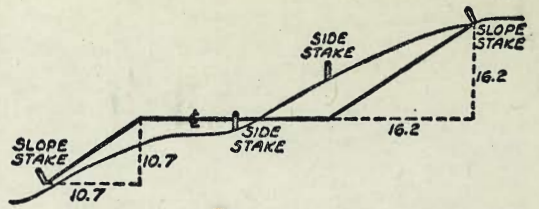


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

5543

30.52 To N. 3-1-99

G-351

IMPROVED TABLES
AND
INFORMATION

1-23 39th st. Juniper st. etc.

24-28 Soap box derby

29-33 Alvarado. Sewer Crossings & lines in Waring tract. To crossings #6-A - #7 & #9

34- Hilltop + 39th Sewer Extention

35- Blk. 23 Fairmount Add. {Storm Drain

36- Conde - congress to Moore

40- Harney " "

45- Jefferson Ampudia to Twiggs

52 Moore - Trias to Arista

55

56- Sunset Cliffs Blvd. {curbs Hill to Adair

6A Tie out Mon. Lots 23 & 24 La Jolla Shores Terrace

65 Tie points Conde & Moore

66 Taft & Colima Curbs.

67 " & Forward

" & Midway

Storm Drain

68. Torrey Pines Road & Charlotte St

69 Alley Blk 6 Chester Park

7A Univ. Ave Sewer (Chocolate Canyon Job) Bdry to Wabash

7C College & Univ. S.w'ly. Cor. Curb stakes

77 {Lot 2 Blk 47 Grantville
{Grade stakes

79 {Santa Margarita.
{Sewer 54th to 55th

INDEXED

39th St, North of Juniper

1/3/55

Sheet 11185-L

		West Lt	ch	ch	East Rt.
1+59.17	E.U.C.	6.99 236.77 C 0.22	6.39 236.77 F 0.38	237.10 237.47 F 0.37	7.28 237.47 F 0.19
1+39.17		6.23 235.80 C 0.43	5.47 235.80 F 0.33	236.30 236.50 F 0.20	7.13 236.50 C 0.63
1+19.17	5.18 on Lt.	5.99 234.93 C 1.06	4.33 234.93 F 0.60	235.35 235.63 F 0.28	6.86 235.63 C 1.23
0+99.17		5.07 234.18 C 0.89	3.81 234.18 F 0.37	234.52 234.88 F 0.36	6.34 234.88 C 1.46
0+79.17	P.U.C.	4.81 233.54 C 1.27	3.05 233.54 F 0.49	233.79 234.24 F 0.45	5.80 234.24 C 1.56
0+42.25	Lt. only				
0+20.29	ch. E.C. N.			232.35 232.50 F 0.15	3.76 232.50 C 1.26
0+05.34 =	ch. E.C. on Lt.	2.73 231.37 C 1.36	1.13 231.37 F F 0.24		
0+00 = Ny. line Juniper on west (left)		BM 233.54 on Pole.			

39th

			Cb.		Cb.	
4+19.37			51.27 249.58 C1.69	9.24 249.58 F0.34	9.91 250.22 F0.31	0.91 250.22 C0.69
3+99.37			50.96 248.91 C2.05	8.53 248.91 F0.38	9.15 249.58 F0.43	9.82 249.58 C0.24
3+79.37			50.34 248.10 C2.24	7.76 248.10 F0.34	8.34 248.79 F0.45	8.94 248.79 C0.15
3+59.37 +20.46	P.V.C.		9.37 247.13 C2.24	6.83 247.13 F0.30	7.59 247.83 F0.24	8.02 247.83 C0.19
3+38.91 33.58	cl. E.C. on Rt.		8.14 246.07 C2.07	5.80 246.07 F0.27	6.65 246.76 F0.11	7.18 246.76 C0.42
3+05.33 33.59	Lt. only (Sycamore St.)		7.01 244.33 C2.68	3.90 244.33 F0.43		—
2+71.76 37.53	cl. B.C. on Rt		5.54 242.59 C2.95	2.08 242.59 F0.51	243.10 243.30 F0.20	4.14 243.30 C0.84
2+34.23 37.53			2.41 240.65 C1.76	0.41 240.65 F0.24	241.22 241.35 F0.13	1.77 241.35 C0.42
1+96.70 37.53			9.45 238.71 C0.74	8.31 238.71 F0.40	238.90 239.41 F0.51	7.82 239.41 F1.59

39th

		Cl.	Cl.		
6+30.90 = start Pepper Drive	Δ 21°-09.58' - ch. 15.96	48.10 251.78 F 3.68	0.96 251.78 F 0.82	1.07 251.80 F 0.73	1.60 251.80 F 0.20
+16.00'					
6+14.90	Δ 14°-06.38 ch=15.96	48.74 251.66 F 2.92	1.56 251.66 F 0.10	1.25 251.73 F 0.48	1.63 251.73 F 0.10
+16.00'					
5+98.90		49.35 251.54 F 2.19	1.41 251.54 F 0.13	1.20 251.66 F 0.46	1.74 251.66 C 0.08
+16.01'	℄ def. = 7°-03.19' ch = 15.97				
5+82.89 = B.C. RT		49.64 251.43 F 1.79	1.17 251.43 F 0.26	1.21 251.60 F 0.39	1.91 251.60 C 0.31
5+48.39		1.35 251.18 C 0.17	0.88 251.18 F 0.30	1.71 251.46 ℄ 0.25	2.32 251.46 C 0.86
5+13.88		2.59 250.93 C 1.66	0.61 250.93 F 0.32	1.02 251.32 F 0.30	2.60 251.32 C 1.28
4+79.37	E.V.C.	2.07 250.68 C 1.39	0.31 250.68 F 0.37	1.25 251.18 C 0.07	2.33 x 2 251.18 C-1.15
4+59.37		1.97 250.45 C 1.52	9.97 250.45 F 0.48	0.85 251.02 F 0.17	2.36 251.02 C 1.34
4+39.37		1.90 250.10 C 1.80	9.58 250.10 F 0.52	0.35 250.70 F 0.35	2.23 250.70 C-1.53

Pepper Drive

INDEVCO Sheet 11186-L

	Rough Grade	curbs		Rough grade
7+66.88 = ch. B.C. on Rt. (2' alloy Rod.)	53.21 252.99 C 0.22	2.55 252.97 F 0.42	2.58 252.97 F 0.39	52.84 252.97 F 0.13
7+16.77 Brk.	50.85 252.44 F 2.09	2.21 252.44 F 0.23	1.78 252.43 F 0.65	52.28 252.43 F 0.15
6+96.77 Brk. 14.67	49.45 252.23 F 2.78	2.28 252.23 C 0.05	1.73 252.23 F 0.50	51.70 252.23 F 0.53
6+82.10 = E.C. 22°-33.94' ch = 5.33 +5.33	49.07 252.10 F 3.03	1.74 252.10 F 0.36	1.65 252.11 F 0.46	1.49 252.11 F 0.62
6+76.77 Brk. 20°-12.99' - ch = 9.98 +10.00	48.79 252.06 F 3.27	1.67 252.06 F 0.39	1.64 252.07 F 0.43	1.48 252.07 F 0.69
6+66.77 15°-48.55' - ch = 9.98 +10.00	48.65 251.99 F 3.34	1.55 251.99 F 0.44	1.59 252.00 F 0.41	1.35 252.00 F 0.65
6+56.77 Brk. 11°-24.11' - ch = 9.98 +10.00	48.36 251.92 F 3.56	1.61 251.92 F 0.31	1.32 251.94 F 0.62	1.37 251.94 F 0.57
6+46.77 6°-59.66" - ch = 9.98 +10.00	8.66 251.86 F 3.20	1.72 251.86 F 0.14	1.25 251.88 F 0.63	1.39 251.88 F 0.49
6+36.77 Brk. Ahead 2°-35.22' = ch = 5.86 +5.97	48.16 251.81 F 3.65	1.17 251.81 F 0.64	1.03 251.83 F 0.80	1.55 251.83 F 0.28

Pepper Dr.

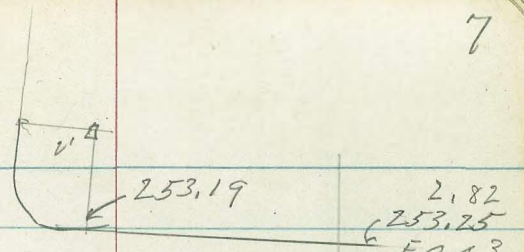
9+96.77	56.05 255.52 C 0.53	5.12 255.52 F 0.40	5.47 255.47 ✓	55.96 255.47 C 0.49
9+76.77 7.59	~~255.30~~	4.64 255.30 F 0.66	4.84 255.23 F 0.39	56.41 255.23 C 1.18
9+69.18 = E.C. R= 55.5' ch. = 26.46 9+69.05 = 2 X 26.45	54.72 255.22 F 0.50	4.65 255.22 F 0.57	4.82 255.15 F 0.33	56.76 255.15 C 1.61
9+42.69 7°-08.4' ch = 26.45	51.74 254.92 F 3.18	4.63 254.92 F 0.29	4.46 254.86 F 0.40	57.10 254.86 C 2.54
9+16.21 5°-21.3' ch = 26.45'	54.47 254.63 F 0.16	4.21 254.63 F 0.42	4.06 254.58 F 0.52	57.14 254.58 C 2.56
8+89.73 3°-34' ch = 26.45	54.91 254.34 C 0.60	3.84 254.34 F 0.50	3.87 254.29 F 0.42	57.37 254.29 C 3.08
8+63.25 df. - 1°-47' ch = 26.45	55.67 254.05 C 1.62	3.73 254.05 F 0.32	3.77 254.01 F 0.24	57.18 254.01 C 3.17
8+36.77 = B.C.	55.77 253.76 C 2.01	3.31 253.76 F 0.45	3.41 253.72 F 0.31	56.11 253.72 C 2.39
7+85 90 = E.C. 2' Rad Alloy ch on Rt	53.88 253.20 C 0.68	2.77 253.17 F 0.40	2.77 253.17 F 0.40	54.37 253.17 C 1.20

3 X 26.45 ch = 26.43

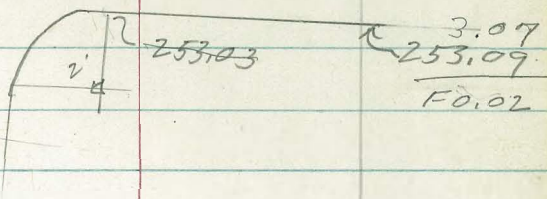
Set as shown on Preliminary notes.

Peppar Dr

7+85.90 253.17



Alloy Blk.31



7+62.88 252.97

10+67.20= Meet sb. + Pave on Rt.	—		7.15 256.70 C0.45	57.25 256.70 C0.56
10+57.76 = Meet Pave + Cb. on Lt.	57.24 256.22 C1.02	5.87 256.22 F0.35		—
10+56.77	256.21	5.84 256.21 F0.37	5.91 256.49 F0.58	57.10 256.49 C0.61
10+36.77	56.77 255.96 C0.81	5.63 255.96 F0.33	5.93 256.10 F0.17	56.92 256.10 C0.82
10+16.77	56.65 255.74 C0.91	5.37 255.74 F0.37	5.91 255.76 C0.15	56.75 255.76 C0.99

Stake Prop. line
S.Ely. side Pepper Dr. + 30th
(Lot #8 - Blk 31)

0+00 = B.C. on 39th

Δ turned - 87°-20'

10' a.c. Def = 7°-09.72' - ch. = 9.97

Set ½ tracks on line as shown below.

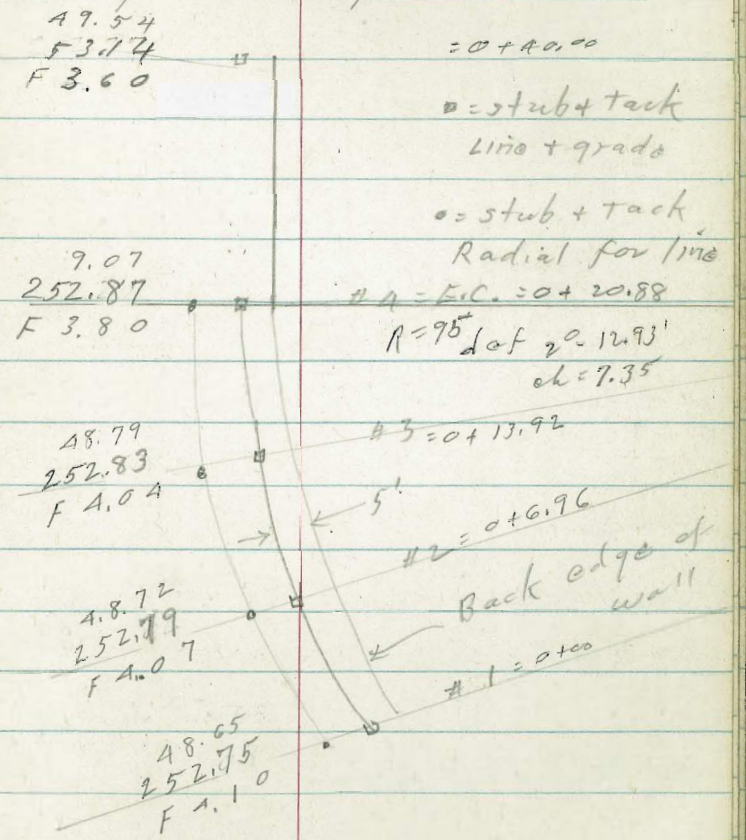
	X-on wall		
	E.C. 0+61.5± 2.10 252.21	0+60	~~252.20~~
Prop. grade set +	F 0.10		
			1.38
		0+50	252.10
			F 0.72
0+61.5± = E.C.	43°-40' Rt.		
			1.40
0+60	42°-58'-32 Rt	0+40	251.99
			F 0.59
0+50	35° 48.60 Rt		
			1.44
0+40	28°-38.88' Rt	0+30	251.90
			F 0.46
0+30	21°-29.16 Rt		
			1.54
0+20	14°-19.44' Rt	0+20	251.84
			F 0.30
0+10	7-09.72 Rt		
			1.54
0+00	0°-0'	0+10	251.87
			F 0.23
	X-on wall		2.11
		0+00	251.70
			C 0.41

Wall - Lot 39 Lexington Park 8
39th + Pepper Drive

Top of wall: Grades set.

stakes - 5' back of back face of wall = (95' Rad. to stake line)

stationing is on Prop. line (R=90')



INDEXED

Sycamore 1-11-55

11487-L

0+00 = Wly line Marigold.

