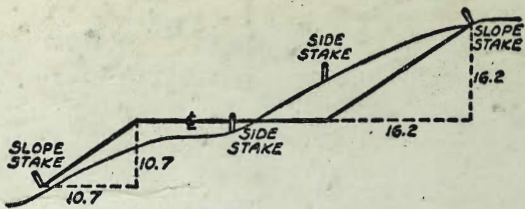




G-360



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 16 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level the cut or fill is small.

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IMPROVED TABLES  
AND  
INFORMATION

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TABLE No. VIII

To find Tangent and External Distance of any other degree, divide by degree of curve and add correction table in column of correction. Degree of curve with a given slope be found by dividing tangent (see column) opposite by given tangent (see column).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the degree.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.078	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.890	.987	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

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C/ARK  
GARBER  
O'NEIL  
ABRENILLA  
4-3-56  
W.O. 31595

IMP'S GREGORY = OCEAN VIEW  
Bldg. to Florence Lane

REF: DWG: 2966-D  
F.B 2293-31

SEWER-MAIN - (E Imp's Gregory)

Elev's

STA.	Elev's:	STA.	Elev's
1+75	6.79 2.30 C 4.49		
1+50	6.67 2.20 C 4.47	3+95.35 - Plug-end	8.14 3.18 C 4.96
1+25	6.58 2.10 C 4.48	3+60.35	8.05 3.04 C 5.01
1+00	6.44 2.00 C 4.44	3+25.35 = Connect to EXIST. P <sup>n</sup>	7.83 2.90 C 4.93
0+75	6.39 1.90 C 4.49	(If city forces here put in to a head) If not - cont. to continue to	7.35 2.80 C 4.55
0+50	6.35 1.80 C 4.55	2+75	7.08 2.70 C 4.38
0+25	6.47 1.70 C 4.77	2+50 = M.H. #2	6.54 2.60 C 3.94
Note: STA'S ON SEWER MAIN S to NORTH " ON ST N to S W	6.67 1.60 = F. Line C 5.07	2+25	6.83 2.50 C 4.33
(= M.H. #1 - meet EXIST E/W. Sewer Imp's ST GREGORY 4 0.65 N.W. of 0+16, N.W. of Line Florence - 1/4 N		2+00	6.81 2.40 C 4.41
B.M. DIR. Elev. Rod:	11.64 = S.W. B. 33rd &		

Note: Sew. LAT'S shown on pg 2 et al  
with ST. grades etc. & STREET STA'S:

↑  
40

NATIONAL

CB'S GREGORY  
OCEAN VIEW TO MARTIN

(E4) LT.				R.T.		LT.				RT (W'ly)	
STA	Prop	CB	♀	CB	Prop	STA	Prop	CB	♀	CB	Prop
						2+75	10.71	10.33 10.71 Fo.38		10.74 10.83 Fo.09	10.83
0+60 = B.V.C.	12.71 13.12 Fo.41	13.04 13.12 Fo.08		12.58 13.04 Fo.46	12.26 13.04 Fo.78						
						2+50	11.19 10.85 Co.34	10.49 10.85 Fo.36		10.84 10.95 Fo.11	11.29 10.95 Co.34
0+40	14.45	14.27 14.45 Fo.18		13.93 14.24 Fo.31	14.24						
						2+25	10.99	10.59 10.99 Fo.40		10.82 11.08 Fo.26	11.08
0+20	15.78	15.74 15.78 Fo.04		15.38 15.44 Fo.06	15.44						
						2+00	11.64 11.13 Co.51	10.90 11.13 Fo.23		11.11 11.20 Fo.09	11.83 11.20 Co.63
0+06 = CB, B.C.	17.14 16.70 Co.44	16.46 16.70 Fo.24		16.08 16.28 Fo.20	16.54 16.28 Co.26						
(17°)						1+75	11.27	11.13 11.27 Fo.14		11.25 11.33 Fo.08	11.33
# 1		16.99 16.70 Co.09		16.38 16.50 Fo.12							
(13°)						1+50	12.07 11.41 Co.66	11.21 11.41 Fo.20		11.30 11.45 Fo.15	11.98 11.45 Co.53
# 2		17.32 17.05 Co.27		16.80 16.60 Co.20							
(30°)						1+25	11.55	11.29 11.55 Fo.26		11.32 11.58 Fo.26	11.58
# 3		17.33 17.20 Co.13		16.76 16.72 Co.04							
(30°)						1+00 = E.V.C.	12.21 11.69 Co.52	11.50 11.69 Fo.19		11.65 11.70 Fo.05	12.11 11.70 Co.41
# = CB, E.C. #		chk. 17.18 17.21		chk. 16.58 16.61							
0+00 = S'ly LINE OCEAN VIEW BLDG.	16.9				16.6	0+80	12.10	12.03 12.10 Fo.09		12.06 12.07 Fo.01	12.07

STA.		LT.	CB	E	RT.	Prop	STA.	LT.	CB	E	RT.	Prop
4485	= SEN LAT #1 RT.			10.25 4.5 C5.75		10.25 5.1 5.15						
4480	= W. S. RT.					10.13 9.81-CB C0.32	6+00	LT. ONLY	8.87			8.69 8.87 Fo.18
4475	9.58	9.32 9.58 Fo.26			9.70 9.83 Fo.13	9.83	5+75	LT. ONLY	9.01 C0.82			8.71 9.01 Fo.30
4450	10.21 9.72 C0.49	9.50 9.72 Fo.22			9.84 9.95 Fo.11	10.80 9.95 C0.85	#3 = ECUMBAT Prop MARTIN					9.3 rough grade only = P.L. MARTIN
4425	9.86	9.86 9.86 Grade			9.74 10.08 Fo.34	10.08	#2					9.48 9.28 C0.20
4400	10.22 10.00 C0.22	9.77 10.00 Fo.23			10.03 10.20 Fo.17	10.84 10.20 C0.64	#1					9.34 9.27 C0.07
3+75	10.14	9.93 10.14 Fo.21			10.29 10.33 Fo.04	10.33	5+62 <sup>18</sup> = CB. B.C. RT ONLY					9.13 9.30 Fo.17
3+50	10.91 10.28 C0.63	10.10 10.28 Fo.18			10.16 10.45 Fo.29	11.11 10.45 C0.66	5+50		9.84 9.15 C0.69	8.99 9.15 Fo.16		9.09 9.39 Fo.30
3+25	10.42	10.19 10.42 Fo.23			10.29 10.33 Fo.04	10.33	5+25		9.84 9.15 C0.69	8.99 9.15 Fo.16		9.12 9.45 Fo.33
3+00	11.09 10.57 C0.52	10.25 10.57 Fo.32			10.16 10.45 Fo.29	11.11 10.45 C0.66	5+00		9.29 9.29 Fo.09	9.20 9.29 Fo.09		9.15 9.58 Fo.43
					10.45 10.58 Fo.13	10.58			9.81 9.44 C0.37	9.22 9.44 Fo.22		9.44 9.70 Fo.26
					10.70 10.70 grade	11.56 10.70 C0.86						10.09 9.70 C0.39



GREGORY - MARTIN to  
FLORENCE LANE

(Lly) LT.

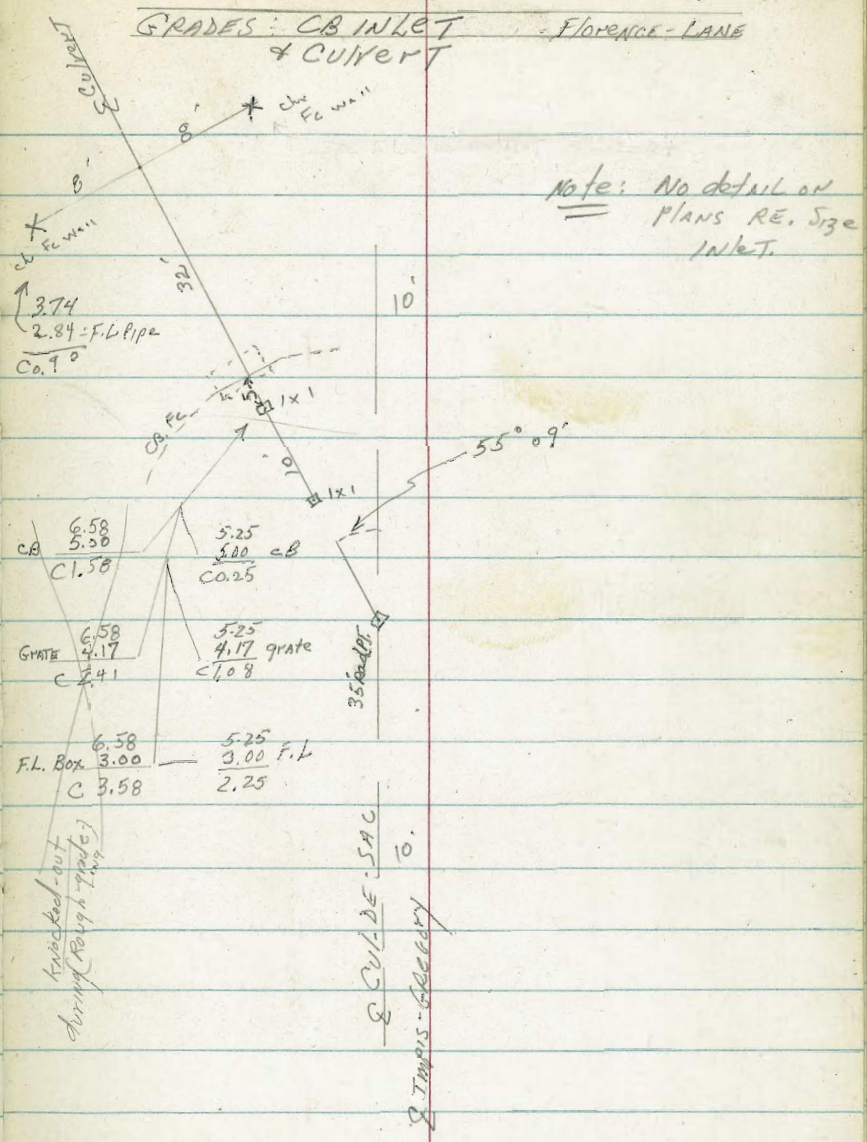
STA	Prop	CB	E	CB	Prop	STA	prop.	CB	E	CB	Prop.
						0+70=MS LT.		8.65 8.33 CB Co.32			
						0+65=SEN LAT # (2) LT.	8.37 5.0 C3.37		8.37 4.7 3.97		
						0+50	8.65 8.45 Co.20	8.28 8.45 Fo.17		8.32 8.55 Fo.23	8.72 8.55 Co.17
						0+25	8.59	8.56 8.59 Fo.03		8.51 8.67 Fo.16	8.67
						0+13=CB B.C.P.T. (Sully) only				8.60 8.73 Fo.13	8.88 8.73 Co.15
						# 1.				8.59 8.80 Fo.21	
						# 2				8.86 8.85 Co.01	
						# 3 = E.CURB at Prop. MARTIN (RT ONLY)				8.77 8.86 Fo.07	
						0+00 = S.LINE MARTIN	9.20 8.73 Co.47	8.61 8.73 Fo.12			8.90 8.80 Co.10
0+25 =	8.73	8.73									
LT. ONLY = S.LY/LINE MARTIN	(0+00 MARTIN to Florence Lane)										

