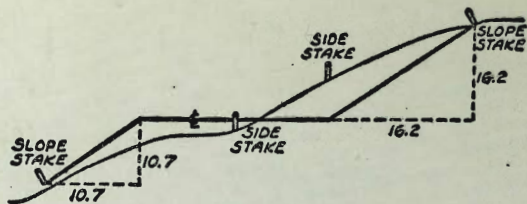


G-354

836 10 ~
817 11 ~



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

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DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level, the cut or fill is side

IMPROVED TABLES
AND
INFORMATION

left column and top row. The number in body
from side stake to slope stake. If ground is not
level estimate the difference in elevation between
the side stake and the lower stake by
this table. It will give the distance in table
amount to cut or fill and the distance in table
set up on the slope stake or on the shoulder
cut stake. It does not make the slight ob-
justment necessary.

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
the correction found in column of corrections.
Degree of curve with radius may be found
by dividing tangent (or external) opposite by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the radius of the tangent
length divided by twice the radius.

Table of Corrections
Tangent Correction
Loss of Tangent

- 0
- 1
- 2
- 3
- 4
- 5
- 6
- 7
- 8
- 9
- 10
- 11
- 12
- 13
- 14
- 15
- 16
- 17
- 18
- 19
- 20
- 21
- 22
- 23
- 24
- 25
- 26
- 27
- 28
- 29
- 30
- 31
- 32
- 33
- 34
- 35
- 36
- 37
- 38
- 39
- 40
- 41
- 42
- 43
- 44
- 45
- 46
- 47
- 48
- 49
- 50

Dis
grou
colum
side s
side s
cut o
If it

Index

✓ California St. Drain	3-35
Convoir Drain	37-46
✓ Calif. St. Drain change 77+06.143 To 80+67.73	47
✓ Backing Data. 29+60 ²³	14
✓ " " 63+10	27
✓ " check 63+10	79
✓ " Data. ^{spruce st.} 44+16	48
✓ " " Thorn St	49
✓ Drain North of Titus ^{west of} Mission Hills	50
✓ " North of Kottner & ^{Blvd.} " "	50
✓ " Estudillo St & San Diego Ave	51
✓ Walnut St drain	53
✓ Chalmers St. drain	54
✓ Sutherland at Moore "	55

Page

✓ Silvergate & Pio Pico - Sewer	56
✓ Trias & San Diego Ave. - Curbs.	57
✓ Alley Blk 30 Ocean Beach	58
✓ " " 29. " "	60
✓ HIGH AVE. ^{Torrey Road to} Virginia way	62
✓ Alley Blk 23 - O.B. Park.	65
Alley Catalina Terrace. ^{between} } Niagara & Narragansett & ^{Ely from} Venice }	67

INDEXED

APR 10 1957

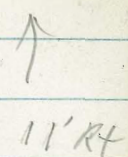
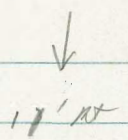
				4482 36.23 C 8.59
1+00		4300 36.98 C 6.02	2+50	
				4447 36.36 C 8.11
0+75		4273 37.11 C 5.62	2+25	
				4421 36.48 C 7.73
0+50		4207 37.23 C 4.84	2+00	
				4392 36.61 C 7.31
0+25		4201 37.36 C 4.65	1+75	
				4358 36.73 C 6.85
0+00 = N. Wily line Noel St.		4257 37.48 C 5.09	1+50	
0-03.6 = Ctr. type "F." C.O. Start 42"		4260 37.50 C 5.10	1+25	4294 36.86 C 6.08

3+89.58 Mid Curve.

~~35.45~~

4+56.66 = E.C.

47.01
33.73
C13.28



3+67²² = B.C.

46.32
35.66
C10.66

4+34.30 = Mid Curve.

46.57
33.85
C12.72

3+50

46.11
35.74
C10.37

4+11.94 = P.R.C.

46.25
33.96
C12.29

3+25

45.77
35.86
C9.91

3+97²³ = Start. 60" pipe

3+00

45.44
35.98
C9.46

3+95 = Ch. Type 'C' C.O.

(46") 46.08 46.08 (60")
35.53 34.03
C10.55 C12.05

Def 12.36'
4 27.78

2+75

45.11
36.11
C9.00

3+92.67
END. 42" pipe



6+00

47.49
33.01
C14.48

7+50.23 = (16)
Def. 0° 44' 20

48.03
32.26
C15.77

5+75

47.00
33.14
C13.86

7+24.46 = B.C.

47.95
32.39
C15.56

5+50

47.32
33.26
C14.06

7+00

47.85
32.51
C15.34

5+25

46.89
33.39
C13.50

6+75

47.77
32.64
C15.13

5+00

47.13
33.51
C13.62

6+50

47.30
32.76
C14.54

4+75

47.03
33.64
C13.39

6+25

47.59
32.89
C14.70

9+00
50.28
31.50
C18.78

8+79.22 = E.C.
hd. 2°-13'
49.72
31.62
C18.10

8+53.42 (1/3)
hd. 1°-28'-00"
Rad. 1012
ch. 26.08
49.04
31.75
C17.29

8+27.63 = (1/3)
hd. 0°-44'-20"
48.45
31.88
C16.57

8+01.84 = P.R.G.
hd 2°-13'
48.12
32.00
C16.12

7+76.04 = (1/3)
1°-28'-00"
R 989+
ch = 25.50
47.76
32.13
C15.63

10+11.83 = E.C.
53.59
30.95
C22.64

1/2 Δ = 12°-21'-15" (77°39')
inside
Ext. Socic 2.06' at Pt.
9+93.07 = (1/3)
53.25
31.04
C22.21

9+7A.31 = B.C.
52.68
31.14
C21.54

9+50
51.73
31.26
C20A7

9+25
0.50
51.01
31.38
C19.63

11+50

49.60
30.26
C 19.34

11+25

51.48
30.38
C 21.10

11 ~

52.58
30.51
C 22.07

10 + 75

0.50

53.19
30.63
C 22.56

12+31.33 = start 70" pipe

48.92
28.88
C 20.04

10 + 50

53.29
30.76
C 22.53

Type "D."
12+29 = ch. C.O.

10 + 25

53.70
30.88
C 22.82

12+26.67 = End. 60" Inch pipe.

49.07
29.88
C 19.19

12 ~

49.56
30.01
C 19.55

11 + 75

49.21
30.13
C 19.08

13+75.76 = B.C.

19.29

48.58
27.72
C 20.86

15+00

45.70
26.73
C 18.97

13+56.47

19.29

48.74
27.87
C 20.87

14+75

46.04
26.93
C 19.11

13+37.17

19.29

48.43
28.02
C 20.41

14+50

47.05
27.13
C 19.92

13+17.87 = E.C.

48.20
28.18
C 20.02

14+25

47.31
27.33
C 19.98

13+02.95 (1/2)

90.5 R. - T. = 17.02

47.75
28.30
C 19.65

PK PK
11 R. G. + 6 R. T. =
14+05.61 = E.C.

94.5 R. - T. = 13.14

47.48 ON LIP of
27.48 CURB
C 20.00

12+88.02 = B.C.

48.72
28.42
C 20.30

13+90.68 = (1/2)

48.24
27.60
C 20.64

16+50

4365
25.53
C 18.12

18+00

4247
24.33
C 18.14

16+25

4378
25.73
C 18.05

17+75

4280
24.53
C 18.27

16+00

4390
25.93
C 17.97

17+50

4299 TP
24.73
C 18.26

17+48 Conc. Lug
for 15" pipe

15+75

4453
26.13
C 18.40

17+25

4315
24.93
C 18.22

15+50

4451
26.33
C 18.18

17+00

4331
25.13
C 18.18

15+25

4550
26.53
C 18.97

16+75

4345
25.33
C 18.12

19+50
 3800
 22.03
 C 15.97

19+25
 3882
 22.47
 C 16.35

19+00
 3963
 22.72
 C 16.71

18+75
 4046
 23.36
 C 17.10

18+50 Brk
 4129
 23.80
 C 17.49

18+25 Brk
 4175
 24.13
 C 17.62

✓
 Clean out.
 20+75 = ctr. type "D"

~~20+70⁶⁷ End. pipe~~

20+50

20+25

20+00

19+75

3478
 17.83
 C 14.95

Top 35.60
 3478
 F 0.22

35.00
 2770
 F 7.30

3515
 20.27
 C 14.88

3554
 20.71
 C 14.83

3617
 21.15
 C 15.02

3723
 21.59
 C 15.64

1 2 3

21+61.48 (1/3)

3224
18.30
C 13.94

23+00

26.88
15.85
C 11.03

21+43.25 = P.R.C.

3265
18.62
C 14.03

22+75

28.43
16.29
C 12.14

21+25.02 (1/3)

32.83
18.74
C 13.89
2.83

22+50

29.19
16.74
C 12.45

21+06.79 (1/3)

33.45
17.26
C 14.19

22+25

30.65
17.18
C 12.87

20+88.50 B.C.