2+50

2+00

1+50 Rt = 177.22

1+00 Lt = 177.22

0+50

0+15 Rt only.

0+05.39 = ob. E.C on Lt.

0+05 = ob. E.C. on Rt.

0+00 = Wly line Marigold

South = Lt. Rt. = North 9

Rough	ob.	ob	Rough
1.45 241.04 C 0.41	241.04 0.56 F 0.48	41.86 1.43 F 0.43	2.98 241.86 C 1.12
1.20 241.42 F 0.22	241.42 0.87 F 0.55	42.25 1.89 F 0.36	3.51 242.25 C 1.26
1.36 241.80 F 0.44	241.80 1.27 F 0.53	42.64 42.24 F 0.40	4.55 242.64 C 1.91
1.51 242.18 F 0.67	242.18 1.70 F 0.48	43.03 2.58 F 0.45	4.55 243.03 C 1.52
3.35 242.56 C 0.79	242.56 2.23 F 0.33	43.42 42.98 F 0.44	4.51 243.42 C 1.09
3.76 242.93 C 0.83	242.93 2.67 F 0.26	243.68 .21 F 0.47	243.68
—		43.79 3.38 F 0.41	5.00 243.79 C 1.21

Sycamore

End ch. - Lt. - wly.

3+59 5/8 = Alloy P.I. on Lt.

3+53 24 = Alloy ch. E.C. on Rt.

3+51 58 = Alloy P.I. on Rt.

3+45.83 = P.U.C.

3+43 02 Alloy P.I. on Lt.

End of ch. Lt.

ch. E.C =

3+41.36 = Alloy ch. B.C. on Lt.

3+35.82 = Alloy line on Rt. = End of ch.

3+33 02 = Alloy B.C. on Rt.

3+00

		240.50 240.47 C 0.03		—
—			41.12 1.11 F 0.01	—
—				—
0.75 240.31 C 0.44				1.43 241.11 C 0.32
— →	End of ch.	1.04 240.46 C 0.58	.29 241.26 C 0.03	wly. = End. on Rt.
240.35 39.86		240.31 39.86 F 0.45		—
—		—	1.73 241.53 C 0.40	241.22 = E.C. ch.
—		—	241.19 1.01 F 0.18	
1.06 240.66 C 0.40		240.66 .27 F 0.39	41.47 1.26 F 0.21	2.15 241.47 C 0.68

Sycamore

A+86.44 = Prop. P.I. on Lt. } No grades
A+79.79 = Prop. B.C. on Lt. }
A+77 38 = cl. B.C. on Lt.
A+81.79 = ℄ Sycamore + (Ely. Line 38 ℄)
A+77.13 = Prop. P.I. on Rt. } No grades
A+67 50 = Prop. B.C. on Rt }
A+65 83 = cl. B.C. on Rt.
A+55 83

A+45 83

A+25 83

A+05 83

3+85 83

3+65 83

3+61 58 = Alley E.C. on Lt.

	43.30 − 3.10 = 40.20 B.C.	46.76 .63 .13	
	43.80 = 3.80 C 2/3	46.50 .70 F 0.10	
3.99 244.10 F 0.11	44.10 = 4.10 C 1/3	46.25 6.00 F 0.25	
→ 3.06 244.22 F 1.16	44.22 3.85 F 0.37	45.87 45.78 F 0.09	657 245.87 C 0.70
24 →	244.10 3.72 F 0.38	—	—
2.29 243.80 F 1.51	43.80 .26 F 0.54	—	—
1.16 242.53 F 1.37	42.53 .20 F 0.33	43.33 3.15 F 0.18	4.56 × 243.33 C 1.23
X 0.39 241.45 F 1.06	41.45 .35 F 0.10	.37 42.25 C 0.12	3.35 X 242.25 C 1.10
0.15 240.73 F 0.58	.97 40.73 C 0.24	41.53 41.67 C 0.14	2.28 241.53 C 0.75
0.32 240.34 F 0.02	57 40.34 C 0.23	41.14 1.00 F 0.14	1.59 241.14 C 0.45
—	40.37 − 40.33 C 0.04		—

INDEVCO

Marigold

1-12-55

67.73

0+00 = Nly line Juniper & ℄ Marigold

curb stakes by F. Osborne

		Lt. = W.			Rt
1+61.72 = B.C. Alley ch. on Lt.			41.43 .33 F 0.10		
1+59.54 ch. on Lt.		1.64 241.40 - ant C-0.24		41.90 .65 F 0.25	46.06 241.90 2° C-4.16
1+39.54 Ont.	143	41.07 240.75 C-0.32	40.75 .32 F 0.43	41.25 40.86 F 0.39	45.78 241.25 C-4.53
1+00 3.60	102	9.95 239.33 C 0.62	39.33 .11 F 0.22	39.81 .67 F 0.14	44.92 239.81 C-5.11
0+71.81 Brk. on Rt.	54	238.31	38.31 .29 F 0.02	.91 38.79 C 0.12	43.58 238.79 C-4.79
0+56.81 = Ch. E.C. + Prop. E.C. on Rt	In 82	9.10 237.77 C-1.33	8.00 37.77 C 0.23	.51 38.48 C 0.03	42.65 238.48 C-4.17
0+29.53 = Prop P.I. on Rt.					
0+06.38 ch. E.C. on Lt.		7.60 235.95 C-1.65	35.95		
0+00 = Nly. Juniper (℄ Marigold)					
0-46.43 = Nail FB 2290 - P.I.	234.50 PK. & Juniper W. Line Marigold				

Marigold

		Lt.			Rt.
2+78 63	= ℄ B.C. Lt.	43.55 242.72 C-0.83	.88 42.72 C 0.16	43.22 3.08 F 0.14	48.00 243.22 C-4.78
2+49 10	= Cl. B.C. on Rt.		.69 42.56 C 0.13	43.07 2.91 F 0.16	
	31.53				
2+47 10	Alley line on Rt	43.69 242.56 C-1.13	= ⊞ end.	43.26 3.00 F 0.26	48.34 243.06 C-5.28
2+23.87	Alley line on Rt.	= E. end		43.13 .05 F 0.08	Nail
	27.56				
2+19.54		42.84 242.41 C-0.43	.43 42.41 C 0.02		48.38 242.91 30 C-5.47
2+11 31	= Cl. B.C. on Rt.			42.86 .60 F 0.21	
1+99 56	Cl. E.C. on Lt.	42.52 242.22 C-0.30	42.21 1.99 F 0.22	42.72 .53 F 0.19	48.76 242.72 C-6.04 40
88.99 = Nail 1+86.99	Alley line on Lt.	= W. end.	.80 42.20 C 0.60		
1+79.54		42.13 241.89 C-0.24		42.39 2.10 F 0.29	48.17 242.39 C-5.78
1+63.76	= Alley line on Rt.	= W. end.	.98 41.68 C 0.30		

Marigold

						Rt.	
4+33 26	Cl. E.C. on Lt.		45.06 244.58 C-0.48		44.58 4.32	Fo.06	—
				2/3	4.29 44.25	C0.04	
4+25 26	= Nly line Sycamore		43.79 = P.C.	1/3	44.00 3.61	= 0.39	—
			— E.C. = Meet.		43.00 .42 93		
4+19 34			—			44.62 4.41 F 0.21	48.35 244.62 C-3.73
				2/3	43.08 43.00 C0.09		
3+99 34			—			4.17 44.14 C 0.03	47.74 244.14 C-3.60
				1/3	43.11 43.08 C0.03		
3+75 26	= E.C. = Nly line Sycamore Def. Δ 24°-53'-30" ℓ ch = 15.80		5 —			3.85 43.78 C 0.07	47.63 243.78 C-3.85
3+65.42	= Cl. P.C.C. on Lt. 22°-21.42' ch = 17.48'	= PCC.	43.62 243.16 C-0.46		43.25 43.16 C 0.09		—
3+59.34	Brk. 20°-47.45' ch = 19.48 ch = 17.10	4	43.69 243.14 C-0.55	10	3.25 43.13 C 0.12	.70 43.66 C 0.04	47.48 243.64 C-3.84
3+40 ℓ Rate = 15.45'	15°-48.53' ch = 19.90 ch = 19.90	3	43.81 243.03 C-0.78	.10	3.22 43.03 C 0.19	43.55 .35 Fo.20	46.96 243.53 C-3.43
3+20 Lt	10°-39.41' ch = 19.90	2	43.66 242.93 C-0.73	.10	42.93 2.93 C	43.44 .20 F0.24	47.64 243.43 C-4.21
3+00 Lt	5°-30.29' ch = 21.32	1	43.66 242.83 C-0.83		3.00 42.83 C 0.17	43.33 .26 F0.07	46.91 243.33 C-3.58

Marigold

6+65 3/4	= ℄ Hub. = E.C. New End.		2/28/55 1.18 251.25 F 0.07	51.28 50.79 F 0.46	1.29 251.75 F 0.46 2-28-55	2-28-55 1.09 251.40 F 0.31
5+85 20	= End Job. 70-37-14" ch. 9.96	Restaked 4-9-55 staked wrong.	52.10 250.90 C-1.20	50.96 0.86 F 0.44	51.78 1.21 F 0.54	T.B.M. 252.65 + 1.00 251.40 C-1.25
5+75 22	= Mid curve ℄ Ch. = 9.96	D = 30-48'-30"	51.55 250.48 C-1.07	50.48 0.18 F 0.30	50.98 0.76 F 0.22	52.32 250.98 C-1.34
5+68.57	= E.C. Alley Ch. on Lt.		0.41 50.90 F 0.49 2/28/55	50.18 0.03 F 0.15		0.78 250.98 F 0.20 2-28-55
5+65 25	= Nly line Alley ℄ = B.C. Nt	81	50.56 250.05 C-0.51 To Alley	50.09 - F 0.06 0.03 0.72 50.21 C 0.51	50.55 50.19 F 0.36	51.97 250.55 C-1.42
5+50 25	= Sly line Alley. on Lt. on ℄ Road		W. end - N.	9.69 49.61 C 0.08		
5+46 25	Alley Ch. B.C. on Lt. 197		To Alley 4— 49.40 249.23 C-0.37	49.49 F 0.50 8.99 49.24 8.99 F 0.25	49.73 9.16 F 0.57	51.59 249.73 C-1.86 2.13
5+00 40.66	173		48.24 247.26 C-1.00	47.26 7.12 F 0.14	47.76 7.36 F 0.40	50.15 247.76 C-2.39
4+59 34	curb stakes by F.O.		45.65 245.53 C-0.12	45.53 5.40 F 0.13	46.03 5.94 F 0.09	49.20 246.03 C-3.17
4+39 34			45.21 244.75 C-0.46	44.75 4.70 F 0.05	45.25 5.06 F 0.19	48.67 245.23 C-3.42

INDEXED

Juniper

		Rough	Ck
r 40'			
1+59.54 (10)		2.79 232.70 C0.09	2.15 232.70 0.55
40'			
1+19.54 (19.10) Brk.		2.63 232.46 C0.17	2.26 232.45 F0.19
1+03.20 (12.76)			2.20 232.40 F0.20
1+02.75 = E.C. Curb		3.17 232.36 C0.81	2.50 232.36 C0.14
39th St.			
0+21.87 (56) = Ol. B.C.		30.08 230.95 F0.87	2.64 30.95 C1.69
0+16.26 (+16.00)			2.25 30.80 C1.45
0+05.76 (05.50)			0.95 30.52 C0.43
0+00 (+01) = wly end Contract.		18.42 230.37 F1.95 Nail	29.53 30.40 F0.87

F Back

Juniper

	Rough	cl.	
3+59 92 = R.K. = ℄ Marigold			
3+14 60 .34 = cl. B.C. on Lt. (Marigold)	3.68 233.89 F ~~1.13~~	3 79 233.69 C 0.10	
2+99 06 Brk.	3.72 233.55 Co.17	3 41 233.55 F 0.14	
2+79 06 Brk. 1.60 ℄ 39.52	4.49 233.41 C 1.08	3 10 233.41 FO.31	
2+39 54 9.59	2.75 233.18 FO.43	2 38 233.18 FO.80	
2+30 33 .20 = Alley cl. E.C. ~~19.94~~ 21.15	2.23 233.12 FO.89	2 26 233.12 FO.86	2 18 233.35 F 1.17
2+09 17 -.04 = Alley cl. B.C. 10.50	2.39 233.00 FO.61	2 03 233.00 F 0.97	2 15 233.24 F 1.11
1+99 54 .10 10.50	2.33 232.94 FO.61	2 20 232.94 F 0.74	

Alley lines + Pivot

Juniper

	Rough G.	curb
6+57.36 P.R.V.C.	9.03 245.00 C 4.03	4.92 245.00 F 0.08
6+37.36	9.90 245.38 C 4.52	5.45 245.38 C 0.07
6+17.36	~~245.58~~	5.62 245.58 C 0.04
5+97.36	50.76 245.63 C 5.13	5.63 245.63 X
5+77.36	50.13 245.45 C 4.68	5.48 245.45 C 0.03
5+57.36	8.00 245.03 C 2.97	4.81 245.03 F 0.22
5+35.95 = Plan Match line	5.42 244.32 C 1.10	4.18 244.32 F 0.14
5+17.36	~~5.42 243.49~~	3.37 243.49 F 0.12
4+97.36	4.83 242.37 C 2.46	2.42 242.37 C 0.05
4+62.09 cl. E.C. on Lt.	2.51 240.09 = prop. C 2.42	0.06 240.14 = cl F 0.08

Juniper

8+33 86	3.72 243.63 C 0.09	3.50 243.63 F 0.13
8+13 86	3.59 243.22 C 0.37	3.19 243.22 F 0.03
7+93 86	3.48 242.95 C 0.53	2.94 242.95 F 0.01
7+82 12	~~242.80~~	2.78 242.80 F 0.02
7+73 86	4.32 242.77 C 1.55	2.67 242.77 F 0.10
7+53 86	4.67 242.77 C 1.90	2.66 242.77 F 0.11
7+33 86	6.15 242.90 C 3.25	2.82 242.90 F 0.08
7+13 86	7.32 243.30 C 4.02	3.30 243.30 X
6+93.36	7.65 243.90 C 3.75	3.82 243.90 F 0.08

Juniper

10+11.34 = ℄ Juniper + wly Tulip

10+06.88 = wly line Tulip + wly line Juniper

9+98.35 = N.B.C. on Lt.

