. # 6 Δ = 0° 40' 30" RT. Stubs set - 8'+16' RT.	Rim 148.92 M.H. 15100 F 2.08 148.92 145.04 = F.L. C 3.88
14+45	148.76 144.59 C 4.17

3.268

EASEMENT to M.H # 2 PITTA

STA.	Elev's
20+05	163.53 158.24 C 5.29
19+70	163.55 157.70 C 5.85
19+35	163.44 157.16 C 6.28
19+00	163.47 156.62 C 6.85
18+65	162.91 156.08 C 6.83
18+30	161.64 155.55 C 6.09
17+95	161.88 155.01 C 6.87
17+59.28 = M.H # 5 Δ = 0°24'30" LT Stubs set — 8'±16' RT℄	159.56 154.46 = F.L. C 4.10
17+40	159.73 153.86 C 5.87

1.54 ↑

3.14 ↑

STA	Elev's
22+81.30 = M.H # 3 = P.O.T. Nails Stubs set — 10'±10' S℄ly of ℄ on Angle { = PT. 2.75 S℄ly N. Line Market ℄ PITTA (grade set on Pav. Nail 6' RT on Angle)	182.21 172.62 = F.L. C 9.59
22+60	182.45 171.34 C 11.11
22+25	179.71 169.24 C 10.47
21+90	174.44 167.14 C 7.30
21+55	170.47 165.04 C 5.43
21+20	167.43 162.94 C 4.49
20+85	165.32 160.84 C 4.48
Chk. 181.86 = 181.86 = SE&R Mkt. & PITTA	
20+54.30 = M.H # 4 { = PT. 20' N'ly & 45' N'ly ℄ PITTA (Set Grade Also on Stub 4.5 RT℄)	164.43 159.00 = F.L. C 5.43
20+40	164.61 158.77 C 5.84

9.09 ↑

1.54 ↑

164.08
159.00
C 5.08

PITTA ST. Nly (CONT.)

STA.	Elev's
	205.54
25+15	195.34
	C 10.20
	203.19
24+80	192.89
	C 10.30
	200.00
24+45	190.44
	C 9.56
	197.56
24+11.73 = GRADE-BVK	188.11 = F.G.
	C 9.45
	195.10
23+85	187.94
	C 10.16
	191.52
23+50	180.77
	C 10.75
	186.99
23+15	176.62
	C 10.37

STA.	Elev's
BVK:	181.89 = 181.86 = S.E.V.B.P. MRT. & PITTA
	211.16
26+38.73 = M.H. #2	204.00 = F.G.
Stubs set - 4.5 & 10' RT	C 8.16
	211.06
26+20	202.69
	C 8.37
	209.77
25+85	200.24
	C 9.53
	208.17
25+50	197.79
	C 10.38

MARKET ST. (& PITTA N'LY)

STA.	Elev's
	184.82
2+80	174.58
	C 10.24
	185.08
2+45	174.33
	C 10.75
	184.79
2+10	174.09
	C 10.70
	185.05
1+75	173.84
	C 11.21
	184.53
1+40	173.60
	C 10.93
	186.28
1+05 (6' RT)	173.35
	C 12.93
	183.64
0+70	173.11
	C 10.53
	183.51
0+35	172.86
	C 10.65
0+00 = M.H #3 = 22+81.30 N'Ly - Pg. 36 (See)	172.62 = F.L
= [PT. & PITTA + 2.75' Sly N. LINE MARKET]	
B.M. DIV. ELEC. RDS.	181.86 = SEB. I MKT + PITTA

0.76 ↑ (Subs. 1.5 - Pat 3)

STA.	Elev's:
	181.90
CK:	= 181.86 = STC B.M.
	178.60
3+85 = D. END.	175.32
	C 3.28
	180.26
3+60	175.14
	C 5.12
	181.67
3+35 = M.H. #1 (P.O.T.)	174.97 = F.L
Stobs set — 4.5' & 10' RT.	C 6.70
	183.06
3+15	174.83
	C 8.23

MARKET ST. - EPITTA - E'ly

STA.		E'lev's
ch K:		=181.86=STG B.M.
1+04 = D.END.		174.75 173.35 F.L C1.40
0+75	(makes 45° ANGLE on W side)	177.29 173.15 C4.14
0+40		180.35 172.91 C 7.44
0+28.27 (Line only)		
0+16.27 = L.P.T.		181.49 172.74 C 8.75
0+04.27 (Line only)		
0+00 = M.H°3 See Pgs 36-38		172.62 = F.L
B.M. Dir. Elev. = Rod:		181.86 = S.E.B.P MKT & PITTA

Clark
Shephard
Brunner
O'Neil
2-4-55
W.O 31577

Imp's. 45th St. - Elizabeth St. Ocean View

Ref: FB# 2314
Dwg: 11380-L
11381-L

45th St. Ocean View to "T"

STA	LT. P.L	LT. CB	LT. ℄	RT. CB	RT. P.L
0+10=CB.B.C. RT. Wly				85.93 86.38 Fo.55	85.85 86.38 Fo.53
=S.Line Ocean View					
0+00 Wly					
#1	86.88	87.02 86.88 Co.14		85.63 86.10 Fo.47	86.10
#2	86.70	86.87 86.70 Co.17		85.25 85.72 Fo.47	85.72
#3=P.Line 45th	86.60 86.60 Grade	86.56 86.60 Fo.04		85.03 85.50 Fo.47	85.00 85.50 Fo.50
#4					
#5					
CB. Rds 20'R., 10' Proj. Ocean View 45th 10'R					
(0+00=S.Line Ocean View Wly of 45th)					

B.M. Dia. Elev. Rod:

85.44=C.Tc. ℄ 45th St. + Ocean View Wly

STA	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
1+89	90.27 89.60 Co.67	89.76 89.60 Co.16		89.16 89.40 Fo.24	89.10 89.40 Fo.30
1+69	89.65	89.44 89.65 Fo.21		89.31 89.50 Fo.19	89.50
1+49	90.09 89.60 Co.49	89.89 89.60 Co.29		89.35 89.45 Fo.10	89.17 89.45 Fo.28
1+29	89.50	89.50 89.50 Grade		89.09 89.30 Fo.21	89.30
1+09	91.26 89.20 C 2.06	89.19 89.20 Fo.01		89.01 89.00 Co.01	89.02 89.00 Co.02
0+89	88.80	88.99 88.80 Co.19		88.36 88.60 Fo.24	88.60
0+69=B.V.C.	90.56 88.28 C 2.28	88.73 88.28 Co.45		87.83 88.20 Fo.37	87.82 88.20 Fo.38
0+44	87.72	87.91 87.72 Co.19		86.81 87.43 Fo.62	87.43
0+19=CB.BC. LT. Ely	88.68 87.17 C 1.51	87.35 87.17 Co.18		86.05 86.66 Fo.61	86.66

45+h (cont.)

STA.	(E4) LT. P.L	LT. CB	℄	RT. CB	RT. P.L
3+59	87.70 87.82 F0.12	87.68 87.82 F0.14		88.12 87.64 C0.48	88.45 87.64 C0.81
3+34	88.10	87.99 88.10 F0.11		88.28 87.90 C0.38	87.90
3+33=W.S.LT.	88.18 88.11 Tp CB C0.07				
3+09	88.81 88.38 C0.43	88.60 88.38 C0.22		88.23 88.17 C0.06	87.96 88.17 F0.21
2+84	88.66	89.14 88.66 C0.48		88.11 88.44 F0.33	88.44
2+59	89.52 88.94 C0.58	88.77 88.94 F0.17		88.19 88.70 F0.51	88.16 88.70 F0.54
2+34.84=W.S. RT	Stob set 5' N&S of H Rods				88.52 88.96 Tp CB. F0.44
2+34	89.22	89.45 89.22 C0.23		88.73 88.97 F0.24	88.97
2+09 E.V.C	89.77 89.50 C0.27	89.40 89.50 F0.10		88.85 89.23 F0.38	88.48 89.23 F0.75

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
5+29=Grade Brk	85.90 85.90 Grade	85.56 85.90 F0.34		85.80 85.80 Grade	86.16 85.80 C0.36
5+09	85.93 86.13 F0.20	85.94 86.13 F0.19		86.12 86.02 C0.10	85.94 86.02 F0.08
4+84	86.40	85.92 86.40 F0.48		86.24 86.29 F0.05	86.29
4+74=W.S. LT.	86.24 86.51 Tp CB F0.27				
4+59	86.42 86.68 F0.26	86.11 86.68 F0.57		86.41 86.56 F0.15	86.42 86.56 F0.14
4+35=W.S. LT.	86.95 86.96 Tp CB F0.01				
4+34	86.97	86.67 86.97 F0.30		86.69 86.84 F0.15	86.84
4+09	87.16 87.25 F0.09	87.09 87.25 F0.16		86.92 87.10 F0.18	87.15 87.10 C0.05
3+84	87.53	87.51 87.53 F0.02		87.34 87.37 F0.03	87.37

Ref: FB 2314-37
FB 1574-14
MAP 11380-L

ELIZABETH: OCEAN VIEW to "T"

STA.	(E'LY) LT. P.L.	LT. CB	E	RT. CB	RT. P.L.
CHK:				85.43	=85.44= STG B.M.
#2 (RAD/CB)		85.54 85.50 C0.04		85.68 85.38 C0.30	
#1	85.53	85.54 85.53 C0.01		85.68 85.40 C0.28	85.40
5799.20=CB.BC LT-ELY PLN: 5799	85.60 85.58 C0.02	85.68 85.58 C0.10			
(F.B. 2319) 5795.04=CB.BC RT-WLY				85.61 85.45 C0.16	85.98 85.45 C0.43
5+79	85.63 85.67 F0.04	85.50 85.67 F0.17		85.36 85.54 F0.18	85.78 85.54 C0.24
5+54	85.79	85.76 85.79 F0.03		85.67 85.67 Grade	85.67