3372
17.59
C 14.13

21+97.94 = E.C.

31.05
17.66
C 13.39

~~20+77.52 start pipe~~

21+79.71 = (1/3)

31.45
17.78
C 13.47

26+02.24=B.C.

2536
13.92
C 11.44

24+50

2511
14.46
C 10.65

26+00

24+25

2530
14.55
C 10.75

25+75

2553
14.02
C 11.51

24+00

2594
14.63
C 11.31

25+50

2560
14.11
C 11.49

23+75 = B+k.

2637
14.72
C 11.65

25+25

2600
14.20
C 11.80

23+50 = B+k.

2675
14.97
C 11.78

25+00

2601 TP
14.28
C 11.73

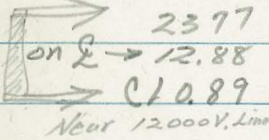
25.5

23+25

2700
15.41
C 11.59

24+75

2545
14.37
C 11.08

27+50	25.82 13.41 C 12.41	29+00	 23.77 12.88 C 10.89	23.66 12.88 C 10.78
27+25	25.91 13.50 C 12.41	28+75	10.89 7.00 C 3.89	23.72 12.97 C 10.75
27+00	24.63 13.58 C 11.05	28+50 ⁰⁸ = E Vine to East. 28+50		23.66 13.06 C 10.60
26+75	25.32 13.67 C 11.65	28+25		24.39 13.15 C 11.24
26+51.54 = E.C.	25.87 13.75 C 12.12	28+00		24.79 13.23 C 11.56
26+26.89 (1/2)	25.75 13.83 C 11.92	27+75		22.26 13.32 C 8.94

31+50
2°-01.20

21.56
12.01
C-9.55

33+00
4°-59.70

22.24
11.53
C10.71

31+25
1°-31.45'

21.68
12.09
C-9.59

32+75
4°-29.95'

22.32
11.61
C10.71

31+00
1°-01.70'

20.63
12.17
C-8.46

32+50
4°-00.20'

21.82
11.69
C10.13

30+75
0°-31.95'

19.53
12.25
C-7.28

32+25
3°-30.45'

21.86
11.77
C10.09

30+48.15 - P.R.C.

19.10
12.36
C-6.74

32+00
3°-00.70'

21.73
11.85
C9.88

30+35.95 (1/2)

19.55
12.48
C-7.07

31+75
2°-30.95'

21.72
11.93
C-9.79

(2.5 Sta. Chord 1456.39 Rad = 25.21)

Clean out.

35+90 - Ctr. Type "E" 12' LT

10.61



34+50

17.20
11.05
C 6.1535+87⁶² and 72"
pipe~~10.62~~

34+25

17.58
11.13
C 6.45

35+75

16.87
10.65
C 6.22

34+00

18.10
11.21
C 6.89

35+50

16.56
10.73
C 5.8333+71⁶⁷ E.C
60-25'18.66
11.30
C 7.36

35+25

16.64
10.81
C 5.83

33+50

50-59.20'

19.11
11.37
C 7.74

35+00

16.89
10.89
C 6.00

33+25

50-29-45'

20.89
11.45
C 9.44

34+75

16.98
10.97
C 6.01

37+00		18.00 10.26 C 7.74	38+50	20.30 9.78 C 10.52
36+75		17.72 10.3A C 7.38	38+25	19.63 9.86 C 9.77
36+50		17.40 10.42 C 6.98	38+00	19.28 9.94 C 9.34
36+20 = ϕ Thorny				
36+25		17.24 10.50 C 6.74	37+75	18.92 10.02 C 8.90
36+00	↑ 14' off	17.13 10.58 C 6.55	37+50	18.47 10.10 C 8.37
35+92 ³³ Start 78' pipe		16.87 10.60 C 6.27	37+25	18.30 10.18 C 8.12

Chisolm cross on signal base 18
1st pt. of 40+50 = El. 26.57

40+00	26.10 9.30 C16.80	41+25	25.91 8.90 C17.01
-------	-------------------------	-------	-------------------------

39+75	25.18 9.38 C15.80	41+00	25.56 8.98 C16.58
-------	-------------------------	-------	-------------------------

39+50	23.87 9.46 C14.41	40+75	26.04 9.06 C16.98
-------	-------------------------	-------	-------------------------

39+25	21.98 9.54 C12.44	40+50	26.57 9.14 C17.43
		40+25	26.30 9.22 C17.08

39+00	21.58 9.62 C11.96	40+	
-------	-------------------------	-----	--

38+75	21.07 9.70 C-11.37		
-------	--------------------------	--	--

clean out.
AA16 = ctr. type "E" - page 20

A2+75
27.12
8.42
C 18.70

AA+13⁶⁷ End 78"
pipe

~~8.00~~ page 20

A2+50
27.07
8.50
C 18.57

AA+00

27.35
8.02
C 19.33

A2+25
26.92
8.58
C 18.34

A3+75

27.55
8.10
C 19.45

A2+00
26.68
8.66
C 18.02

A3+50

27.48
8.18
C 19.30

A1+75
26.45
8.74
C 17.71

A3+25

27.39
8.26
C 19.13

A1+50
26.15
8.82
C 17.33

A3+00

27.33
8.34
C 18.99

45+25

28.67
7.42
C21.25

46+75

29.31
6.95
C22.36

45+00

28.50
7.50
C21.00

46+50

29.25
7.03
C22.22

44+75

28.31
7.57
C20.74

46+25

29.16
7.11
C22.05

44+50

27.55
7.65
C19.90

46+00

29.06
7.19
C21.87

44+25

27.44
7.73
C19.71

45+75

28.94
7.26
C21.68

44+18 ³² start 84" pipe

27.33 78" To N.W.
8.00
C19.33

27.33 84" To S.E.
7.75
C19.58

45+50

28.79
7.34
C21.45

stakes at
44+16

48+25	3025 6.49 C 23.76	49+75	3033 6.02 C 24.31
48+00 ✓	3008 6.57 C 23.51	49+50	3035 6.10 C 24.25
47+75	29.96 6.64 C 23.32	49+25	3015 6.18 C 23.97
47+50	29.72 6.72 C 23.00	49+00	3033 6.26 C 24.07
47+25	29.56 6.80 C 22.76	48+75	3032 6.33 C 23.99
47+00	29.48 6.88 C 22.60	48+50	3042 6.41 C 24.01

51+25

30 21
5.56
C 24.65

52+75

29 29
5.09
C 24.20

51+00

30 02
5.64
C 24.38

52+50

29 74
5.17
C 24.57

50+75

29 82
5.71
C 24.11

52+25

29 96
5.25
C 24.71

50+50

30 05
5.79
C 24.26

52+00

29 54
5.33
C 24.21

50+25

30 13
5.87
C 24.26

51+75

29 76
5.40
C 24.36

50+00

30 26
5.95
C 24.31

51+50

30 16
5.48
C 24.68

5A+25

28.45
4.63
C 23.82

55+25

4.32

27.60
4.34
C 23.26

↑

etc

55+08

5A+00

28.65
4.71
C 23.94

55+00

4.40

27.89
4.42
C 23.47

53+75

28.84
4.78
C 24.06

B.C. C.O.
5A+86.33 = Ctr. Type E.

53+50

28.96
4.86
C 24.10

5A+84.33 = B.C.

28.07
4.45
C 23.62

27.54
2
29.07

53+25

29.19
4.94
C 24.25

5A+75

28.20
4.47
C 23.73

53+00

29.26
5.02
C 24.24

5A+50

28.26
4.55
C 23.71

56+50	2616 3.96 3.9/A C 22.20	58+00	2385 3.49 3.4/7 C 20.36
56+25	2655 4.04 4.0/2 C 22.51	57+75	2425 TP 3.57 3.5/5 C 20.68
56+00	2710 4.11 4.1/9 C 22.99	57+50	2461 3.65 3.6/3 C 20.96
55+		57+25	2506 3.73 3.7/1 C 21.33
55+ 75	2710 4.17 4.1/7 C 22.81	57+00	2548 3.80 3.7/8 C 21.68
55+ 50	2730 4.24 4.2/4 C 23.04	56+75	2583 3.88 3.8/6 C 21.95

		2173 3.03		1996
59+50	3.61	C 18.70	60+64.09 (3/5)	2.66
				C 17.30

		2199 3.11		2085
59+25	3.69	C 18.88	60+45" (3/5)	2.72
				C 18.13

		2238 3.18		2043
59+00	3.16	C 19.20	60+25.91 (1/5)	2.78
				C 17.65
			chd = 19.05 6° 21.5'	