9+85.54 Brk. 50.36

9+35.18 50.37

8+84.21 = E.C. Alley Cl. 21.38

8+63.43 = Cl. B.C. (Alley) 9.57

8+53.86 E.V.C.

Prop Cr.

252.10

2.94
251.54
C 1.40

2.26
250.57
C 1.69

9.49
248.17
C 1.32

5.69
245.77
F 0.08

~~244.70~~

4.11
244.25
F 0.14

252.17

1.31
251.54
F 0.23

0.45
250.57
F 0.12

8.11
248.16
F 0.05

4.76
245.74
C 0.98

4.30
244.73
F 0.43

4.05
244.25
F 0.20

Cl.

5.05
245.81
F 0.76

Alley ∞ + prop.

4.25
244.92
F 0.67

N.W'ly Cl. Rot

Juniper + Marigold

stake line (Rad = 115.40) Rate = 14.888'

Curbs.

E.C. on Marigold

235.95	E.C. #6	Curb. 6.29 235.95	Rough Gr. 7.60 235.95	
	20°-06'-30"	C 0.34	C 1.65	
235.40	#5	5.75 235.40	7.38 235.40	
	16°-21'	C 0.35	C 1.98	
234.90	#4	5.87 234.90	7.25 234.90	
	12°-36	C 0.97	C 2.35	
234.45	#3	4.92 234.45	7.00 234.45	
	8°-50'	C 0.47	C 2.55	
234.10	#2	4.50 234.10	6.64 234.10	
	5°-05'	C 0.40	C 2.54	
	ch. 15.17			
233.81	#1	3.92 233.81	233.81 F 0.41	
	1°-19'	C 0.11	x.40	
	ch. 5.38			
233.69		233.69	233.69 F 0.32	

#0 = B.C. Juniper

N.Ely. Cl. Rot.

Juniper + Marigold

35.95 F 0.15
.40

E.C. Marigold #1 — 8.55 238.48 C 0.07

35.40
.15
F 0.25
#2 — 8.32 238.47 F 0.15

34.90
.68
F 0.22
#3 — 8.44 238.53 F 0.09

34.45
34.38
F 0.07
#4 — 9.04 238.90 C 0.14

34.10
33.92
F 0.18
#5 — 9.54 239.55 F 0.01

B.C. Juniper #6 — 0.06 240.14 F 0.08

Wly. ck. Rat.
39th & Juniper

INDEXED

Ely. ck. Rat.
39th & Juniper

		E.C.	2.50 232.36 C 0.14 (5)
E.C. - 39th	1.15 231.37 F 0.22	Restake. ←	E.C. Inlet #3	3.09 232.30 C 0.79 (5)
# 1/3	~~1.79~~ 231.20 C 0.58		#2	2.38 232.31 C-0.07 (5)
# 2/3	3.04 231.10 C-1.94		#1	2.18 232.31 F 0.13 (3)
B.C. Juniper	2.64 230.95 C-1.69		B.C. - 39th	2.50 232.50 Grade Existing Ck

Soap Box Derby Track.
Finish grades.

G.B. 317
45

4-10-55
W.O. 29006
Ref. G.B. 317-P 45
F.B. 2170

Finish grade in

C.H.S.
Bogy
Pullen
Schellin

16+00
~~0+00~~ end of slow down ramp =
= (16+00 - G.B. 317. P-51.

Backed stations in

13+50

14+00

14+50

15+00

15+50

16+00
~~0+00~~

Note

Grades shown are Profile Grades
Grades set are 1.13 above
grades shown in notes.

Track raised 1.00 to assure
drainage at low point. C.H.S.

Parks

19.10 19.10

Soap Box Derby Track.
Finish grades.

Finish grade in G.B. 317
45

4-10-55
W.O. 24006
Ref. G.B. 317-P 45
F.B. 2170

C.H.S.
Begg
Pullen.
Schelm

16+00
~~0+00~~ end of slow down ramp =
=(16+00 - G.B. 317. P-51.

Backed stations in

13+50

14+00

14+50

15+00

15+50

16+00
~~0+00~~

Note

Grades shown are Profile Grades
Grades set are 1.13 above
grades shown in notes.

Track raised 1.90 to assure
drainage at low point. C.H.S.

19.10 19.10

Rake @ 1/0

10+70			
11+20			
11+60	P.V.C.	15.90	15.90
11+80		15.58	15.58
12+00 =	Finish line	15.40	15.40
12+20		15.38	15.38
12+~~40~~	E.V.C.	15.50	15.50
12+80			
13+00			

Rake

Rake

7+40	Rake @ 6%		
7+65			
7+90	P.V.C.	24.90	24.90
8+10		23.80	23.80
8+30		22.90	22.90
8+50		22.20	22.20
8+70	E.V.C.	21.70	21.70
8+95	↑		
9+20			
9+45			
9+70			
9+95			
10+20	↓ Rake @ 2%		
10+45			

Rake

Rake

3+50		
~~3+70~~		
3+70	E.V.C.	
~~3+40~~	~~= E.V.C.~~	
3+65	—	El: 3+65 = 50.40 take out
3+90		
4+15		
4+40		
4+65		
4+90		
5+15		
5+40		
5+65		
5+90		
6+15		
6+40		
6+65		
6+90		
7+15		

51.40	51.40
~~53.45~~	~~53.45~~
50.00	50.00
~~51.90~~	~~51.90~~

changed. From 3+70 to 4+00 4/17/53

Revised

7.56
58 8.64

2+15 = B.k.		71.30	71.30
2+14.67 =		56.64 ✓	56.64 ✓
	℄ R = 5417		
2+24.67 = starting line = E.C.		65.04 ✓ ~~69.37~~	~~69.37~~ 65.04 ✓
~~2+60 P.V.C.~~		~~62.30~~	62.30
~~2+80~~		~~58.65~~	~~58.65~~
2+90 P.V.C.		58.00	58.00
~~3+00~~		~~55.70~~	~~55.70~~
3+10		55.40	55.40
3+30		53.20	53.20

Alvarado Sewer lines in Waring Tract. To crossing #7

4-12-55

INDEXED

sheet 2831-D

F.B. 2040-P32

El. = 349.67

B.M. = Existing M.H. #37 - (2831-D) F.B. 2040-32

stakes C/L of ℄

2+12.25 = Meet existing crossing #7

1+69.80

1+27.35

0+84.90

0+42.45

Δ to Lt. (off Alvarado sewer) 76°-30' at sta 167+66.66 = 0+00 branch line

8.30
352.60
C 5.70

7.72
352.11
C 5.61

7.40
351.63
C 5.77

7.55
351.15
C 6.40

7.75
350.67
C 7.08

0+00

7.60
350.19
C 7.41

Alvarado line
To crossing #9

4/12/55

2831-D

B.M. = Existing M.H 0+00 EL. = 326.80
Rim EL. = 337.32

stakes 6' Rt of ℄

2+64.25 — A-X- 42.125'

2+22.12

1+80 = Brk

1+35

0+90 — A-X-45'

0+45

0+00

149+87.45 (F.B. 2040-P28) =
& Lt. of 74°-57' off Alvarado line sta.

52 55
342.42
C 10.13

48.11
338.21
C 9.90

41.01
334.00
C 7.01

7.97
332.37
C 5.60

8 43
330.75
C 7.68

3718
329.12
C 8.06

35 50
327.50
C 8.00

To crossing # 9

3+88.5 = Meet existing crossing # 9

3+58.5 = start Conc. casement.

3+48.50 = M.H. # A

3+06.37

9.36
352.20
C 7.16

6.70
350.84
C.5 86

54 33
340.63
C 7.70

TP 5.15

Alvarado line to Crossing #6-A

4/11/55

stakes 6' Rt of ℄

□ in top of dam Ely edge of state College grounds. EL. = 320.11

7.66

327.77 π

2.48

325.29

6.32

331.61

3.50

328.11 = Ely Rim

4.86

332.99

6.78

326.19

3+53.12 A.S.

3+06.56 A.S.

T.B.M.

2+60 = M.H. #2

2+08

1+56

1+04 S.S.

0+52

0+00 = M.H. #1

Alvarado line (F.B. 2040-P.26) ~

Δ-Lt. of 78°-45' off sta 138+44.55

#31

M.H. 135+73.84

F.B. 2040-Page 26

6.19

320.01 = M.H. #2

C 6.18

6.59

330.75

C 5.84

33.67

327.38

C 6.29

30.75

324.01

C 6.74

9.75

323.32

C 6.43

8.52

322.64

C 5.88

8.45

321.96

C 6.49

8.59

321.28

C 7.31

6.19

320.60 = 0+00

C. 5.59

To crossing # 6-A.

4+66.25 = meet existing crossing # 6-A.

4A 12
337.90
C 6.22

4+57. = start conc. casement

4+46.25 = M.H. # 3

43.73
337.50
C 6.23

3+99.68

40.82
334.12
C 6.70

Hilltop - west of 39th St.
Sewer Extention.

~~9~~ 4-20-55

W.O. 20009

stakes 2' Right of ℄

76.91
169.82 0+51 ——— ℄ Hilltop
7.09

76.09
169.38 0+34
C6.71

76.72
168.94 0+17
C 7.78

2.6%

0+00
168.50 meet pipe I.E. End of existing 6" sewer
Sheet 3723-L

W021037 Storm Drain Lots 7-8 & 9
Blk 23 Fairmount Add.
(Estrella South of Polk
5/2/55

FB 2212 - page 7
sheet 5617-B.
stakes 10' Rt: Looking North

0+78 - Existing drain Lot #7 Nly. side	15 82 306 22 C 9.60	
0+52	10 88 306 10 C 4.78	
0+26	9 38 305.97 C 3.41	
0+00 - Existing drain Sheet 5617-B Nly line Lot #10	8 53 305.85 C 2.68	

Conde Street

Congress to Moore

5/3/55
W.O. 32209

1+60	0 5'	3.58 11.61 C 1.97	11.61	12.11	3.41 12.11 C 1.31	3'
1+40	0 5'.	3.77 11.78 C 1.99	1185 11.78 C 007	1226 12.28 F 0.02	3.9 12.28 C 1.4	0 8'
1+20	0 5'	3.98 12.17 C 1.81	1237 12.17 C 0 15	1262 12.67 F 0 05	3.18 12.67 C 0.51	3'
1+00	0 5'	4.14 12.75 C 1.39	1770 12.75 F 0.05	1318 13.25 F 0.01	4.10 13.25 C 0.85	3'
0+80 = P.V.C.	0 5'	4.34 13.55 C 0.79	1359 13.55 C 0.04	1403 14.05 F 0 02	5.37 14.05 C 1.32	IV. 0.36 IN
0+44	Line	5.55 15.17 C 0.38	1515 15.17 F 002	1569 15.67 E 0.02	6.02 15.67 C 0.35	IV. 0.18 IN
0+08 = C.E.C.	Line	7.26 16.79 C 0.47	1677 16.79 E 0.02	1767 17.29 C 0.38	8.52 17.29 C 1.23	N 0.32 IN
0+00 = W/y line Congress		17.25			17.68	

Condo.

3+00 = Ely. line Jefferson		6.13 13.87 C 2.25			15.75
2+95 = ch. B.C. on RT.		—		15.91 15.56 C 0.35	20.45 15.56 1' C 4.89
2+85 = ch. B.C. on LT. 2+67.5 on RT. only		16.50 14.68 C 1.82	14.73 14.68 C 0.05	4.69 = 2+67.5 sta. 14.52 C 0.17	
2+40 E.Y.C.		13.89 12.97 C 0.92	3.20 12.97 C 0.23	13.48 13.47 Grade	16.69 13.47 C 3.22
2+20		13.14 12.31 C 0.83	12.56 12.31 C 0.25	12.67 12.81 F 0.14	16.26 1' 12.81 C-3.45
2+00		13.22 11.88 C 1.34	12.09 11.88 C 0.21	12.31 12.38 F 0.07	15.00 N. 12.38 0.81h C-2.62
1+80		3.41 11.63 C 1.78	11.60 11.63 F 0.03	11.98 12.13 F 0.15	13.68 3' 12.13 C-1.55

Conde

1+60	4.51 5' 4.54 F0.03	4.46 4.54 F0.08	5.06 4.96 C 1.10	8.68 4.96 C3.72	3'
1+40	6.05 5' 5.23 C0.82	5.18 5.23 F 0.05	5.55 5.76 F 0.21	11.26 5.76 C5.50	5'
1+20	5.92 5' 6.13 F0.21	5.83 6.13 F 0.30	6.47 6.73 F 0.26	14.60 6.73 C7.87	5'
1+00	6.95 5' 7.22 F0.27	7.30 7.22 C 0.08	7.68 7.89 F 0.21	14.44 7.89 C6.55	Lino
0+80 Map. P.V.C.	7.56 5' 8.50 F0.94	8.13 8.50 F 0.37	9.27 9.24 C 0.03	16.02 9.24 C6.78	0.43 IN
0+45	09.50 5' 10.90 F 1.40	10.57 10.90 F 0.33	11.58 11.76 F 0.18	17.87 11.76 C 6.11	0.44 IN
0+10 = Ab. E.C. on Lt.	11.45 5' 13.31 F 1.86	13.42 13.31 C 0.11		—	
0+05 = Ab. E.C. on Rt.	—		4.76 14.64 C 0.12	19.52 14.64 C4.88	0.33 IN
0+00 = Wly line Jefferson	13.20			15.00	

Conde

3+00	~~Rt. only~~ Ely. line	Moore St	End of ob.		3.07 3.18 F0.11	2.66 2.70 F0.04	3.28 Line 2.70 C0.58
2+90	ob. B.C. Lt. only			1' 3.01 3.20 F0.19	3.16 3.20 F0.04		
2+55	Rt. only					2.88 3.24	3.20 0½ 3.24 IN
2+50	Lt. only			Line 3.82 3.45 C0.37	3.28 3.45 F0.17	F0.36	F0.04
2+10				Line 4.22 3.69 C0.53	3.56 3.69 F0.13	3.20 3.78 F0.58	3.56 0⅘ 3.78 IN F0.22
2+00 = E.V.C.				Line 4.42 3.76 C0.66	3.60 3.76 F0.16	3.48 3.92 F0.44	5.95 0.2 3.92 Back. C2.03
1+80				5 4.24 4.06 C0.18	3.90 4.06 F0.16	4.28 4.35 F0.07	5.25 0⅘ 4.35 IN C0.90

INDEXED

Harney St.

