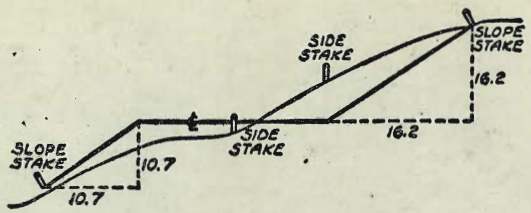


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

IMPROVED TABLES
AND
INFORMATION

Index

Page	
2-7	Manzanita
8-11	Snowdrop
12-14	Sycamore East of Snowdrop
15-	Snowdrop - Storm Drain
16-18	Poppy Place
19-23	Poppy Place + Manzanita curb Returns
24	Manzanita Storm Drain
25	" Prop Ties
26-32	Tuberose
33-36	Violet Grds Sly end to Sycamore. + Storm Drain
37-45	Sycamore
46	Tulip
47-50	Shamrock
51-56	Pepper Drive
57-62	Violet (Sycamore to Poplar)
63	Sears Hgts. {Cervantes St.} Sewer Lab
64	Tecolote Road - curb stakes
65	Tulip + Trailing - Gutter grades
66	Ch. Ref. West Ft. Loma Blvd + Muir

Page

Page	
67	Pump Station A. Witherby & Hancock Sts.
68	Kendall St. & Malden - Sewer
69	Alley Blk 113 - Pac. Beach
70	" " 262 " "
72	" " 80 " "
73	Everts St & Grand - Curb.
74	Lot stakes Lot 14 ~~in~~ Villa Tract. La Jolla
75	South Lane - La Jolla
78	Alley East of Blk A. South La Jolla

Manzanita

	1+72.5 PC →	283.40	3.48 283.40 C 0.08	4.03 284.00 C 0.03	
1+89.20 = E.C. Def 48°-06'-08		Line 4.08 283.19 C 0.89	3.47 283.19 C 0.28	3.68 283.80 F 0.12	4.56 Line 283.80 C 0.76
1+72.50	Ch. = 33.08				
1+56.00 = P.R.C. on Lt.	Def. 39°-39'-40" ch 26.15	3.85 283.60 C 0.25	3.71 283.60 C 0.11	4.17 284.20 C 0.17	5.33 284.20 C 1.13
1+29.79	Def 32°-59'-50 ch 26.15	—	See page 19	4.64 284.49 C 0.15	5.19 284.49 C 1.00
1+03.58 3 pts	Def. = 26°-20' Ch. 26.15	30.49 3 ch. Lt.		4.74 284.78 F 0.04	5.47 284.78 C 0.69
0+77.37 = P.R.C. on Lt.	Def 19°-40'-10" Ch. 14.94.	4.60 285.40 F 0.80	285.30 285.40 C 0.38	5.03 285.06 F 0.03	6.00 285.06 C 0.94
0+62.42 2 pts	Ch. 14.94 Def 15°-52'-10" (91.68 Rad Ch = 12.17)	5.40 285.82 F 0.42	6.09 285.82 C 0.27	5.49 285.40 C 0.09	6.51 285.40 C 1.11
0+47.48 P.R.C. on Lt.	Def. 12°-04'-10" (134.68 Rad Ch. = 11.85)	5.92 286.25 F 0.33	6.34 286.25 C 0.09	285.75	6.91 285.75 C 1.16
0+00 = N/y Violet = start Job.		286.94	286.94	286.46	286.46

Manzanita

3+30.26		281.42	~~8~~	2.00 82.02 F0.02	282.02
3+25.45	Prop. Nly line alley at		2.29 281.65 C0.64	—	—
3+23.01	Alley B.C. Lt.		1.90 281.52 C0.38	—	—
3+18.48 = ℄ E.C. dlf 41°-08'-30" Ch.=8.21		(3) 4.31 281.63 C 2.68	1.98 81.63 C0.35	2.00 82.22 F0.22	2.77 282.22 C0.55
3+10.26 = P.C.C. 35°-54.33' ch 18.66		(3) 4.28 281.72 C 2.56	2.16 81.72 C0.44	1.78 82.33 F0.55	3.24 282.33 C0.91
2+91.45	23°-56.22' ch. 18.66	4.50 281.95 C 2.55	1.77 81.95 F0.18	2.54 82.56 F0.02	X-5 5.04 282.56 C 2.48
2+72.65 3 quarters	dlf. 11°-58' ch=18.66	4.61 282.18 C 2.43	1.65 ~~1.83~~ 82.18 Reset ~~F0.35~~ F0.53	3.05 82.79 C0.26	5.31 282.79 C2.52
2+53.85 = B.C. Lt.		4.53 282.40 C 2.13	2.14 82.40 F0.26	3.14 83.01 C0.13	5.17 283.01 C2.15
2+21.52		3' 4.99 282.80 C 2.19	2.98 82.80 C0.18	3.40 83.40 X	4.77 283.40 C1.37

Manzanita

4+73.09	Rt. only	—	—	6.46 76.19 C 0.27	Line 7.88 276.19 C 1.69
4+31.40 (GZ) =	B.C. Poppy on Lt.	(line) 80.14 277.79 C 2.35	7.60 77.79 F 0.19	—	—
4+30.26	E.V.C.	~~277.84~~	7.58 77.84 F 0.26	8.38 78.44 F 0.06	Line 9.45 278.44 C 1.04
4+10.26		Line 80.81 278.83 C 1.98	9.11 78.83 C 0.28	9.68 79.43 C 0.25	Line 80.23 279.43 C 0.80
3+90.26		Line 81.87 279.68 C 2.19	80.11 79.68 C 0.43	0.46 80.28 C 0.18	Line 1.10 280.28 C 0.82
3+70.26		Line 2.52 280.39 C 2.13	1.00 80.39 C 0.61	1.37 80.98 C 0.39	Line 2.24 280.98 C 1.26
3+50.26		(3) 3.3 280.97 C 2.3	1.21 80.97 C 0.24	1.75 81.57 C 0.18	2.3 281.57 C 0.7
3+42.14	E.C. Alley on Lt.	—	1.22 281.18 C 0.04	—	—
3+40.49	at. Prop. Sly line Alley on Lt.	3.45 81.35 C 2.10	1.99 281.35 C 0.64	—	—

Manzanita

6+95.37 = E.C.	9°-12'-30"		4.99 263.90 C 1.09	3.63 63.90 F 0.27	4.45 64.50 F 0.05	6.95 264.50 C 2.45
22.76						
6+72.61	7°-40'-25"		5.90 265.10 C 0.80	5.07 65.10 F 0.03	5.45 65.70 F 0.25	Line 8.46 265.70 C-2.76
22.77						
6+49.84	6°-08'-20"		6.33 266.30 F 0.97	6.00 66.30 F 0.30	6.52 66.90 F 0.38	9.26 266.90 C-2.46
22.77						
6+27.07	4°-36'-15"		5.64 267.50 F 1.86	7.40 67.50 F 0.10	7.76 68.10 F 0.34	0.25 268.10 C 2.15
22.77						
6+04.30	dlt 3°-04'-10"		9.20 268.70 C 0.50	8.46 68.70 F 0.24	9.43 69.30 C 0.13	1.87 269.30 C 1.77
22.77						
5+81.53	Dlt. 10°-32'-05"		7.49 269.90 C-1.59	9.87 69.90 F 0.03	0.33 70.50 F 0.17	Line 12.53 270.50 C 2.03
22.77						
5+58.76 = B.C.			2.02 270.11 C 0.91	1.05 71.11 F 0.06	1.79 71.71 C 0.08	Line 3.41 271.71 C 1.70
5+42.77 = Wly 40th. on Lt. only			12.65 271.82 C 0.83	1.94 71.82 C 0.12	—	—
5+15.93	Rt. only		—	—	4.20 73.95 C 0.25	Line 6.06 273.95 C-2.11
4+98.21 Cl. E.C. on left			3.64 274.51 C 1.13			—

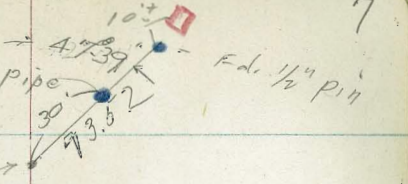
6 - Pts
Ch = 22.77

	Manzanita					
9+24.64=	Ctr. Barrio	See Page 7				
				See barrio Resel		
8+92.70	ob. B.C.		0.54 251.20 F 0.66	~~1.30~~ ~~51.20~~ ~~Cp.10~~	1.12 51.20 F 0.08	(D) 1.16 251.20 F 0.04
8+61.47			(E) 3.30 253.54 F 0.24	2.55 (?) 53.54 F 0.99	3.78 53.73 C 0.05	4.38 253.73 C 0.65
8+30.24	E.V.C.		6.04 255.89 C 0.15	5.78 55.89 F 0.11	6.01 56.26 F 0.25	(D) 5.94 256.26 F 0.32
8+10.24			8.08 257.35 C 0.73	7.35 57.35 X	8.05 57.81 C 0.24	(E) 9.44 257.81 C 1.63
7+90.24			60 00 258.69 C 1.31	8.69 58.69 X	9.43 59.22 C 0.21	10.44 259.22 C 1.22
7+70.24			61.56 259.91 C 1.65	9.75 59.91 F 0.10	0.67 60.48 C 0.19	2.20 260.48 C 1.82
7+50.24	P.V.C.		3.78 261.01 C 2.77	1.25 61.01 C 0.24	1.61 61.61 X	3.88 261.61 C 2.27

Manzanita Banjo

Sta 0+00 = P.R.C. on Right (North)

Tie to Prop. Pin.



249.51 = Top. Face Ctr. of Banj.

	Rough Gr.	ol.
(1/2) 1st #7	9.33 248.70 C 0.63	9.35 248.70 5/18 C 0.65
Δ 11°-54'-30"		
#6	~~248.65~~	9.05 248.65 C 0.40
Δ 19°-26'		
#5	~~248.50~~	
Δ 11°-15'		
#4	9.08 248.60 C 0.48	8.68 #3 248.60 in Ord.
Δ 19°-26'		
#3	~~248.80~~	50.07 #2 248.80 C 1.27
Δ 16°-42'		
(1/4) #2	50.93 249.10 C 1.83	50.93 1/4 249.10 1.83
Δ 34°-47'		
Sta 0+00 = #1	0.66 250.00 C 0.66	1.07 #1 250.00 C 1.07

Rock Lake

	Rough Gr.	ol.
		0.93 251.20 F 0.37 ← Reset 3-15-55
P.C. on south		
#12 = P.R.C.	D 0.21 250.30 F 0.09	0.25 250.30 F 0.05
Δ 34°-47'		
#11 (3/4)	X line 9.77 249.70 C 0.07	9.78 249.70 C 0.08
Δ 22°-30'-30"		
#10	249.40	9.58 249.40 C 0.18
Δ 22°-29'-30"		
#9	9.55 249.10 C 0.45	9.57 249.10 C 0.47
Δ 22°-29'-30"		
#8	~~248.90~~	9.54 248.90 C 0.64
Δ 22°-30'-30"	248.10	

Snowdrop. 2/14/58

Sycamore Dr. – To Sly. end

Sheet # 11

1+37 E.V.C. Lt. lowered 0.15 to take out a bad break	4.39 274.10 C 0.29	3.51 274.10 ~~F 0.59~~ F 0.44	3.75 274.10 F 0.35	4.18 274.10 C 0.08
1+17	5.87 275.25 C 0.62	5.11 275.25 F 0.14	4.66 275.25 F 0.59	4.77 275.25 F 0.48
0+97	7.61 276.30 C 1.31	6.34 276.30 C 0.04	6.27 276.13 C 0.14	6.21 276.13 C. 08
0+77	8.90 277.15 C 1.75	6.73 277.15 F 0.42	6.60 276.85 F 0.25	6.84 276.85 F 0.01
0+57 = ℄ E.C. on Lt.	9.75 277.95 C 1.80	7.50 277.88 F 0.38	7.25 277.45 F 0.20	7.68 277.45 C 0.23
0+37 Rt. only			8.04 278.15 F 0.11	8.06 278.15 F 0.09
0+17 Rt. only			278.65 V	278.65
0+00 = N. Ely. cor. + Snowdrop. Sycamore Dr.				

Snowdrop.

(11)

9

2+49.30 = cl. B.C. Lt. + Rt.	5.63 263.95 C 1.68	4.00 263.95 C 0.05	4.21 263.95 C 0.26	2.96 263.95 F 0.99
2+44.63	5.76 264.30 C 1.46	4.30 264.30 X	4.50 264.30 C 0.20	3.26 264.30 F 1.04
2+24.63	6.70 265.70 C 1.00	5.70 265.70 X	5.49 265.70 F 0.21	4.72 265.70 F 0.98
2+04.63 P.O.C.	9.73 267.50 C 2.23	7.54 267.50 C 0.04	7.53 267.50 C 0.03	6.22 267.50 F 1.28
1+71.1	270.80	0.42 270.80 F 0.38	1.73 270.80 C 0.93	270.80

Rough Gr.

Banjo - End of Snowdrop

Rough

For Rough Gr.

curb.

#7		
#6	℄ Banjo	
#5		
#4		
#3		
#2		
#1		
0 P.R.C. on Rt.		

#3	1.37 262.15 F 0.82	
#4	1.26 262.00 F 0.74	1.19 262.00 F 0.81
#5	0.85 261.85 F 1.00	0.92 261.85 F 0.93
		0.55 261.90 F 1.35
#6	0.51 262.40 F 1.89	0.44 262.40 F 1.96
wly. P.R.C.	3.61 263.15 C 0.46	2.01 263.15 F 1.14

#11 = P.R.C. on Left

#10 = P.R.C. on Lt.

