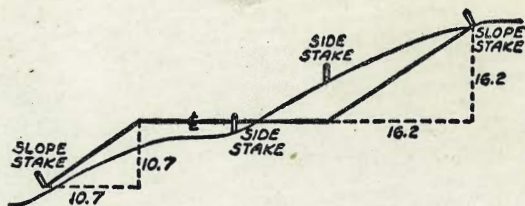


G-352



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 16 1965

$$2 + 73.5 = B.R.K.$$

$$\begin{array}{r} 1 \\ \underline{69} \\ 1704 \end{array}$$

$$1 + 67 = \text{Gun}$$

$$1 + 69 = \text{face of @b.}$$

$$\begin{array}{r} 35 \\ \underline{35} \\ 0 \end{array}$$

$$2 + 04 \text{ (35)}$$

$$2 + 39 \text{ (345)}$$

$$+ 73.5 = \text{Brk}$$

$$2 + 03 \text{ (30)}$$

$$+ 33 \text{ (30)}$$

$$+ 63 \text{ (30)}$$

$$+ 93 \text{ (26.2)}$$

$$4 + 19.7$$

$$\begin{array}{r} 2 + 73.5 \\ \underline{1462} \\ 4 + 197 \\ \underline{3193.5} \\ 26.2 \end{array}$$

DIRECTIONS FOR USE OF TABLES

TABLE NO. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill is small.

IMPROVED TABLES

AND

INFORMATION

To find Tangent and Distance from center of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or distance) opposite by given tangent (or distance).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

0	0.00
1	1.00
2	2.00
3	3.00
4	4.00
5	5.00
6	6.00
7	7.00
8	8.00
9	9.00
10	10.00
11	11.00
12	12.00
13	13.00
14	14.00
15	15.00
16	16.00
17	17.00
18	18.00
19	19.00
20	20.00
21	21.00
22	22.00
23	23.00
24	24.00
25	25.00
26	26.00
27	27.00
28	28.00
29	29.00
30	30.00
31	31.00
32	32.00
33	33.00
34	34.00
35	35.00
36	36.00
37	37.00
38	38.00
39	39.00
40	40.00
41	41.00
42	42.00
43	43.00
44	44.00
45	45.00
46	46.00
47	47.00
48	48.00
49	49.00
50	50.00

Distance ground is column on side stake cut or fill. If it does

Curb stakes - A St. - Edgemont - East.
 Plan - 11209-L - W.O. 32340 - 4-28-55 - 7.0.

214.94 = 1+95 on S. = Cross.

Edgemont
 0+00 = E.L.

N.

S.

		29.06					
+20	29.17	29.24	F 0.07				
+30	29.25	29.26	F 0.01				
+40	29.13	29.14	F 0.01				
+65	28.58	28.49	C 0.09				
+90	27.22	27.85	F 0.63	S. end	26.19	26.56 19	F 0.37
+95	27.03	27.68	F 0.65	E.C. - to Alley	26.18	26.30 18	F 0.12
1+00	26.93	27.45	F 0.52	To st. 1+12 = PC - Alley	26.18	26.20	F 0.02
+20	26.24	26.33	F 0.09	1+20	25.60	25.95	F 0.35
+30	26.06	25.61	C 0.45		25.60	25.47	C 0.16
+40	24.28	24.53	F 0.25		23.66	24.50 3.26	F 0.84
+50	23.49	23.10	C 0.39		22.52	23.10 2.52	F 0.58
+75	19.24	19.10 ²⁴	C 0.14		19.67	19.10 ⁶⁷	C 0.57
+85	17.17	17.27	F 0.10		16.28	17.27 28	F 0.99
+95	14.92	15.00	F 0.08		14.16	15.00 14.16	F 0.84
2+13 = P.C. 2' Rad.	11.44	10.50 ⁴⁴	C 0.94	6' bk 13.90 10.50 2.40	14.01	10.50 ⁰¹	C 3.51
E.C. = Cross cb. Drain	09.40	09.98 ⁴⁰	F 0.58		08.40	09.98 8.40	F 1.58
End. of cb. at	09.84	09.70 ⁸⁴	C 0.14		09.40	09.70	F 0.30
End. of Drain - ϕ	08.11	06.50 ¹¹	C 1.61		07.50	06.50 ⁵⁰	C 1.00

curb stakes - 69th El Cajon to Amherst
 Plan - 11699-L - 100-32410 - 5-2-55 7.0.

		West			East	
Amherst						
End on NL	54.14	54. ¹⁴ 09	C 0.05	55.10	54.46 ¹⁰	C 0.64
P.C. = 0+00	54.13	54.15	F 0.02	54.80	54.50 ⁸⁰	C 0.30
+35'	54.26	54.29	F 0.03	54.96	54.62 ⁹⁶	C 0.34
+70	54.52	54. ⁵² 43	C 0.09	54.73	54.74	F 0.01
1+05'	54.62	54. ⁶² 57	C 0.05	55.25	54.86 ²⁵	C 0.39
+37.68 = P.C. to st	54.92	54. ⁹² 69	C 0.23	55.55	54.97 ⁵⁵	C 0.58
E.C. = To Alley	54.92	54. ⁹² 74	C 0.18	55.55	55.02 ⁵⁵	C 0.53
End = Prop.	55.20	54. ²⁰ 90	C 0.30	55.69	55.18 ⁶⁹	C 0.51

Curb stakes - Twain + Mission Gorge
 Plan - 5715-B - w.p. 62432 - 5-5-55 - 710.

Rd.

3

End on Twain	84.15	^{+ .15} 82.42	C 1.73
38.14			
B.C.	79.63	^{9.63} 77.82	C 1.81
1/3	77.42	^{7.42} 76.25	C 1.17
2/3	75.92	^{7.35} 75.35	C 0.57
= 0 + 00 E.C. = on Mission	76.68	^{6.68} 74.97	C 1.71
0 + 35	74.80	^{.80} 74.76	C 0.04
+ 66.19 = PC.	74.86	^{.86} 74.57	C 0.29
+ 96.19	74.58	^{.58} 74.39	C 0.16
1 + 26.19	74.28	^{.28} 74.21	C 0.07
+ 45.19 = end.	74.15	^{.15} 74.10	C 0.05

Stake Sewer - Alley Blk 4 - Camel Hts.
 Plan - 2835 - D - W.O. 21303 - 5-9-55 - 70.

Stakes - 6' Lt.

0+00 = M.H. N. of Nutmeg.	73.30	^{73.30} 60.40	12.90
+38	67.51	^{7.51} 60.59	6.92
0+41 = ± Enc.			
+43	67.62	^{7.62} 60.69	6.93
+48	68.35	^{8.35} 60.91	7.44
+53	68.25	^{8.25} 61.25	7.00
+58	68.93	^{8.93} 61.72	7.21
+95	75.53	^{75.53} 65.98	9.55
1+30	78.78	^{8.78} 70.02	8.76
+65	83.01	^{83.01} 74.03	8.98
2+00	86.98	^{86.98} 78.10	8.88
+35	90.38	^{90.38} 82.15	8.23
+70	93.60	^{93.60} 86.17	7.43
3+06.62 = ± Middle M.H.	96.44	^{96.44} 90.44	6.00
0+35	98.87	^{8.87} 91.61	7.26
+70	00.67	^{00.67} 92.78	7.89
1+05	01.97	^{01.97} 93.93	8.02
+40	04.29	^{04.29} 95.12	9.17
+75	05.55	^{05.55} 96.29	9.26

2+10

06.42

^{06.42}

97.46

8.96

+45

07.18

^{07.18}

98.63

8.55

+80

06.31

^{06.31}

99.80

6.51

± Palm.

3+06.40 = M.H.

07.05

^{07.05}

200.68

6.37

00.79 = 14 ±

Stake Sewer - Tres Lomas - Blk. 11
 Plan - 11920-L 5-10-55 - 7.0.
 w.o. 62405

8595 = I.R.

± Cumberland. 0+00 = M.H.	95.25	2 86.25	9.00	1+05	17.66	05.23	12.43
+35	94.74	86.63	8.11	+30	19.16	06.74	12.42
+70	94.59	87.01	7.58	+47.8 = Plug.	20.00	20.00 07.80	12.20
1+05	94.58	87.39	7.19				
+40	94.78	87.77	7.01				
+75	95.12	88.15	6.97				
2+10	95.31	88.53	6.78				
+35	95.62	88.80	6.82				
2+59.71 = M.H. 1	96.05	89.06	6.99				
0+35	97.32	89.44	7.88				
+70	98.74	89.82	8.92				
1+05	00.19	90.20	9.99				
+42.47 = M.H. 2	Back 01.83 ahead. 02.00	90.60	11.23 11.40				
0+35	03.99	92.71	11.28				
+70	06.69	94.83	11.86				
1+05	09.50	96.94	12.56				
+37.17 = M.H. 3	11.69	98.89	12.80				
0+35	13.87	101.00	12.87				
+70	15.59	103.12	12.47				

Stake Alley - Blk. 27 - Higgins Add.

Plan - 11364 - L

W.O. 32417 - 5-11-55 7.0.

0.25' Excepted - Both sides

6

West.

East.

Broadway
0+00 = NL

88.28 = cut.

88.14 = cut.

+10 88.42 88.⁴²02 Co.40 0.25 B. 88.77 87.⁷⁷87 Co.90

+40 87.13 87.²⁵25 Fo.12 0.21 B. 87.86 87.⁸⁶07 Co.79

+70 86.85 86.⁴⁷47 Co.38 0.32 B. 87.15 86.¹⁵27 Co.88

+80 86.80 86.²⁵25 Co.55 0.38 B. 86.92 86.⁰⁵05 Co.87

+90 86.28 86.²⁵25 Co.03 0.36 B. 86.63 86.⁶³05 Co.58

+15 85.69 86.³⁸38 Fo.69 0.36 B. 86.12 86.¹⁸18 Fo.06

+40.36 = Alley 85.60 86.⁵⁰50 Fo.90 85.97 86.³⁰30 Fo.33

+50.36 = # 85.81 = Top Pipe 86.46 86.²⁵25 85.96 Co.21
 † = 85.86 = 27" from EL

+60.36 Alley 86.39 86.⁶⁰60 Fo.21 86.49 86.⁴⁹40 Co.09

+80 - 0.39' B = cut 87.24 86.⁷⁰70 Co.54 86.23 86.⁵⁰50 Fo.27

+2+00 0.34' B. 87.14 86.⁸⁰80 Co.34 86.37 86.⁶⁰60 Fo.23

+10 86.42 86.⁹¹91 Fo.49 86.59 86.⁷¹71 Fo.12

+20 86.38 87.¹⁴14 Fo.76 86.95 86.⁹⁴94 Co.01

+40 - 0.29 B. 88.05 87.⁷¹71 Co.34 87.40 87.⁵¹51 Fo.11

+50 - 0.24 B. 88.70 88.²²22 Co.48 91.41 88.⁰²02 C 3.39

+60 0.29 B. 90.06 89.¹⁷17 Co.89 91.41 88.⁹⁷97 C 2.44

+90 - 0.30 B. 93.64 92.⁷⁰70 Co.94 94.24 92.⁵²52 C 1.72

+3+00.73 = SL C 93.27 93.31 93.68 93.71

Curb Stakes - Marilou + Brookline
 Plan - 2738-D - 5-16-55 7.0.

222.82 = Top F.H. NE. Date + Brookline

7

48th + Marilou

Sw. Alley Ret.

along Brookline
 E.C. = 0+00

W. end

P.C. - Alley

E.C. - Join

Nw. Alley Ret.

W. end.

P.C. to Alley

E.C. to st.

1/2

E.C. = 0+00

+ 14.24

+ 28.48

39.09
 + 67.57

+ 87.57

1 + 07.57

+ 27.57 = P.C.

1/3

2/3

30.94

30.57

30.57

30.91

30.74

30.74

30.37

29.90

29.74

29.35

28.21

27.50

26.34

25.63

25.03

24.02

30.66

30.54

30.50³

30.45⁹¹

30.33⁷⁴

30.27⁷⁴

30.14³⁷

29.90⁹⁰

29.80⁸⁰

29.53³⁵

28.52²¹

27.88⁵⁰

27.00^{6.34}

26.00^{6.3}

25.22⁰³

24.43⁰²

C 0.28

C 0.03

C 0.07

C 0.46

C 0.41

C 0.47

C 0.23

F 0.10

F 0.06

F 0.18

F 0.31

F 0.38

F 0.66

F 0.37

F 0.19

F 0.41

0+31.5

0+63.01

SL. Date
 + 83.01 =

PC = inlet

1/3

2/3

P.R.C.

1/3

2/3

E.C. = 0+00

0+40

+ 80

1+20

+ 58.47

1+98.47

2+38.47

+ 78.47

23.05

21.64

20.15

19.62

S. 19.35
 N. 19.41

19.31

19.49

19.55

19.77

19.48

19.27

19.50

20.01

20.90

21.66

22.32

23.68

23.91

23.65

22.07

20.50

19.70

19.60

19.62

19.68

19.81

19.96

20.11

20.25

20.79

21.32

21.86

22.37

23.01

23.68

24.43

F 0.60

F 0.43

F 0.35

F 0.08

F 0.31

F 0.19

F 0.26

F 0.19

F 0.63

F 0.98

F 1.29

F 1.31

F 0.96

F 0.71

F 0.69

G.

F 0.52

229.09 - Pole

E. Elm + Brookline

217.21 = Pole Tilded

8

3 + 13.47 24.57 25.13_{4.57} F 0.56+ 48.47 25.27 25.83₂₇ F 0.56+ 83.47 25.88 26.53_{8.88} F 0.654 + 20.41 = P.C. 26.67 27.27_{6.67} F 0.601/4 27.30 27.48₃₀ F 0.181/2 27.62 27.69₆₉ F 0.073/4 = Elm. 27.82 27.90₈₂ F 0.08E.C. = 0 + 00 27.69 28.05_{9.69} F 0.360 + 07 27.57 28.10_{7.57} F 0.53+ 20 27.45 28.00_{7.45} F 0.55+ 55 27.31 27.69₃₁ F 0.38+ 90 27.17 27.38₁₇ F 0.21

1 + 25 27.00 27.07 F 0.07

+ 60 26.69 26.76₆₉ F 0.07

+ 95 26.00 26.45 F 0.45

2 + 30 = T.P. 25.54 26.14_{5.54} F 0.60+ 65 25.10 25.83_{5.10} F 0.73+ 90.87 24.73 25.60_{4.73} F 0.873 + 10.87 24.24 25.10_{4.24} F 0.86+ 30.87 23.53 24.30_{3.53} F 0.773 + 50.87 22.65 23.10_{2.65} F 0.45+ 70.87 21.47 21.30₄₇ C 0.17+ 96.25 19.09 18.40_{19.09} C 0.694 + 11.32 18.21 17.30_{8.21} C 0.91+ 26.40 17.56 16.80_{7.56} C 0.76+ 41.47 = B.C. 17.12 16.60_{7.12} C 0.521/3 16.90 16.49₉₀ C 0.412/3 16.80 16.38₈₀ C 0.42

Meet. cb = 16.20 16.27

S.E. Cor. - Brookline + Date

S.L. Date 19.88 19.60₈₈ C 0.28Brookline P.C. to 19.68 19.50₆₈ C 0.18

E.C. to Date 19.52 19.50 = Meet.

Pave Edge Grades
Brookline St East edge

staked 3' BK
pave edge

staked 3' BK paving edge
n/sly

Sly line Date St curb end 219¹⁰ meet +57⁵ wly 228⁵²
+20 South 220⁰⁰ 0²⁷ C.O. 99

+51⁵⁰ South 220⁵⁷ 1²⁰ C.O. 13 +77⁵ wly 229⁰⁰

+83⁰¹ E.C. South 223¹⁵ 2⁸⁷ F.O. 28 +96⁵⁷ wly SEC. 229⁵³
55.5' pav. edge Radius 11 1/2' pav. Rad.

1/4 Mid Pt. 223⁸⁸ 4⁰⁴ C.O. 16 229²⁵

1/2 Meet existing ch + gutter 48¹⁴ St. 224⁶² 229⁹⁸ meet

3/4 225³⁶

B.C. Marilou Rd Sly edge 226¹⁰

+17⁵ wly toward 48¹⁴ 227⁰⁰

+37⁵ wly 227⁸⁸

continued top pt page

Stake 18" Drain - Ash st. Hwy. to
Kettner - Plan - 2768-D - 8-3055 7.0

0+00 = ⁰⁺⁰⁰ Cross

1242 = □ in Signal Base - S. side at R.R.