STA.	(E'LY) LT. P.L.	LT. CB	E	RT. CB	RT. P.L.
0+50	72.30 70.68 C1.62	70.71 70.68 C0.03		69.89 70.12 F0.23	71.15 70.12 C1.03
0+30=E.V.C	72.17 70.56 C1.61	70.75 70.56 C0.19		69.78 70.00 F0.22	70.76 70.00 C0.76
0+20	70.56	70.76 70.56 C0.20		69.58 69.90 F0.32	69.90
0+10=CB.B.C.'s	72.02 70.70 C1.32	70.64 70.70 F0.06		69.49 69.75 F0.26	70.30 69.75 C0.55
#1	70.75	70.78 70.75 C0.03		69.42 69.55 F0.13	69.55
#2	71.15	71.72 71.15 C0.57		69.25 69.30 F0.05	69.30
#3	71.84 71.50 C0.34	71.87 71.50 C0.37		68.84 69.00 F0.16	68.91 69.00 F0.09

CB: Rad's:
CB: R=20'
10' PKG OCEAN VIEW
12' PKG-ELIZABETH

[0+00 = S. LINE OCEAN VIEW]

B.M. (See Pg 40)

ELIZABETH (CONT.)

STA.	P.L.	CB.	℄	CB.	P.L.
				RT.	
2+75	72.01	71.87 72.01 Fo.14		71.62 71.45 Co.17	71.45
2+50	73.89 71.86 C2.03	71.65 71.86 Fo.21		71.36 71.30 Co.06	71.78 71.30 C0.48
2+25	71.71	71.62 71.71 Fo.09		71.26 71.15 Co.11	71.15
2+00	72.83 71.57 C1.26	71.40 71.57 Fo.17		70.82 71.01 Fo.19	71.31 71.01 Co.30
1+75	71.42	71.33 71.42 Fo.09		70.87 70.86 Co.01	70.86
1+50	72.09 71.27 Co.82	71.02 71.27 Fo.25		70.82 70.71 Co.11	71.67 70.71 C0.96
1+44.84=Sew.Lat #1 RT.			71.03 64.70 C6.33		71.03 Fl.Prop 65.30 C 5.73
1+25	71.12	71.02 71.12 Fo.10		70.55 70.56 Fo.01	70.56
1+00	72.37 70.97 C1.40	70.80 70.97 Fo.17		70.35 70.41 Fo.06	71.87 70.41 C1.46
0+75	70.82	70.84 70.82 Co.02		70.17 70.26 Fo.09	70.26

STA.	P.L.	CB.	℄	CB.	P.L.
		LT.		RT.	
4+80	73.74	73.75 73.74 Co.01		73.49 73.22 Co.27	73.22
4+74.84=Sew Lat #2 RT.			72.90 66.90 C 6.00		72.90 Fl.Prop. 67.50 C 5.40
4+60	75.29 73.34 C1.95	73.32 73.34 Fo.02		72.90 72.79 Co.11	72.46 72.79 Fo.33
4+40	73.04	73.38 73.04 Co.34		72.64 72.49 C0.15	72.49
4+20=B.H.C.	74.30 72.86 C1.44	73.01 72.86 Co.15		72.41 72.30 Co.11	72.16 72.30 Fo.14
4+00	74.02 72.73 C1.29	72.67 72.73 Fo.06		72.19 72.18 Co.01	72.06 72.18 Fo.12
3+75	72.58	72.54 72.58 Fo.04		72.14 72.03 Co.11	72.03
3+50	73.87 72.44 C1.43	72.32 72.44 Fo.12		71.97 71.88 Co.09	71.78 71.88 Fo.10
3+25	72.30	72.01 72.30 Fo.29		71.57 71.74 Fo.17	71.74
3+00	73.50 72.15 C1.35	72.04 72.15 Fo.11		71.62 71.59 Co.03	71.54 71.59 Fo.05

ELIZABETH

STA.	LT. P.L	CB.	E	RT. CB	P.L
CLK					=85.61= City Disc. E 43rd Ave "T"
CHK				85.44	=85.44= ST C.B.M.
#2 = N.L. "T"	78.55	79.07 78.55 C0.52		78.03 78.05 F0.02	78.05
# 1 = BNK	78.40	78.64 78.40 C0.24		77.95 78.00 F0.05	78.00
5494.84 = CB. B.C's:	79.80 78.10 C1.7	77.71 78.10 F0.39		77.67 77.70 F0.03	76.22 77.70 F1.48
5474.84 = Sew Lat. #4 LT. F.L. Prop	72.20		67.7		
5467.42	76.89	76.61 76.89 F0.28		76.60 76.49 C0.11	76.49
5+34.84 = W.S. LT.	75.53 T.P.C.B.				
5+40 = E.V.C.	77.26 75.69 C1.57	75.40 75.69 F0.29		75.08 75.29 F0.21	74.63 75.29 F0.66
5424.84 = Sew Lat #3 LT. F.L. Prop	76.66 70.70 C5.96		76.66 67.30 C9.36		
5420	74.92	74.96 74.92 C0.04		74.63 74.48 C0.15	74.48
5400	75.60 74.27 C1.33	74.39 74.27 C0.12		74.09 73.74 C0.35	73.74 74.4 73.74 Grade
4484.84 = W.S. RT.					73.31 73.30 T.P.C.B. Grade

Clark
Shephard
Brunner
O'Neill
3-10-55

W.O. 21206

SANITARY SEWER : VICINITY 54th & MARKET : CROSSING SD-VE. R.W. ELY OF 54th, SLY MKT.

REF: DWG: #11213-L
F.B. 2270-47

Note: See also Pg 33

STA.		Elev's
CHK:		
0+52 = ℄ EXIST M.H	[DWG: 1440-D] #10 (8" Sewer) ELY OF 54th 97' NLy-NWly LINE R.R.R.W.	115.36 109.00 = F.L. EXIST 6.36 (Stubs 6" R.L. RT M.H)
0+20	(stubs set 4.5 W'LY℄) 5-20%	118.83 107.34 C 11.49
0+00 = ℄ EXIST M.H	(15"-TRUNK-Sewer) SLy R.R. & ELy 54th	119.41 (℄ TP First joint Reading Down)] 105.64 = INVERT EXIST M.H 106.30 = INVERT C 13.11 8" Sewer
B.M.	Dir. Elev. Rod.	119.76 = TP RIM M.H (EXIST) 15" Sewer SLy R.R. & ELy 54th

C/Clark
Shepherd
Bruner
O'Neil
3-30-55

W.O. 20622

DRAINAGE DITCH - LOT 358 - SUNSHINE GARDENS & SOUTH CHOLLAS CREEK N'Ly to Rena ST.

Ref: F.B. # 2242 - 56-19
DWG: 5535-B-34B
T.P.S. # 3339

Note: Plans changed to Current grades No. 1 set 4/6

STA.	LT.	℄	RT. (E'ly)
2+07 = N'ly Fc. 6' x 5' x 10" Conc. Hdwall (= End 29" x 18" C.M.P.) (Y) (X)		73.70 F.L	
1+82		72.75	
1+57 = S'ly Fc. 6 x 5 x 10" Conc. H'dwall (Beg 29" x 18" C.M.P.) (Y) (X)		71.80 = F.L.	
1+20		71.69	
0+80		71.57	
0+40		71.45	
0+00		71.33 F.L	

Note Base Ditch 0+00 to 1+57 = 1.5'
S = 1:1
Grade = 0.32%

STA.	LT.	℄	RT. (E'ly)
4+18.39 = N'ly End INLET			
3+98.39 = S'ly End 20' B-2 CB. INLET (meet EXIST. CB. grades) (NEW CB's Fc to be 10")			
3+58.39 = E.C (Beg 40' of 29" x 18" C.M.P.			F.L
3+46.52 = mid. PT.			
3+34.65 = B.C Δ = 25° LT. ER = 514'			F.L
2+92			
2+52			
2+12 = Grade Brk			75.00 F.L

Base Ditch = 2'
S = 1:1
Grade = 1.5%

Clark
Shephard
Bruner
O'Neil

6-29-55
W.O. 32315

Ref: F.B. 2254-39
Dwg: 11767-L

IMP's Alley Blk 2 - Swan's Addit.
From N'ly Line Olive - 300' N'ly

STA.	LT		RT	
1+20	293.41 292.77 C 0.64		293.24 292.47 C 0.77	
1+05 = Sew Lat #2 - RT.		293.3 280.7 F.L. C 12.6 ℄	286.2	293.31 286.7 = F.L. C 6.61 Prop.
1+00	294.01 292.97 C 1.04			293.20 292.67 C 0.53
0+80 = B.V.C.	293.76 293.00 C 0.76			292.83 .80 292.70 .70 C 0.13 C 0.10
0+60 = Sew Lat. #1 - RT.		292.6 280.5 F.L. C 12.1 ℄	292.6 286.1 = B.V.C. C 6.5 grade	292.66 F.L. 286.6 = Prop. C 6.06
0+60 (alley grade)	293.86 292.94 C 0.92			292.14 292.64 F 0.50
0+40	294.65 292.88 C 1.77			292.63 .59 292.58 .58 C 0.05 Cond
0+20 2' BK	294.30 292.82 C 1.48		292.82 292.26 ℄ C 0.56	292.82 292.52 C 0.30
0+00 = N'ly Line Olive 2' BK	293.69 292.70 C 0.99		292.82 292.00 C 0.82 ℄	292.82 292.40 C 0.42
Chk: 1+77 10' RT F/ gar.	=	290.85 = 290.87 FB 2254-42		
B.M. Dir. Elev. Rod:				297.19 = S.E. B.P. Fairmount & Quincy