#9

#8

	Curb	Rough
Ely	3,97	5,18
P.R.C.	263.20	263.20
	C 0.77	C 1,98
#1	2.92	2.91
	262.75	262.75
	C 0.17	C 0,16
#2	1.66	1.90
	262.35	262.35
	F 0.69	F 0,45

Sycamore sheet #10

East of Snowdrop.

1+56				
1+56 07	5' 80.90 279.90 C 1.00	9.70 279.90 F 0.20	9.36 279.40 F 0.04	5' 7.55 279.40 F 1.85
1+36 07	—	9.45 279.79 F 0.34	9.15 279.29 F 0.14	—
1+16 07 = P.V.C.	Line 81.65 279.71 C 1.94	9.67 279.71 F 0.04	9.29 279.21 C 0.08	5' 8.45 279.21 F 0.76
0+68 36	Line 82.46 279.57 C 2.89	9.64 279.57 C 0.07	9.48 279.07 C 0.41	5' 9.90 279.07 C 0.83
0+20 65 = Cl. E.C. on Lt.	Line 81.93 279.42 C 2.51	8.95 279.42 F 0.53	8.96 278.92 C 0.04	5' 9.70 278.92 C 0.78
0+06 45 = Cl. E.C. on Rt	—		8.59 278.65 F 0.06	5' 9.88 278.65 C 1.23
0+00 = Elg. line Snowdrop on right.			8.55 278.35 C 0.20	Mid. Point return

Sycamore (10)

Also = end prop. on Rt.

4+42.16 = End el. on Rt.	5' 4.46 283.20 C 1.26	3.00 283.20 F 0.20	1.97 282.70 F 0.73	5' 80.50 282.70 F 2.20
4+00 95	5' 4.62 282.68 C 1.94	2.66 282.68 F 0.02	2.09 282.18 F 0.09	5' 2.51 282.18 C 0.33
3+59 73	1' 4.45 282.17 C 2.28	1.97 282.17 F 0.20	1.86 281.67 C 0.19	5' 2.90 281.67 C 1.23
3+18.51 5 x 41.22	5' 3.57 281.66 C-1.91	1.70 281.66 C 0.04	1.52 281.16 C 0.36	Line 2.91 281.16 C 1.75
2+77 29	5' 2.05 281.15 C 0.90	1.03 281.15 F 0.12	80.85 280.65 C 0.20	Line 2.02 280.65 C 1.37
2+36 07 = E.V.C.	5' 0.44 280.64 F 0.20	80 63 280.64 F 0.01	80.15 280.14 C 0.01	Line 0.35 280.14 C 0.21
2+16 07	—	80 10 280.41 F 0.01	9.80 279.91 F 0.11	—
1+96 07	5' 0.87 280.21 C 0.66	9 94 280.21 F 0.27	80.85 279.71 C 1.14	5' 8.17 279.71 F 1.54
1+76 07	—	9.87 280.04 F 0.17	9.46 279.54 F 0.08	—

Sycamore (10)

A+76 OT = End Prop. on Lt.	5' 3.97 283.62 C 0.35			—
A+71 = end sb. on Lt.	—	3.39 283.62 F 0.23		—

Snow drop. 2/15/55

Storm Drain sheet #11

Stakes 6' Lt. (East) of ℄

0+00 = inside wall of box. (1st back of ch. face.)

			17 ℄ ditch
1+25.50 (Face of head wall)	22.13 222.15 F-0.03		2.70 222.15 C 0.55
1+13.50	27.05 222.45 C-4.60		2.10 222.45 F 0.35
1+05.66	30.22 224.03 C-6.19		4.12 224.03 C 0.09
0+74.01	45.94 236.45 C-9.49		
0+42.36	57.97 248.86 C-9.11	3' Lt.	8.08 248.86 F 0.78
0+34.69	58.29 251.12 C-7.17		50.34 251.12 F 0.78
0+00	60.91 258.14 C-2.77		6.94 258.14 F 1.20

Poppy Place

Sheet #(3)

0+00 = E.C. S.Ely Rct. Manzanita & Poppy Place.

0+63.34 = Nly line Alley on Rt. (end alley ct.)		—	1.99 281.79 C 0.20	
0+61.34 = Alley B.C. on Rt.	—	—	1.16 281.59 F 0.43	—
0+58.99 = Alley E.C. on Lt.	—	9.92 281.19 F 1.27	—	—
0+56.99 = Sly Line alley on Lt. (end ~~Ct.~~ alley ct.)	—	0.97 281.45 F 0.48	—	—
0+40.14 = Nly. line alley on Lt. (also = end alley ct.)	81.06 (1) 281.76 F 0.70	1.62 281.76 F 0.14	—	82.73 282.35 C 0.38
0+33.81 = Alley B.C. on Lt.	—	0.96 281.87 F 0.91	—	—
0+14.34 = E.C. From Manzanita on Rt.	2.69 282.60 C 0.09	1.71 282.60 F 0.89	2.30 283.30 F 1.00	3.53 283.30 C 0.23
0+00 = E.C. From Manzanita on Lt.	3.20 (2) 283.20 X	2.31 283.20 F 0.89	—	

Poppy + (3) &

2+25.37	Δ 83°-26'		6.82 277.65 F 0.83	7.25 277.65 F 0.40	7.11 277.77 F 0.66	80.25 277.77 C 2.48
1+99.58	Δ 50°-56'		7.91 277.79 C 0.12	7.84 277.79 C 0.05	7.88 277.86 C 0.02	80.03 277.86 2.17
1+79.58	Δ 25°-28'		9.00 277.86 C 1.14	7.80 277.86 F 0.06	7.27 278.01 F 0.74	80.15 278.01 C 2.14
1+59.58 =	B.C.	El. Rad. ½ = 280.93	9.14 278.02 C 1.12	7.28 278.02 F 0.74	7.70 278.33 F 0.63	80.33 278.33 C 2.00
1+39.58			8.04 278.36 F 0.32	7.53 278.36 F 0.83	8.35 278.81 F 0.46	80.8± 278.81 C 2.0
1+19.58	P.U.C.		8.58 278.87 F 0.29	8.40 278.87 F 0.47	7.06 279.46 F 0.40	81.20 279.46 C 1.74
0+99.58			79.51 279.57 F 0.06	8.85 279.57 F 0.72	—	—
0+86.46 = Alley E.C. on RX			—	—	0.22 280.67 F 0.45	—
0+80.12 =	end alley at Sly line Alley on RX.		80.47 80.29 C 0.18	—	1.74 280.87 C 0.87	① 81.52 280.87 C 0.65

Poppy (#3)

Maozanita

4+26.91 = ob. B.C. on Lt	5.64 275.40 C 0.24	page 23 6.39 275.40 C 0.99	—	—
4+23.27 = ob. B.C. on Rt.	275.60	6.13 275.60 C 0.53	6.65 277.10 F 0.55	9.83 277.10 C 2.73
.07				
4+03.27	6.05 276.35 F 0.30	5.88 276.35 F 0.47	6.55 277.17 F 0.62	(L) 9.36 277.17 C 2.19
.07				
3+83.27	6.43 276.80 F 0.43	6.10 276.80 F 0.70	6.58 277.24 F 0.66	(L) 9.14 277.24 C 1.90
.15				
3+39.23	6.85 277.04 F 0.19	6.44 277.04 F 0.60	6.61 277.39 F 0.78	(L) 9.64 277.39 C 2.25
.15				
2+95.20	5.25 277.28 F 2.03	7.50 277.28 C 0.22	7.22 277.54 F 0.32	(L) 9.98 277.54 C 2.44
.15				
2+51.17 = E.C. Δ 116°-37'	(L) 6.86 277.51 F 0.65	6.83 277.51 F 0.68	7.08 277.69 F 0.61	80.33 277.69 C 2.64

Curb Returns Manzanita

sheet #3

Ely. ch. Rot. at Nly end of Poppy

0+00 = (0+77.31 Manzanita)

= E.C. Poppy

= 0+00 Page 16

0+55.33 = E.C.	#6		23°-59'-30"	2.31 283.20 F 0.89	
0+44.26 =	#5		19°-11'-36"	2.55 283.60 F 1.05	
0+33.20	#4		14°-23'-42"	3.10 284.10 F 1.00	
0+22.13	#3		9°-35'-48"	3.69 284.50 F 0.81	
0+11.07	#2	Def	4°-47'-54"	5.30 284.90 C 0.40	
P.R.C. = 0+00 =	#1			5.68 285.30 C 0.38	
0+77.31 P-2 = Manzanita					

Δ = 47°-59' 5 parts on ch. 3 back of ch. stakes

Station ing

ch. Rad = 66.09'

Rad = 63.09 - ch = 10.52

Manzanita + Poppy — Nly. end.
Curb return — sheet #3

Wly. Rot. Nly. end of Poppy Place
ch. Rad = 29.90

P.R.C. Manzanita

℄ 0+49.03 #5 = P.R.C. Manzanita df 46°-01' 3.71 / 283.60 / C 0.11

℄ 0+36.80 #4 df 35°-15'-30" 3.81 / 283.70 / C 0.11

℄ 0+25.58 #3 df = 24°-30'-30" 4.25 / 283.70 / C 0.55

Equal pts.

For Rad. = 26.90 — ch. = 10.04

℄ 0+14.35 #2 Def. = 13°-45' 3.42 / 283.60 / F 0.18

ch. 26.90 R = 12.79

℄ 0+00 = #1 2.30 / 283.30 / F 1.00

0+00 = B.C. Poppy Place

(Sta 0+14.34 - Page 16)

Nly. cl. Rot - Manzanita

Wly. end of Poppy.

0+00 = B.C. on Manzanita =

= Sta. A+31.62 Page A.

Δ - 85°-52' Turned.

A - Parts (Set off. Radius point)

⑧ +30.00 = #5 - E.C. on Poppy	Δ 85°-52'	6.65 277.10 F 0.55
#4	Δ = 64°-24'	6.78 277.10 F 0.32
#3	Δ 42°-56'	7.28 277.20 C 0.08
#2	Δ 21°-28'	7.32 277.40 F 0.08
0+00 = #1 B.C. on Manzanita Manzanita		7.60 277.79 F 0.19

S/y. Cl. Rot. Manzanita

W/y end of Poppy Place.

0+00 = B.C. Poppy. Poppy place
Sta 4+26.91 – page 18

Set off radius point.

Δ = 94°-08' ✓ Turned. (Sta. 4+93.21 P-5)

0+19.70 = # = E.C. Manzanita

0+06.9 = #1 Δ = 28°-40'-28"

0+00 = #1 B.C. Poppy.

4.38
274.51
F 0.13

4.88
275.12
F 0.24

6.39
275.40
C 0.99

Storm Drain Wly. end Manzanita

2/23/15
Sheet #2
" #9

0+00 = Face of curb.

stakes 9' Lt. of ℄
1+26.00
1+15.00 } = ℄ R.P.'s

1+03.74 = end Pipe

0+95.83

0+91.95

0+88.29.

0+63.76

0+60.56

0+53.12

0+01.5
start pipe
= inside of box.

	Stakes 9' Lt. of ℄	℄ stakes
	6.30 1.89 8.19	
4 cuts	6.30 216.65 ~~F 0.35~~ C 1.54	6.12 216.65 F 0.53
4 cuts	19.92 217.88 C ~~2.04~~ C 3.93	7.50 7.88 F 0.38
1.89 to	21.55 218.83 C ~~2.72~~ C 4.61	8.50 8.83 F 0.33
	3.58 220.44 C ~~3.14~~ C 5.03	19.80 20.44 F 0.64
bench add	236.51 233.93 C ~~2.58~~ C 4.47	
	8.05 235.34 C ~~2.71~~ C 4.60	
Wrong	40.64 237.17 C ~~3.47~~ C 5.36	
	247.39 245.20 C ~~2.19~~ C 4.08	

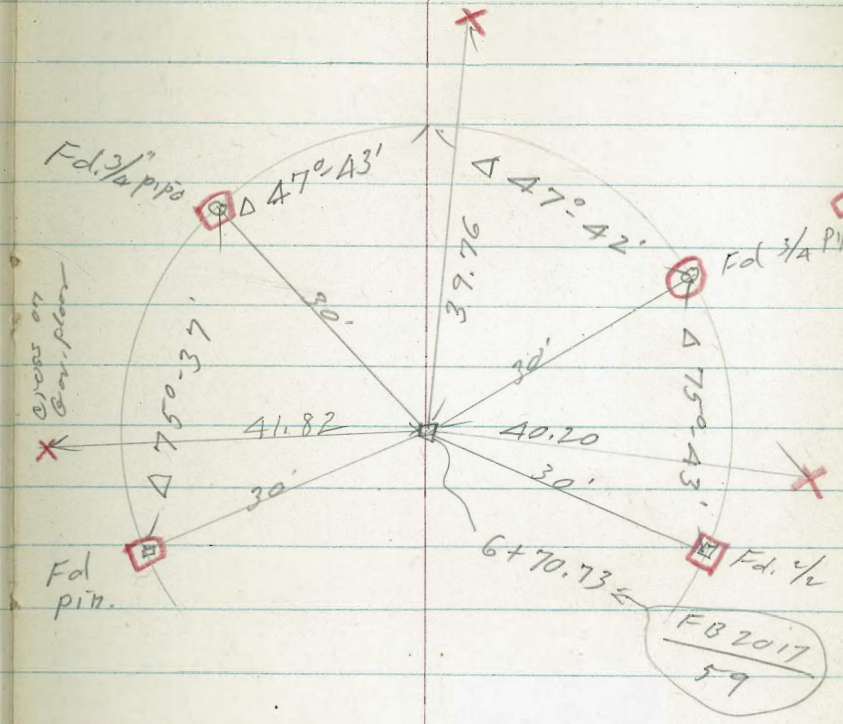
Prop pipes fd. at Wly. end Manzanita

X = cross cut into drive

□ = set ½" dist - 4/24/55

○ = Reset pipe (also cross on conc. under pipe) 4/24/55

℄ Produced.