10

0+00 = Beg. 18" across Kettner = 6.75'

0+00 = Meet Box

0.83 0.86

S'rt.

0+36.45' = Φ 17.15 ^{17.15} 7.12 10.03

Sta. 0+18 on St.
0+26 = P.C.

4.13 4.13 1.14 c 2.99

0+72.9 = Φ pipe 18.20 ^{18.20} 7.50 10.76

+55 5.81 5.81 1.64 c 4.17

at cb. line

+90 6.28 6.28 2.13 4.15

10 N. 12.62 ^{12.62} 5.40 c 7.22

1+25 7.63 7.63 2.63 5.00

Φ Box 3+05.43 12.62 5.00 c 7.62

+60 8.62 8.62 3.12 5.50

E. of Pipe Cross Ash

+95 9.65 9.65 3.62 6.03

0+00 7'S. 12.20 ^{12.20} 5.40 6.80

+26.37 = Meet. 4.07

+82.37 = Beg. - Meet. 4.77

= Φ 12.50 ^{12.50} 6.15 c 6.35

7'S. 12.33 ^{12.33} 6.90 c 5.43

3+05.43 = Φ Box 12.20 ^{12.20} 5.00 c 7.20

= cb. Line = Φ Box

+40 12.50 ^{12.50} 5.37 c 7.13

+75 13.34 ^{13.34} 5.75 c 7.59

4+10 14.10 ^{14.10} 6.13 c 7.97

+45 14.86 ^{14.86} 6.51 c 8.35

+66.52 = Φ Box 15.08 ^{15.08} 6.75 8.33
= 0+00 ahead.

Curb Line + Grade for Boxes

3+05.43 = \pm Box - N. Side - See P. 10

W. edge Box = cb. Grade	11.87	12.27	F 0.70
= gut	11.67	11.72	C 0.25
E. edge Box	11.67	12.38	F 0.71

Box on S. - By R.R.

W. edge Box - cb.	11.44	12.20	F 0.76
gut - flat.	11.37	11.36	C 0.01
E. edge Box - cb.	11.37	12.32	F 0.95

Box at N.W. Cor. Kettner

W. edge Box - cb.	14.45	15.91	F 1.46
gut	14.45	15.30	F 0.85
E. edge = P.C.	13.23	16.02	F 2.82

Box on N.E. Cor. gut = 16.98 17.23 F 0.25

P.C. + edge Box - 3's	16.98	18.05	F 1.07
= N. edge - Meet.	18.09	18.10	
+ 2.67	18.11	18.14	

Corb. Stakes Ash St. Hwy. to Kettner

N. Side

S. Side

Join

SE. Ret. at Pac. Hwy

0+00		7.56		Join	4.00		
+37	8.59	8.77 ⁵⁹	F 0.18	1/3	3.66	4.03 ^{3.66}	F 0.37
+74.50	9.68	9.99 ⁶⁸	F 0.31	2/3	3.82	4.12 ^{3.82}	F 0.30
+91 = end.	10.55	10.50	C 0.05	P.C. = 0+00	4.11	4.28 ^{4.11}	F 0.17
100 Row				0+16	4.40	4.47 ^{4.40}	F 0.27
0+00 = Line = wly. of Box				+50	5.64	5.74 ^{5.64}	F 0.10
0+53.3 = Ely. of Box	12.31	12.38		+85 ³⁵	6.67	6.85 ^{6.67}	F 0.18
+35	12.85	13.02 ^{2.85}	F 0.17	+20	7.91	7.95 ^{7.91}	F 0.04
+50	13.05	13.42 ⁰⁵	F 0.37	+55	8.77	9.06 ^{8.77}	F 0.29
+75	13.62	14.02 ^{3.62}	F 0.40	+74.50 ^{16.50}	9.53	9.67 ^{9.53}	F 0.14
1+00	14.42	14.62 ⁴²	F 0.20	1+91.50 = end.	9.59	10.14 ^{9.59}	F 0.55
+25	14.91	15.21 ^{4.91}	F 0.30	100' Row			
+50	15.51	15.80 ⁵¹	F 0.29	0+00 = Line Beg.	11.66	11.67	F 0.01
+60 - out.		15.88		+22.75 = E Box		12.27	
edge of Box +67 = P.C.	16.01	16.02		+50	12.54	12.82 ^{12.54}	F 0.28
1/4	16.23	16.16 ²³	C 0.07	+85	13.52	13.62	F 0.10
1/2	16.11	16.28 ¹¹	F 0.17	+20	14.22	14.42	F 0.20
3/4	16.35	16.40	F 0.05	+60	14.97	15.34 ^{14.97}	F 0.37
F.C. = Meet.	16.52	16.50					

N.E. Cov. Kettner.

Meet. 18.11 18.14
 + 2.67 = edge Box
 + 8 = P.C. 18.05
 1/2 18.04 18.05 F0.01
 EC 18.16 18.12 C0.04
 25' from E.L. 18.66 18.75⁶⁶ F0.09
 40' 19.21 19.10 C0.11
 70 19.84 20.01 F0.17
 100 = Meet. 20.92

S. Side

1+70 = P.C. 15.19 15.46₉ F0.27
 1/3 15.20 15.51₂₀ F0.31
 2/3 14.88 15.49_{4.88} F0.61
 EC = Meet. 15.46
 S.E. Cov. Kettner.
 EC = Kettner Meet. 16.96
 1/4 16.68 17.00 F0.32
 1/2 16.67 17.05_{16.67} F0.38
 3/4 16.81 17.13_{6.81} F0.32
 BC = Ash Meet. 17.25

Stake Alley - Block 35 - Parish + Loomis
 Plan - 11715 - L w.O. 32416 - 11-10-55

Sub. 26⁴¹ + E. B.M. 106.18 - 0-20 Cross 14
 169.24 = Pole - N. end.

N. + S. Alley - 19.55 wide West

2' Back unless Noted.

East.

0-10					65.11	64.88 ^{5.11}	C 0.23
0-05	68.74	67.80 ^{8.74}	C 0.94		65.32	65.05 ³³	C 0.27
0+00 = N.L. of E.	69.14	67.75 ^{9.14}	C 1.44		64.95	65.10 ^{4.10}	F 0.15
+10	69.30	67.06 ^{9.30}	C 2.24	1.38 B.	65.52	65.20 ⁵²	C 0.32
+20	69.23	66.38 ^{9.23}	C 2.85	1.35 B.	65.34	65.30 ³⁴	C 0.04
+30	68.36	65.90 ^{8.36}	C 2.46		65.25	65.40 ²⁵	F 0.15
+40	68.52	65.80 ^{8.52}	C 2.72		65.21	65.50 ²¹	F 0.29
+75	68.36	66.15 ^{8.36}	C 2.21		65.35	65.85 ³⁵	F 0.50
1+10	67.84	66.50 ^{7.84}	C 1.34		65.62	66.20 ⁶²	F 0.58
+40.06 = S.L. E+W Alley	69.04	66.30 ^{9.04}	C 2.74	2' Bk Both ways	65.90	66.00 ⁹⁰ 5.99	F 0.10
+60.06 = N.L.	68.95	66.30 ^{8.95}	C 2.65		65.57	66.00 ⁵⁷	F 0.43
+90	69.48	66.92 ^{9.48}	C 2.56		64.31	66.64 ⁴⁸ 7.31	F 2.33
2+23.3 = Meet Conc.		67.60				67.11	

E+W Alley - Cont. from P. 15

South

North

2+75	65.11	65.30 ¹¹	F 0.19		65.57	65.30 ⁵⁷	C 0.27
+80.59 = E.L. of Alley		66.00				66.00	

E. + W. Alley - 19.50' wide - except E-end = 1' on S. side

159.22 = Tot. in Cr. of wall

15

162.48 = ± Cross - N + S Alley

		South.			North
0+00 = W.L. Alley		61.93			63.09
+05 - 0.25 Bk.	61.59	61.75 ⁵⁹	F 0.16	62.41	62.05 ⁴¹ C 0.36
+30	58.36	55.57 ³⁶	F 0.21	56.35	55.87 ³⁵ C 0.48
+40 - 1.40 Bk.	53.99	53.42 ⁹⁹	C 0.57	54.45	53.72 ⁴⁵ C 0.73
+50 - 1.60 Bk.	53.55	51.90 ⁵⁵	C 1.65	53.29	52.20 ²⁹ C 1.09
+70 - 1.29 Bk.	50.99	49.50 ⁹⁹	C 1.49	50.24	49.80 ²⁴ C 0.44
+90	47.30	47.20 ³⁰	C 0.10	1.45 Bk. 47.73	47.50 ⁷³ C 0.23
1+00	46.80	46.20 ⁸⁰	C 0.60	1' Bk. 46.95	46.50 ⁹⁵ C 0.45
+10	46.49	45.45 ⁴⁹	C 1.04	45.36	45.75 ³⁶ F 0.39
+20	45.26	45.23 ²⁶	C 0.03	45.13	45.53 ¹³ F 0.40
+30 - 1.50 Bk.	45.16	45.20	F 0.04	45.28	45.50 ²⁸ F 0.22
+40	44.95	45.28 ⁹⁵	F 0.33	44.63	45.58 ⁶³ F 0.95
+50	44.76	45.40 ⁷⁶	F 0.64	45.73	45.70 C 0.03
+60	45.05	45.62 ⁰⁵	F 0.57	46.15	45.92 ¹⁵ C 0.23
+70 - 5 Bk.	45.56	46.10 ⁵⁶	F 0.54	46.36	46.40 F 0.04
+90	49.35	48.83 ³⁵	C 0.52	0.07 Bk. 49.89	49.02 ⁸⁹ C 0.87
2+20 - 4 Bk.	54.02	54.73 ⁰²	F 0.71	54.40	54.85 F 0.45
+45	59.13	59.64 ¹³	F 0.51	60.67	59.70 ⁶⁷ C 0.97
+70	64.59	64.55 ⁵⁹	C 0.04	65.43	64.55 ⁴³ C 0.88

Cont. on P. 14

Stake Alley - Block 317 - Land + Town
 28th + Hensley - Plan - 12012 - A - L

67.51
 .17
 .34

16

W.O. 32004

1-16-56

7.0.

Sly.

		Nly	at PC.	68.59	67.18	C 1.41
= 2' Rad.	67.10	67.25 F 0.15	at Ang. 2' Rad	67.80	67.36	C 0.44
Top cb = end By Hensley	Top 68.01	67.58 C 0.43	at Line = end Top	67.79	67.42	C 0.37
0+00 = NL. + Sub.	9ut.	67.38 C 0.63		68.22	67.38	C 0.84
+08.11	67.75	67.51 C 0.24	67.17 - 34 up	68.33	67.51	C 0.82
+35	68.13	67.93 C 0.20		68.46	67.93	C 0.53
+70	68.77	68.48 C 0.29		68.89	68.48	C 0.41
1+05	69.22	69.03 C 0.19		69.55	69.03	C 0.52
+28.11	69.70	69.39 C 0.31		70.00	69.39	C 0.61
+38.11	70.07	69.47 C 0.60	New	70.05	69.47	C 0.58
+48.11	70.25	69.42 C 0.83		70.54	69.44	C 1.10
+58.11	70.15	69.22 C 0.93		70.65	69.30	C 1.35
+68.11	69.87	68.88 C 0.99		70.63	69.05	C 1.58
+77.31	Top cb. 68.76	68.51 C 0.25	1.5 Bk.	70.68	68.74	C 1.94
+93.91 = Pop. on S. = W.L. 28 th			Top cb.	69.10	68.60	C 0.50

Rough Grades - Hensley - Commercial - S to End
 See. P. 16

E.

W.

Commercial
 0 + 00 = SL.

66.4 66.0 C 0.4

66.0 65.8^{6.0} C 0.2

+ 50

66.6 66.6 C

67.2 66.4^{7.2} C 0.8

1 + 00

3 in

68.2 67.0^{8.2} C 1.2

+ 02.27 = P.C. on E.

+ 16.69 = P.C. on W.

Curb Stakes.

0 + 00 = SL

66.06 66.04⁰⁶ C 0.02

65.72 65.76⁷² F 0.04

+ 35

66.21 66.45²¹ F 0.24

66.10 66.18 F 0.08

+ 70

66.82 66.86⁸² F 0.04

66.60 66.59 C 0.01

+ 95

67.43 66.88^{7 43} C 0.55

1 + 02.27 = P.C.

67.25

3 BK.
 = P.C. 2 Rad.

67.68 67.14⁶⁸ C 0.54

+ 16.69 = P.C. on W.

Stake Alley - Block 221 - Pac. Beach
 Plan- 12694-L - W.O. 62452 2-2-56 7.0.

BM. 39.53 = N.W.B.P. Garnet + Everts 18.
 B.M. 41.68 = spike in Pole # 1254

North

South

0+00 = E.L. Everts

37.14

6.91

36.86

+25 - 2' B.

37.81

37.59⁸¹ Co.22

37.29

37.37²⁹

F 0.08

+50 - 0.10 B.

38.46

38.04⁴⁶ Co.42

0+49

37.76

37.85⁷⁶

F 0.09

+75 - 0.10 B.

39.20

38.49²⁰ Co.71

38.17

38.38¹⁷

F 0.21

1+00 0.37 B.

39.71

38.93⁷¹ Co.78

38.74

38.88⁷⁴

F 0.14

+20 0.37 B.

39.61

39.23⁶¹ Co.38

38.95

39.21⁹⁵

F 0.26

+40

40.02

39.50⁰² Co.52

28.

39.64

39.49⁶⁴

Co.15

+60

40.16

39.70¹⁶ Co.46

39.88

39.70⁸⁸

Co.18

+80

40.41

39.86⁴¹ Co.55

40.09

39.86⁰⁹

Co.23

2+10 = end.

39.95

40.07⁹⁵ F 0.12

40.46

40.07⁴⁶

Co.39

0+86.5

39.23

38.70²³ Co.53

= ± of openings

1+10

39.35

39.08³⁵ Co.27

2+00

40.33

40.00³³

Co.33

Curb Grades - Commercial - EVANS
 Plan - 12011-L - 2-10-56 7.0.

To 29+2

19

	N				S.
0+04 = Meet.	64.96	- 64.01			
0+00 = E.L. Evans	65.00			65.00	.02
+10	65.18	65.08 ¹⁸	C 0.10	65.19	65.03 ¹⁹ C 0.16
+35 = 33.3	65.43	65.25 ⁴³	C 0.18	64.91	65.09 ^{4.91} F 0.18
+70 = +66.6	66.00	65.50 ⁶⁰⁰	C 0.50	65.24	65.18 ²⁴ C 0.06
1+01 = Meet. 29+01 .83	65.75				
+05				65.32	65.27 ³² C 0.05
+40				65.48	65.36 ⁴⁸ C 0.12
+75				65.73	65.45 ⁷³ C 0.28
2+00				65.83	65.50 ⁸³ C 0.33
+10 = W.L. Hensley = P.C.				65.80	65.56 ⁸⁰ C 0.24
1/2				65.62	65.64 ⁶² F 0.02
E.C.		s. side - 2' N. of edge		65.52	65.72 ⁵² F 0.20
F. w.gut	65.34	65.13 ³⁴	C 0.21		
Beq. E. Side E.gut.	65.63	65.36 ⁶³	C 0.27		
E.C.				65.70	66.02 F 0.32
1/2				66.06	65.98 ⁰⁶ C 0.08
P.C.					
+00 = E.L. Hensley = P.C.	66.07 ⁰⁷	67.08 ⁰⁷		66.17	65.94 ¹⁷ C 0.23
+10	66.88	67.10 ⁸⁸	C 0.38 = to gut.	66.21	66.00 ⁸⁸ C 0.21

Cont. on P. 20

		67.99					
		66.58	C 0.41 = 10	got.			
0 + 45	66.99	67.17	F 0.18		66.66	66.66	C 0.53
+63 = Meet.		6.99					
+80		67.20 - 67.22			66.52	66.52	C 0.27
1 + 15					66.68	66.68	C 0.30
+50.25 = WL 28 th						66.50	
Req. E. Side 28 th							
Meet		67.82					
4-5 = P.C.	67.63	67.74	F 0.11				
1/2		67.59	F 0.03	end at Prop	67.86	67.96	F 0.10
EL 28 th	67.56	67.59		EC.			
E.C. = 0 + 00 =	67.54	67.44	C 0.10	0 + 00	67.88	67.78	C 0.16
+22.57 inlet		67.67		2' Rad.			
+33.5		67.67		2 + 14.50 = P.C.	67.88	67.69	C 0.19
+43.5	67.94	67.70	C 0.24	+49.50	67.93	67.78	C 0.15
+73.5	67.61	67.80	F 0.19	+84.50	67.90	67.88	C 0.02
1 + 03.5	67.66	67.90	F 0.24	3 + 19.50	68.10	67.97	C 0.13
+33.5	67.85	68.00	F 0.15	+54.50	68.18	68.07	C 0.11
+67 = P.C. 2' Rad.	67.88	68.11	F 0.23	+89.50	68.47	68.16	C 0.31
E.C.	67.88	68.16	F 0.28	4 + 24.50	68.39	68.26	C 0.13
End	68.76	68.40	C 0.36	4 + 59.50	68.50	68.35	C 0.15
				+84.50 WL.	68.36	68.42	F 0.06
				+94.50 = Meet.		68.46	

N.