Note: Stubs set IN Ref: to edge Pav - Not Mon. Line

47

STA.	LT	RT
[Chk: 2 x 2 ℄ P.O.T. = 286.43	= 285.41	= 286.44 FB 2254-43]
3+00	285.82 5.76 283.25 3.25 C 2.57 C 2.51	281.81 281.98 282.75 282.75 F 1.14 F 0.77
2+80	289.13 289.08 284.68 284.68 C 4.45 C 4.40	284.74 284.34 284.38 284.38 C 0.36 F 0.04
2+60	290.70 290.65 286.10 286.10 C 4.60 C 4.55	287.26 287.22 285.80 285.80 C 1.46 C 1.42
2+40 = E.V.C.	292.40 287.53 C 4.87	289.66 289.23 287.23 287.23 C 2.43 C 2.00
2+28 = Sew Lat #3 - RT.	289.69 281.8 = F.L. C 7.87 ℄	282.1 289.61 282.7 = F.L. C 6.97 Prop.
2+20	292.96 288.87 C 4.09	290.63 289.98 288.57 288.57 C 1.46 C 1.41
2+00	293.38 290.02 C 3.36	290.69 290.16 289.72 289.72 C 0.57 C 0.43
1+80	293.19 290.98 C 2.21	290.81 290.68 C 0.13
1+60	292.46 291.76 C 0.70	292.56 291.46 C 1.10
1+40	293.08 292.34 C 0.74	292.96 292.04 C 0.92

Clark
Shephard
Bruner
O'Neil

Imp's: Franklin Ave: Evans to 28th

6-30-55
W.O. 32380

Ref: FB 2262-54
Dwg: 2653-D

STA	LT. Gutt.	℄	RT. Gutt.
3+40 = Gutt Brk	77.50	78.52	79.33
0+10 = Gut. Brk	70.71	71.76	71.57
0+00 = Ely Line Evans	70.50	71.43	71.35
0-10 = E. CB. Line Evans	70.45	71.18	71.12

B.M. Div. Elev. Rod: 71.03 = SW. 7" C.T. Evans Y Franklin

Note: CB's Exist.- Gutt. grades set at Sta's. shown. Y taken in between Brks.

48

STA	LT. Gutt.		RT. Gut.	
0+20 = G. Brk	81.63	82.67	82.49	
0+00 = Ely Line Sampson St.	81.32	82.19	82.42	
6+00 = Wly Line Sampson St.	81.36	82.08	82.36	
5+80 = Gutt Brk	81.19	82.26	82.10	

FRANKLIN AVE:- (CONT.)

STA.	LT. GUTT.	E	RT. GUTT.
CHK:			
2+45.46 = Prop COIN. RT.			83.35
2+42.14 = CB. B.C IN RT.			83.34
1+82.40 = CB. BC LT.	82.43		
2+12.81: E only		83.30	
1+79.08 = Prop. Conn (FRANKLIN & W'ly 284ft.) ON LT.	82.50	83.40	83.06
1+79 G. Brk RT. only		83.26	82.93

Clark
Shephard
Brunner
O'Neil

8-16-55

W.O. 32424

Imp's: Calle Del Oro

From E'ly Line La Jolla Shores Drive to W'ly Line Calle Del Cielo

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
0+50	31.75	31.68 31.75 Fo.07		31.63 31.75 Fo.12	31.75
0+25	31.02	31.08 31.02 Co.06		30.89 31.02 Fo.13	31.02
0+00=E.Line La Jolla Shores Drive	30.46 30.30 Co.16	30.45 30.30 Co.15		30.23 30.30 Fo.07	30.19 30.30 Fo.11
0-20	29.80	29.50 29.80 Fo.30		29.67 29.90 Fo.23	29.90
0-39.5 =C.B.C.	28.40 29.53 F1.13	28.75 29.53 Fo.78		28.89 29.70 Fo.81	29.70
# 1	29.47	28.66 29.47 Fo.81		29.09 29.75 Fo.66	29.75
# 2	28.81 29.41 Fo.40	28.78 29.41 Fo.63		30.66 29.83 Co.83	30.46 29.83 Co.63
#3 = End Co. LT+RT		28.86 29.40 Fo.54		30.67 29.84 Co.83	

B.M.: Div. Elev. Rod:

27.69 = SW'ly. Disc.

Ref: F.B. 2348-6
F.B. 1827-51
DWG: 11944-L

50

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
2+10	40.46 38.72 C1.74	38.85 38.72 Co.13		38.73 38.72 Co.01	39.31 38.72 Co.59
1+85	37.41	37.53 37.41 Co.12		37.39 37.41 Fo.02	37.41
1+60=E.V.C.	37.17 36.10 C1.07	36.21 36.10 Co.11		36.30 36.10 Co.20	36.82 36.10 Co.72
1+40 (=WAT. Service Rt.)	36.21 35.09 C1.12	35.22 35.09 Co.13		34.66 35.09 Fo.43	35.96 TP on CB 35.09 WAT. Serv. Co.87
1+25=Sew Lat. # 1 - RT.	(stub 5' Bk Prop as 5' ely)		35.30 28.40 ℄ C6.90		35.3 29.5 Prop. L C5.8
1+20	34.19	35.05 34.19 Co.86		34.38 34.19 Co.19	34.19
1+00	33.80 33.38 Co.42	33.91 33.38 Co.53		33.45 33.38 Co.07	33.89 33.38 Co.51
0+80	32.67	32.74 32.67 Co.07		32.74 32.67 Co.07	32.67
0+60=B.V.C.	32.50 32.05 Co.45	32.02 32.05 Fo.03		32.03 32.05 Fo.02	32.08 32.05 Co.03

(L.S. 2201) La Jolla Shores Drive & Camino Del Oro

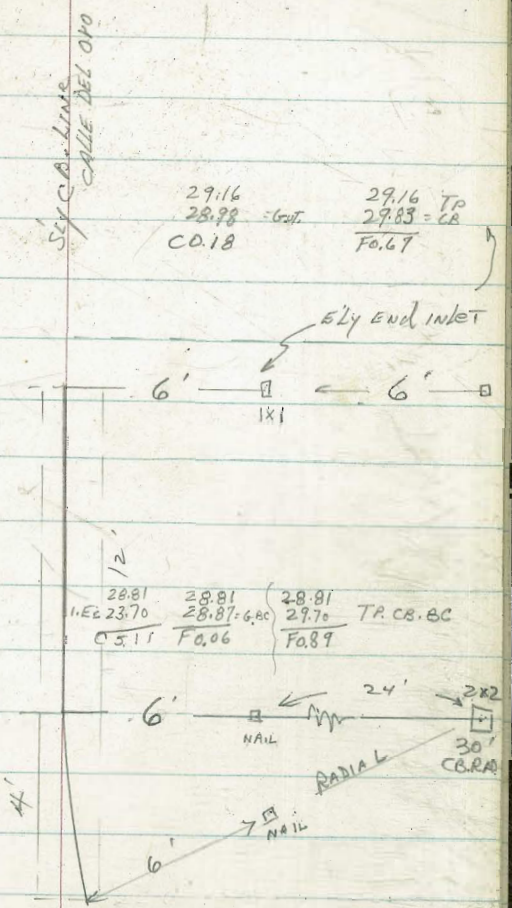
STA.	P.L	CB.	E	CB.	P.L
3+60 = E.V.C.	49.04 48.40 C0.64	48.48 48.40 C0.08		48.52 48.40 C0.12	49.28 48.40 C0.88
3+40	46.56	46.69 46.56 C0.13		46.71 46.56 C0.15	46.56
3+20	46.37 44.95 C1.42	45.17 44.95 C0.22		45.24 44.95 C0.29	46.17 44.95 C1.22
3+00	43.56	43.64 43.56 C0.08		43.90 43.56 C0.34	43.56
2+80 B.V.C	43.72 42.40 C1.32	43.18 42.40 C0.78		42.56 42.40 C0.16	43.30 42.40 C0.90
2+60	42.73 41.35 C1.38	41.22 41.35 F0.13		41.35 41.35 grade	42.10 41.35 C0.75
2+40 = MAT. service RT. only					40.84 40.29 = TPCB C0.55
2+35	40.03	40.01 40.03 F0.02		40.40 40.03 C0.37	40.03
2425 = SEW LAT #2 - RT			40.38 31.70E C8.68		40.38 34.00 P.I. line C6.38

STA	P.L	LT. CB	E	RT. CB	RT. P.L
				67.25 67.94 F0.69	67.94
#2 = END CB RT. (CALLE CIELO)					
#1 RT.				65.74 65.97 F0.23	65.97
5+10 LT. only		64.41 63.71 C0.70			
5+07.99 = CB. RT. only B.C. RT.				63.55 64.00 F0.45	62.64 64.00 F1.36
4+87.99 RT. only				61.59 61.17 C0.42	61.17
4+85 LT. only		60.61 61.16 F0.55			
4+67.99 (= B.V.C.) (on RT. only)	59.22 58.93 C0.29			59.24 58.93 C0.31	61.03 58.93 C2.10
4+60	58.14	58.11 58.60 F0.49		58.46 58.14 C0.32	58.14
4+35	55.70	55.72 56.05 F0.33		56.00 55.70 C0.30	55.70
4+10	53.64 53.26 C0.38	53.34 53.50 F0.16		53.45 53.26 C0.19	53.58 53.26 C0.32
3+85	50.83	50.84 50.95 F0.11		50.91 50.83 C0.08	50.83

Note: GRADE CHANGE ON N'LY SIDE ST. AS PER OFFICE ORDER - CONST. CB ON N'LY SIDE TO MEET EXIST. INLET ——— (Remove 29" R.C.P. type CB)

STA.	LT. P.L	LT. CB	Ø	RT. CB.	RT. P.L
CHK:		67.86	= 67.89 = TP CB Ø		
			5450.2		
5+48.A≠ = W'ly end EXIST. INLET - N'ly side ST.		67.63 = Meet EXIST			
5+35 LT. only		66.08 66.26 Fo.18			
CHK:	63.90				
5+19 ≠ LT. only (Meet EXIST. CB. LT.)	63.90				
5+16 = N.W. Corn. P.C.	63.61				
(See Note Pg. 51)					

15' TYPE B-2 CB. INLET
S'ELY CAILE DEL ORO
Y LA JOLLA Shores Drive



C/a H.K. GARBER BRUNER. O'NEIL

10-17-55

W.O. 32452

Imp's - Roosevelt Ave: (CB. & Rough-Grades)

[E. Line Alley Blk 17 to Kendall]

Ref: Dwg: 2804-D T.P.B. = 20 (F.B 23.6 NOT Fd.)