		2267 3.26		2179	20607
58+75	3.24	C 19.71	60+06.82 = P.C.C.	2.84	2.84 Rt
				C 18.95	C 17.76

		2307 3.33		2193
58+50	3.31	C 19.77	60+00	2.86
				C 19.07

		2339 3.41		2146
58+25	3.39	C 19.98	59+75	2.96
				C 18.50

See page 27
63+10⁰⁰ to 64+30⁰⁰ To be jacked

62+00
1774
2.20
C 15.54

61+75
1857
2.30
C 16.27

61+50
1873
2.40
C 16.33

61+25
1931
2.50
C 16.81

= 61+12.13 Ahead.
61+02.26 ^{FC.} ₍₄₎
1961
2.54
C 17.07

60+83.19 ₍₄₎
1976
2.60
C 17.16

Start of Jacking

63+10

1.75 ✓

63+00

1.80 ✓

62+98 ✓

62+75

15.75
1.90
C 13.85

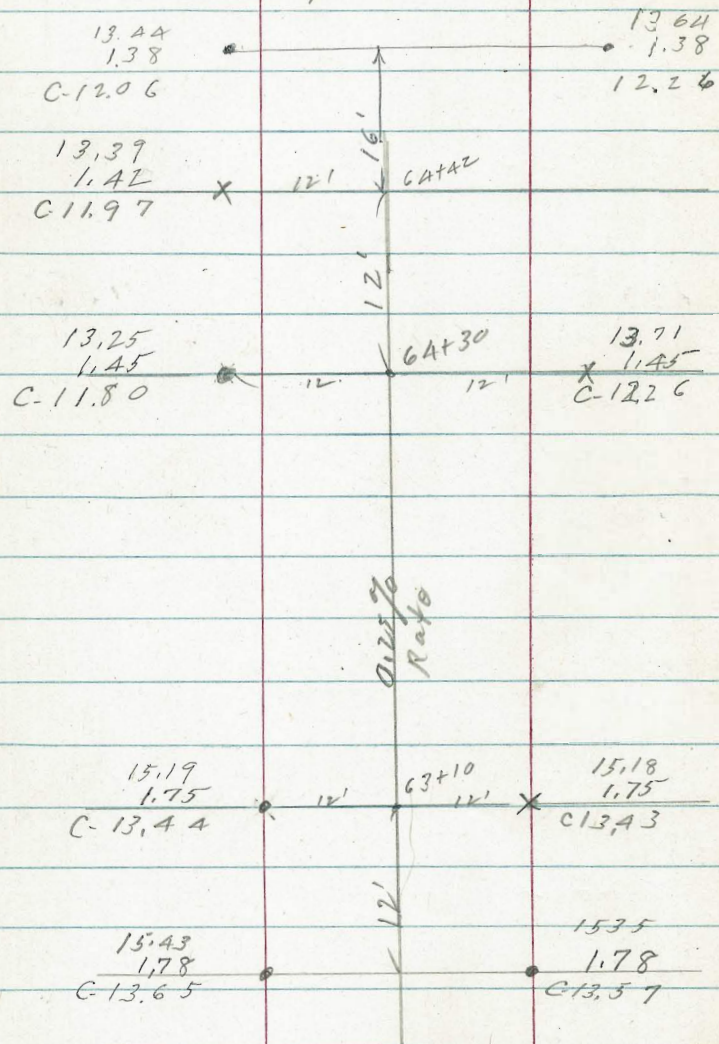
62+50

16.24
2.00
C 14.24

62+25

17.01
2.10
C 14.91

Sta. 63+10 to Sta. 64+30
Jacking Data.



B.M. = Nail in
wly end of south
Bottom stringer EL. 1.68

27
11-9-55

64+49 ^E	0.24 1.40 F 1.16	wly pipe
64+39 ⁹	0.48 1.42 F 0.94	ctr. pipe
64+39 ^L	0.50 1.43 F 0.93	ELY pipe
64+30 = End Jacking	EL. = 1.45	

65+00.91 (A) E.C.

1312
0.40
C 12.72

64+89.74 (A)

1321
0.58
C 12.63

64+79.48 (A)

1333
0.77
C 12.56

64+69.02 (A)

1334
0.96
C 12.3864+58⁵⁶ B.C.1339
1.15
C 12.2464+30
End Jacking

1.45

13.41
13.39

66+25

1200
- 0.65
C 12.65

66+00

1222
- 0.44
C 12.66

65+75

1243
- 0.23
C 12.66

65+50

1259
- 0.02
C 12.61

65+25

1287
0.19
C 12.68Clear out.
65+10⁰⁰ = Cr. Type "E"1300
0.32
C 12.68

$$67 + 40.76 = E.C.$$

$$\begin{array}{r} 1062 \\ - 1.64 \\ \hline C 12.26 \end{array}$$

$$68 + 75$$

$$\begin{array}{r} 821 \\ - 2.78 \\ \hline C 10.99 \end{array}$$

$$67 + 22.74 \left(\frac{4}{3}\right)$$

$$\begin{array}{r} 1079 \\ - 1.48 \\ \hline C 12.27 \end{array}$$

$$68 + 50$$

$$\begin{array}{r} 867 \\ - 2.57 \\ \hline C 11.24 \end{array}$$

$$67 + 04.73 \frac{1}{3}$$

$$\begin{array}{r} 1108 \\ - 1.33 \\ \hline C 12.41 \end{array}$$

$$68 + 25$$

$$\begin{array}{r} 900 \\ - 2.35 \\ \hline C 11.35 \end{array}$$

$$66 + 86.72 = B.C.$$

$$\begin{array}{r} 1127 \\ - 1.18 \\ \hline C 12.45 \end{array}$$

$$68 + 00$$

$$\begin{array}{r} 960 \\ - 2.14 \\ \hline C 11.74 \end{array}$$

$$66 + 75$$

$$\begin{array}{r} 1145 \\ - 1.08 \\ \hline C 12.53 \end{array}$$

$$67 + 75$$

$$\begin{array}{r} 1020 \\ - 1.93 \\ \hline C 12.13 \end{array}$$

$$66 + 50$$

$$\begin{array}{r} 1172 \\ - 0.87 \\ \hline C 12.59 \end{array}$$

$$67 + 50$$

$$\begin{array}{r} 1047 \\ - 1.72 \\ \hline C 12.19 \end{array}$$

$$67 \quad 69 + 96.77 = EC$$

$$\begin{array}{r} 692 \\ - 4.00 \\ \hline C 10.92 \end{array}$$

$$71 + 25$$

$$\begin{array}{r} 394 \\ - 6.53 \\ \hline C 12.47 \end{array}$$

$$6 \quad 69 + 79.76 \frac{2}{3}$$

$$\begin{array}{r} 695 \\ - 3.80 \\ \hline C 10.75 \end{array}$$

$$71 + 00$$

BRK

$$\begin{array}{r} 588 \\ - 6.15 \\ \hline C 12.03 \end{array}$$

$$6 \quad 69 + 62.95 \frac{1}{3}$$

$$\begin{array}{r} 721 \\ - 3.59 \\ \hline C 10.80 \end{array}$$

$$70 + 75$$

$$\begin{array}{r} 611 \\ - 5.63 \\ \hline C 11.74 \end{array}$$

$$69 + 45.74 = B.C.$$

$$\begin{array}{r} 728 \\ - 3.38 \\ \hline C 10.66 \end{array}$$

$$70 + 50$$

$$\begin{array}{r} 635 \\ - 5.11 \\ \hline C 11.46 \end{array}$$

$$69 + 25$$

$$\begin{array}{r} 751 \\ - 3.20 \\ \hline C 10.71 \end{array}$$

$$70 + 25$$

$$\begin{array}{r} 660 \\ - 4.59 \\ \hline C 11.19 \end{array}$$

$$69 + 00$$

$$\begin{array}{r} 791 \\ - 2.99 \\ \hline C 10.90 \end{array}$$

$$70 + 00$$

$$\begin{array}{r} 676 \\ - 4.07 \\ \hline C 10.83 \end{array}$$

Top 16" + 1.30 west hole
+ 1.41 East Hole

3.1

6 72+25

5.14
- 8.12
C 13.26

73+75

- 9.21

3.96
- 8.91
C-12.87

6 72+00

5.29
- 7.72
C 13.01

+55
73+50

- 9.18

4.10
- 8.91
C-13.01

6 71+75

8.55
- 7.33
C 12.88

73+25

- 9.14

4.41
- 8.91
C-13.32

71+71.81 = E.C.

5.64
- 7.28
C 12.92

+02
73+02 Brk

- 9.10

4.62
- 8.91
C-13.53

71+56.82 1/2

5.68
- 7.05
C 12.73

+84
72+75 Brk

4.80
- 8.91
C 13.71

71+41.84 = B.C.

5.76
- 6.81
C 12.57

72+50 ✓

5.03
- 8.51
C 13.54

See plan.
~~74+83 = C.O.~~1
2

-9.37

76+00

14' offset

3.67
-9.55
C 13.22

74+

75+75

3.47
-9.51
C 12.98

set at ↘

-8.91

74+75

9.36 ^{3.85}
-8.91
C 12.76

75+50

3.58
-9.48
C 13.06

-8.91

+53
74+50-9.33 ^{3.98}
-8.91
C 12.79

75+25

3.69 ^{3.68}
-9.44
C 13.13

C 12.59

+35
74+25-9.29 ^{4.17}
-8.91
C 13.08

75+00

-9.40 ^{3.70}
-8.91
C-12.61

74+00

-9.25 ^{3.82}
-8.91
C 12.73

1000 Rad. Rate = 1.65276'

stakes
12' Lt. of E

stakes
12' Lt. of E

stakes
12' Rt. of E

#1
77+21.27 1/6
A°-56'-40"

3.52
-9.73
C 13.25

= 78+02.14 Ahead }
78+05.55 Back } L.A.