End at Prop.	69.67	69. ⁶⁷ 16	C0.51	2+33.5	68.89	68. ⁸⁹ 13	C0.76
P.C.	68.62	68.92	F0.35	+63.5	68.88	68. ⁸⁸ 22	C0.66
E.C. = 4+21.72	68.62	68.89	F0.27	+93.5	68.72	68. ⁷² 30	C0.42
+57.97	68.45	68.99	F0.54	^{26.2} 4+19.7 = Beg. cb.		68.38	
+84.22	68.75	69.06	F0.31	Beg. Conc. Sect. on S. - at 28 th			
+94.22 = w.L. 29 th = Meet.		69.09 = .11		0+00 = E.L. 28 th			

Rails on N. side

+50

2+88	68.04 = C004	Ext. Grade	68.00	1+00 = end Conc. in	67.13	66.52	-.49 = got
3+02.7		68.04		+12 = Brk	67.81	66.62	C1.19
3+13	Line 68.10	68.07	C0.03	²⁵ +37	67.82	66.76	C1.06
3+43.8	68.30 3 rd = C0.08	68.16		+62	67.81	66.90	C0.91
4+10.8 = end. - 3 rd	68.54 = Trade C0.13	68.35	.41	+87	67.95	67.04	C0.91

Beg. Stakes for Conc. Sect. on N.

2+12.5 = Meet cb.

1st out from edge

1+69 = end cb.	Stakes 1 st Bk of Prop.	67.62		3+03.5	67.59	68. ⁰⁵ 13	F0.46
³⁵ 2+04	68.50	67.74	C0.76	+33.5	67.81	68. ¹³ 13	F0.32
+39	68.57	67.85	C0.72	+63.5	67.96	68. ²² 16	F0.26
+73.5 = Brk. = 0.55 Brk	69.13	67.96	C1.17	+93.5	68.06	68. ³⁰ 05	F0.25
³⁰ 3+03.5	68.94	68. ⁰⁵ 05	C0.89				

Stake Drain - Winamar + Avenida
Plan - 11936-L - 2-16-56 7.0.

Cresta B.M. = 63.41 = NW \square .

22

Req. 12" Concr. at Inlet.

Gutter Grades.

4-end	63.91	^{63.91} 57.40	C 6.51				
± H Inlet - 5' bk. = 0+00	63.85	^{63.85} 57.31	6.54	E.C. Meet	^{-90'} 64.82	64.60	- Meet
+34.20 = B.C.	62.70	^{62.70} 56.62	6.08	+13.7	64.51	^{+ .51} 63.80	C 0.71
1/4	63.01	^{63.01} 56.52	6.49	+13.7	63.82	⁸² 63.20	C 0.62
1/2	62.79	^{62.79} 56.42	6.37	+8.6 = ± Inlet	63.85	^{3.85} 62.90	C 0.95
3/4	62.50	^{62.50} 56.32	6.18	+5 = B.C. = 0+00	63.73	⁷³ 63.06	C 0.67
+53.83 = E.C.	62.19	^{62.19} 56.23	5.96	+35	63.85	⁸⁵ 63.19	0.66
+89.53	59.07	^{59.07} 55.52	3.55	+70	63.95	⁹⁵ 63.32	0.63
+99.53	58.20	^{58.20} 55.11	3.09	+05	64.07	^{4.07} 63.45	0.62
1+09.53	57.27	^{7.27} 54.49	2.78	+40	64.14	^{4.14} 63.58	0.56
+19.53	56.30	^{6.30} 53.66	2.64	+75	63.89	^{.89} 63.71	0.18
+29.53	55.26	^{5.26} 52.62	2.64	2+10	64.37	^{4.37} 63.84	0.53
+64.53	51.29	^{51.29} 48.24	3.05	+49.45 = B.C.	64.59	^{4.59} 63.98	0.61
+99.53	46.96	^{6.96} 43.87	3.09	²⁵ +74.45	64.76	⁷⁶ 64.07	0.69
2+34.53	42.63	^{42.63} 39.50	C 3.13	+99.45	64.71	⁷¹ 64.16	0.55
+58.53 = Ang.	39.61	^{9.61} 36.50	3.11	²⁵ 3+24.45	64.85	⁸⁵ 64.26	0.59
+70.53 Ang.	38.11	^{8.11} 35.00	3.11	+49.45	65.01	^{5.01} 64.41	0.60
+86.53 = Conn.	36.14	^{6.14} 33.00	3.14	²⁵ +74.45	65.24	^{5.24} 64.56	0.68
				³⁵ 4+09.45	65.46	^{5.46} 64.96	0.50

Stake Curb - West Side of Coast Blvd.

23

	29.78		29.4			
0+00 = Meet end of Exist. curb.				30.58		
+10 =			30.23	30.72 ₂₃	F 0.49	
+25 =			30.42	31.00 ₄₂	F 0.58	
+50 =		31.39	31.25	31.60 ₂₅	F 0.35	
+75 =	32.07	32.21	32.63	32.30 ₆₃	C 0.33	
1 ~						
+35 =	got 33.93	33.11 E	33.28	33.40 ₂₈	F 0.12	
+70 =		34.43 E	34.09	33.55	34.44 ₅₅	F 0.89
+70 =		34.16	34.37	34.70 ₃₇	F 0.33	
2+05 =	34.21	34.41	34.40	34.73	34.83	F 0.10
+40 =		34.55	34.62	34.98 ₆₂	F 0.36	
+75 =		34.68	34.57	35.13 ₅₇	F 0.56	
3+10 =	34.58	34.81	34.85	34.34	35.28 ₃₄	F 0.94
+45 =			34.82	35.40 ₈₂	F 0.58	
+80 =		35.06	35.08	35.04	35.52 ₀₄	F 0.48
3+18 = E inlet		34.89	5.17			
4+15 =			35.19	35.19	35.64 ₁₉	F 0.45
+50 =		35.44	35.32	35.45	35.75 ₄₅	F 0.30
+85 =			35.83	35.90	F 0.07	
5+20 =	35.19	35.63	35.64	36.27	36.05 ₂₇	C 0.22
+55 =			36.63	36.20 ₆₃	C 0.43	

	±	Edge			
5+90 = E.C.	35.91	35.98	36.60	36.35 ⁶⁰	C 0.25
6+10			36.78	36.44 ⁷⁸	C 0.34
+40		36.19		7.23	
6+45	35.76	36.10	36.15	37.23	36.58 C 0.65
6+80	36.04	36.35 ^{11.4}	36.56	36.26 ⁵⁶	C 0.30
		35.83		6.21	
7+11.45			36.21	35.94	C 0.27
7+18.45	35.76	35.36		35.84 = Top	
		90+			

Stake Alley - Block 128 - M+S. Sub.

Map. 209 + 379

25

See Plan -

11992-L

7.0.

B.M. 37.40 = S.W. CP. Newton + Evans.

W.O. 32467

4-12-56

N

S

0+00 = E.L. Dewey	5.89	35.92		35.43		35.61	35.54	
+20 0.07 BK.	37.22	^{7.22} 36.24	C 0.98	2' BK.	35.50	35.93	F 0.40	
+55	37.09	^{7.09} 36.80	C 0.29	1.50 BK.	36.85	^{15.3} 36.49	C 0.36	
+90	37.78	^{7.8} 37.35	C 0.43	1' BK.	37.57	^{5.7} 37.04	C 0.53	
1+25	38.25	^{8.25} 37.90	C 0.35	2' "	37.86	^{8.6} 37.60	C 0.26	
+60	38.68	^{6.8} 38.46	C 0.22	1.50 BK.	37.67	^{6.7} 38.15	F 0.48	
+95	39.92	^{9.2} 39.02	C 0.90	1.50 "	38.71	38.70	C 0.01	
2+30	39.85	^{8.5} 39.57	C 0.28		39.57	^{5.7} 39.26	C 0.31	
+65	41.17	^{1.17} 40.13	C 1.04		40.24	^{4.0} ^{2.4} 39.82	C 0.42	
3+00	41.78	^{1.78} 40.68	C 1.10		41.05	^{0.5} 40.37	C 0.68	
+35	42.20	^{2.20} 41.24	C 0.96		41.39	^{1.39} 40.93	C 0.46	
+70	43.70	^{3.70} 41.79	C 1.91		42.19	^{2.19} 41.48	C 0.71	
4+05	42.99	^{9.9} 42.35	C 0.64		42.12	^{1.2} 42.04	C 0.08	
+40	43.70	^{3.70} 42.90	C 0.80	120 BK.	42.99	^{9.9} 42.60	C 0.39	
+80 0.50 BK.	43.69	^{6.9} 43.53	C 0.16		42.48	^{2.48} 43.08	F 0.60	
5+00 1.50 BK.	43.67	^{6.7} 43.82	F 0.15	0.73 BK.	43.69	^{6.9} 43.32	C 0.37	
+20	44.73	^{7.3} 44.06	C 0.67		43.59	^{5.9} 43.56	C 0.03	
+40 - 0.36 in	45.44	^{5.44} 44.27	C 1.17	E Grade 0.40 Dip.	43.69	43.80	F 0.11	
+70 - 2.14 BK.	45.65	^{5.65} 44.58	C 1.07	^{5.65} 43.96	^{4.13} 43.96	44.13	^{6.9} 44.03	C 0.10
6+00.77 = W.L. Evans.		44.89		43.69	^{0.17} 44.34		^{4.26} 44.26	

Tie out 7' points along S. Side of Univ
in way of Telephone Cond.

w.o. 20575
4-30-56 7.0

Corner.	Univ. &			
SW	15.2201 7 + W.L.	"	39 th	8' Cross - NE + SE
SW.	7'	"	40 th	10' SW - P.K. - 10' NW - Cross
SE	7'	"	40 th	8' P.K. - SE + 8' Cross NE.
SW	7'	"	Central	9' Cross - NW + SW.
SE - cross	7'	"	Central	10' Cross NE + SE.
SW	7'	"	41 st	10' Cross - NW + SW.
SE	7'	"	Marlborough	10' Cross NE + SE.
SW.	7'	"	42 nd	10' Cross - NW + SW.
SW	7'	"	Van Dyke	8' Cross NW + SW.
SW.	7'	"	43 rd	8' Cross - NW + SW.
SE	7'	43 rd + Wightman		8' Cross NE + SE.
NE.	7'	"	Landis	7' Cross - SE - 9' Cross NE.
SE.	7'	"	Landis	7' Cross - NE + SE.
SW.	7'	Myrtle + Fairmount		9' Cross - SW - 63' Cross in db. on Line to chimney of House
NE.	O.K.	7'	Thorn + Fairmount	44' Cross - NE + 20' SE. in Conc. gut.
SE.	O.K.	7'	" + "	65.97 Bet. cts + Cross 20' - Ely.
SE.	O.K.	7'	Quince + Fairmount	16.28 To x in Hyd. Top 15' Cross - SE.

Stake Curbs on Lowry Place - S. Side
at Roseland Dr. - See Plan - 3514-D.

6-22-56

27

7.6.

No W.O. -

Lowry + Roseland.

B.M. = Const. Bench = Top Hyd. SE. Cr. 48.71

Set B.M. on Mon. - NE. PC. Lowry + Alamar 43.21

0+00 = P.C. at Roseland. 47.45 44.21 C 3.24

+35 5' Bk. 47.48 43.24 C 4.24

+70 3' Bk. 42.84 42.26 C 0.58

1+04.02 - 3' Bk. 40.23 41.31 F 1.08

+24.02 39.87 40.61 F 0.74

+44.02 39.44 39.64 F 0.20

+63.22 = B.C. 39.29 38.40 C 0.89 ch -

¹³/₄ 76.33 38.03 37.58 C 0.45 13.66 5° 25' 20"

¹¹/₂ 89.44 37.24 36.76 C 0.48 10° 50' 40"

¹⁶/₃ 42+02.55 - 3' Bk. 37.08 36.15 C 0.93 16° 16'

+ 18.66 = Meet. 35.26 - 21° 41' 20"

cb. Rad. = 69.29

3' Bk. = 72.29

Total Δ = 43° 22' 40"

Total to 52.46' on curb.

3' Move to Meet.

Rough Grade Stakes -

33rd - N. of

Date. - Plan - 3175 - D

w.o. 32577 - 7-3-56

7.0.

B.M. = 17' ct S.W. Cor. - 33rd + Date

234.96

West.

East.

			West.			East.	
0+00 = N.L. Date	-35' out	35.3	^{5.3} 34.0	C 1.3	30.5 out	37.3	^{7.3} 33.0 C 4.3
+38 = Sewer lat. - S.B.K.		33.7	^{33.70} 29.00	C 4.70			
+50	35' out	33.4	^{3.4} 32.6	C 0.8	35 out	34.5	^{4.5} 31.6 C 2.9
+90	31' out	33.7	^{3.7} 30.5	C 3.2	30' out	33.1	^{3.1} 29.5 C 3.6
1+30	35' out	28.7	^{8.7} 26.8	C 1.9	35' out	26.7	^{6.7} 25.8 C 0.9
+45.71 = P.C. = 3' B.K.		27.4	^{7.4} 24.9	C 2.5	3' B.K.	25.1	^{5.1} 23.9 C 1.2
+80 = Turnaround - 5' B.K.		23.5	^{3.5} 21.4	C 2.1	5' B.K.	23.8	^{3.8} 20.4 C 3.4
2+10 = End.	- 5' B.K.	19.4	19.5	F 0.1			19.5

Set B.M. = □ in Step - House on Lt. 219.08

stake = $\frac{03.2}{F 16.3}$
24.4 out
from Prop. - $\frac{0.8}{5}$

Top stake ⊥ Prod. ⊥

stake = $\frac{191.8}{F 27.7}$
41.5 out. 19.5 - $\frac{1.4}{5}$

Water Services Stakes.

Top curb. Grade

Sewer to be lowered.

0+06 - Lt. 32.99 33.77 F 0.78

0+67.3 Rt. 31.07 ^{1.07} 30.88 C 0.19

0+83 Lt. 30.58 ^{0.58} 31.02 F 0.44

1+22.7 - Rt. 27.01 ^{7.01} 26.53 C 0.48

1+27 - Lt. 27.02 27.08 F 0.06

2.55 of P.R.C. - Rt. 23.21 ^{3.21} 22.40 C 0.81

1+77 = Lt on Turn. 21.82 ⁴² 21.65 C 0.17

Stakes for "K" Inlet.

7' from ± Inlet at cb. Line

7' W. - Top. cb. 18.85 19.50 F 0.65

7' E. - I.E. 11.67 ^{18.85} C 0.718

7' E. - Top cb. 18.00 19.50 F 1.50

I.E. 11.67 ^{8.00} C 6.33

0+40 = 31.53 ^{31.53} 28.00 C 3.53

+60 30.64 ^{30.64} 27.44 C 3.20

0+80 = Conn. 29.38 ^{29.38} 26.88 C 2.50

Stakes for 18" R.C. Pipe - 10' Rt.

0+00 = Ang. Pt. on ± 2.90' N. of cb. face

0+33.13 = Wall 204.34 ^{04.34} 194.50 C 9.84
I.E. pipe

0+66.25 - 10' Rt. 84.14 ^{4.14} 82.20 C 1.94

I.E. end 10' Lt. 85.66 ^{5.66} 82.20 C 3.46
Pipe

0+76.58 = Stake on 82.85 ^{2.85} 81.90 C 0.95
± 5' from end of Apron.
Top-end apron.

Grade Stakes - Alley Blk. 12 - Pt.

Plan - 3194-D - 7-24-56

7.0.

W.O. 31870

44.93

42.90^{4.93} C 2.03

Loma Hts.