Congress to Jefferson

1+75			25.18 ✓ G.		
1+70		—		5.20 25.28 F0.08	5.16 ◻ 0.50 25.28 F0.12
1+50 O. on Lt.			25.05 ✓ G		
1+40= E.V.C.		—		5.12 25.16 F0.04	5.45 25.16 C0.29
1+25			24.99 ✓ G		
1+20		—		5.20 25.07 C0.13	5.39 25.07 C0.32
			Meet P.C.		
1+00		25.37	24.73 ✓ G	4.95 24.85 C0.10	4.96 24.85 C0.11
0+80	◻ L.	4.63 25.13 F0.50	4.66 25.13 F0.47	4.75 24.81 F0.06	5.34 24.81 C0.53
0+60 P.V.C.	N -0.1	4.98 24.82 C.1.6	4.36 24.82 F0.46	4.51 24.64 F0.13	4.52 24.64 F0.12
0+34			3.91 24.21 F0.30	4.27 24.35 F0.08	
0+08= ℄ E.C.		3.05 23.60 F0.55	3.48 23.60 F0.12	4.15 24.06 C0.09	4.13 24.06 C0.07
0+00= Sly line Congress					

Harney

	Wly. cl. Rot. Line of Jefferson.		4.80 24.57 C 0.23	
	Wly. cl. Rot. Line of Harney		4.72 24.75 F 0.03	
Middle of Return			25.52 25.32 C 0.20	
2+98 21 = Nly line Jefferson		25.11 ✓ = G		
2+93 21 = cl B.C. on Rt.	—		5.46 25.41 C 0.05	5.10 B 25.41 0.50 F 0.29
2+75	—		5.42 25.47 F 0.05	5.16 D 25.47 0.30 F 0.31
2+50	—	25.39 ✓ = G	5.47 25.50 F 0.03	5.22 D 25.50 0.50 F 0.28
2+25	—	25.35 ✓ G.	5.50 25.47 C 0.03	5.54 D 25.47 0.50 C 0.07
2+00	—	25.31 ✓ = G	5.37 25.40 F 0.03	5.55 D 25.40 0.50 C 0.15

HARNEY St.

Jefferson to Moore

1+97 ⁵⁄₈			9.31 16.18 C-3.13	6.33 16.18 Co.15	5.73 15.68 Co.05	8.30 15.68 C-2.62	
1+77.03 =			22.17 18.53 C-3.64	8.39 18.53 F 0.14	8.40 18.03 Co.37	20.65 18.03 C 2.62	□ 3'
1+60		N 3'	2.51 20.45 C 2.06	1.38 20.45 C 0.93	9.90 19.95 F 0.05	21.60 19.95 C 1.65	□ 3'
1+40		N. 0.30 in	3.17 21.93 C 1.24	2.76 21.93 F 0.23	1.49 21.43 Co.06	3.03 21.43 C 1.60	□ 3'
1+20		N. 5⁵⁰/₁₂ in	3.12 22.98 Co.04 1 Mcat ck.	3.24 22.98 C 0.26 ~~123.43~~	2.68 22.48 Co.20	2.87 22.48 Co.39	X 1'
1+05	123.43 ✓						
1+00 P.V.C.					3.20 23.10 Co.10	3.16 23.10 Co.06	□ 0.40
0+50 ⁵⁰			—		4.24 24.10 Co.14	3.94 24.10 F 0.16	□ 0.50
0+05 ⁵⁰ = Cl. E.C. on Rt.			—		~~4.69~~ ~~24.82~~	4.61 24.82 F 0.21	□ 0.50
0+00 = S/y line Jefferson					Return see p. 41		

Harmony

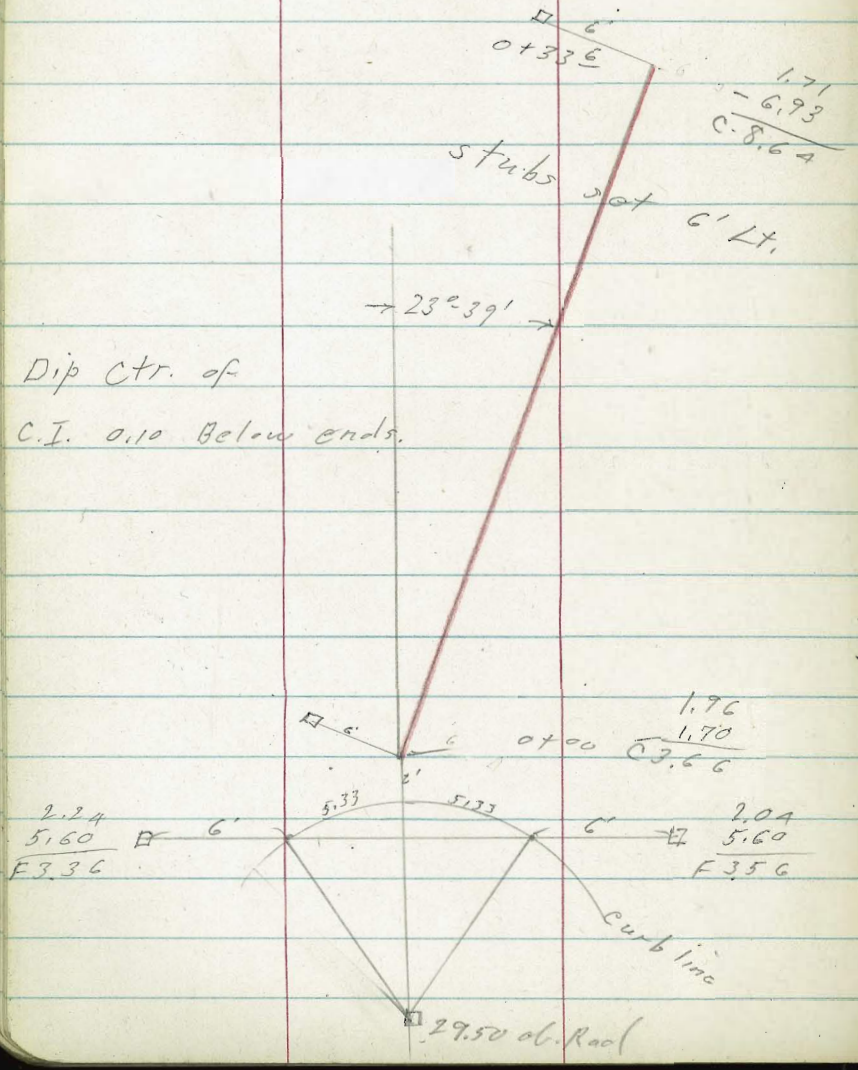
A.80

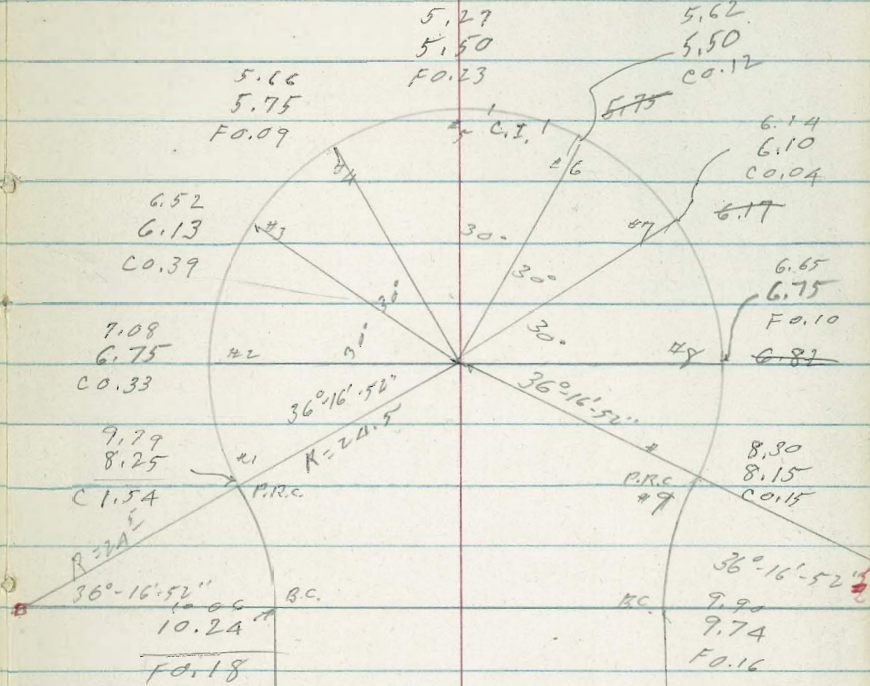
See page 44 for Banjo + Drain

2+97.53 = end of Harmony St.	2.00 4.97 F 2.97	—	—	1.67 4.97 F3.30
2+68.03 = Rad. = Ctr. Banjo	6.08 6.75 F 0.67	—	—	5.68 6.82 F1.14
2+53.53 = P.R.C. Banjo	~~8.25~~	—	—	~~8.15~~
2+39.03 = ℄ B.C.	13.18 10.24 C-2.94	10.06 10.24 F0.18	7.90 9.74 C0.16	8.98 9.74 F0.76
2+27.03	14.51 11.90 C-2.61	5.04 11.90 C-3.14	1.45 11.40 C0.05	14.14 11.40 C2.74
2+17.03	5.84 13.40 C 2.44	4.00 13.40 C0.60	2.75 12.90 F0.15	14.64 12.90 C1.74

Harney St.
Banjo + Drain

2.85

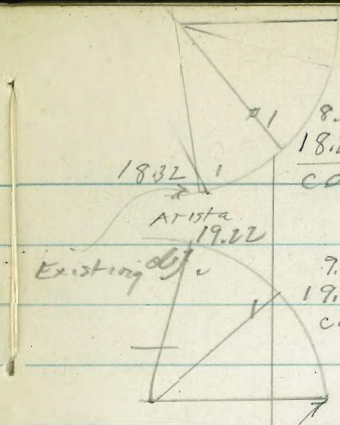




INDEXED

Jefferson

Ampudia to Arista 5/24/57



3+00 = S.Ely. Arista St					0.86 20.50 C0.36	2.38 20.50 C1.88
2+90= cl. B.C. Lt.		0.15 20.45 F0.30	20.39 20.45 F0.06			—
2+50		2.33 22.27 C0.06	F0.10		C0.22	7.78 22.80 C4.98
2+00		3.85 24.50 F0.65	F0.12		F0.17	8.60 25.07 C3.53
1+50	4.47% Lt 4.55% Rt	4.85 26.73 F1.88	F0.13		F0.47	31.04 27.34 C3.70
1+00		8.88 28.96 F0.08	F0.15		C0.80	32.94 29.61 C3.33
0+50		1.70 31.19 C0.71	C0.52		C1.10	4.18 31.88 C2.30
0+00= c&G.C N.Ely. Ampudia		33.42 ✓	33.42		3.91 34.15 F0.24	34.15 ✓

4+80	N.L 10.21 E 9.23 C 0.98	9.23 9.23 X	9.50 9.73 F 0.23	11.86 9.73 C 2.13	D-L
4+60	N 1.95 0.12 in 10.27 C 1.68	0.07 10.27 F 0.20	0.55 10.77 F 0.22	2.11 10.77 C 1.34	D-L
4+40 = P.V.C.	N 3.47 0.4 in 11.63 C 1.84	1.44 11.63 F 0.19	1.91 12.13 F 0.22	3.12 12.13 C 0.99	D-L
4+00 Lt only	D 5.60 L 14.69 C 0.91	4.93 14.69 C 0.24		—	
3+95 Rt only	—		5.34 15.58 F 0.24	6.35 15.58 C 0.77	D-L
3+60 = ch. E.C. on left. only	D 8.20 Little 17.74 C 0.46	7.96 17.74 C 0.22		—	
3+50 = N.wly Arista Rt. only	—		9.23 19.02 C 0.21	20.50 19.02 C 1.48	D-L
3+26 Rt.	—		9.88 19.75 C 0.13	20.80 19.75 C 1.05	D-L
3+14 Rt.	—		20.15 19.85 C 0.30	21.11 19.85 C 1.26	D-L

Jefferson

Returns on P-55.