Tuberose. 2/25/53

Poplar to Sly. End.

	→	—		—
#1 1+54.04 dip 3°-14'-15" (℄ ch. 14.03)		—	5.48 285.23 C0.25	4.77 284.93 F0.16 —
~~Alloy ch. E.C. on Lt.~~		—		
1+44 Alloy ch. E.C.		—	5.58 285.41 C0.17	5.45 285.03 C0.42 —
=℄ B.C.				
1+40= Sly. Alloy also start ch.		6.76 285.41 C1.35	6.67 285.56 C1.11	5.72 285.18 C0.54 5.94 285.03 C0.91
1+25= Nly. alloy also end ℄ ch.		6.62 285.54 C1.08	6.34 285.69 C0.65	6.17 285.43 C0.74 6.08 285.18 C0.90
1+21 = alloy ch. B.C.		—	5.41 285.54 F0.13	5.14 285.18 C0.26 —
	→		6.00	5.93
0+82 + 0+87 on Rt.		6.70 286.17 C0.53	285.96 C0.04	285.64 C0.29 6.54 6.13 285.89
0+43 Lt + 0+48 on Rt.			6.20 286.38 F0.18	286.10 C0.03 C0.65
0+05 = ch. E.C.	→	286.80	286.80	286.60 286.60
0+00 = Sly. line Poplar.				

Tuberose

	= Cl. B. C. on	Rt. To Pepper Dr.	—	—	3.55 283.43 C 0.12	(L) 3.4 283.43 X
#2 2+67.72	2°-29'-15	↑	3.18 284.07 F 0.89	4.18 284.07 C 0.11	3.57 283.69 F 0.12	(L) 3.38 283.69 F 0.31
#1 2+45.98	dfl. = 1°-14'-37½"	℄ Ch. = 21.71	—	4.48 284.21 C 0.27	3.97 283.92 C 0.05	—
#6 P.R.C. 2+24.24	19°-25'-30.	℄ Ch. = 14.03	4.70 (D) 284.34 C 0.36	4.54 284.34 C 0.20	3.91 284.15 F 0.24	(D) 4.05 284.15 F 0.10
#5 2+10.20	16°-11'-15"	↓	—	4.75 284.51 C 0.24	3.38 - ? 284.30 F 0.92	—
#4 1+96.16	12°-57'		6.01 (D) 284.70 C 1.31	4.96 284.70 C 0.26	4.26 284.45 F 0.19	(A) 4.95 284.44 C 0.51
#3 1+82.12	9°-42'-45		—	5.05 284.88 C 0.17	4.51 284.61 F 0.10	—
#2 = 1+68.08	6°-28'-30"		6.40 (L) 285.06 C 1.34	5.39 285.06 C 0.33	4.63 284.75 F 0.12	(A) 5.47 284.73 C 0.74

Tuberose

#8 = E.C. 3+98.18	9°-57' also Match line.	7.9.67 282.23 F 2.56	1.92 282.23 F 0.31	2.49 282.34 Co. 15	4.67 282.34 C 2.33
#7 3+76.42	8°-42'-22½"	—	1.40 282.49 F 1.09	2.80 282.56 Co. 24	—
← d. E.C. Here					
#6 3+54.68	7°-27'-45"	78.52 282.75 F 4.23	1.72 282.75 F 1.03	~~1.74~~ ~~282.77~~ ~~Co 1.03~~	4.24 282.79 C 1.45
= d. E.C. on RT. ?		—	~~283.02~~	3.73 282.71 C 1.02	282.71
3+40 = Sly Pepper Dr. produced				~~282.74~~	282.74
#5 3+32.94	6°-13'-07½"	283.28	2.88 283.28 F 0.40	~~283.01~~	283.01
#4 3+11.20	4°-58'-30"	2.77 283.55 F 0.78	3.44 283.55 F 0.11	~~283.24~~	3.57 283.24 Co. 33
#3 2+89.46	Left 3°-43'-5½"	—	3.98 283.81 Co. 17	~~283.46~~	283.46
2+83.60 = Nly. Pepper Dr. on RT.		—	~~284.07~~	—	~~283.39~~

Tuberosa

5+28 18		1.47 280.61 C 0.8C	0.55 280.61 F 0.0C	1.04 280.91 C 0.13	(L) 3.15 280.91 C-2.21
5+08 18		280.89	0.85 280.89 F 0.04	1.34 281.19 C 0.15	281.19
5+01 12 = E.C. Alloy Cb. on Rt.		—	—	1.72 281.30 C 0.42	—
4+97.15 = Sly line alloy on Rt.		—	—	3.70 281.47 C 2.23	(L)
4+88.18 ~~B+t~~ P.U.C.		2.58 281.14 C 1.44	2.49 281.14 C 1.35	~~2 8 1 4 1~~	4.3C 281.41 C-2.95
4+81.29 = Nly. line Alloy on Rt.		—	—	2.77 281.63 C 1.14	—
4+75.36 = alloy cl. B.C. on Rt.		—	—	2.04 281.44 C 0.60	—
4+43.18		(L) 2.91 281.68 C 1.29	1.65 281.68 F 0.03	2.00 281.87 C 0.13	(L) 4.53 281.87 C-2.66

Tuberose

7+03.03 Lt. only.	(E) 7.14 277.64 F 0.50	7.56 277.65 F0.09	—	—
6+93.38 = cl. E.C. on Rt.	—	—	8.00 277.94 C0.06	9.56 277.94 C 1.62
6+89.18 = Sly. line Sycamore Rt. only.	—	—	—	278.02
6+58.08 Lt. only.	7.37 278.42 F 1,05	8.42 278.42 grade.	—	—
6+29.31 = Nly. Sycamore on Rt. only	~~7.7~~	—	—	279.12
6+23.60 = cl. B.C. on Rt. (Sycamore Dr.)	—	—	7.28 279.23 C0.05	(D) 81.41 279.23 C 2.18
6+13.13 Lt. only. Lt. in 5 parts 44.95 Each	7.30 279.19 F 1.89	9.19 279.19 Grade	—	—
6+00 Rt. only			C0.09	↙ Raked
5+68.18 E.V.C.	81.13 279.97 C 1.16	80.02 279.97 C0.05	0.45 280.25 C0.20	(2) 2.38 280.25 C 2.13
5+48.18	—	0.15 280.30 F0.15	0.70 280.60 C0.10	—

Tuberose

Elev. N.w. ch. Rod = 277.95

N.W. Rot.

			#5 5.27	#6 5.43	4.75	7.20 End.
1.80 #2 274.90 F 3.10	3.01 #3 274.61 F 1.60	4.51 #4 274.36 C 0.15	274.10 C-1.17	274.00 C 1.43	274.25 C 0.50	274.25 C-2.95
			274.00	—	4.75 274.40 C 0.35	7.20 EC. 274.40 C-2.80
also: 5' East of Ctr. Banjo						Mid.
8+46.16 - Lt. only. = #1 of Banjo			2.31 275.19 F 2.88	—	5.00 274.85 C 0.15	7.45 274.85 C 2.60
See page 32 for Banjo						
7+92.91 - Brk. on Lt. ch. B.C. on Rt.			4.93 276.10 F 1.17	6.24 276.10 C 0.14	5.97 275.60 C 0.37	7.88 275.60 C 2.28
7+72.91 = Rt. only.			—	—	6.31 276.35 F 0.04	276.35
7+52.91 = Rt. only.			—	—	6.75 276.84 F 0.09	8.68 276.84 C 1.84
7+47.98 Lt. only			5.68 276.87 F 1.19	7.16 276.87 C 0.29	—	—
7+23.15 - Rt only			—	—	7.22 277.39 F 0.17	—

Banjo - End of Tuberose

#C = E.C. (5' Rad) also = end of cb.
4.85
274.00
C 0.185

#5 = P.R.C.
5.38
274.10
C 1.28

#4
4.23
274.36
F 0.13

#3 1/2 point
3.52
274.61
F 1.09

#2
3.13
274.90
F 1.77

#1 1/4 point
4.62
275.19
F 0.57

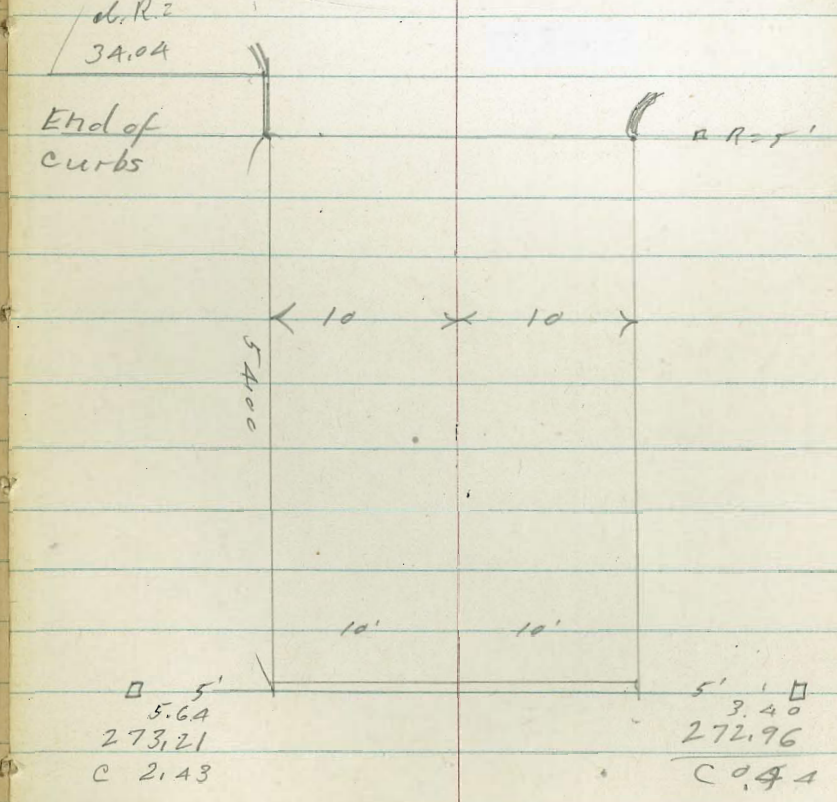
B = P.R.C.
5.76
275.50
C 0.26

5.95
275.70
C 0.25

8+23.03
A = cb. B.C. on Left.
from here (sheet #11197-L)
Banjo around to left

7+92.91 = cb. B.C. on Rt.

Cut off wall
Tuberose Lane



Violet
Sly. end to Sycamore

Drain Sly. end Violet

0+00 = inside of C.I. box.