STA.	Prop.	LT. CB.	&	RT. (S'LY) CB.	Prop
1+00 = W. Line	Kendall				
0+87.5	Gutt. at B.C	27.14 26.57 Co.57		26.99 26.55 Co.44	Gutt. at B.C
0+87.5 = CB. BC	27.73 27.07 Co.66	27.14 27.07 Co.07		26.99 27.05 Fo.06	28.39 27.05 C1.34
0+75	27.12	27.21 27.12 Co.09	26.98 27.10 Fo.12	26.98 26.10 Co.88	27.10 ~~26.10~~
0+50	28.30 27.20 C1.10	27.24 27.20 Co.04		27.15 27.18 Fo.03	28.54 27.18 C1.36
0+25	27.29	27.32 27.29 Co.03		27.23 27.27 Fo.04	27.27
0+02 = Alley B.C		26.57 27.36 Fo.79		26.58 27.37 Fo.79	
Alley E.C.		26.57 27.42 Fo.85		26.58 27.40 Fo.82	Alley E.C.
0+00 = E. Line Alley Blk 17 (CB. P.I.)	28.16 27.38 Co.78	28.30 27.74 TP.CB Prop Co.56		28.80 27.72 TP.CB Prop C1.08	28.32 27.36 Co.96
B.M.	Dif. Elev. Rod:			24.89 - C.T. N'ly CB. La Playa & Yosemite	

Roosevelt (Cont.)

E. Line Kendall to N. Line Sequoia

STA	Prop	LT. CB	&	RT. (S'LY) CB.	Prop
1+17 = Alley B.C.		24.42 24.72 Fo.30		24.69 24.72 Fo.03	
Alley E.C	→	24.42 24.80 Fo.38		24.69 24.80 Fo.11	← Alley E.C.
1+15 = E.L. (CB. P.I.) Alley →	25.75 24.76 Co.99	25.59 25.12 TP.CB Prop. Co.47		26.71 25.12 TP.CB Prop C1.59	27.11 24.76 C2.35
1+00 = W.L. (CB. P.I.) Alley →	26.84 24.94 C1.90	26.74 25.30 TP.CB Prop. C1.44		26.96 25.30 TP.CB Prop C1.66	27.00 24.94 C2.06
Alley E.C	→	24.83 24.98 Fo.15		24.76 24.98 Fo.22	← Alley E.C.
0+98 = Alley B.C		24.83 24.96 Fo.13		24.76 24.96 Fo.20	
0+75	25.22	25.09 25.22 Fo.13		25.47 25.24 Co.23	25.24
0+50	26.90 25.49 C1.41	25.46 25.49 Fo.03		25.62 25.54 Co.08	26.81 25.54 C1.27
0+25	25.77	25.63 25.77 Fo.14		25.79 25.83 Fo.04	25.83
0+12.5 = CB. B.C.	27.37 25.91 C1.46	25.89 25.91 Fo.02		25.99 25.98 Co.01	27.18 25.98 C1.20
0+00 = E. Line Kendall	26.04	chk: 26.04 26.04		26.13	26.13

ROOSEVELT (CONT.)

SEQUOIA to LAMONT.

STA	LT. P.L.	LT. CB.	£	RT. (SLY) CB.	RT. (SLY) P.L.
		21.57 21.65 Fo.08 21.57 21.75 Fo.18		21.49 21.64 Fo.15 21.49 21.70 Fo.21 ← Alley E.C.	
Alley E.C.		24.19			
1+15 = E.L. Alley	24.43 TP CB Prop. 21.67 TP CB Bk. walk C2.76	22.67 C1.52 21.80 22.07 Fo.27		22.30 22.02 TP CB Prop. Co.28	22.34 21.66 Co.68
1+00 = W.L. Alley	24.49 TP CB Prop. 21.72 TP CB Bk. walk C2.77	24.44 22.72 C1.72 21.89 22.12 Fo.23		22.51 22.07 TP CB Prop. Co.44	22.42 21.71 Co.71
Alley E.C.		21.78 21.80 Fo.02		21.69 21.75 Fo.06 ← Alley E.C.	
0+98 = Alley B.C.		21.78 21.73 Co.05		21.69 21.72 Fo.03	
0+75	21.84	21.97 21.84 Co.13		21.84 21.84 Grade	21.84
0+50	25.10 21.96 C3.14	22.05 21.96 Co.09		21.97 21.96 Co.01	23.51 21.96 C1.55
0+25	22.08	22.29 22.08 Co.21		22.04 22.08 Fo.04	22.08
0+12.5 = CB. BC	25.13 22.14 C2.99	22.23 22.14 Co.09		22.05 22.14 Fo.09	23.27 22.14 C1.13
0+00 = E.L. Sequoia	22.20				22.20

ROOSEVELT (CONT.)

STA	LT. P.L.	LT. CB.	£	RT. (SLY) CB.	RT. (SLY) P.L.
2+15 = W.L. Sequoia	CH# 2290 22.90				22.88
2+02.5 = CB. B.C.	25.53 23.13 C2.40	23.01 23.13 Fo.12		23.07 23.11 Fo.04	24.35 23.11 C1.24
2+00	23.18	23.05 23.18 Fo.13		23.14 23.16 Fo.02	23.16
1+75	23.65	23.62 23.65 Fo.03		23.87 23.63 Co.24	23.63
1+50	25.38 24.11 C1.27	23.99 24.11 Fo.14		24.36 24.10 Co.26	26.54 24.10 C2.44
1+25	24.57	24.73 24.57 Co.16		24.80 24.57 Co.23	24.57

ROOSEVELT (CONT.)

E. LINE - LAMONT to CROWN PT. DR. (W. LINE)

STA.	LT. P.L.	LT. CB.	LT. ℄	RT (S'LY) CB.	RT (S'LY) P.L.
2+15 = W.L. LAMONT.	chk 20.92 20.96				20.56
2+05 = CB. B.C	22.94 21.02 C1.92	21.09 21.02 C0.07		20.75 20.67 C0.08	22.11 20.67 C1.44
2+00	21.06	21.17 21.06 C0.11		20.97 20.73 C0.24	20.73
1+75	21.27	21.50 21.24 C0.26		21.15 21.00 C0.15	21.00
1+50	23.58 21.42 C2.16	21.47 21.42 C0.05		21.26 21.28 F0.02	22.43 21.28 C1.15
1+25	21.60	21.64 21.60 C0.04		21.45 21.55 F0.10	21.56

STA.	E. LINE					
1+35.7 = Alley B.C		19.88 19.94 F0.06				
	Alley E.C →	19.88 19.99 F0.11				
1+33.7 = E.L. Alley LT.	20.32 19.95 C0.37	20.44 Alley Prop. 20.31 C0.13				
1+18.7 = W.L. Alley LT.	20.44 20.00 C0.44 (E.C.) →	20.48 20.36 Alley Prop. C0.13 19.96 20.04 F0.08 19.96				
1+16.7 = Alley B.C		19.99 F0.03		19.55 19.32 = END CB. C0.23	#2	
1+16 = Prop. Corn. = R.T.				19.75 19.72 = 1 C0.33	19.49 19.43 C0.06	
1+08.59 = C.B.B.C (TIE-PT dn.T) R.T.				19.78 19.52 C0.26	19.52	
1+00	21.02 20.09 C0.93	20.14 20.09 C0.05		19.71 19.61 C0.10	19.94 19.61 C0.33	
0+75	20.22	20.30 20.22 C0.08		20.05 19.89 C0.16	19.89	
0+50	21.46 20.35 C1.11	20.45 20.35 C0.10		20.27 20.17 C0.10	21.22 20.17 C0.05 C1.05	
0+25	20.47	20.57 20.47 C0.10		20.50 20.45 C0.05	20.45	
0+10 = C.B.B.C	21.60 20.54 C1.06	20.56 20.54 C0.02		20.78 20.62 C0.16	21.01 20.62 C0.39	
0+00 = E.L. LAMONT.	20.59				20.73	

GRAND ST. (See also Pg 57)

SELY CB. RET. GRAND & INGRAHAM

STA.	P.L	CB.	℄	CB.	P.L
	END CB = #1	19.70			
		19.82			
	20.69	Fo 12			
1476.42 = Prop.	19.80				
Conv. LT.	Co. 89				
	20 59	19.63			
1456.96 = CB	19.89	19.89			
B.C. LT.	Co. 70	Fo 26			