3.14
-9.85
C 12.99

77+06.43 B.C.

3.60 353
-9.70 -970
C 13.30 13.23

77+90.00 F.M. EL. top of
16" (u) c - 0.30

#6
77+95.49 = (P) E.C.
29°-40'

3.03 3.90
-9.83 -9.83
C 12.86 C 13.73

Cont. on Page 47

#4 offset

77+00

-9.70

#5
77+80.64 5/6
24°-45'-10"

3.58
-9.81
C 13.39

76+75

3.52
-9.66
C 13.18

#4
77+65.80 1/6
19°-46'-40"

3.43
-9.79
C 13.22

76+50

3.53
-9.62
C 13.15

#3
77+50.96 3/6
14°-50'

3.40
-9.77
C 13.17

76+25

3.61
-9.58
C 13.19

#2
77+36.11 1/6
9°-53'-20"

3.42
-9.75
C 13.17

74' Rad. Ch. = 12.75'
86' " = 14.82'
98' " = 16.88'

79+20

3.99
- 10.02
C 14.01

79+00

3.83
- 9.99
C 13.82

78+80

3.74
- 9.96
C 13.70

78+62
78+60

1.91
- 9.93
C 11.84

vault. = -5.57
78+45 El. floor telephone

78+40

2.40
- 9.90
C 12.30

78+20

2.98
- 9.87
C 12.85

80+40

1.93
- 10.20
C 12.13

on 12' Rt. offset line
80+33⁴⁰ = P.O.T. cross on wall

80+20

3.64
- 10.17
C 13.81

80+00

3.73
- 10.14
C 13.87

79+80

3.73
- 10.11
C 13.84

79+60

3.81
- 10.08
C 13.89

79+40

3.84
- 10.05
C 13.89

81+40

2.18
~~-10.35~~ set at
 C12.53 C12.59

81+33¹¹ = Harbor Di. ~~14~~

2.36
~~-10.34~~
 set at -10.64 → C12.70

81+20

1.88
~~-10.64~~ set at
 C12.52 ~~C12.25~~ C-12.12

End of P.P.O.
 82+24

0.50
~~-10.48~~
 C10.98

81+00

2.09
~~-10.64~~
 C12.73 ~~C12.41~~

82+16 on wall

1.72
~~-10.47~~
 C-12.19

80+80

1.21
~~-10.64~~
 C11.85 ~~C11.50~~

81+80

1.20
~~-10.41~~
 C11.61

= 80+07.73 Ahead.
 New sta 80+90.90 back

80+60

1.96
~~-10.23~~
 C12.18

81+60

1.44
~~-10.38~~
 C.11.82

Laid in at -11.05

I.K. checked 11/19/55

A

A

Calif. St. Drain
Thru Convaire.

37

stakes 12' RT of

1+25
5.78
- 3.58
C-9.36

2+75
5.01
- 3.41
C-8.42

1+00
5.51
- 3.60
C-9.11

2+50
5.04
- 3.44
C-8.48

0+75
5.24
- 3.63
C-8.87

2+25
5.47
- 3.47
C-8.94

0+50
0.11
4.92
- 3.66
C-8.58

2+00
5.75
- 3.49
C-9.24

0+25
4.68
- 3.68
C-8.36

1+75
5.95
- 3.52
C-9.47

0+00
4.31
- 3.70
C-8.01
Existing Box

1+50
5.99
- 3.55
C-9.54

See sheet 2755-D

A+17⁴⁵ Rot. 12' offset

5.65

38

A+25

5.68
-3.25
C-8.93

5+75

6.27
-3.08
C-9.35

A+00

5.63
-3.27
C-8.90

5+50

6.11
-3.11
C-9.22

3+75

5.35
-3.30
C-8.65

5+25

5.95
-3.14
C-9.09

3+50

5.23
-3.33
C-8.56

5+00

5.86
-3.16
C-9.02

3+25

5.10
-3.36
C-8.46

A+75

5.77
-3.19
C-8.96

3+00

5.13
-3.38
C-8.51

A+50

5.71
-3.22
C-8.93

7+00 = 7.12

7+25

7.21
- 2.92
C 10.13

7+00

7.08
- 2.94
C 10.02

6+75

6.95
- 2.97
C 9.92

6+50

6.72
- 3.00
C 9.72

6+25

6.47
- 3.03
C 9.50

6+00

6.38
- 3.05
C 9.43

39

Cleanout
8+66 = Ctr. Type "B"

- 2.75

8+50

8.05
- 2.77
C 10.82

8+25

7.79
- 2.80
C 10.59

8+00

7.55
- 2.83
C 10.38

7+75

7.33
- 2.86
C 10.19

7+50

7.21
- 2.89
C 10.10

9+50

$$\begin{array}{r} 7.96 \\ -2.65 \\ \hline C 10.61 \end{array}$$

11+00

$$\begin{array}{r} 7.99 \\ -2.49 \\ \hline C 10.48 \end{array}$$

 7+29.19 E.C.
 16°-17'-37.5"

$$\begin{array}{r} 7.94 \\ -2.68 \\ \hline C 10.62 \end{array}$$

10+75

$$\begin{array}{r} 8.31 \\ -2.52 \\ \hline C 10.83 \end{array}$$

 9+16.40 $\frac{3}{4}$
 12°-13'-30"

$$\begin{array}{r} 7.94 \\ -2.69 \\ \hline C 10.63 \end{array}$$

 10+52
 10+50

$$\begin{array}{r} 8.46 \\ -2.55 \\ \hline C 11.01 \end{array}$$

 9+03.60 $\frac{1}{4}$ 12.79
 8°-09'

$$\begin{array}{r} 8.03 \\ -2.71 \\ \hline C 10.74 \end{array}$$

10+25

$$\begin{array}{r} 8.38 \\ -2.58 \\ \hline C 10.96 \end{array}$$

 8+70.80 $\frac{1}{4}$ chord = 12.79
 4°-02'-30"

$$\begin{array}{r} 8.20 \\ -2.73 \\ \hline C 10.93 \end{array}$$

10+00

$$\begin{array}{r} 8.22 \\ -2.60 \\ \hline C 10.82 \end{array}$$

8+78 = B.C.

$$\begin{array}{r} 8.28 \\ -2.74 \\ \hline C 11.02 \end{array}$$

9+75

$$\begin{array}{r} 7.89 \\ -2.63 \\ \hline C 10.52 \end{array}$$

12+50

8.14
-2.33
C 10.47

14+00 ^{± Vail} EL=7.90

7.83
-2.16
C 9.99

12+25

7.80
-2.36
C-10.10

13+75

7.76
-2.19
C-9.75

12+00

7.56
-2.38
C 9.94

13+50

7.75
-2.22
C-9.77

11+75

7.72
-2.41
C 10.13

13+25

7.85
-2.25
C-10.10

11+50

7.87
-2.44
C 10.31

13+00

8.00
-2.27
C 10.27

11+25

7.80
-2.47
C-10.27

12+75

8.23
-2.30
C 10.53

clean out
15+45 = Ctr. Type B

7.80
7.82
- 1.98

15+25

7.82
- 2.04
C 9.86

7.76 ← Pipe
- 2.04 - 0.06
C 9.80 low.

15+00

8.03
- 2.07
C 10.10

14+75

7.95
- 2.09
C 10.04

14+50

8.20
- 2.11
C 10.31

14+25

7.95
- 2.14
C 10.09

□ Foot of ladder Bldg. #4

42

15' west of P.I. EL. = 8.57

16+37.41

1/2

8.11

- 1.91

14°-52'-40"

C 10.02

16+26.24

1/2

8.12

- 1.92

7°-26'-20"

C 10.04

16+15.08 B.C.

