

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 16 1965

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DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side of road
stake for any width roadway, slope 1 1/2 to 1
If ground is level, the distance from the side of the
road to the stake is the same as the distance from the
stake to the center of the road.

IMPROVED TABLES
AND
INFORMATION

cut taper. If it does not make the right
adjustment necessary.

TABLE No. VII

To find Tangent and Distance from curve of
any other degree, divide by degree of curve and
add correction found in column of correction.
Degree of curve, with a given T and L, found
by dividing tangent (or distance) by
given tangent (or distance).
The distance from a point on the tangent to
the curve is nearly the square of the tangent
length divided by twice the radius.

Curb Stakes - Thorn St.
 Plan - 11320-L - 10-21-54 :70.
 W.O. 32083

	South		
0+00 = E.L. Fairmount		18.00	
+35	16.69	16.20 ⁶⁹	C 0.49
+70	14.62	14.39 ⁶²	C 0.23
1+05	13.08	12.58 ^{3.08}	C 0.50
+22.73 = P.C.	11.70	11.66 ⁷⁰	C 0.04
To Alley	11.70	11.60	C 0.10
S. end.	11.40	11.85 ⁴⁰	F 0.45

	North		
		19.20	
	17.33	17.23 ³³	C 0.13
	15.27	15.27	C 0.07
	12.70	13.20 ^{2.70}	F 0.50
1+27.47 = P.C.	11.46	11.91 ⁶⁶	F 0.25
To Alley	11.66	11.85 ⁶⁶	F 0.19
S. end - W	12.29	12.10 ²⁹	C 0.19
S. end - E.	14.31	11.50 ^{4.31}	C 2.81
To Alley	10.70	11.25 ^{0.70}	F 0.55
P.C. = 0+00	10.70	11.10 ^{0.70}	F 0.40
+30	09.04	09.62 ^{0.4}	F 0.58
+60	07.59	08.13 ^{7.59}	F 0.54
+90	06.20	06.64 ²⁰	F 0.44
1+15 = Meef.		05.40	

44th

44th - To E.

2

South

North

0+00 = PC - Meet.

04.98

05.36

+30

5.87

06.80
5.87

F 0.93

7.08

07.34

F 0.26

+60

8.31

08.62

F 0.31

9.06

09.32
06

F 0.26

+90

10.64

10.44
64

C 0.20

11.31

11.30

C 0.01

1+15 = PC.

12.22

11.97
22

C 0.25

12.90

12.95

F 0.05

To Alley

12.22

12.14
22

C 0.08

12.90

13.12

F 0.22

End - w

12.53

12.40
53

C 0.13

13.48

13.38
290

C 0.10

Highland - Rough Grades.

30' R.P. Hub = 295.06

3

		West		East
0 + 00 = S.L. Thorn		21.5		22.0
+50			23.3	^{3.3} 20.2 C 3.1
1 ~			20.8	^{20.8} 18.4 C 2.4
+50			19.0	^{9.0} 16.6 C 2.4
2 ~	cb. = 13.87	13.75	16.9	^{6.9} 14.7 C 2.2
+50	11.4	^{10.4} 10.7	15.4	^{5.4} 11.7 C 3.7
3 ~	06.8	07.6	14.3	^{14.3} 08.7 C 5.6
+50	05.0	04.8	11.4	^{11.4} 05.8 C 5.6
4 ~ = End. cbs.	96.5	01.9	97.6	^{9.7} 02.9 C 6.8
+60	88.7	98.4	06.7	^{06.7} 99.4 C 7.3
5 + 00	70.9	76.8	01.5	^{01.5} 96.1 C 5.4
+40	65.2	89.6	✓ 99.0	^{9.0} 90.8 C 8.2
6 + 00.22 = N.L. Redwood.	59.4	80.0	F 1.0	^{91.0} 81.8 C 10.1

97.56
 262
 94.94

Rough Grades - Jewell St. - Reed to
 W.O. 32160 - 10-27-54 - 7.0.
 Plan - 11292-L

Garnet. - 58.43 = NE BP - Reed. 4
 49.33 = Cross - Thomas

		West		
0+00 = N.L. Reed	58.15	58.21		
+50 - 2 Bk	59.2	57.7 ^{9.2}	C 1.5	
1+00	58.2	56.6 ^{8.2}	C 1.6	
+50 - 3' B.	53.6	53.9	F 0.3	
2+00	51.2	51.1 ^{1.2}	C 0.1	
+50	46.6	48.4 ^{6.6}	F 1.8	
+69.68 = S.L. Thomas	47.45	47.50		

0+00 = N.L. Thomas	46.65	46.66		
+50 - 0.1 B.	46.6	46.2 ^{6.6}	C 0.4	
+90 = on Julet.		45.96		
1+45 = N.L. Alley	47.0	46.5 ^{7.0}	C 0.5	
+95 - 0.5 B.	51.9	48.0 ^{51.9}	C 3.9	
2+45	49.9	49.8 ^{9.9}	C 0.1	
+69.46 = S.L. Grand.	50.65	50.68		

	East.		
	cb. 58.57	58.64	
	61.9	58.2 ^{61.9}	C 3.7
2 B.	60.5	57.0 ^{60.5}	C 3.5
	59.1	54.5 ^{9.1}	C 4.6
4' B.	52.7	51.6 ^{7.7}	C 6.1
	55.7	48.8 ^{55.7}	C 6.9
		48.03	
		47.24	
	46.9	46.5 ^{6.9}	C 0.4
		45.96	
	45.8	46.5 ^{5.8}	F 0.7
	46.0	48.0 ^{6.0}	F 2.0
	47.1	49.7 ^{7.1}	F 2.6
	50.59	50.61	

Grand to Hornblend.

5

		West		East	
0+00 = N.L. Grand	51.82	52.00		51.82	52.00
+50 - 0.2 B	55.2	^{5.2} 53.5	C 1.7	53.6	^{3.6} 53.5 C 0.1
1 ~	55.6	^{5.6} 55.0	C 0.6	54.7	55.0 F 0.3
+50		56.5	2 B.	57.0	^{7.0} 56.5 C 0.5
2 ~		58.0		57.6	58.0 F 0.4
+50		59.4		59.3	59.4 F 0.1
+70.20 = SL	59.67	60.00		59.83	60.00
Hornblend					
0+00 = N.L.	61.27	61.32		61.27	61.32
+50 - 8 in	63.3	^{3.3} 63.2	C 0.1	62.7	^{2.7} 63.0 F 0.3
1 ~	64.6	^{4.6} 64.4	C 0.2	63.6	64.1 F 0.5
+50	65.8	65.6	C 0.2	65.7	^{3.6} ^{5.7} 65.3 C 0.4
2 ~	67.0	66.8	C 0.2	66.6	^{6.6} 66.3 C 0.3
+50	68.3	68.0	C 0.3	67.9	^{7.9} 67.4 C 0.5
+68.90	end 68.48	68.50 66	1 in	67.73	67.87

Garnet

Rough Grades -
Plan - 11263-L

53rd - Imperial to Santa Margarita
11-3-54 7.0.

156.03 - SE. Pole Imperial
157.53 - R.P. Cross - NE. Santa Marg

		W.			East.	
1+61.55 = PC. on W.	56.6	^{6.6} 55.2	C 1.4		55.6	^{5.5} 54.9 C 0.6
1+20	56.4	^{6.4} 55.4	C 1.0		56.1	^{6.1} 55.1 C 1.0
0+80	56.8	^{6.8} 55.6	C 1.2		55.7	^{5.7} 55.4 C 0.3
+40	59.1	^{9.1} 55.8	C 3.3	Line	55.5	55.5 G
0+00 = PC. on E.	60.8	^{60.8} 56.2	C 4.6	= 1+43.84	56.5	^{6.5} 55.9 C 0.6
42.685 = Prop. PC.	62.1	^{62.1} 57.1	C 5.0	1+06.70	57.2	^{7.2} 56.8 C 0.4
1/3	62.4	^{62.4} 57.8	C 4.6	0+81.18 = EC. cb.	57.6	57.6 F 0.1
2/3	63.4	^{63.4} 59.4	C 4.0	+50.72 = PC. cb.	57.8	58.1 7.8 F 0.3
E.C.	64.2	^{4.2} 61.4	C 2.8	+24.33	58.3	58.3 G
				0+00 = Prop. PC.	58.8	^{8.8} 58.4 C 0.4

Rough Grades - San Jacinto

89.37 = \pm ct. Church ward + San Jacinto 7

West.

East. 91.69 = Top.

0-91.42		86.54		
0-42.23 = cb. PC	87.6	88.0 7.6	F 0.4	
0+00 = \pm PC.	85.8	85.8	G	
+40 = Esta.	83.6	83.5 3.6	C 0.1	
+80	81.2	81.2	G.	
1+26.41 = PC. on W.	78.2	77.3 8.2	C 0.9	
+27.34				
+67.34 = on E.				
2+07.34				
Prop. PC's				
0+00 = opp	71.1	71.2	F 0.1	
+50	67.0	67.0	G	
1+00	66.0	64.0 6.0	C 2.0	
+50	61.9	61.1 6.9	C 0.8	
2+00	60.3	58.7 60.3	C 1.6	
+40	57.9	57.0 7.9	C 0.9	
+62.77				
+64.27 = PC.	57.4	56.1 7.4	C 1.3	
End on Imp.	57.2	55.42 7.2	C 1.8	

= Prop. PC

= PC on E.

= PC.

92.1	91.3 2.1	C 0.8
92.4	89.0 92.4	C 3.4
89.7	86.8 9.7	C 2.9
87.6	84.6 7.6	C 3.0
85.8	82.0 5.8	C 3.8
81.3	78.0 81.3	C 3.3
78.1	76.7 8.1	C 1.4
75.6	76.3 5.6	F. 0.7
75.3	72.2 5.3	C 3.1
72.0	68.0 72.0	C 4.0
69.5	65.0 9.5	C 4.5
64.2	62.1 4.2	C 2.1
60.9	59.7 60.9	C 1.2
59.3	58.0 9.3	C 1.3
58.2	57.1 8.2	C 1.1
58.2	55.9 8.2	C 2.3

Rough Grades - Santa Margarita

8

		South		North			
0 + 00 = B.C.	76.9	^{6.9} 74.8	C 2.1	cb. P.C.	71.8	74.0	F 2.2
+ 40	77.3	^{7.3} 74.1	C 3.2		72.4	73.4	F 1.0
+ 80	76.5	^{6.5} 73.6	C 2.9		72.8	72.7	C 0.1
1 + 20	75.8	^{5.8} 73.2	C 2.6		70.9	72.1	F 1.2
+ 60	75.6	^{5.6} 72.2	C 3.0		70.7	71.6	F 0.9
+ 99.11 = R.C.	75.6	^{5.6} 72.1	C 3.5		70.2	71.0	F 0.8
^{29.50} 2 + 28.61	75.5	^{5.5} 72.0	C 3.5		68.4	71.0	F 2.6
+ 68.61 = End on S.	76.7	^{6.7} 74.0	C 2.7		71.6	72.4	F 0.8
^{27.86} + 96.47					69.6	74.7	F 5.1
3 + 24.33					73.5	77.0	F 3.5
^{50.85} 75.18 = Meet						80.68	

Curb Stakes - Jewell

11-5-54 7.0

9

Reed to Thomas.

West.

East.

0+00 = N.L. Reed.

58.15

58.21

58.57

58.64

+24.92

58.16

57.97^{8.16} C 0.19

58.90

58.43⁹⁰ C 0.47

+49.84

57.76

57.73⁷⁶ C 0.03

58.50

58.23⁵⁰ C 0.27

+69.84

57.49

57.44⁴⁹ C 0.05

58.02

57.94⁸⁰² C 0.08

+89.84

57.12

56.92⁷¹² C 0.20

57.41

57.42 F 0.01

1+09.84

56.76

56.15⁷⁶ C 0.61

56.70

56.65⁷⁰ C 0.05

+20.82 = P.C.

56.56

55.59⁶⁵⁶ C 0.97

56.22

56.09²² C 0.13

= Alley P.C.

56.56

55.47⁶⁵⁶ C 1.09

56.22

55.97⁶²² C 0.25

= End. 3

57.39

55.79 C 1.60

60.15

56.29^{60.15} C 3.86

54.62

54.66 F 0.04

58.82

55.16 C 3.66

= Alley

54.18

54.34 F 0.16

54.75

54.84 F 0.09

1+48.82 = P.C.

54.18

54.03¹⁸ C 0.15

54.75

54.53⁷⁵ C 0.22

+74.84

52.92

52.58⁹² C 0.34

53.51

53.08⁵¹ C 0.43

2+04.84

51.08

50.89¹⁰⁸ C 0.19

T.P.

51.47

51.39⁴⁷ C 0.08

+34.84

49.38

49.20³⁸ C 0.18

49.55

49.70⁵⁵ F 0.15

+59.68 = P.C.

47.98

47.80⁹⁸ C 0.18

48.28

48.30 F 0.02

47.47

48.05

Jewell-Thomas to Grand.
cb. Stakes

West.

East.

0+00 = N.L. Thomas	46.66				47.23		
+10 = P.C.	46.42	46.58	F 0.16		47.22	47.07	C 0.15
+46.85	46.31	46.27	C 0.04		46.55	46.51	C 0.04
+83.70 = End Inlet.	.93	45.96				45.96	
1+20.78 = P.C.	46.45	46.15	C 0.30		46.18	46.15	C 0.03
To Alley	46.45	46.26	C 0.19		46.18	46.26	F 0.08
End. - S.	46.39	46.58	F 0.19		46.11	46.58	F 0.47
End. - N.	47.17	46.85	C 0.32		46.21	46.85	F 0.64
To Alley	46.80	46.53	C 0.27		46.55	46.53	C 0.02
1+48.78 = P.C.	46.80	46.56	C 0.24		46.55	46.56	F 0.01
+64.78	47.33	46.99	C 0.34		46.97	46.99	F 0.02
+99.78	48.29	48.22	C 0.07		48.27	48.20	C 0.07
2+34.78	49.41	49.46	F 0.05		49.39	49.41	F 0.02
+69.56 = S.L.		50.68			50.58	50.61	
Grand = Meet.							

Jewell - Grand to Hornblend.
cb. stakes

		West		East
0+00 = N.L. Grand	51.81	52.00		51.82 52.00
+30	53.08	52. ^{3.08} 89	C 0.19	52.71 52.89 F 0.18
+60	54.05	53. ^{4.05} 78	C 0.27	53.71 53.78 F 0.07
+90	55.03	54. ^{5.03} 67	C 0.36	54.56 54.67 F 0.11
1+21.12 = P.C.	55.67	55. ⁶⁷ 58	C 0.09	55.35 55.58 F 0.23
To Alley	55.67	55.78	F 0.11	55.35 55.78 F 0.43
End - S.	55.87	56. ⁶⁷ 10	F 0.23	55.18 56.10 F 0.92
End - N. - cb. in		56.70		56.76 56.70 C 0.06
To Alley		56.38		56.07 56.38 F 0.31
1+49.12 = P.C.				56.07 56.42 F 0.35
+80				57.02 57.33 F 0.31
2+15				58.01 58.37 F 0.36
+50				59.18 59.40 F 0.22
+60 = P.C.				59.61 59.70 F 0.09
+70.25 = S.L. Hornblend.				59.81 59.83
				+10 59.95

Jewell - Hornblend to Garnet.