STA.	GUTT.	CB.	
		53.96	Chk:
#6 = CB. E.C. GRAND	53.29	53.96	(meet EXIST.)
	54.07	54.07	
#5	53.38	54.01	
	Co. 69	Co. 06	
	53.95	53.95	
#4	53.42	54.02	
	Co. 53	Fo. 07	
	54.06	54.06	
#3	53.45	54.01	
	Co. 61	Co. 05	
	53.99	53.99	
#2	53.42	53.95	
	Co. 57	Co. 04	
19°20'			
#1			
= CB B.C. INGRAHAM	53.31	53.81	meet EXIST

Chalk
Garber
O'Neil
Steffens
10-27-55
W.O. 32382

IMPS. GRAND ST. (CB GRADES)

JEWELL to KENDALL

STA.	P.L	LT. CB	℄	RT. (S'Ly) CB	P.L
1+50		51.93 51.87 C0.06		50.95 50.79 F0.04	
1+25		51.86 51.80 C0.06		50.79 50.72 C0.07	
1+00		51.90 51.72 C0.18		50.75 50.64 C0.11	
0+75		52.00 51.65 C0.35		50.28 50.57 F0.29	
0+50		51.91 51.57 C0.34		50.88 50.49 C0.39	
0+25		51.97 51.50 C0.47		51.39 50.42 C0.97	
0+10 = CB.B.C	(Set By C.S)	51.45		51.21 50.37 C0.84	
0+00 = E. Line Jewell					

(Note: For SE'Ly RT. GRAND + INGRAHAM - see Pg 56)

B.M. Dir. Elev. Rod.

STA.	P.L	LT. CB	℄	RT. (S'Ly) CB	P.L
3+75		51.59 51.50 C0.09		50.74 50.42 C0.32	
3+50		51.71 51.57 C0.14		50.87 50.49 C0.38	
3+25		51.71 51.65 C0.06		50.62 50.57 C0.05	
3+00		51.73 51.72 C0.01		51.17 50.64 C0.53	
2+75		51.82 51.80 F0.28		51.01 50.72 C0.29	
2+50		51.68 51.87 F0.19		50.76 50.79 F0.03	
2+25		51.74 51.95 F0.21		50.64 50.87 F0.23	
2+00 = Grade BM2		51.70 52.02 F0.32		51.30 50.94 C0.36	
1+75		51.86 51.95 F0.09		50.71 50.87 F0.16	

GRAND ST. (Cont.)

JEWELL to KENDALL

STA	LT. P.L	LT. CB.	℄	RT. CB.	RT. P.L
(4+99.73) 5+00 = W. line Kendall					
4+90 (4+89.73) = CB. B.C		51.15		50.07	
(Set B&C's)					
4+75		51.20		50.90 50.12 C0.78	
4+50		51.57 51.27 C0.30		50.88 50.19 C0.69	
4+25		51.70 51.35 C0.35		50.98 50.27 C0.71	
4+00		51.67 51.42 C0.25		50.76 50.34 C0.42	

GRAND ST.

CB. RET'S: GRAND & JEWELL

N'W'LY

STA.	GUTT.	CB's.
# 5 = E.C JEWELL (meet)	51.78	52.28
# 4	51.92 51.54 C0.38	51.92 52.08 F0.16
# 3	51.88 51.40 C0.48	51.88 51.98 F0.10
# 2	51.74 51.33 C0.41	51.74 51.94 F0.20
# 1	52.22 51.30 C0.92	52.22 51.95 C0.27
CB. B.C. GRAND (meet)	51.32	51.99

S'W'LY

	GUTT.	CB.
# 5 = E.C JEWELL		50.16 50.09 C0.16
# 4		50.58 50.30 C0.28
# 3		50.69 50.55 C0.14
# 2		50.61 50.72 F0.11
# 1		50.92 50.85 C0.07
CB. BC. GRAND		50.96 (Set B&C's)

CB. Rot's: GRAND & JEWELL

STA. N'ELY	GUTT.	CB's:
#5 = E.C JEWELL	(meet)	52.28 (meet)
#4		51.86 52.01 F0.15
#3		51.68 51.78 F0.10
#2		51.47 51.63 F0.16
#1		51.84 51.55 C0.29
B.C. GRAND		51.45 (set by C.S)

S'ELY	GUTT.	CB.
#5 = E.C JEWELL (Meet)	50.63 50.63 49.40 49.30 C1.23 C1.33	50.63 50.63 49.80 49.90 C0.83 C0.73
#4	50.86 49.50 C1.36	50.86 50.06 C0.80
#3	50.76 49.58 C1.18	50.76 50.20 C0.56
#2	50.97 49.62 C1.35	50.97 50.30 C0.67
#1	50.26 49.67 C0.59	50.26 50.34 F0.08
B.C. GRAND	49.70	50.37

CB. Rot's: GRAND & Kendall

STA. N'W'LY	GUTT.	CB's
#5 = E.C Kendall	50.73 chk 50.72	51.54 chk 51.55 (meet)
#4	51.61 50.98 C0.63	51.61 51.48 C0.13
#3	51.31 50.91 C0.40	51.31 51.41 F0.10
#2	51.62 50.83 C0.79	51.62 51.33 C0.29
#1	51.81 50.75 C1.06	51.81 51.25 C0.56
B.C GRAND	50.32	51.15

S'W'LY		
#5 E.C Kendall		50.60
#4		50.56 50.47 rod ck. C0.09
#3		50.49 50.30 C0.19
#2		50.56 50.20 C0.36
#1		50.71 50.12 C0.59
B.C: GRAND		50.07

CB. Ret's: GRAND & KENDALL

STA. N'ELY	GUTT:	CB'S:
# 5 E.C Kendall	50.82 50.75	51.67 51.58
# 4	51.60 51.07 C0.53	51.60 51.57 C0.03
# 3	51.48 51.02 C0.46	51.48 51.56 F0.08
# 2	51.48 50.97 C0.51	51.48 51.53 F0.07
# 1	51.57 50.92 C0.63	51.57 51.54 C0.03
B.C GRAND	50.86	51.53 (meet)

S'E'LY	GUTT:	CB'S:
# 5 E.C Kendall	50.32	50.82
# 4	50.56 50.18 Ca.38	50.56 50.70 end CB F0.14
# 3	50.43 50.07 C0.36	50.43 50.63 F0.20
# 2	50.65 49.99 C0.66	50.65 50.60 C0.05
# 1	50.67 49.92 C0.75	50.67 50.57 C0.10
B.C. GRAND	49.87	50.57 chk: 50.54 meet

CB. Ret's: GRAND & LAMONT

N'W'LY

(Standoby C.S.)

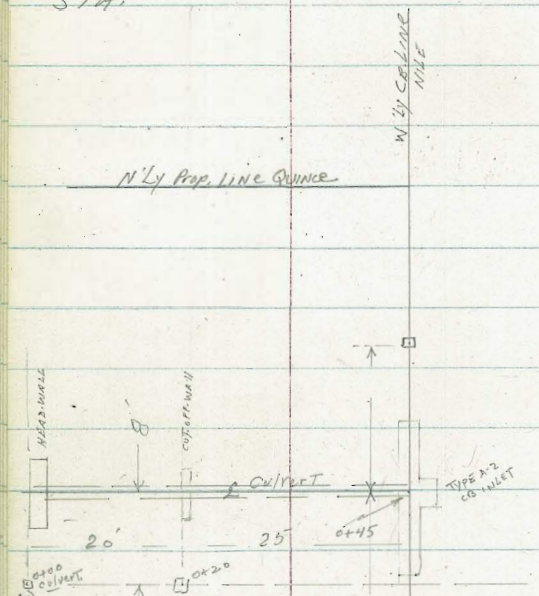
S'W'LY	GUTT:	CB. 48.60 EXIST.
# 5 E.C. LAMONT.	48.00	48.50
# 4	48.70 48.08 C0.62	48.70 48.73 F0.03
# 3	48.69 48.15 C0.54	48.69 48.80 F0.11
# 2	48.65 48.20 C0.45	48.65 48.85 F0.20
# 1	48.83 48.23 C0.60	48.83 48.90 F0.07
CB. B.C. GRAND	48.09	48.92 (meet)

Clark
GARBER
BRUNER
O'NEIL
12-1-55
W.O. 32500

Imp's: QUINCE ST: NILE to HALLER

Culvert = NILE & QUINCE

STA.



Void
Change - P/ANS (INLET)
McKee

See Pg 66 & 67

Void
Change - P/ANS
McKee (NILE ST. CONNECT)

℄ QUINCE

277.55
277.50 T.P. C.B. ℄ INLET & S'Ly END
C0.05

277.55
276.67 = GUTT. ℄ INLET
C0.88

277.55
271.00 = F.L. BOX ℄ INLET
C 6.55

277.55
276.80 = GUTT. 8' S'Ly ℄ INLET
C0.75

shot on stub 260.04
16' RT 0+00
Culvert

Ref: DWG: 1041-L
F.B. 231-18

61

C.B. GRADES - W'Ly END QUINCE Across

STA	C.B.	GUTT.
0+60 = S'Ly Line QUINCE	277.00	277.20
0+50	277.50	277.00
0+30 = ℄ QUINCE	277.50	276.80
0+22 = ℄ INLET	277.50	276.67
0+00 = END EXIST. C.B. W'Ly LINE QUINCE & W'Ly C.B. LINE NILE	278.44	277.81

CB. GRADES @ QUINCE: NILE to VANCOUVER

STA.	P.	CB	E	CB.	P.
	283.19	280.87		280.85	281.29
1+00	281.30	281.30		280.77	280.77
	C 1.89	F 0.43		C 0.08	C .52
				279.95	
0+80 (OK. ON RT)				280.11	
				F 0.16	
0+60 = B.V.C					
0+40					
0+20					
[Rough-grade stubs - Set on P. Lines]					
= E.C. LT.					
0+00 = E. LINE NILE (TO NORTH)					
0-60 RT. ONLY					

See Pg 66 For CHANGE

LT. PT.