LT.					RT. (W.4)						
STA.	Prop	CB	E	CB	Prop	STA.	Prop	CB	E	CB	Prop
2+60	END ABANDON Sewer					3+50	7.89 6.75 C1.14	6.71 6.75 F0.04		6.87 7.05 F0.18	7.58 7.05 C0.53
2+25	beg 35 E Sewer. MAIN ABANDON	7.29 7.46 F0.17		7.56 7.67 F0.11	7.67	3+32	EXIST SEW. LAT. LT. - ENCASE				
2+25	END SEWER ENCASE = EXIST. LAT. RT. ENCASE					3+25	6.89 F0.10	6.79 6.89 F0.10		7.00 7.17 F0.17	7.17
2+00	Beg ENCASE. E Sew. MAIN	8.91 7.60 C1.31	1.46 7.60 F0.14	7.62 7.80 F0.18	8.23 7.80 C0.43	3+20	W.S. RT.			7.82 7.19 CB C0.63	
1+75		7.74	7.46 7.74 F0.28	7.74 - TR 7.92 F0.18	7.92	3+15	SEW LAT # (5) RT.			7.96 3.3 C4.66	7.96 3.9 C4.06
1+70	W.S. LT. + EXIST SEW. LAT. RT ENCASE	9.05 7.76 CB C1.29				3+00	8.44 7.03 C1.41	6.80 7.03 F0.23		7.17 7.30 F0.13	8.09 7.30 C0.79
1+65	SEW. LAT # (3) LT ENCASE	9.29 5.4 C3.89		9.29 4.8 C4.49		2+75		7.06 7.18 F0.12		7.26 7.42 F0.16	7.42
1+50		8.75 7.89 C0.86	7.63 7.89 F0.26	7.96 8.05 F0.09	8.67 8.05 C0.62	2+70	EXIST SEW LAT. RT. - ENCASE				
1+25		8.03	7.91 8.03 F0.12	8.04 8.17 F0.13	8.17	2+70	W.S. RT.			7.95 7.44 CB C0.51	
1+00		8.47 8.17 C0.30	7.99 8.17 F0.18	8.05 8.30 F0.25	8.80 8.30 C0.50	2+65	SEW LAT # (2) RT.			8.06 3.5 C4.56	8.06 4.1 C3.96
0+75		8.31	8.11 8.31 F0.20	8.18 8.42 F0.24	8.42	2+50		8.70 7.32 C1.38	7.10 7.32 F0.22	7.39 7.55 F0.16	7.97 7.55 C0.42

STA.	Prop	CB	Σ	CB	Prop.	STA.	Prop	CB	Σ	CB	Prop.
4+90=SEW LAT #10 RT ENCASE			6.61 2.6 C 4.01		6.61 3.2 C 3.41	6+11.20= CB B.C. RT				5.68 5.75 Fo.07	6.39 5.75 C 0.64
4+85=WS RT.					6.65 6.37 CB C 0.28	6+00 RT ONLY				5.63 5.80 Fo.17	5.80
4+75	6.04	5.50 6.04 Fo.54		6.19 6.42 Fo.23	6.42	5+90=SEW LAT #10 RT ENCASE			6.31 2.2 C 4.11		6.31 2.8 C 3.51
4+50	6.98 6.18 C 0.80	5.74 6.18 Fo.44		6.41 6.55 Fo.14	6.68 6.55 C 0.13	5+85=WS RT					6.31 5.86 CB C 0.45
4+30=SEW LAT #10 LT.	6.7 3.2 C 3.5		6.7 2.8 C 3.9			5+82.91=CB B.C. RT.	6.08 5.43 C 0.65	5.10 5.43 Fo.33			
4+25	6.33	5.98 6.33 Fo.35		6.60 6.67 Fo.07	6.67	5+75	5.48	5.10 5.48 Fo.38		5.71 T.P. 5.92 Fo.21	5.92
4+10=WS LT.	6.96 6.40 CB C 0.56					5+50	6.49 5.62 C 0.87	5.18 5.62 Fo.44		5.86 6.05 Fo.19	6.41 6.05 C 0.36
4+00	6.98 6.47 C 0.51	6.15 6.47 Fo.32		6.77 6.80 Fo.03	6.93 6.80 C 0.13	5+40=SEW LAT #10 RT ENCASE			6.36 2.4 C 3.96		6.36 3.0 C 3.36
3+90=SEW LAT #6 RT.			7.00 3.0 C 4.0		7.00 3.6 C 3.4	5+35=WS RT.					6.51 6.11 CB C 0.40
3+85=WS RT.					6.85 CB (IN)	5+25	5.76	5.34 5.76 Fo.42		5.94 6.17 Fo.23	6.17
3+75	6.61	6.28 6.61 Fo.33		6.68 6.92 Fo.24	6.92	5+00	6.76 5.90 C 0.86	5.53 5.90 Fo.37		5.95 6.30 Fo.45	6.51 6.30 C 0.21

GRADES: CB INLET & CULVERT - Florence-LANE

STA	LT.		RT.	
	Prop	CB	CR	Prop
<u>CHK:</u>			14.90 =	14.92 =
			S.E.B.P	
			OCEAN-View Blvd	
			+33'nd	
6+80.54 = SLY LINE Florence LANE	8.7 5.00 C 3.7	6.4 5.3 = CB C 1.1	7.25 5.50 C 1.75	
6+60.54 = NLY LINE Florence LANE	6.00 C 1.00		6.78 5.50 C 1.28	
6+40.54 = RAD. PT. CUL-DE-SAC (Stubs 5' BK CB) ON R. grade	5.10 C 1.0		6.54 5.55 C .99	
6+35 = W.S RT.			6.35 5.55 = CB C .80	





CLARK  
GARBER  
ONEIL  
ABRENILLA  
5-8-56  
N.O. 31793

52nd - REX - LANDIS - STERLING COURT  
ET - AL: OAK PARK ANNEX

REF: DWG: 306 3-D - 3072-D  
F.B: 2105 - 1569 - 2338 - 2383 - 2296 - 2230

52nd ST. (UNIV. to REX)

STA.	LT. (E.S.)		RT		STA.	Prop	CB	E	CB	Prop
	Prop	CB	E	CB						
0+90	325.41 324.23 C1.18	324.11 324.23 Fo.12		323.79 323.73 Co.06	334.64 323.73 C10.91 332.4 = CB C12.4	1+39.59 Alley B.C.LT.	328.40		328.67 328.40 Co.29	
0+75 = W.S. RT										
0+70	322.18	321.77 322.18 Fo.41		321.39 321.68 Fo.29	321.68	Alley E.C.	328.32		328.67 328.32 Co.35	
0+50	320.36 319.93 Co.43	319.33 319.93 Fo.60		319.35 319.43 Fo.08	333.20 319.43 C13.77	1+37.58 Alley at Prop	332.70 328.44 C1.26		332.88 328.44 C4.44	
0+40	318.75	318.40 318.75 Fo.35		318.62 318.25 Co.37	318.25	1+30 RT only			327.37 327.20 Co.17	334.25 327.20 C7.05
0+30	317.65	317.67 317.65 Co.02		317.62 317.32 Co.30	317.32	1+22.58 Alley at Prop	328.80 327.29 C1.51		328.69 327.29 C1.40	
0+20 = CB B.C.	317.35 316.85 Co.50	317.24 316.85 Co.39		316.84 316.72 Co.12	331.48 316.72 C14.76	Alley E.C. LT.	327.17		327.19 327.17 Co.02	
# 1		316.76 316.44 Co.32		316.50 316.50 grade		1+20.59 Alley B.C. LT	327.03		327.19 327.03 Co.16	
# 2		316.75 316.16 Co.59		316.23 316.32 Fo.09						
# 3		316.34 315.84 Co.50		316.28 316.18 Co.16	(Co.12)	1+25 = W.S. AT				334.2 326.8 = 48 C7.4
# 4 = E.C. UNIV.		315.52		315.92						
						1+10	326.07		326.19 326.07 Co.12	325.74 325.57 Co.17
B.M. DIP. E/RT. ROD:				333.37	N.E. B. P 52nd + REX					

Note: grades of alley  
ref at prop. changed  
by insp. after alley  
Rets were staked  
7-25-56  
J.M.C.



REX: 52nd WLY to D.END.

STA.	Prop.	LT. CB	±	RT. (NLY) CB.	Prop.
1+25	332.52	332.67 332.52 Co.15		332.25 332.14 Co.11	332.14
1+00	333.43 332.97 Co.46	332.95 332.97 Fo.02		332.71 332.70 Co.01	334.01 332.70 C1.31
0+85 = E.V.C.	333.54 333.24 Co.30	333.10 333.24 Fo.14		333.14 333.04 Co.10	333.83 333.04 Co.79
0+65	333.45	333.23 333.45 Fo.22		333.17 333.42 Fo.25	333.42
0+45 = B.V.C.	333.58 333.36 Co.22	333.33 333.36 Fo.03		333.32 333.36 Fo.04	334.16 333.36 C.80
0+26.15 mid-brk	333.23	333.18 333.23 Fo.05		333.32 333.23 Co.09	333.23
0+07.25 = C.B. E.C. Co.61	333.71 333.10	333.10		333.10	334.2 333.10 C1.1
[For Ret's see pg 10]					
(0+00 = W. Line) 52nd					
B.M.				333.37 = N.E. B.P. Nex to 52nd	

STA.	Prop.	CB.	±	CB.	Prop.
2+45 R4. Water					329.14 329.45 F-0.31
2+44.97 = END CONST. = WLY LINE LOTS 7+10	331.42 330.35 C-1.07	331.54 330.35 C1.19	329.90	327.90 329.45 F1.55	328.25 329.45 F-1.20
2+31.62 = P.R.C.	330.59	330.59 Grade		329.92 329.73 Co.19	329.73
2+20 = C.B. B.C.	330.80	330.65 330.80 Fo.15		330.50 329.99 Co.51	329.99
2+15 = NAT. SERV. RT.					329.76 330.14 = CB Fo.38
2+10 = SEW LAT #17 RT.				329.75 323.6 ± C 6.5	329.75 325.2 Prop. C4.55
2+00	331.92 331.17 Co.75	331.16 331.17 Fo.01		330.95 330.44 Co.51	330.50 330.44 Co.06
1+75	331.62	331.75 331.62 Co.13		331.47 331.01 Co.46	331.01
1+50	333.11 332.07 C1.04	332.27 332.07 Co.20		331.75 331.57 Co.18	332.19 331.57 Co.62