		West.		East
Hornblend.	-10	61.12		61.13
0+00 = NL	-	61.30		61.30
+10 = PC.	62.12	^{2.12} 61.70	C 0.42	61.44 61.70 F 0.26
+29.45	62.31	62.69	F 0.29	62.21 62.45 F 0.24
+49.45	64.16	^{4.16} 63.20	C 0.96	62.74 63.03 F 0.29
³⁵ +84.45	64.58	⁵⁸ 64.04	C 0.54	63.67 63.82 F 0.15
1+20.46 = PC	65.19	^{5.19} 64.91	C 0.28	64.67 64.67 C 0.03
To Alley	65.19	65.09	C 0.10	64.67 64.81 F 0.14
S. end.	65.93	65.43	C 0.52	64.76 65.13 F 0.37
N end	66.16	^{6.16} 65.89	C 0.27	65.57 65.58 F 0.01
To Alley	65.60	65.57	C 0.03	65.33 65.26 C 0.07
1+48.46 = PC.	65.60	65.59	C 0.01	65.33 65.27 C 0.06
+75	66.28	66.24	C 0.04	66.25 ^{6.25} 65.86 C 0.39
2+05	67.17	^{7.17} 66.96	C 0.21	66.65 66.53 C 0.12
+35	67.92	^{9.2} 67.69	C 0.23	67.08 67.20 F 0.12
+62.92 = Meet.	68.49	68.35		67.76 67.78
+68.92 = SL Garnet.	68.63			67.84
	-10 68.71			+10 67.86

Curb Stakes - Highland -

		East		West
of Thorn				
0+00 = SL	22.06	22.00		
+30	21.22	^{1.22} 20.92	C 0.30	
+60	20.11	^{20.11} 19.83	C 0.28	
1+90	18.79	⁷⁹ 18.74	C 0.05	
1+20	17.41	⁴¹ 17.65	F 0.24	
+50	16.14	¹⁴ 16.56	F 0.42	
+80	14.97	⁹⁷ 15.47	F 0.50	
2+00	14.04	⁰⁴ 14.65	F 0.61	Meet. ¹³²⁹
+20	13.20	²⁰ 13.53	F 0.33	12.83
+55	11.48	⁴⁸ 11.39	C 0.09	10.58
+90	09.08	⁰⁸ 09.25	F 0.17	07.99
3+20	07.48	⁴⁸ 07.52	F 0.04	06.28
+50	05.51	⁵¹ 05.79	F 0.28	04.82
+80	04.00	⁰⁰ 04.05	F 0.05	03.01
4+00 = End	03.07	⁰⁷ 02.89	C 0.18	01.86
				12.87
				⁸³ 12.62
				⁵⁸ 10.43
				²⁵ 08.25
				²⁴ 06.52
				⁰³ 04.79
				⁰⁴ 03.05
				⁰³ 01.89

Curb Stakes - 35th Ocean View to
 N. End. - Plan - 10950-L
 11-10-54 75. ... w.o. 31769

	West.			East.			
O.V.							
0+00=NL	65.86	66.00		65.86	66.00		
+10	67.17	66.30 ^{2.17}	C0.87	66.90	66.50 ^{.90}	C0.40	
+37.5	69.52	68.65 ^{9.52}	C0.87	69.51	68.95 ^{9.81}	C0.86	
+65	71.64	71.00	C0.64	71.67	71.40 ^{.67}	C0.27	
+85	72.80	72.50 ^{.80}	C0.30	72.90	72.90	G	
1+05	73.42	73.60 ^{.42}	F0.18	73.95	74.00 ^{.95}	F0.05	
+25	73.70	74.10 ^{.70}	F0.40	74.25	74.60 ^{.75}	F0.35	
+45	73.53	74.20 ^{.53}	F0.67	out.			
				1+48=PC.	73.73	74.68 ^{.95}	F0.95
				To Alley	73.73	74.74 ^{.73}	F1.01
				S. end.	74.34	74.88 ^{.34}	F0.54
				N. end	74.95	74.81 ^{.95}	C0.14
				To Alley	73.98	74.64 ^{.98}	F0.66
				1+62 = PC.	73.98	74.58 ^{.98}	F0.60
1+80	73.34	73.95 ^{.34}	F0.61	74.28	74.45 ^{.28}	F0.17	
2+15	73.28	73.70 ^{.28}	F0.42	74.05	74.20 ^{.05}	F0.15	
+50	73.30	73.46 ^{.30}	F0.16	74.01	73.96 ^{.01}	C0.05	
+85	73.00	73.22	F0.22	73.70	73.72	F0.02	
3+20	72.96	72.98	F0.02	73.30	73.48 ^{.30}	F0.18	

West.

East.

3+55	72.60	72.74 ₆₀	F 0.14	73.20	73.24 ₂₅	F 0.04
+80 = PC	71.92	72.57 ₉₂	F 0.65	72.98	73.07 ₉₈	F 0.09
1/2	72.36	72.38	F 0.02	72.95	73.00	F 0.05
End = P.L.	72.20	72.05 ₂₀	C 0.15	73.10	72.90 ₂₀	F 0.20
= Frank lin.						
End.	71.93	72.25 ₉₃	F 0.32	73.39	73.10 ₃₉	C 0.29
1/2	72.38	72.45 ₃₈	F 0.07	73.11	73.00	C 0.11
PC = 0+10	72.63	72.55 ₆₃	C 0.08	73.00	73.05	F 0.05
0+25	72.55	72.61 ₅₅	F 0.06	73.17	73.16	C 0.01
+45	72.74	72.68 ₇₄	C 0.06	73.17	73.29 ₁₇	F 0.12
+65	72.36	72.65 ₃₆	F 0.29	73.16	73.27 ₁₆	F 0.11
1+00	72.20	72.47 ₂₀	F 0.27	72.90	73.11 ₉₀	F 0.21
+35	72.05	72.29 ₀₅	F 0.24	72.81	72.96 ₈₁	F 0.15
+70	71.82	72.10 ₈₂	F 0.28	72.60	72.81	F 0.21
2+05	71.82	71.92	F 0.10	72.43	72.65 ₄₃	F 0.22
+40	71.59	71.74 ₅₉	F 0.15	72.27	72.50 ₂₇	F 0.23
+75	71.60	71.55	C 0.05	72.13	72.35 ₁₃	F 0.22
3+10	71.52	71.57 ₅₂	C 0.15	71.93	72.20 ₉₃	F 0.27
+45	71.13	71.19	F 0.06	71.96	72.05 ₉₆	F 0.09

	West.			East.		
2+80	71.08	71.00	C0.08	71.80	71.90	F0.10
4+15	70.85	70.82	C0.03	71.70	71.75	F0.05
+50	70.68	70.64	C0.04	71.45	71.60	F0.15
+85	70.62	70.45 ⁶²	C0.17	71.36	71.45 ³⁶	F0.09
5+20	70.21	70.27	F0.06	71.15	71.30	F0.15
+55	69.89	70.09 ⁸⁹	F0.20	71.07	71.15	F0.08
+75	69.79	69.96 ⁷⁹	F0.17	70.98	71.04 ⁹⁸	F0.06
+95	69.69	69.80 ⁶⁹	F0.11	70.94	70.87 ⁹⁴	C0.07
6+15	69.65	69.59 ⁶⁵	C0.06	70.75	70.65 ⁷⁵	C0.10
+35	69.48	69.34 ⁴⁸	C0.14	70.54	70.58 ⁵⁴	C0.16
+50=PC.	69.21	69.13 ²¹	C0.08	70.54	70.15 ⁵⁴	C0.39
1/3	69.25	68.92 ²⁵	C0.33	70.77	70.10 ⁷⁷	C0.67
2/3	68.84	68.58 ⁸⁴	C0.26	70.81	70.40 ⁸¹	C0.41
E.C.	68.14	68.00 ¹⁴	C0.14	71.21	71.00	C0.21
Webster						
E.C.	68.61	68.40 ⁶¹	C0.21	71.83	71.50 ⁸³	C0.33
1/3	69.08	68.75 ⁰⁸	C0.33	71.43	70.74 ⁴³	C0.69
2/3	69.23	69.00 ²³	C0.23	70.99	70.22 ⁹⁹	C0.77
PC.=0+10	69.30	69.10 ³⁰	C0.20	70.46	70.67 ⁴⁶	C0.36

Webster to Banjo

	West.				East.		
0+40	69.22	69.40 ₂₂	F0.18	71.07	70.40 ^{1 07}	C0.67	
+70	69.76	69.70	C0.06	71.16	70.70 ^{1 16}	C0.46	
1+00.35 = P.C.	70.09	70.00	C0.09	71.17	71.00	C0.17	
1/2	70.29	70.05 ²⁹	C0.24	71.08	71.21	F0.13	
End at P.L.	70.25	70.00	C0.25	73.44	71.60 ^{3 08 4 4}	C1.84	
End.	70.92	69.85 ^{0 92}	C1.07	74.81	71.57 ^{4 81}	C3.24	
1/2	70.12	69.88 ^{0 12}	C0.29	71.01	71.00	C0.01	
P.C. = 0+13.6	69.61	69.60	C0.01	70.22	70.60 ₂₂	F0.38	
0+45	68.45	68.28 ⁴⁵	C0.17	68.96	69.28 ^{5 96}	F0.32	
+80	66.88	66.81	C0.07	67.77	67.81 ^{7 77}	F0.04	
1+15	65.27	65.34 ₂₇	F0.07	T.P.	66.48	66.34 ^{7 48}	C0.14
+40 = B.C.	64.43	64.29 ⁴³	C0.14	65.55	65.29 ^{5 55}	C0.26	
Mid Point	64.14	63.90	C0.24				
+18.54 = P.R.C.	64.11	63.50	C0.61	+60	64.77	64.45 ^{7 77}	C0.32
+13.91	63.75	63.02 ⁷⁵	C0.73	+80 = B.C.	64.06	63.61 ^{4 06}	C0.45
+13.91 = P.C. on E.	63.05	62.68 ^{3 05}	C0.37	+15.04	63.09	63.05 ^{5 9}	C0.54
+15.04	62.61	62.45 ⁶¹	C0.16	+15.04	62.64	62.67	F0.03
+15.04	62.27	62.36 ₂₇	F0.09	+12.02	62.73	62.46 ^{7 3}	C0.27
+10.04 = E inlet	62.31	62.35		+50.2 to E			
±	62.55	62.40	C0.15				

Curb Grades - Pardee -

Along S.L. of Alley	West		N.L. of 16' Alley	Pave -	East.
w.L. Pardee	67.56	68.40 ^{7.56} F 0.84	25' E. 68.73	8.73 66.95	C 1.78
+10	67.48	68.20 ^{7.48} F 0.72	+10.5 68.52	8.52 66.60	C 1.92
+15 = ±	67.85	67.90 F 0.05	End. E.L. -cb. 67.69	69 67.65	C 0.04
+15	67.95	67.60 ⁹⁵ C 0.35	PC. 4' Rad. 67.64	67.65	F 0.01
+24.5 L.	Top cb. 67.33	67.29	to st. 0+10 = PC. 67.64	67.75 ⁶⁴	F 0.11
+10.5	68.23	67.29 ^{8.23} C 0.94			
N. Side of Alley					
End at w.L.	68.95	68.21 ⁹⁵ C 0.74			
PC - 4' Rad.	68.69	68.08 ⁶⁹ C 0.61			
PC = 0+04.	68.69	68.08 ⁶⁹ C 0.61			
0+06					
+45	69.04	68.94 ^{9.04} C 0.10	68.71	68.64 ⁷¹	C 0.07
+80	69.61	69.67 ⁶¹ F 0.06	69.77	69.53 ⁷⁷	C 0.24
1+15	70.33	70.40 F 0.07	70.42	70.42	G
+50	71.06	71.13 F 0.07	71.05	71.31 ⁰⁵	F 0.26
+85	71.79	71.86 ⁷⁹ F 0.07	71.66	72.20 ⁶⁶	F 0.54
2+20 = PC.	72.56	72.60 F 0.04	72.77	73.10 ⁷⁷	F 0.33
1/2	72.69	72.88 ⁶⁹ F 0.19	73.06	73.40 ⁰⁶	F 0.34
End.	73.18	73.10 F 0.02	73.55	73.70 ⁵⁵	F 0.15

Franklin

Franklin	West.		East.			
End.	73.83	73.80	C 0.03	75.20	⁵²⁰ 74.50	C 0.70
1/2	74.19	¹⁹ 73.98	C 0.21	74.86	⁸⁶ 74.60	C 0.26
P.C. = 0+10	74.25	74.30	F 0.05	74.96	⁹⁶ 74.80	C 0.16
0+45	74.90	⁴⁹⁰ 75.32	F 0.42	75.60	⁸⁰ 75.82	F 0.22
+80	76.14	⁷⁴ 76.34	F 0.20	76.59	⁵⁹ 76.84	F 0.25
1+15	77.01	⁰¹ 77.36	F 0.35	77.50	⁵⁰ 77.86	F 0.36
+50	78.05	⁰⁵ 78.38	F 0.33	78.61	⁶¹ 78.88	F 0.27
+85	79.15	¹⁵ 79.40	F 0.25	79.76	⁷⁶ 79.90	F 0.14
2+20	80.27	²⁷ 80.42	F 0.15	81.05	⁰⁵ 80.92	C 0.13
+55	81.12	¹² 81.44	F 0.32	82.17	¹⁷ 81.94	C 0.23
+80 = T.P.	81.88	⁸⁸ 82.17	F 0.29	82.70	82.67	C 0.03
3+00	82.70	82.75	F 0.05	83.27	83.25	C 0.02
+20	83.25	²⁵ 83.32	F 0.07	83.91	⁹¹ 83.82	C 0.09
+40	83.80	83.86	F 0.06	84.44	⁴⁴ 84.36	C 0.08
+60	84.27	²⁷ 84.36	F 0.09	84.73	⁷³ 84.86	F 0.13
+80	84.82	84.84	F 0.02	85.31	85.34	F 0.03
4+00	85.28	85.28	G	85.65	⁶⁵ 85.74	F 0.13
+20	85.85	⁸⁵ 85.70	C 0.15	86.17	¹⁷ 86.20	F 0.03
+55	86.59	⁵⁹ 86.40	C 0.19	86.55	⁵⁵ 86.90	F 0.35

West.

East.

4+90	87.17	87.10	C 0.07
5+25	87.79	87.80	F 0.01
+60	88.45	88.50 ₄₅	F 0.05
+95 ₃₅	89.12	89.20 ₁₂	F 0.08
6+30	89.78	89.90 ₈₀	F 0.12
+50 = P.C. - T.P.	90.46	90.28 ₄₆	C 0.18
1/3	90.43	90.10 ₄₃	C 0.33
2/3	89.21	89.50 ₂₁	F 0.29
EC. = on Webster.	88.78	88.75 ₃₈	F 0.37

87.24	87.60 ₂₄	F 0.36
88.12	88.30 ₁₂	F 0.18
88.91	89.00 ₉₁	F 0.09
89.65	89.70	F 0.05
90.26	90.40 ₂₆	F 0.14
90.19	90.80 ₁₉	F 0.61
90.88	91.10 ₈₈	F 0.22
91.21	91.50 ₂₁	F 0.29
91.66	92.00 ₆₆	F 0.34

Curb Grades - 53rd - Imperial -
 Plan - 11262-L - 11-18-54 7.0.