(6) 1+98 End. 11.74 / 207.00 / C 4.74

(6) 1+58 5.47 / 220.62 / C 4.85

(6) 1+13.25 44.02 / 237.81 / C 6.21

(6) 0+68.5 9.80 / 255.00 / C 4.80

(2.25) 0+29.5 6.99 / 263.50 / C 3.49

(6) 0+00 9.23 / 265.00 / C 4.23

S.Ely End Banjo

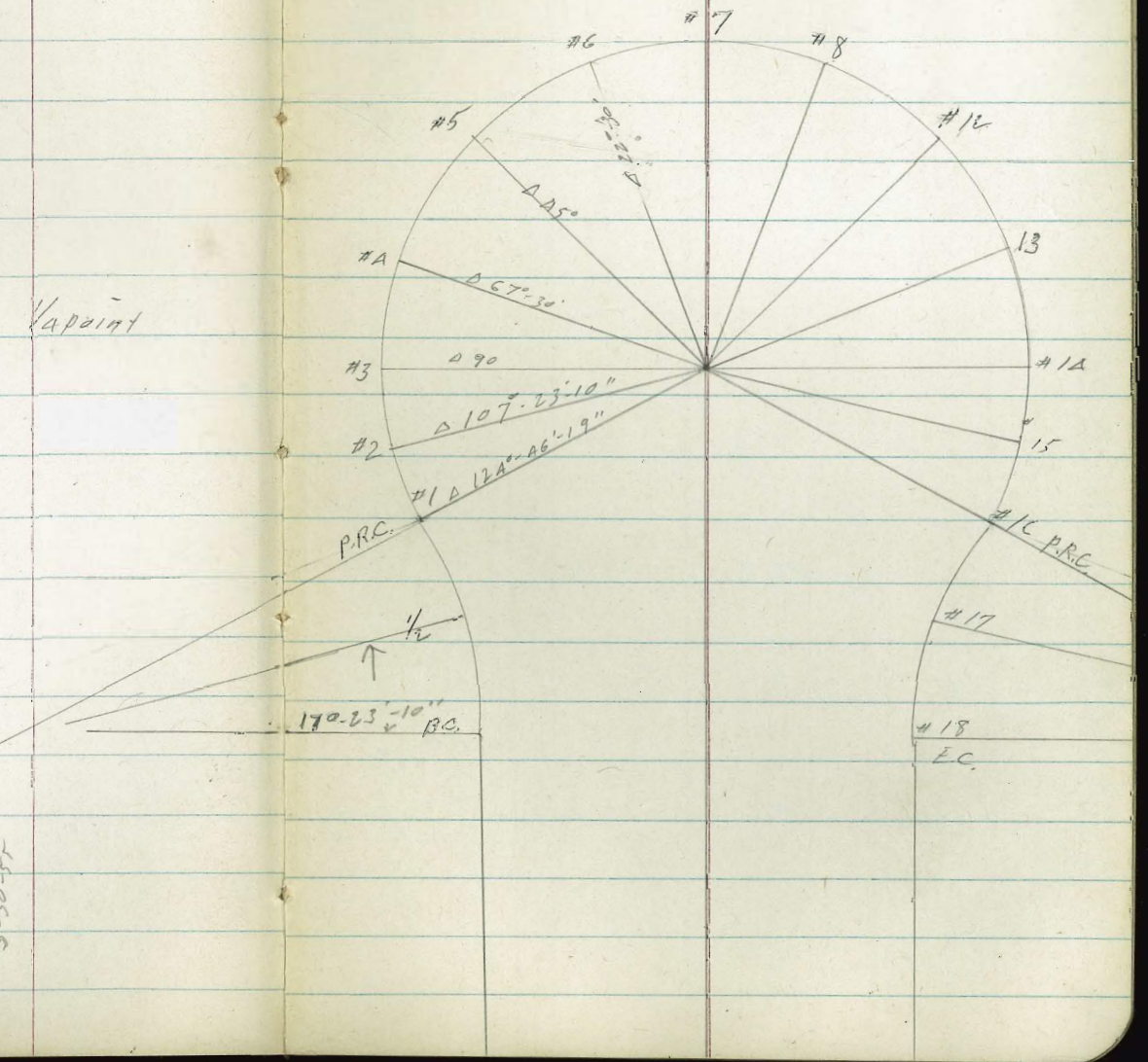
3-30-55

		E.C.		
#8	9.12 ~~269.18~~	#18	0.40 270.12	
	Meet ~~E occ~~		Co.28	
℄ = #7	9.49 269.21 Co.28	#17	9.97 269.95 Co.02	
#6	9.49 269.25 C 0.24	#16 P.R.C.	9.75 269.80 F 0.05	
#5	9.58 269.29 Co.29	#15	9.66 269.66 grade	
#4	69.58 269.38 Co.20	#14	9.51 269.51 grade.	½ point
½ point #3	70.02 269.51 Co.51	#13	9.36 269.36 Grade.	
#2	70.07 269.66 Co.41	#12	~~9.18~~ ~~269.18~~ Meet	
P.R.C. #1	70.16 269.80 Co.36.	#11		
½ Curve.	0.29 269.95 C0.34	#10		
B.C.	0.26 270.11 C0.15	#9		

#8 to #12 Ind. = Curb Inlet. Built prior to 3-30-55

Banjo

Δ = 9°00'
℄ Violet Produced



Violet
sly end

0+00 = Ctr. Banjo

39.79

1+88.42 — 3.72 / 273.39 / C 0.33 — F 0.13 — C 0.10 — 3.65 / 273.28 / C 0.37

39.79

1+50.63 = E.C. 4' ch. Rad
1+48.63 = G.E.C. Alley Ch. on Rt. — 3.01 / 272.56 / C 0.48 — C 0.02 — C 0.11 — 3.00 / 272.47 / C 0.53

1+46.63 = Nly. line Alley on Rt — 272.52 — 3.05 / 272.57 / C 0.48 — 272.43

21.43

1+25.20 = Sly. Alley line on Rt. — 2.62 / 272.07 / C 0.55 — 2.46 / 272.14 / C 0.32 — 2.47 / 272.00 / C 0.47

4.06

1+19.76 4' Rad
1+21.14 = Alley Ch. B.C. on Rt — 271.98 — C 0.11 — F 0.23 — 271.97

44.60

0+76.54 — 1.45 / 271.05 / F 0.40 — C 0.60 — C 0.05 — 1.15 / 271.01 / C 0.14

AA 5°

0+31.94 = ch. E.C. — 9.88 / 270.12 / F 0.24 — 0.40 / 270.12 / C 0.28 — 0.26 / 270.11 / C 0.15 — 0.15 / 270.11 / C 0.04

C

0+00 = Ctr. Banjo

Violet
South of Sycamore

Cont. Page 57

2+75.08 = el. B.C. on Rt.				4.92 275.03 F0.11	6 1/2 275.03 C 1.19
7.08			Nail 19Q Back		
2+68.00 el. B.C. on Lt.	5 01 275.04 F0.03		5.00 275.04 C0.56	C0.21	274.90
39.79					
2+28.21					
	4.4 ± 274.22 C0.2		F0.14	F0.14	5 00 274.09 C 0.91

Sycamore (17) 3/1/55

Tuberose to Violet

0+00 = Nly Sycamore + Wly. Tuberose

1+20			9.76 279.85 Fo.09	0.23 280.38 Fo.15	
1 —		9.81 279.80 Co.01	9.61 279.80 Fo.19	0.16 280.35 Fo.19	1.74 (L) 280.35 C 1.39
0+80			9.48 279.60 Fo.12	0.02 280.17 Fo.15	N. 7 20 Bk
0+60	P.V.C.	80.30 279.26 C 1.04	9.10 279.26 Fo.16	82.04 279.85 C 2.19	81.47 (L) 279.85 C 1.62
0+28.37 =	cl. E.C. Lt.	9.70 278.60 C 1.10	8.42 278.60 Fo.18	8.86 279.25 Fo39	81.35 279.25 C 2.10
0+17.04 Bk.			—	9.18 279.07 Co.11	~~279.07~~
0+7.37 = S.w.7 ½					
0+05.71 =	cl. E.C. Rt.		—	9.08 279.00 C 0.08	81.48 5 in 279.00 C 2.48
~~0+00~~	M. d' curve		8.21 8.24 Fo.03	9.44 9.05 Co.39	

Sycamore

	cb. $\Delta = 68°57'$	cb. $\Delta = 90°$	
E.C. on Violet	4.92 275.03 F 0.11	6.79 276.75 C 0.04	
Mid curve	5.12 275.23 F 0.11	6.78 276.70 C 0.08	
3+48.65 = cb. B.C. on Lt.	③ 6.35 275.43 C 0.92	~~5.57~~ 5.50 275.43 ~~C 0.07~~ CO.14	—	
3+07.95 cb. B.C. on Lt.	② 7.06 276.30 C 0.76	6.38 276.30 C 0.08	6.72 276.80 F 0.08	8.21 (L) 276.80 C 1.41
2+65.30	② 7.80 277.26 C 0.54	7.01 277.26 F 0.25	7.69 277.76 F 0.07	9.15 (L) 277.76 C 1.39
2+22.65 3+42.65	③ 8.64 278.21 C 0.43	8.02 278.21 F 0.19	8.71 278.71 ×	9.95 278.71 C 1.24
1+80 = E.V.C.	② 9.85 279.16 C 0.69	9.07 279.16 F 0.09	9.20 279.66 F 0.46	80.85 (L) 279.66 C 1.19
1+60		9.42 279.53 F 0.11	9.66 280.03 F 0.37	
1+40	① 80.12 279.76 C 0.36	9.56 279.76 F 0.20	9.92 280.27 F 0.35	130 (L) 280.27 C 1.03

Sycamore

Violet to Azelea Park

1+43.31 Alley Prop. on Rt. — A°-AA'-35"

1+34.68 #1 dif. 3°-12'

1+30.12 = Alley Prop. on Rt. — dif 2°-22'-45"

1+25.54 A'd. Rad. dif 10-33.88' - A'd. Rad ~~10-53'-12"~~

++27.37 = Alley B.C. on Rt

=1+16.84 B.C. Lt.

1+16.64 Equal.

8 parts for rough grade.

Ch. = 17.84

Dif. shown diff. 17.64

0+75.91

0+35.18 = ch. E.C. on Lt.

1/3 ℄ 31°29'20"

0+30 = Ch. E.C. on Rt.

2/3 62°58'40"

0+00 = ℄ Violet produced from S.E.

			(X) 4'3 Ly	
—			1/10 of face 4.85 C 1.58	273.27 use
2.80 272.72 C 0.08	2.63 F 0.09			4.37 273.34 C 1.03
—			Pk. 4' Ly 4.53 1/10 of face C 0.96	273.57 use
—			4' Rad Pk. 3.65 C 0.11	273.54 ~~273.50~~
3.04 273.12 F 0.08	2.87 F 0.25		4.84 3.86 C 0.13 273.73	4.37 273.73 C 0.64
3.84 274.03 F 0.19	4.05 C 0.02		4.53 F 0.10	5.04 274.63 C 0.41
4.95 274.95 ad. 275.12	4.83 F 0.12 4.89 F 0.23		5.52 F 0.03	275.55
— 275.17	4.84 F 0.33		275.65	5.65 275.65 ad.

Sycamore

2+59.57 = E.C. #8	25°-35'				
2+41.72 #7	22°-23'	8.57 269.89 F 1.32	985 F0 04	7062 C0 08	147 (L) 270.54 C-093
2+23.88 #6	19°-11'	0.30 270.29 C0.01	028 F0 01	7093 F0 01	2.05 (L) 270.94 C-1.11
2+06.04 #5	16° 00'	270.70	103 C0 33	143 484 C0 09	2.40 (L) 271.34 C-1.06
1+88.20 #4	12°-48'	1.56 271.10 C0.46	121 C0 04	179 484 C0 05	2.75 (L) 271.74 C1.01
1+70.36 #3	9°-36'	271.51	156 C0 05	220 484 C0 06	3.45 (L) 272.14 C-1.31
1+52.52 #2	dy 6°-23'-45"	2.13 271.91 C.022	194 C0 03	261 484 C0 07	05 in x 4.74 272.54 C 2.20
1+46.93 -4' ol. Rad	dy 5°-03'-52"	272.32	209 F0 23	299 484 C0 05	5 in x 4.90 272.94 C 1.96
1+45.10 = Alley E.C. on RX. (on St.)	5°-23'30" - 4' ol. Rad.			C0 13 484 Rep. 319 ✓	273 05 ~~273.09~~
Alley BC				F0 02	273 21

Sycamore

5+17.94	Δ = 99°-59'		5.98	5.21	5.53	-6.88
	ob. P.R.C. on Lt.		264.85	264.85	F0.21	265.54
36.93			C 1.13	C 0.36		C 1.34
				(Page 50)		
4+81.01	Δ = 71°-46'		—		6.37	67.22
					C0.22	266.15
36.93						C 1.07
4+44.08	Δ = 43°-33'-30"		66.75	6.41	6.84.08	67.43
	ob. P.R.C. on Lt.		266.06	C0.35	C0.28	266.76
16.99			C0.69			C0.67
4+27.09	Δ = 30°-34'	Set from Rad. point	7.45	6.47	6.97	7.82
			266.34	C0.13	F0.07	267.04
20			C 1.11			C0.78
4+07.09	Δ = 15°-17		7.17	7.22	7.24	8.59
			266.68	C0.54	F0.14	267.38
20'			C0.49			C 1.21
3+87.09	= B.C. RX = Match line		6.45	7.13	7.51	8.62
			267.06	C0.07	F0.25	267.76
			F0.61			C0.86
3+67.09			①	7.57	7.89	
			~~267.46~~	C0.11	F0.27	~~268.16~~
3+47.09	3+44.59 = Rough Gr. Sta.		8.80	7.95	9.08	9.78
			767.90	C0.05	C0.49	268.59
			C0.90			C1.19
3+03.33	3+02.08 " "		8.91	8.99	9.54	10.71
			768.90	C0.09	F0.03	269.57
2+81.45			Grade	269.39 9.45 C0.06	270.03 7.24 C0.21	C. 1.14

Sycamore

6+79.84 = P.C.C. 26°-31'-30"
ch. 7.66
7.66

6+72.18 24°-13'-30"
ch. 19.95
20'

6+52.18 18°-12'-30"
ch. 19.95
20'

6+32.18 12°-00'-30"
ch. 20.16
20.41 arc.

6+11.97 Dg. 6°-05' - ch. 20.16
20.21 arc.

5+91.76 = B.C. Lt.