8.07

- 1.93

C 10.00

16+00

7.96
- 1.95 - 1.94
C 9.90

15+75

7.84
- 1.98 - 1.96
C 9.80

15+50

7.83
- 2.04 - 1.97
C 9.80

17+25

8.34
-1.80
C 10.14

18+75

8.60
-1.62
C 10.22

17+00

8.30
-1.83
C 10.13

18+50

8.48
-1.66
C 10.14= 16+81.23 Ahead
16+82.07 Back E.C.
44°-38'8.25
-1.85
C 10.10

18+25

7.59
-1.69
C 9.2816+70.90 $\frac{1}{6}$
37°-11'-40"8.27
-1.87
C 10.14

18+00

8.02
-1.72 X 10' RT
C 9.7416+59.74 $\frac{1}{6}$
29°-45'-20"8.28
-1.88
C 10.16

17+75

7.98
-1.74
C 9.7216+48.57 $\frac{1}{6}$
22°-19'8.14
-1.89
C 10.03

17+50

8.08
-1.77
C 9.85

A3 R. Chord = 11.13

53' R. ... = 8.52

20450

8.66
-0.95
C-9.61

12' AT

Clean out. u.p.
18+97 = ctr. type H8.68
-1.12
C-9.80

20425

8.78
-0.98
C-9.76

12' AT

20400

8.98
-1.01
C-9.99

10' AT

18+

start
36" pipe

19+75

8.90
-1.03
C-9.93C.O. 8.54
18+83 = ctr. Type B. - 1.63 in
C-10.178.54
-1.13 out
C-9.67

19+50

8.65
-1.06
C-9.71

18+

End
42"
pipe

19+25

8.65
-1.09
C-9.74

22+00	8.54 -0.79 C. 9.33	C.O. 23+06 [±] ctr. type "H"	-0.67 in -0.17 out
21+75	8.55 -0.81 C. 9.36	23	End 36" pipe
21+50	8.54 -0.84 C. 9.38	23+00	8.85 -0.68 C. 9.53
21+17 ⁷⁶ = Δ 1 ⁰⁵ RT.	8.42 8.45 -0.87 C. 9.32	22+75	8.68 -0.70 C. 9.38
21+00	8.46 -0.89 C. 9.35	22+50	8.61 -0.73 C. 9.34
20+75	8.53 -0.92 C. 9.45	22+25	8.60 -0.76 C. 9.36

24+16		8.57	8.51	10' RT
24+20		-0.04	-0.04	
		C 8.61	C 8.55	

24+02		8.80	8.77	10' RT
24+00	10' RT.	-0.06	-0.06	
		C 8.86	C 8.83	

23+75		8.99	8.99	
		-0.09	-0.09	
		C 9.08		

23+50		9.10	9.10	± PK. = 8.18 El.
		-0.12	-0.12	End of line.
		C 9.22		

				Cleanout - " "
24+39 ⁵				ctr. type. G
		8.72	8.72	
		-0.02	-0.02	10' RT.
		C 8.74		

23+25		9.05	9.05	
		-0.1A	-0.1A	
		C 9.19		

23+	Start 30" pipe			
-----	-------------------	--	--	--

From page 33

= 80+67.73 Ahead P-35

47

80+90.90 E.C.

-10.64

79+00
10-48.44'

M. Rate = 1.58841

0.85
-10.18
C 11.03

80+81.04

-10.62

78+75
10-08.73'

Grade = 0.242%

2.20
-10.12
C 12.32

80+71.17 P.R.C.
6°-20.335

1.44
-10.59
C 12.03

78+50
0°-29.02'

3.20
-10.06
C 13.26

80+50
5°-46.70'

3.67
-10.54
C 14.21

78+31.73 = P.C.
29°-54' 1A

3.57
-10.01
C 13.58

80+25
5°-07'

3.61
-10.48
C 14.09

78+09.29 #3
21°-25'-30"

98' Rad. ch. = 25.50

3.29
-9.96
C 13.25

80+00
4°-27.28

3.64
-10.42
C 14.06

77+86.85 #2
14°-57'

A x 22.44

3.97
-9.90
C 13.87

79+45
3°-47.57'

3.63
-10.36
C 13.99

77+64.41 #1
7°-28'-30"

A x 22.44

4.27
-9.85
C 14.12

79+51.45 Mid C₄ r.o.

3.75
-10.30
C 14.05

77+41.97 = New B.C.
+ 35.54

4.15
-9.80
C 13.95

79+50
3°-07.86'

-10.30

77+06.43 = old B.C.

-9.71

79+25
2°-28.15'

3.76
-10.24
C 14.00

77+09 : 2.36 1.64
Top of P.R.C. = $\frac{4}{1.64} = 2.44$ 7.66
-9.30

Spruce St. Line
Sheet 2750-D.

EL 78" drain = ctr. C.O. = 0+00 Spruce
0+15 = start of jacking

EL. 0+04 = 13.75. This = inside
wall of C.O.

EL. 1+24 = 32.95 (16% for 120')

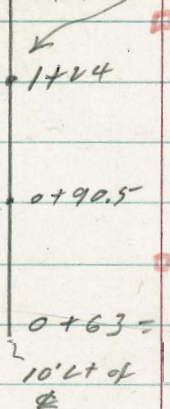
Make connection
to existing pipe

40.47
32.95
C-7.52

38.12
28.07
C-10.05

28.87
23.19
C-5.68

27.72
15.51
C 12.21

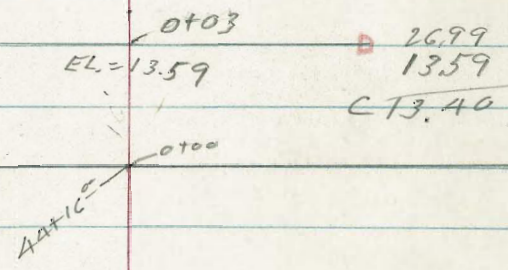


0+63 = end Jacking

0+15
I.E. = 15.51
27.46
15.51
C 11.95

27.22
13.59
C 13.63

Calif St. Drain



0+03
EL = 13.59
26.99
13.59
C 13.40

IN

Thorn street line 1/3/56
 shoot - #2750-D

Set. B.M. in Pole # P3410 EL = 14.94

14.24
 15.50 □ 12' 0+64 12' □ 7.28
 F 1.26 End pipe 15.50
 § = Face of C 1.78
 Head wall

• 0+27⁰⁵ = P.K. in sly.
 side of Tie

21.65
 14.70 □ 12' 0+16 12' □ 14.70
 C 6.95 start jacking C 7.02

9.44
 14.50 □ 12' 12' □ 14.50
 C 3.94 0+04 = start pipe C 3.62

35+90

0-14 = stub. □ 12'

4
 78

INDEXED

APR 10 1957

North of Titus St
West of Mission Hills Blvd.

1/3/56

Sheet # 275A-D.

0+00 = Nly. End 60" Existing pipe.
(I.E. = 86.75 ±)
(80' 30" pipe)

0+80 End pipe

92.67
89.60
C 3.07

0+60

93.86 N. 52°
88.95 Rt.
C 4.91

0+40

93.85 N. 56°
88.30 Rt.
C 5.55

0+20

92.80 N. 63°
87.65 Rt.
C 5.15

0+00 = Δ 30° Rt.

5.66 N
86.99 3' Rt.
C-8.67

INDEXED

APR 11 1957

North of Kettner Blvd
Mission Hills Blvd.

50

1/3/56

sheet # 275A-D.

I.E. = 84.7A
↓

0+63.6
0+00 = Sly end existing 60" pipe
(63.6' - 30" pipe)
stakes 8' Right.

existing 60" pipe.

0+63.6 = Meet

4.74
84.74 Meet

0+39.6 = E.C.

9.34
84.28
C 5.06

S.T. = 15.96
Ext. = 1°

0+23.8 = Mid Curve.
Δ = 20°

9.26
83.97
C-5.29

0+08 = B.C. Rt

8.87
83.66
C-5.21

0+00 = start pipe
in Kettner Blvd.
Δ 30° Rt.