157.53 = Cross
 156.03 = Pole

W.O. 32107

West

Santa Margarita

East

End	63.49	^{3.49} 61.35	C 2.14
1/2	62.27	^{2.27} 60.76	C 1.51
P.R.C. = Beg. 30' Rad.	60.77	⁷⁷ 60.18	C 0.59
1/4	59.22	⁴⁴ 59.44	F 0.22
1/2	58.36	³⁶ 58.71	F 0.35
3/4	57.63	⁶³ 58.13	F 0.50
E.C. = 0 to 4.11 _{23.97}	58.32	³² 57.76	C 0.56
0 + 28.08 = Prop. P.C. _{22.68}	57.14	57.13	C 0.01
+ 50.76	56.39	56.59	F 0.20
+ 70.76 = Prop. P.C.	55.98	⁹⁸ 56.71	F 0.23
+ 90.76	55.60	⁶⁰ 55.96	F 0.36
To St.	55.30	³⁰ 55.78	F 0.48
To Alley 1 + 17.09 = 2' Rad.	55.30	³⁰ 55.81	F 0.51
End - S. side 2' Bk.	56.34	³⁴ 55.91	C 0.43
1 + 42.90 = end N.	55.98	⁹⁸ 55.80	C 0.18
P.C. To Alley 2' Rad.	55.14	¹⁴ 55.70	F 0.56
1 + 45.20 = P.C.	55.14	¹⁴ 55.63	F 0.49
+ 70.76	55.66	⁶⁶ 55.50	C 0.16
2 + 00.76	55.30	55.35	F 0.05

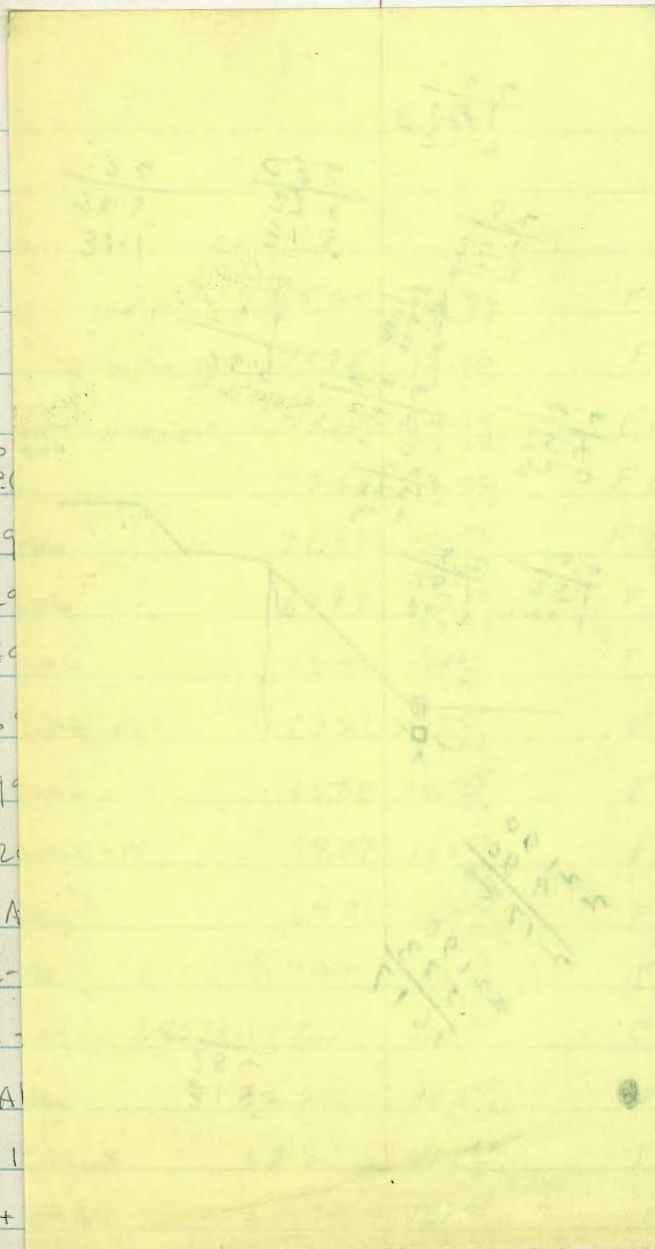
End	58.58	⁵⁸ 58.41	C 0.17
+ 25.85 = P.C.	57.97	⁹⁷ 58.26	F 0.29
1/2	57.77	⁷⁷ 58.17	F 0.40
P.R.C. = Beg. 30' Rad.	58.12	58.08	C 0.04
1/4	57.66	⁶⁶ 58.03	F 0.37
1/2	57.79	⁷⁹ 57.93	F 0.14
3/4	57.55	⁵⁵ 57.80	F 0.25
E.C. = 0 to 3	57.43	⁴³ 57.57	F 0.14
0 + 30.76	56.61	⁶¹ 56.76	F 0.15
+ 50.76	56.29	²⁹ 56.29	F 0.01
+ 70.76 = Prop. P.C.	55.94	55.91	C 0.03
+ 90.76	55.64	55.66	F 0.02
1 + 10.76	55.42	⁴² 55.51	F 0.09
+ 40.76	55.17	¹⁷ 55.35	F 0.18
+ 70.76	55.31	³¹ 55.20	C 0.11
2 + 00.76	55.04	55.05	F 0.01
2 + 32.31 _{23.57}	54.64	⁶⁴ 54.90	F 0.26
+ 55.88	54.72	⁷² 54.78	F 0.06
+ 65.76 = P.C.	54.84	54.73	55.07

2+32.31 C 43	55.43	55.20 ⁴³	C 0.23				
+38.74 = cb.PC.	55.36	55.17 ³⁶	C 0.19	End inlet	54.80	54.74	
end inlet	55.13	55.06		1/2	54.79	54.75	C 0.04
1/3	55.60	55.09 ⁶⁰	C 0.81	end.	54.60	54.80 ⁶⁰	F 0.20
2/3	56.03	55.14 ⁶⁰³	C 0.89				
end.	56.27	55.18 ⁶²⁷	C 1.09				

Curb Stakes - San Jacinto Dr.

				west.		East.
Meet.	86.01	86.07	86.12			
1/4		86.24	86.45 ₂	F 0.21	Meet. 91.68	91.77
1/2		86.48	86.74 ₃	F 0.31	B.C. 91.66	91.69 ₂₆ F 0.03
3/4		86.55	87.03 ₃	F 0.48	E.C. 91.54	91.59 ₃₇ F 0.05
E.C.		86.93	87.29 ₉	F 0.36	1 90.38	91.15 ₀ F 0.59
P.C.		87.94	87.90 ₉	C 0.04	2 90.23	90.55 ₂ F 0.32
1/4		88.10	88.17 ₁₀	F 0.07	3 89.84	89.80 C 0.04
1/2		87.75	88.28 ₇	F 0.53	4 = P.C. 89.50	89.00 ₅₀ C 0.50
3/4		87.91	88.24 ₇	F 0.33	+20.45 1/2 88.53	87.90 ₈ C 0.63
P.R.C.		88.39	88.88	C 0.39	P.R.C. 87.32	86.80 ₇ C 0.52
1/2		87.47	86.90 ₆	C 0.57	1 85.85	85.50 ₈ C 0.35
P.R.C.		86.28	85.80 ₆	C 0.48	2 84.32	84.20 ₃ C 0.12
1		84.39	83.94 ₄	C 0.45	3 82.98	82.90 ₉ C 0.08
2		82.15	82.08 ₂	C 0.07	4 = Prop P.C. 81.85	81.49 ₈ C 0.36
3	30' Rad.	79.87	79.98 ₈	F 0.11	5 80.87	79.82 ₂₀ C 1.05
4 = P.C.		77.54	77.25 ₅	C 0.29	6 = ch. P.C. 79.41	78.02 ₉ C 1.39
1		77.10	76.29 ₇	C 0.81	1 78.98	77.20 ₈ C 1.78
2		76.62	75.55 ₆	C 1.07	2 78.60	76.54 ₈ C 2.06
3		75.26	75.12 ₂	C 0.14	3 = E.C. 78.23	76.56 ₈ C 1.67
4		74.94	74.94	G	+6.85 = End. 78.65	76.75 ₈ C 1.90

west.



S = R.C.	74.76	74.76	Q ₁	S	
Santa Margarita					
BC.	73.32	73.98 ₃₂	F 0.66	End	1.14
1	73.17	74.00 ₁₇	F 0.83	1	1.35
2	72.54	73.78 ₂₅₄	F 1.24	2	0.97
3 T.P.	71.73	73.27 ₁₇₃	F 1.54	3 = P.C.	0.46
4	70.71	72.44 ₇₁	F 1.73	0 + 09	0.21
S = P.C.	70.03	71.56 ₀₀₃	F 1.53	+ 20	0.37
0 + 23.21	68.35	69.30 ₈₃₅	F 0.95	+ 40	0.21
+ 43.21	67.15	67.63 ₇₁₅	F 0.48	+ 60	0.04
+ 63.21 E.V.C.	65.55	66.25 ₅₅₅	F 0.70	+ 90	0.45
+ 93.21	64.27	64.53 ₂₇	F 0.26	1 + 20	0.23
1 + 15.66 = P.C.	63.20	63.35	F 0.05	To A	0.08
To Alley	63.20	63.10	C 0.10	End -	0.07
End - S.	65.22	63.42 ₅₂₂ ob face	C 1.80	End -	1.21
End - N.	62.37	62.27 _{NO} ob face	C 0.10	To A	0.73
To Alley	61.55	61.95 ₅₅	F 0.40	P.C. = 1	0.42
P.C. = 1 + 43.69	61.55	161.64 ₅₅	F 0.09	1 +	0.54
1 + 68.83	60.33	160.28 ₃₃	C 0.05	+ 94.68	59.91
				160.36	991
					F 0.45

26.1
2.2
2.9

22.2
22.6
5.5

22.0
25.4
6.6

20.1
25.1
5.0

22.2
26.1
6.1

24.6
22.0
25.4
26.6

30.3
28.1
5.2

31.5
22.9
8.6

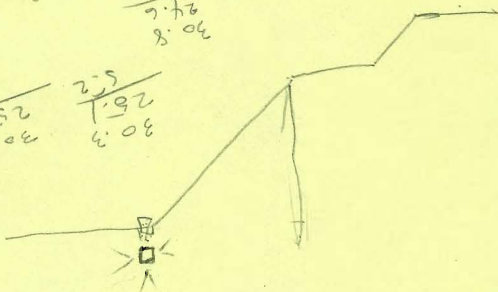
22.0
25.9
3.9

31.1
28.5
2.6

22190
217
4

22190
573
1617

31.5
28.4
3.1



west.				East.				
5 = P.C.	74.76	74.76	Q _u	5				
Santa Margarita					deflected L.S.			
B.C.	73.32	73.98 ₃₂	F 0.66	End	34° 10'	75.20	76.34 ₃₂	F 1.14
1	73.17	74.00 ₁₇	F 0.83	1	22° 46' 40"	73.95	75.30 ₃₉₅	F 1.35
2	72.54	73.78 ₂₅₄	F 1.24	2	11° 23' 20"	73.22 ^{c=18.66}	74.19 ₇₃₂₂	F 0.97
3 T.P.	71.73	73.27 ₁₇₃	F 1.54	3 = P.C.	= 0 + 00	72.60	73.06 ₂₆₀	F 0.46
4	70.71	72.44 ₆₇₁	F 1.73	0 + 09.06		71.99	172.20 ₁₉₉	F 0.21
5 = P.C.	70.03	71.56 ₀₀₃	F 1.53	+ 29.06		69.93	170.30 ₆₉₉₃	F 0.37
0 + 23.21	68.35	69.30 ₈₃₅	F 0.95	+ 49.06		68.42	168.63 ₈₄₂	F 0.21
+ 43.21	67.15	67.63 ₇₁₅	F 0.48	+ 69.06 E.V.C.		67.21	167.25 ₇₂₁	F 0.04
+ 63.21 E.V.C.	65.55	66.25 ₅₅₅	F 0.70	+ 99.06		65.08	165.53 ₆₅	F 0.45
+ 93.21 ₂₂₄₈	64.27	64.53 ₂₇	F 0.26	1 + 20.68 = P.C.		64.07	164.30 ₀₇	F 0.23
1 + 15.66 = P.C.	63.20	63.25	F 0.05	To Alley		64.07	164.15 ₀₇	F 0.08
To Alley	63.20	63.10	C 0.10	End - S	64.40 ^{5/10} ob face		164.47 ₄₅₃	F 0.07
End - S.	65.22 ^{5/10} ob face	63.42 ₅₂₂	C 1.80	End - N	64.53 No ob face		163.32 ₄₅₃	C - 1.21
End - N.	62.37 No ob face	62.27	C 0.10	To Alley		62.27	163.20 ₂₂₇	F 0.73
To Alley	61.55	61.95 ₅₅	F 0.40	P.C. = 1 + 48.68		62.27	162.69 ₂₂₇	F 0.42
P.C. = 1 + 43.69 ₂₅₁₄	61.55	161.64 ₃₃	F 0.09	1 + 74.68		60.74	161.28 ₀₇₄	F 0.54
1 + 68.83	60.33	160.28 ₃₃	C 0.05	+ 94.68		59.91	160.36 ₉₉₁	F 0.45

1+88.83 ₂₅	59.33	159 ³⁶	F 0.03	2+19.68 ₂₅	58.86	159 ³¹ ₈₈₆	F 0.45
2+13.83 ₇	58.27	158 ³¹	F 0.04	+44.68	57.92	158 ²⁶ ₇₉₂	F 0.34
+28.83	57.46	157 ²⁶ ₇₄₆	C 0.20	+71.68 = P.C.	56.29	157 ¹² ₆₂₉	F 0.83
+67.33 = P.C.	56.49	156 ⁰⁶ ₆₀₆	C 0.43	1/4	55.98	156 ⁶³ ₅₉₈	F 0.65
1/4	56.22	155 ⁷⁰ ₆₂₂	C 0.52	1/2	55.94	156 ²¹ ₅₉₄	F 0.27
1/2	55.85	155 ⁵⁰	C 0.15	3/4	56.42	155 ⁹⁷ ₆₄₂	C 0.45
3/4	55.83	155 ⁴⁴ ₈₃	C 0.39	P.C. Imperial	56.36	155 ⁸⁸ ₆₃₆	C 0.48
P.P.C. Imperial	155.51	152 ⁴²					

curb stakes - Santa Margarita

South

North

PC. 30' Rad.

PC. 30' Rad.

8 = Brk	74.68	74.50 ⁶⁸	C0.18	8 = Brk	73.47	73.75 ⁹⁷	F0.28
7	74.31	74.19 ³¹	C0.12	7	73.10	73.40 ¹⁰	F0.30
6	74.09	73.89 ⁴⁰⁹	C0.20	6	72.85	73.06 ²⁸⁵	F0.21
5	73.91	73.58 ³⁹¹	C0.33	5	72.50	72.71 ³⁰	F0.21
4	74.01	73.27 ⁴⁰¹	C0.74	4	72.12	72.36 ¹²	F0.24
3	73.22	72.97 ³²²	C0.25	3	71.53	72.02 ⁵³	F0.49
2	72.71	72.66 ⁷¹	C0.05	2	71.35	71.67 ³⁵	F0.32
1	72.19	72.36 ¹⁹	F0.17	1	70.39	71.33	F0.94
PC. ^{= 0+00 to w.} T.P.	71.84	72.05 ⁸⁴	F0.21	PC.	70.41	70.98 ⁴¹	F0.57
intet	71.79	71.85			70.87	70.85	
0+29.50	71.66	72.00 ⁶⁶	F0.34		70.93	70.98 ⁹³	F0.05
+49.50	72.20	72.79 ²⁰	F0.59		71.51	71.42 ⁵¹	C0.09
+69.50	73.35	74.00 ³⁵	F0.65		72.10	72.35 ¹⁰	F0.25
+99.50	75.00	76.30 ⁰⁰	F1.30		74.62	74.86 ⁶²	F0.24
1 ^{28.42} +28.42 = PC. _{+60 +29.02}	77.33	78.52 ³³	F1.19	2' Rad. 1+23.22 =	76.25	76.83 ²⁵	F0.58
1	78.26	79.33 ²⁶	F1.07	To Alley	76.25	77.04 ²⁵	F0.79
2 T.P.	79.36	80.15 ³⁶	F0.79	End - E.	75.05	77.20 ⁰⁵	F2.15
3 = P.L.	80.03	80.78 ⁰³	F0.75	End - w.	76.16	78.95 ¹⁶	F2.79

North

4	80.18	^{0.18} 81.08 0.18	F0.90	To Alley	77.04	78.79 7.04	F1.75
5 = E.C.	80.02	80.91 0.02	F0.89	PC = 1 + 47.22 28.85	77.04	78.85 7.04	F1.81
0 + 29.46	79.48	80.22 9.48	F0.74	1 + 76.07 = Meet.	80.58	80.68	
+ 58.92 = Meet.	79.42	79.52					