5+59.59 = E.C. Δ 131°-46' Ahead
20.82

5+38.75 Δ: 115°-52'-30
20.81

2,45 262.35 C0.10	2,39 262.35 C0,04	3,05 263.05 ×	4,05 ② 263.05 C 1.00
~~262.43~~	2,47 262.43 C0,04	3,16 263.13 C 0,03	~~263.13~~
2,54 262.66 F0.12	2,64 262.66 F0.02	4,15 263.36 C 0,79	64.89 ① 263.36 C 1.53
2,74 262.96 F0.22	3,00 262.96 C0,04	3,61 263.66 F0.05	64.28 263.66 C 0.62
3,07 263.30 F0.23	3,29 263.29 ×	3,90 263.99 F0.09	64.85 263.99 C 0.86
3,20 263.63 F0.43	3.63 263.63 ×	4,23 264.33 F0.10	65.43 264.33 C 1.10
~~1.99~~ ~~264.16~~ ~~F2.17~~	4.05 264.16 F0.11	4.83 F0.03	66.00 264.86 C 1.14
64.36 264.50 F 0.14	4.95 264.50 C 0.45	5.18 F0.02	66.40 265.20 C 1.20

3.15
264.16
F 1.01

Sycamore

Lt. Cont. P-45

Rt. Cont P-44

Lef

			Lt. Cont. P-45		Rt. Cont P-44	
#8	8+35.24	~~Δ 38° 12' 30"~~ ch. P.R.C. on Rt. 24°-03'-53"	58.89 261.60 F 2.71	1.53 261.60 F 0.07	2.18 262.31 F 0.13	2.45 262.31 C 0.14
#7	8+14.73	20°-53'	1.04 261.70 F 0.66	1.78 261.70 C 0.08	2.24 262.40 F 0.16	62.70 X (L) 262.40 C 0.30
#6	7+74.22	17°42'-30"	1.12 261.79 F 0.67	1.79 261.79 X	2.45 262.49 F 0.04	62.40 (L) 262.49 F 0.09
#5	7+73.71	14°-32'	1.43 261.87 F 0.44	1.91 261.87 C 0.04	2.50 262.57 F 0.07	64.10 (1½ in) 262.57 X in C 1.53
#4	7+53.20	11°-22'	1.51 261.96 F 0.45	1.89 261.96 F 0.07	2.63 262.66 F 0.03	64.11 (1½ in) 262.66 C 1.45
#3	7+32.69 #3	18°-11' ch. 20.50	1.80 262.05 F 0.25	1.90 262.05 F 0.15	2.78 262.75 C 0.03	64.95 (1 in) 262.75 C 2.20
#2	7+12.18 Brk #2	ch. 20.50 Def 5°-00.30 ch. 19.99	1.87 262.13 F 0.26	2.10 262.13 F 0.03	3.05 262.83 C 0.22	5.84 X 262.83 C 3.01
#1	6+92.18 Brk #1	Def. 1°-54' ch. 12.34	2.28 262.26 C 0.02	2.30 262.26 C 0.04	3.04 262.96 C 0.08	4.01 262.96 C 1.05

6 x 20.51 arc. = Rad. = 185'

Sycamore

& alley corner

9+89.30 = End of Tgb on Lt. & Prop.
dfl. 9°-47'-36"
ch. = 4.18

9+85.12 Lt. = ch. B.C.
Dfl. 8°-50'
ch. 4.15

9+80.97 = End ch. on Rt.
dfl. 7°-53'
ch. 15.13

9+65.84 on Lt.
Dfl. 4°-25' ch. = 2.07

all def. from P.R.C. sta. 9+46.57

9+63.77 on Rt.
ch. 17.89 Dfl 3°-56'-30" -

= P.O.C. on Lt ~~dfl~~ 42°-31'-30"

9+46.57 = P.R.C. on Rt. & ch. 18.86

		3.62 261.61 C 2.01	1.57 261.61 ~~F 0.02~~		
				1.63 261.65 ~~F 0.02~~	5.22 261.65 C 3.57
		(2) 4.68 261.74 C 2.94	1.62 261.74 F 0.12		
				1.85 261.76 C 0.09	5.42 (1) 261.76 C 3.66
		(X) (L) 4.95 261.87 C 3.08	1.78 261.87 F 0.09	1.90 261.87 C 0.03	5.39 (2) 261.87 C 3.52
9+27.65	dfl 35°-18' ± ch = 28.50			1.97 261.97 ~~F~~	5.11 (1) 261.97 C 3.14
8+99.07	dfl 24°-23' ± ch. 26.18			2.29 262.09 C 0.20	4.12 (1) 262.09 C 2.03
8+72.75	dfl 14°-2' ± ch. 37.13			2.36 (X) (3) 262.19 C 0.17	3.30 (1) 262.19 C-1.11

13.56
ch. 20.45
Spring Creek
18.85
ch. 26.74

Nail in pole 12.32

Sycamore from
8+35.24 (P.O.C.) Page 43
Lt. 17 to Tulip St.

℄ Stationing
on Tulip St.
Meet curb

9+36.74 Lt.	15°-43' ch. 10.12	3' line = 8.97 ch. ch. = ~~9.16~~	260.67	0.67 260.67 ~~F0.04~~	— —
9+26.59 Lt.	14°-09' ch. 24.84	3' line = 22.02 ch. ch. = ~~22.40~~	58.97 260.81 F 1.84	0.64 260.81 F 0.17	—
9+01.73 Lt.	10°-18' ch. 19.96	3' line = 17.74 Cl ch = ~~18.00~~	59.51 261.14 F 1.63	0.87 261.14 F 0.27	—
8+81.73 Lt.	7°-12' ch. 19.96	3' line = 17.74 Cl. ch. = ~~18.00~~	56.76 261.36 F 4.60	1.07 261.36 F 0.29	—
8+61.73 Lt.	def 4°-06' ch 26.15	3' line = 23.45 ch ch = ~~23.87~~	55.87 261.50 F 5.63	1.38 261.50 F 0.12	—
8+35.24 (start def. of 0°00')			261.60 Page 43 F 4.17	261.60	

Tulip S.Ely. from
Sta. 9+46.57 - Page 44

9+46.57 = 0+00 going S Ely. to
Existing Pavement on Tulip

℄ stationing			ch.	RoughGr.
				Existing ch.
1+01.29	def. 23°-13. Meet Pavement + ch	ch = 0.16	1.45 261.59 F 0.14	1.47 261.59 F 0.12
~~1+01.11~~	~~def 23°-19 Meet ch. of right ch. 14.97~~	~~3' ch = 12.96 ch. 12.84~~	—	~~261.59~~
0+86.11	19°-44' ch 19.98	3' ch 16.61 ch. 17.07	1.58 261.86 F 0.28	3.91 261.91 C 2.00
0+66.11	def. 15°-09' ch 19.98	3' = 16.61 ch 17.07	2.05 262.19 F 0.14	4.12 (L) 262.19 C 1.93
0+46.11	def 10°-34' ch. 45.84	3' ch = 19.16 ch. ch. = 19.70	2.19 262.14 C 0.05	4.68 (L) 262.14 C 2.54
0+23.05	def. 5°-17'	3' ch. = 19.16 ch. Ch = 19.70	2.05 262.00 C 0.05	(X-L) 262.00
0+00 = (9+46.57 P-44			261.87 Page 44	261.87

3/9/55 (18)

Shamrock St. (L-11206)

From Sycamore Dr. to Sly. End

0+00 = S.sly. cb. E.C. Shamrock + Sycamore streets.

1+60

1+40

1+20

1+00 = P.O.C.

0+65.36

0+30.73 = cb. E.C. Lt.

0+00 = cb. E.C. Rt.

	5.66 264.79 C 0.87	4.79 264.79 X	4.00 264.29 F 0.29	4.44 (G) 264.29 C 0.15
	5.85 265.10 C 0.75	5.00 265.10 F 0.10	4.37 264.60 F 0.23	4.85 (1) 264.60 C 0.25
(1)	5.83 265.31 C 0.52	5.15 265.31 F 0.16	4.71 264.81 F 0.10	5.07 (1) 264.81 C 0.26
(1)	6.17 265.43 C 0.74	5.45 265.43 C 0.02	4.97 264.93 C 0.04	5.83 (0.4) 264.93 C 0.90
(L)	6.36 265.54 C 0.82	5.78 265.54 C 0.24	4.87 265.04 F 0.17	6.25 (L) 265.04 C 1.21
	7.13 265.65 C 1.48	6.44 265.65 C 0.79	5.23 265.15 C 0.08	7.07 (L) 265.15 C 1.92
		—	5.42 265.24 C 0.18	6.78 (E) 265.24 C 1.54
		—		

Shamrock

4+75.81 = E.C.				
dlb. 14°-45'-30"				
ch. 19.97				
4+55.81				
dlb 10°-11'30				
ch. 19.97				
4+35.81				
dlb. 5°-36'-30"				
ch. = 24.43				
4+11.34 = B.C.R.X. R = 125'				
3+65.08				
3+18.81				
2+72.54				
2+26.27				
1+80 = E.V.C.				

X	258.68	7.86	7.24	7.56
5'	257.48	257.48	256.98	256.98
	C 1.20	C 0.38	C 0.26	C 0.58
①	9.63	8.20	7.60	7.7
	258.03	258.03	257.53	257.53
	C 1.60	C 0.17	C 0.07	C 0.2
②	9.93	8.64	8.17	8.34
	258.52	258.52	258.02	258.02
	C 1.41	C 0.12	C 0.15	C 0.32
①	60.06	9.62	8.64	8.81 ①
	259.08	259.08	258.58	258.58
	C 0.98	C 0.54	C 0.06	C 0.23
	59.84	0.22	9.62	9.31 ①
	260.14	260.14	259.64	259.64
	F 0.30	C 0.08	F 0.02	F 0.33
③	6.067	60.96	0.55	1.27 X 0.2
	261.20	261.20	260.70	260.70
	F 0.53	F 0.24	F 0.15	C 0.57
⑤	63.33	2.42	1.76	2.11
	262.26	262.26	261.76	261.76
	C 1.07	C 0.16	X	C 0.35
	3.85	3.25	2.70	2.7 (0.2)
	263.32	263.32	262.82	262.82
	C 0.53	F 0.07	F 0.12	F 0.07
	4.67	4.29	3.60	4.04
	264.38	264.38	263.88	263.88
	C 0.29	F 0.09	F 0.28	C 0.16

Shamrock

= Sly. Into Lexington Park.

5+49.45 = End of Job

	5.13	5.19	5.00	3.70
	255.05	255.05	254.55	254.55
	C 0.08	C 0.14	C 0.45	F 0.85
5+15.81 ①	6.64	6.26	6.19	6.36
	256.21	256.21	255.71	255.71
	C 0.43	C 0.05	C 0.48	C 0.65
4+95.81 ①	8.35	6.93	6.42	6.70
	256.88	256.88	256.38	256.38
	C 1.47	C 0.05	C 0.04	C 0.32

Shamrock + Sycamore Curb Returns

S.W/ly Ret. = 0+00 = 400 on Sycamore

Running to North west

= 5+17.94 - P.41

P.R.C. = 4/4 = #4 — 5,21 / 264.85 / C 0.36 — Δ - P.41 = 20° 27'

3/4 — #3 — 5,50 / 264.97 / C 0.53 — Δ 15° - 20' - 15"

1/4 — #2 — 5,55 / 265.10 / C 0.45 — Δ 10° - 13' - 30"

1/4 — #1 — 5.59 / 265.18 / C 0.41 — Δ 5° - 06' - 45"

0+00 = B.C. — 5.42 / 265.24 / C 0.18 P.47

Stake line Δ = 9.62

R = 54'

S. Ely. Ret.

0+00 = E.C. - 0+30.73 P.47

5/5 = Sta 4+44.08 - P.41 — Δ 82° - 40' — #5 — Cl. P.R.C. - P.41 — 6.41 / 266.06 / P.41 = C 0.35

4/5 — Δ 66° - 08' — #4 — C.43 / 265.92 / C 0.51

3/5 — Δ 49° - 36' — #3 — P.A.I. — C.40 / 265.82 / C 0.38

2/5 — Δ 33° - 04' — #2 — C.48 / 265.75 / C 0.73

1/5 — Δ 16° - 32' — #1 — C.32 / 265.70 / C 0.62

Stake line Rad = 34.00

0+00 = B.C. — C.44 / 265.65 / C 0.79 — 0+30.73 Lt. P.47

Pepper Drive 3/8/55 (Roberts)

Violet to Tuberose

	Rough. Gr.	Curb.		Rough Gr.
3+00	6.89 285.45 C 1.44	5.54 285.45 C 0.09	5.01 284.94 C 0.07	6.67 ~~284.94~~ C 1.73
2+80 P.V.C.	5.88 285.20 C 0.68	5.07 285.20 F 0.13	4.74 284.70 C 0.04	6.35 284.70 C 1.65
2+40	5.72 284.56 C 1.16	4.50 284.56 F 0.06	4.06 284.06 Grade	5.30 284.06 C 1.24
2+00	5.42 283.92 C 1.50	4.05 283.92 C 0.13	3.52 283.42 C 0.10	5.24 283.42 C 1.82
1+50	3.34 283.13 C 0.21	3.20 283.13 C 0.07	2.61 282.63 F 0.02	3.90 282.63 C 1.17
1+00	N. 0.1 3.83 282.33 C 1.50	2.55 282.33 C 0.22	1.67 281.83 F 0.16	2.93 281.83 C 1.10
0+50	N. 0.1 3.10 281.54 C 1.56	1.71 281.54 C 0.17	1.12 281.04 C 0.08	2.58 281.04 C 1.54
0+10= Cb. E. C. at Violet.	N. 0.5 2.62 280.90 C 1.72	1.11 280.90 C 0.21	0.98 280.40 C 0.58	1.39 280.40 C 0.99
0+00=		1.85 280.80 C 1.05	9.72 280.15 F 0.43	

Mid curve.

Pepper Dr.

4+29.88 Meas. - cl. B.C. Lt.

4+20.08

~~4/3 cu~~

~~4+10.08~~

~~4+29.88 cl. B.C. on Lt. Rough Gr.~~

3+96.18 cl. B.C. on Rt

3370

3+80 - E.Y.C.

3+60

3+40

3+20

E.C. on tuberose	3.55 283.43 C 0.12 (P.27)		
Mid curve on Lt.	3.40 283.40 Grade.	3.73 282.71 C 1.02 (P.28)	1/3 on Tuberose on Rt: E.C.
	3.29 283.55 F 0.26	3.90 ~~3.83~~ 283.00 ~~C 0.83~~ C 0.90	2/3 Curve on Rt
	3.71 283.85 F 0.14	3.65 ~~3.45~~ 283.65 ~~F 0.20~~ Grade	1/3 Curve on Rt
	4.15 ~~284.15~~ Grade.		
① 83.88 283.55 C 0.33			—
—	—	3.71 ~~3.63~~ 283.97 ~~F 0.34~~ F 0.26	4.35 B.C. 283.97 C 0.38
3.95 284.94 C 1.01	5.16 284.94 C 0.22	4.22 284.36 F 0.14	5.15 284.36 C 0.79
6.33 285.30 C 1.03	5.52 285.30 C 0.22	4.73 284.73 Grade.	5.60 284.73 C 0.87
6.82 ~~285.50~~ C 1.32	5.62 285.50 C 0.12	5.09 284.96 C 0.13	6.03 ~~284.96~~ C 1.07
7.04 285.55 C 1.49	5.51 285.55 F 0.04	5.15 285.03 C 0.12	6.35 285.03 C 1.32

3/11/55

Pepper Drive

Violet to Azalea Park.