52nd - REX to LANDIS

STA	Prop	LT. CB	E	CB	RT. Prop	STA	(Ely) Prop	LT. CB	E	CB	RT. Prop
0+15.75=CB	333.00	332.91				1456.28	333.19	333.17			
BC LT	333.25	333.25				Alley at Prop LT	332.77	332.77			
S'ly	Fo.3	Fo.34					Co.42	Co.40			
# 1	333.18	332.86				141.28	333.27	333.31			
		333.18				Alley at Prop LT	332.85	332.85			
		Fo.32					Co.42	Co.52			
# 2=EXIST CB	332.98	332.98				Alley E.C. LT	332.73	332.83			
								332.73			
						(Blk.3)		Co.10			
<del>E.C. REX</del>	332.77					1+39.28	332.70	332.83			
						Alley BC LT	332.70	332.70			
								Co.13			
0+08.62=S'ly											
LINE REX-Ely						1+25	332.77	332.86		332.36	
								332.77		332.28	332.28
								Co.09		Co.08	
0+05=CB BC				333.10	333.59		333.26	332.87		332.49	332.43
swly RT.				332.88	332.88	1+00	332.89	332.89		332.40	332.40
				Co.22	Co.71		Co.37	Fo.02		Co.09	Co.03 grade
# 1				333.02		0+75	333.02	333.11		332.70	
				332.94	332.94			333.02		332.53	332.53
				Co.08				Co.09		Co.17	
# 2				333.17		0+50	333.11	333.19		332.77	332.99
				333.02	333.02		333.14	333.14		332.66	332.66
				Co.15			Fo.03 grade	Co.03		Co.11	Co.33
E.C. REX				333.06							
S'ly				333.10	333.10						
				Fo.04		0+28.62 LT. only	333.25	333.13			
								333.25			
0+00=S'ly Line						0+25 RT. only		Fo.12		332.87	332.87
REX (W'ly)										332.78	332.78
										Co.09	Co.09

## 52nd - Rex to LANDS (CONT.)

13

STA.	(E4) LT.		CB.	E	RT.		STA.	LT.		E	RT.	
	Prop	CB			CB.	Prop		Prop	CB		CB	Prop
#2 END CB					330.94 331.70 Fo.76	331.70	2+80 RT ONLY	333.26	333.26		332.77 332.77 Grade	332.77
#1					331.78 331.88 Fo.10	331.88						
1+95=CB BCRT. NWLY 52nd + WIGHTMAN					331.92 331.97 Fo.05	331.34 331.97 Fo.63	2+60	332.91	332.71 332.91 Fo.20		332.56 332.42 Co.14	332.42
1+80.	332.50	332.55 332.50 Co.05			332.00 332.01 Fo.01	332.01	#2 END CB				331.61 331.80 Fo.19	331.80
							#1				332.26 332.15 Co.11	332.15
							2+55=CB.BCRT. SWLY 52nd + WIGHTMAN				332.52 332.35 Co.17	331.90 332.35 Fo.45
1+75 (cut set.)							2+40 LT. only	333.28 332.65 Co.63	332.62 332.65 Fo.03			
1+58.28 Alley B.C.LT.	332.60	332.71 332.60 Co.11					2+20 LT. only	332.50	332.63 332.50 Co.13			
Alley E.C. LT.	332.65	332.71 332.65 Co.06					2+00 = E 10 CON: Gross-GUTT.	332.65 332.45 Co.20	332.46 332.45 Co.01			
1+50 RT - only					332.06 332.15 Fo.09	331.85 332.15 Fo.30						



## 52nd - Rex to LANDIS (CONT)

15

		LT.		RT				LT.		RT.	
STA	Prop	CB	E	CB	Prop	STA	Prop	CB	E	CB	Prop
Ally F.C. LT.	332.78	332.91 332.78 Co. 13				#1	327.04	326.82 327.04 Fo. 22			
4476.83 Ally AT Prop	333.04 332.90 Co. 14	332.80 332.90 Fo. 10				5499.30 = CB, BC, LT NEly 52nd & LANDIS	326.63 327.10 Fo. 47	327.02 327.10 Fo. 08			
4461.83 Ally AT Prop	333.45 333.68 Fo. 23	333.70 333.68 Co. 02				5497.99 RT only				326.61 326.48 Co. 13	326.48
Ally F.C. LT.	333.56	333.68 333.56 Co. 12				5490	327.21	327.46 327.21 Co. 25		326.58 326.65 Fo. 07	326.65
(RICK)						5480 = W.S. RT.					325.15 327.14 = CB Fo. 99
4459.83 Ally B.C. LT.	333.62	333.68 333.62 Co. 06				5470	327.82	328.60 327.82 Co. 18		327.15 327.35 Fo. 20	327.35
4460 RT only				333.24 333.21 Co. 03	333.21	5450	329.39 328.80 Co. 59	328.68 328.80 Fo. 12		328.26 328.31 Fo. 05	327.35 328.31 Fo. 96
#2 = CB END				334.09 333.82 Co. 27	333.82	5425	330.15	330.12 330.15 Fo. 03		329.62 329.67 Fo. 05	329.67
#1				333.91 333.73 Co. 18	333.73	5400	331.97 331.50 Co. 47	331.53 331.50 Co. 03		331.01 331.03 Fo. 02	331.43 331.03 Co. 40
4455.08 CB BC RT. SWly 52nd & Tangle				333.37 333.43 Fo. 06	333.86 333.43 Co. 43	4475 RT only				332.57 332.39 Co. 18	332.39
						4478.83 Ally B.C. LT.	332.63	332.91 332.63 Co. 28			

52nd - REX to LANDIS (CONT.)

STA	(Elev)		E	CB	RT	prop	STA	(Elev)		♀	CB	RT	prop
	Prop	CB						Prop	CB				
E.C. - LANDIS -	327.90	327.90					7+69.59	338.03 331.15 C6.88	331.00 331.15 Fo.15		329.29 329.22 Co.07	330.23 329.22 C1.01	
#2	327.92	327.70 327.92 Fo.22					7+51.41	331.10	331.25 331.10 Co.13		329.29 329.05 Co.24	329.05	
#1	328.03	327.97 328.03 Fo.06					7+33.23	336.88 331.00 C5.88	331.06 331.00 Co.06		329.04 328.84 Co.20	329.27 328.84 Co.43	
6+59.10 = CB BC. LT SELY 52nd + LANDIS	329.57 328.25 C1.32	328.19 328.25 Fo.06					= END 52nd ST BEG LANDIS ST. WILLY						
6+58.90 = CB BC. WILLY C.B. LINE 52nd ST - ON RT	RT			327.43 327.02 Co.41	325.73 327.02 F1.29		7+14.15	330.60	330.90 330.60 Co.30		328.44 328.58 Fo.14	328.58	
6+49.65				327.12 326.80 Co.32	326.80								
6+35 = W.S. RT.					322.6 326.6 CB F4.0								
6+25.98				326.23 326.45 Fo.22	326.45		6+95.07	337.27 329.90 C7.37	330.22 329.90 Co.32		327.96 328.10 Fo.14	327.02 328.10 Fo.98 326.54 327.95 CB F1.41	
6+11.81 = ♀ 7' INLET RT	(See p. 20) For grades			326.35	326.35		6+91 = W.S. RT						
							6+75.99	329.00	329.01 329.00 Co.01		327.62 327.53 Co.09	327.53	
E.C. LANDIS	327.23	327.23											
#2	327.04	326.79 327.04 Fo.25					6+59.65 = Prop. B.C. 52nd. (WILLY) (6+56.90 =) ♀ B.C.						

LANDIS ST - W 'Lij

STA	Prop	LT CB	Σ	RT CB	Prop
7+16.85				325.56 325.77 Fo. 21	325.77
Req. CB on LT. AT SWLY B.C. LEMONA					
Note: END CB ON LT. here					
FOR LANDIS ST. STAS:					
Pickup on LEMONA - P. STATIONS:					
8+96.85		326.98 326.47	326.41 326.47	326.79 327.09 Fo. 30	326.69 327.09 Fo. 43
= E.C. LANDIS Co. 51					
[= P.R.C. LEMONA ON LT.]					
8+78.67		330.21 327.90 C 2.31	328.00 327.90 Co. 110	328.04 328.05 Fo. 01	327.67 328.05 Fo. 38
8+60.49	329.28		329.31 329.28 Co. 03	328.73 328.80 Fo. 07	328.80
8+42.31	333.59 330.12 C 3.47	330.00 330.12 Fo. 12		329.26 329.20 Co. 06	329.50 329.20 Co. 30
8+24.13	330.68	330.68 330.68 grade		329.27 329.38 Fo. 11	329.38
8+05.95	336.61 330.96 C 5.65	330.89 330.96 Fo. 07		329.54 329.45 Co. 09	330.38 329.45 Co. 93
7+87.77	336 331.12	331.10 331.12 Fo. 02		329.39 329.38 Co. 01	329.38

STA	Prop	LT CB	Σ	RT CB	Prop
10+36.85	318.26	318.28 318.26 Co. 02			317.92 317.94 Fo. 02
10+16.85	319.44 319.35 = B.V.C Co. 09	319.23 319.35 Fo. 12			319.08 319.16 Fo. 08 C 3.27
E.C. LEMONA	319.80	319.62 320.00 Fo. 38			
# 2	320.34	319.83 320.34 Fo. 51			
# 1	320.19	320.09 320.19 Fo. 10			
10+05.14 = CB	320.02 320.05	319.92 320.05			
BC. SWLY LEMONA LANDIS	Fo. 03 grade	Fo. 13			
7+91.85 RT ONLY		320.60 320.81 Fo. 21	320.78 320.81 Fo. 03 grade		
7+66.85 RT ONLY		322.48 322.47 Co. 01	322.47		
7+41.85 RT ONLY		323.94 324.12 Fo. 18	324.39 324.12 Co. 27		

Sc. T. P. M

320.55 = chd WALK N.E. Corn 9th AT = 51.59 LANDIS (SWLY LANDIS & LEMONA)

LANDIS-W'ly (Cont.)