Stake Drain - 53rd Imperial to Maranja

28

Plan - 11266-L - 11-22-54 7.0 r

Grades lowered because of water pipe at Imperial

0+00 = Meet		^{55.00} 55.00	46.20	C 8.80	5+80	37.26	^{7.26} 34.04	C-9.22
+10	45.00	54.90	45.50	C-9.10	6+15	36.08	^{1.08} 32.75	C-9.33
+20	44.40	54.52	45.10	C 9.42	+50	34.82	^{4.82} 31.47	C-9.35
+56.76 = PC	43.93	53.57	44.53	C 9.04	+89.43 = B.C.	31.12	^{4.12} 30.02	C 4.10
Mid. pt. +70.99	43.75	53.20	44.30	C 8.90	+97.33 = M.	31.17	^{3.17} 29.73	C 4.44
0+85.22 = E.C.	43.58	53.05	44.08	C 8.97	7+05.23 = E.C.	34.23	^{3.23} 29.44	C 4.79
1+20	43.13	52.72	43.53	C 9.19	7+28.40	34.09	^{3.09} 28.57	C 5.52
+55	42.67	52.30	42.97	C 9.33	7+51.56 ^{10'} Inst	33.19	^{3.19} 27.70	C 5.99
+90	42.22	52.00	42.42	C 9.58	10' West	33.22	^{3.22} 27.70	C 5.52
2+25	41.77	51.54	41.87	C 9.67				
+60		50.63	41.32	C 9.31				
+95	49.63		40.77	C 8.86				
3+30	48.64		40.22	C 8.42				
+65	47.33		39.67	C 7.66				
4+00	46.94		39.12	C 6.82				
+35	44.52		38.57	C 5.95				
+73.16 = C.D.	42.32		37.97	C 4.35				
5+10 TP	40.33		36.61	C-3.72				
+45	38.82		35.32	C-3.50				

Stake Obs 36th St Ocean View to Imperial

	3' BK L ₂ W ₁ cb face 4 1/4" @ Prop	80 ³¹ F1 ⁴⁴	81 ⁷⁵	Rt. Fly 3' BK cb face		L ₂ W ₁ 3' BK cb face		Rt. Fly 3' BK cb face	
1460 Alley Nly Prop	0 ⁰⁰ cb face				3+70	1 ²⁸ C0 ¹²	91 ¹⁶	92 ¹¹	2 ⁵⁸ C0 ¹⁷
1450 Alley Sly Prop	0 ⁰⁰ cb face	4 1/4" @ Prop 79 ¹⁴ F1 ⁸⁷	81 ⁰¹	81 ⁸⁹	3+50	90 ²² C0 ¹⁸	90 ⁵⁴	91 ⁷⁹	1 ²² C0 ¹³
1446 4 1/4" Alley Nad	F0 ³² C0 ¹²	80 ⁵⁶ 80 ⁸⁸ Alley 80 ⁴⁴ EVC			3+30 EVC	90 ⁰⁸ C0 ³³	89 ⁷⁵	91 ⁰⁰	1 ⁰⁹ C0 ⁰⁹
1430		91 ¹⁴ C0 ¹²	79 ⁰²	80 ⁰¹	3+00	8 ⁶⁴ C0 ²⁰	88 ⁴⁴	89 ⁶⁸	9 ⁵⁴ C0 ¹⁵
1410		7 ²² C0 ⁰⁹	77 ¹³	77 ⁸⁵	2+70	7 ²¹ C0 ⁰⁹	87 ¹²	88 ³⁷	8 ⁶² C0 ²⁵
0+90		5 ⁰³ C0 ¹⁰	74 ²³	75 ¹¹	2+45	5 ⁹⁰ C0 ⁰⁹	85 ⁸¹	87 ⁰⁶	7 ²² C0 ¹⁶
0+70		2 ¹⁵ F0 ⁰⁵	72 ⁵⁰	72 ⁶⁹	2+10 EVC	4 ⁶⁴ C0 ¹⁴	84 ⁵⁰	85 ²⁵	5 ⁶⁹ F0 ⁰⁶
0+50 EVC		6 ⁸⁴ C0 ⁰⁴	69 ⁸⁰	69 ⁶⁹	1490	3 ⁵⁸ C0 ⁰⁸	83 ⁵⁰	84 ⁸¹	4 ⁶⁷ F0 ¹⁴
0+25		6 ⁵⁸ F0 ³²	66 ³⁰	65 ⁷⁵	1470		82 ²⁷	83 ⁴⁹	3 ⁷³ C0 ²⁴
0+00 Nly Ocean View	meat		62 ⁸¹	61 ⁸¹	1464 4 1/4" Alley Nad	F0 ²⁸ 81 ⁰⁵ F0 ⁵⁷	81 ³³ EVC	81 ⁶² Alley	

BM

SE cor
64²⁴ top Fire Nad
36th Ocean View

36th St

	Lt. Wly 3' BK to 6 face		Rt. Fly 3' BK to 6 face			Lt. Wly 3' BK to 6 face		Rt. Fly 3' BK to 6 face	
5729	370 C058	92 ¹³	94 ³⁴	438 C004	0440	509 F002	95 ¹¹	94 ⁵⁹	9427 F032
5709 ⁰⁵ BVC	372 C080	92 ⁹²	94 ¹⁸	420 C005	0410 EOC			94 ⁴⁰	9417 F023
4774 ²³	370 C114	92 ⁵⁶	93 ²¹	418 C037	Nly Gilmore 0400	452 F018	94 ²⁰	94 ²⁵	9421 F004
4749 ⁵³ Nwly E.C. Return	336 C106	92 ³⁰			20' Rod NWly Fly end Return			94 ⁵⁰	9410 C0.10
Nly Franklin 4739 ⁵³ EVC	223 C073	92 ²⁰	93 ⁴⁵	391 C076	6+2225 E Gilmore	432 C004	94 ²⁸	93 ⁵² gutter	93 ⁶⁵ rod return
20' Rod end return NWly	994 F186	91 ⁸⁰			20' Rod NWly end return NWly			412 93 ⁵⁰	94.12 C0.62
4714 ⁵³ E Franklin 4710	91 ³¹ rod. EVC	91 ²⁰ gutter	93 ¹⁵	339 C024	Sly Gilmore 5799 ⁰⁵	420 C015	93 ⁸⁵	417 93 ²⁵	9417 C0.42
20' Rod end return SWly	8968 F154	91 ²²			BC 5789 ⁰⁵	388 C014	93 ⁷⁴	94 ⁰⁰	404 C004
Sly Franklin 3789 ⁵³	164 C014	91 ⁵⁰	92 ⁸⁸	298 C010	5769	377 C024	93 ⁵³	94 ²⁵	487 C062
3779 ⁵³ BOC	158 C018	91 ⁴⁰			5749	368 C035	93 ³³	94 ³⁷	459 C022

36 th St	Lt. Wly		At. Ely		Lt. Wly		At. Ely	31
2782	681 FO21	9702	9602	9614 C-0.09	20' Rd NWly 1/3	9724 C-0.69	9555	
2762	645 FO56	9701	9604	9584 FO.20	B.C. Webster 1772 1/2 E Webster	9725 C0.25	97.00 9529 utter	9518 F0.07
2742	617 FO80	9627	9527	9590 F0.07	Ec on Webster 1/3	9708 C0.08	9700	
2722	608 FO80	9688	9589	9560 FO.29	4472 1/2 1/3	9625 C0.07	9658	9538 F0.02
2702	612 FO63	9675	9577	9542 FO.35	4432 1/2 BC 1/2	665 C0.10	9655	
1782	626 FO32	9658	9560	9523 FO.27	4412	683 C0.21	9662	9552 F0.13
1762 B.V.C.	648 C011	9637	9540	9521 FO.19	3782	665 FO.07	9672	9565 F0.54
1730	594 FO10	9604	9522	9508 FO.11	3752	652 FO.29	9681	9577 F0.21
1700	564 FO.09	9573	9492	9491 FO.08	3722 E.V.C.	665 FO.25	9620	9520 F0.35
0770	547 C005	9542	9479	9468 FO.11	3702	680 FO.18	9628	9528 F0.33

36th St

Lt. Wly

Rt. Ely

Stake Curbs - Gas Station
Euclid and Imperial
Plan 11892-L
11-26-54
Hatch

32

BM

93²⁵ SE 7425117
Imperial
36th15' Rad Swly
end return90.97
F0.43 91⁷⁰End Cb. on Euclid 64 54 164.19^{4 54} C 0.35
+26.40 69 12 166.83^{7 12} C 0.29Sly Durant
6409⁰²91.07
F0.53 91⁶⁰Cb. B.C. 70 65 170.50^{0 65} C 0.15
P.L. B.C. 71 01 170.83^{1 01} C 0.185495⁴² B.S. Lt.91.60
F0.36 91⁹⁶1/3 from Cb. B.C. 72 42 172.45^{2 42} F 0.03
2/3 73 74 174.00^{3 74} F 0.26SEly 20' Rad
end return Rt93²⁰ MEETP.L. E.C. 74 29 174.50^{2 29} F 0.21
Cb. E.C. 74 12 174.60^{4 12} F 0.48Sly Imperial
5479¹⁹92.60
F0.20 92⁸⁰ 93²²93.68
C-0.09+15 Brk 73 78 174.75^{3 78} F 0.97
+35 edge drive 73 18 174.37^{3 18} F 1.195469¹⁹ B.C. M.93.18
F0.07 93²⁵ 93²⁴94.03
C 0.2958.09 72 57 173.51^{2 57} F 0.94
4' Rad. B.C. Street 72 04 172.65^{0 4} F 0.615435⁸²95.05
C-0.47 94⁵⁸ 94⁴²95.20
C 0.78" E.C. 72 64 172.58^{0 4} F 0.54
End Ret. 72 06 172.68^{0 6} F 0.625412⁴⁶ F.C. 36²⁴95.83
C 0.33 95⁵⁰Nly Weas. en.
5402⁴⁶ 2/396.07
C 0.07 96²⁰ 95⁴⁰95.24
C 0.14

Stake-Curbs Gas Station

33

Euclid and Imperial

Plan 11892-L 11-26-54

(continued) Hatch

Prop. inters. at

alley n.w. cor. 71.24 171.93₂₄ F 0.69

20' n.th. 70.63 171.00₀₆₃ F 0.37

E alley 68.63 170.45₈₆₃ F 1.82

east side alley 69.15 170.70₉₁₅ F 1.55

end cb. (east) 69.88 171.19₉₈₈ F 1.31

4' Rad. (alley) 70.00 171.09 F 1.09

(street) 70.00 170.85 F 0.85

11-30-54
Curb Stakes - Webster St.
36th To Pardee Hatch

36th to 35th St.

South			North		
s.w. ret. Webster +36 th					
0+10=B.C.	97.00		v.w. 36 th Webster	97.25	97.00
+20	97.32	97.25 ³²	0+10=B.C.	97.49	97.32 ⁴⁹
+40	97.73	97.63 ⁷³	+20	98.04	97.83 ⁸⁰⁴
+60	97.64	97.76 ⁶⁴	+40	98.31	98.09 ³¹
+80	97.85	97.70 ⁸⁵	+60	98.05	98.09
1+00	97.52	97.39 ⁵²	+80	97.88	97.84
+13=P.C. st.	97.15	97.04 ¹⁵	1+00	97.40	97.32 ⁴⁰
east P.C. alley	97.15	97.03 ¹⁵	+20	96.71	96.55 ⁷¹
s.e. end ret.	97.47	97.20 ⁴⁷	+40	95.14	95.20 ¹⁴
s.w. end ret.	96.59	96.68 ⁵⁹	1+71.66	93.96	93.85 ⁹⁶
west P.C. alley	96.42	96.51 ⁴²	2+03.33	92.32	92.50 ³²
+32=P.C. st.	96.42	96.39 ⁴²	+35	90.09	91.04 ⁰⁹
+40	96.06	96.05 ⁰⁶	+65 T.P.	89.24	90.10 ²⁴
+71.33	94.94	94.70 ⁹⁴	+85	88.32	88.93 ³²
2+02.67	93.42	93.35 ⁴²	3+05	87.27	87.61 ²⁷
+33.10 B.C.	91.88	92.00 ⁸⁸	+25	85.83	86.13 ⁸³
s.e. Pardee & Webster			+45	83.60	83.75 ⁶⁰
			+75	81.78	81.37 ⁷⁸
			4+05 T.P.	79.18	79.00 ¹⁸
			+35		

Curb Stakes ~ Webster St.
Pardee to 35th St.

35th To Francis

South

North

s.w. cor. Pardee + Webster	88.75	F 0.37	4+65	77.10	⁷¹⁰ 76.63	C 0.47
0+10=B.C.			+95	74.35	³⁵ 74.19	C 0.16
+45	86.13	C 0.13	N.E. Webster + 35 th			
+80	83.35	C 0.12	5+29=B.C.	71.83	71.50	C 0.33
1+13=PC.st	80.86	C 0.23	N.W. Webster			
alley P.C. TP	80.86	C 0.35	+ 35			
end ret s.e.	^{2.65} 82.65	C 1.97	0+10=EC + 10	68.61	68.40	C 0.21
end ret s.w.	^{80.50} 80.35	C 1.05	0+20	68.15	⁸¹⁵ 67.85	C 0.30
alley P.C.	79.00	F 0.33	+55	65.37	⁵¹ 65.33	C 0.18
1+32=PC.	79.00	F 0.13	+90 TP	63.09	^{3 09} 62.80	C 0.29
+65	76.59	C 0.07	1+25	60.44	⁴⁴ 60.27	C 0.17
2+00	^{73.58} 73.55	F 0.21	+60	58.20	^{8 20} 57.74	C 0.46
+35.06=B.C.	71.00		+95	53.45	⁴⁵ 55.21	C 0.24
s.e. 35 th st. + Webster			2+30	52.85	⁸⁵ 52.68	C 0.17
s.w. 35 th + Webster			+65	50.18	50.15	C 0.03
0+10=P.C.	68.14	C 0.14	+95	48.19	⁸¹⁹ 47.90	C 0.29
+40	⁶¹³ 66.13	C 0.28	3+25	45.21	²¹ 45.65	F 0.44
+70	⁸⁰ 63.86	C 0.17				
1+00	⁵⁷ 61.57	C 0.04				
+28=PC.st. at alley	⁸⁵ 59.85	C 0.34				

Curb Stakes ~ Webster
 (Continued)
 35TH To Francis
 South

1+30 = P.C. alley	59.85	59.41 ³⁵	C0.44
S.E. end ret.	61.27	59.58 ^{1.27}	C1.69
S.W. end ret.	59.03	58.50 ^{9.03}	C0.53
1+45 = P.C. alley	58.68	58.33 ⁶⁸	C0.35
1+47 P.C. st.	58.68	58.15 ⁶⁸	C0.53
1+75	56.36	56.13 ³⁶	C0.23
2+05 ^{IP}	54.20	53.97 ^{4.20}	C0.23
+35	51.69	51.81 ⁶⁹	F0.12
+65 = P.C.	49.25	49.65 ²⁵	F0.40
S.E. Webster + Francis Mid Point	48.67	48.82 ²⁵	F0.15
S.W. Webster + Francis End of Ob.	46.36	46.10	C0.26

Alley Staking
 Froude to Ebers
 Nail in Pole 0+52
 126.66 Lt.

3/4 Prop pipe 14.
 3700
 95.36

Alley Blk. 22
 Plan 11306-L Rt.

Ocean Beach
 12-10-54
 Hatch

0+00 = West Cb. line

Station	Left	Right	Notes	Left	Right	Notes
0+10	31.96	132.02	F0.06	133.00	132.04	C0.96
+20	31.18	131.18	Grade	133.00	131.07	C1.93
+30	29.49	130.02	F0.53	32.81	129.84	C2.97
+40	28.11	128.55	F0.44	32.74	128.34	C4.40
+70	23.19	123.63	F0.44	21.63	123.43	F1.80
+95	21.53	119.54	C1.99	18.58	119.34	F0.76
1+20	19.07	115.45	C3.62	T.P.	115.78	C0.53
+45	16.36	111.36	C5.00	4' Bl.	12.27	C1.11
+70	07.65	107.27	C0.38	05.48	107.07	F1.59
+80	05.93	105.73	C0.20	04.36	105.53	F1.17
+90	04.27	104.37	F0.10	03.70	104.17	F0.47
2+00	02.71	103.19	F0.48	03.02	102.99	C0.03
+10	01.83	102.20	F0.37	02.42	102.00	C0.42
+46.67	98.22	98.90	F0.68	3' Bl.	101.17	C2.47
+83.33	96.38	95.60	C0.78	96.87	95.40	C1.47
3+20	95.02	92.30	C2.72	93.41	92.10	C1.31
+40	91.70	90.55	C1.15	90.19	90.35	F0.16
+60	90.84	88.91	C1.93	88.28	88.71	F0.43

Lt.