Rough Grade by Roberts

1+03.67 = Ely. line Alloy on Lt.

0+99.57
1+01.40 = B.C. Alloy ch. on Lt.

set alloy ch. stakes as shown by me on my copy of sheet 11201-L 4/11/55

1+00

0+99.40 = Ely. line Alloy on Rt.

0+95.48
~~0+97.65~~ = Alloy ch. B.C. on Rt.

0+50

0+19.86 = ch. E.C. on Rt.

0+00 = ch. E.C. on Lt. = S. W'ly. Cor Violet & Pepper

Pipe→	6.56 274.98 C 1.58	—	—
	5.32 274.95 C 0.37	—	—
6.75 274.99 C 1.76			C.36 ~~5.67~~ Re. set 274.49 ~~C 1.18~~ C 1.87
—	—	5.99 274.61 C 1.38	on 4'
—	—	5.61 274.56 C 1.05	on 4'
8.32 276.56 C 1.76	C 0.09	C 0.39	6.91 276.06 C 0.85
8.30 277.50 C 0.80	7.69 277.50 C 0.19	277.00	7.96 277.00 C 0.96
278.65 278.02 C 0.63	7.79 277.82 F 0.03	← 0+09.93	—
	278.02	← 0+00 ch	

Pepper Drive

2+44.33	10°-08.23'	1.66 270.72 C 09.4	1.05 270.22 C 0.83	0.30 270.22 C 0.08	69.60 270.22 F 0.62
2+24.33	7°-43.63	2.60 271.21 C 1.39	1.26 271.21 C 0.05	0.88 270.71 C 0.17	1.14 270.71 C 0.43
2+04.33	5° 19.03	3.29 271.75 C 1.54	2.23 271.75 C 0.48	1.42 271.25 C 0.17	1.53 271.25 C 0.28
1+84.33	2°-54.53	4.32 272.35 C 2.02	2.76 272.35 C 0.41	2.10 271.85 C 0.25	~~2.15~~ ~~1.55~~ 271.85 C 0.28
1+60.19 = B.C.		5.45 273.10 C 2.35	3.29 273.10 C 0.19	2.43 272.60 F 0.17	~~2.95~~ ~~3.60~~ 272.60 ~~C 1.00~~ C 0.35
1+22.65 ± ~~1+20.48~~ = 110' Ch. E.C. on Lt.			5.19 274.35 C 0.84	———	———
1+18.73 = Wly line Alley on Lt.		Pipe →	5.95 274.51 C 1.44	———	———
~~1+18.56~~ ± ~~1+16.73~~ = Alley Ch. E.C. on Rt.		———	———	4.83 273.97 C 0.86	- on 4'
1+14.46 = Wly line Alley on Rt		———	———	5.16 274.14 C 1.02	on 4'

Rake

Pepper Drive

5+50	2°-28.60'	6.45 264.45 X	C0.36	C0.12	5.88 263.87 C 2.01
5+00	2°	6.76 265.47 C 1.29	C0.14	C0.03	5.90 264.90 C 1.00
4+50	1°-31.78'	7.25 266.49 C 0.76	C0.25	C0.10	7.53 265.94 C 1.59
4+00	1°-03.37	8.51 267.51 C 1.00	C0.70	C0.19	8.68 266.97 C 1.71
3+50	0°-35'	8.73 268.53 C 0.20	C0.22	C0.11	9.06 268.01 C 1.05
3+00	0°-06.85'	10.09 269.55 C 0.54	F0.09	C0.14	9.00 269.04 F 0.04
2+88.47 = P.C.C.	15°-27.50	10.17 269.78 C 0.39	9.90 269.78 C 0.12	9.43 269.28 C 0.15	9.41 269.28 C 0.13
2+64.33	12°-32.83'	0.24 270.28 F 0.04	9.30 270.28 C 0.02	9.84 269.78 C 0.06	9.80 269.78 C 0.02

Pepper Drive

		Existing ch. 3.05			
6+16.80 = End ch. on Lt. 3°-06.56'		263.03			
					Existing ch. 2.67
6+06.71 = End ch. on Rt 3°-01'		—	—	—	262.72
		5.13			5.29
6+00	2°-57'	263.43	C 0.31	F 0.09	262.83
		C 1.70			C 2.46

Violet

Sycamore to Poplar

1+24.92 = Sly line. End alley cl. Alley on Rt. =

1+23.76 = B.C. - cl. on Lt.

1+20.92 B.C. Alley Cl. on Rt.

1+00

0+50

0+32.11 = cl. E. C. on Lt.

0+05 = cl. E. C. on Rt.

0+00 = Nly line Sycamore to East

See P. 36 - For block south

			9.40 278.40 =	end of cl.
			C 1.00	
89.6 277.87 C 1.1	79.6 C0.09			
		F0.06		
78.8 277.55 C 1.2	75.6 C0.01	F0.08	9.64 277.99 C 1.7	
71.61 276.85 C 0.7	68.1 F0.04	F0.07	9.10 277.34 C 1.8	
77.00 276.60 C 0.4	63.9 F0.39	F0.06	8.79 277.10 C 1.7	
276.40 curve on Left 276.17		76.79 276.75 C 0.04	8.19 276.75 C 1.4	
275.90				
275.65 BC Left				

Violet

3+25

3+22.83 = ob. E.C. on Rt.

3+00

2+75

2+56.83 = ob. B.C. on Rt

2+41.63 = ob. E.C. on Lt.

2+17

2+00

1+50

1+43.92 = E.C. Alley ob. on Rt.

1+39.92 = N'ly line alley on Rt. = start alley ob.

280.64
80 23
C 0.29

0.85
280.85
C 0.00

2.15
280.85
C 1.3

1.14
280.30
C 0.8

80 48
C 0.18

279.96
80 20
C 0.24

9.57
280.00
F 0.49

1.70
280.00
C 1.70

80.07
279.49
C 0.6-

F 0.27

Grade

80.81
279.29
C 1.5

80 45
278.64
C 1.8

C 0.15

C 0.71

Rake

9.93
278.60
C 1.33

-End of ob.

Violet

5+00					
4+75					
4+58.83	= E.C. Alley ch. on Rt.				
4+54.83	= start alley ch. Nly line alley on Rt. =			4.25 282.59 C 1.66	= end of ch.
4+50		2.65 283.08 Fo.4 282.73	3°03 F0°05 3°0 G0 37	C0.14	4.6 283.16 C 1.4
				C0.01	
4+50		2.39 282.38 ~~C0.01~~ grade	2°24 F0 14		4.0 282.51 C 1.5
4+39.83	= End alley ch. Sly line alley on Rt. =			3.61 282.40 C 1.21	= end of ch.
4+35.83	= Alley ch. B.C. on Rt.			C0.050	← 2' back
4+25		282°03	1°87 F0 16		
4+00		1.72 281.69 Grade X 281.34	1°62 F0°07 1°68 G0 34	C0.17	3.35 281.86 C 1.5
3+75					
3+50		1.29 280.99 C0.3	81°01 E0°02	C0.13	2.43 281.21 C 1.2

Violet

5+70± P.C.C. = Meet Existing cl. on Rt.

5+59.60 = cl. opposite Prop on Rt.

5+55.75 = cl. B.C. on Rt.

5+52.33 End of cl. on Lt.

5+21.04 = P.V.C. on Lt.

283.43

5+42.33 — 283.54

5+32.33 — 283.48

2.50
283.32
F 0.18

2.80
F 0.63

3.06
F 0.48

3.18
F 0.30

3.13
F 0.19

~~283.88~~

3.69
283.80
F 0.11

C 0.28

Meet cl

283.80

Violet & Pepper Dr.
S.W. Return

0700 Pg 5-3

B.C. Pepper Dr. 278°02 7.73 F0.29 (2184)

23° 43' 15"

1/4 2788 8.60 C0.43

47° 26' 30"

1/2 278.16 7.89 F0.27

71° 09' 45"

3/4 278°02 8.12 C0.10

E.C. Violet St 277.87 7.96 C0.09
H23 26 Pg 5-7

Δ = 94° 53'
C & Rad = 25'

Wly Return
Sycamore Dr. & Violet

61

E.C. Violet 276.60 6.30 F0.30

26° 38' 30"

1/4 276.40 6.09 F0.31

53° 17' 00"

1/2 276.17 6.39 C0.20

79° 55' 30"

3/4 275.90 5.93 C0.03

B.C. Sycamore 275.65 5.57 F0.08

Δ = 106° 34'
C & R = 26.56

Wly Return Violet & Pepper Dr.

0+19.86 rg 53		
B.C. Pepper Dr	277.00	6.93 F 0.07
14° 11' 10"		
1/6	277.41	7.37 F 0.04
28° 22' 20"		
1/3	277.80	9.54 C 0.14
42° 33' 30"		
1/2	278.23	8.23 C
56° 44' 40"		
2/3	278.72	8.34 F 0.38
70° 55' 50"		
5/4	279.18	9.24 C 0.06
	-	
EC Violet st	279.49	80.26 C 0.77
2+41.63 10.58		
Δ = 85° 07'		
Cb Rad 55°		

Cervantes Street.
Sewer Laterals

Sheet #11802-L
" 11804 L

Grades for Laterals take off 0.30 above I.E. Main line and then extend to Prop. line on 0.2% grade.

2-3 + 4 should be encased

B.M. = chiseled square Ely. end of N.E. cb. Rot. Euclid + Cervantes
El. = 135.60

#5	#6	#7	#8
6.60	7.85	9.71	32.00
21.32	22.07	23.71	25.65
C 5.28	C 5.78	C 6.00	C 6.35

Tecalote Road Curb stakes

5/29/55

Set. 20' ch. Rad. for drives into Armory grounds

Set. B.C. + E.C. stakes 3' back of ch.

0+00 = Ely. line Armory grounds (= end sly. ch.)

B.M. = ~~end of ch.~~

chiseled □ end of sly ch.

Profile #4463 EL. =

Drives spotted 16' off main Bldg. as per contractors plan. (state plans)

6+08.5 = ch. E.C. — 3.07 / 252.36 / C 0.71

5+44.5 = ch. B.C. — 5.06 / 254.27 / C 0.79

1+67 = ch. E.C. — 6.44 / 261.42 / C 0.02

1+03 = ch. B.C. — C1.25 / 261.81 / F 0.56

0+00 = end existing ch.

Tulip + Trailing
Cross Gutter 6/10/55

~~0+00 = B.C. S.E ch. Rot.~~

0+00 = 9^{E} North of B.C. S.Ely. ch Rot.

0+78^{E} = E.C. N.Ely. ch. Rot.

0+67 = Meet gutter 199.33 C. 0.18 Nail 3' Lt.

0+51 = Brk. 199.00 C-0.08 "

Note This leaves a

0+41 rather bad bump in C 0.14 "

gutter but o.k. because

0+27 Trailing to East is a C 0.34 "

short dead end street

0+16 C-020 "

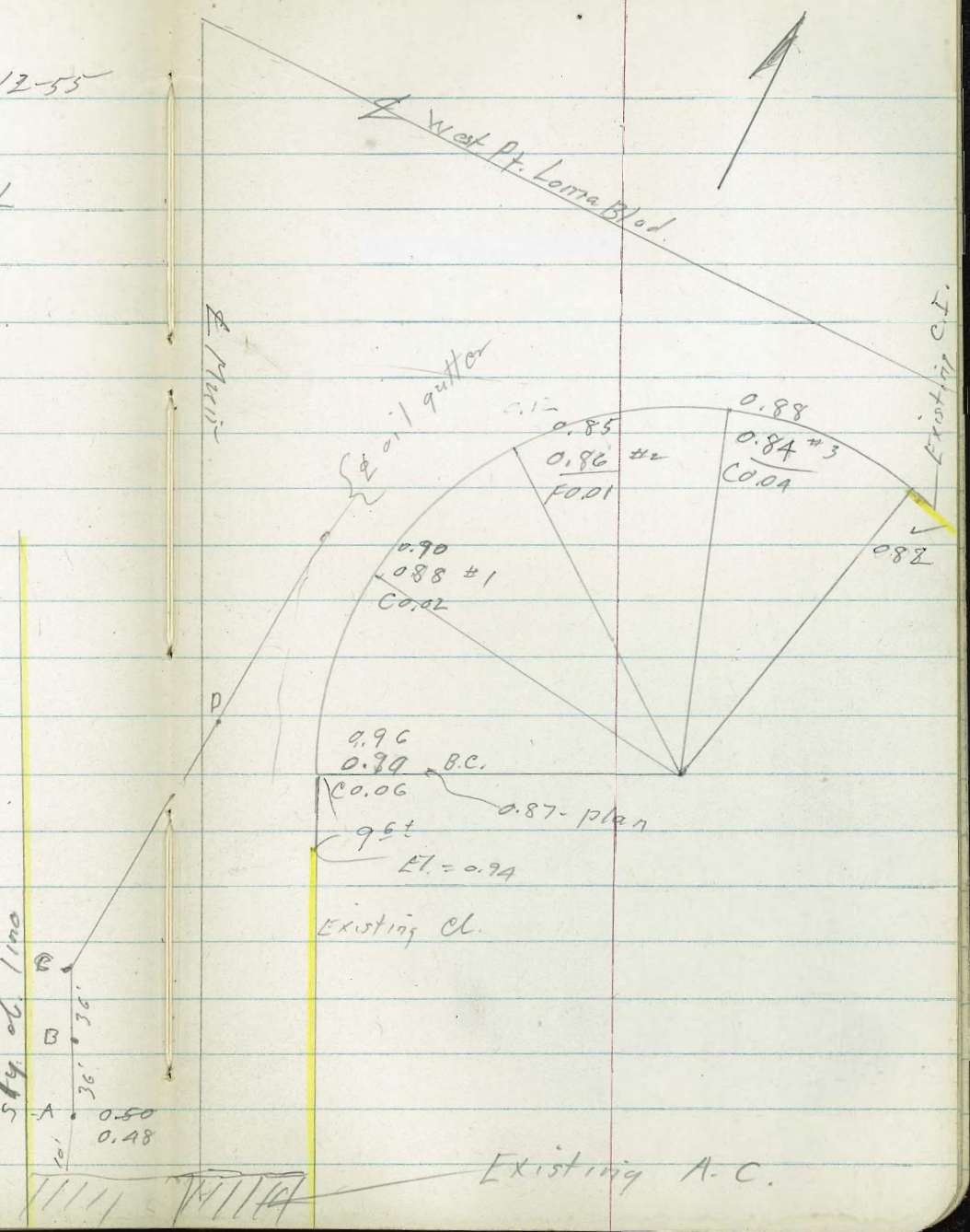
0+09^{E} 198.35 - C 0.08 "

0+00 Meet gutter.