STA.	P.	CB	E	CB.	P.
		284.20			
1+70.10 Alley E.C	284.37	284.37			
		F 0.17			
ALLEY AT Prop (1+70.10) ELY LINE ALLEY	284.53	286.64 284.53			
		C 2.11		283.88	284.39
1+65 RT ONLY				283.75	283.75
				C 0.13	C 0.64
(1+50.10)		284.25			
ALLEY AT. Prop (W'LY LINE ALLEY)	283.51	283.51			
	284.25 283.69	C 0.74			
(to meet exist imp's Alley)	C 0.56				
		282.30			
1+50.10 = Alley E.C	283.35	283.35			
		F 1.05			
		282.30			
1+48.10 = ALLEY B.C	283.21	283.21			
		F 0.91			
	282.90	282.21		282.42	282.56
1+40 = E.V.C	282.80	282.80		282.50	282.50
	C 0.10	F 0.53		F 0.08	C 0.06
		281.58		281.87	
1+20	282.00	282.00		281.56	281.56
		F 0.42		C 0.31	

STA	LT. P.	LT. CB	LT. ℄	RT. CB.	RT. P.
(3+20.21)		CLK 292.46-EXIST.			
3+20 = E.C EXIST	292.46	292.46		291.50	291.50
3+00	291.39	291.20 291.39 FO.19		290.34 290.50 FO.16	290.50
2+90	293.00 290.84 2.16	290.87 290.84 CO.03		289.69 290.00 FO.31	290.53 290.00 CO.53
2+65	289.48	289.57 289.48 CO.09		288.59 288.75 FO.16	288.75
2+40	289.66 288.12 C1.54	288.05 288.12 FO.07		287.76 287.50 CO.26	288.11 287.50 CO.61
2+15	286.77	286.98 286.77 CO.21		286.22 286.25 FO.03	286.25
1+90	287.19 285.41 C1.78	285.42 285.41 CO.01		284.92 285.00 FO.08	285.93 285.00 CO.93
1+72.10 = ALLEY B.C	284.43	284.20 284.43 FO.23			

STA	P.	CB	℄	CB	P.

CB. GRADES, QUINCE / VANCOUVER TO HALLER

STA.	P.	LT. (N'LY) CB.	E	RT. CB.	P.
1+47.86 = Alley B.C	293.27	292.67 293.27 Fo. 60		291.58 292.77 F 1.19	292.77
1+40	293.50	293.21 293.50 Fo. 29		292.25 293.00 Fo.75	293.00
1+20	294.74 293.80 C0.94	293.28 293.80 Fo. 52		292.52 293.30 C0.22	293.99 293.30 C0.69
1+00	293.90	293.39 293.90 Fo. 51		292.94 293.40 Fo. 46	293.40
0+80 = B.V.C	294.71 293.80 C0,91	293.56 293.80 Fo. 24		293.06 293.30 Fo.24	294 20 293.30 C0,90
0+60	293.58	293.60 293.58 C0.02		292.94 293.00 Fo.06	293.00
0+40	294.65 293.35 C1.30	293 43 293.35 C0,08		292.51 292.70 Fo. 19	293 54 292.70 Co. 84
0+20	29313	292.98 293.13 Fo. 15		292.35 292.40 Fo.05	292.4
(E.C. EXIST) 0+00 = E. LINE VANCOUVER	meet EXIST. 292.90	meet EXIST. 292.90		meet EXIST 292.10	292.10

STA.	P.	LT. CB	E	CB.	P.
2+00	293.26 291.20 C 2.06	290.54 291.20 Fo,66		290.94 290.70 C0.24	29254 290.70 C1.84
1+80	292.10	291.43 292.10 Fo.67		291.79 291.60 C0.19	291.60
1+71.86 = Alley B.C	292.43	291.78 292.43 Fo. 65		291.88 291.93 Fo.05	291.93
1+69.86 = Alley E.C	292.54	291.78 292.54 Fo. 76		291.88 292.04 Fo. 16	292.04
(469.86) Alley at Prop. (E'LY LINE Alley)	294 13 292.70 C1,43	294 07 292.70 C 1.37		292.17 292.20 F 0.03 Fo.13 (turnout pave)	292.20
(449.86) Alley at Prop. (W'LY LINE Alley)	294.73 293.40 C1.33	294192 293.40 C1.32		293.78 292.90 C0.88	292.90
1+49.86 = Alley E.C	292.67 293.24 Fo.57	292.67 293.24 Fo.57		291.58 292.74 F1.16	292.74

STA.	LT. P.	LT. CB.	℄	RT. CB.	RT. P.
(3+19.72)	286.09	282.23		282.46	286.10
3+20 = W.	280.80	280.80		280.60	280.60
LINE HALLER	C5.29	C1.43		C1.86	C5.5
3+10	282.00	282.35 282.00 C0.35		283.42 281.50 C1.92	281.50
3+00	283.10	283.04 283.10 F0.06		283.99 282.60 C1.39	282.60
2+80	290.01 285.10 C4.91	285.19 285.10 C0.09		285.60 284.60 C1.00	289.54 284.60 C4.94
2+60	287.00	286.78 287.00 F0.22		286.96 286.50 C0.46	286.50
2+40	291.87 288.60 C3.27	288.49 288.60 F0.11		288.28 288.10 C0.18	290.93 288.10 C2.83
2+20	290.00	289.43 290.00 F0.57		289.83 289.50 C0.33	289.50

CLARK

INTERSECTION: NILE & QUINCE

Plans changed to meet Nile st. Connect.

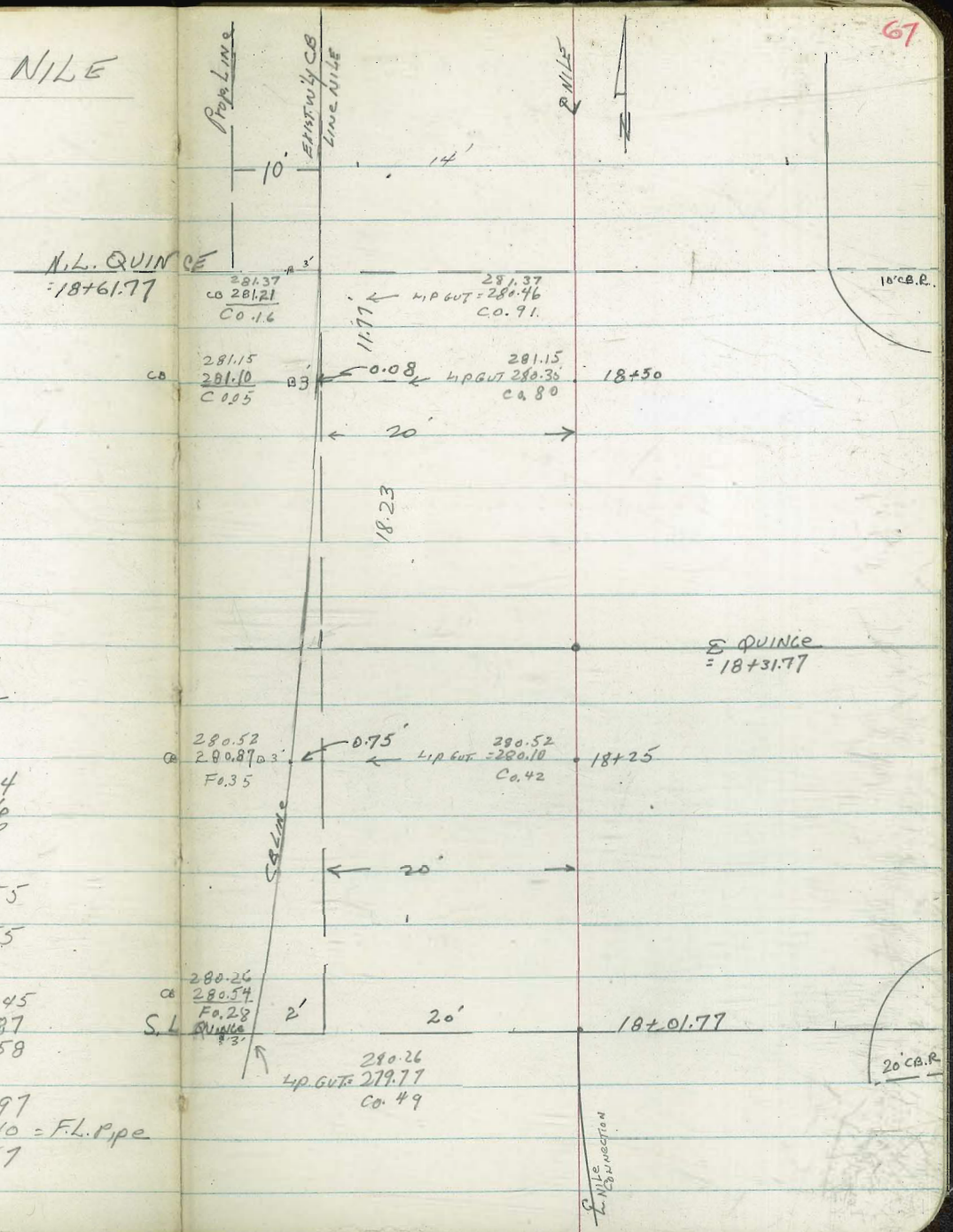
STA.	P.	CB	E	CB (Mckee)	P. Prop.
#1 (stubs 5' BK CB Fc)			GUT.	278.29 277.47 C0.82	278.29 277.97 CB C0.32
0+12 = B.C RT.	279.72	279.41 279.72 F0.31	GUT.	278.33 277.74 C0.59	278.33 278.24 CB C0.09
0+00 = E.Line Nile (= B.C LT.	279.92 279.60 C0.32	278.98 279.60 F0.62			
#1 - mid RT	279.53	278.95 279.53 F0.58			
E.C (Nile) ST.	279.92 279.62 C0.30	meet const. 279.66 279.62			
0-60	278.40 281.04 F2.64	281.04		280.37	276.13 280.37 F4.24