B.M. = 7' Disk - Oliphant

122.10

30

43.51

42.90^{3.51}

C 0.61

E.

2' Bk. unless Noted.

W.

0+00 = Sl. Oliphant

22.39

22.61

+35

25.02

24.14^{5.02} C 0.88

25.53

24.31^{15.53} C 1.22

+70

26.04

25.89^{5.04} C 0.15

26.72

26.01⁷² C 0.71

1+05

27.86

27.64⁸⁶ C 0.22

28.29

27.71⁸²⁹ C 0.58

+40

29.02

29.39⁸⁶ F 0.37

29.61

29.40⁶¹ C 0.21

+60

30.34

30.63³⁴ F 0.29

0.34 B.

31.06

30.64^{1.06} C 0.42

+80 - 1.70 B.

32.63

32.33³³ C 0.30

32.76

32.33⁷⁶ C 0.43

2 2+15

36.13

35.70^{6.13} C 0.43

37.06

35.70^{7.06} C 1.36

1 +50

39.64

39.07⁶⁴ C 0.57

39.57

39.07⁵⁷ C 0.50

+70

41.06

40.74⁰⁶ C 0.32

40.70

40.74 F 0.04

+90

42.31

41.90³¹ C 0.41

42.04

41.90^{2.04} C 0.14

3 +15

43.56

43.02⁵⁶ C 0.54

43.08

43.02⁰⁸ C 0.06

+40

45.40

44.15⁴⁰ C 1.25

0.75 B.

44.83

44.15⁸³ C 0.68

+60

45.53

44.88⁵³ C 0.65

0.75 B.

44.83

44.88⁸³ F 0.05

+80

46.67

45.28⁶⁷ C 1.39

1' B

44.87

45.28⁸⁷ F 0.41

4 +00

47.07

45.35⁰⁷ C 1.72

45.35

45.35 G

+20

46.21

45.11²¹ C 1.10

45.54

45.01⁵⁴ C 0.53

+40

47.91

44.59⁹¹ C 3.32

1.13 B.

46.38

44.34³⁸ C 2.04

+68.4 = N.L. Macauley

44.93

43.59⁹³ C 1.34

43.51

42.59⁵¹ C 0.92

Curb Stakes Byron St.
 Rosecrans To Scott.
 5 Wly

31

N. Fly

BC = MEET EXIST CR	18.30 ⁵	Meet		16.75 ⁵	Meet	
1	18.18			⊗ 16.91	16.88	C0.03
2	17.96			⊗ 17.00	16.90	C0.10
3	17.70			16.55	16.85	F0.30
4	17.45	17.40	C0.05	16.78	16.75	C0.03
5	17.08	17.08	Gr.	16.63	16.58	C0.05
EC = 0+19	16.61	16.76	F0.15	16.06	16.36	F0.30
+ 45.4	15.75	15.92	F0.17	15.52	15.53	F0.01
+ 71.8	14.55	15.09	F0.54	14.66	14.70	F0.04
+ 98.2	14.10	14.25	F0.15	13.96	13.86	C0.10
1 + 24.6	13.92	13.42	C0.50	13.36	13.03	C0.33
+ 51	12.97	12.58	C0.39	12.90	12.20	C0.70
+ 77.4	12.35	11.74	C0.61	11.86	11.37	C0.49
2 + 03.8	11.69	10.91	C0.78	10.77	10.54	C0.23
+ 30.2	10.46	10.07	C0.39	10.39	9.70	C0.69
+ 56.6	10.44	9.24	C1.20	9.77	8.87	C0.90
13C = 2+83.	8.94	8.40	C0.54	8.68	8.04	C0.64

Wly Cb. Ret. Byron & Scott

Nly. Cb. Ret. Byron & Scott

BC = 2+83

8.94 8 40 C 0.54

8.68 8 04 C 0.64

1 8.68 8 ¹⁵15 C 0.538.37 7 ³⁷86 C 0.51

2 8.02 7 95 C 0.07

7.73 7 70 C 0.03

3 7.83 7 90 F 0.07

6.89 7 ⁸⁹65 F 0.764 7.43 7 ³⁵85 F 0.42

7.09 7 60 F 0.51

5 7.53 7 80 F 0.27

7.05 7 55 F 0.50

EC = MEET EXIST CB.

7 ⁹¹88 Meet7.03 7 ³50 F 0.47

Stake Alley - Block 17 - Normal

Hts. - Plan - 3347 - D

33

W.O. 31231 - 8-23-56 7.0

RC. = Meest. 91.66 West

91.81 = PC Meest.
East

Top cb. ^{1.86} Bk. of cb. face	92.75	^{2.75} 92.16	C 0.59	Top cb.	92.61	92. ⁶¹ ₀₃	C 0.58
0+00 = NL. Collier Ave	92.75	^{2.75} 92.91	C 0.84	^{2.14} Bk. cb. face	92.61	91. ⁶¹ ₉₃	C 0.68
+20 - 1.86	94.17	^{4.17} 93.12	C 1.05	2.14	94.46	92. ⁴⁶ ₈₇	C 1.59
+40 1.86	94.71	^{4.71} 93.74	C 0.97	2.14	94.99	93. ⁴⁹ ₄₉	C 1.50
+60 1.86	94.53	^{4.53} 94.14	C 0.39	2.14	95.09	93. ⁰⁹ ₈₉	C 1.20
+80 1.86	94.40	^{4.40} 94.31	C 0.09	2.14	94.98	94. ⁹⁸ ₀₆	C 0.92
1+10 - ^{0.71} 0.85 Bk.	95.81	^{5.81} 94.40	C 1.41	2.14	94.76	94. ⁷⁶ ₁₅	C 0.61
+40 - ^{0.46} 0.60 Bk.	95.90	^{5.90} 94.49	C 1.41	3' Bk 3.14	94.05	94. ⁰⁵ ₂₄	F 0.19
+70 - ^{0.86} Bk.	95.97	^{5.97} 94.88	C 1.39	3' Bk 3.14	94.58	94. ⁵⁸ ₃₃	C 0.25
2+00 - ^{0.86} Bk.	96.19	^{6.19} 94.67	C 1.52	1' Bk 1.14	94.78	94. ⁷⁸ ₄₂	C 0.36
+30 - ^{1.13} 1.27 Bk.	96.19	^{6.19} 94.76	C 1.43	2+50 = Pipe 2.14 235. +.13 out. - end of wall	94.76	94. ⁷⁶ ₅₁	C 0.25
+60 1.86	95.16	^{5.16} 94.85	C 0.31	0.37 0.23 Bk.	96.17	94. ¹⁷ ₆₀	C 1.57
+80 1.86	95.39	^{5.39} 94.88	C 0.51	0.37 0.23 Bk.	95.49	94. ⁴⁹ ₆₃	C 0.86
3+00 - ^{1.61} 1.76 B.	96.16	^{6.16} 94.85	C 1.31	Pipe = 36 out Cor. RE 9102 0.42 B. 0.57	95.35	94. ³⁵ ₆₀	C 0.75
+35 1.85	94.59	94.75	F 0.16	0.67 B. 0.82	95.23	94. ²³ ₅₀	C 0.73
+70 1.85	94.63	^{4.63} 94.64	F 0.01	0.85 0.70 B.	95.04	94. ⁰⁴ ₃₉	C 0.65
4+05 1.85	94.80	^{4.80} 94.54	C 0.26	2.15	95.08	94. ⁰⁸ ₂₉	C 0.79
+40 1.85	94.77	^{4.77} 94.43	C 0.34	0.10 0.25 in	96.10	94. ¹⁰ ₁₈	C 1.92
+75 1.85	95.08	^{5.08} 94.33	C 0.75	2.15	94.75	94. ⁷⁵ ₀₈	C 0.67

			W.		E.			
5+00	21.85	94.75	^{4.75} 94.25	C 0.50	2.15	94.50	^{4.50} 94.00	C 0.50
+20.62	1.85	94.86	^{4.86} 94.19	C 0.67	^{1.65} 1/5 Bk.	94.85	^{4.85} 93.94	C 0.91
+40.62	1.85	94.89	^{4.89} 94.11	C 0.78	+ Bk. 1.15	94.79	^{4.79} 93.86	C 0.93
+60.62	2 Bk. 2.85	95.26	^{5.26} 93.98	C 1.28	3 Bk. 3.65	94.86	^{4.86} 93.73	C 1.13
+80.62	1.85	94.93	^{4.93} 93.81	C 1.12	2.15	94.59	^{4.59} 93.56	C 1.03
6+00.62 = S.L. Copley			^{3.09} 92.97	C 0.12			^{93.25} 92.96	C 0.29
Top cb			93.09				93.25 = Top cb.	

Rough Grades - 52nd Trojan to El Cajon.
 Plan - 3149 - D 8-27-56 7.0.

265.01 - sty. cd. in walk. 35
 348.43 = Top of Porch - □
 327.53 = Pole - SW. Trojan
 325.34 = □ on Water Vault - NE. Cor.

25' Lt. = Prop.	W.	Dist. Rt. to Prop.	E.
0+00 = NL Trojan	29.2 28.1 9.2 C 1.1	29.27	26.9 27.25 F 0.9
0+23	34.0 31.0 34.0 C 3.0	28.97	29.5 30.6 F 1.1
+63	37.8 37.8 36.8 C 1.0	28.47	34.7 36.4 F 1.7
+93	42.9 41.1 42.9 C 1.8	28.09	39.4 40.7 F 1.3
1+33	51.3 46.6 51.3 C 4.7	27.58	44.4 46.2 F 1.8
+73	56.5 51.0 56.5 C 5.5	27.07	53.3 50.6 C 2.7
2+13	66.8 54.5 66.8 C 12.3	26.57	54.6 54.1 C 0.5
+53	70.5 57.1 70.5 C 13.4	26.07	55.5 56.7 F 1.2
+584 = +93	67.3 58.9 67.3 C 8.4	26	63.6 58.5 C 5.1
3+33	67.1 59.8 67.1 C 7.3	26	64.1 59.4 C 4.7
+73	68.1 60.2 68.1 C 7.9	26	62.0 59.8 C 2.2
4+13	64.4 60.7 64.4 C 3.7	26	60.8 60.3 C 0.5
+53	62.0 61.1 62.0 C 0.9		64.4 60.7 C 3.7
+93	62.6 61.5 62.6 C 1.1		61.8 61.2 C 0.6
5+33	62.7 62.3 62.7 C 0.4		61.7 61.9 F 0.2
+73	64.5 63.6 64.5 C 0.9		63.4 63.2 C 0.2
6+13	68.7 65.5 68.7 C 3.2		67.3 65.1 C 2.2
+53	70.6 68.0 70.6 C 2.6		70.2 67.6 C 2.6

			W				F.
7+13		73.0	^{3.0} 72.1	C 0.9		71.7	71.6 C 0.1
+53		73.4	^{3.4} 73.2	C 0.2		73.0	73.2 F 0.2
+73.6 = SL. El Cajon		73.9	^{3.9} 73.6	C 0.3	7+75.93 = PC on SL.	73.7	73.8 F 0.1
7+76.10 = PC on W.							

Water + Sewer Lat.

	E		W.				E.
0+66	4+26.2	⑥	60.33	^{60.33} 55.35	C 4.98	⑬ - 0+66	36.93 ^{6.93} 32.31 C 4.62
+76						⑭ +76	38.4 38.3 C 0.1
4+45 = ⑭ W			67.35	67.5	F 0.15	⑫ 1+26	46.54 ^{6.54} 41.04 C 5.50
1+4.2	6+81.2 = ①		70.97	^{70.97} 64.61	C 6.36	⑮ 1+41.2	47.8 47.1 C 0.7
1+7.2						⑯ 1+76.2	51.95 ^{51.95} 47.97 C 3.98
1+9.2						⑰ 1+91.2	52.9 52.3 C 0.6
2+15 = ⑩ -2' in			55.12	5.12	50.23	C 4.89	
2+26.2						⑩	55.50 ^{5.50} 50.34 C 5.16
2+40	⑮	cb Gr.	56.4	56.0	C 0.4		
2+41.2						⑰	55.9 56.0 F 0.1
2+76.2						⑨	58.12 ^{8.12} 52.85 C 5.27
+91.2						⑱	58.4 58.4 G
3+26.2						⑧	59.38 ^{9.38} 54.30 C 5.08
3+41.2						⑲	59.46 ^{9.46} 59.5 G
3+76.2						⑲	59.85 ^{9.85} 54.90 C 4.95

Curb stakes - 33rd + Date

Plan - 3175 - D - 8-31-56

7.0.

37

West.

East.

15' Rad - Ret. at Date

Meet

33.92

33.95

1/2

34.03

34.10₀₉

F 0.07

33.55

33.75₅₅

F 0.20

P.C. = 0-10

33.35

34.15₃₅

F 0.80

32.90

33.38₂₉₀

F 0.48

0+00 = N.L. Date

33.07

34.00₀₇

F 0.93

33.07

33.06

C 0.07

+25

33.16

33.28₁₆

F 0.12

32.43

32.28₄₃

C 0.15

+50

32.48

32.56₄₈

F 0.08

31.53

31.56₅₃

F 0.03

+70

31.47

31.76₄₇

F 0.29

30.98

30.76₉₈

C 0.22

+90

30.37

30.53₃₇

F 0.16

29.56

29.53₅₆

C 0.03

1+10 + 11 on W.

28.62

28.76₆₂

F 0.14

28.04

27.86₀₄

C 0.18

+30 - T.P.

26.75

26.76

F 0.01

26.03

25.76₀₃

C 0.27

+45.71 = P.C.

25.13

24.94₅₁₃

C 0.19

24.27

23.94₂₇

C 0.33

P.R.C.

23.56

23.15₅₆

C 0.41

22.69

22.15₆₉

C 0.54

90° To ϕ

21.42

21.40

C 0.02

19.85

20.40₈₅

F 0.55

End of walk

19.69

20.32₆₉

F 0.63

18.65

19.75₆₅

F 1.10

1/2

20.04

19.78₀₄

C 0.26

19.51

19.52

F 0.01

Inlet.

19.45

19.50

19.50

B.M. = Cross ϕ Inlet = 2+10 on ϕ

219.45

Stake Drain + Inlets at 68th

+ Akins

38

Wly. cross on MH

250.18

ϕ of E. - "K" Type curb Inlet.

5' Bk. of cb. face on Rad. Line

53.47 3 21 C 2.17

Top of cb.

53.21 51.30 C 1.91

I.E. of Pipe

53.21 44.00 C 9.21

W. Inlet - Type "K"

Moved 7' N.

51.93 = Top S.

10' Bk. of cb. - N. end - cross

50.77 51.88 F 1.11

= Top of cb.

51.09 = Conc. 51.10

10' " " " S. end = PC.

50.56 51.62 F 1.06

= " " "

52.16 = Top - N.

I.E. of Box + Pipe

50.56 43.00 C 7.56

51.29 = Conc. 51.33

P.C. = 0+00.67

0+31

49.16 41.50 C 7.66

0+62 = 10' Rt. end Pipe

34.56 40.00 F 5.44

= I.E. of End.

0+79.5 = S. end apron

46.64 45.00 C 1.64

= Top of Slope

+84.5 = on E
Prod.

47.58 45.00 C 2.58

" " "

Stake Wall at Cemetery - Plan-12906-L
 W.O. 21462 - 9-22-56 7.0

35.48 = S.W. B.P. San Diego + Arista 39
 43.32 = spike in Pole

SE Wall.

0+00 = S. Cor.	34.90	39.10	F 4.20
+30	36.53	40.71	F 4.18
+60	38.00	42.32	4.32
+90	39.64	43.93	4.29
1+21 = Cor.	41.64	45.60	F 3.96

N.E. Wall

0+00 = Sly. Cor.	43.11	45.60	F 2.49
+31.2 Gate	43.04	45.60	2.56
+36.2	43.05	45.60	2.55
+66.2	42.95	45.60	2.65
+94 = Cor. - PK. 2' int. = Ang.	42.28	45.60	3.32

N.W. Wall = Cor.

0+00 = N.W. Cor.	34.88	39.10	F 4.22
+35	36.79	41.35	4.56
+72	39.98	43.73	3.75
1+01.1 = Ang. Cor.	42.06	45.60	3.54

S.W. Wall.

0+00 = S.W. Cor.	34.86	39.10	F 4.24
+10.7	34.84	39.10	4.26
+15.7 } Gate	34.68	39.10	4.42
+45.7	34.70	39.10	4.40
+75.7	34.70	39.10	F 4.40
1+01.7 = Cor.	34.20	39.10	4.90

Stake curbs at Coast Blvd. + Ocean St. - Plan-3869-D

40

w.o. 21489 - 9-24-56 7.0.