87.21
83.50
C 3.71

0-47 = T Lt. = 4

83.66

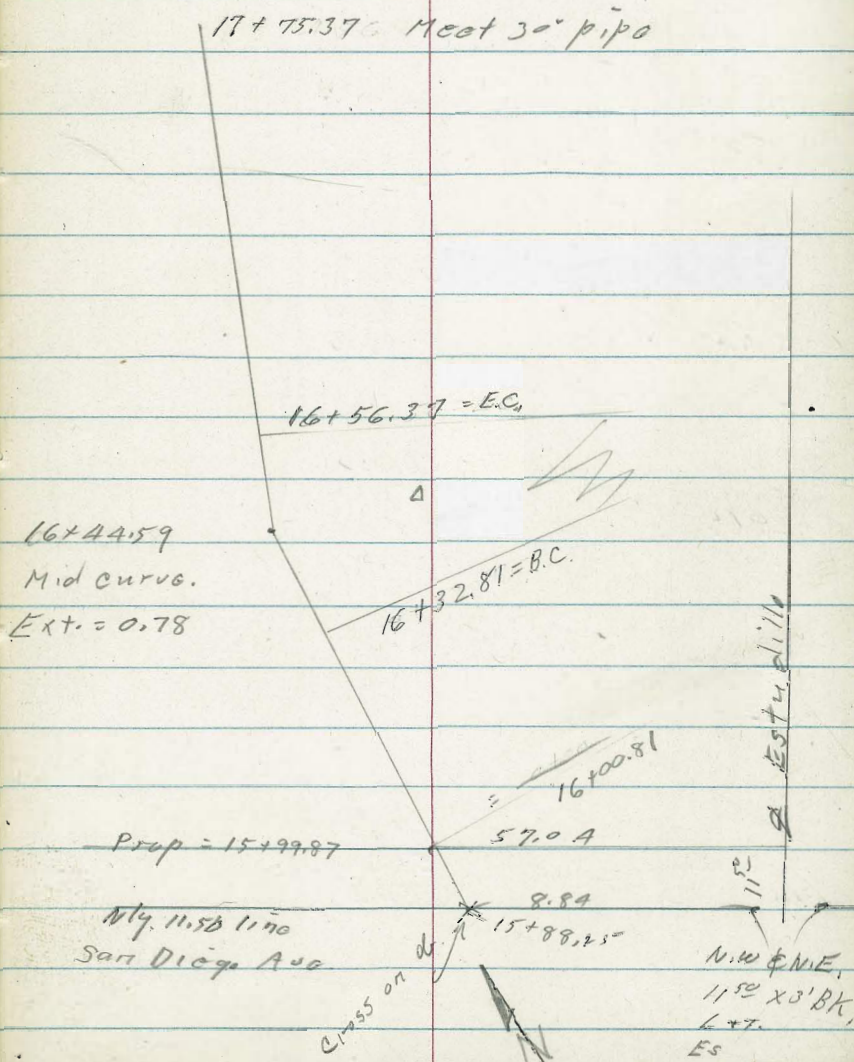
A.C. drive thru
auto court

30°		
Meet Existing =	92.78	7.77
17+75.37	74.74	92.78 8'LT
(23.44)		C-4.99
	4.68	4.68
17+51.93	88.38	88.90 8'LT
(23.43)		C-5.78
	2.67	
17+28.50 Brk	85.02	8'LT
(8')	C-7.65	
	2.15	
17+20.50 Brk	83.98	8'LT
(8')	C-8.17	
	1.76	
17+12.50 Brk	83.10	11'LT
(28.06)	C-8.66	
	9.21	
16+84.43	80.57	12'LT
(28.06)	C-8.64	
	7.51	
16+56.37 Brk	78.05	15'LT
	C-9.46	
	6.27	
16+44.59	76.99	15'LT
Mid Curve	C-9.28	
	5.51	
16+32.81 Brk	75.93	12'LT
(32')	C-9.58	
	8.91	
16+00.81	73.05	10'LT
	C-5.86	

INDEXED

51

Draw 1957
 A. Prad west of
 Estudillo St. & North of
 San Diego Ave.
 sheet 2756-D. 1/4/56



Drain at Calif., San Diego and
Sutherland
2754-D

52

~~0+89.3 Edge
Box~~

~~1+87.3 Make
Cont.~~

6082
56.00 ±
C 4.82

0+15.3 BRK

6620
56.83
C 9.37

1+61.3

6312
56.17
C 6.95

0+57.3 BRK

6618
57.00
C 9.18

1+35.3 PRC

6547
56.35
C 9.12

0+29.65

6635
58.11
C 8.24

1+20.3 Mid pt.

6569
56.46
C 9.23

~~0+02 Edge Box~~

1+05.3 BC

6596
56.56
C 9.40

0+00 Calif
cb Line

6723
59.21
C 8.02

0+91.3 cb Face
San Diego

6603
56.66
C 9.37

INDEXED

APR 10 1957

alnut St. Drain 3/23/52

St. to Kottner Blvd

B.M. = Cut stakes on Calif. St Drain

4112

53

SEly Cor

1450	33.25 25.51 C 7.74	3+32 = C.I.	41.72 37.00 C 4.72	
1425	32.43 23.51 C 8.92	2+98.75	41.33 36.68 C 4.65	
0+91	30.76 20.79 C 9.97	2+65E = C.O.	40.29 34.75 C 5.54	40.73 36.86 C 4.37
0+75	30.42 19.70 C 10.72	2+50	36.44 33.51 C 2.93	
0+59	29.70 18.78 C 10.92	+25	35.39 31.51 C 3.88	
0+31	27.90 17.46 C 10.44	2 ~	34.88 29.51 C 5.37	
0+03	26.47 16.15 C 10.32	1+75	34.22 27.51 C 6.71	
0+00 = 4' 72"				

INDEXED

Chalmers St. drain
APR 10 1957
California St to Kettner Blvd
Sheet # 2752-D. A-3-56

stakes 8' Lt. of \pm
 \pm Calif. St. drain = 0-04⁰⁰

1+40.50
44.22
37.14
C-7.08

0+98.25
42.03
34.52
C-7.51

0+56
38.86
31.90
C-6.96

0+48
38.11
31.22
C-6.89

0+40
37.16
30.36
C-6.80

0+00
~~25.30~~
35.10
25.00
C-10.10

2+272 = ctr. C.O.

2+25 = end pipe
48.62
42.38
C-6.24

1+82.75
47.10
39.76
C-7.34

INDEXED

APR 10 1957

Drain
Sutherland St.

at Moore 5-456

Sheet 2748-D

55

to Existing 30"

Make Conn.

0+58.53

52.19

47.00 ±

C 5.19

0+20^B = E.C.

48.40

42.19

E 6.21

0+00 = Existing drain
(New Const.)

39.00

New Elev set

by ?

INDEXED

Dewer - Silvergate

APR 10 1957

S. of Pio Pico

310' 8" line

5/25/56

56

2+50

308.76
295.96
C 12.80

2+00

306.13
294.36
C 11.77

1+50

303.52
292.76
C 10.76

1+00

301.24
291.16
C 9.88

0+50

98.89
289.58
C 9.31

0+00

96.77
287.98
C 8.77

Lat # 2 (1+52±)

302.93
293.84
C 9.09

Lat # 1 (3+22±)

112.75
298.78
C 13.97

3+10 = M.H. #1

11.99
297.88
C 14.11

3+00

11.50
297.56
C 13.940+00 = M.H. North of Pio Pico.
Exist M.H. sheet 60A6-B

INDEXED

rbs-

San Diego Ave

W.O.# 25020

57

APR 10 1957

Trias

5-28-56

stakes - 3' outside of cl. face

N. Ely. Cor. - (138' along S. D. Ave.)

sheet 3306-L

" 3305-L

" - T.A. 521.

Plans o.k. Per line. - N.G. for
grade. Met existing Impts.

Exist pave.

cl. Gr.

1+38

49.52

49.55
50.12
F0.57

1+03.5

50.27

0.42
50.97
F0.55

0+69

51.22

1.27
51.82
F0.55

0+34.5

51.95

52.04
52.67
F0.63

0+00

52.79

52.94
53.52
F0.58 Meet.

Existing cl. E.C.

INDEXED

Alley BIK 30-0. B.

W.O. 3174A

B.M. = S.Wly. B.P. Cape May.

58

APR 10 1957

SUNSET CLIFFS

6-28-56

between Cape May & Saratoga.

0+00 = wly. line Ebers. (sheet 3128-D)

		Lt. South	Rt. North			Lt.	Rt.	
					3+80 EUC. D.V.	9.87 29.76 C 0.11	30.70 29.46 C 1.24	N. - 0.40
1+80	D-1'	6.52 35.73 C 0.79	5.97 35.43 C 0.5A	D-2'	3+60 X-V	0.79 30.23 C 0.56	0.21 29.93 C 0.28	D-2'
1+60 P.O.C.	N. line	7.00 36.22 C 0.78	6.33 35.92 C 0.41	D-2'	3+40 D-V	1.02 30.77 C 0.25	0.60 30.47 C 0.13	D-6'
1+25	N. 35	7.84 37.02 C 0.82	7.00 36.72 C 0.28	D-2'	3+20 P.O.C. N-0.60	4.28 31.40 C 0.88	1.55 31.10 C 0.45	X-5'
0+90	D-2	8.14 37.82 C 0.32	8.77 37.52 C 1.25	N-0.35 8.13 C-1.2	2+80 N-1' 33.35	3.86 32.70 C 1.16	2.96 32.40 C 0.56	X-2' 33.05 C 0.18
0+55	X-2	9.12 38.62 C 0.50	8.60 38.32 C 0.28	D-2	2+40 EUC. N-1	5.45 33.99 C 1.46	3.94 33.69 C 0.25	D-2'
0+20	N-1.85	40.60 39.42 C 1.18	40.84 39.12 C 0.72	N. Line	2+20 X-2'	5.04 34.62 C 0.42	4.68 34.32 C 0.36	D-2'
0+00		39.82 [✓]	39.77 [✓]		2+00 D-V	5.28 35.20 C 0.108	6.46 34.90 C 1.56	D-2'

		LT.	RT.		
Cliff Elyline Sunset					
6100±		25.05 ^v	24.98 ^v		
5+56	C.20 25.99 C0.27	6.42 25.99 C0.43	8.21 25.88 C0.33	X-3'	6.11 25.88 C0.23
5+12	D-0.60 X-0.50 D-2'	7.00 26.73 C0.07	8.88 26.78 C0.10	X-2.50 D-1'	6.86 26.78 C0.08
4+68	D-1' 9.3 A	7.79 27.87 F0.08	7.75 27.67 C0.08	X-2'	
4+24	D-1'	8.74 28.81 C0.13	8.68 28.57 C0.11	X-2'	

INDEXED

APR 10 1957

Wey B/K 29 - Ocean Beach
6-28-56
Ebers to Sunset Cliff Blvd. W.O.# 31744

Between Brighton & Cape May.