6+50 = S. Ely. Condo		—			—
6+37 = cl. B.C.	D-1'	11.23 13.37 F 2.14	3.30 13.37 F0.07	4.00 13.87 C 0.13	15.55 13.87 D-L C 1.68
6+20	D'	9.42 11.89 F 2.47	2.07 11.89 C0.18	2.17 12.39 F 0 22	13.43 D-L 12.39 C 1.04
6+00	D-L	9.10 10.44 F 1.34	0.58 10.44 C0.14	0.45 10.94 F 0 49	11.17 D-L 10.94 C 0.23
5+80	D-L	8.65 9.33 F0.68	9.45 9.33 C0.12	9.57 9.83 F0.26	10.92 D-L 9.83 C1.09
5+60	D-L	8.43 8.53 F0.10	8.50 8.53 F0.03	9.22 9.03 C0.19	10.04 D-L 9.03 C0.99
5+40		8.07	on C.I. 8.07 L	8.79 8.57 C0.22	11.55 D-L 8.57 C2.98
5+20		7.57 8.13 F 056	8.00 8.13 F0.13	8.67 8.63 C-0.04	11.30 D-L 8.63 C 2.67
5+00	N-L	9.42 8.52 C 0.90	8.50 8.52 F0.02	8.87 9.02 F0.15	11.32 D-L 9.02 C2.30
5					

JEFFERSON

Conde to Harney

1+60		4.71 25.06 F 0.35	5.06 25.06 X		25.56
1+40	D-0.2	4.58 24.84 F 0.26	4.84 24.84 X		
1+20	D-0.2	4.30 24.57 F 0.27	4.60 24.57 C 0.03		
1+00	D-0.1	4.22 24.27 F 0.05	4.27 24.27 X		Existing ℄
0+77	D-L	3.77 23.37 C 0.40	3.35 23.37 F 0.02		~~23.87~~
0+57	D-0.1	2.88 22.03 C 0.85	2.13 22.03 C 0.10	2.56 22.53 C 0.03	3.32 22.53 D-1' C 0.79
0+37	D 1'	2.63 20.13 C 2.50	0.21 20.13 C 0.08	0.72 20.63 C 0.09	2.61 20.63 D-0.2 C 1.98
0+08 = ℄ E.C.	D-L	20.43 16.65 C 3.78	6.56 16.65 F 0.09	7.45 17.15 C 0.30	20.42 D-0.10 17.15 C 3.27
0+00 = N.W'ly line Conde.					

JEFFERSON

3+00

2+80

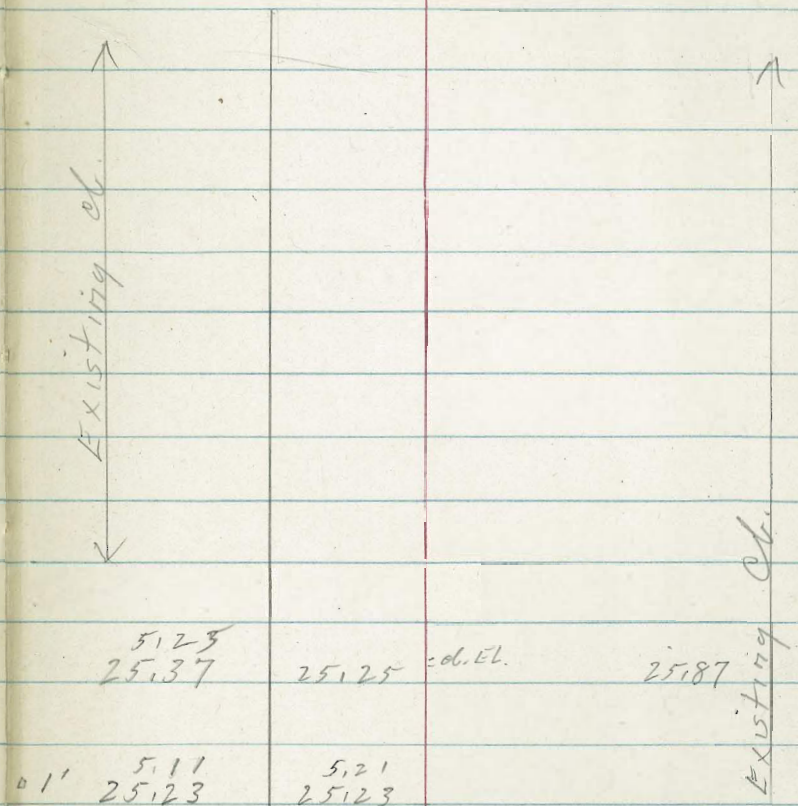
2+60

2+40

2+20

2+00

1+80



JEFFERSON

Harney to N.wly end of Job

2+12.28 = B.C. ch.		3.57 N.	4.82	3.88	4.16	
	□-1'	23.85	23.85	23.97	23.97	□-1'
		F 0.28	C 0.97	F 0.09	C 0.19	
1+87.78 = E.C.		3.62 N.	4.93	4.82	4.43	
	□-1'	23.90	23.90	24.12	24.12	□-1
		F 0.28	C 1.03	C 0.74	C 0.31	
1+75.28 = P.R.C.		3.73	4.02	4.29	4.51	□
	□-1'	23.95	23.95	24.20	24.20	0.3' in
		F 0.22	C 0.07	C 0.07	C 0.31	
1+62.78 = ch. B.C.		3.63	23.99	4.29	4.70	□
	□-1'	23.99	23.99	24.29	24.29	0.5 in
		F 0.36	×	×	C 0.41	
1+23.33		3.94	4.09	4.53	4.53	
	□-1'	24.18	24.18	24.53	24.53	×-1'
		F 0.24	F 0.09	×	×	
0+83.89		4.14	4.35	4.75	5.12	
	□-0.5'	24.38	24.38	24.78	24.78	□-1'
		F 0.24	F 0.03	F 0.03	C 0.34	
0+44.45		4.34	4.44	5.13	4.81	□-1'
	□-0.5'	24.57	24.57	25.02	25.02	
		F 0.23	F 0.13	C 0.11	F 0.21	
0+05 = Ch. E.C.		4.58	4.72	5.38	5.21	
	□-0.5'	24.77	24.77	25.27	25.27	□-1'
		F 0.19	F 0.05	C 0.11	F 0.06	
0+00 = N.Wly line Harney						

39.44 ½ A Times

check plans?

1+25 End of Job.

2+22.28 = E.C. ob

			4,05 23,90 D-1 C 0.15
D-1 2,91 23,80 F 0,89			
stub 4' Radial — 4	3,48 23,80 F 0.32	3,94 23,90 C 0.04	4 — Nail 4' Radial —

INDEXED

MOORE ST.

Trias to Ampudia

1+90		P.K. 9.96 2' in 29.67 C 0.29	30.01 29.67 C 0.34	3'		30.67
1+70		□ 9.76 2' in 29.80 F 0.04	9.80 29.80 ✓	3'		30.80
1+50		□ 9.98 3' in 29.80 C 0.18	9.95 29.80 C 0.15	3'		30.80
1+30		□ 9.96 3' in 29.67 C 0.29	9.88 29.67 C 0.21	2'		30.67
1+10		□ 9.78 3' in 29.40 C 0.38	9.71 ~~9.70~~ 29.40 C 0.31	2'		30.40
0+90 P.V.C.		3' in 9.39 □ 29.00 C 0.39	9.31 29.00 C 0.31	2'		30.00
0+45		□ 8.84 3½ in 28.00 C 0.84	8.68 28.00 C 0.68	2'		29.00
0+00 = N.W'ly Trias St. = ℄ P.C.		□ 7.89 4' in 27.00 C 0.89	8.61 27.00 C 1.61	N. 2'		28.00

Moore

3+00 = S. Ely. Ampudia Jr. B.C.		28.00	8.27 28.00 C 0.27	3'	29.00
2+55	D 2' IN	8.93 28.70 C 0.23	8.92 28.70 C 0.22	3'	29.70
2+10 = E.V.C.	D 2' IN	9.74 29.40 C 0.34	9.71 29.40 C 0.31	3'	30.40

Moore St.

Ampudia to Arista

Returns – P. 55

3+00 = S. Ely. Arista	D-5'	8.12 25.00 C 3.12	A. 95 25.00 F 0.05		7.64 D-line 25.03 C 2.61
2+90 = Cl. B.C. on Rt.	D-5'	8.13 25.10 C 3.03	—	A. 85 25.13 F 0.28	7.64 D line 25.13 C 2.51
2+50	N 0.30	8.90 25.50 C 3.40	F 0.19	F 0.27	7.78 D line 25.66 C 2.12
2+00	N-0.20	8.78 26.00 C 2.78	F 0.23	C 0.05	8.17 D line 26.33 C 1.84
1+50	N-0.30	8.82 26.50 C 2.30	F 0.43	C 0.03	8.23 D-5' 27.00 C 1.23
1+00	N-Line	8.48 27.00 C 1.48	F 0.08	F 0.18	8.25 D line 27.67 C 0.58
0+50	N-Line	8.59 27.50 C 1.09	F 0.15	F 0.35	8.40 28.34 C 0.06
0+00 = N.Wly Ampudia = Cl. E.C.		28.00	8.14 28.00 C 0.14		29.00

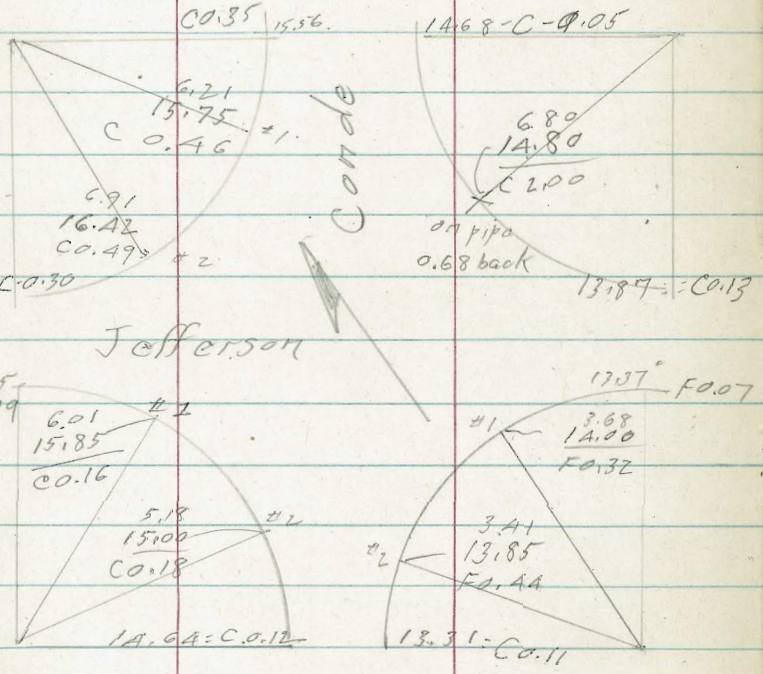
INDEXED

INDEXED

6/20/55 55

Returns Conde + Jefferson

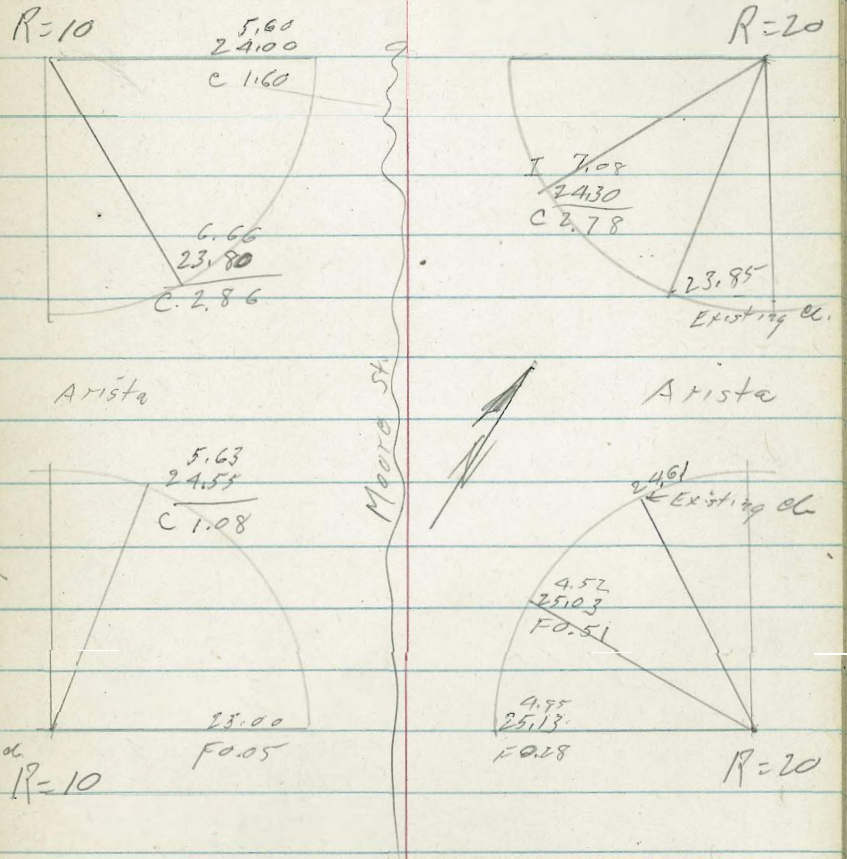
see page 48 for E.C. + B.C.



Moore + Arista

cl. Returns - 11317-L

From - P-54



Stake Wly. Curb 8/16/55
Sunset Cliffs Blvd.
Hill to Pt. Loma Ave.

Plan # 3079-D
F.B. 2251 - P-52.