0+00 = End Exist. cb.		36.08 = Top
P.R.C.	36.56	⁵⁶ 36.13 C0.43
E.C. = 0+18.5	36.64	⁶⁴ 36.19 C0.45
+40	36.72	⁷² 36.33 C0.39
+62.5	35.26	⁵²⁶ 36.47 F1.21
+85	36.38	³⁸ 36.60 F0.22
1+05	37.41	⁷⁴¹ 36.68 C0.73
+25	37.22	⁷²² 36.64 C0.58
+45	36.84	⁸⁴ 36.58 C0.26
+65	36.59	⁵⁹ 36.48 C0.11
+85	36.64	⁶⁴ 36.39 C0.25
2+05	36.36	³⁶ 36.29 C0.07
+25	36.08	⁰⁸ 36.20 F0.12
+45	35.82	⁸² 36.10 F0.28
+61 = P.C.	35.79	⁷⁹ 36.02 F0.23
P.R.C.	35.98	35.98 Gr.
Meet. = 2+79.7		⁹⁸ 35.93 = Top cb. sly. opening

Stake Storm Drain - 54th + Univ. - 7.0
 Plan - 12968 - W.O. 21261 - 10-16-56

B.M. = Cross on Pipe 300.28
 35' RP. = B.M. 282.90

		10' Rt.	
0+00 = Beg. Pipe	.7702	77.02 76.00	1.02
+35	85.61	85.61 76.86	8.75
+70	83.95	83.95 77.72	6.23
1+05	85.09	85.09 78.58	6.51
+40	88.78	88.78 79.44	9.34
+75 = TP	87.69	87.69 80.30	7.39
2+10	87.86	87.86 81.16	6.70
Type G Cleanout +45.69 = Box	90.25	90.25 82.00	8.25
+47.19 = Ang Pt. - No Stake		90.25 86.00	4.25 = To Top
+80	86.52	86.52 84.41	2.11
3+15	88.32	88.32 86.98	1.34
+50	90.77	90.77 89.55	1.22
+85	98.66	98.66 92.12	6.54
4+20	97.41	97.41 94.69	2.72
+58.10 = BC = 11' Rt.	03.40	03.40 97.50	5.90
+64.63 = 1/2 = 11' Rt.	03.76	03.76 97.78	5.98
+71.16 = Conn = E.C.		98.06	

Stake Sewers - Ardatth Rd. - La Jolla
w.o. 31841 9-20-56

- Plan - 3034-D

42

8' = 10' from M.H. Conn. to Exist.		stakes 10' rt.					
	53.07	53.07 45.00	8.07	11+40	75.09	75.09 68.63	6.46
M.H. 42 = 5+01.01	53.70	53.70 45.25	8.45	+75	76.56	6 ⁵⁶ 70.35	6.21
5+35	54.41	54.41 46.18	8.23	12+10	78.12	8.12 72.07	6.05
+70	54.97	54.97 47.14	7.83	+45	79.81	9.81 73.79	6.02
6+05	55.75	55.75 48.10	7.65	+80	81.62	81.62 75.51	6.11
+40	56.58	56.58 49.06	7.52	13+15	83.85	3.85 77.23	6.62
+75	56.96	6.96 50.02	6.94	+50	85.89	5.89 78.95	6.94
7+10	57.77	7.77 50.98	6.79	+85	87.57	7.57 80.67	6.90
+45	58.90	8.90 51.94	6.96	14+20	89.94	9.94 82.39	7.55
+80	59.92	9.92 52.90	7.02	+55	91.86	1.86 84.11	7.75
8+15	60.80	60.80 53.86	6.94	+94.75 = Back +93.75 = M.H. 45 ahead.	96.02	6.02 86.05	9.97
+56.47 = M.H. 43	64.74	64.74 54.99	9.75	15+30	96.98	6.98 88.37	8.61
+90	64.85	64.85 56.59	8.26	+65	99.35	9.35 90.62	8.73
9+25	66.4	66.11 58.26	7.85	16+00	102.75	2.75 92.87	9.88
+60	67.44	67.44 59.92	7.52	+35	04.33	4.33 95.12	9.21
+95	68.97	8.97 61.58	7.39	+70	05.64	5.64 97.37	8.27
10+30	70.36	6.36 63.25	7.11	17+12.25 = M.H. 46	07.27	7.27 99.99	7.28
+65	71.84	71.84 64.93	6.91	+50	10.58	10.58 101.21	9.37
11+08.42 = M.H. 44 Back	73.76	73.76 66.99	6.77	+85	11.53	11.53 02.34	9.19
+06.45 ahead.							

18+20	12.06	^{12.06} 03.47	8.59
+55	13.75	^{13.75} 04.60	9.15
+90	15.75	⁵⁷⁵ 05.73	10.02
19+29.50 = MH 47	17.34	^{17.34} 06.99	10.35
+60	18.85	⁸⁸⁵ 08.30	10.55
+95	20.24	^{20.24} 09.80	10.44
20+30	21.68	^{1.68} 11.31	10.37
+65	24.24	^{4.24} 12.81	11.43
21+00	27.90	^{7.90} 14.32	13.58
+35	28.67	⁷⁸⁶⁷ 15.83	12.84
+65 = Anq. Pt.	28.33	^{8.33} 17.12	11.21
22+00	28.86	^{8.86} 18.62	10.24
+35	30.27	^{30.27} 20.13	10.14
+69.27 = MH 48	32.23	^{32.23} 21.60	10.63
23+00	33.25	^{3.25} 22.70	10.55
+35	35.27	^{35.27} 23.96	11.31
+70	36.41	^{36.41} 25.22	11.19
+97.54 = Plug.	37.08	^{37.08} 26.22	10.86

Stub at MH 44		Stakes 10' Pt.
0+00 = \pm MH 44		66.99
+40	73.80	^{73.80} 67.51
+80 = Plug.	74.90	^{74.90} 68.03
		6.29
		6.87
Stub at MH 45		" "
0+00 = \pm MH 45		86.05
+40	93.10	^{93.10} 86.33
+80 = Plug.	93.73	^{93.73} 86.61
		6.77
		7.12

Stub at MH 47 - stakes 5' Lt.

0+00 = \pm MH 47		106.99
+35	18.79	^{8.79} 08.93
+70	20.10	^{20.10} 10.87
+05	21.74	^{21.74} 12.81
+40	23.75	^{23.75} 14.75
+82 = Plug.	25.82	^{25.82} 17.07
		8.93
		9.00
		8.75

180.34 = Pole 44

180.00 = 20' RP = PK.

Stub at M.H. 48

Stakes 10' Lt.

0+00 = E.M.H. 48

121.60

3+05

44.27

44.27

36.58

7.69

+35

33.63

^{33.63}
23.73

9.90

+33.97 = M.H. 49

54.00

^{54.00}
42.00

12.00

+70

35.50

^{5.30}
25.86

9.64

+65

51.26

^{51.26}
42.84

8.42

1+05

37.37

^{7.37}
27.99

9.38

+95

51.55

^{51.55}
43.65

7.90

+40

38.98

^{8.98}
30.12

8.86

4+25

52.98

^{52.98}
44.46

8.52

+65

40.10

^{40.10}
31.64

8.46

+55

53.29

^{53.29}
45.27

8.02

+89.32 = Plug. 5' Lt.

41.02

^{41.02}
32.11

7.91

+83.73 = M.H. 50

53.60

^{53.60}
46.04

7.56

Beg. Line up Hill at M.H. 46 - stakes 10' Rt.

5+15

56.21

^{56.21}
49.30

6.91

0+00 = E.M.H. 46

07.27

99.99

+45

59.59

^{59.59}
52.43

7.16

+30

07.33

^{7.33}
101.84

c 5.49

+75

64.82

^{64.82}
55.56

9.26

+60

07.84

^{7.84}
03.69

4.15

6+05

69.56

^{69.56}
58.70

10.86

+90

09.58

^{9.58}
05.54

4.04

+37.50

72.26

^{72.26}
62.10

10.16

1+20

12.71

^{12.71}
07.39

5.32

+50

73.11

^{73.11}
63.18

9.93

+50

15.95

^{15.95}
09.23

6.72

+62.5

73.22

^{73.22}
63.82

9.40

+62.5

17.44

^{7.44}
10.39

7.05

+95

73.99

^{73.99}
64.93

9.06

+75

19.07

^{9.07}
12.33

6.74

7+25

77.92

^{77.92}
65.95

11.97

2+10

24.24

^{24.24}
18.86

5.38

+55

80.65

^{80.65}
66.97

13.68

+45

29.93

^{9.93}
25.39

4.54

+85 = M.H. 51

67.99

+80

35.40

^{5.40}
31.92

3.48

Exist. M.H.	= Cross							
0+00 = Conn. to		92.93	92.93 89.45	3.48	6+15 - 7' Lt	43.14	43.14 33.22	9.92
+35		92.86	92.86 89.80	3.06	+50 - 8' Rt.	48.60	48.60 37.52	11.08
+70		92.09	2.09 90.15	1.94	+86.58 = M.H. C	49.35	49.35 42.03	7.32
1+05		92.76	3.76 90.29	3.47	7+20 - 5' Rt	52.87	52.87 45.93	6.94
+40		94.25	4.25 90.43	3.82	+55 - 5' Rt	56.73	56.73 50.03	6.70
+57 = B.C.		93.58	90.50	3.08	+90 - 5' Lt	62.40	62.40 54.13	8.27
+75 = E.C.		93.67	90.57	3.10	8+25 - 5' Lt.	65.40	65.40 58.23	7.17
2+00		94.40	4.40 90.67	3.73	+49.25 = M.H. 7	65.76	65.76 61.06	4.70
+26.04 = M.H. 3-A	5' Lt.	96.23	6.23 90.77	5.46	+85 - 5' Rt.	70.54	70.54 65.60	4.94
+12.98 ahead.		98.04	8.04 92.60	5.44	9+20 - 5' Rt.	77.65	77.65 70.05	7.60
+45 - 5' Lt.		98.04	92.60	5.44	+55 - 5' Rt.	81.06	81.06 74.50	6.56
+80 - 5' Lt.		100.12	0.12 94.60	5.52	+90 - 3.8' Lt.	83.80	83.80 78.94	4.86
3+10.04 = M.H. 4	8' Lt = P.K.	06.65	06.65 96.32	10.33	10+25 - 4' Lt.	88.76	88.76 83.38	5.38
+45 - 8' Lt.		10.20	10.20 100.52	9.68	+44.8 = end Pipe		85.90	
+80 - 5' Lt.		14.09	14.09 04.72	9.37	10+60 - 4' Lt.	93.26	93.26 87.82	5.44
4+15 - 5' Lt.		18.33	18.33 08.92	9.41	10+95 - 4.66 Lt	97.85	97.85 92.27	5.58
+50 - 5' Lt.		22.89	22.89 13.12	9.77	11+06.6 = Ang.	04.34	04.34 93.53	10.81
+85 - 6' Rt.		28.43	28.43 17.31	11.12	+27.7 5' Lt.	04.67	04.67 95.54	9.13
5+08.25 = M.H. 5	-10 Rt.	36.93	36.93 20.10	16.83	+48.3 = M.H. 8	05.50	05.50 97.50	8.00
+45 - 10' Lt.		35.59	35.59 24.62	10.97				
+80 - 8' Lt.		42.30	42.30 28.92	13.38				

Beq. Line Thru yard - from M.H. 7

25' RP = 17206

=PK 183.29 = on Road.

0+00 = M.H. 7	161.06		
+25 - 5' Lt.	69.32	65.00	C 4.32
+43.36 = Ang. - 5' Lt.	74.49	69.41	C 5.08
+62.5 - 4' Rt.	79.55	74.00	C 5.55
+70.02 = Ang. 3' Rt.	81.05	75.38	C 5.67
+75 - 5' Rt.	82.22	76.30	C 5.92
+87.5 - 2.5' Rt. = Cross	85.16	77.22	C 7.94
1+10 - 5' Lt.	84.04	77.62	6.42
+31.34 = M.H. 17 5' Lt. on Line	83.77	77.99	5.78
+70 - 5' Lt.	86.52	80.70	5.82
2+05	88.29	83.15	5.14
+40	90.38	85.61	4.77
+75	92.94	88.06	4.88
3+10	96.09	90.52	5.57
+45.18 = M.H. 18 - 5' Rt.	99.83	93.00	6.83
+80 - 5' Rt.	01.47	94.22	7.25
4+15	04.06	95.44	8.62
+50	04.55	96.67	7.88
+88	05.57	97.90	7.67

199.85 = Rock = Cor. of wall
210.00 = Pole by M.H. 19

46

5+20 - 4' Rt.	09.60	99.12	6.48
+55 5' Rt.	06.89	200.34	6.55
+90	08.23	01.57	6.66
6+13.86 = M.H. 19 14.24 6+12	08.98	02.40	6.58
+50	09.83	03.67	6.16
+85	11.24	04.89	6.35
7+16 = Plug.	12.37	05.97	6.40
0+00 = M.H. 19			
+40 - 5' Lt.	12.38	08.36	4.02
+78 = Rvk. - 7' Lt.	19.73	14.02	5.71
1+13	27.34	24.17	3.17
+47.03 = M.H. 20 30 6+12	39.07	34.04	5.03
0+00 +40	41.24	39.64	1.60
+78.80 = Plug.	47.57	45.07	2.50

Beq. Hidden Valley Road.

	stakes	5' Lt = PK.				
			6+50	96.70	16.70 89.00	7.70
0+05 = M.H. 43	54.99		+85	99.94	9.94 91.93	8.01
+40	64.59	64.59 55.29	9.30	7+21.97 = M.H. 58	03.23 95.02	8.21
+75	64.91	64.91 55.59	9.32	+55	06.06 97.73	8.33
1+10	65.45	65.45 55.89	9.56	+90 -10' rt.	09.04 100.60	8.44
+45	65.60	65.60 56.19	9.41	8+25 70 rt.	12.14 12.14 03.47	8.67
+80	66.16	66.16 56.49	9.67	+60	15.29 06.34	8.95
2+03.93 = M.H. 53	66.43	66.43 56.68	9.75	+93.12 = M.H. 59	17.75 09.08	8.70
+35	66.88	66.88 56.96	9.92	9+05.38 ahead.	19.54 11.11	8.43
+70	67.53	67.53 57.27	10.26	+25	19.54 22.34 14.77	7.57
3+05	68.35	68.35 57.58	10.77	+60	22.34 25.69 18.45	7.24
+29.12 = M.H. 56	69.12	69.12 57.80	11.32	+95	25.69 29.42 9.42 22.12	7.30
+65	70.89	70.89 61.54	9.35	10+30	29.42 33.29 33.29 25.78	7.51
4+00	73.68	73.68 65.19	8.49	+65	33.29 37.13 37.13 29.46	7.67
+35	76.80	76.80 68.84	7.96	11+00	37.13 40.70 40.70 33.12	7.58
+70	80.36	80.36 72.49	7.87	+35	40.70 44.20 44.20 36.80	7.40
5+05	83.69	83.69 76.14	7.55	+70	44.20 47.61 47.61 40.46	7.15
+42.33 = M.H. 57	86.96	86.96 80.02	6.94	12+05	47.61 50.85 50.85 44.07	6.78
+80	90.10	90.10 83.16	6.94	+39.51 = M.H. 60	50.85 54.58 54.58 47.48	7.10
6+15	93.33	93.33 86.08	7.25	+75	54.58 58.05 58.05 50.84	7.21
				13+10	58.05	

13+45	61.53	^{61.53} 54.20	7.33	M.H. 54' = 0+00		75.38	
+75.51 = Plug	64.52	^{64.52} 57.13	7.39	+30	89.20	9.20 80.86	8.34
				+60	94.08	94.08 86.34	7.74
				+90	98.60	8.60 91.82	6.78
Req. Line at M.H. 53				1+20	104.84	04.84 97.30	7.54
0+00 = M.H. 53		56.68		+49.50	13.14	13.14 102.69	10.45
+35	67.37	^{67.37} 58.58	8.79	+62	14.75	14.75 04.80	9.95
+70	69.03	^{69.03} 60.48	8.55	+74.5	15.40	15.40 06.57	8.83
1+05	70.84	^{70.84} 62.38	8.46	2+00	18.07	18.07 09.83	8.24
+40	72.40	^{72.40} 64.28	8.12	+30	24.52	24.52 13.67	10.85
+75	73.80	^{73.80} 66.18	7.62	+60	24.91	24.91 17.51	7.40
2+10	75.15	^{75.15} 68.08	7.07	+94.80 = M.H. 55	33.05	33.05 21.97	11.08
+45	76.95	^{76.95} 69.99	6.96	3+25	35.84	35.84 26.59	9.25
+80	79.32	^{79.32} 71.90	7.42	+55	38.11	8.11 31.19	6.92
3+15	82.42	^{82.42} 73.81	8.61	+80 = Plug	42.84	42.84 35.00	7.84
+43.79 = M.H. 54	84.67	^{84.67} 75.38	9.29				
+70	88.02	^{88.02} 79.92	8.09				
4+00	94.28	^{94.28} 85.12	9.16				
+28.3 = Plug	100.91	^{100.91} 90.00	10.91				

Req. Line to School from MH .56 - Hidden Valley Rd.