Sheet 3127-D

B.M. = SWly. B.R. Cape May
Ebers - Elev. = 3642

60

	0+00 = wly line Ebers.				4+20 N-130	7.21 27.98 C 1.23	8.63 27.68 C 0.95	a-2'	
					3+80 N-012	7.27 28.26 C 1.01	7.38 27.96 C 1.42	N-0.13'	
1	1+20 E.V.C.	N-0.67'	1.91 30.85 C 1.06	1.03 30.55 C 0.48	N-1.30'	3+40 a-1'	8.65 28.54 C 0.11	7.65 28.24 C 1.41	N-0.15'
6	1 ~	N-0.120	2.83 31.27 C 1.56	0.87 30.97 F 0.10	a-2'	3+00 a-2'	7.04 28.82 C 0.22	9.44 28.52 C 0.92	N-0.120
5	0+80 P.O.C.	N-0.15V	3.01 32.00 C 1.01	1.50 31.70 F 0.20	a-V	2+60 B.K. a-1'	7.35 29.10 C 0.25	8.94 28.80 C 0.14	a-2'
5	0+50	X-2'	3.07 33.32 F 0.25	2.60 33.02 F 0.42	a-2'	2+40 B.K. a-1'	9.18 29.30 F 0.12	7.50 29.00 C 0.50	a-2'
4	0+20 (Meas 1938)	a-2'	4.78 34.65 C 0.13	3.83 34.35 F 0.52	a-2'	2+00 a-2'	9.92 29.82 C 0.10	29.52	
1	0+00		35.28 ✓ 35.23 ✓		1+60 N-030'	1.24 30.34 C 0.90	1.04 30.04 C 1.00	N-0.168	

Alley B/K. 29- O.B.

61

Sunset Cliffs

Ely. line

6+00

25.02 25.04

5+80

N. 0.30

7.79 6.20
26.01 25.87
C 1.78 C 0.33

0.0

5+60 N-1.48

N-.48'

7.79 6.25
26.79 26.53
C 1.00 F 0.28

0.2

5+40 P.O.C.

0.2'

7.48 6.77
27.14 26.84
C 0.34 F 0.07

0.0

5+00

N-1.60

7.82 8.24
27.42 27.12
C 0.40 C 1.12

N-.75

4+60

N-1.35

8.90 8.49
27.70 27.40
C 1.20 C 1.09

0.2'

122.64
INDEXED

High Ave.

6-29-56

WD# 31141

wly.

Eastly.

62

APR 10 1957

Sheet 12699-L

Rough
Grade

Curb

Curb

Rough
Grade

Torrey Road to Virginia Way.

1+40 Alley cl. E.C.

1.52 3.00
121.69 123.19
F0.17 F0.19

1+37 Alley
cl. B.C.

1.52 3.00
121.75 123.24 123.1
F0.23 F0.24

1+20

0.96 2.29 3.50 4.91
122.35 122.35 123.85 123.85
F1.39 F0.06 F0.35 C1.06

1+00

2.40 3.45 4.59 5.29
123.33 123.33 124.83 124.83
F0.93 C0.12 F0.24 C0.46

0+60

4.40 5.66 7.11 7.90
125.56 125.56 127.06 127.06
F1.16 C0.10 C0.05 C0.84

0+20

5.23 8.31 9.56 1.13
127.80 127.80 129.30 129.30 2' in
F2.57 C0.51 C0.26 C1.83

0+06 = cl. E.C.

7.48 8.74 9.90 1.45
128.60 128.60 130.00 130.00 2' in
F1.42 C0.34 F0.10 C1.45

0+00 = Nly line Virginia Way.

Curb returns - High Ave. at Virginia way Road.

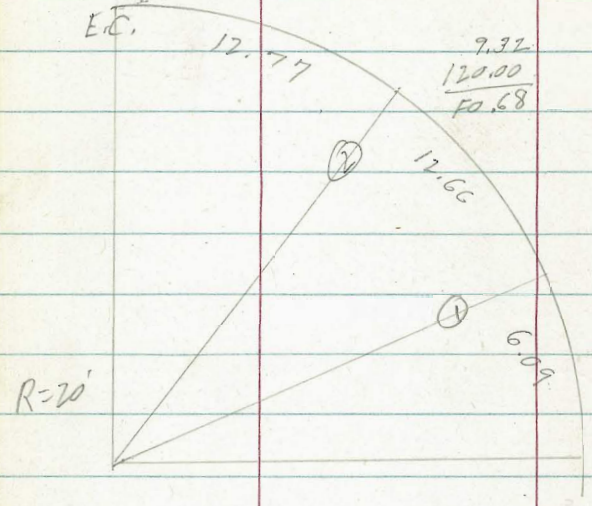
6A

INDEXED

119.37
1957

2.90
122.90
x

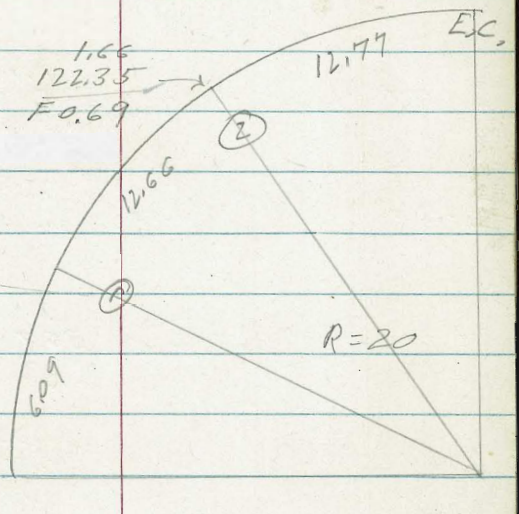
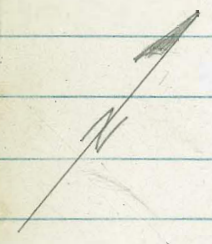
← Torrey Road →



7.32
120.00
F0.68

9.89
120.40
F0.51

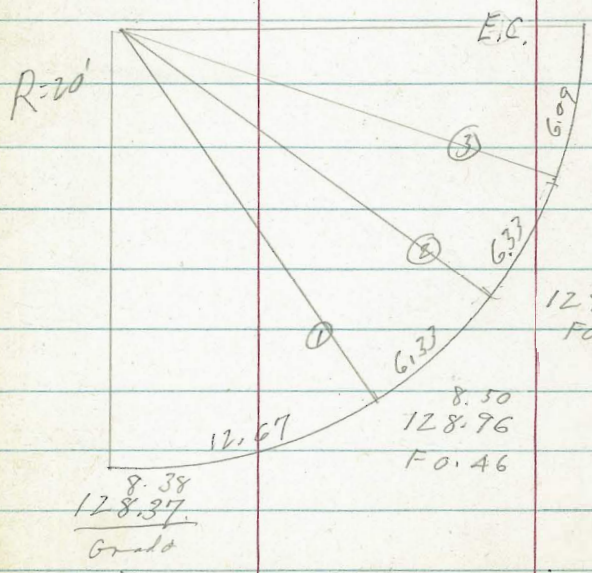
9.75
120.50
F0.75



1.65
122.35
F0.69

1.42
122.05
F0.63

1.84
122.00
F0.16



8.38
128.37
G0.34

8.75
129.00
F0.25

8.70
129.08
F0.38

8.50
128.96
F0.46

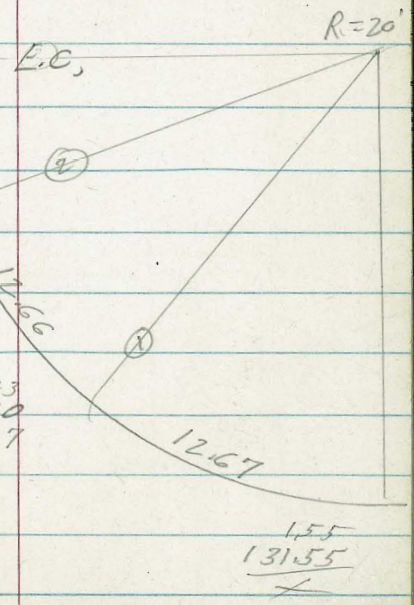
8.38
128.37
Grade
x

↑
High Ave.
↓

9.90
130.00
F0.10

9.77
130.30
F0.53

0.43
130.90
F0.47



1.55
131.55
x

← Virginia Way →

INDEXED

APR 17 1957

Key Bk. 23. O. B. Park.
 Fraude to Ebers w.o.# 32300
 Between Lotus & Greene. Street # 12464-L
 8/20/56

Lt.
5514

Rt. = N14.