STA	Prop	CB	E	CB	prop
12+25	316.80 315.05 C 1.75	314.99 315.05 Fo.06		314.31 314.45 Fo.14	315.01 314.45 Co.56
12+00	315.17	315.15 315.17 Fo.02		314.56 314.57 Fo.01	314.57
11+75	317.02 315.30 C 1.72	315.16 315.30 Fo.14		314.73 314.70 Co.03	315.37 314.70 Co.67
11+50	315.43	315.17 315.43 Fo.26		314.77 314.83 Fo.06	314.83
11+36.85 = E.V.C	316.84 315.50 C 1.34	315.58 315.50 Co.08		314.31 314.90 Fo.59	315.27 314.90 Co.37
11+16.85	315.69	315.84 315.69 Co.15		314.83 315.10 Fo.27	315.10
10+76.85	316.72 316.06 Co.66	315.90 316.06 Fo.16		315.46 315.50 Fo.04	319.45 315.50 C 3.95
10+76.85	316.61	316.35 316.61 Fo.26		316.04 316.12 Fo.08	316.12
10+76.85 = SW LAT #18 RT			315.21 stub 309.4 C 5.81	315.21 stub 311.1 prop C 4.11	
10+71.85 = W.S RT				315.31 stub 316.32 = CB	
10+56.85	317.62 317.34 C 0.28	317.16 317.34 Fo.18		316.97 316.92 Co.05	320.58 316.92 C 3.66

STA	prop	CB	E	CB	prop
13+32.77 = E 10' Cross-GOTT	317.5 314.50 C 3.0	314.61 314.50 Co.11		313.75 313.82 Fo.05 11' cross-GOTT	314.05 312.30 C 1.75 312.94 313.00 Fo.06
13+20.52	314.55	314.12 314.55 Fo.43			313.41 313.50 Fo.09 313.59 313.75 Fo.16
CONT. CB, LTI END CB LANDIS ON RT.					end. cont. as per plan 313.75 # 3
(Extend Pav Along N'ly Line Landis, Proj. W'ly)					
				313.75 313.60 Co.15	313.75 313.90 Fo.15 313.80 313.95 Fo.15
				grade Pav. 12+52 11' E GOTT.	313.90 # 2 # 1
13+12.13 CB, B.C. RT. NEW ALTADENA & LANDIS	317.48 314.60 C 2.88	314.27 314.60 Fo.33			313.99 314.00 Fo.01 314.64 314.00 Co.64
13+00	314.66	314.63 314.66 Fo.03			313.96 314.06 Fo.10 314.06
12+75	317.46 314.79 C 2.67	314.78 314.79 Fo.01			314.12 314.19 Fo.07 315.15 314.19 Co.96
12+50	314.92	314.96 314.92 Co.04			314.24 314.32 Fo.08 314.32

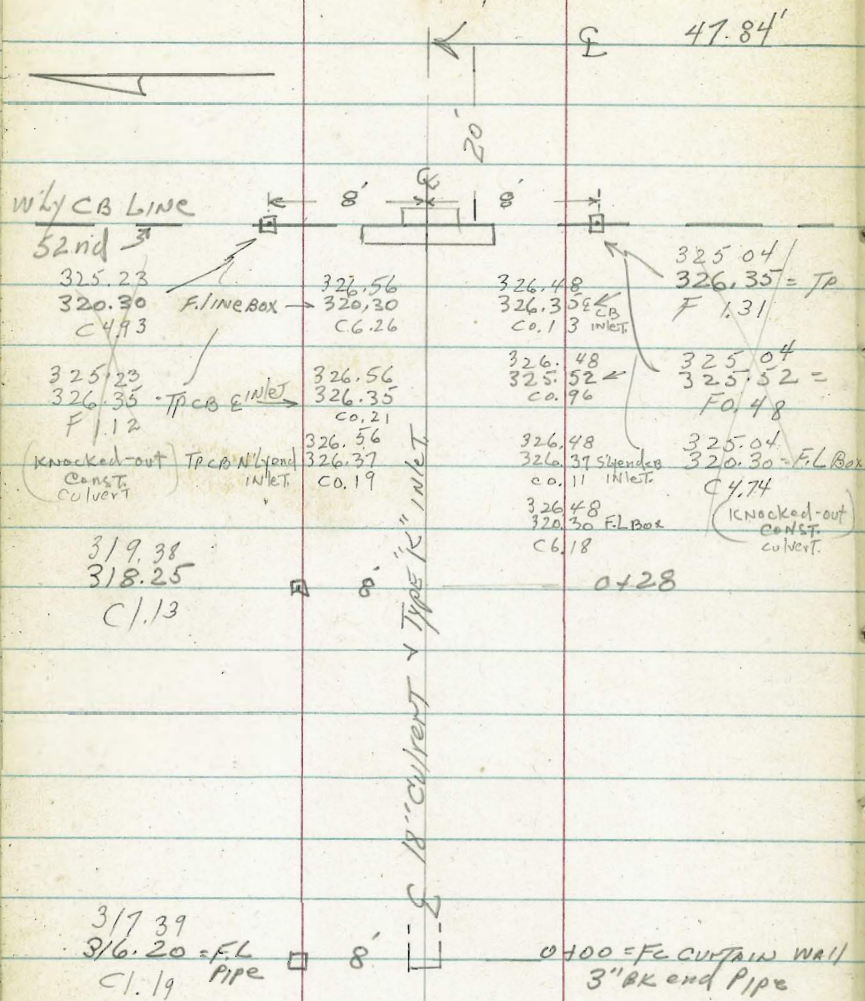
CB, RT, RT (W'ly)

E.C.  
ON  
ALTADENA  
RT.





TYPE "K" CB INLET & 56' Culvert  
52nd & LANDIS



S.C.

325.04 / 326.35 = TP CB INLET 326.37 = TP CB east end INLET  
 F 1.31  
 325.04 / 325.52 = 60' E INLET (GRATE) 325.54 = 60' end's INLET  
 F 0.48  
 325.04 / 320.30 = F.L. Box  
 C 4.74  
 (Knocked-out CONST. Culvert)

80' STORM DRAIN - EXTENDED W/ly  
 LANDIS & 52nd - See opp. pg.  
 Ref. DWG: 6194-B

0+80 = W/ly end EXIST 18" pipe (See opp. pg.)  
 0+40  
 0+00 = W/ly end EXIST (80' 18" pipe)  
 Meet F.L. INLET  
 316.20 = F.L. WE  
 315.39  
 314.10  
 C 1.29 F.L. INLET  
 312.74  
 312.00 = F.L. INLET  
 Co. 74

Note: See opp. pg. For EXT. OF DRAIN W/ly 80' →

LANDIS ST. - 52nd, Ely to OGDEN

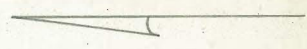
STA.	(N'ly) LT.		E	RT	
	Prop	CB		CB	Prop
1+00	331.69 332.00 Fo. 31	331.62 332.00 Fo. 38		331.97 332.50 Fo. 53	334.11 332.50 C 1.61
0+80 = E.V.C.	330.35 330.50 Fo. 15	330.15 330.50 Fo. 35		330.48 331.00 Fo. 52	332.70 331.00 C 1.70
0+60	329.16	328.91 329.16 Fo. 25		329.19 329.66 Fo. 47	329.66
0+40	327.87 328.15 Fo. 28	328.06 328.15 Fo. 09		328.43 328.63 Fo. 20	329.52 328.63 C 0.89
0+20	327.46	327.28 327.46 Fo. 18		327.79 328.00 Fo. 21	328.00
0+07.24 = CE BC, LT.	326.96 327.23 Fo. 77	326.95 327.23 Fo. 28			
0+07.19 = CB EC, RT				327.46 327.90 Fo. 44	327.72 327.90 Fo. 18 <small>IRLIN CONC. WALL</small>
0+00 = E. Line 52nd For Ret's 50-1916					
Set T.B.M.				330.47	SELY CB RADIUS PT. (2x2)

STA.	LT.		E	RT	
	Prop	CB		CB	Prop
3+00	347.25 343.33 C 3.92	343.26 343.33 Fo. 07			343.18 342.97 C 0.21
2+80 = E.V.C.	346.55 343.05 C 3.50	342.78 343.05 Fo. 27			342.66 343.18 Fo. 52 344.69 343.18 C 1.51
2+60	342.62	342.09 342.62 Fo. 53			342.56 342.89 Fo. 33
2+40	343.25 341.89 C 1.36	341.36 341.89 Fo. 53			342.00 342.18 Fo. 18 342.63 342.18 C 0.45
2+23 = SOW LAT #15 LT.	340.87 336.00 Prop C 4.87 Prop	340.53			340.60 341.35 Fo. 75
2+20	340.85	340.48 340.85 Fo. 37			340.60 341.35 Fo. 75
2+00 B.V.C.	339.84 337.50 C 0.34	339.22 339.50 Fo. 28			339.35 340.00 Fo. 65 339.78 340.00 Fo. 22
1+75	337.62	337.42 337.62 Fo. 20			337.61 338.12 Fo. 51 338.12
1+50	335.28 335.75 Fo. 47	335.49 335.75 Fo. 26			335.01 336.25 Fo. 44 336.28 336.25 C 0.03 grade
1+25	333.87	333.57 333.87 Fo. 30			333.61 334.37 Fo. 76 334.37



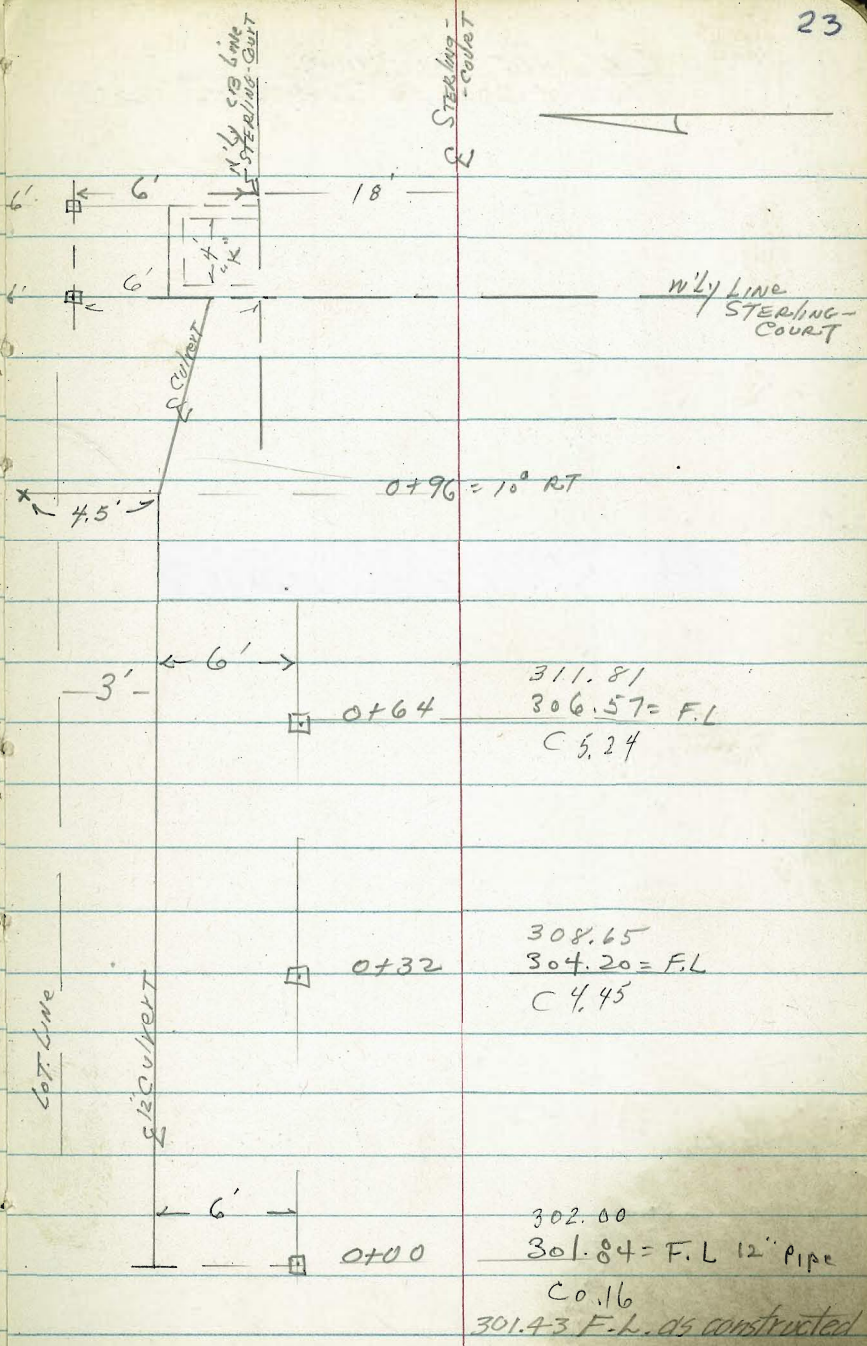
Ref: 5622-B  
3068-B

# CB Inlet & Culvert WLY END STERLING-COURT



1+13.82 Ely edge Box	314.44 313.00 TPCB C 1.44	314.44 309.86 = FL C 4.58
1+08.48 = WLY Edge Box	314.23 312.70 TPCB C 1.53	314.23 309.86 = FL C 4.37