MH 56 = 0+00	5' Lt.	57.80					
+35		65.76	57.80	7.71	2+75.25 = MH .64	90.95	75.01 15.94
+70		64.12	65.76	5.83	3+05	92.64	78.58 14.06
1+05		62.71	64.12	4.17	+40	95.14	82.78 12.36
=45.25	-8' Lt.		62.71		+75	97.58	86.98 10.60
+46 = MH .61		62.67	62.67	3.85	4+01.95 = Plug.	99.28	90.21 9.07
+35		64.37	62.67	5.20			
7+70		67.89	64.37	8.37	Req. at MH .64 = Line to Rt		
1+08.19 MH .62	5' Lt. online	69.87	67.89	9.97	0+00 = MH .64	90.95	75.80 15.15
+35	= 0+00	71.47	69.87	11.57	+30	88.81	76.17 12.64
+60		67.03	71.47	6.83	+60	86.83	76.54 10.29
+95		64.86	67.03	4.36	+90	85.59	76.90 8.69
1+20		67.14	64.86	6.04	1+20	85.21	77.27 7.94
1+53.8 = MH .63	5' Lt. both ways	68.01	67.14	6.60	+47.68 = MH .65	85.92	77.60 8.32
0+35 - 4.8' Rt.		70.24	68.01	7.10	+75	87.44	78.26 9.18
+70 - 5' "		71.48	70.24	6.61	2+10	89.91	79.10 10.81
1+05		72.69	71.48	6.09	+45	92.38	79.94 12.44
+40 - Nail		75.97	72.69	7.64	+80	94.00	80.78 13.22
+75		76.03	75.97	5.97	3+15	95.51	81.62 13.89
2+10		77.74	76.03	5.95	+50	97.14	82.46 14.68
+45		81.99	77.74	8.47	+85	98.63	83.30 15.33

Beq. Hidden Valley Rd - MH. 51 50
See P. 44

5' Rt.

4+20	99.54	99.54 84.14	15.40	7+85 = M.H. 51	82.00	82.00 67.99	14.01
+55	00.23	00.23 84.98	15.25	8+25	83.01	83.01 68.39	14.62
+90	00.88	00.88 85.82	15.06	+65	84.28	84.28 68.79	15.49
-2 cuts -10'	00.33		14.02			86.11	
5+10.62 = M.H. 66 5' on line	00.77	00.77 86.31	14.46	9+05	86.11	86.11 69.19	16.92
+45	03.66	03.66 93.53	10.13	+45 = M.H. 52	88.01	88.01 69.59	18.42
+80 = Plug.	06.67	06.67 100.88	5.79	+85	90.39	90.39 75.11	15.28
6+00 = M.H. 66 5' on	00.77	00.77 87.00	13.77	10+25	92.58	92.58 80.63	11.95
+30	99.91	99.91 87.12	12.79	+65	94.97	94.97 86.15	8.82
+60	97.64	97.64 87.24	10.40	+95 = Plug.	96.74	96.74 90.29	6.45
+90	96.11	96.11 87.36	8.75				
1+20	94.53	94.53 87.48	7.05				
+52.12 = Plug.	93.80	93.80 87.61	6.19				

Beq. Line in Roseland - Conn. to Exist.

0+00 = Conn.	77.99	⁷⁹⁹ 71.10	6.89	6+10	32.68	^{32.68} 23.71	8.97
				+45	33.80	^{33.80} 27.04	6.76
0+45.02 = M.H. 32	78.79	⁸⁷⁹ 71.55	7.24	+70	35.63	^{35.62} 29.42	6.21
+75 = Brk.	79.58	^{79.58} 71.85	7.71	+97.45 = M.H. 36	36.70	^{6.70} 32.04	4.66
1+10	81.03	^{81.03} 73.42	7.61	= 0+00		^{43.75} 34.94	8.81
+45	82.90	^{82.90} 75.00	7.90	+35	43.75	^{47.31} 37.84	9.47
+73.82 = M.H. 33	84.72	^{84.72} 76.31	8.41	+70	47.31	^{9.19} 41.06	C 8.13
2+05	85.16	^{85.16} 78.10	7.06	1+08.70 = Plug	49.19		
+35	87.00	^{87.00} 79.81	7.19				
+65	89.14	^{9.14} 81.52	7.62				
+95	91.39	^{11.39} 83.23	8.16				
3+26.15 = M.H. 34	92.80	^{2.80} 85.00	7.80				
+65	97.64	^{7.64} 91.21	6.43				
4+00	03.54	^{03.54} 96.81	6.73				
+35	09.18	^{09.18} 02.41	6.77				
+70	14.56	^{14.56} 08.01	6.55				
5+07.08 = M.H. 35	19.87	^{9.87} 13.95	5.92				
+40	24.49	^{24.49} 17.07	7.42				
+75	28.78	^{8.78} 20.39	8.39				

Beq. at M.H. 8 - in Soledad.

5' Lt.

= M.H. 8		97.50		1+69	37.96	7.96 30.70	7.26
43.05				2+04	36.97	6.97 31.40	5.57
ahead.	-6.5 on line	09.30	09.30	+33.27 = M.H. 13	38.17	8.17 31.99	6.18
11+95.92 M.H. 9		97.95	11.35			42.27 37.29	4.98
12+30		04.66	4.73	+70	42.27	7.11 42.35	4.76
+65		06.38	4.42	3+05	47.11	58.59 47.41	11.18
13+00		09.90	5.89	+40	58.59	62.78 52.50	10.28
+35		13.65	7.60	+75.21 = M.H. 14	62.78	61.91 56.05	5.86
+59.66 = M.H. 10	7+11	13.88	6.39	= 0+00	0+21.15 = Ang.	66.89 60.90	5.99
27.5 Rt. = Plug		14.13	4.99	+50	66.89	72.83 66.78	6.05
+95		16.45	6.91	+85	76.37	78.77 73.44	5.33
14+28.96 = M.H. 11		18.48	6.97	1+09	83.43	85.19 87.34	7.95
+65		17.54	5.67	+21.15			
15+00		15.25	3.03	+43.15			
+33.17 = Plug.		20.66	8.11	+67.5			
0+00 = M.H. 11		11.51		Line to W. from M.H. 14			
+35		22.84	6.50	0+00 = M.H. 14			
+70		25.57	4.70	+35	60.89	60.89 52.74	8.15
1+05		32.06	6.06	+70	58.86	8.86 52.99	5.87
+34 = M.H. 12 = Bk.		37.53	7.53	1+00 = Plug.	56.95	6.95 53.20	3.75
ahead.		37.57	7.57	Line to E. from M.H. 14			
				0+00 = M.H. 14			

Beq. at MH 21 - Roseland
To Poison Pak!

53

0+30	64.59	64.59 54.39	10.20				
+60	66.83	66.83 56.28	10.55	0+01 = MH.21	70.47	70.47 62.60	7.87
+90	68.72	68.72 58.17	10.55	+35	73.02	73.02 65.70	7.32
1+20	70.12	70.12 60.06	10.06	+70	75.98	75.98 68.89	7.09
+50	71.28	71.28 61.95	9.33	1+00 = Ang.	79.10	79.10 71.62	7.48
+80	72.41	72.41 63.84	8.57	+30	80.95	80.95 74.36	6.59
2+10	72.61	72.61 65.73	6.88	+60	85.42	85.42 77.10	8.32
+32 = MH.15	73.58	73.58 67.12	6.46	+90	88.37	88.37 79.84	8.53
⁰⁺⁰⁰ +25	74.58	74.58 67.87	6.71	2+24.79 = MH.22	91.16	91.16 83.01	8.15
+50	75.19	75.19 68.62	6.57	+55	93.91	93.91 86.73	7.18
+75	75.57	75.57 69.37	6.20	+90	01.61	01.61 91.03	10.58
1+00	76.36	76.36 70.12	6.24	3+25	05.67	05.67 95.34	10.33
+25	77.02	77.02 70.87	6.15	+55.16 = MH.23	05.31	05.31 99.06	6.25
+45 = MH.16	77.75	77.75 71.47	6.28	+90	11.96	11.96 104.91	7.05
⁰⁺⁰⁰ +25	78.62	78.62 71.72	6.90	4+25	19.95	19.95 10.79	9.16
+50	79.50	79.50 71.97	7.53	+50.16 = MH.27	24.39	24.39 15.02	9.37
+75	80.30	80.30 72.22	8.08	+63.28	30.06	30.06 18.87	11.19
+92 = Plug.	81.11	81.11 72.39	8.72	76.40	30.63	30.63 22.72	7.91
				+89.53 = E.C.	33.17	33.17 26.57	6.60
				5+25.50	42.55	42.55 36.97	5.58

Stub. at M.H. 31

0+00 = M.H. 31

76.89

5+60	52.28	^{52.28} 47.23	5.05	+29.41	91.75	^{91.75} 78.94	12.81
+87.5	60.21	^{60.21} 55.33	4.88	^{12.50} 41.91	93.69	^{93.69} 80.54	13.15
6+00	63.57	^{63.57} 58.48	5.09	54.41	95.56	^{95.56} 83.57	11.99
+12.5 ¹⁴ M.H.	65.93	^{65.93} 60.25	5.68	84.41 = Plug.	200.08	^{200.08} 92.57	7.51
+42.5	71.20	^{71.20} 63.20	8.00				

^{71.22 = Bk.} 5' Rt.
6 + ~~70.08~~ = M.H. 28
ahead.

Beq. at M.H. 23

0+00 = M.H. 23

99.06

7+05	79.95	^{79.95} 67.76	12.19	+43	10.12	^{10.12} 106.51	3.61
+40	80.55	^{80.55} 69.51	11.04	+49.25	13.63	^{13.63} 07.79	5.84
+75.03 = M.H. 29	81.80	^{81.80} 71.26	10.54	+55.50	16.11	^{16.11} 09.47	6.64
8+10	78.85	^{78.85} 72.31	6.54	+61.75	17.78	^{17.78} 11.53	6.25
+45	79.84	^{79.84} 73.36	6.48	+68	20.60	^{20.60} 14.00	6.60
+69.91 = M.H. 30	85.13	^{85.13} 74.11	11.02	+87.79 = Ang.	27.80	^{27.80} 22.43	5.37
9+05	83.41	^{83.41} 74.81	8.60	+98.5	32.39	^{32.39} 27.01	5.38
+40	82.57	^{82.57} 75.51	7.06	1+05.5	35.00	^{35.00} 29.70	5.30
+75	84.10	^{84.10} 76.21	7.89	+12.5	37.31	^{37.31} 31.80	5.51
10 + 08.80 = M.H. 31	85.78	^{85.78} 76.89	8.89	+19.5	39.55	^{39.55} 33.31	6.24
³⁰ +38.80 - 4' Rt.	84.47	^{84.47} 77.49	6.98	+26.5	39.93	^{39.93} 34.24	5.69
⁷⁶ +64.80 = Plug.	89.80	^{89.80} 78.01	9.79	+41.40 = M.H. 24		35.93	

Stub. at M.H. 27

0+00 = M.H. 27

+30	31.84	31.84 23.17	8.67
+60	39.71	9.71 31.33	8.38
+90	48.47	48.47 39.49	8.98
1+25	53.93	53.93 49.00	4.93

Stub to E. from M.H. 25

0+00 = M.H. 25

+35	55.83	55.83 48.37	7.46
+65 = Plug.	58.33	58.33 51.60	6.73

Req. at M.H. 24 - Boulevard Place

0+00 = M.H. 24	39.49	9.49 38.93	3.56
+40	45.36	45.36 38.13	7.23
+80	49.99	9.99 40.33	9.66
1+20	53.03	53.03 42.53	10.50
+58.12 = M.H. 25	54.16	54.16 44.61	9.55
0+00	58.25	8.25 50.00	7.65
+30.23	61.76	61.76 54.00	7.76
+42.73	61.91	61.91 55.60	6.31
+67.65 67.73 = M.H. 26	66.59	66.59 57.00	9.59
0+00 To Lt.	63.05	63.05 57.50	5.55
0+25	63.40	63.40 58.00	5.40
0+50 = Plug.	68.33	68.33 57.25	11.08
To Rt. From M.H. 26 0+25	67.32	67.32 57.50	9.82
0+50 = Plug.			

Beq. at M.H. 38 - Torrey Road.

55.00 = Pole
by M.H. 38

56

= Exist. Sewer - 10' Rt.

0+00 = M.H. 38	52.66	52.66 45.56	7.10	+70	66.30	6.30 60.54	5.76
+35	53.91	53.91 47.01	6.90	1+03.24 = Plug.	69.36	9.36 62.65	6.71
+70	53.57	53.57 48.47	5.10	Beq. SideLine from M.H. 39			
1+05	55.47	55.47 49.92	5.55	0+00 = M.H. 39			
+40	59.29	9.29 51.37	7.92	0+35 - 5' Rt.	62.69	62.69 58.17	4.52
+76.71 = M.H. 37	63.44	63.44 52.91	10.53	+52.5 - 6' Rt.	63.70	63.70 59.60	4.10
2+10	65.90	65.90 53.58	12.32	+70 - 5' Rt.	65.66	5.66 61.95	3.71
+45	64.96	64.96 54.28	10.68	1+05 - 6' Rt.	70.44	70.44 66.85	3.59
+80	61.36	61.36 54.98	6.38	+35.34 - 5' Rt.	75.71	5.71 71.10	4.61
3+10 = Plug.	61.63	61.63 55.58	6.05				

Line in Road. From M.H. 38

0+00 = M.H. 38			
+35	54.85	54.85 47.92	6.93
+70	56.47	6.47 50.28	6.19
1+05	58.62	8.62 52.64	5.98
+40	60.76	60.76 55.00	5.76
+56.24? = M.H. 39	61.93	61.93 56.10	5.83
0+35	64.04	64.04 58.32	5.72

0 to 0 = Conn.	47.01	47.03	4.98	1 + 25.5	91.04	91.04	85.50	5.54
+35	48.16	43.03	5.13	+ 54 = Plug <small>28.5</small>	93.40	93.40	90.06	3.34
+70	49.20	44.03	5.17	Stub. from MH 3				
1 + 03.43 = MH 1	54.38	45.00	9.38	0 + 19.73 = Plug.	87.93	87.93	81.91	6.02
^{= 0 to 0} +35	60.0	61.02	9.87					
+70 <small>86 = 65.0 f = low 66.7</small>	66.7	67.44	10.14					
+96.80 = MH 2	71.26	72.04	10.04					
^{= 0 to 0} +30	68.6	68.98	6.32					
+60	68.0	69.08	5.75					
+90	69.4	69.85	5.85					
1 + 22.5	70.1	70.04	4.84					
+35	71.4	70.90	4.90					
+47.5	72.7	73.94	6.94					
+77.5	79.0	78.74	7.24					
<small>29.3</small> 2 + 06.80 = M.H. 3	86.64	75.99	10.65					
^{= 0 to 0} +35	85.04	76.85	8.19					
+65.5	85.12	77.60	7.52					
+78	86.30	78.33	7.97					
+90.5	87.32	79.90	7.12					

Stake Sewers - Muirlands - Plan

W.O. 32555 - 6-21-57

7.0.

3970-74-D

58

361.03 = 25' R.P.