~~Stake~~ 3' Wly of curb face.
Curve datum shown is stake line

2+54.59	Δ 16°-40"		9.33 ✓
	ch 32.43		A 9.77
			F 0.44
2+22.37	2°-08'-20		A 7.39
	ch 32.43		A 7.91
			F 0.52
1+90.16 = P.R.C.	R 434.5		5.39
	Δ 25°-40'		A 6.04
			F 0.65
1+79.80 = P.R.C.	R = 97' ch = 9.39		4.86
	Δ 5°-33		A 5.45
			F 0.59
= P.R.C.	R = 103 ch = 15.95		
	Δ = 8°-53 Rate =		
1+64[3] = start new curb.			4.13
			A 4.55 Brk.
			F 0.42
1+40[3] - Start Job (Re-top curb.)			3.63
			A 3.63 Brk
			✓

5+50			8.52 59.03 F 0.51	Brk.	8+00		4.55 55.05 F 0.50	
5+01.4			7.67 58.14 F 0.47		7+78.89 E.C. 2°-41'-15" ch 35.52		5.18 55.71 F 0.53	Brk
4+52.7	3×48.67		6.73 57.25 F 0.52		7+43.37 (℞) ∆ 1°-20'-38" ch 35.52		6.24 56.80 F 0.56	
4+04		T.P.	5.80 56.35 F 0.55	✓ Brk	Rad = 758.78 ∆ 5°-22'-30" 7+07.85 B.C.		7.40 57.90 F 0.50	Brk
3+83.46 E.C. 12°-50'			5.32 55.87 F 0.55	Brk.	7+04.24 E.C. 2°-04'-26" ch = 32.66		7.54 58.04 F 0.50	Brk
3+56.06 - 11°-11'-15"			4.58 55.10 F 0.52	Brk	6+71.87 = 14°43' ch. 32.66		8.69 59.18 F 0.49	Brk
3+28.67 - 9°-22'-30"			3.50 54.05 F 0.55	Brk	6+39.51 ∆ 7°-21'-30"	T.P.	59.32 59.82 F 0.50	✓ Brk
3+19.03 8°-33'-20" ch 32.43			3.05 53.49 F 0.44		R = 127.5 - ch = 32.66 6+07.15 B.C. Lt.		9.37 59.90 F 0.53	Brk
2+86.81 6°-25' ch 32.43	51.79		1.16 54.63 F 0.47		5+78.57		9.08 59.55 F 0.47	Brk

12+50		0.59 41.10 F0.51	Brk	15+64.33	6.94 37.47 F0.53
12+00		2.09 42.65 F0.56		15+40.48	7.08 37.58 F0.50
11+50		3.67 44.20 F0.53		15+16.60	7.17 37.69 F0.52
11+00		5.20 45.75 F0.55	✓	14+92.75	7.29 37.80 F0.51
10+50		6.75 47.30 F0.55		14+68.89 B.C. 4.	7.39 37.90 F0.51 ✓ Brk
10+00 3.1%		8.31 48.85 F0.54		14+34.45	7.55 38.09 F0.54
9+50		9.85 50.40 F0.55		T.P. 14+00	37.78 38.27 F0.49 Brk
9+00		1.34 51.95 F0.61		13+50	8.30 38.79 F0.49 Brk
8+50		2.97 53.50 F0.53	✓	13+00	9.27 39.77 F0.50 Brk

23.85 Chd
6 Parts

17+83.68 = 29.61 (10 parts of 2.961)

6°-07

6.17
36.65
F0.48

17+53.96

4°-04'-40"

6.25
36.76
F0.51

17+24.24 Def 2°-02'-20"

6.42
36.87
F0.45

Δ = 40°-46'-30" stake Rad = 416.14

16+94.52 P.R.C. Def 9°-38°-30"

6.46
36.98 Brk.
F0.52

16+67.64 dL = 27.06 (3 parts) Def 6°-26'

6.51
37.07
F0.56

16+40.76 Def 3°-13'

6.70
37.16
F0.46

Δ 19°-17'-stake Rad. = 241.09

16+13.89 B.C.H.

6.72
37.24
F0.52

16+12.03 E.C. 2°-04'-12"

6.72
37.25 Brk.
F0.53

15+88.18 1°-43'-30"

6.90
37.36
F0.46

20+50 3.45 %

5.18
35.68
F0.50

20+00

5.37
35.86
F0.49

19+91.74 = E.C. Def 10°-23'-20"

5.42
35.89 Brk.
F0.47

19+62 18°-21'

5.49
36.00
F0.51

19+32.28 16°-18'-40"

5.65
36.10
F0.45

19+02.56 14°-16'-20"

5.81
36.21
F0.40

18+72.84 12°-14'

5.79
36.32
F0.53

18+43.12 10°-11'-40"

5.97
36.43
F0.46

18+13.40 8°-09'-20"

6.05
36.54
F0.49

1 23+91.18	7°-12'	3.96 34.51 F 0.55	26+51.40 9°-12.09' ? on true line	?
1 23+58.57 ch. = 32.51	5°-24'	4.11 34.62 F 0.51	26+32 6°-26.19' ch = 22.73	2.96 33.45 Brk. F 0.49
1 23+25.96 10 parts	3°-36'	4.25 34.73 F 0.48	26+09.42 3°-13' ch = 22.73	3.14 33.65 F 0.51
1 22+93.35 def	1°-48'	4.36 34.84 F 0.48	25+86.84 = P.R.C. 18°-00'	T.P. 3.31 33.85 Brk. F 0.54
Δ = 36°- Stake Rad. = 517.50 1 22+60.74 B.C.R.C.		4.48 34.96 Brk. F 0.48	25+54.23 16°-12'	3.45 33.96 F 0.51
1 22+50		4.47 35.00 F 0.53	25+21.62 14°-24'	3.48 34.07 F 0.59
1 22+00	T.P.	4.62 35.17 F 0.55	24+89.01 12°-36'	3.66 34.18 F 0.52
1 21+50		4.75 35.34 F 0.59	24+56.40 10°-48'	3.77 34.29 F 0.52
1 21+00		4.97 35.52 F 0.55	24+23.79 9°-00'	3.87 34.40 F 0.53

Stake line ch = 32.51

29+10.82 — 1.46 / 32.00 / F0.54

28+64.22 — 1.73 / 32.27 / F0.54

28+17.62 — 2.00 / 32.54 / F0.54

27+71.02 E.C. 26°-15' — 2.39 / 32.81 / F0.42 — B.k.
ch = 20.84

27+50.34 23°-19' — 2.49 / 32.84 / F0.35
ch = 20.84

27+29.67 20°-22' — 2.51 / 32.87 / F0.36
ch = 20.84

27+09 17°-24.65' — 2.43 / 32.90 / F0.47 — B.k.

26+89.90 14°-41.32 ? Tan line dg. — ?

26+70.8 = ℄ C.I 11°-58' ? — 2.71 / 32.70

32+23.06 dg 17°-28'-47" — 29.71 / 30.31 / F0.60
ch 22.98

32+00 P.O.C. — 0.03 / 30.43 / F0.40
dg = ℸ 15°-38'-22"

omit 80' of ch.

31+20.30 P.O.C. 9°-16'-45" — 0.68 / 30.85 / F0.17

30+91.23 6°-57'-30" — 30.36 / 31.00 / F0.64

30+62.16 4°-38'-20" — 0.68 / 31.15 / F0.47

30+33.09 dg 2°-19'-10" — 0.85 / 31.30 / F0.45

30+04.02 B.C. — 0.96 / 31.45 / F0.49 — B.k.

T.P. 29+57.42 — 1.25 / 31.73 / F0.48

ch = 28.94

7.14 - 45

34+52.92	9°-12'	8.48 29.01 F0.53	37+31.71 P.C.C.	6.11 26.63 F0.52
34+26.14	7°-40'	8.59 29.17 F0.58	37+09.52	6.37 26.94 F0.57
33+99.36	6°-08'	8.77 29.32 F0.53	36+87.33	26.69 27.25 F0.56
33+72.58	4°-36	9.00 29.48 F0.48	36+65.14 B.C.	6.96 27.55 F0.59 Brk
33+45.80	3°-04'	9.16 29.63 F0.47	36+25.48	7.30 27.84 F0.54
33+19.02	1°-32' T.P.	29.27 29.79 F0.52	35+85.81	7.66 28.13 F0.47
32+92.24 P.R.C.	23°-00'	9.48 29.95 Brk F0.47	35+46.14	7.91 28.42 F0.51
32+69.18	21°-09'-35"	29.55 30.07 F0.52	35+06.47 E.C.	8.20 28.70 Brk F0.50
32+46.12	19°-19'-10"	29.60 30.19 F0.59	34+79.70	8.35 28.85 F0.50

8 pts. Chord = 26.89

Δ = 22.20

Δ 8°-04' Ch. Rad. 717.3

Δ = 37.67

R=357.57 ch = 22.98'

38+85 = End of Job.		23.95	Brk.
↕ Rebuild Existing ℄.			
End New Curb.			
38+59.16 E.C.	7°-47'	4.11 24.55	Brk
ch 13.85		F 0.44	
38+45.20	8°-42'-45"	4.35 24.85	
ch 13.85		F 0.50	
38+31.25	7°-38'-30"	4.61 25.15	Brk
ch. 19.31		F 0.54	
38+11.80	6°-08'-55'	4.78 25.45	
ch 19.31		F 0.47	
37+92.35	4°-39'-20"	5.29 25.75	
ch 19.31		F 0.46	
37+72.90	3°-09'-44'	5.61 26.05	Brk.
ch. 20.45		F 0.44	
37+52.30	1°-35'	25.88 26.34	
ch 20.45		F 0.46	

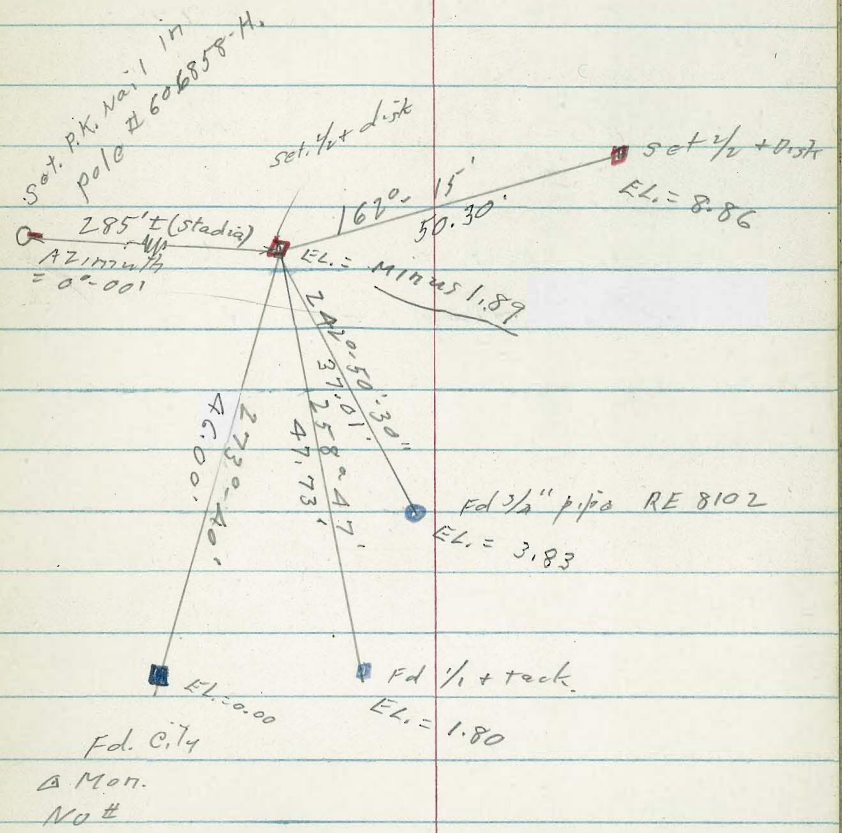
R.P. to City Mon. (No. #)

△ Point

8-15-55
W.O. 20006

Set as shown in sketch.
Angles in azimuth from P.K. Nail ✗
Elevations shown are relative
above Mon.

Near Ely. Cor. Lots 23 + 24
La Jolla Shores Terrace
Map # 2996. sheet 4

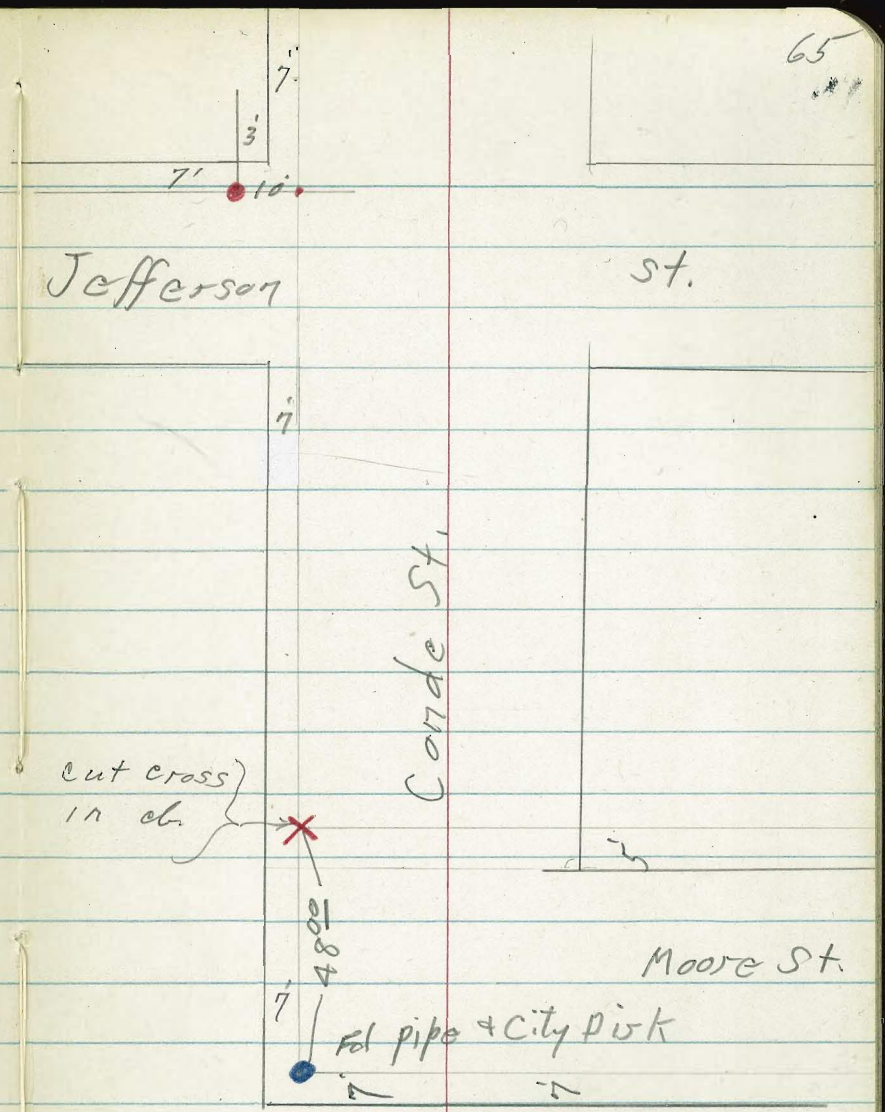


INDEXED

Tie Points

Moore & Conde 8/19/55

Could not set disk as cross is near face of curb.