Rt.

3480	2' cross	88.23	87.38 ⁸²³	C 0.85	86.74	87.18 ⁶⁷⁴	F 0.74
4~	2' PK.	86.72	85.96 ⁶⁷²	C 0.76	85.41	85.76 ⁴¹	F 0.35
+36.67	3' BL	85.27	83.45 ⁵²⁷	C 1.82	82.76	83.25 ²⁷⁶	F 0.49
+73.33		83.15	80.95 ³¹⁵	C 2.20	1.86 80.87	80.75 ⁸⁷	C 0.12
5710	Nail 0.60 BK	79.14	78.44 ⁹¹⁴	C 0.70	78.04	78.24 ⁸	F 0.20
+30	Nail 0.65	78.01	76.76 ⁸⁰¹	C 1.25	76.21	76.56 ⁰⁴	F 0.35
+50	2' cross	75.57	74.48 ⁵⁵⁷	C 1.09	74.78	74.28 ²⁸	C 0.50
+70	PK 0.40 BK	72.81	71.60 ²⁸¹	C 1.21	72.97	71.40 ²⁹⁷	C 1.57
+90		70.12	68.16 ⁰¹²	C 1.96	70.83	67.96 ⁷⁰⁸³	C 2.87
5199.20		66.92	66.59		66.15	66.08	
		Top			Top		
		Cb			Cb.		

Stake Drain - Juniper + 39th
 Plan - 1183-L - 12-29-54 - 70.

B.M.

39

stakes - 10' N.

I.E.

N.E. Ret.

0+00 = Φ Box

33.22 ^{33.22} 26.00 C 7.22

+ 29.66

32.71 ^{32.71} 25.00 C 7.71

+ 59.33

33.49 ^{33.49} 24.00 C 9.49

+ 89 = Φ Box

28.04 ^{28.04} 23.00 C 5.04

= w. edge of Box
 = 0+00

+ 33.25

23.57 ^{23.57} 18.08 C 5.49

+ 66.49 = B.C.

20.08 ^{20.08} 13.16 C 6.92

+ 82.24

18.48 ^{8.48} 10.77 C 7.71

+ 97.99

16.07 ^{16.07} 8.39 C 7.68

1 + 13.74 = E.C.

13.66 ^{13.66} 06.01 C 7.65

+ 23.74

12.28 ^{12.28} 04.05 C 8.23

+ 33.74

7.39 ^{7.39} 01.62 C 5.77

+ 43.74

3.761 ^{03.76} 98.73 C 5.03

+ 66.24

95.26 ^{5.26} 91.19 C 4.07

+ 88.74

86.40 ^{6.40} 83.65 C 2.75

2 + 18.79 = B.C.

77.24 ^{7.24} 73.62 C 3.62

+ 30.57 = E.C. ^{End pipe}

75.65 ^{75.65} 69.66 C 5.99

End of Headwall

74.73 ^{74.73} 69.00 C 5.73

Stake Sewer - West Coast Tract.
 Plan - 11885-L - 1-14-55 7.0.
 W.O. 62394

B.M. 170.73 = Nail in Pole

0+00 = MH. 1	69.20	160.45 ^{9.20}	C 8.75
+28.5	69.60	60.57 ^{9.60}	C 9.03
+57	69.66	60.68 ^{9.66}	C 8.98
+85.5	70.45	60.80 ^{70.45}	C 9.65
1+14 = MH. 2	71.20	60.91 ^{71.20}	C 10.29
+40	71.00	61.01 ^{71.00}	C 9.99
+75	69.90	61.15 ^{9.90}	C 8.75
2+10	66.44	61.29 ^{6.44}	C 5.15
+45	64.50	61.43 ^{4.50}	C 3.07
+80	64.28	61.57 ^{4.28}	C 2.71
3+15	64.83	61.71 ^{4.83}	C 3.12
+50	65.74	61.85 ^{5.74}	C 3.89
+80 = End.	65.53	61.97 ^{5.53}	C 3.56

Stake Sewer - Spruce St. - Plan - 5545-B
w.o. 62407 - 1-17-55 7.0.

B.M. = Sw. 7' ct. Spruce St. 10597

To E.			
0+75	09.22	01.90	C 7.32
+51	08.46	01.42	C 7.04
+25	07.29	00.90	C 6.39
0+00 = M.H. 1	06.00	106.40	C 5.60
+35	05.85	00.58	C 5.27
+70	06.06	00.75	C 5.31
1+05	05.29	00.93	C 4.36
+40	05.27	01.10	C 4.17
+74	05.00	01.27	C 3.73

Stake Drain - Dass Manor
 Plan - 11567-L 1-25-55 7.0.
 W.O. 23955

Inlet + 12" RC pipe

⊕ inlet - I.E.	53.17	53.17 47.14	C 6.03
Top	53.17	53.17 49.50	C 3.67
+24.6	53.10	53.10 46.92	C 6.18
+49.2	53.00	53.00 46.69	C 6.31
+73.8 = end Meet Dip outlet	52.77	52.77 46.46	C 6.31

3+45

53.03

^{3.03}
51.47

C 1.56

+80 = End.

53.06

^{3.06}
51.65

C 1.41

Beq. Ditch to S.

0+00 = edge of Box

		49.50	
+35	51.68	^{1.68} 49.72	C 1.96
+70	51.40	^{1.40} 49.94	C 1.46
+90	51.31	^{1.31} 50.06	C 1.25
1+10 = Ang.	51.30	^{1.30} 50.18	C 1.12
+43.3	51.41	^{1.41} 50.38	C 1.03
+76.6	51.64	^{1.64} 50.59	C 1.05
2+10 = Ang.	51.88	^{1.88} 50.80	C 1.08
+43.3	52.11	^{2.11} 50.97	C 1.14
+76.6	52.45	^{2.45} 51.14	C 1.31
3+10 = Ang.	52.76	^{2.76} 51.30	C 1.46

Stake 6" Sewer for Boys Club.

W.O. 21198 - 1-31-55 7.0

See Plan - D-40

M.H. 11.60' from 0+00 I.E. = 347.10 = B.M.

M.H. 11585 To S. I.E. 350.14

0+00 = Conn. to Exist 8" 47.45

Beq. New Line 53.15 47.60 C 5.55

0+35 57.52 50.84 C 6.68

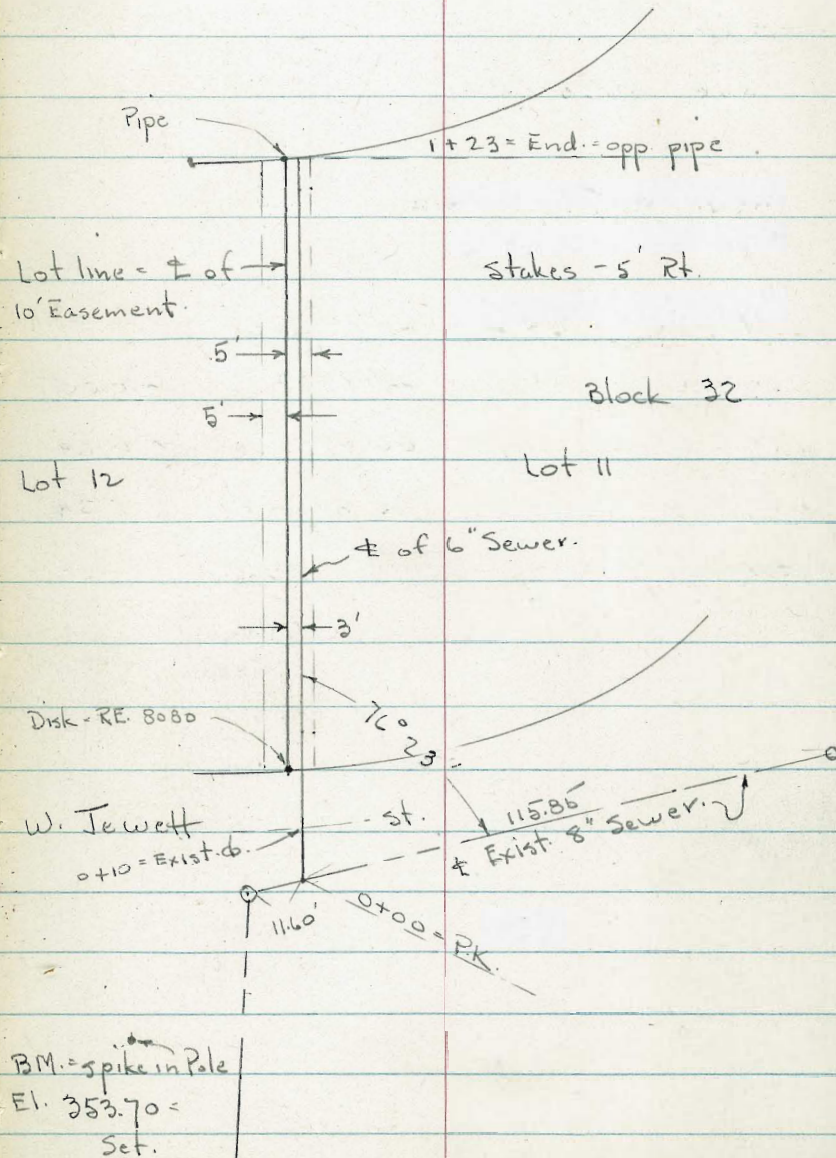
+70 60.50 54.08 C 6.42

1+00 61.01 56.86 C 4.15

+23 = End. 62.70 59.00 C 3.70

Boys Club.

43



Stake 80' sidewalk on
Marine View Ave.
East of 41st St

W.O. 20007 2-2-55 Hatch
6731-L
1774
Book 1716-36

0+00 = 3/4" pipe at alley

63.34 63.86 F0.52

0+31.4 64.20 65.17 F0.97

0+51.4 64.82 65.87 F1.05

0+71.4 65.65 66.47 F0.82

0+79.94 = 66.95 66.59⁷¹ C 0.36

R.E. 1534 3/4"

Rough Grades ~ Franklin St.

47th to 48th

W.O. 32388

2-3-55

Plan 11345-L

Hatch
South

(45)

110.95 s.e. spike
47th + Franklin

123.78 spike in s.
pole at alley

North

0+00 = East line 47 th	109.45	108.97		Top Cb. 109.50	109.75	
0+30	11.4	110.0	C 1.4	11.7	110.2	C 1.5
+50	11.6	110.3	C 1.3	12.4	110.6	C 1.8
+90	12.5	111.1	C 1.4	13.6	111.5	C 2.1
1+30	13.4	112.0	C 1.4	14.4	112.4	C 2.0
+70	14.0	112.9	C 1.1	20.4	113.3	C 7.1
2+10	14.5	113.9	C 0.6	20.5	114.2	C 6.3
+50	15.4	114.8	C 0.6	20.6	115.1	C 5.5
+80	16.5	115.5	C 1.0	20.2	115.7	C 4.5
3+10	17.8	116.2	C 1.6	20.2	116.4	C 3.8
+40	18.4	116.85	C 1.6	20.7	117.0	C 3.7
+60	18.8	117.4	C 1.4	20.9	117.5	C 3.4
+80	19.5	117.9	C 1.6	21.0	118.0	C 3.0
4~	20.5	118.6	C 1.9	21.1	118.6	C 2.5
+20	21.1	119.4	C 1.7	21.6	119.3	C 2.3
+40	21.8	120.3	C 1.5	22.1	120.0	C 2.1
+60	22.5	121.5	C 1.0	23.0	121.0	C 2.0
+80	23.8	122.85	C 1.0	23.7	122.2	C 1.5
5+00	25.9	124.4	C 1.5	24.9	123.7	C 1.2

(Continued)
 Rough grade stakes
 Franklin St.
 47th to 48th St.
 South

5+20	27.8	126.3	C1.5
+55	30.5	129.6	C0.9
+75	32.3	131.6	C0.7
5+94.80	33.9	133.0	C0.9
6+04.80	34.9	133.75	C1.1
E 48th St.			
0+00 = E. line 48th	39.9	136.7	C3.2
+40	42.9	138.6	C4.3
+75	44.5	140.3	C4.2
1+15	45.5	142.0	C3.5
+55	46.8	143.1	C3.7
+95	47.3	143.6	C3.7
2+57 = Cb. B.C.	47.0	143.9	C3.1
3+37 = Cb. P.C.	45.2	144.4	C0.8
+50	44.9	144.5	C0.4
4~	45.0	144.7	C0.3
+50	45.6	145.0	C0.6
5~	46.5	145.3	C1.7

(46) 138.55 S.E. Hyd.
 48th & Franklin
 145.62 S.W. 3' LYT
 49th & Franklin
 North

25.6	125.5	C0.1
27.7	128.9	F1.2
29.7	130.7	F1.0
31.1	132.3	F1.2
31.9	132.8	F0.9
34.0	134.7	F0.7
37.3	136.2	C1.1
39.4	138.1	C1.3
40.6	139.8	C0.8
38.6	141.5	F2.9
41.0	142.7	F1.7
44.1	143.4	C0.7
43.6	143.8	F0.2

2+50

5+50

46.3 145.5 C0.8

6+00

46.8 145.7 C1.1

Stake Curbs - Franklin St.

48

Gloria to 49⁴
 Plan - 11346-L 1-8-55 7.0.

SE Ret. Gloria

4.50

45.17

Meet

44.48⁴⁶ - ?

1/2

44.44 44.36⁴⁴ C 0.08

45.12

P.C. = 0+00

44.54 44.39⁵⁴ C 0.15

+35

44.53 44.57 F 0.04

+70

44.45 44.74⁴⁵ F 0.29

1+05

44.98 44.92⁹⁸ C 0.06

+40

45.26 45.09²⁶ C 0.17

+75

45.32 45.27³² C 0.05

2+10

45.51 45.44⁵¹ C 0.07

+45

45.50 45.62⁵⁰ F 0.12

+67

45.30 45.73³⁰ F 0.43

28.3 = PC

45.52 45.67⁵² F 0.15Meet - 49⁴

45.65 - ?