Set chx tp wall 315.99  
308.94 = FL  
C 7.05



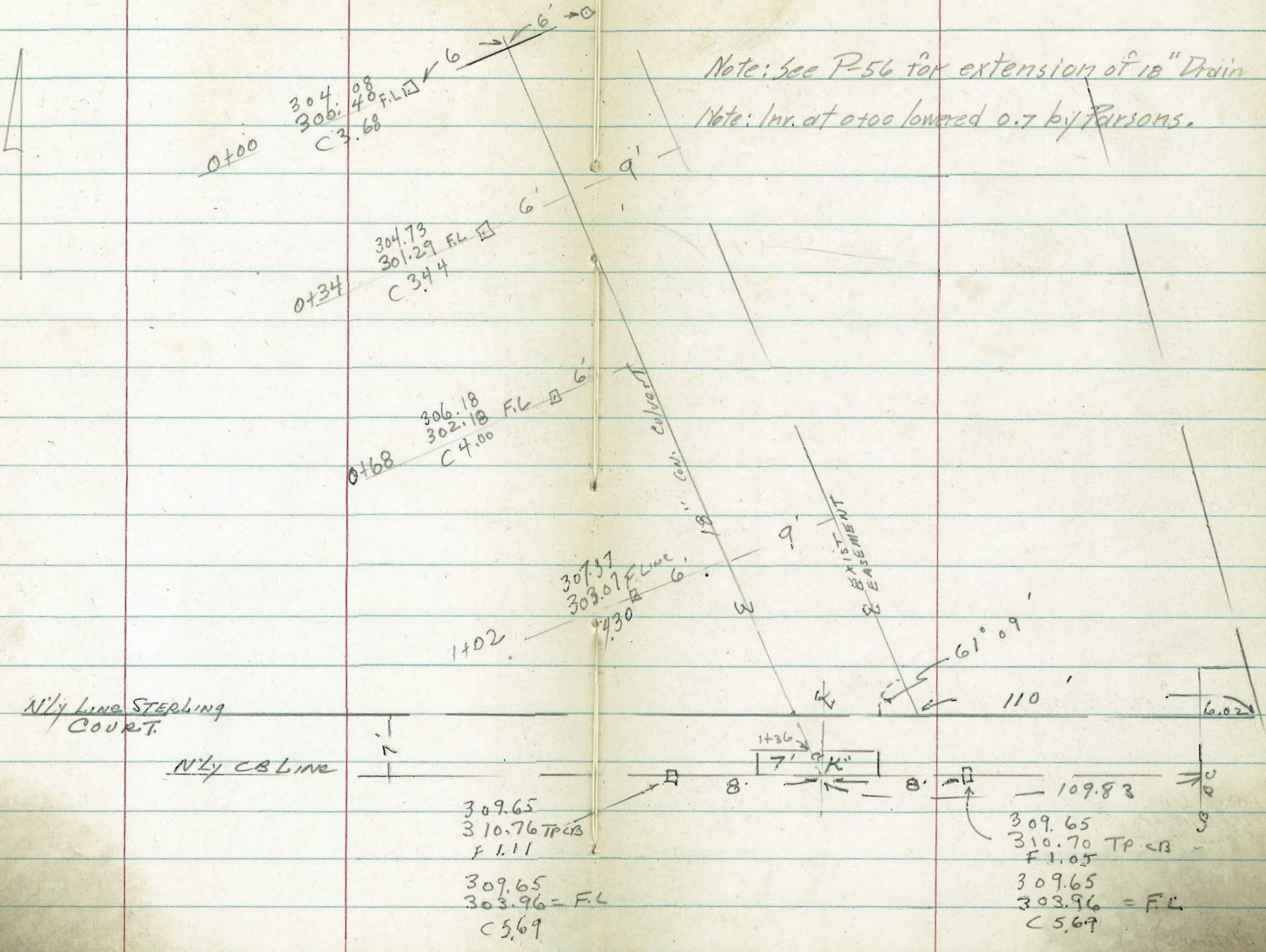
Set T.B.M

318.27 = NW CORN  
CON. POINT  
at 5015 STERLING-COURT WLY

302.00  
301.84 = F.L 12" Pipe  
C 0.16  
301.43 F.L. as constructed

Ref. 5623-B  
3068-D

CB Inlet & Culvert  
N<sup>1/4</sup> of Sterling Court 110' WLY  
OF ALTADENA AVE



Note: see P-56 for extension of 18" Drain  
Note: Inr. at 0+00 lowered 0.7 by Parsons.

N<sup>1/4</sup> Line Sterling Court

N<sup>1/4</sup> CB Line

309.65  
310.76 TP CB  
F 1.11  
309.65  
303.96 = FL  
C 5.69

309.65  
310.70 TP CB  
F 1.05  
309.65  
303.96 = FL  
C 5.69

STERLING-COUNT  
ALTADENA, ELY TO LEMONA

STA	LT.			RT			STA	LT.			RT		
	Prop	CB	Σ	CB	Prop			Prop	CB	Σ	CB	Prop	
1+03	317.72 317.79 Fo.09	317.58 317.79 Fo.21		317.13 317.40 Fo.27	317.38 317.40 Fo.02		2+70.76= CB BC RT. (SW'LY 51ST) STERLING				310.97 310.90 Co.07	312.92 310.90 C 2.02	
0+83	317.74	317.43 317.74 Fo.31		317.03 317.34 Fo.31	317.34		2+50	311.66 312.13 Fo.47	312.01 312.13 TP Fo.12		311.97 311.89 Co.08	313.62 311.89 C 1.73	
0+63=B.V.C	317.92 317.39 Co.53	317.26 317.39 Fo.13		317.00 317.09 Grade	316.94 317.00 Fo.06		2+25	313.32	313.63 313.32 Co.31		313.05 313.04 Co.01	313.04	
0+36	316.74	316.65 316.74 Fo.09		316.51 316.35 Co.16	316.35		2+00	313.36 314.50 F 1.14	314.69 314.50 Co.17		314.39 314.19 Co.20	315.05 314.19 C 0.86	
0+09.09=C.B.A.C. (S'ELY) RT	316.10	315.93 316.10 Fo.17		315.70	316.14 315.70 Co.44		1+75	315.67	315.60 315.67 Fo.07		315.25 315.34 Fo.09	315.34	
							1+63=E.V.C	314.88 316.24 F 1.36	315.99 316.24 Fo.25		315.72 315.89 Fo.17	316.23 315.89 Co.34	
0+00.99=C.B.A.C. (NE'LY) LT.	317.05 315.90 C 1.15	315.90					1+43	315.71 317.04 F 1.33	316.58 317.04 Fo.46		316.64 316.67 Fo.03	317.33 316.67 C 0.66	
0+00=E LINE ALTADENA ATE STERLING CT.							1+23	317.56	317.24 317.56 Fo.32		317.01 317.18 Fo.17	317.18	
(E STATIONS)							1+13	305.71 317.71 F 2.00	317.56 317.71 Fo.15		317.11 317.32 Fo.21	317.33 317.32 Co.01	

STERLING-CT. E'ly (CONT.)

STA	Prop	CB	E	CB	prop	STA	Prop	CB	E	CB	Prop
# 3 = EC 51ST				310.06 309.70 Co. 36		# 2 RT				302.91	302.91
# 2				309.42 309.00 Co. 42		# 1 RT				303.41 303.22 Co. 19	303.22
# 1				308.49 308.42 Co. 07		4+68.34 CB BC RT (swly)	304.40	304.51 304.40 Co. 11		303.56 303.60 Fo. 04	301.68 303.60 F 1.72
3+30.75 = CB B.C. RT (SE'ly 51ST) STERLING				307.90 308.00 Fo. 10	308.14 308.00 00.14	4+50	303.99 304.80 Fo. 81	304.78 304.80 Fo. 02		303.94 304.12 Fo. 18	302.79 304.12 F 1.33
3+23 LT only B.V.C.	309.34 308.69 Co. 65	308.75 308.69 Co. 06				4+25	305.38	305.30 305.38 Fo. 08		304.74 304.85 Fo. 11	304.85
3+00 LT only	310.42 309.77 Co. 65	309.77 309.77 Grade				4+03 = E.V.C.	305.40 305.89 Fo. 49	305.81 305.89 Fo. 08		305.42 305.49 Fo. 07	303.97 305.49 F 1.52
2+75 LT only	310.95	310.96 310.95 Co. 01				3+83	306.40	306.46 306.40 Co. 06		305.85 306.00 Fo. 15	306.00
EC 51ST				310.31 310.50 Fo. 19		3+63	307.85 307.05 Co. 80	307.16 307.05 Co. 11		306.61 306.65 Fo. 04	306.11 306.65 Fo. 54
# 2				310.14 310.32 Fo. 18		3+43	307.81	308.03 307.81 Co. 22		306.97 307.41 Fo. 44	307.41
# 1				311.03 310.51 Co. 52							

(N4) LT.

RT.

STERLING - CT. Ely (CONT.)

(NW) LT

Pop

CB

E

CB

RT

Pop

W.S  
5105.7 RT

302.3  
302.4 CB  
Fo.1

#3 = E.C  
Lemona  
(NW)

305.39

305.35  
305.39  
Fo.04

#2

304.76

304.91  
304.76  
Co.15

#1

304.22

304.25  
304.22  
Co.03

Co.32  
4481.23 = CB  
BC. LT

303.75  
304.10  
Fo.35

304.36  
304.10  
Co.26

302.74  
303.16  
Fo.22

(767' E 1/4)  
60TH

#3 = END OF  
CB AT  
S. LINE

302.66  
302.60  
Co.06

302.47  
302.60  
Fo.13



51' ST.