65

		Lt. = 514	Rt. = N14		Ebers Ely line				
2+70	N-0.35	6.96 35.57 C 1.39	7.37 35.57 C 1.80	.25' N	6+00		31.88	31.69	
2+30	N-0.50	7.68 36.14 C 1.54	6.68 36.14 C 0.54	0-2'	5+60 Brk.	N-1'	2.69 32.18 C 0.51	2.12 32.04 C 0.08	0-2'
1+90 Brk	0-2'	7.04 36.71 C 0.33	7.00 36.71 C 0.29	0-2'	5+15	X 2'	2.62 32.57 C 0.11	2.71 32.43 C 0.28	0-0.32
1+70 Brk	0-2'	7.22 37.05 C 0.17	7.64 37.04 C 0.60	N-1.95'	4+70 Brk	0 2'	2.91 32.85 C 0.06	3.12 32.83 C 0.29	0-2'
1+50 Brk	0-2'	7.46 37.48 C 0.02	7.81 37.46 C 0.35	N-2.08'	4+50 Brk	N-0.80	3.27 33.03 C 0.24	3.12 33.03 C 0.09	0-2'
1+06.67		8.00 38.53	8.00 38.45 C 0.45	0-2'	4+30 Brk	N-0.92	4.07 33.29 C 0.78	3.56 33.29 C 0.27	X-1'
0+63.33	N-0.04	9.97 39.58 C 0.39	9.57 39.44 C 0.13	0-2'	3+90	0 1 ⁰⁰	3.96 33.86 C 0.10	4.13 33.86 C 0.27	0-2'
0+20 Brk	0-2'	1.46 40.64 C 0.82	1.01 40.43 C 0.58	X-1'	3+50	0 2'	4.86 34.43 C 0.43	5.01 34.43 C 0.58	0-2'
0+00 wly. line Fraude		41.12	40.89		3+10	N-0.39	6.58 35.00 C 1.58	5.44 35.00 C 0.44	0 2'

P-CC

Grades at garages etc

Lt.

±

Rt.

6+00

1.56
31.56
X

3+70

5.05
34.15
C 0.90

3+00

3+00

5.63
on M.H. 34.77
C 0.845.78
35.14
C 0.64

□

2+80

6.02
35.71
C 0.51

X

0+00

0.88
40.85
C 0.03

INDEXED

APR 10 1957

Catalina Terrace

Ely. From Venice St. &

From Niagara to Narragansett,

11-13-56

W.O.# 32677

Plan # 3551-D

(N.Wly & S.Ely. Alley) { Niagara to Narragansett }

1+30 ²⁵	End wall S.Wly. side in S.Wly. line alley		6.15 66.35 F 0.20	9.04 66.60 C 2.44	N-007 to To Prop.
1+08		X-2.25	6.10 66.42 F 0.32	7.05 66.67 C 2.38	N-007 Prop.
0+86		X 2.50	5.89 66.48 F 0.59	7.42 66.73 C 2.69	N-007 Prop.
0+64		N-2.93'	6.08 66.55 F 0.47	7.30 66.80 C 2.50	N 0.05 to Prop.
0+48 =	Start wall S.Wly side				X-on line
0+42		□ 2'	5.06 66.61 F 1.55	8.04 66.86 C 1.18	□ - 1.25 to E.P.
0+20 =	Brk	□ 2'	5.23 66.68 F 1.45	8.07 66.73 C 1.14	□ 1.12'
0+00 =	S.Wly. line Niagara		66.46 ^v	66.71 ^v	

27
25
19
27

67

N. wly & S. Ely. Alley.

68

outs to E.P. unless
otherwise noted

3+00 = N. Ely line Narragansett.

165.30

✓
166.22

2+80 B.K.

DP-2'

6.16
165.90
C 0.26

7.74
166.15
C 1.57

N-0.35 E.P.

2+58

X-0.75

6.87
65.97
C 0.90

8.13
66.22
C 1.91

N-0.40
E.P.

2+00 End wall on S. wly. side

N-0.25 back
OF Prop.

2+36

X-75

6.88
66.03
C 0.85

8.04
66.28
C 1.76

N-0.20
Prop

2+14

N-0.60

7.23
66.10
C 1.13

8.16
66.35
C 1.81

N-0.20
Prop.

1+92

X-1.50

6.82
66.16
C 0.66

8.10
66.41
C 1.69

N-0.35 to
Prop.

1+695 = Start wall - S. wly. side
1+70 = Δ in S. wly. line of alley

N-2'

6.88
66.23
C 0.65

8.13
66.48
C 1.65

N-0.17 to
Prop.

1+50 = ⊥ Alley to S. west.

X-2.62'

6.67
66.29
C 0.38

INDEXED

Ely & S.Wly. Alley
Catalina Terrace.

APR 10 1957

0+00 = S.Wly line of N.Wly &
S.Ely Alley.1+50 = $\frac{1}{2}$ opening to N.E. - No grade set.1+40²⁵ 29⁷⁵ RT. = Ely Cor. Pavement.
14⁷⁵ RT. = E.C. Pave1+35²⁵ = B.C. on RT. (Rad. = 5') 9⁷⁵ RT.0+92⁵

0+50 = Brk.

0+30 = Brk

0+10 = Δ in Alley Pavement = Brk.

0+00

outs to edge of Pave.

69

Lt.

Rt.

D 1.15

136
181.40
Eo.04

D-2'

7.42
177.34
Co.08

D-2'

4.12
173.28
Co.84

X-6'

1.66
171.03
Co.53

X-0.57

70.25
168.14
C2.09

E.C.

3.20
182.46
Co.74Pnt. 3.53 $\frac{1}{2}$ 5'
184.20
Fo.673.20
181.40
C 1.80

0.17 5' Rad

7.65
177.34
Co.31

D-2'

3.40
173.28
Co.18

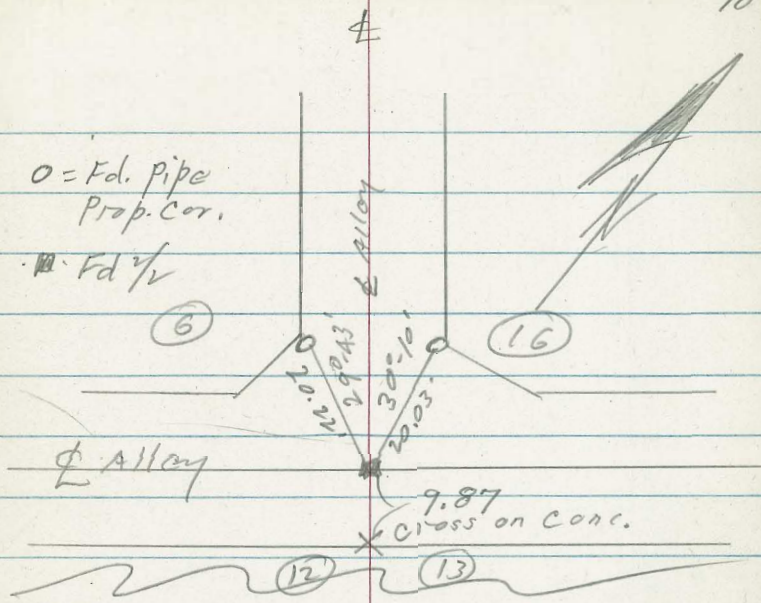
D-2'

70.98
171.03
Fo.05

X-2'

70.27
168.14
C2.13

N-0.145



1+80 = End pave

1+64⁷⁵ 9⁷⁵ Rt. = E.C. Pave.

29⁷⁵ Rt. = Nly. Cor. pave.
 1+59⁷⁵ 14⁷⁵ Rt. = B.C. Alley pave.

	LT.	RT.	
0.2'	6.60 185.70 C 0.90	6.96 185.70 C-1.26	0.2'
0.2'	2.79 184.26 F 1.47	5.82 184.26 C 1.56	on 5' Rad.
		BC 5.82 184.26 C 1.56	Nly. 6.60 Cor. 185.70 C 0.90

168
8.35 Boot.
10.03 T.P.

6A+22.70 = 1.35

1.33

1.31

1.33

1.30

1.34

1.41

1.57

1.75

1.90

1.94

1.86

1.83

1.70

1.64

572

216

43
BR.9
213
30

1939
12.79
4(6.60
1.63
1279

7444

3/12 1/4

7.75 4.00
218 276
-5.57 -1.24
7.67
-8.91

925
6.25

6.75
25
7.00
4.00
7.67

10.95
12.00

11.67
276
-8.91

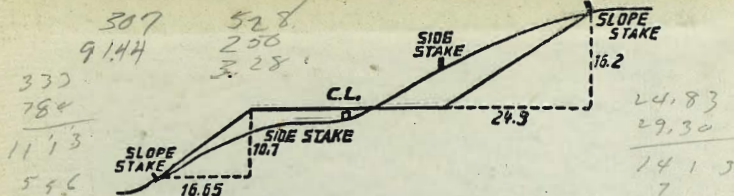
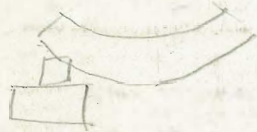
10.5

7.00

73.05

.58
25
83
12
63

275
75.80
35.00
10.75
24.24



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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