B.M. 279.69 = N.E. B.P. Nile & Quince

FOR CB ACROSS W'LY END QUINCE SEE Pg 67

STA.	P.	CB	E	CB	P.
(CONT. ON Pg 62)					
0+80 Meet DWG: 12041-L ON LT (N'LY)	282.08 280.80 C1.28	280.68 280.84 F0.12			
0+60 Meet DWG: 12041-L ON RT (S'LY)	281.63 280.45 C1.18	280.32 280.45 F0.13		279.56 279.58 F0.02	279.58 279.58 Grade
0+36	281.21 280.09 C1.12	279.66 280.09 F0.43		278.76 278.90 F0.14	282.89 278.90 C3.99
#4 = E.C Nile			GUT.	277.73 276.63 C1.10	277.73 277.13 CB C0.60
#3			GUT.	279.19 276.93 C2.26	279.19 277.43 CB C1.76
# 2" mid RT 4" E CB INLET	(stubs 7' BK CB) INLET F.L. 281.79 INLET 272.87 C8.92	281.79 FRONT OF GRATE 277.20 C4.59	BK. OF GRATE	281.79 276.87 C4.92	281.79 277.70 CB C4.09

CULVERT - INTERSECTION NILE & QUINCE



1+03.6 = CB Fc. ℄ Inlet.
See Pg 66

281.79
272.87
C8.92

0+74.3

277.64
271.96
C5.68

0+45 = ℄ RT.

277.55
271.0
C6.55

0+20 = Fc. Cut-off Wall

265.45
258.87
C6.58

0+00 = Fc. H'd Wall

257.97
248.40 = F.L. Pipe
C9.57

Clark
Garber
Bruner
O'Neil

12-29-55
W.O. 21271

CULVERT: LOT C - RESUBDIV. LA JOLLA HILLS #2

Ref: F.B. 2362-2
Dwg: 5463-B

0+60 = End Ditch — meet Exist. grid-level

0+40 = Beg Ditch 20.19 20.19
End Pipe & Fc. Hdwall Base-wall 6.00 8.40 = F.L. Inc Pipe
C 14.19 C 11.79

16.79
4.20
C 12.59

0+20

(Stubs set 10' RT (w'ly) ℄)

0+00 = End Exist 30" Pipe meet — 0.00 = F.L.

B.M. = Dir. Elev. Rod: (8.90) — 9.22 = Ch □ — 5' w'ly Tp CB 2' RT ℄ Inlet.

Clark
GARBER
BRUNER
O'NEIL
1-4-56
W.O. 31505

Imp's: Hugo St. Clove to Plum to D. End

CB's: Clove to Plum

STA.	Prop	LT. (N'ly) CB	E	RT CB	Prop
	112.39	113 32		113 42	114.91
1+10	113.30	113.30		113.90	113.90
	Fo.91	Co.02		Fo.48	C1.01
		114 67		115.28	
0+90	114.75	114.75		11515	115.15
		Fa08		Co.13	
	115.30	115 98		116.95	121.13
0+70	116.25	116.25		116.70	116.70
	Fo.95	Fo.27		Co.25	C4.43
		118 22		119 12	
0+50	118.30	118.30		118.90	118.90
		Fo.08		Co.22	
		120.02		120 72	
0+37.50	119.90	119.90		120.50	120.50
		C012		Co22	
	123.17		123.17		
0+30=Sew	117.3 prop		116.60 &		
LAT. #1 LT.	C5.87		C6.47		
	123 99	121.45		122.52	126.71
0+25 CB. BC	121.70	121.70		122.50	122.50
	C1.29	Fo.25		Co.02	C4.21
		124.1			
0+20=W.S	El. CB	122.4			
LT.		C1.7			
		123 32		124.44	
0+12.5=#1		123.60		124.70	
(on Return)		Fo.28		Fo.26	
		125.48 chk:		chk: 126.85	
0+00=S'ly	125.5 Proj	125.46		126.86 = Exist Mheet	
Line Clove					
(℄ Sta.)					

B.M. Div. Elev. Rod:

96.34 = N'ly Corn. Exist. CB (N'ly) - 145' S'ly Plum St (Hugo St)

Ref: Dwg: 2902-D
F.B. 2220-70

RT. 70

STA	Prop	CB	℄	CB	Prop
	111.60				109.76
3+00 = Prop	107.95				106.90
	C3.65				C2.86
		111.10		109.50	
#3		107.80		105.95	#3
		C3.30		C3.55	
		109.11		108.27	
#2		107.95		106.90	#2
		C1.16		C1.37	
		108.30		108.15	
#1		108.15		107.80	#1
		C0.15		C0.35	
	111.73	108.56		108 44	109.38
2+75 = CB. BC	108.40	108.40		108.40	108.40
N'ly Plum	C3.33	C0.16		C0.04	C0.98
		108 93		108 85	
2+53.75	108.70	108.70		108.83	108.83
		C0.23		C0.02	
	111.00	109 01		109.30	109.60
2+32.50	109.00	109.00		109.25	109.25
	C2.00	C0.01		C0.05	C0.35
		109.39		109.59	
2+11.25	109.30	109.30		109.68	109.68
		C0.09		F0.09	
	111.06	109 74		110.25	112.09
1+90 = E.V.C.	109.60	109.60		110.10	110.10
	C1.46	C0.14		C0.15	C1.99
		110 11		110 51	
1+70	110.20	110.20		110.70	110.70
		F0.09		F0.19	
	111.32	111 06		111 79	112.60
1+50	110.90	110.90		111.50	111.50
	C0.42	C0.16		C0.29	C1.10
		112 10		112 60	
1+30	112.00	112.00		112.60	112.60
		C0.10		Grade	

CB's: Hugo ÷ Plum to Turnaround

STA	(N'ly) LT. Prop	CB	℄	RT. CB	Prop
0+80=Sew Lat #2 LT.	103.15 95.90 C 7.25	prop	103.15 92.50 ℄ C 10.65		
0+76.48=CB B.C. of T. Turnaround	103.40 101.16 C 2.24	100.24 101.16 Fo 92		101.29 101.16 C0.13	103.42 101.16 C 2.26
0+50	102.88	103.02 102.88 Co. 14		103.09 102.88 Co. 21	102.88
0+30=Sew Lat #3 LT	107.01 99.20 prop C 7.81		107.01 95.77 ℄ C11.24		
0+25=CB BC	107.20 104.50 C 2.70	104.52 104.50 C0.02		104.51 104.50 C0.01	109.96 104.50 C 5.46
0+00 (℄ Ly Lwe Plum)	107.68 106.35 C1.33				109.15 104.95 C4.20
#1		105.51 105.31 C0.20		105.02 105.00 C0.02	
#2		106.65 106.35 C0.30		106.66 104.95 C1.71	
#3		107.89 107.15 Co. 74		109.79 104.40 C 5.37	
(℄ STA's:)					

B.M. (See Pg 70)

STA	LT. Prop	CB	℄	RT. CB	Prop
1+50=D. End ST.	88.90 96.40 F7.5				93.26 96.40 F3.14
#6 1+45=mid-PT. Turnaround		96.56 CB. 96.20 Co 36		meet EXIST. at S4 end inlet: 96.18	
#5 meet EXIST.	96.34	96.34 meet 96.34		97.56 96.65 Co. 91	96.65
#4 1+30 office change to meet EXIST 21 Rcd. of EXIST INLET.	97.36	97.01 99.00 Co.01		98.03 97.47 Co. 56	97.47
#3 1+17	99.29 98.33 Co.96	98.65 97.95 Co.70		98.51 98.40 Co.11	98.08 98.40 Fo 32
#2 1+03.49=P.R.C. Turnaround	101.62 99.27 C2.35	99.14 99.27 FO.13		100.88 99.35 C 1.53	101.95 99.35 C 2.60
#1 0+89.99 = mid-PT. curve	100.20	98.86 100.20 F 1.34		99.84 100.20 FO. 36	100.20