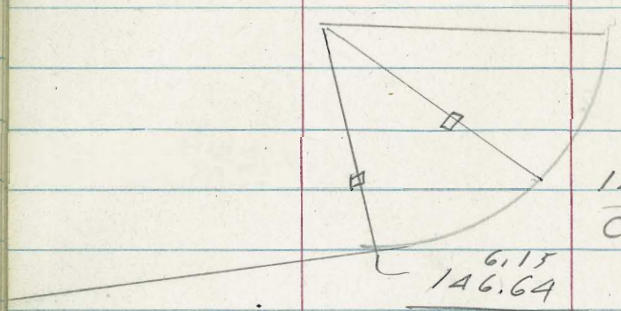


INDEXED

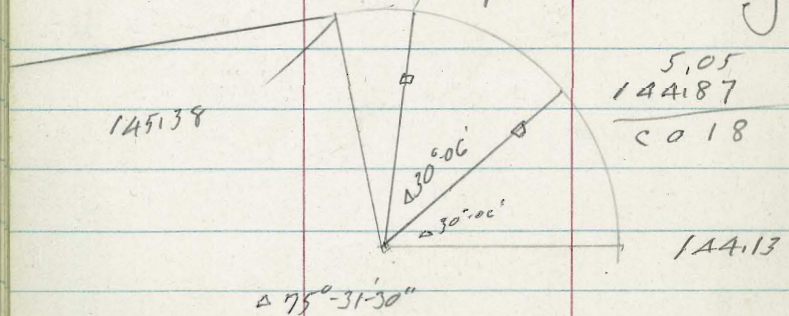
Curbs Taft + Colima

11-9-55

Sheet 2663-AD.

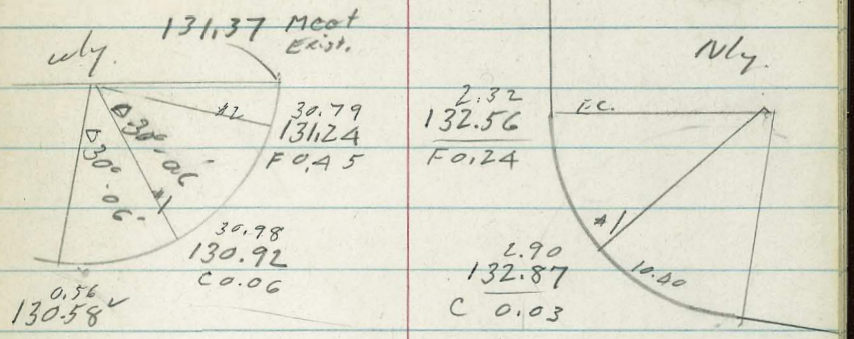


Taft



Midway & Taft.

66

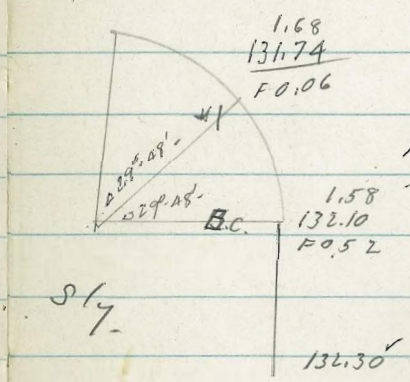


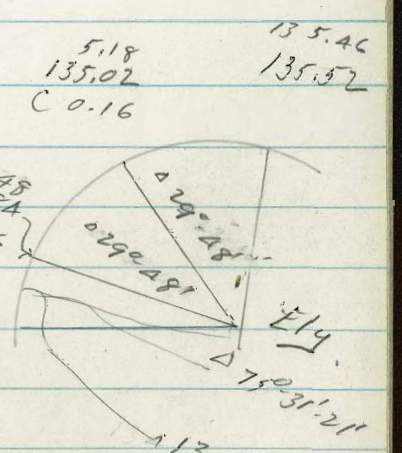
Taft

Midway St

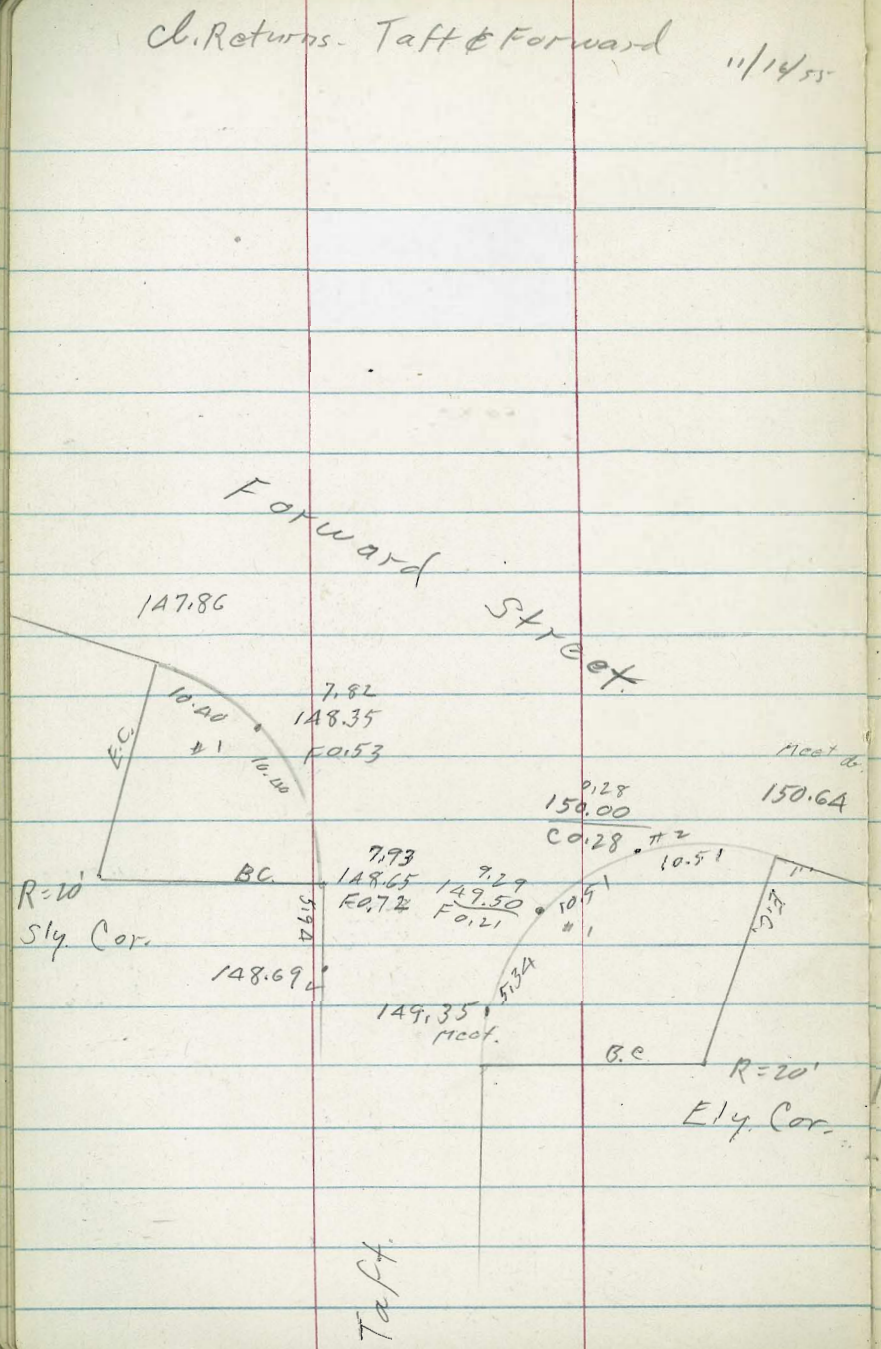
N

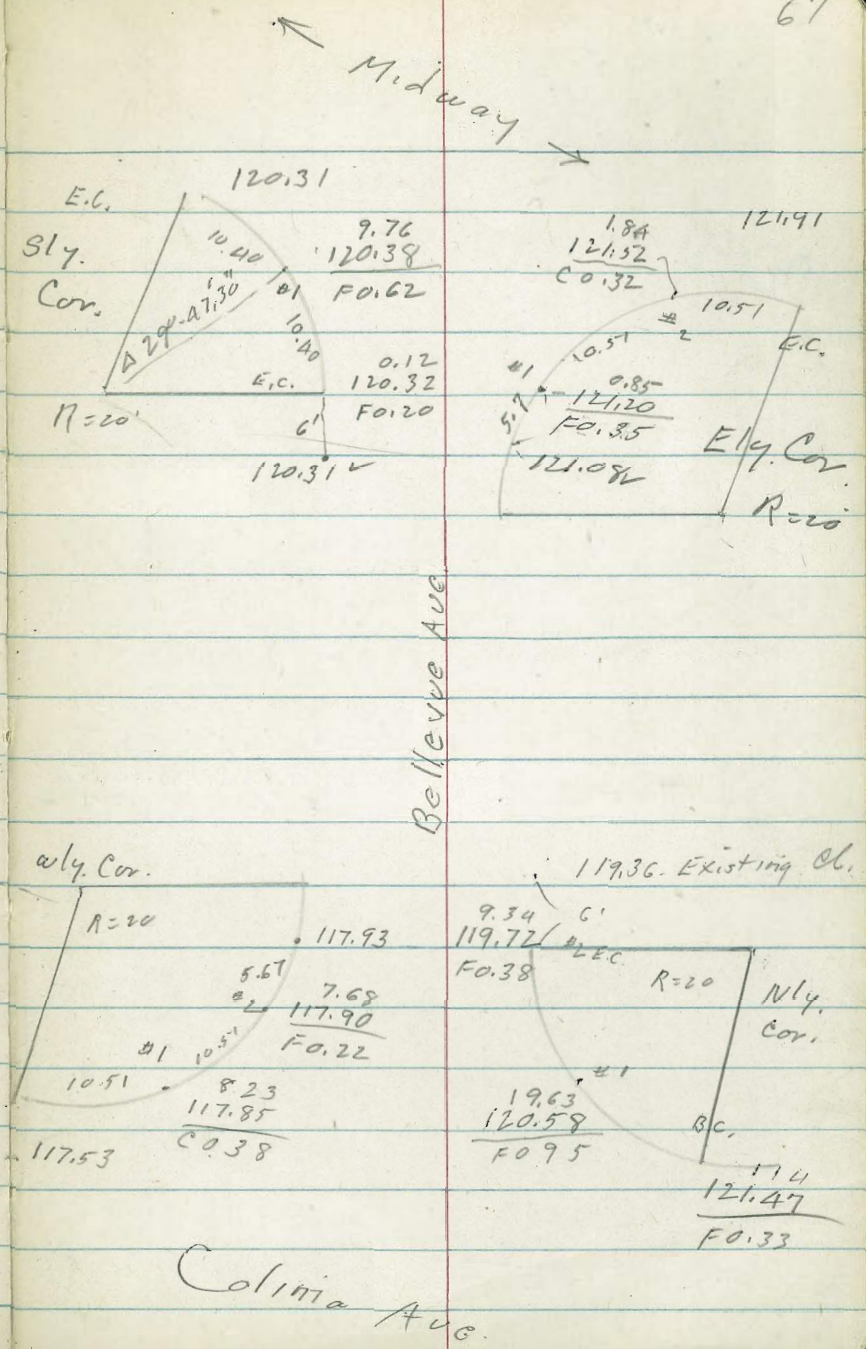
131.38





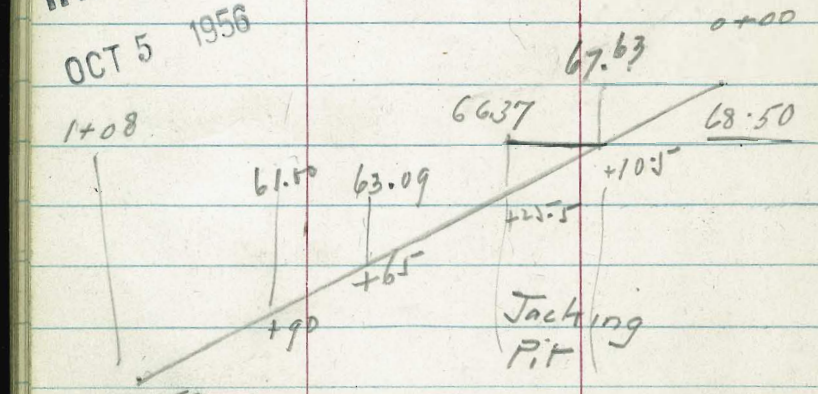
Ch. Returns - Taft & Forward 11/14/55





Begg. ☐
Shelin ↑
puller, CA

Storm Drain Const Torry



Sheet

S E L + T. Prospect & Torrey Rd. 5729-B.

152.31		
0.30		
152.61		103.24
12.98		0.33
139.63		103.57
0.50		12.23
140.13		91.34
12.58		1.18
127.55		92.52
1.50		6.46
129.05		86.06
12.88		5.04
116.17		91.10
0.28		5.07
116.45		86.03 = ☐ on deck at N'ly
13.21		Cor. pump house.
103.24		

Note - 3/19/56. ↘

0+00 built 0.7' west of ℄ as per 5729 B
1+08 " 1.0' " " " " "
IE. ~~1+08~~ 1+08 =
Top Hd wall =

68

Pine Road & Charlotte St

See 5729 B

Type H ch. inlet

Top. ch.		85.19	4.03	
0+00	☐	86.24	86.24	☐ 10' Rt
	10' Lt.	F. 1.05	F 2.21	
1+08		59.15 59.50 F. 0.35		
0+90		66.48 61.00 C - 5.48		
0+65		81.89 63.09 C-18.80		
0+25	☐	83.44	82.92	
	10' Lt	66.37 C-17.07	66.37 C-16.55	☐ 10' Rt
0+10	☐	84.55 67.63 +N — 10' →	83.21 67.63	☐
		C-16.92	C-15.58	
0+00		84.03 68.50	— I.E. P. pc	
Face Prop. curb		C-15.53	☐ - 10' Rt	

INDEXED Alley Blk. 6 Chester Park

4-23-56
Sheet 3172-D
Index J-18
W.O.# 31981

Orange to El. Cajon.