$\frac{72.68}{222} = 74.90$

B.M. = D = 311.98				2 + 45	48.07	38.78	9.29	
0 + 00 = ± Ext. M.H.	12.28	3	^{12 28} 03.83	8.45	+ 80	51.40	^{51 40} 41.32	10.08
+ 35	13.18		^{3 18} 06.60	6.58	2 + 15	54.33	^{54 33} 43.85	10.48
+ 70	14.22		^{4 22} 09.37	4.85	+ 50 = M.H. 3	57.04	^{57 04} 46.38	10.66
1 + 09.50 = Ang.	17.34		^{7 34} 12.50	4.84	0 + 35	59.15	^{9 15} 51.63	7.52
+ 45	22.22		^{22 22} 15.31	6.91	+ 70	63.33	^{63 33} 56.88	6.45
+ 80	28.89		^{28 89} 18.08	10.81	1 + 05	69.64	^{9 64} 62.13	7.51
2 + 07.82 = M.H. 1	34.13		^{34 13} 20.28	13.85	+ 30 = M.H. 4	74.90	^{74 90} 65.88	9.02
0 + 35 - 10' Rt.	29.91		^{9 91} 20.42	9.49				
+ 70 10' Rt.	27.43		^{7 43} 20.56	6.87				
1 + 05 10' Rt.	24.24		^{4 24} 20.70	3.54				
+ 40 8' Rt.	23.67		^{3 67} 20.84	2.83				
+ 81 = M.H. 2 ^{7.5 Rt.}	27.15		^{7 15} 21.00	6.15				
0 + 35	30.69		^{0 69} 23.54	7.15				
+ 70	33.89		^{3 89} 26.08	7.81				
1 + 05	37.89		^{7 89} 28.62	9.27				
+ 40	40.43		^{0 43} 31.16	9.27				
+ 75	40.54		^{40 54} 33.70	6.84				
2 + 10	43.38		^{43 38} 36.24	7.14				

Line in El Camino Del Teatro
Wild Location

59

M.H. 5 0+00 = end Exist 8"	88.24	^{8 24} 82.76	5.48	2+80	42.76	^{2 76} 36.00	6.76
+35	90.91	^{0 91} 85.62	5.29	3+15	46.25	^{6 25} 38.75	7.50
+70	94.48	^{4 48} 88.48	6.00	+43.60 = M.H. 8	49.08	^{9 08} 41.00	8.08
1+05	97.43	^{7 43} 91.34	6.09	Correct. loc. 0+35	63.20	^{6 320} 49.95	13.25
+40 = M.H. 6	00.22	94.20	6.02	+70	66.04	^{6 04} 58.90	7.14
0+35	03.81	^{3 81} 97.17	6.64	^{7 +14} +97.64 = M.H. 9	70.68	^{7 0 68} 66.00	4.68
+70	06.80	^{6 80} 00.14	6.66	0+35	72.52	^{2 52} 67.31	5.21
1+05	09.52	^{9 52} 03.11	6.41	+70	74.64	^{4 64} 68.62	6.02
+40	12.44	^{2 44} 06.08	6.36	1+05	75.23	^{5 23} 69.93	5.30
+75	15.57	^{5 57} 09.05	6.52	+40	76.12	^{6 12} 71.24	4.88
2+10	18.49	^{8 49} 12.03	6.46	+75	76.38	^{6 38} 72.55	3.83
+33 = M.H. 7	19.93	^{9 93} 14.00	5.93	2+00 = M.H. 10	76.66	^{6 66} 73.50	3.16
0+35	22.42	^{2 42} 16.75	5.67	0+30	77.80	^{7 80} 73.95	3.85
+70	25.00	^{5 00} 19.50	5.50	+60	78.57	^{8 57} 74.40	4.17
1+05	27.68	^{7 68} 22.25	5.43	+90.32 = Plug.	78.99	^{8 99} 74.85	4.14
+40	30.65	^{0 65} 25.00	5.65				
+75	33.63	^{3 63} 27.75	5.88				
2+10	36.67	^{6 67} 30.50	6.17				
+45	39.58	^{9 58} 33.25	6.33				

M.H. - 10 - 13 + 17

Fly Cross

0+00 = Exist M.H. 10	91.96	91.96 85.65	6.31
+35	01.92	01.92 94.18	7.74
+70	10.93	10.93 02.71	8.22
1+04.42 = M.H. 13	21.80	21.80 11.10	10.70
0+30	26.11	6.11 14.61	11.50
+60	30.23	30.23 18.12	12.11
+90	32.48	32.48 21.63	10.85
1+20	36.83	36.83 25.14	11.69
+52.88 = M.H. 17	37.48	37.48 29.00 4.88 (432.60) (20yd)	8.48

Req. at M.H. 13 - To S.

0+00 = M.H. 13	21.80	21.80 11.50	10.30
+35 18.9	17.84	7.84 11.64	6.20
+70 16.9	16.77	6.77 11.78	4.99
1+05 15.2	13.57	3.57 11.90	1.67
+35 15.9	13.89	3.89 12.10	1.79
+65 16.6	15.08	5.08 12.80	2.28
+95 17.9	16.59	6.59 13.50	3.09
2+25 18.6	17.50	7.50 14.50	3.00

440.32 = Top Hyd. by M.H. 14

60

2+52 20.1	18.81	8.81 15.50	3.31
+77 21.4	19.66	9.66 17.70	1.96
3+02 = M.H. 14	21.08	22.4 18.20	2.88
0+35	25.27	5.27 20.52	4.75
+70	27.51	7.51 22.84	4.67
1+05	29.09	9.09 25.16	3.93
+40	31.85	1.85 27.48	4.37
+75	36.23	6.23 29.80	6.43
+96.24 = M.H. 15	39.11	9.11 31.20	7.91
0+35	43.27	3.27 35.38	7.89
+70	48.35	8.35 39.56	8.79
1+05 = T.P.	52.34	2.34 43.74	8.60
+40	56.23	6.23 47.92	8.31
+75	59.31	9.31 52.10	7.21
2+05 = M.H. 16	60.30	0.30 55.70	4.60
0+35	62.55	2.55 57.78	4.77
+70	63.30	3.30 59.86	3.44
1+00.94 = Plug.	64.86	4.86 61.70	3.16

MH 17 to 18 (Muir Lands & EL Paso Real)

DWGS 3973-D + 3974-D -

NOTE - Grade changes Per Boyd -

10' 5" Per Boyd -
Muir Lands - Moved
At Vista Verde Dr +

Elev of
Chisel X
Grade CUT

0+00 = MH#17

43.38.55 432.60 - 5.95

5 Part of 39.36

0+39.36

41.41 434.96 - 6.45

0+78.72

44.13 37.32 - C681

1+18.08

46.90 39.68 - C722

1+59.44

49.62 42.04 - C758

1+96.80 = BVC

52.43 44.40 - C803

10'

2+06.80

53.11 45.12 - C799

10'

2+16.80 = EVC

53.81 45.96 - C785

30

2 MH#18

2+46.80 =

55.96 449.20 - C676

Then Ely in EL Paso Real to MH# 24, 25 + To Plug 61
200' S.E. of MH#25 in EL Paso Real.
Stake 6' Wly of Pipe - 17 to 18'

From MH#18 Ely in EL Paso Real to MH# 24, 25 + Plug 61
IF (ON RR) CUT

0+00 = MH#18 -

449.70 455.73 6.03

0+40

457.20 455.12 3.92

0+80 = BVC

452.70 457.55 4.85

1+00

453.60 458.98 5.38

+20

454.90 460.16 5.26

+40 = EVC

456.60 461.46 4.86

1+70.13 = BC

459.14 463.67 4.53

1+95.18

461.15 465.56 4.41

2+20.24

463.16 467.67 4.51

2+45.30 = MH#24

465.17 469.71 4.54

2+85.30

468.42 472.99 4.57

3+26.15 = BC

471.74 476.63 4.89

3+54.61

474.05 479.23 5.18

3+83.07

476.36 481.89 5.53

4+11.53

478.67 484.30 5.63

4+40.00 MH# 25

481.00 486.15 5.15

4+80

482.10 487.99 5.89

5+20

483.20 488.97 5.77

5+60

484.30 489.90 5.60

6+00

485.40 490.84 5.44

6+40 = Plug

486.50 491.75 5.25

Station	IE Pipe	Stake	CUT	Station	IE Pipe	Stake	CUT
6+95 ⁸⁴	481.19	86.08	C4 ⁸⁹	10+79 ¹⁸	502.36	12.88	C105 ²
6+61 ¹⁶	479.13 ✓	84.09	C4 ⁹⁶	40 50' 33"			
6+26 ⁴⁸	477.07 ✓	82.35	C5 ²⁸	10+567 ²	501.84	C 9.06 510.90	C90 ⁶
= MH# 19 -				30' 13' 42"			
5+91 ⁸⁰	475.01	80.71	C5 ⁷⁰	10+342 ⁶	501.32	508.96	C-76 ⁴
5+63.80	472.98 ✓	749.20	C6 ²²	10 36' 51"			
5+35 ⁸⁰	470.94 ✓	77.27	C6 ³³	Chords = 22.48			
5+07 ⁸⁰	468.91 ✓	75.30	C6 ³⁹	L = 224.62			
4+79 ⁸⁰	466.87 ✓	73.14	C6 ²⁷	D = 32017 - R = 39815			
4+51 ⁸⁰	464.84	70.94	C6 ¹⁰	# 21 + BC			
4+23 ⁸⁰	462.80 ✓	68.84	C6 ⁰⁴	10+1180 = MH	500.80	507.36	C6 ⁵⁶
3+95 ⁸⁰	460.77 ✓	66.75	C5 ⁹⁸	9+75 ²³	498.20	504.01	C5 ⁸¹
3+67 ⁸⁰	458.73 ✓	64.63	C5 ⁹⁰				
3+39 ⁸⁰	456.70 ✓	62.66	C5 ⁹⁶	Treatro + Muirlands			
3+11 ⁸⁰	454.66 ✓	60.70	C6 ⁰⁴	Camino Del -			
3+01 ⁸⁰	453.82	60.00	C6 ¹⁸	Staked 6' 54" of L.			
+ EL Paso Real				Thence Ely in Camino Del Treatro			
#18 - Muirlands							
3+46 ⁸⁰ = MH	449.20			MH# 20			
				9+386 ⁷	495.61	502.26	C6 ⁶⁵
				9+02 ⁹²	493.55	499.87	C6 ³²
				8+69 ²⁴	491.49	497.55	C6 ⁰⁶
				8+34 ⁵⁶	489.43	495.17	C5 ⁷⁴
				7+99 ⁸⁸	487.37	492.65	C5 ²⁸
				7+65 ²⁰	485 ²¹	490.20	C4 ⁸⁹
				7+30 ⁵²	483.25	488.13	C4 ⁸⁸

Station	IE PIPE	Stake	Cut	Station	IE PIPE	Stake	Cut
$2R = 400'$ $D = 27^{\circ} 29' 30''$ 13+11.20 = BC	506.30	25.48	C1918				
12+73.81	506.15	26.92	C2077	14+83.91	507.02	525.78	C1876
MH# 22+EC 12+36.42 = E	506.00	26.46	C2046	12° 22' 15"			
16° 08' 30"				14+64.72	506.94	24.78	C1784
12+13.94	505.48	25.32	C1984	10° 59' 47"			
14° 31' 39"				14+45.53	506.86	23.65	C1679
11+96.42 = Begin Cradle - No Grade				9° 37' 19"			
13° 15' 48"				14+26.34	506.78	22.76	C1598
11+91.48	504.96	23.51	C1855	8° 14' 51"			
12° 54' 48"				14+07.15	506.70	22.23	C1553
11+69.02	504.44	22.35	C1691	6° 52' 22"			
11° 17' 57"	503.72			13+87.96	506.62	22.00	C1538
11+46.56	503.92	518.96	C1504	5° 29' 54"			
9° 41' 06"				13+68.77	506.54	22.16	C1562
11+24.10	503.40	16.81	C1341	4° 07' 25"			
8° 04' 15"				13+49.58	506.46	22.94	C16.48
11+01.64	502.88	14.79	C1191	2° 44' 57"			
6° 27' 24"				13+30.39	506.38	24.19	C17.81
				1° 22' 28"			
				chords 4/19.19±			

Muir Lands Sewer - 8" VCES IN easement in lots 5+6, Block 19 The Muir Lands Map # 2024. Alignment as shown on 3972 D between Manholes 11+12 NO good - See separate page (no number)

station IE Pipe stake

Line Between MH 12+11

Station IE Sewer stake

Muir Lands Dr
MH # 11 in

47 39
64.39
23.0

1+87.39 = 2 339.88 45.68 C580

23.10

1+64.39 341.14 49.36 C822

(22.98)

1+41.41 342.38 51.80 C942

(22.98)

1+18.43 343.62 53.13 C951

(22.98)

0+95.45 = EC 344.86 53.40 C854

endline

6° 49' ch = 23.80

MH # 23

0+71.65 346.14 53.75 C761

15+63.39 = 2 507.31 C1921 526.52

4° 32' 40" ch = 23.78

(30.26)

0+47.86 347.42 54.90 C748

15+33.13 507.22 C1957 526.79

2° 16' 20" ch = 23.79

(30)

A = 13038' R = 300'

15+03.13 = EC 507.10 C1943 526.53

0+24.07 = BC 348.70 559.05 C1035

13° 44' 35"

Block 19

Chord 19.22

12 in blk 4+5
0+08 = L MH # 350.00 263.24 C13.24

Sewer from MH #12 DWG 3972-D
IN NAVIRLAN 55 SWLY 117.02 TO PLUG

Sewer from MH #12 DWG 3972-D 65
IN NAVIRLAN 55' NELY to PLUG

Station	IE	Stake	Station	IE Sewer	Stake
1417 ⁰³ - Plug	364.00	68.94-C494			
0+93 ⁶⁰	361.20	66.05-C485			
0+70 ²⁰	358.40	65.12-C672	Plug- 0+55=	366.00	373.51-C751
0+46 ⁸⁰	355.60	64.40-C880	0+36 ⁶⁵	360.66	370.98-C1032
0+23 ⁴⁰	352.80	63.58-C1078	0+18 ³³	355.33	368.53-C1320
#12 0+00=LNH	350.00	64.55-C1455	#12 0+00=LNH	350.00	362.24-13.24

Stake 15' Alley - Block 13 -

- Plan - 13165 - L W.O. 32163

Pave - 14.50 wide - .25 Exc.

La Jolla Strand.

12-19-57 F.O.

842
27
17

66

	North			South			
Orsta Del Mar 0+00 = E.L. - Meet.							
+20 - 2'	37.87	^{7 87} 36.70	C 1.17	1.23 B	37.93	^{7 93} 36.95	C 0.98
+50 2'	40.88	^{0 88} 40.72	C 0.16	1.23 B	41.72	^{1 72} 40.97	C 0.75
+80 - 2'	44.59	⁵⁹ 44.75	F 0.16	1.17 B	45.80	45.00	C 0.80
1+10 - 2'	48.10	⁵⁹ 48.07	C 0.03	2' B	49.27	^{9 27} 48.32	C 0.95
+40 - 3' B.	51.61	^{1 61} 51.39	C 0.22	1.50 B	52.25	^{2 25} 51.64	C 0.61
+70 - 2' B.	55.82	^{5 82} 54.71	C 1.11	2' B	54.97	54.96	C 0.01
2+00 - 0.40 B.	59.47	^{9 47} 58.03	C 1.44	0.02 B	60.14	^{0 14} 58.28	C 1.86
+20 - 0.45 B.	61.75	^{1 75} 60.25	C 1.50	2' B	61.18	^{1 18} 60.50	C 0.68
+40 - 2' B.	62.17	¹⁷ 62.09	C 0.08	2' B	62.32	62.34	F 0.02
+60 - 0.55 B.	64.07	^{4 07} 63.20	C 0.87	2' B	63.84	⁸⁴ 63.45	C 0.39
+92 - 0.86 B.	65.38	^{5 38} 64.40	C 0.98	2' B	64.80	^{4 80} 64.65	C 0.15
3+24 - 1.40 B.	66.36	^{6 36} 65.61	C 0.75	2' B	65.95	^{9 5} 65.86	C 0.09
+56 - 0.92 B.	67.42	^{7 42} 66.82	C 0.60	2' B	67.07	67.07	G
+88 - 2' B.	68.52	^{5 2} 68.02	C 0.50	2' B	68.98	^{9 8} 68.27	C 0.71
4+20 - 1.40 B.	69.83	^{8 3} 69.23	C 0.60	2' B	70.05	^{0 05} 69.48	C 0.57
+52 2' B.	70.41	^{8 3} 70.43	F 0.02	2' B	70.88	^{8 8} 70.68	C 0.20
+84 - 2' B.	71.72	^{7 2} 71.64	C 0.08	2' B	72.43	^{2 43} 71.89	C 0.54

North				South			
5 + 16 - 2' B.	73.75	7	^{3.75} 2.84 C 0.91	4' B.	73.45	73.09	C 0.36
+ 48 - 2' B.	74.18	7	¹⁸ 4.06 C 0.12	4' B.	74.94	74.31	C 0.63
+ 80 - 0.48 B.	76.42	7	^{6 42} 5.25 C 1.17	4' B.	75.50	75.50	G
La Jolla Blvd.							
6 + 03.50 = W.L.				= Meet.			