STERLING CT. S'y to D. END

STA	(Ely) - LT		RT	
	Prop	CB	E	Prop
1+20	321.62	321.56 321.62 F0.06	322.19 322.12 C0.07	322.12
1+00	319.70 320.35 F0.65	320.11 320.35 <sup>FP</sup> F0.24	320.71 320.85 F0.14	322.73 320.85 C1.88
0+80	318.56	318.09 318.56 F0.47	319.11 319.06 C0.05	319.06
0+60 = B.V.C	314.14 316.28 F2.14	315.95 316.28 F0.33	316.33 316.78 F0.45	316.82 316.78 C0.04
0+50	315.01	314.68 315.01 F0.33	315.02 315.52 F0.50	315.52
0+25	311.84	311.78 311.84 F0.06	312.00 312.36 F0.36	312.36
0+13 RT only			310.69 310.85 F0.16	310.85
0+08 = CB E.C (For Ret's See Pgs 25-26)	308.81 309.70 F0.89	309.70	310.01 310.50	313.23 310.50 C2.73
(0+00 = S. Line STERLING CT.)				

28

LT

RT

STA	Prop	CB	E	CB	Prop
3+01 = Sew LAT # 5 RT	(CON. ENCLOS.)		318.4 312.38 C6.1		318.42 313.00 PL C5.42
3+00	311.73 314.19 F2.46	313.86 314.19 F0.33		314.32 314.70 F0.38	318.42 314.70 C3.72
2+80	316.03	315.70 <sup>FP</sup> 316.03 F0.33		316.39 316.53 F0.14	316.53
2+60 = B.V.C	316.34 317.62 F1.28	317.22 317.62 F0.40		318.10 318.12 F0.02	320.05 318.12 C1.93
2+40	319.08	318.89 319.08 F0.19		319.56 319.58 F0.02	321.65
2+20 = E.V.C	320.21 320.54 F0.33	320.14 320.54 F0.40		320.94 321.04 F0.10	322.60 321.04 C1.56
2+00	321.75	321.48 321.75 F0.27		321.52 322.25 F0.73	322.25
1+80	322.13 322.45 F0.32	322.00 322.45 F0.45		322.38 322.95 F0.57	325.35 322.95 C2.40
1+60	322.76	322.31 322.76 F0.45		322.85 323.26 F0.41	323.26
1+40	322.34 322.39 F0.05	322.18 322.39 F0.21		322.71 322.89 F0.18	325.24 322.89 C2.35

## 51 ST. (CONT.)

29

STA.	Prop	CR	Σ	CR	prop
(3+60.13 F.B. 2105)					
3+59.98=END	302.40	306.78		308.86	306.35
CONST.	307.30	307.30		307.80	307.80
	F4.90	F0.52		C1.06	F1.45
3+40	306.40	309.50		310.29	311.45
	309.75	309.75		310.27	310.27
	F3.35	F0.25		C0.02	C1.18
3+30=N.S. SERV.	307.1				
LT	311.0 CR				
	F3.9				
3+20	312.10	311.70		312.13	312.60
		312.10		312.60	
3+15=N.S. RT		F0.40		F0.47	316.1
					313.2 CR
					C2.9

LEMONA AVE  
STERLING COURT - N'y to LANDIS

STA.	Prop	CB	E	CB	Prop
1+00	306.27				306.76
0+90 = N.S. RT					310.9 306.1 CB C 4.8
0+89.45	305.58				309.79 306.08 C 3.71
0+86.40 = CB, EC LT (NW'y Lemona + Sterling Ct.)	305.57 305.39 C 0.18				
0+74.02 RT only					305.12
0+50 RT only					307.37 303.55 C 3.82
0+25 RT only					302.03
0+00 = Beg CB, RT (E'y) only				300.48	306.15 300.48 C 5.87 5.67
(0+00 = Sly Line of Sterling Court & Ely B. Line LEMONA)					

1+14

CB Grades LEMONA

STA.	LT.	E	RT
2+49.69	315.89 316.02 Fo.13		316.22 315.94 Co.28
2+29.76	314.27 314.69 Fo.42		314.89 314.65 Co.24
2+09.83= B.C. LEMONA	312.96 313.37 Fo.41		313.63 313.37 Co.26
2+00	312.41 312.71 Fo.30		313.08 312.80 Co.28
1+75	311.04 311.09 Fo.05		311.56 311.40 Co.16
1+50	309.58 309.47 Co.11		310.02 310.01 Co.01
1+25	308.01 307.85 Co.16		308.71 308.61 Co.10
1+00	306.26 306.23 Co.03		307.12 307.22 Fo.10
0+89.45	305.52 305.58 Fo.06		306.44 306.63 Fo.19
0+86.40 =CB, EC, LT. only	305.35 305.39 Fo.04		
0+74.02 RT. only			305.59 305.77 Fo.18
0+50 RT. only			304.04 304.43 Fo.39
0+25 RT. only			302.83 303.03 Fo.20
0+00 - Beg CB RT - Ely			303.07 301.64 C1.43

↑  
-0.5642

↑  
-0.782

↑  
-0.06472

↑  
-0.550

CB Grades - LEMONA

LT

E

RT

4+08.95=EC  
LEMONA  
A+L AND IS

3+84.08  
RT only

3+59.21  
RT only

3+34.34  
RT only

3+09.47=CB  
EC LT

2+89.55

2+69.62

319.62  
320.00  
Fo.38

318.32  
318.67  
Fo.35

317.19  
317.34  
Fo.15

326.41  
~~326.89~~  
326.47  
~~Co.42~~  
Fo.06

Knocked-out 324.87 324.74  
324.81 324.81 ↑  
Co.06 Fo.07

323.06  
323.14  
Fo.08

321.70  
321.47  
Co.23

319.99  
319.80  
Co.19

318.96  
318.51  
Co.45

317.56  
317.22  
Co.34

5180.00

LEMONA AVE

STERLING COURT - N'ly to LANDIS

STA.	Prop	CB	±	CB	Prop	STA	Prop	CB	±	CB	Prop
1+00	306.27				306.76						
						2+49.69	318.26 315.79 C 247				318.53 316.19 C 234
0+90 = W.S. RT					310.9 306.1 CB C 4.8						
					309.79	2+29.76	314.45				314.90
0+89.45	305.58				306.08 C 3.71	5 ft 5 ft 2) ± Acc = 19.93 ± Chg = 19.89 5' + 2.51' = def.					314.58 313.62 C 0.96
	305.57 0+86.40 = CB, EC LT (NW 1/4 Lemona + Sterling Ct.)	305.39 C 0.18				2+07.83 = B.C. LEMONA	313.69 313.12 C 0.57				
0+74.02 RT only					305.12	2+00	312.50				313.00
0+50 RT only					307.37 303.55 C 3.82	1+84 = W.S. LT.					312.1 = CB
0+25 RT only					302.03						
0+00 = Beg CB RT (± 24) on hwy				300.48	306.15 300.48 C 5.83 5.67	1+75	311.54 310.94 C 0.60				314.48 311.44 C 3.04
						1+50	309.38				309.88
						1+25	307.52 307.82 F 0.30				311.62 308.32 C 3.30
						1+14 = W.S. LT.	307.02 307.10 F 0.08				

(0+00 = S'ly Line  
of Sterling Court  
& E'ly CB Line  
LEMONA)

LEMONA (CONT.)

4+0895=  
E.C

326.47

3+87.08  
RT. only

327.86

3+59.21  
RT. only

324.44  
323.26  
C 1.18

3+34.34  
RT. only

321.65

DIV. 4 PTS  
2 1/4" = 140.15"

3+09.47=C.B  
B.C.L.T.

320.67  
319.80  
C 0.87

323.23  
320.05  
C 3.18

2+89.55

320.34  
318.46  
C 1.88

322.14  
318.76  
C 3.38

2+69.62

317.12

317.47







## ALTA DENA (CONT.)

LT.

RT.

STA.	P.L.	CB	Q	CB	P.L.	STA.	P.L.	CB	Q	CB	P.L.
5+66.10 = EC	319.44 314.88	314.96 314.88									
ALTA DENA LT only	C456	Co.08				6+56.10	319.62	319.65 319.62 Co.03			319.03 318.89 Co.14
5+56.10 LT only	314.57	314.78 314.57 Co.21				6+36.10	321.90 318.27 C3.63	318.28 318.27 Co.01			317.46 317.54 Fo.08
5+36.10 LT only	318.11 314.14 C3.97	314.64 314.14 Co.50				6+16.10	317.06	316.88 317.06 Fo.18			315.74 316.17 Fo.43
5+16.10 LT only	313.86	314.07 313.86 Co.21									
						CB E.C. on Sterling					T.P. 313.32 313.40 Fo.08
CB. E.C. on Sterling				312.30 312.20 Co.10		#2					313.71 313.78 Fo.07
						#1					315.05 314.28 Co.77
#2				312.62 312.38 Co.24							314.89 314.90 Fo.01
						5+97 = CBB RT Lewis -					316.69 314.90 C1.79
#1				312.78 312.44 Co.34		5+76.10 LT only	320.63 316.04 C4.59	316.08 316.04 Co.04			
5+29.88 CB BC RT. ALTA DENA NW on Sterling				312.64 312.51 Co.13	313.32 312.51 Co.81	5+76.10 LT only	315.21	315.28 315.21 Co.07			

ALTADENA (CONT.)

STA	P.L	CB	E	EB	P.L	STA	P.L	CB	E	CB	P.L
						9+75	323.20 321.38	321.01 321.38		320.46 320.78	323.20 320.78
7+62.88	325.20	324.67 325.20 Fo.53		323.79 324.44 Fo.65	324.44	9+53.7 = W.S LT.	C1.82 324.04 322.06 C1.78	Fo.37		Fo.32	C2.42
<small>Rough grade &amp; fobs W.S. Set 5' from prop on E by side - main set on West.</small>						9+50	322.18	321.86 322.18 Fo.32		321.35 321.56 Fo.21	321.56
7+57.40 = E.C. ALTADENA	327.86 325.08 C2.78	324.66 325.08 Fo.42		323.41 324.29 Fo.88	327.86 324.29 C3.57	9+25	325.00 322.99 C2.01	322.71 322.99 Fo.28		322.20 322.33 Fo.13	325.10 322.33 C2.67
7+43.7 = W.S LT.	327.77 324.63 C3.14					9+00	323.79	323.50 323.79 Fo.29		323.15 323.10 C0.05	323.10
7+42.88	324.60	324.39 324.60 Fo.21		323.24 323.83 Fo.59	323.83	8+83.7 = W.S LT.	C1.3 + 0.08				
						8+82.88 = E.C.	325.64 324.35 C1.29	323.88 324.35 Fo.47		323.55 323.64 Fo.09	325.64 323.64 C2.00
7+22.88	323.77	323.69 323.77 Fo.08		322.74 323.00 Fo.26	323.00	8+62.88	325.06	324.51 325.06 Fo.55		324.18 324.30 Fo.12	324.30
7+16.55	326.56 323.48 C3.08	323.61 323.48 C0.13		322.46 322.66 Fo.20	326.56 322.66 C3.90	8+42.88	326.58 325.52 C1.06	324.89 325.52 Fo.63		324.58 324.76 Fo.18	326.58 324.76 C1.82
7+02.88	322.72	323.02 322.72 C0.30		321.62 321.97 Fo.35	321.97	8+22.88	325.76	325.05 325.96 Fo.11		324.59 325.00 Fo.41	325.00
6+82.88	321.47	321.57 321.47 C0.10		320.67 320.72 Fo.05	320.72	8+13.7 = W.S LT.	326.94 325.77 C1.17				
6+75.9 ± = B.C. (RT.) ALTADENA	323.50 320.98 C2.52	321.00 320.98 C0.02		320.32 320.24 C0.08	321.94 320.24 C1.70	8+02.88	327.36 325.79 C1.57	325.17 325.79 Fo.62		324.63 325.03 Fo.40	327.36 325.03 C2.33
CHK.						7+82.88	325.60	324.92 325.60 Fo.68		324.32 324.84 Fo.52	324.84

326.30 = 2" Pipe 6' RT Ely Line F.B. 2296  
ALTADENA ON S. Line OAK PARK ANNEX

ALTADENA (CONT.)