Curb Stakes - Franklin -
48th to Gloria -

BM 138³⁵ SE Hyd (A)
Franklin 48th

staked 3' BK of face

South

North

Notes	Station	Station	Station	Station	Station	Station
	Meet	136 ⁴⁵	✓			
		136 ⁵²	36 ²³ C0.21	E.L. = 0+00	36.45	36.16 ⁴⁵ C0.29
Ely 48 th St 0+00 = P.C.		137 ⁰⁵	37 ¹⁴ C0.09	+25	37.70	37.38 ⁷⁰ C0.32
+33.5		138 ⁶⁸	38 ⁹⁶ C0.28	+50	38.78	38.60 ⁷⁸ C0.18
+67 B.V.C.		140 ³²	40 ⁴⁸ C0.16	+75	39.82	39.82 C0
+87		141 ²²	41 ³⁰ C0.08	+95	40.71	40.74 F0.03
1+07		141 ²⁹	42 ³⁰ C0.31	1+15	41.57	41.52 C0.05
2 nd Red. 1+15 Wly Alley BC	st 142 ²³	42 ²⁶ C0.03		+35	42.12	42.19 F0.07
1417 Wly Alley Prop	A 142 ²³	42 ²⁶ F0.07		+55	42.50	42.73 ⁵⁰ F0.23
1432 Ely Alley Prop	3/10 Obs 142 ⁴⁹	45 ³⁸ C0.28		+75	43.06	43.14 ⁵⁰ F0.08
2 nd Red. 1+34 Ely Alley EC	3/10 Obs 142 ²⁸	44 ⁷² C1.80		+95	43.48	43.44 C0.04
1447	A 142 ²⁴	42 ²⁵ C0.19		2+30	43.89	43.72 ⁸⁹ C0.17
1467	st 142 ²²	42 ²⁵ C0.18		+65	44.26	44.00 ²⁶ C0.26
1487 E.V.C.	143 ⁰⁹	43 ¹⁹ C0.10		Meet.	44.35	44.16
2+19	143 ⁴¹	43 ³⁷ F0.04				
Gloria St. 2+48 ⁸⁹ BC Rd	143 ⁶⁰	43 ⁷⁰ C0.10				
Mid Pt	143 ⁷⁵	44 ⁰⁴ C0.29				
	143 ⁹⁰	44 ⁰³ C0.13				
	144 ⁰²	44 ²⁰ C0.18				
	144 ²⁰	✓				
	Meet	✓				

Cb stakes Franklin 48th wly to Alley on South
staked 3' BK ob face

North

		Next						
existing cb rod		134 ⁶³	✓					
Mid Pt.		133 ²¹	33 ²⁴	FO.17	± 48 th	34.74	34.70	C 0.04
0+00 wly 48 th		133 ⁵⁴			+25' 10' E.	33.62	33.61	C 0.01
0+08 BC		133 ¹⁶	32 ⁹⁰	FO.26	0+10	32.05	32.27 ₀₅	F 0.22
0+30 ³⁶		131 ⁵⁷	31 ¹²	FO.45	0	30.26	30.70 ₇₀	F 0.44
0+50 ³⁶		129 ⁶³	29 ²⁰	FO.43		28.61	28.89 ₆₁	F 0.28
0+85 ³⁶		126 ²⁶	26 ⁰³	FO.23	+85.36	25.08	25.51₅₈	F 0.43
1+05 ³⁶		124 ⁴⁴	24 ³¹	FO.13	1+05.36	22.50	23.72	F 0.22
1+23 ^{2nd BC}		St. 123 ⁰² A 122 ⁸⁸	23 ⁰⁰	G CO.13	+25.36	22.31	22.21	C 0.10
1+25 Ely Prop Alley	5/8 ob face	123 ⁰⁴	24 ⁴⁸	C.144	+45.36	21.14	20.98 ₁₄	C 0.16
1+40 wly Prop Alley	no ob face	122 ⁰²	22 ⁶⁵	CO.63	+65.36	20.17	20.03 ₁₇	C 0.14
1+42 ^{2nd BC}		St. 121 ⁸⁶	21 ⁶⁵	FO.21 FO.03	+85.36	19.34	19.26 ₃₄	C 0.08
1+45	staked 5' BK ob face	121 ⁴⁸			+05.36	18.57	18.59	F 0.02
1+65	↓	120 ³⁴	20 ²³	FO.11	+25.36	17.85	18.01 ₈₅	F 0.16
1+85		119 ³⁹	19 ³⁴	FO.05	2+45.36	17.16	17.51 ₁₆	F 0.35
1+105		118 ⁵⁷	18 ⁷⁰	CO.13	+80.36	16.57	16.74 ₅₇	F 0.17
2+125		117 ²⁰	17 ⁹⁰	G.	3+15.36	15.90	15.96	F 0.06
2+45 ³⁶ FVC		117 ³⁶	17 ²⁶	FO.10	+50.36	15.16	15.18	F 0.02
1+2+72		116 ²³	16 ⁶⁰	FO.13	+85.36	14.30	14.40	F 0.10
					4+20.36	13.39	13.62 ₃₉	F 0.23

2+99		116 ¹⁰	15 ⁸⁸	F0.22
3+25	see bottom pg for 6' Alley drain ditch	115 ^{AS}		
3+53		114 ⁹⁵	14 ⁷⁰	F0.15
3+80		114 ²²	14 ⁰⁵	F0.17
4+07		113 ⁶⁰	13 ⁶⁹	C0.09
4+34		112 ⁹⁷	12 ⁹⁷	G.
4+61		112 ³⁵	12 ⁴⁶	C0.11
4+88		111 ⁷²	11 ⁹⁶	C0.24
5+14 ³⁰ BVC		111 ⁰	11 ²³	C0.13
5+34 ³⁰		110 ⁶⁷	10 ⁸⁶	C0.19
5+54 ³⁰		110 ³⁰	10 ³⁸	C0.08
5+74 ³⁰		109 ⁹⁷	09 ⁷⁸	F0.19
5+94 ³⁰ 20' rd. BC.		109 ⁶³	09 ¹⁶	F0.47
	0904 walk	109 ⁴⁵	09 ¹⁸	(F0.27)
3+16 ³ 2' rd. BC.	st. A	115 ⁷¹	15 ⁸⁹	C0.18
		115 ⁷⁰		C0.19
3+18 ² Fly Alley Prop	5/10 cb	115 ⁸⁶	17 ³¹	C1.45
3+24 ² wly Alley Prop	5/10 cb	115 ⁷³	16 ⁶⁰	C0.87
	A.	115 ⁵⁷		C0.86
3+26 ² 2' rd. EC.	st.	115 ⁴⁸	16 ⁴³	C0.95

4+55.59 = P.C.	12.88	12.84 ⁸⁸	C0.04
To Alley	12.88	12.84	C0.04
end - E.	13.63	13.00 ⁶³	C0.63
End - w	14.20	12.66 ²⁰	C1.54
To Alley	12.34	12.50 ³⁴	F0.16
4+74.59 = P.C.	12.34	12.42 ³⁴	F0.08
+94.84	11.85	11.97 ⁸⁵	F0.12
5+24.84	11.25	11.31 ²⁵	F0.06
+54.84	10.65	10.64	C0.01
+74.84	10.13	10.24 ¹³	F0.11
+94.84 = B.C.	09.87	09.90	F0.03
end. = E.L.	09.69	09.75 ⁶⁹	F0.06
47+1/2			
1st Drain			
P.C. = 0+78.66	25.71	26.16 ⁷¹	F0.45
To Drain	25.71	26.01 ⁷¹	F0.30
end - E	25.83	26.17 ⁸³	F0.34
end - w.	25.50	25.59	F0.09
To Drain	24.90	25.43 ⁹⁰	F0.53
P.C. = 0+88.66		25.21	F0.31

2nd Drain

1+93.57 = P.C.	19.05	^{9.05} 18.99	C 0.06
To Drain	19.05	^{9.05} 18.92	C 0.13
End - E.	21.40	^{21.40} 19.08	C 2.32
End - W.	21.18	^{21.18} 18.88	C 2.30
To Drain	18.59	18.72	E 0.13
2+03.57 = P.C.	18.59	^{18.59} 18.65	F 0.06

Cont. from P. 53

W.

E

End.	63.4	^{3.4} 61.7	C 1.7	Park	65.7	^{5.2} 61.7	C 3.5
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Rough Grades - Pepper Dr. + Tulip
Thru Park - Plan - 11181-L

w.o. 21165 - 3-2-55 70

		North		Park	South
w.L. of Park 0+00 = \pm Pepper		56.2		0+11.70 =	56.70
0+38.75 ⁺ +11.25	58.1	56.8 ^{8.1}	C 1.3		57.7 ^{5.7}
0+80	58.8	57.7 ^{8.8}	C 1.1		59.0 ^{9.0}
1+13.46 = PC	59.2	58.4 ^{9.2}	C 0.8	3' Bk.	58.7
1+58.22 E.C.	60.4	59.3 ^{60.4}	C 1.1	= PC.	60.3
1+92.73	61.6	60.6 ^{61.6}	C 1.6	E.C. } Ret.	60.3
2+37.04	62.9	60.9 ^{62.9}	C 2.0	= PC.	64.6
3+75.10	63.9	61.7 ^{63.9}	C 2.2		65.6
+13.17 = P.C.C.	63.0	62.5 ^{63.0}	C 0.5		65.7
+12.55 = Park	63.4	62.7 ^{63.4}	C 0.7		63.0

		West		East
Tulip:				
B.C. of Curve	60.0	60.90	F 0.8	EC Ret. 63.5
Bk	60.0	61.0	F 1.0	64.1
1/4	60.4	61.1	F 0.7	64.8
1/2	60.6	61.3	F 0.7	64.4
3/4	62.0	61.4	C 0.6	63.7
Alley	62.2	61.6	C 0.6	64.1
				64.9

P. 52

Stake Sewer - 47[±] - Aurora - Uvas
 + Market - Plan - 2572 - D
 w.o. 32349 3-8-55

107.47 - R.P. Cross at gate

54

	88.19		
0+00 = M.H. 1	88.30	88.30 82.21	6.09
+20	89.03	89.03 82.46	6.57
+40	90.86	90.86 82.88	7.98
+60	92.81	92.81 83.60	9.21
+80	94.24	94.24 84.57	9.67
1+15	95.16	95.16 86.70	8.46
+50	96.96	96.96 88.83	8.13
+85	02.52	02.52 90.96	11.56
2+20	03.82	03.82 93.09	10.73
+51.14 = M.H. 2	05.10	04.64 95.00	10.10 C 9.64
+35	05.69	05.69 96.14	C 9.55
+70	06.45	06.45 97.28	9.17
1+05	07.05	07.05 98.42	C 8.63
+40	07.47	07.47 99.56	C 7.91
+81.67 = M.H. 3	07.99	07.99 100.90	7.09
+35	08.87	08.87 01.80	C 7.07
+70	09.39	09.39 02.70	6.69
1+05	10.17	10.17 03.60	6.57

1+40	10.95	10.95 04.50	C 6.45
+60 = M.H. 6	12.07	12.07 05.00	7.07
0+30	13.56	13.56 06.18	C 7.38
+60	14.58	14.58 07.35	7.23
+90	15.29	15.29 08.52	6.77
1+20 = Plug	16.32	16.32 09.70	6.62
Req. Uvas.			
0+00 = M.H. 3	1	00.90	
+35	08.50	08.50 01.04	7.46
+70	08.45	08.45 01.18	7.27
1+05	08.28	08.28 01.32	6.96
+40	08.40	08.40 01.46	6.94
+75	08.69	08.69 01.60	7.09
2+10	09.49	09.49 01.74	7.75
+45	11.94	11.94 01.88	10.06
+71.32 = M.H. 4	14.67	14.67 02.00	12.67
0+30	18.97	18.97 06.50	12.47
+60	22.32	22.32 11.00	11.32
+82	24.55	24.55 14.30	10.25
1+02	26.70	26.70 16.94	9.76

Pole Uvas & Market

13174

55

Pole at E. end.

129.91

1+22	28.48	^{28.48} 18.85	9.63	M.H. 5 to E.			
+42	29.60	^{29.60} 20.03	9.57	0+00 = M.H. 5		21.00	
+62	30.36	^{30.36} 20.48	9.88	+28 PC.	30.69	^{30.69} 21.11	C 9.58
+92	30.68	^{30.68} 20.62	10.06	+65	31.90	^{31.90} 21.25	10.65
2+22	31.20	^{31.20} 20.77	10.43	1+00	31.81	^{31.81} 21.39	10.42
+52	31.31	^{31.31} 20.90	10.41	+35	31.31	^{31.31} 21.53	9.78
+75.28 = M.H. 5	30.65	^{30.65} 21.00	C 9.65	+70	31.03 31.92	^{31.92} 21.67	^{9.36} 10.25
				2+05 T.P.	30.79 32.19	^{32.19} 21.81	^{8.98} 10.38
Market - West of M.H. 5				+40	31.98	^{31.98} 21.75	10.03
0+00 = M.H. 5	30.65	^{30.65} 21.60	9.05	+75	31.47	^{31.47} 22.09	9.38
+25	30.53	^{30.53} 21.80	8.73	3+10	30.98	^{30.98} 22.23	8.75
+50	30.73	^{30.73} 22.00	8.73	+45	28.58	^{28.58} 22.37	6.21
+75	30.93	^{30.93} 22.20	8.73	+70 = M.H. 8	29.88	^{29.88} 22.48	7.40
1+00	31.05	^{31.05} 22.40	8.65	0+35	29.07	^{29.07} 22.62	6.45
+25	30.83	^{30.83} 22.60	8.23	+70	28.82	^{28.82} 22.76	6.06
+50	30.73	^{30.73} 22.80	7.93	1+05	28.57	^{28.57} 22.90	5.67
+75	30.21	^{30.21} 23.00	7.21	+40	28.33	^{28.33} 23.04	5.29
2+00	30.67	^{30.67} 23.20	7.47	+70 = Plug.	28.12	^{28.12} 23.16	4.96
+25	30.65	^{30.65} 23.40	7.25				
+50 = M.H. 7	30.73	^{30.73} 23.60	7.13				

Curb Stakes - Azalia Park
 Pepper Dr. + Tulip - Plam - 11181-L

3-14-54

7.0.

56

Pepper - Beg. at Park

W.

S.

0+00.74 = Meet.

56.22 ✓

+18.75 56.18 56.50₈ F 0.32

+38.75 56.48 56.84₄₈ F 0.36

+58.75 56.90 57.23₉₀ F 0.33

+86.06 57.54 57.79₅₄ F 0.25

1+13.37 = P.C. 58.08 58.36₀₈ F 0.28

+35.79 58.44 58.82₄₄ F 0.38

+58.21 59.00 59.28₀₀ F 0.28

+92.72 59.67 59.99₆₇ F 0.32

2+14.86 60.17 60.45₁₇ F 0.28

+37 = opp. P.C. Ret. 60.65 60.90₆₅ F 0.28

+62.38 61.10 61.43₁₀ F 0.33

+87.76 61.57 61.96₅₇ F 0.39

3+13.14 62.19 62.48₁₉ F 0.29

+11.66 62.46 62.72₄₆ F 0.26

End at Park - East.

0+10.18 = Meet.

56.70⁷⁵

+44.58 57.06 57.42₀₆ F 0.36

+78.98 57.73 58.14₇₃ F 0.41

1+13.37 = P.C. 58.53 58.86₅₃ F 0.33

+35.79 59.15 59.32₁₅ F 0.17

+58.21 = P.C. Ret. 59.63 59.79₆₃ F 0.16

P.C. 61.15 61.41₁₅ F 0.26

61.66 61.94₆₆ F 0.28

62.17 62.46₁₇ F 0.29

62.57 62.98₅₇ F 0.41

+1.65 62.97 63.03₉₇ F 0.06

Beq. Tulip - at Pepper

West.

East.

		59.79		1	61.14	61.30	F 0.16
1/3	59.82	59.97	F 0.15	2	60.99	61.20	F 0.21
2/3	59.94	60.15	F 0.21	3	60.98	61.15	F 0.17
E.C.	59.99	60.34	F 0.35	4 = E.C.	60.74	61.10	F 0.36
BC. of Big Curve	60.20	60.80	F 0.60		60.55	61.10	F 0.55
12° = Brk	60.60	61.00	F 0.40		60.63	61.16	F 0.53
1	60.81	61.13	F 0.32		60.75	61.25	F 0.50
2	60.81	61.26	F 0.45		61.00	61.34	F 0.34
3	61.08	61.39	F 0.31		61.07	61.43	F 0.36
PC. 4' Rad.	60.88	61.48	F 0.60		61.30	61.53	F 0.23
E.C.	60.88	61.58	F 0.70				
End	61.23	61.64	F 0.41				
End. - on E. = E.C.	63.81	61.72	C 2.09	= PRC. = E.C.	61.42	61.58	F 0.16
PC. 2' Rad.	61.58	61.65	F 0.07		61.63	61.65	F 0.02
E.C. = End	61.58	61.61	F 0.03				

Stake Sewer - Kearny Mesa - Plan-12068-L
w.o. 62416 - 4-1-55 7.0.

58

0+00 = Exist. MH # 57	40	5.66	
+35	22.96	05.77	17.19
+70	23.29	05.87	17.42
1+05	23.29	05.98	17.31
+40	23.81	06.08	17.73
+75	24.15	06.19	17.96
2+05 = Lat ⁱⁿ ①			
+10	24.68	06.29	18.39
+45	24.68	06.40	18.28
+80	24.73	06.50	18.23
3+15	25.20	06.61	18.59
+50 = M.H. 1	25.64	06.71	18.93
0+85	25.04	06.82	18.22
+70	25.49	06.92	18.57
1+05	24.14	07.03	17.11
+33 = Lat ②	23.98		
+35 = Plug	23.98	07.12	16.86

Stake Alley - Block 2 - Bartlett Sub.
 Plan - 11363-L - 4-12-55 7.0.
 W.O. 32417

2' Bk. = 11.75 from t

West

0+00 = N.L. E.		71.77	
+30 - 0.5 B	73.70	^{3.70} 71.67	C 2.03
+50 - 0.5 B	73.65	^{3.65} 71.77	C 1.88
+70 - 0.25 B	73.41	^{3.41} 72.20	C 1.21
+80 0.25 B	73.43	^{3.43} 72.50	C 0.93
1+00	75.27	^{5.27} 73.00	C 2.27
+20	75.26	^{5.26} 73.32	C 1.94
+55	76.03	^{6.03} 73.70	C 2.33
+90	77.75	^{7.75} 74.08	C 3.67
2+10	75.79	^{5.79} 74.51	C 1.28
+30	76.59	^{6.59} 75.35	C 1.24
+60	77.59	^{7.59} 76.91	C 0.68
+90.30 = End.	78.43	^{78.48} _{.43}	F 0.05

10' from S.L. Broadway

BM = Spike in Pole - 252 = 172.22
 " " " 2+20 = 176.09

59

East.