Clark
Gamber
O'Neil
Abrenilla
3-12-56
W.O. 32378

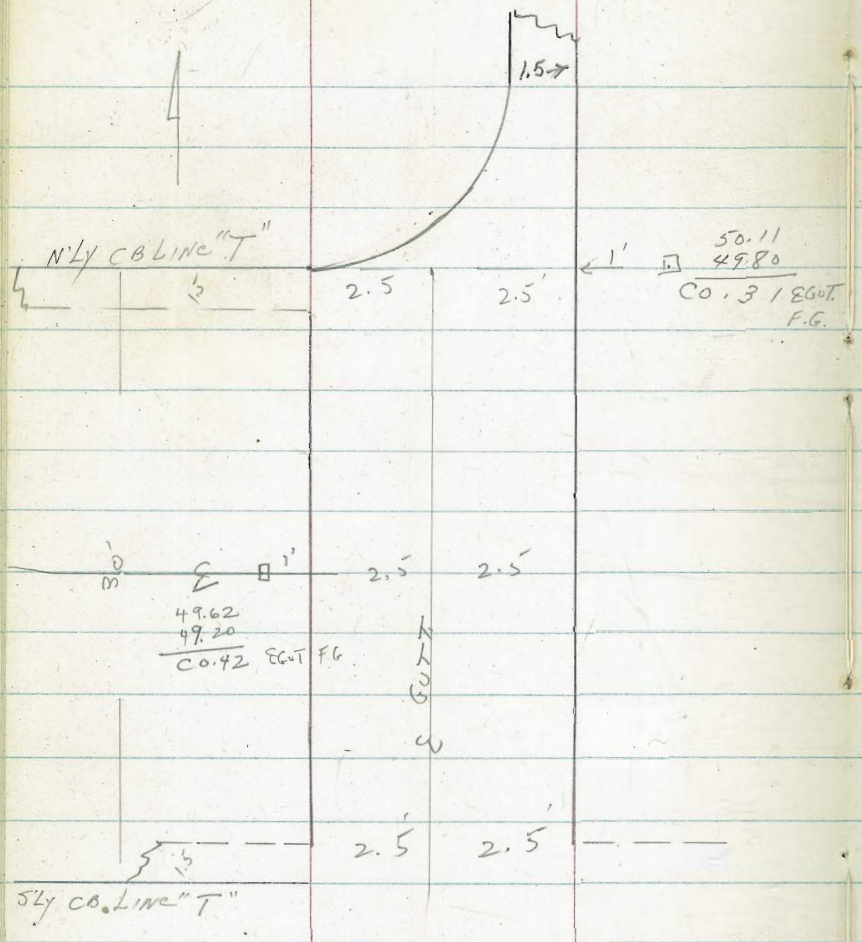
Imp's "T" St. 39+4 to 40+4

STA.	LT.		RT.
6+52.6 = CB. B.C.LT.	50.50 G = 50.00		CB 49.50 / G = 49.00
Note: CB's EXIST. Set GRADE FOR CUTTING			
0+30	G 65.27		
0+00 = E. LINE 39+4	CB 66.50 GUTT. 65.88		CB 67.50 G = 67.00
B.M.:	Dif. Elev. Rod:		91.89 = S.E. B. P 38+4 "T"

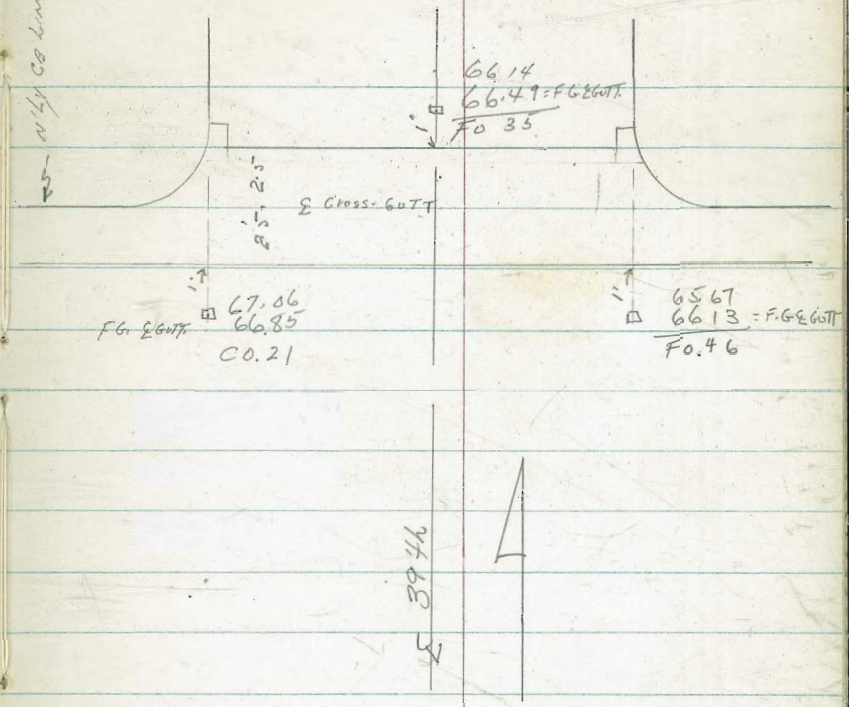
GRADES 50' CB : From W'ly Line 40+4 – 50' E'ly – 5'4y side "T"

STA.	LT.		RT. (5'4y)
0+50 = END CB.			49.49 48.54 C 0.95
0+40			49.76 48.65 C 1.11
0+30			50.00 48.80 C 1.20
0+20			50.20 49.00 C 1.20
0+10			50.08 49.23 C 0.85
0+00 = END EXIST. CB W'ly LINE 40+4			49.50 = EXIST.

Conc. Cross-Gutt 40'+L + "T"



Conc. Gross-Gutt. 39'+L "T"



CLARK
GARBER
O'NEIL
ABRENILLA
5-8-56
W.O. 31793

ALTADENA AVE Sewer - S'ly Line

OAK PARK ANNEX } S'ly to end ST.

Note: Blue-Line DATA = Change Office DWG.

Ref: DWG: 3067-D - 3072-D
F.B. 2296-33

STA	Elev. Lat's:		Elev. MAIN
~~1+55 = Sew LAT #8 LT.~~	325.7 319.8 prop C 5.9	325.7 319.2 ℄ C 6.5	
1+40			325.58 304.89 C 20.69
1+05			326.62 304.78 C 21.84
1+05 #8 LT. ~~0+75 = Sew LAT #7 LT.~~	326.85 Prop 320.8 C 6.05	326.8 320.2 ℄ C 6.6	
0+70			327.02 304.68 C 22.34
0+35 = Sew LAT #6 LT	327.73 320.00 Prop C 7.73	327.7 319.4 ℄ C 8.3	327.05 304.57 22.48
0+00 = M.H #1 Δ = 10°24'10" RT. 10' 28'	(Beg Conc. cradle) (DWG.)		325.78 304.47 21.31
0-54.02 EXIST Stub-end 98.68 - S'ly of ℄ Sterling Court			321.47 304.31 C 17.16

(Note: See Pg 76 For Grades 0-54 to 0-152.7)

B.M. DIM. ELEV. ROD: 326.30 = 2" Pine 35'

STA:	Elev. LAT's:		Elev. MAIN
3+50 = Sew. LAT #12 LT.	319.56 311.9 Prop C 7.66	319.56 311.3 ℄ C 8.26	316.68 305.52 C 11.16
3+40 = M.H #2 P.O.T.			317.18 305.49 C 11.69
3+15			318.32 305.41 C 12.91
3+15 ~~3+05 = Sew LAT #11 LT~~	320.87 313.7 prop C 7.17	320.87 313.1 ℄ C 07.77	
2+80			319.73 305.31 C 14.42
2+75 = Sew LAT #9 RT. 2+60 End Cradle		318.62 stub ℄ 307.40 C 11.22	318.62 Prop 308.00 C 10.62
2+45			321.00 305.20 C 15.80
2+45 ~~2+35 = Sew LAT #10 LT.~~	322.95 311.6 Prop C 11.35	322.95 311.0 ℄ C 11.95	
~~2+15 = Sew LAT #9 LT~~	323.18 317.4 Prop C 5.78	323.18 316.8 ℄ C 6.38	
2+10			322.75 305.10 C 17.65
Sew LAT #9 1+75	325.2 Prop 318.5 C 6.7	325.2 317.9 ℄ C 7.3	324.32 304.99 C 19.33

46' RT ℄ ALTADENA to S'ly ON S. LINE OAK PARK ANNEX (F.B. 2296-36)

6+65	Not set	306.46
6+30		311.38 306.36 C 5.02
5+95		310.91 306.25 C 4.66
5+60		310.85 306.15 C 4.70
5+25		311.24 306.04 C 5.20
4+90		311.98 305.94 C 6.04
4+55		312.86 305.83 C 7.03
4+20		313.94 305.73 C 8.21
3+85		315.11 305.62 C 9.49
3+71.50 = Beg 10° Cn. Enc.		

Chk: 326.29 - 326.30 = STG BM

Set T.B.M. 2X2 HUB 50' R.P. E'ly = 310.80
OF E'ly E HUB (E ALTADENA St'y L.)

8+52.06 = Plug end.	313.92 307.02 C 6.90
8+40	313.96 306.98 C 6.98
8+05	313.92 306.88 C 7.04
7+70	313.63 306.78 C 6.85
7+35	313.07 306.67 C 6.40
7+00	312.65 306.57 C 6.08
6+70.88 = M.H. #3 L 13° 27' 30" LT. (PNG.) 13° 28'	312.19 306.48 C 5.71

ALTADENA Sewer (added to this Cont.)

98.7' 8" Sewer to replace EXIST 6" Sewer

(Cont. on Pg 74)

0-54.02 — See Pg 74. — 304.31

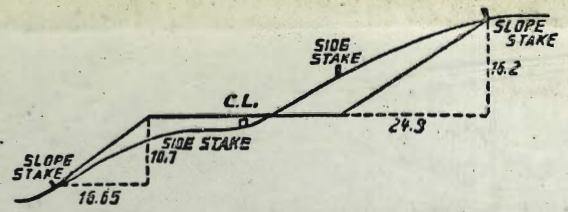
0-86.9 — 319.61 / 304.21 / C15.40

0-119.8 — 318.40 / 304.11 / C14.29

0-146.8 = Sew. LAT #16 LT. — 319.4 / 310.1 prop / C9.3 — 319.4 / 309.5 = Σ / C9.7

This piece Sewer (6") with 8" by Contractor supposedly replaced by City: to be done by

0-152.7 = EXIST M.H E Sterling Court W'ly & ALTADENA B.M - See Pg 74) — CHK: 303.95 Meet 304.01



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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