Between Euclid & 47th

Nly. line Orange Ave = 0+00 Lt. = west

		Plan Grade	Grade Set	
1+20	T-0.35	3.52 52.02 C 1.50		
1+00	□-2'	3.26 52.65 C 0.61		
0+80	N. 0.33 in	4.38 53.34 C 1.04		
0+60	X-0.85	4.43 53.93 C 0.50		
0+40	N-0.88	5.35 54.29 C 1.06		
0+20	□ 2'	4.83 54.42 C 0.41		
0+00		4.32 54.29		

B.M. = N.W.B.P. Orange & Euclid. EL. = 350.69

69

Rt = East

	℄	Grade Set.	Plan Grade	
			2.21 51.77 C 0.44	N-0.50
			3.10 52.40 C 0.70	T-0.50
			3.81 53.09 C 0.72	T-0.25
			3.95 53.68 C 0.27	T. line
	54.16		4.15 54.04 C 0.11	□1' .04+4 Rim M.H. 3.99 = M.H 4.08 F 0.09
	54.05		4.45 54.17 C 0.28	□1'
	4.14 53.96 C 0.18		54.08	

		Plan Grade	Grade set.			Grade set	Plan Grade	
3+00	N-0.35	9.79 48.37 C 1.42					9.95 48.12 C 1.83	N-0.25
2+80	N-0.05	9.78 48.59 C-1.19					50.05 48.34 C 1.71	N-0.25
2+60	N.-0.05	9.91 48.86 C 1.05					9.97 48.61 C 1.36	N-0.28'
2+40	+2'	9.82 49.17 C 0.65					9.15 48.92 C 0.23	X-0.50
2+20	X-2'	0.13 49.53 C 0.60					9.33 49.28 C 0.05	X-0.25'
2+00	☐1'	9.56 49.94 F 0.38					8.61 49.69 F 1.08	☐-2'
1+80	☐0.50	0.52 50.39 C 0.13					9.31 50.14 F 0.83	☐-2
1+60	☐-2	1.73 50.89 C 0.84					9.87 50.64 F 0.77	☐-2
1+40	☐-2'	2.41 51.44 C 0.97					0.23 51.19 F 0.96	☐-2'

		Plan Grade	Grade Set
5+40	T-0.48	9.04 47.42 C 1.62	
5+10	N-0.60	9.77 47.51 C 2.26	
4+80	N-0.90	9.36 47.60 C 1.76	
4+50	N. 1.20	9.64 47.69 C 1.95	
4+20	0.2'	9.10 47.78 C 1.32	
3+90	N-1.21'	50.13 47.87 C 2.26	
3+60 E.V.C.	N 0.76	9.91 47.97 C 1.94	
3+40	N-0.83	50.05 48.05 C 2.00	
3+20	N 0.85	9.76 48.19 C 1.57	

	Grade Set	Plan grade	
		7.37 47.17 C 0.20	0-2'
		7.45 47.26 C 0.19	0 2'
5+04 7.47 = Ex. gr M.H. El. = 7.11 C 0.36		7.91 47.35 C 0.56	RIM M.H. 47.47 5+04 0-2'
		8.81 47.44 C 1.37	N-1.40'
		9.65 47.53 C 2.12	X-1.25
		9.36 47.62 C 1.74	X-1.15'
		9.53 47.72 C 1.81	T-1.00
		9.54 47.80 C 1.74	T-0.20
		50.54 47.94 C 2.60	T-0.15

		Plan Grade	Grade set			Grade set	Plan Grade	
8+10	□ 4' O X	6.02 46.59 F 0.57					7.21 46.34 C 0.87	X-1'
7+80	X on Fence String or	7.69 46.68 C 1.01					7.29 46.43 C 0.86	X 1.50'
7+50	X	7.44 46.78 C 0.66					6.70 46.53 C 0.17	□-2'
7+20	X-	7.33 46.87 C 0.46					6.57 46.62 F 0.05	□-2'
6+90	□-2'	7.54 46.96 C 0.58					6.48 66.71 F 0.23	□-2'
6+60	□-3'	7.73 47.05 C 0.68					6.70 46.80 F 0.10	□2'
6+30	X-2'	7.50 47.14 C 0.42					9.25 46.89 C 2.36	T 2.25
6+00	X2'	7.92 47.23 C 0.69					7.85 46.98 C 0.87	N 0.65
5+70	X-2'	7.98 47.33 C-0.65					7.96 47.08 C 0.88	N. 0.65

6.32
6.07
2 | 12.39
6.20
.25
5.95

Rim MH 5.78 / 5.80 / FOOT

		plan grade	grade set		℄	grade set	plan grade	
Sly. Line El. Cajon								
9+51.07	X-line	6.62 A6.05 C0.57			5.89 A5.80 grade		6.47 A5.90 C0.57	P.K. -1'
9+30 Brk	X-line	7.05 A6.23 C0.82			A5.86		6.91 A5.98 C0.83	D 1'
9+00	X-Line	7.43 A6.32 C1.11					6.83 A6.07 C0.76	D 1'
8+70	X-Line	7.50 A6.41 C1.09					6.70 A6.16 C0.54	D 1'
8+40	D-2'	6.57 A6.50 C0.07					6.98 A6.25 C0.73	T-0.95'

Unio Ave Portion Chocolate Canyon Sewer.

From Alley West of Boundary to Alley west of Wabash Ave.

W.O.# 21398

5/1/56

0+00 = 6+28.61 sheet 3367-D.

stakes 5' Lt of ℄ sewer

	21.34	21.34
1+25	316.87	17.00
	C4.47	C-4.34
	23.05	23.05
1+00	316.77	16.95
	C6.38	C6.10
	23.81	23.81
0+75	316.67	16.90
	C7.14	C-6.91
	24.61	24.61
0+50	316.57	16.85
	C8.04	C-7.76
	25.42	25.42
0+25	316.47	16.80
	C8.95	C-8.62
	26.14	26.14
0+00 - M.H.#4	316.37	16.75
	C9.77	C 9.39

changed to meet Existing line

N.W.B.P. Boundary + Unio-B.R.-EL = 333.34

		26.98	
A+00		321.91	
		C5.07	
		25.50	
3+50		320.56	
		C4.94	
		24.03	
3+00		319.21	
		C4.82	
		22.47	
2+50		317.86	
		C4.61	
		21.91	
2+28.61 M.H.#3		317.28	
		C-4.63	
		21.41	21.41
2+00		317.17	17.20
		C4.24	C4.21
		21.46	21.46
1+75		317.07	17.12
		C4.39	C4.34
		21.75	21.75
1+50		316.97	17.05
		C4.78	C4.70

changed to clear storm drain

End of Job.

6+28.61 = M.H. #1
32.39
328.17
C 4.22

2.80%

5+81.73
31.71
326.71
C 5.00

Δ 15°-42' Rt.

5+34.86 = M.H. #2
30.99
325.55
C 5.44

94

5+00.
30.02
324.61
C 5.41

10%

4+50
28.50
323.26
C 5.24

N

5/4/56

S.Wly Cor. College & University

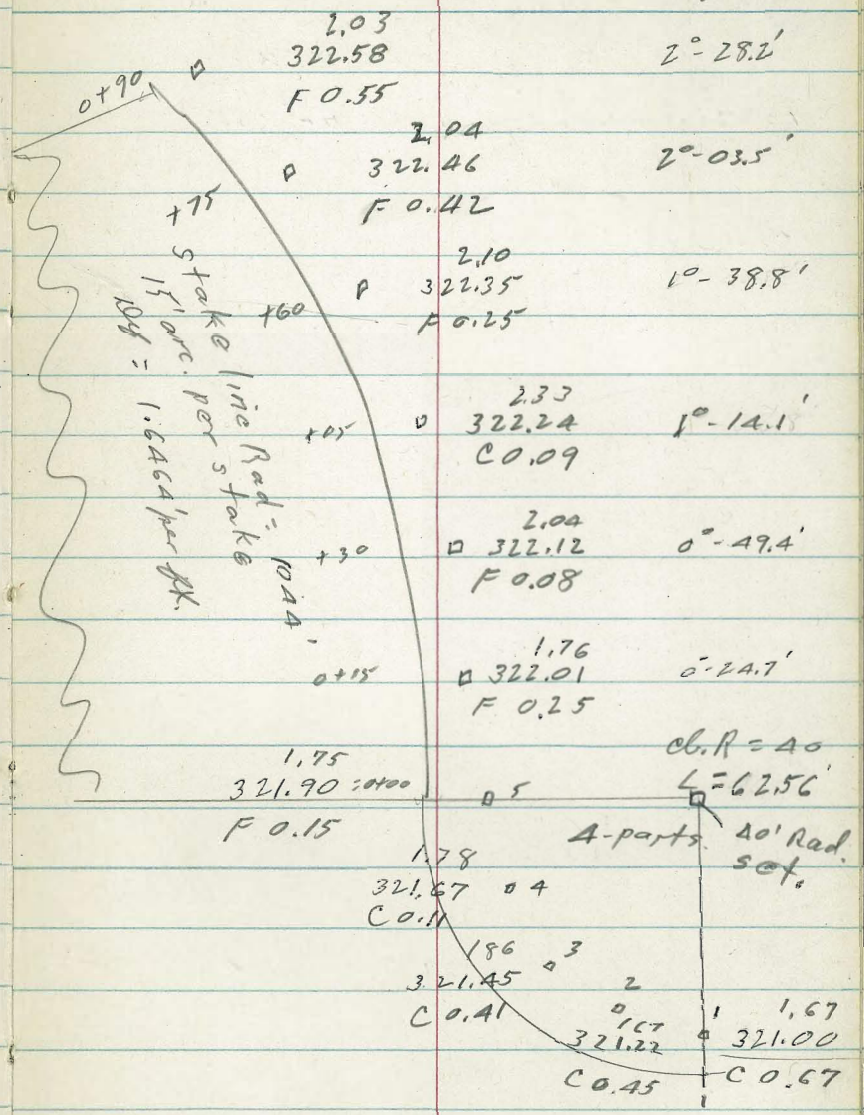
Curb returns

Staked as per pencil datum on 1012A-L (By. Remington)

B.M. = ☐ on N.wly Ret. College & Univ. EL. = 322.22

Stakes 3' back of Cb. Face

Stationing on arc. of 1044' Rad.



5/11/56

Curb Stakes

INDEXED

Lot 2 - Blk 47 Grantville

Sheet # 2707 D & 2708 D
" # 6088-B
drawing # 2707-D. Elev. = 71.18 city datum
B.M. = □ N.E. wing wall of bridge

Curb line
Set sub grade
1' below curb
32%

stakes 8' Back

2+20 — 7°-16.67'
8.03
68.94
F 0.91

1+80 — 5°-57.27'
7.83
68.81
F 0.98

1+40 — 4°-37.88'
8.57
68.70
F 0.13

1 — 3°-18.48'
7.59
68.56
C 1.03

0+60 — 1°-57.09'
8.65
68.48
C 0.17

0+20.77 — 0°-41.22'
8.16
68.30
F 0.14

B.C. 0+00
7.86
68.23
F 0.37

0-40
~~8.80~~ 7.80
~~68.15~~ 68.15
~~C 1.65~~ F 0.35

	20ft.		1' below curb Sub grade	Set. 0.50 below pave.
6+07 62	20°-0C'		68.31 70.18 F 1.87	
5+80	19°-11.21'		67.5C 70.10 F 2.54	
5+40	17°-51.17'		7.30 69.97 F 2.67	
5+00	16°-32.42'		9.24 69.84 F 0.60	
4+60	15°-13.03'		8.31 69.71 F 1.40	
4+20	13°-53.63'		8.80 69.58 F 0.78	
3+80	12°-34.24'		8.75 69.45 F 0.70	
3+40	11°-14.85'		8.61 69.32 F 0.71	
3				
3 —	9°-55.45'		7.74 69.20 F 1.48	
2+60	8°-36.06'		7.77 69.07 F 1.30	

INDEXED

Santa Margarita 5/12/56

sewer 54th to 55th

Sheet 6068-B W.O. # 62471

0+00 = 20' Ely from ℄ 54th St.

Stakes - 5' Rt. of ℄ * El.: 157.00

B.M. = I.E. M.H. - 54th & Santa Margarita

Rim M.H. = El. 164.18

Lat # 1 = 3+29 Lt.

2+40 — 67.45 / 160.08 / C-7.37

Lat # 2 = 2+25 Rt

1+95 — 66.97 / 159.77 / C-7.20

Lat # 3 = 1+70 Rt

1+50 M.H. #1 — 66.68 / 159.45 / C-7.23

Lat # 4 = 1+20 Rt

1+00 — 66.20 / 159.10 / C-7.10

0+50 — 65.98 / 158.75 / C-7.23

3+30 — 68.17 / 160.71 / C-7.46

0+00 — 65.72 / 158.40 / C-7.32

2+85 — 67.88 / 160.40 / C-7.48

Sanchez - foreman 39th

2+99.06
15 28
3+17.34

1223
1034
189

51.42

101
312
119

1934

326.80
10.52
337 32

2+30.33
21.15
2+51.48

1267
490
787

54
14
216
54

160

2+09.17
21.15
2+30.32

90.
54,00

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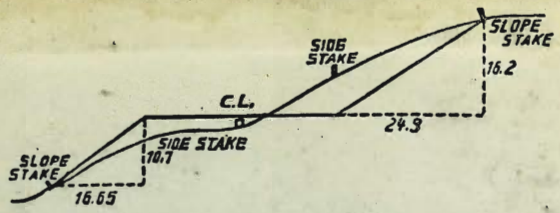

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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