Grade Stakes - Sullivan St.

E. of 63rd = Lot 4 - Block J. -

See - L-23 - Sheet I

= 24 above cb Grade
Prop. Grade

3+00.12 = W.L. Lot 4	28.79	⁸⁷⁹ 20.21	C 8.58
+25	26.22	⁶²² 20.13	C 6.09
+50	25.34	⁵³⁴ 20.04	C 5.30
+75	21.05	¹⁰⁵ 19.95	C 1.10
4+00.15 = E.L. Lot 4	22.20	²²⁰ 19.86	C 2.34

22.12

20.21

1.91 = above Prop. grade

B.M. = Spike in Pole - 3+00

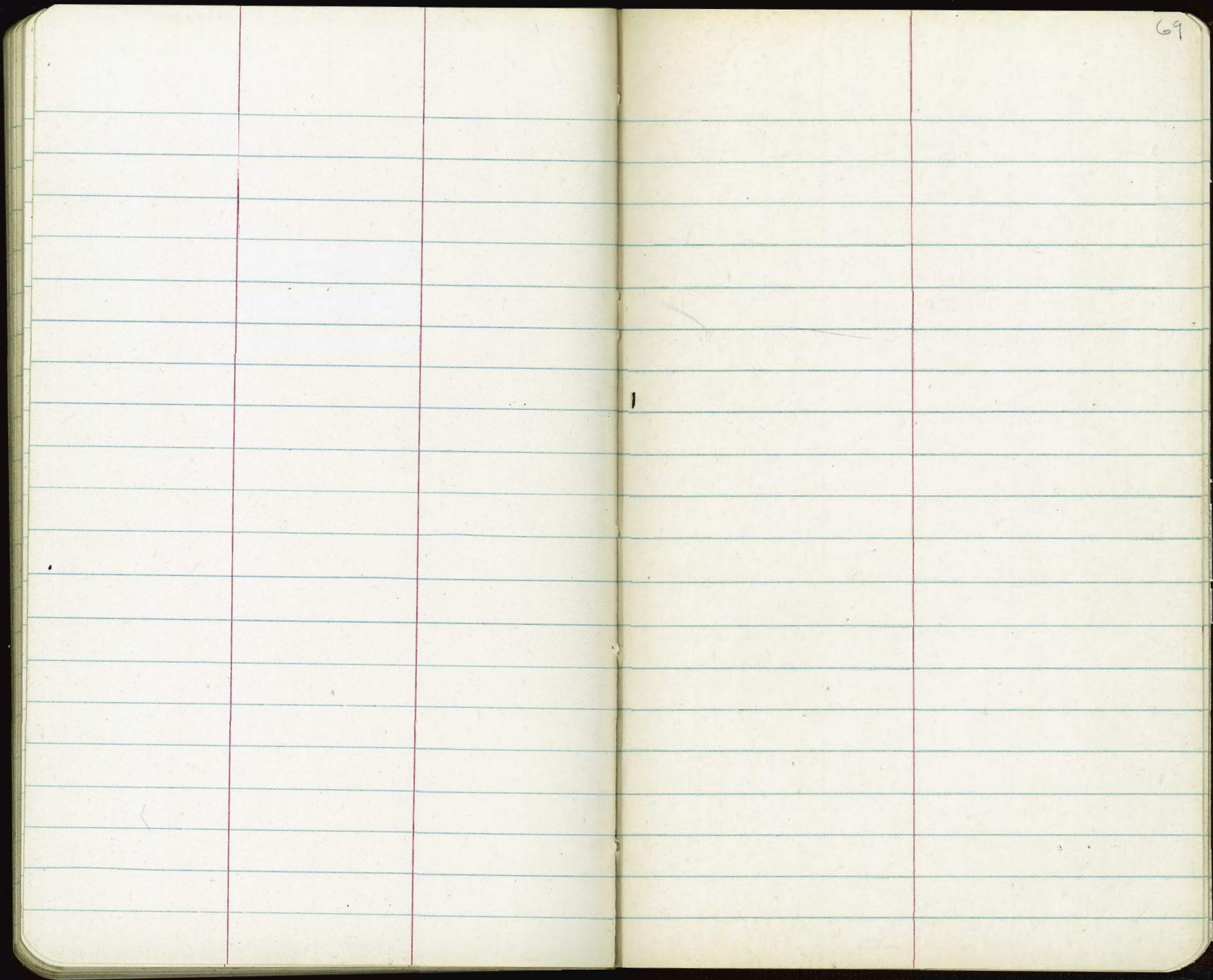
425.10

68

Map. 1170

± Grade = 30' S. of NL

24.84	⁴⁸⁴ 19.47	C 5.37
21.37	¹³⁷ 19.39	C 1.98
18.29	⁸²⁹ 19.30	F 1.01
16.95	⁶⁹⁵ 19.21	F 2.26
15.66	⁵⁶⁶ 19.12	F 3.46



curb stakes - 52nd Trojan to El Cajon
 Plan - 3149-D - 3150-D, w.o. 32 308 - 10-29-56

7.0

71

	W.			E.		
- end cb.						
0+00 = N.L. Trojan	28.15	28.10	C 0.05	27.30	27.25	C 0.05
+08 = PC.	29.12	^{9.12} 28.80	C 0.32	27.95	28.40	F 0.45
+23	31.10	^{1.10} 30.98	C 0.12	30.38	30.58	F 0.20
+63 = T.P.	36.80	36.78	C 0.02	36.12	36.38	F 0.26
+93	41.17	41.13	C 0.04	40.82	⁸² 40.73	C 0.09
1+13	44.06	44.03	C 0.03	43.68	43.63	C 0.05
+33	46.61	⁶¹ 46.57	C 0.04	45.86	46.17	F 0.31
+53	49.02	^{9.02} 48.88	C 0.14	49.67	^{9.67} 48.48	C 1.19
+73	51.19	^{1.19} 50.99	C 0.22	50.73	⁷³ 50.57	C 0.16
+93	52.71	52.84	F 0.13	52.32	52.44	F 0.12
2+13	54.38	³⁸ 54.49	F 0.14	54.18	¹⁸ 54.09	C 0.09
+33	55.92	55.93	F 0.01	55.28	55.53	F 0.25
+53	57.11	57.14	F 0.03	56.26	56.74	F 0.48
+73	57.95	^{7.95} 58.13	F 0.18	57.46	57.74	F 0.28
+93	58.66	⁶⁶ 58.90	F 0.24	58.33	58.51	F 0.18
3+13	59.24	²⁴ 59.45	F 0.21	58.92	59.06	F 0.14
+33	59.63	⁶³ 59.78	F 0.15	58.78	59.39	F 0.61
+73	60.20	60.22	F 0.02	59.52	59.83	F 0.31
4+13	60.77	⁷⁷ 60.66	C 0.11	60.24	60.27	F 0.03

W.

E.

4+53	.61.18	61.10	C 0.08		60.66	60.71	F 0.05
+93	61.37	61.54	F 0.17		61.21	61.15	C 0.06
5+13	61.85	61.83	C 0.02		61.78	61.74	C 0.34
+33	62.22	62.28	F 0.06		63.03	61.89	C 1.14
+53	62.41	62.86	F 0.45		63.78	62.47	C 1.31
+73	63.40	63.60	F 0.20		64.29	63.21	C 1.08
+93	64.25	64.48	F 0.23		64.74	64.09	C 0.65
6+13	65.49	65.52	F 0.03		65.56	65.13	C 0.43
+33	66.49	66.69	F 0.20		66.60	66.30	C 0.30
+53	67.72	68.02	F 0.30		68.30	67.63	C 0.67
+83	69.86	70.04	F 0.18		69.79	69.61	C 0.18
7+13	71.75	72.06	F 0.31		71.07	71.57	F 0.50
+33	72.32	72.68	F 0.36		71.61	72.46	F 0.85
+53	72.98	73.15	F 0.17		72.21	73.15	F 0.94
+76.10 = PC.	72.71	73.65	F 0.94	+75.93 = PC.	72.97	73.74	F 0.77
1/3	73.35	73.80	F 0.45		73.17	73.85	F 0.68
2/3	73.32	73.95	F 0.63		73.05	74.00	F 0.95
E.C. = Meet.		74.09			73.91	73.95	

Grades for storm Drain - 52nd + El Cajon - Plan - 3150-D

W.O. 32308

Conn. to Exist. Box S. cb. El Cajon - E. of 52 nd				2+10	61.94	61.94 55.06	6.88
1+04.51 = Conn.	73.62	73.62 58.73	14.89	+45	61.24	61.24 54.57	6.67
0+95.65 = E.C. - 10' lt.	73.07	73.07 58.62	14.45	+80	60.39	0.39 54.08	6.31
0+80.60 = B.C.	73.06	73.06 58.54	14.52	2+15	60.08	0.08 53.59	6.49
0+43.02 = E.C. ahead.	73.42	73.42 58.35	15.07	+50	59.97	9.97 53.10	6.87
0+30.46 = B.C.	73.55	73.55 58.29	15.26	+85	59.40	9.40 52.61	6.79
0+32.30 = Back - 6' rt.		72.79					
0+00 = Cleanout #1	72.79	58.14	14.65	4+20	58.71	8.71 52.12	6.59
15' inlet W. of 52 nd				+55	58.18	8.18 51.63	6.55
W. end = Meet cb.		74.39		+80		7.51 51.28	6.23
E. end opening - Top cb.	74.12	74.09	0.03				
I.E. Pipe + Box	74.12	74.12 68.26	5.86	+35	54.96	54.96 47.05	7.91
0+30.2 = Cleanout	72.79	72.79 68.13	4.66	+70	52.27	52.27 43.10	9.17
Req. 24" Pipe							
0+00 = Cleanout #1	72.79	73.50	70.71	6+05	49.14	9.14 39.14	10.00
+35	71.75	71.75 57.51	14.24	+40	45.26	5.26 35.18	10.08
+70	70.01	70.01 57.02	12.99	+75	40.43	4.43 31.22	9.21
1+05	67.75	67.75 56.53	11.22	7+10	35.27	5.27 27.26	8.01
+40	65.43	65.43 56.04	9.39	+30	32.45	32.45 25.36	7.09
+75	63.38	63.38 55.55	7.83	+50	29.74	9.74 24.17	5.57
				+80	27.06	7.06 22.91	4.15

B.M. = SW. Pole
Galveston + Napier

94.61

74

Stake Sewer - Galveston + Napier
for City Crew.

10-23-56 - 7.0

8+10	25.83	^{5.83} 21.66	C 4.17
+38.89	22.11	^{2.11} 20.46	C 1.65
1/2	21.31	^{21.31} 19.98	C 1.33
+61.93 = end.	19.95	⁹⁵ 19.50	C 0.45

0+00 = ~~E~~ Exist M.H.

I.E. of M.H.	93.77	^{93.77} 87.16	6.61
	93.48	^{93.48} 88.92	4.56
	94.78	^{94.78} 90.68	4.10

Rough Grades - Opal - Fanuel to Gresham
 Plan - 11492-L - W.O. 32335 10-18-56 7.0

75

N.

S.

0+00 = E.L. Fanuel	51.50	^{3.9} 52.3	Meat	51.6	49.45	Meat
+40	53.9	^{5.0} 53.4	C 1.6	51.6	51.3	C 0.3
+80	55.0	^{5.6} 54.6	C 1.6	52.9	52.5	C 0.4
1+20	55.6	^{7.3} 55.7	C 1.0	54.0	53.7	C 0.3
+60	57.3	^{8.4} 56.8	C 1.6	55.3	55.0	C 0.3
+97.63	58.4	^{9.7} 57.9	C 1.6	56.6	56.1	C 0.5
2+37.63	59.7	^{10.8} 58.8	C 1.8	57.6	57.2	C 0.4
+77.63	60.8	^{11.6} 59.5	C 2.0	58.4	58.2	C 0.2
3+17.63	61.6	^{12.2} 60.1	C 2.1	58.3	59.0	F 0.7
+57.63	62.2	^{12.6} 60.5	C 2.1	58.9	59.5	F 0.6
+97.63	62.6	^{12.9} 60.8	C 2.1	59.3	60.0	F 0.7
4+37.63	62.9	^{13.4} 61.1	C 2.1	59.7	60.3	F 0.6
+77.63	63.4	^{13.5} 61.3	C 2.3	60.3	60.6	F 0.3
+97.63 = W.L. Gresham	63.5	61.3	C 2.2	60.4	60.5	F 0.1

Curb stakes - Opal - Fanuel to
 Plan 11492-L w.o. 32335 10-24-56

Gresham
 70

76

		N		S B.M.
0+00 = E.L. Fanuel = Meet		51.50		49.45
+20	52.00	51.80	C 0.20	50.85 50.40 C 0.45
+40	52.51	52.25 ⁵¹	C 0.26	51.59 51.25 ⁵⁹ C 0.34
+80	53.48	53.40	C 0.08	52.68 52.48 C 0.20
1+20	54.60	54.55	C 0.05	53.93 53.72 ⁹³ C 0.21
+60	55.80	55.70	C 0.10	55.18 54.95 ⁵¹⁸ C 0.23
+97.63	56.87	56.80	C 0.07	56.54 56.11 ⁵⁴ C 0.43
2+17.63	57.48	57.35 ⁴⁸	C 0.13	57.09 56.70 ⁷⁰⁹ C 0.39
+37.63	58.05	57.86 ⁸⁰⁵	C 0.19	57.65 57.24 ⁶⁵ C 0.41
+57.63	58.54	58.33 ⁵⁴	C 0.21	58.04 57.73 ⁸⁰⁴ C 0.31
+77.63	59.06	58.75 ⁹⁰⁶	C 0.31	58.34 58.18 ³⁴ C 0.16
+97.63	59.39	59.14 ³⁹	C 0.25	58.80 58.59 ⁸⁰ C 0.21
3+17.63	59.76	59.48 ⁷⁶	C 0.28	58.94 58.95 F 0.01
+37.63	59.99	59.79 ⁹⁹	C 0.20	59.10 59.27 F 0.17
+57.63	60.14	60.05 ¹⁴	C 0.09	59.34 59.54 F 0.20
+77.63	60.38	60.27 ³⁸	C 0.11	59.32 59.77 F 0.45
+97.63	60.58	60.45 ⁵⁸	C 0.13	59.69 59.95 ³² F 0.26
4+37.63	61.05	60.77 ⁸⁵	C 0.28	60.23 60.27 ⁶⁹ F 0.04
+77.63	61.25	61.09 ²⁵	C 0.16	60.44 60.59 ²² F 0.15

N

4+87.63 = PC. 61.22 61.17²² C 0.05
 +97.63 = W.L. Gresham 61.27 61.37 F 0.10
 End = Prop. Line 62.59 61.90⁵¹ C 0.69
 East Ret.
 End = Prop. Line 62.21 62.00²¹ C 0.21
 Meet cb. at EL. 61.46

S

60.66 60.54⁶⁶ C 0.12
 60.54 60.34 C 0.24
 60.23 59.68²³ C 0.55
 60.38
 60.38 59.74 C 0.64
 60.08

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page is divided into three vertical columns by two red lines. The left page has a wide left column, a narrow middle column, and a wide right column. The right page has a wide left column, a narrow middle column, and a wide right column. The notebook is bound in the center, and the dark cover is visible at the edges. The number '79' is handwritten in the top right corner of the right page.

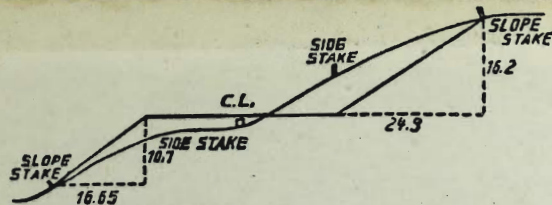
43rd - 5' E. of E. cb.

Myrtle - 3' S. of S. cb.

Thorns Fairmount = on E. Prop

check NE. Cor. Quince & Fairmount

Slive along Fairmount 3' W. of E.L.
To Laurel



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

THE NATIONAL BLANK BOOK COMPANY

HOLYOKE

MASSACHUSETTS

MASSACHUSETTS

NEW YORK

CHICAGO

BOSTON

SAN FRANCISCO