S. Ely. Cl: Ret.
West Pt. Loma Blvd & Muir Street.

7-12-55

sheet 12246-L



oiled
Gutter grades

X-3'

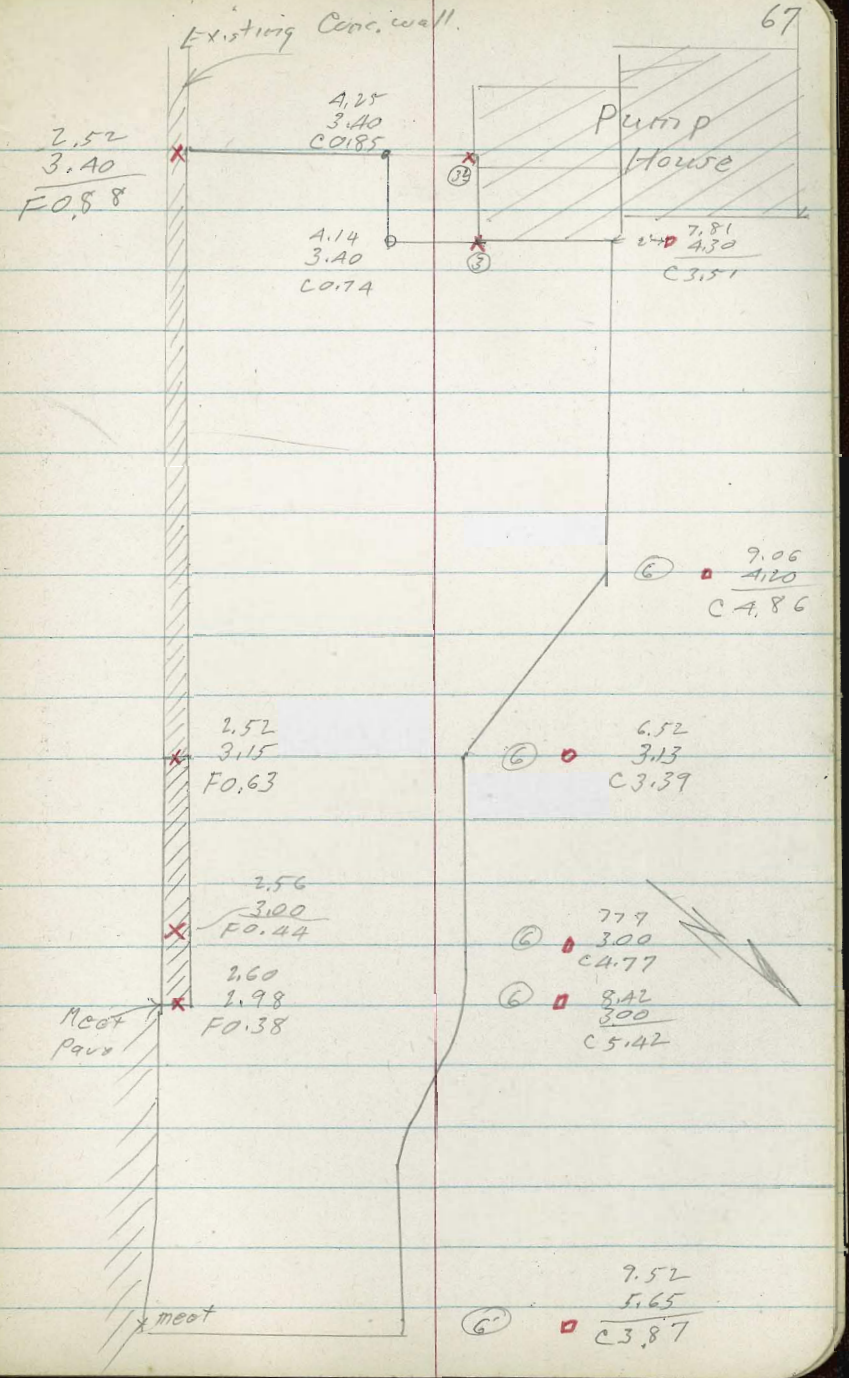
A	B	C	D
1.22	1.15	1.37	
0.48	0.40	0.31	
C0.74	C0.75	C1.06	

Pump Station #A

Witherby St. at Hancock St.

Re-stake 7-26-55

w.o. 20979



Kendall & Malden Sewer

8-2-55

W.O.# 62422

F.B. 2269 - Page 62 Sheet # 12173-L

0+00 = Existing M.H. & Malden to west & & Kendall to South.

Rim 217.60

241.76

25.50 T.P.
34.18 T.P.
42.61 T.P.

0+93.48 = & 13°-20'-30" Rt.		33.36 226.66 C-6.70	
0+61.74		7.24 220.51 C-6.73	
0+30	Sta. + Encasement	22.11 214.35 C 7.76	
0+20		20.89 212.45 C 8.44	1+64.10 = Plug.
0+10		19.58 210.85 C-8.73	1+56.10 = M.H.# 1
0+00		18.20 209.80 C-8.40	1+24.79

9.65
240.29
C-9.36

47.65
238.80
C 8.85

9.40
232.73
C-6.67

Alley Blk 113 Pac. Beach

Cass to Dawes

between Chalcedony & Law.

8-15-55

W.O. 32477

B.M. = SE.B.P. Chalcedony & Dawes.

EL.: 69.40 - RB 2262 P 65

Cook - grade South

Kingswood Conc.

69

	South	North.	Ely. line Cass	North
2+10	N. 0.20 — 8.68 / 68.43 / C 0.25	9.00 / 68.73 / C 0.27 — N. 0.95	5+00 — 3.99 / 64.07	4.39 / 64.37
2+00	N. 0.20 — 9.00 / 68.55 / C 0.45	9.35 / 68.85 / C 0.50 — N. 0.85	4+80 — X 0.75 — 7.41 / 65.16 / C 2.25	6.12 / 65.46 / C 0.66 — X 0.30
=1+90 Map. 1+88.54 ch.	D V' — 8.69 / 68.69 / X	9.35 / 68.99 / C 0.36 — N 0.65	4+70 — X .83 — 7.44 / 65.59 / C 1.85	6.12 / 65.89 / C 0.23 — X 0.25
1+50.8	D V — 9.54 / 69.33 / C 0.21	70.03 / 69.62 / C 0.41 — N. 0.85	4+60 — X 1.1 — 8.10 / 65.81 / C 2.29	6.12 / 66.11 / C 0.01 — X 0.25
1+13.1 X 3'	70.85 / 69.97 / C 0.88	1.24 / 70.25 / C 0.99 — N. 0.75	4+10 — X 0.75 — 8.06 / 66.33 / C 1.73	7.17 / 66.63 / C 0.54 — X 0.25
0+75.4	D V' — 1.74 / 70.60 / C 1.14	2.30 / 70.88 / C 1.42 — N. 1	3+60 — N 0.23 — 8.40 / 66.85 / C 1.55	8.33 / 67.15 / C 1.18 — N 2.45
0+37.7	N. 0.40 — 2.67 / 71.24 / C 1.43	2.55 / 71.51 / C 1.04 — D V'	3+10 — N 0.65 — 9.05 / 67.38 / C 1.67	8.86 / 67.68 / C 0.68 — D V'
0+00	1.91 / 71.87	2.20 / 72.15	2+60 — N 0.25 — 9.20 / 67.90 / C 1.30	8.73 / 68.20 / C 0.53 — N. 0.90
W'ly. line Dawes				

8-15-55
W.O.# 32399

N. & S. Alley Blk. 262 Pacific Beach

Reed to Thomas. Wly. of Bayard.

0+00 = Nly line of Reed

B.M. = N.E. 4 Lft. Bayard & Reed El. = 4.98
Sheet # 11937-L

		0.09	−0.22	D 2'			
1+80		0.82	0.82				
		F 0.73	F 1.04				
	D-2'	0.50	0.48				
1+45		0.72	0.68 ←				
Sly line E & W. Alley		F 0.22	F 0.20	D 2' Both ways			
	D 2'	0.49	0.95				
1+25		0.66	0.58 ↙				
Nly line E & W. Alley		F 0.26	C 0.37				
		1.76	0.49	D-2'	Sly line Thomas.	3.29	3.41
0+90	× 0.25	0.57	0.51		2+70	3.25	3.35
		C 1.19	F 0.02	0.27 0.46			
0+65 N.T.							
		1.74	0.27	F 0.19		3.62	3.73
0+55	× 0.20	0.47	0.44	× 0.25	2+60 D-2'	3.20	3.21 D 2'
		C 1.27	F 0.23			C 0.42	C 0.52
	×	2.09	0.26	×		1.85	2.69
0+20 Brk	0.25	0.37	0.37	0.25	2+20 D 2'	1.66	1.66 D 2'
		C 1.72	F 0.11			C 0.19	C 1.03
0+00						0.86	0.78
Nly line		0.31	0.30		2 — D-2'	1.07	1.07 D-2'
Reed.		0.37	0.33			F 0.21	F 0.29
		0.10					

Ely + Wly Alley
Blk 262 Pacific Beach

8-15-55
sheet #11937-L

0+00 = Wly line Bayard.

2+00	N. 0.40	1.89 1.06 C 0.83		3.54 1.26 C 2.28	N. 0.43
1+80	N 0.10	1.97 1.40 C 0.57		3.54 1.60 C 1.94	N 0.10
1+35	□1'	2.17 2.41 F 0.24	~~2.44~~	2.78 2.50 C 0.28	X-1'
1+15	X-1'	2.77 2.86 F 0.09	~~2.90~~	2.82 2.90 F 0.08	X-1'
0+80	X-1'	4.16 3.65 C 0.51	~~3.67~~	3.99 3.60 C 0.39	X-1'
0+50	X 1'	4.75 4.33 C 0.42		4.44 4.20 C 0.24	X-1'
0+20	X 1'	5.20 5.00 C 0.20		5.00 4.80 C 0.20	X 1'
0+00 wly. Bayard		5.22 5.15		5.26 5.20	

N+S alley
Ely line

2+76.10		0.95 0.58 C 0.37		0.48 0.68 C 0.20
2+48.05	2'	-0.20 0.72 F 0.92		0.27 0.87 F 0.60
2+20	0-0'	0.36 0.86 F 0.50		-0.02 1.06 F 1.08

□ 0.90
0 2'

Alley Blk. 80 Pac. Beach

Bayard to Mission Blvd

Between Law + Beryl.

W.O. 32102
8-19-55

0+00 = Wly. line Bayard.

B.M. = N.W. L+T. Mission Blvd + Law. El. = 53.82

2+00	N-0.20'	2.78 62.08 C 0.70	3.96 62.38 C 1.58	N 1.50'	
1+60	⊡ -1.50	2.69 62.94 F 0.25	3.70 63.24 C 0.46	X-2'	
1+20	X-1'	3.71 63.79 F 0.08	4.72 64.09 C 0.63	X-1'	
1 ~	X-1'	3.74 64.00 F 0.26	4.10 64.30 F 0.20	⊡1'	
0+80	N. 0.25	4.03 63.78 C 0.25	4.67 64.08 C 0.59	N. 0.39	
0+40	N. 0.55	3.93 62.88 C 1.05	4.50 63.19 C 1.31	⊡2'	
0+00		1.98 ✓ 61.98	2.31 ✓ 62.31		

Wly line Bayard

0+30 Rt. = (S) #1 } 64.00 / 57.90 / C 6.10
Staked = 5' Rt.