			70.24	
	70.38	71.01		F 0.63
1' Bk	70.90	71.52		F 0.62
	69.31	72.03		F - 2.72
	69.54	72.29		F 2.75
on line	73.05	72.72		C 0.33
0.25 B	73.02	73.02		C
	72.83	73.40		F 0.57
	72.96	73.78		F 0.82
	73.17	74.20		F 1.03
	75.95	75.80		C 0.95
	78.33	76.74		C 1.59
	78.86	78.48		C 0.38

Stake Drain - 25th + Broadway
 Plan - 11364-L - 4-13-55 - 7.0.

0+00 = outlet.	78.63	78.13 ⁶³	C 0.50
+20	87.52	78.25	C 9.27
+45	87.87	78.40	C 9.47
+67.33 = B.C.	87.96	78.53	C 9.43
+79.47	87.58	78.60	C 8.98
+91.62	88.05	78.67	C 9.38
1+03.76	88.05	78.75	C 9.30
+15.91 = F.C.	87.80	78.82	C 8.98
+45	86.66	78.99	C 7.67
+77.54 = \pm inlet	86.14	79.17	C 7.01
^{37.46} 2+15	85.62	79.40	C 6.22
2+50	86.21	79.61	C 6.60
+86.54 = \pm Inlet.	85.62	79.82 ⁶²	C 5.80
³⁰ 3+16.54 = End.	86.20	82.06	C 4.14
+46.54	88.37	83.13	C 5.24
+71 = \pm CL. - end.	91.25	84.00	C 7.25

90.89 = Bot. of opening?

81.00 - C 4.62 = 12" ahead.

Rough Grade Stakes - "A" St. Edgemont
 Plan - 11209-L - 4-14-55 7.0
 W.O. 32340

North

0+00 = E.L. Edgemont	29.06		
+30	30.5	^{30.5} 29.3	C 1.2
+80	28.7	⁷ 28.1	C 0.6
1+00	28.2	^{8.2} 27.5	C 0.7
+30	27.0	^{2.0} 25.6	C 1.4
+50 - 1 in	23.7	^{3.7} 23.1	C 0.6
+75	19.6	^{9.6} 19.1	C 0.5
+95	17.1	^{2.1} 15.0	C 2.1
2+25	05.2	^{07.5} 5.2	F 2.3

E.

227.77 = Sw. B.P. A + Edgemont.

20.40 61

$\frac{12.2}{0.52}$

South

cut 0+00

+20	27.73
+30	27.85
+40	27.84
+67.5	27.61
+93 = P.C.	26.91
E.C. = Alley	26.27
end.	26.25

26.92 26.44

C 0.48

From Top.

Rough Grades + cb. cuts - 69th
 El Cajon to Amberst. - Plan - 11699-L
 W.O. 32410 - 4-18-55 70.

5' Blk.

62

West.

East.

0 to 5 = N.L. Amberst.

+10 = P.C.	54.2	54.2	G	55.7	54.5 ^{5.7}	C 1.2
+60	53.9	54.4 ^{5.4}	F 0.5	55.4	54.7 ^{5.4}	C 0.7
+10	54.0	54.6	F 0.6	55.6	54.8 ^{5.6}	C 0.8
+50 = Alley	55.0	54.7 ^{5.0}	C 0.3	54.7	55.0 ^{4.7}	F 0.3

Rough Grades - Marilou Rd. - Brookline
 + Elm - Plan - 2738-D
 W.O. 62905 - 4-19-55 7.0.

Beg. 48th + Marilou

PC. to W. 31.2 30.3 C 0.9

= E.C. to N.
 0+00 = 48th 30.0 30.0 G

+ 28.5 = P.C. to S. 29.2 29.5 F 0.3

+ 67.6 27.8 28.5 F 0.7

+ 87.6 27.0 27.9 F 0.9

1 + 27.6 = B.C. on N. 25.4 26.0 F 0.6

1/2 24.4 24.8 F 0.4

Now West. on Brookline

0+00 = E.C. 23.6 23.7 F 0.1

+ 31.5 21.8 22.1 F 0.3

+ 63 20.8 20.5 C 0.3

+ 87 = Prop. P.C. 19.9 19.6 C 0.3

R.R.C. 20.0 19.8 C 0.2

E.C. = 0+00 20.1 20.3 F 0.2

+ 40 20.6 20.7 F 0.1

+ 80 21.0 21.3 F 0.3

1+20 21.6 21.8 F 0.2

228.82 = Pipe to Marilou + E.L. Brookline
 222.82 = Top F.H. N.E. Date + Brookline

63

S.

30.7 30.7 C 1.2
 29.5 29.5
 31.4 31.4 C 2.9
 28.5 28.5
 31.5 31.5 C 3.6
 27.9 27.9
 32.1 32.1 C 6.0
 26.1 26.1
 31.9 31.9 C 6.5
 25.4 25.4
 29.8 29.8 C 5.2
 24.6 24.6
 23.8 23.8 F 0.1
 23.9 23.9

Top
 31.1 / 26.2k 3 RP 31.4
 31.5 3=C 39 31.5
 4.6
 32.2 - 6.6 32.1
 7.10
 32.0 - 6.6 31.9
 7.60
 30.1 - 6.2 29.8
 6.50

on S.
 1 + 25.1 = B.C. 32.2 - 6.6 32.1
 7.10

E.C. = East. 23.0 23.2 F 0.2
 22.7 22.7 C 1.1
 21.8 21.8 C 1.8
 20.0 20.0

w. Side of Brookline

229.09 = Pole - E. - Elm + Brookline

64

217.21 = Pole Tilden

1 + 58.47	22.3	22.4	F 0.1	4 + 16.25	19.0	^{9.0} 17.2	C 1.8
+ 98.47	22.9	23.0	F 0.1	^{25.22} + 41.47 = B.C.	19.5	16.6	C 2.9
2 + 38.47	23.6	23.7	F 0.1	Water Stakes - Elm.			
+ 78.47	24.1	24.4	F 0.3	0 - 10 = Conn.			
3 + 28.47	24.8	25.4	F 0.6	0 + 00	28.4	^{4.4} 24.7	C 3.7
+ 78.47	26.0	26.4	F 0.4	+ 50	27.7	^{7.7} 24.6	C 3.1
4 + 20.41 = B.C.	27.5	27.3	C 0.2	1 ~	27.1	^{7.1} 24.2	C 2.9
Beq. S. side of Elm.				+ 50	26.8	^{6.8} 23.8	C 3.0
0 + 00 = E.C.	27.8	^{7.8} 28.1	F 0.3	2 ~	26.5	^{6.5} 23.4	C 3.1
+ 20	27.7	28.0	F 0.3	+ 44	26.3	^{6.3} 23.1	C 3.2
+ 70	27.2	27.6	F 0.4	+ 92	25.5	^{5.5} 22.6	C 2.9
1 + 20	26.7	27.2	F 0.5	3 + 40	24.9	^{4.9} 22.6	C 2.9
+ 70	26.5	26.7	F 0.2	+ 80	23.6	^{3.6} 20.7	C 2.9
2 + 20	25.0	26.2	F 1.2	4 + 20	21.2	^{21.2} 17.7	C 3.5
+ 70	24.8	25.8	F 1.0	+ 40	19.0	^{9.0} 15.5	C 3.5
+ 90.87	24.7	^{4.7} 25.6	F 0.9	+ 60	17.2	^{7.2} 13.7	C 3.5
3 + 30.87	23.6	^{3.6} 24.3	F 0.7	+ 82.5 Lt.	16.8	^{6.8} 12.8	C 4.0
+ 70.87	21.2	21.3	F 0.1				
^{25.38} + 96.25	18.7	⁷ 18.4	C 0.3				

Stake Sewer - Winnett - Plan - 2424-D

w.O. 32387- 4-21-55 7.0.

277.10 = Pole - sw. Winnett + Fed.

4.15075 = Pole at Tooley

367.68 = Pole = Lt 2+35 - Det M.H. 4+5

334.11 = Pole - Below M.H. 4

308.66 = Pole Below M.H. 3

65

- Sh.		74.01	74.01						
0+00 = Conn. in Federal		74.01	269.01	5.00	3+55.80 = M.H. 4	36.07	36.07	29.00	7.07
+35		79.36	72.51	6.85	+35	39.73	32.98	31.73	6.75
+70		84.10	76.01	8.09	+70	43.70	36.96	43.70	6.74
1+05		88.63	79.51	9.12	1+05	47.50	40.94	7.50	6.56
+40	T.P.	92.95	83.01	9.91	+40	51.77	44.72	51.77	6.87
+75		96.81	86.51	10.30	+75	56.04	48.90	56.04	7.14
2+10		00.17	90.01	10.16	2+10	60.38	52.88	60.38	7.50
+45		03.18	93.51	9.67	+45	64.43	56.86	64.43	7.57
+80		06.30	97.01	9.29	+80	68.74	60.84	8.74	7.90
3+19.90 = M.H. 3		09.80	01.80	8.80	3+15	72.65	64.81	72.65	7.84
+35		12.35	03.75	8.60	+52 = M.H. 5	76.93	69.00	76.93	7.93
+70		14.58	06.50	8.08	0+35	80.93	73.11	80.93	7.82
1+05		16.62	09.26	7.36	+70	85.24	77.21	85.24	8.03
+40		18.85	12.01	6.84	1+05	89.41	81.32	9.41	8.09
+75		21.01	14.77	6.24	+40	93.27	85.42	93.27	7.85
2+10		23.41	17.52	5.89	+75	97.36	89.53	97.36	7.83
+45		25.99	20.28	5.71	2+10 - T.P.	01.54	93.63	01.54	7.91
+80		28.82	23.03	5.79	+30 = Brk	03.87	95.97	03.87	7.90
3+15		32.01	25.79	6.22	+50	06.09	98.16	06.09	7.93

45.94

59.61

73.60

87.72

445.90 = SW Pole Tooley + Republic
 449.30 = Pole - Tooley - 2+45 - Bet MH 9+10

66

2+70	08.51	400.01	8.50	2+42.64 = MH.8	44.72	44.72	14.96
+90	11.13	01.13	9.59	0+35	45.14	29.76	15.24
3+10	14.03	02.03	11.28	+70	45.98	45.98	15.94
+30	15.74	03.74	12.10	1+05	47.37	47.37	17.19
+50 = M.H. 6	5' Lt. 14.64	04.64	10.44	+40	48.65	48.65	18.33
Req. Tooley to w.	10' S. 13.47	04.20	9.27	+72.69 = MH 9	49.40	49.40	18.95
0+35	15.50	07.50	7.75	0+35	49.81	49.81	19.22
+70	18.28	11.28	6.99	+70	49.81	49.81	19.08
1+05	22.17	14.84	7.33	1+05	49.66	49.66	18.79
+40	26.73	18.38	8.35	+40	49.42	49.42	18.41
+75	31.24	21.93	9.31	+75	49.51	49.51	18.36
2+10	35.68	25.48	10.20	2+10	49.45	49.45	18.16
+42.63 = M.H. 7	39.74	28.79	10.95	+45	48.67	48.67	17.24
0+35	43.50	33.50	14.57	+80	46.77	46.77	15.20
+70	45.72	29.07	16.65	3+15	44.54	44.54	12.83
1+05	46.08	29.21	16.87	+50.04 = M.H. 10	41.28	41.28	9.43
+40	45.40	29.35	16.05	0+10 = Plug.	40.11	40.11	8.22
+75	44.74	29.49	15.25				
2+10	44.68	29.63	15.05				

Beq. Fulmar St. - Tooley - N.

Pole Fulmar at End 440.39

0+00 = M.H. 9		30.45	
+35	49.11	49.11 30.59	18.52
+70	48.35	48.35 30.73	17.62
1+05	47.02	47.02 30.87	16.15
+40	45.29	45.29 31.01	14.28
+75	43.85	43.85 31.15	12.70
2+10	42.67	42.67 31.29	11.38
+45	41.17	41.17 31.43	9.74
+80	39.05	39.05 31.57	7.48
3+00 = M.H. 11	37.72	37.72 31.65	6.07
0+38 = Plug.	35.20	5.20 31.81	3.39

Beq. Republic - S. of Tooley

0+00 = M.H. 8		29.76	
+20	44.83	44.83 31.47	13.36
+40	45.93	45.93 32.89	13.04
+60	46.92	46.92 34.02	12.90
+80	48.56	44.56 34.84	13.72
1+00	50.03	50.03 35.37	14.66
+20	51.11	51.11 35.60	15.51
+55	52.49	52.49 35.74	16.75

456.41 = BM in Pole By. MH-12

67

1+75 = c = ch. 1+90 = c	53.46	53.46 35.88	17.58
2+25 35	54.08	54.08 36.02	18.06
+60	54.38	54.38 36.16	18.22
^{2+50 c} ^{2+90 c} 3+00 = M.H. 12	54.72	54.72 36.32	18.40
0+35 - 75 ft	55.11	55.11 36.46	18.65
+70 +75 - 95 = c	55.51	55.51 36.60	18.94
1+05	55.85	55.85 36.74	19.11
+40	55.88	55.88 36.88	19.00
+75 = c	55.79	55.79 37.02	18.77
+95 = c	55.65	55.65 37.16	18.49
2+10	55.60	55.60 37.30	18.30
+45	55.60	55.60 37.30	18.30
+80 = c	55.53	55.53 37.44	18.09
3+00 = M.H. 13	55.53	55.53 37.52	18.01
^{0+10 = c} 0+35	55.58	55.58 37.66	17.92
+70	55.74	55.74 37.80	17.94
1+05	56.15	56.15 37.94	18.21
+33 = c +40	56.47	56.47 38.08	18.39
+48 = c +75	56.70	56.70 38.22	18.48
2+05.17 = B.C.	56.65	56.65 38.34	18.31
+24.14	56.50	56.50 38.42	18.08

455.89 = Pole E. of curve

2+43.10	56.31	56.31 38.49	17.82
+45-c			
+62.07	55.91	55.91 38.57	17.34
+81.03	54.90	54.90 38.64	16.26
3+00 = M.H. 14	53.99	53.99 38.72	15.27
0+10=c			
0+19.76	53.07	53.07 38.80	14.27
+39.52	51.76	51.76 38.88	12.88
+59.28	50.07	50.07 38.96	11.11
+79.04	48.89	48.89 39.04	9.85
+98.81 = EC.	47.28	47.28 39.12	8.16
1+25	46.53	46.53 39.22	7.31
+60	45.89	45.89 39.36	6.53
+95	45.22	45.22 39.50	5.72
2+30	45.18	45.18 39.64	5.54
+65	45.61	45.61 39.78	5.83
3+00 = M.H. 15	45.54	45.54 39.92	5.62
+30	45.02	5.02 40.04	4.98
+60	44.07	4.07 40.16	3.91
+90 = Plug.	43.68	3.68 40.28	3.40

Tooley - To East. 457.99 = Pole 60
Tooley + Oriole

440.82 = Pole by M.H. 6

Winnett	7' Lt.		
0+00 = M.H. 6		404.20	cut
+35	15.75	15.75 07.57	8.18
+70	18.19	18.19 10.94	7.25
1+05	21.56	21.56 14.31	7.25
+40	25.13	25.13 17.68	7.45
+75	28.46	8.46 21.05	7.41
2+10	31.99	31.99 24.42	7.57
+45	35.62	35.62 27.79	7.83
+69.78			
+70 = M.H. 16	37.82	7.82 30.20	7.62
0+35	39.79	9.79 31.19	8.60
+70	40.58	10' Rt 40.51 = 8.33 32.18	8.40
1+05 - 10' Rt.	41.26	41.26 33.17	8.09
+40 10 Rt.	42.60	42.60 34.16	8.44
+75 10' Rt.	44.02	44.02 35.15	8.87
2+00 10' Rt.	44.60	44.60 35.86	8.74
+26.48 = M.H. 17	46.01	46.01 36.60	9.41
0+35 - 10' Rt 48.00 37.64	47.42	47.42 37.64 = 7' Lt.	9.78
+70 - 7' Lt.	50.47	50.47 38.67	11.80
1+05	53.68	53.68 39.71	13.97

456.83 = Pole - Swan + Tooley

74t.