Set T.B.M

310.80 ± 50' 2x2R.P 36

ELY 8 on Sub Line  
At 6 ELY Lin e ALTADENA

STA = APPROX 13+86

ELY LT				RT		ELY RT						
STA.	P.L	CB	±	CB	P.L	STA.	P.L	CB	±	CB	PT	P.L
11+92.88	312.38 314.13 F1.75	314.03 314.13 Fo.10		314.20 314.27 Fo.07	312.38 314.27 F1.89	13+86.73 = = mid-pt curve	312.16 312.49 Fo.33	312.23 312.49 Fo.26		312.16 312.71 Fo.55	PT	312.16 312.71 Fo.01 Grade
11+72.88	314.68	314.62 314.68 Fo.06		314.61 314.73 Fo.12	314.73	13+69.01	312.58	312.44 312.58 Fo.14		312.27 312.80 Fo.53		312.80
11+52.88 = B.P.C	314.25 315.35 F1.10	315.00 315.35 Fo.35		315.07 315.28 Fo.21	314.25 315.28 F1.03	13+51.49	312.66	312.53 312.66 Fo.13		312.67 312.89 Fo.22		312.89
11+27.98	316.26	315.76 316.26 Fo.50		315.90 316.06 Fo.16	316.06	13+34.22 nly 13+33.82 = B.C (LT.) ALTADENA	310.21 312.74 F2.53	312.50 312.74 Fo.24		312.86 312.98 Fo.12		310.21 312.98 F2.77
11+02.88 only LT.	318.75 317.17 C1.58	316.79 317.17 Fo.38		316.85 316.92 Fo.07	318.75 316.92 C1.83	13+25	312.79	312.52 312.79 Fo.27		312.89 313.03 Fo.14		313.03
11+00 RT only												
10+82.88 only LT.	317.88	317.13 317.88 Fo.75		317.43 317.69 Fo.26	317.69	13+00	310.04 312.94 F2.90	312.73 312.94 Fo.21		312.82 313.18 Fo.36		310.04 313.18 F3.14
10+75 RT only												
10+62.88 LT only	320.62 318.55 C2.07	317.89 318.55 Fo.66				12+75	313.09	312.96 313.09 Fo.13		313.02 313.33 Fo.31		313.33
10+58.7 = W.S LT.	320.85 318.65 C2.20											
10+50	318.96	318.58 318.96 Fo.38		318.15 318.47 Fo.32	318.47	12+52.88 = E.V.C	310.02 313.23 F3.21	313.16 313.23 Fo.07		313.26 313.47 Fo.21		310.02 313.47 F3.45
10+25	322.42 319.77 C2.65	319.24 319.77 Fo.53		319.08 319.24 Fo.16	322.42 319.24 C3.18	12+32.88	310.88 313.41 F2.53	313.14 313.41 Fo.27		313.52 313.64 Fo.12		310.88 313.64 F2.76
10+23.7 = W.S LT. + RT	322.56 319.84 C2.72											
10+00	320.57	320.13 320.57 Fo.44		319.61 320.01 Fo.35	320.01	12+12.88	313.65 313.72 Fo.07	313.65 313.72 Fo.07		313.88 313.91 Fo.03		313.91

## ALTA DENA (CONT.)

STA.	P.L.	CB	E	CB	P.L.
15+67.60	314.97 311.60 C 2.37	311.31 311.60 F 0.29		311.39 311.80 F 0.41	314.07 311.80 C 2.27
15+50	311.68	311.61 311.68 F 0.07		311.80 311.88 F 0.08	311.88
15+25	315.81 311.81 C 4.00	311.88 311.81 C 0.07		311.72 312.01 F 0.29	315.81 312.01 C 3.80
15+00	311.93	311.82 311.93 F 0.11		311.86 312.13 F 0.27	312.13
14+75	312.94 312.06 C 0.88	311.66 312.06 F 0.40		312.04 312.26 F 0.22	312.94 312.26 C 0.68
14+50	312.18	311.98 312.18 F 0.20		312.22 312.38 F 0.16	312.38
14+39.52 E/C ALTA DENA	312.53 312.24 C 0.29	311.98 312.24 F 0.26		312.02 312.44 F 0.42	312.53 312.44 C 0.09
14+21.96	312.33	312.10 312.33 F 0.23		312.07 312.53 F 0.46	312.53
14+04.35	312.41	312.02 312.41 F 0.39		312.24 312.62 F 0.38	312.62

STERLING COURT - ALTADENA WLY to D. END

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
1+15.85 = E INLET 4 E 10' CROSS GUTT.		311.74 311.70 C 0.04	310.54 310.70 (Stop) F 0.16			2+25 = W.S. LT.	315.2 313.7 CB C 1.5				
1+11.66 = ELY TYPE K INLET RT.			310.18 303.96 FL C 6.22 Box	310.18 310.70 CB F 0.52		2+20 = Sew LAT #4 LT.	315.2 308.6 P.L. C 6.6		315.2 306.1 E C 9.1		
1+00	312.56 311.71 C 0.85	311.86 311.71 C 0.15		310.48 310.73 F 0.25	309.12 310.73 F 1.61	2+00	313.77 313.09 C 0.68	312.84 313.09 F 0.25		312.17 312.50 F 0.33	310.84 312.50 F 1.66
0+90 = Sew LAT #2 LT.	313.5 306.8 P.L. C 6.7		313.5 305.2 E C 8.3								
0+80	312.56 311.88 C 0.22	311.86 311.88 C 0.22		310.60 310.85 F 0.25	309.12 310.85	1+80 = EVC	312.60 312.57 C 0.03	312.37 312.57 F 0.20		311.84 311.89 F 0.04	310.06 311.88 F 1.82
0+60 = B.V.C	313.80 312.20 C 1.60	312.40 312.20 C 0.20		311.09 311.16 F 0.08	310.18 311.16 F 0.98	1+60	312.49 312.12 C 0.37	312.08 312.12 F 0.04		311.16 311.34 F 0.18	309.62 311.34 F 1.72
0+45 = Sew LAT #1 LT.	315.4 307.4 P.L. C 8.0		315.4 304.8 E C 10.6								
0+50	312.56 312.40 C 0.18	312.58 312.40 C 0.18		311.40 311.36 C 0.04	311.36	1+40	312.88 311.83 C 1.05	311.85 311.83 C 0.02		310.68 310.97 F 0.29	309.08 310.97 F 1.89
0+25	312.90	313.06 312.90 C 0.16		311.97 311.84 C 0.13	311.84	1+30 RT. ONLY				310.52 310.85 F 0.33	310.85
0+06.02 = CB. E.G. RT				312.20	313.43 312.20 C 1.23	1+30 = W.S LT	313.3 311.8 CB C 1.5				
0+15 LT Only	313.10	313.13 313.10 C 0.03									
0+05.5 CB EC LT.	316.11 313.40 C 2.71	313.32 TP 313.40 F 0.08				1+25 = Sew LAT #3 LT.	313.3 306.7 AL C 6.6		313.3 305.4 E C 7.9		
0+00 = WLY line ALTADENA						1+20 = WLY END "K" INLET RT.	311.70 311.70 Grade	311.70 311.70		309.46 307.93 = GUT F 0.41	309.46 310.76 CB F 1.30

STERLING CT. WLY (Cont.)

LT					RT (WLY)		LT.			RT WLY		
STA.	P.L.	CB	E	CB	P.L.	STA	PL	CB	E	CB	P.L.	
						# 2				315.66		
										315.78	315.78	
										Fo. 12		
1 4+00	317.04	317.24 317.04 Co.20		317.01 317.41 Fo.40	317.41							
						# 1				315.06		
										315.30	315.30	
										Fo.24		
1 3+80	317.30 317.22 Co.08	317.13 317.22 Fo.09		317.36 317.56 Fo.20	317.98 317.56 Co.42							
						4+65 = CB.80 RT				314.71	316.14	
										314.84	314.84	
										Fo.13	C 1.30	
c 3+60	317.12	316.59 317.12 Fo.53		317.22 317.39 Fo.17	317.39							
						4+60 LT. only	314.60	314.74				
							314.82	314.82				
							Fo.22	Fo.08				
c 3+40=B.V.C	317.54 316.74 Co.80	316.59 316.74 Fo.15		317.04 316.91 Co.13	317.47 316.91 Co.56							
						4+40 LT only	315.84	316.14				
								315.84				
								Co.30				
c 3+25	316.35	316.38 316.35 Co.03		316.63 316.43 Co.20	316.43							
						4+20 LT. only	316.54	316.58				
							316.58	316.58				
							Fo.04	Grade				
c 3+00	317.04 315.69 C 1.35	315.61 315.69 Fo.08		315.58 315.64 Fo.06	316.32 315.64 Co.68							
						# 3 = EC 50' to				317.26		
										317.35	EC on 50' to	
										Fo.09		
c 2+75	315.04	314.93 315.64 Fo.11		314.84 314.85 Fo.01	314.85							
						# 2				317.10		
										316.80		
										Co.30		
c 2+50	315.43 314.39 C 1.04	314.29 314.39 Fo.10		314.09 314.07 Co.02	313.62 314.07 Fo.45							
						# 1				316.98		
										316.80		
										Co.18		
2+25	313.74	313.72 313.74 Fo.02		312.82 313.28 Fo.46	313.28							
						4+05 = CB CC RT.				317.14	317.82	
										317.35	317.35	
										Fo.21	Co.47	

STERLING CT. W'ly (cont.)

Set T.B.M.

318.27 = chd NW Corn Porch  
at 5015 Sterling CT.