Ely line Mission Blvd. 5+00		6.85 56.87	9.16 57.14		
4+70	X-2'	7.21 57.07 C 0.14	7.40 57.35 C 0.05	X-1'	
4+40	⊡ -0.45	7.24 57.27 F 0.03	7.41 57.57 F 0.16	⊡1 1/2	
4+20	N 0.45	8.14 57.47 C 0.67	7.74 57.77 F 0.03	⊡ 0.90'	
4+00	⊡1'	8.05 57.83 F 0.22	8.06 58.13 F 0.07	⊡ -0.75	
3+60	N-0.80	9.55 58.68 C 0.87	8.86 58.98 F 0.12	⊡ 0.65	
3+20	N. 0.55	9.63 59.53 C 0.10	9.83 59.83 ✓	0.2'	
2+80	N-0.50	0.65 60.38 C 0.27	2.68 60.68 C 2.00	N-0.40	
2+40	N-0.20'	1.83 61.23 C 0.60	2.97 61.53 C 1.44	N-0.20	

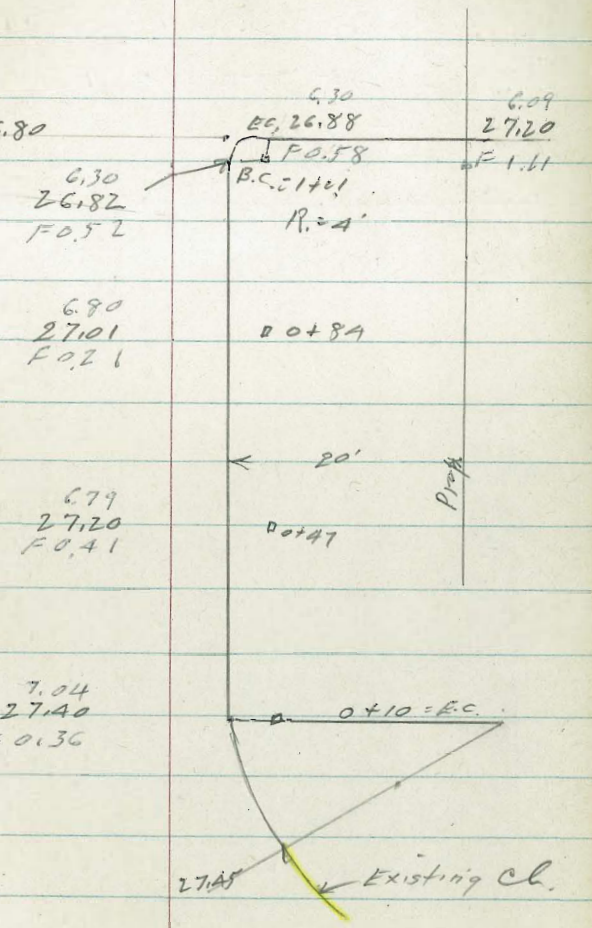
Prop. pipe - R.P. Nails in fence posts.
0.44 West
0.45 North

Curb Stakes
Everts & Grand

11/8/55

w/y side Everts.
Grand s/y to Alley

Profile # 1139



11-8-55

Replace stakes Lot 14 Blk 77- Villa Tract. La Jolla Park

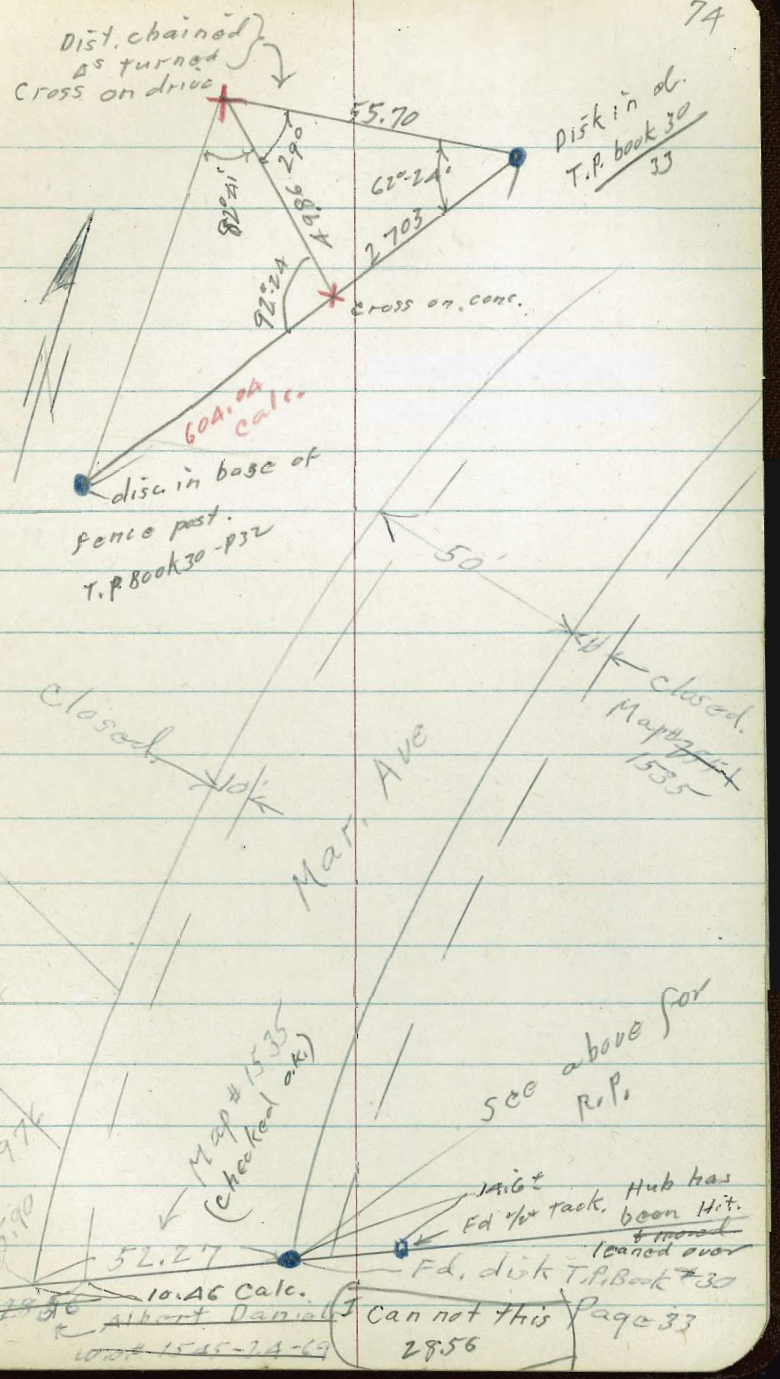
T.P. Book #30 - page 33

Map. #1535 Map 2551

#976

~~Albert W Daniels (Plat - W.O. 1545-24-69)~~

sheet #1457-B.



Sheet 609AA-L.

3-15-56
W.O. 32429

South Lane - La Jolla

15' wide - 14.5' paved,

0+00 = Wly. line La Jolla Blvd.

	South	℄	North	
	3.43		3.28	
1+38 +-3'	72.98		72.98	D-2'
	C0.45		C0.30	
1+20	3.66 / 3.48			
	C0.18			
	3.89		3.81	
1+11 D-2'	73.71		73.71	D-1'
	C0.18		C0.10	
10+27	4.59		5.17	
0+84 D-2'	74.44		74.44	+-2'
	C0.15		C0.73	
	5.26		5.43	
0+57 D-2'	75.17		75.17	+-2'
	C0.09		C0.26	
	6.02		6.55	
0+30 Brk. D-2'	75.90		75.90	D-2'
	C0.12		C0.65	
	C38			C72
	76.21			76.19
	C0.17			C0.53
0+15 D-2'	6.38		6.72	D-2'
	76.16		76.14	
	~~C0.22~~		~~C0.58~~	
	C0.17		C0.53	
	6.09	~~76.60~~	6.14	
0+00	76.07	75.95	76.13	
		Meas.		
		76.00		

	South	℄	North	
	6.44		6.50	
4+20 N-1.08	65.75		65.75	N-0.56
	C0.69		C0.75	
			3+	
	8.06		7.39	
3+80 N-1.18	66.70		66.70	D-0.20
	C1.36		C0.69	
3+40 5+40			3+70	7.81
	8.25		8.00	
3+40 D-1'	67.65		67.65	D-2'
	C0.60		C0.35	
	9.36		9.56	
3+00 Brk. D-1'	68.60		68.60	+-3'
	C0.76		C0.96	
	9.86		9.89	
2+73 D-2'	69.33		69.33	N-0.59
	C0.53		C0.56	
	0.75		1.05	
2+46 N-0.21	70.06		70.06	N-0.55
	C0.69		C0.99	
	0.93	Pole #	1.17	
2+19 D-2'9	70.79	PA-424	70.79	N-0.59
	C0.14	EL=72.47	C0.38	
	1.93		2.10	
1+92 +-3'	71.52		71.52	+-3'
~~1+74~~	C0.41		C0.58	
	2.43		2.90	
1+65 D-2'	72.25		72.25	+-3'
	C0.18		C0.65	
~~1+58~~				
	C0.53			

	South	℄	North			South	℄	North	
7+20 N-0.57	9.30 58.41 C0.89		8.43 58.41 C0.02	□-2'	9+70 □-2'	1.25 51.84 F0.59		3.26 51.91 C1.35	N-1,10 BK
7+00 N-0.33	9.69 59.00 C0.69		9.17 59.00 C0.17	□-2'	9+30 □-2'	2.33 52.31 C0.02		2.78 52.31 C0.47	□-2'
6+80 □-0.75	0.22 59.55 C0.67		9.88 59.55 C0.33	□-2'	9+10 □-1'	2.75 52.59 C0.16		3.16 52.59 C0.57	PK-2'
6+60 POC ~~BK~~ □-0.50	0.72 60.05 C0.67		0.47 60.05 C0.42	□-2'	8+90 □-2'	3.34 52.98 C0.36		3.47 52.98 C0.49	PK-2'
6+20 □-2'	1.19 61.00 C0.19		1.40 61.00 C0.40	□-2'	8+70 □-2'	3.87 53.48 C0.39		4.38 53.48 C0.90	PK-2'
5+80 +-2' 4 x 40'	2.38 61.95 C0.43		2.22 61.95 C0.27	□-2'	8+50 □-2'	4.30 54.09 C0.21		4.75 54.09 C0.66	PK-2'
5+40 □-2'	3.41 62.90 C-0.51		3.30 62.90 C0.40	+-3'	8+13.34 N-1.75 7776.67 x 3 □-2'	6.78 55.32 C1.46		5.80 55.32 C0.48	□-2'
5+00 ~~BK~~ □-2' 4+96 - 64.41 4+80 64.82	4.31 63.85 C0.46		4.27 63.85 C0.42	□-2'		7.02 56.54 C0.48		6.73 56.54 C0.19	□-2'
4+60 N-0.58	5.87 64.80 C1.07		5.27 64.80 C0.47	□-2'	7+40 □-1'	8.18 57.76 C0.42		7.85 57.76 C0.09	□-2'

	South	℄	North		Sewer. Lat #1	℄ Alley
					1+05 Lt. prop. 73.92 68.85 C 5.07	68.70
					staked 5' west of ℄	
Mid Curve □-2'	0.25 48.80 C 1.45		0.26 50.05 C 0.21	□-2'	M.H. ℄ Alley Both ways.	
					7.68 8.53 C 1.15	
Pave. B.C. 10+85. □-2'	0.76 49.65 C 1.11		0.68 50.13 C 0.55	□-2'		
Prop. B.C. 10+75 □-2'	0.84 50.20 C 0.64		0.83 50.40 C 0.43	□-2'		
□-4' 10+62.5	1.16 50.65 C 0.51		1.11 50.85 C 0.26	□-2'		
10+50 N-1.78 IN	2.46 50.90 C 1.56		1.68 51.10 C 0.58	□-2'		
10+10 +0.50	2.43 51.37 C 1.06		2.07 51.51 C 0.56	PK-2'		

3/15/56

Alley Ely. of. Blk A
South La Jolla (Sheet. 6094 AL)

	West	℄	East	East
1+95 N-0.20'	1.34 50.25 C 1.09		2.13 50.45 C 1.68	N-1.43
1+80 N-0.23'	1.40 50.20 C 1.20		1.23 50.40 C 0.83	□-2'
1+70 □-2'	0.11 50.05 C 0.06		0.84 50.25 C 0.59	□-2'
E.C. on Rt 1+60 □-2'	0.15 49.75 C 0.40		0.30 50.00 C 0.30	□-2'
1+37.5 □-2'	0.13 48.73 C 1.40		48.85	
E.C. on Rt 1+15 □-2'	0.43 47.70 C 2.73		8.33 47.90 C 0.43	□-0.85
1+05 □ 2'	8.41 47.25 C 1.16		8.16 47.45 C 0.71	□ 1.5 Bk
Existing Pave. 1+00	47.04	4663	47.24	
0+00 = Nly. Bon Air.				

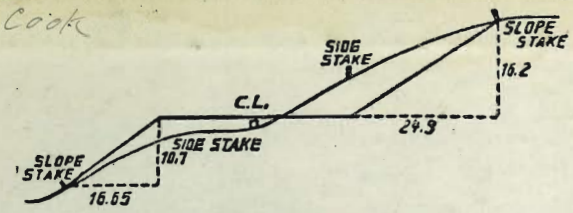
	West	℄	East
Nautilus sly line 2+75	48.21 ✓ 48.21	48.20 ✓	48.74 ✓
2+55 □-0.65	9.92 49.04 C 0.88		2.25 49.36 □-2' C 2.89
2+35 □-0.75	0.33 49.55 C 0.78		1.94 49.75 □-2' C 2.19
2+15 N-0.15	1.33 50.00 C 1.33		2.48 N 50.20 1.75 C 2.28

Cuts for checking
South Lane La Jolla

M = Mark on Conc.

F 0.04 10+40
9+50 C 1.00 □
8+31 C 0.39 M
6+40 C 0.55 M
M C-0.72 5+95
5+65 C 0.60 M
M C-0.48 5+55
M C 0.46 4+96
M C 0.50 4+80
3+70 C 0.87 M
M- C 0.21 1+74
M C 0.56 1+58
M. C 0.18 1+20
0+00 = Why Line La Jolla Blvd.

Cook



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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