1+40	55.61	40.74	14.87
+75 - T.P.	57.11	41.78	15.33
2+10	58.27	42.81	15.46
+48.05 = M.H. 18	58.88	43.94	14.94
0+35	59.47	44.08	15.39
+70	60.11	44.22	15.89
1+05	60.14	44.36	15.78
+40	59.37	44.50	14.87
+75	58.40	44.64	13.76
2+10	57.91	44.78	13.13
+48.05 = M.H. 19	57.59	44.93	12.66
0+35	57.65	45.07	12.58
+70	57.86	45.21	12.65
1+05	57.69	45.35	12.34
+40	56.46	45.49	10.96
+75	55.06	45.63	9.43
2+05 = M.H. 20	54.68	45.75	8.93
0+35	55.81	45.89	9.92
+70	58.08	46.03	12.05
1+05 - T.P.	60.76	46.17	14.59

461.92 = 2" pipe Tooley + Paradise = Pole - 463.55
sw

69

1+40	62.63	46.31	16.32
+75	63.99	46.45	17.54
2+03.62 = M.H. 21	63.16	46.56	16.60
0+35	63.34 46.56 C 16.78	46.83	C 15.13
+70	60.79	46.84	C 13.95
1+05	59.54	46.98	C 12.56
+40	58.48	47.12	C 11.36
+75	55.35	47.26	C 8.09
1 80° = 48' 4t.		52.37	52.70
+95.20 = M.H. 22 BK	52.37	47.34	47.35 = 0+05
= 2+00.20 Ahead = 0+00		C 5.03	C 5.35 Ahead
0+35	54.61	47.48	C 7.13
+70	54.50	47.62	C 6.88
1+05	55.37	47.76	C 7.61
+40	56.45	47.90	C 8.53
+75	56.92	48.04	C 8.88
2+12.13 = M.H. 23	57.16	48.19	C 8.97
0+30	56.92	48.31	C 8.61
+60	56.54	48.43	C 8.11
+90	56.42	48.55	C 7.87
1+20 = Plug	55.32	48.67	C 6.65

Swan - St. - Tooley - North

0+00 = MH. 19	44.93		
+35	58.41	45.07	13.34
+70	58.26	45.21	13.05
+05	57.33	45.35	11.98
+40	55.85	45.49	10.36
+75	53.59	45.63	7.96
2+00 = plug.	49.93	45.73	4.20

Paradise St. South of Tooley

70

B.M. = Pole Tooley & Paradise
(page 69) EL = 463.555/7/55
GHS.

st. - lbs. 7' RT.

0+00 = MH. 21	63.18	63.19 46.56	C 16.62
0+25	62.47	62.47 46.70	C 15.77
0+70	61.68	61.68 46.84	C 14.84
1+05	61.14	61.14 46.98	C 14.16
1+40	60.69	60.69 47.12	C 13.51
1+75	60.02	60.02 47.26	C 12.76
2+10	59.55	59.55 47.40	C 12.15
2+23 = MH. 2A	59.28	59.28 47.45	C 11.83
0+35	58.50	58.50 47.59	C 10.91
0+70	57.88	57.88 47.73	C 10.15
1+05	56.77	56.77 47.87	C 8.92
1+27	55.93	55.93 47.96	C 7.97

Oxide St. Tooloy south

0+00= M.H. #17		36.60	
0+50 P.V.C.	48.64	48.64 41.92	C-6.72
0+70	51.88	51.88 43.92	C-7.96
0+90	54.93	54.93 45.76	C-9.17
1+10	57.66	57.66 47.13	C-10.53
1+30	59.47	59.47 48.35	C-11.12
1+50	60.73	60.73 49.30	C-11.43
1+70 E.V.C. M.H. #25	61.53	61.53 50.00	C-11.53
2+05	62.24	62.24 50.14	C-12.10
2+40	62.54	62.54 50.28	C-12.26
2+75	62.80	62.80 50.42	C-12.38
3+10	62.57	62.57 50.56	C-12.01
3+45	61.70	61.70 50.70	C-11.00
3+70 plug	59.77	59.77 50.80	C-8.97

Stake Curbs - Dwight St. - Nile - East.
 W.O. 31572 - 6-28-55 7-0.

Plan - 11504 - L

on Ret.
 Meet Exist. cb.

N
 stake
 17.10

S.

16.44

E.L. Nile on 42' Rad. 16.56 17.09^{0.53} F 0.52 16.09 16.50^{0.09} F 0.41

PC. = 0+14.65 16.55 17.12^{0.55} F 0.57 15.95 16.62^{0.67} F 0.67

0+40 17.05 17.33^{0.28} F 0.28 16.36 16.83^{0.47} F 0.47

+70 17.57 17.58 F 0.01 16.79 17.08^{0.29} F 0.29

1+00 18.21 17.83^{0.38} C 0.38 17.20 17.33^{0.13} F 0.13

+20 17.86 17.58^{0.28} C 0.28 17.15 17.62^{0.47} F 0.47

+36 = 4' Rad. 16.97 16.72^{0.25} C 0.25 17.11 16.20^{0.91} C 0.91

To Alley 16.97 16.58^{0.39} C 0.39 17.11 16.28^{0.83} C 0.83

End at PL. 17.14 16.90^{0.24} C 0.24 16.44 16.40^{0.04} C 0.04

1+60 = E.L. of 20' Alley 15.65 16.65^{1.00} F 1.00 - End. at Prop. 17.16 16.16^{1.01} C 1.01

20' = cb. line Prod. 14.47 16.25^{1.78} F 1.78 3' West. 14.74 15.75^{1.01} F 1.01

± 14.81 16.00^{1.19} F 1.19

End of Drain - N 13.53 14.95^{1.42} F 1.42 + Grade - S. 13.68 14.95^{1.27} F 1.27

2' bk of Cor. on Line 13.53

Stake Sewer in Winnett St. from
Federal Blvd. to 12" Trunk to N.

Plan - 5401-B - W.O. 21262 - 7-28-55 7.0.

B.M. = spike in Pole - P 65 277.10

Stakes - 5' Rt.

0+00 = M.H. 1 - 63' from M.H. 21 on 12" UC.

0+00	69.90	^{9.90} 263.00	66.90
+35	69.12	^{9.12} 63.54	5.58
+70	71.36	^{21.36} 64.08	7.28
1+05	71.56	^{21.56} 64.62	6.94
+40	72.04	^{22.04} 65.16	6.88
+64.10 = M.H. 2	72.75	^{72.75} 65.53	7.22
0+20.10	72.88	^{72.88} 66.20	6.68
+30.010	73.07	^{73.07} 66.80	6.27
+40	73.01	^{73.01} 67.40	5.61
+60 = Conn.	73.80	^{73.80} 69.01	4.79

Stake 24" Drain + Inlet. Alley Blk 4
Carmel Hts. - Plan - 11899-L - 8-29-55
W.O. 32337 . 70.

74

± Inlet - 5' Rt.	68.64	$\begin{matrix} 8.64 \\ 63.09 \end{matrix}$	C 5.55
Top	68.64	$\begin{matrix} 70.71 \\ 8.64 \end{matrix}$	F 2.07

± end - Conn. - 5' Rt.	71.37	$\begin{matrix} 71.37 \\ 61.83 \end{matrix}$	C 9.54
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Stakes for Laterals

① = 0 + 35' 35"	70.54	$\begin{matrix} 70.54 \\ 67.70 \end{matrix}$	C 2.84
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② 0 + 65' 35"	69.23	$\begin{matrix} 9.23 \\ 66.30 \end{matrix}$	C 2.93
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③ 1 + 05' 35"	74.58	$\begin{matrix} 4.58 \\ 70.10 \end{matrix}$	C 4.48
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④ 1 + 50' 35"	80.06	$\begin{matrix} 80.06 \\ 74.90 \end{matrix}$	C 5.26
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Stake Alley - Blk 4 - Carmel Hts.
 Plan-11899- L - 10-17-55 70.

75

		West			2' Blk - unless Noted	East		
0+00 = S.L. Palm		06.49				06.45		
0+20 0.55' Blk.	07.72	06.82	C 0.90		07.72	06.79	C 0.93	
+40	07.23	06.92	C 0.31		07.10	06.92	C 0.18	
+60	06.53	06.64	F 0.11		06.47	06.64	F 0.17	
+80 - 1.60' Blk.	07.05	05.95	C 1.10	0.73' Blk.	06.80	05.95	C 0.85	
1+20 1' Blk.	04.16	04.15	C 0.01	0.70' Blk.	05.69	04.15	C 1.54	
+60 1' Blk.	02.11	02.35	F 0.24	0.77' Blk.	03.76	02.35	C 1.41	
1+99 2+00 0.55' Blk.	01.21	00.60	C 0.61	1.35' Blk.	00.87	00.55	C 0.32	
+40 0.63' Blk.	99.40	98.75	C 0.65	1' Blk.	99.20	98.75	C 0.45	
+60	97.12	97.70	F 0.58	3' Blk.	97.72	97.70	C 0.02	
+80	95.98	96.36	F 0.38	3' Blk.	97.73	96.36	C 1.37	
3+00	94.57	94.73	F 0.16	1' Blk.	95.94	94.73	C 1.21	
+20	92.62	92.79	F 0.17		94.88	92.79	C 2.09	
+60	89.09	88.64	C 0.45	0.23' Blk.	89.85	88.64	C 1.21	
4+00	84.94	84.48	C 0.50		85.30	84.48	C 0.82	
+40	80.40	80.32	C 0.08		81.93	80.32	C 1.61	
+80 - 2' Blk.	76.12	76.16	F 0.22	2' Blk.	77.74	76.16	C 1.58	
5+20 - 5' Blk.	70.09	72.00	F 1.91	5' Blk.	71.81	72.00	F 0.19	
+25	69.59	71.56	F 1.97		71.23	71.55	F 0.32	

West.

5+35	⁷⁷ 69.33	71.12	F 1.35
+45	⁷⁰¹² 69.97	71.30	F 1.79
+55	³³ 70.36	72.08	F 1.18
+65	⁷⁰⁸⁴ 70.76	72.47	F 1.33
+70	71.73	74.40	F 1.75
+85 s'bk	74.81	77.40	F 1.72
+95.70 = NL. Not met	79.43	79.40	F 2.68
0-07	82.15	80.70	F 2.71
0-11.8 = end cb.	81.95	81.93	F 2.67
0-14	81.89	81.80	F 2.67
0-19.8 = P.C.	81.86	81.77	F 2.67
To st. = Meet			
0-21.8 = cb.	81.90		
gut	80.90		

East.

S' Bk.	70.14	71.07	F 0.93
	70.83	71.15	F 1.12
	71.35	71.79	F 0.44
	71.55	73.28	F 1.73
	71.70	74.20	F 2.50
S' Bk	74.95	77.08	F 2.13
	79.48	79.00	C 0.48
	80.17	80.17	C 0.47
= Top cb.	80.20	80.69	F 0.49
= gut.	80.14	79.90	C 0.24
	80.27	80.53	F 0.26
Meet		80.35	
		79.67	

Stake Wall - Alley Blk. 4 - at Nutmeg
Plan - 5840 - B - W.O. 32339 - 11-2-55 7.0.

0+00 = N.L. of Nutmeg. ^{wall} Grade of Top of.

Stake 5 To Back of wall

0+05.37 = Beg. Wall 77.86 78.60 F 0.74
7.86

+10.47 74.96 77.58 F 2.62
4.96

+15.37 74.70 76.62 F 1.92
4.90

+20.37 71.84 75.66 F 3.82
1.84

+25.54 71.71 74.70 F 2.99
1.71

+30.50 71.56 73.78 F 2.22
1.56

+35.37 71.57 72.97 F 1.40
1.57

+40.54 71.36 72.29 F 0.93
1.36

+45.37 = end wall 71.35 71.93 F 0.58
35

Stake Sewer for Girl Scout Bldg.
Plan - 12711-L - w.o. 21433 - 1-25-56

in Balboa Park
7.0.

78

BM. 280.51 = \square in cb. w. of Dr.	to Bldg.	
0+00 = Exist. M.H.	78.70	73.27 5.43
+35	78.92	73.41 5.51
+73.35 = M.H. 1	79.17	73.56 5.61
⁼⁰⁺⁰⁰ +35	78.83	73.70 5.13
+70	78.66	73.84 4.82
1+05	78.82	73.98 4.84
+40	79.10	74.12 4.98
+75	79.30	74.26 5.04
2+10	80.20	74.40 5.80
+45	80.76	74.54 6.22
+80	80.12	74.68 5.44
3+02.40 = M.H. 2	79.66	74.77 4.89
⁰⁺⁰⁰ +35	79.57	74.91 4.66
+70	79.64	75.05 4.59
1+05	80.03	75.19 4.84
+40	80.29	75.33 4.96
+75	80.49	75.47 5.02
2+10	81.31	75.61 5.70
+55.52 = M.H. 3	81.99	75.79 6.20
= end.		

Stake Alley Blk. 151 - Pac. Beach
 Plan - 12053-L w.o. 31660 - 2-2-56 70.
 South

0+00		55.21	
+20 - 0.50 B.	55.60	⁶⁰ 55.50	C 0.10
+40 0.50 B.	55.61	55.60	C 0.01
+60 0.04 B.	55.84	⁸⁶ 55.40	C 0.46
+80	54.72	55.20	F 0.48
1+00	55.16	^{4 72} _{5 16} 54.80	C 0.36
+20	53.95	^{3 75} 54.40	F 0.45
+40	53.90	53.90	G
+60	53.46	⁴⁶ 53.60	F 0.14
+80 - 0.70 B.	53.04	⁰⁴ 53.20	F 0.16
2+00 - 1.00 B.	52.48	⁴⁸ 52.80	F 0.32
+30	50.85	^{0 85} 51.97	F 1.12
+60	50.50	^{0 50} 51.05	F 0.55
+80	50.39	³⁹ 50.66	F 0.27
+85	50.36	³⁶ 50.58	F 0.22

0+55 = Sewer Lat. # 1 on N.

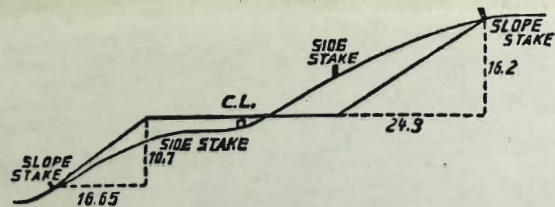
BM = 56.62 = Pole - U. Side 0-18 79
 B.M. 53.35 = Pole - N. 2+80
 North

		55.49	
		⁹⁸ 55.80	C 0.18
		^{6 25} 56.25	C 0.35
		⁹³ 55.93	C 0.18
		⁷⁵ 55.75	C 0.20
		⁶³ 55.63	C 0.43
0.21 B.		55.52	^{5 52} 54.71
0.20 B.		55.49	54.23
0.21 B.		54.09	^{4 08} 53.75
		54.28	^{4 28} 53.27
0.38 B.		53.98	^{3 98} 52.79
0.62 B.		53.66	^{3 66} 52.97
0.27 in		53.01	^{3 01} 51.35
Line		52.10	^{2 10} 50.96
		52.09	^{2 09} 50.88

Cor. Ends of Apron

0+29	56.06	^{6 06} 55.21	C 0.85
0+96.5	55.44	^{5 44} 54.41	C 1.03
I.E.		49.90	

20 Rad.
 $A = 91^{\circ} 26'$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE $1\frac{1}{2}$ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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