5+00 = END  
w'ly  
K. INLET RT

312.47  
CO 312.65  
FO.18

312.80  
312.90  
CO.10  
314.59  
312.70  
C 1.89

312.80  
309.86 FL Box  
C 294  
312.80  
311.87 = GOTT  
Co.93

312.47  
312.15  
GUT CO. 32

4499.50

312.97  
312.90  
CO.07  
313.28  
312.90  
CO.38

4494.66 ELY END TYPE  
K. INLET RT.

313.00  
313.00  
Grade  
313.00

313.00  
CO.04

4475

314.10  
314.30  
314.10  
CO.20

314.09  
314.20  
FO.11  
314.20

#8 = FC  
ON 50th

316.02  
316.05  
FO.03



50<sup>th</sup> ST. - STERLING CT. - NLY to

42

D. END

LT

(RT-64)

STA.	P.L.	CB.	♀	CB	P.L.	STA.	P.L.	CB	♀	CB	P.L.
			319.62 CB 318.95								
1+60 = END CONST.	318.96 318.30 Co. 66	319.13 318.30 Co. 83	319.62 318.95 GUT	319.55 318.80 Co. 75	319.06 318.80 Co. 26						
0+80	317.99	318.10 317.99 Co. 11		318.56 318.48 Co. 08	318.48						
0+75 = W.S. LT.	320.9 317.9 CB C 3.0				318.48						
0+70 = SEN LT	320.9 313.8 P.L.		320.9 313.0 ♀								
<u>19</u> LT	C 7.1		C 7.9								
0+60	317.67	317.54 317.67 Fo. 13		318.32 318.18 Co. 14	318.18						
0+48 EVIC ON LT	317.68 317.48 Co. 28	317.30 317.48 Fo. 18		318.24 317.98 Co. 26	318.41 317.98 Co. 43						
0+28	316.95	316.78 316.95 Fo. 17		317.45 317.66 Fo. 21	317.66						
0+08 = CB EC S.	316.52 316.05 Co. 47	316.05		317.35	317.67 317.35 Co. 32						

0+00 = NLY  
LINE STERLING  
CT.

Clark  
Garber  
O'Neil  
A. Brennan  
8.14.56  
W.D. 20617

STORM DRAIN: Lots 48-49+50  
PACIFIC VIEW Homestead

Ref: F.B. 2021-73-22  
DWG: 6174-B

STA.

Elevs:

0+56 = End Const.

119.80  
118.36  
C 1.44

0+28

120.54  
119.06  
C 1.48

(stubs 5' 4" E  
Ely)

0+00 = End EXIST  
30" R.C.P.

Met. EXIST  
119.76

B.M. = F.L. EXIST 30" R.C.P. 0+00

112.87

F.B. 2021-74

Clark  
Moore  
O'NEIL  
ABTENILLA

Sewer-Alley BIK 1  
BUENA-VISTO TRACT

9-7-56  
No. 32554

REF: DNG: 12615-L  
F.B. 2330-7

44  
F.B. 2330-8  
E. 41st + N. by Lina Alley  
178.13 = 178.12 = E. Rim M.H.

STN

Elev.

CHK:

5+47.5 = Plug End

184.92  
177.25 = FL  
C 7.47

2+45

171.15  
165.56  
C 5.59

5+15

185.87  
176.92  
C 8.95

2+10

169.75  
165.42  
C 4.33

4+75

185.13  
176.52  
C 8.61

1+75

169.12  
165.28  
C 3.84

4+35 = M.H. #1

183.96  
176.12 = FL  
C 7.84

1+40

169.24  
165.14  
C 4.10

(Stubs set 8'48"  
RT M.H.)

1+05

170.77  
165.00  
C 5.77

4+20

182.42  
175.22  
C 7.20

0+70

172.30  
164.86  
C 7.44

3+80

180.62  
172.82  
C 7.80

0+35

Stubs set 5' RT)

173.70  
164.72  
C 8.98

3+40

177.51  
170.42  
C 7.09

0+00 = M.H. #3

Const. to meet  
EXIST. & Sewer  
42nd + Conn.  
EXIST. LAT.

(Stubs on M.H.  
set 8'48" RT  
M.H.)

175.34  
164.58 = F.L. (plan)  
C 10.76

3+00

174.75  
168.02  
C 6.73

2+60 = M.H. #2

(Stubs set 8'48"  
RT M.H.)

172.45  
165.62 = F.L.  
C 6.83

B.M

174.74 = NAIL Pole-

# 177973 (F.B. 2330-9)

CLARK  
O'NEIL  
ABRENILLA  
9-13-56  
W.O. 32547

IMPS' GARDENA ST.

(30" STORM DRAIN)  
GARDENA PLACE

(2+38 = E GARDENA)

(not set)

20.22

2+18 = CB Fc

24.73  
20.00  
4.73

24.88  
20.00 F.L. Pipe Nly  
C 4.88  
Knocked-out

2+18 = CB Fc SLY  
CB LINE GARDENA  
INLET #1

24.73  
19.90  
C 4.83

24.88  
19.90 = F.L. BOX  
+ Pipe Sly  
C 4.98

2+00

24.62  
19.80  
C 4.82

1+60

24.49  
19.56  
C 4.93

1+20

24.19  
19.32  
C 4.87

0+80

24.37  
19.08  
C 5.29

0+40

(Subsio LT(W) E)

23.53  
18.87  
C 4.69

0+00 = Pt. 238 FT  
SLY OF E GARDENA  
ON A LINE 15 WLY  
OF ELY LINE  
GARDENA PL.

21.60  
18.60  
C 3.00

B.M.

Dir Elev. Rod:

22.49 = E Con Mon ILLION + GARDENA

CB INLETS

45

INLET # 2

25.81  
21.40 = F.L. Box  
C 4.41

25.81  
25.70 CB  
C 0.11

25.82  
25.75 CB  
C 0.07

CB Fc Nly

INLET #1

10' 10'  
24.73  
25.01 = B  
Fo 28  
24.73  
19.90 = F.L. BOX  
C 4.83

25.19  
25.06 CB  
C 0.11

CB Fc SLY

4+03 = End Pipe (plug)

28.49  
22.00  
C 6.49

3+60

26.72  
21.54  
C 5.18

3+20

26.12  
21.11  
C 5.01

2+80

25.56  
20.68  
C 4.88

2+59.65 = 18" pipe 25' RT  
(AT WLY END INLET #2)

25.97  
21.40 = F.L. BOX  
C 4.59

(Knocked-out)

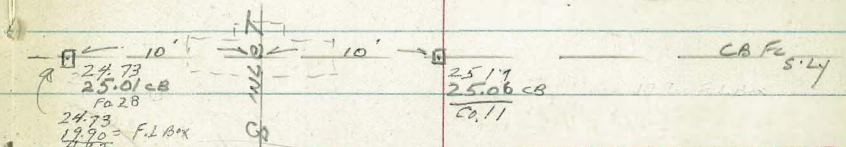
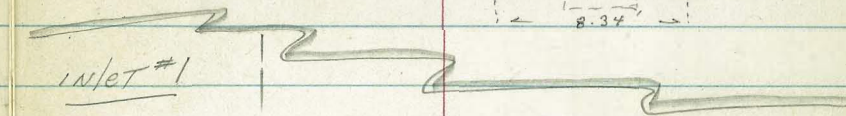
25.33  
21.00  
C 4.33

25.52  
21.00 = F.L. 18" pipe to sly  
C 4.52

2+59.65 = E 24" F 18"  
Pipe to INLET #2

25.33  
20.46  
4.87

25.52  
20.46 = F.L. 30" pipe  
C 5.06





(NLY) LT				RT		(NLY) LT				RT	
STA.	P.L.	CB	Σ	CB	P.L.	STA.	P.L.	CB	Σ	CB	P.L.
4+25	23.91	$\frac{24.15}{23.91}$ C-0.24		$\frac{23.44}{23.45}$ F-0.01	23.45	6+25 RT only				$\frac{24.54}{24.79}$ F-0.25	24.79
4+16 = W.S. RT				23.03 23.35 TR CB F-0.32		#1 = END CB LT	25.30	$\frac{25.19}{25.30}$ F-0.11			
4+00	$\frac{24.20}{23.73}$ C-0.47	$\frac{23.95}{23.73}$ C-0.22		$\frac{23.83}{23.28}$ C-0.05	$\frac{23.09}{23.28}$ F-0.19	6+08.78 = CB BC LT (NLY)	$\frac{25.07}{25.18}$ F-0.11	$\frac{24.79}{25.18}$ F-0.39		$\frac{24.32}{24.68}$ F-0.36	24.68
3+75	23.57	$\frac{23.79}{23.57}$ C-0.22		$\frac{23.23}{23.11}$ C-0.12	23.11	6+00	25.11	$\frac{25.12}{25.11}$ C-0.01		$\frac{24.55}{24.62}$ F-0.07	$\frac{24.61}{24.62}$ Grade
3+50	$\frac{24.15}{23.40}$ C-0.75	$\frac{23.87}{23.40}$ C-0.47		$\frac{22.97}{22.95}$ C-0.02	$\frac{22.91}{22.95}$ F-0.04	5+75	24.94	$\frac{24.86}{24.94}$ F-0.08		$\frac{24.42}{24.41}$ F-0.03	24.45
3+25	23.24	$\frac{23.52}{23.24}$ C-0.28		$\frac{22.76}{22.78}$ F-0.02	22.78	5+50	$\frac{24.67}{24.77}$ F-0.10	$\frac{24.57}{24.77}$ F-0.20		$\frac{24.43}{24.29}$ C-0.14	$\frac{24.11}{24.29}$ F-0.18
3+00	$\frac{23.60}{23.07}$ C-0.53	$\frac{23.35}{23.07}$ C-0.28		$\frac{22.65}{22.61}$ C-0.04	$\frac{22.38}{22.61}$ F-0.23	5+25	24.60	$\frac{24.50}{24.60}$ F-0.10		$\frac{24.14}{24.12}$ C-0.02	24.12
2+75	22.91	$\frac{23.16}{22.91}$ C-0.25		$\frac{22.33}{22.44}$ F-0.11	22.44	5+00	$\frac{24.41}{24.43}$ F-0.02	$\frac{24.35}{24.43}$ F-0.08		$\frac{23.89}{23.95}$ F-0.06	$\frac{23.89}{23.95}$ F-0.06
2+50	$\frac{22.92}{22.74}$ C-0.18	$\frac{22.89}{22.74}$ C-0.15		$\frac{22.29}{22.28}$ C-0.01	$\frac{22.33}{22.28}$ C-0.05	4+75	24.27	$\frac{24.30}{24.27}$ C-0.03		$\frac{23.69}{23.78}$ F-0.09	23.78
2+28 = Sew LAT #10 RT.			21.6 15.3 Σ C-6.3	21.6 17.00 Prop C-4.6		4+50	$\frac{24.29}{24.09}$ C-0.20	$\frac{24.23}{24.09}$ C-0.14		$\frac{24.65}{23.62}$ C-0.03	$\frac{23.40}{23.62}$ F-0.22

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
						8+00	25.99 26.35 F0.36	26.20 26.35 F0.15		25.91 25.85 C-0.06	26.14 25.85 C0.29
6+84.78=CB BC LT	25.97 25.70	25.70				7+75	26.21	26.04 26.21 F-0.17		25.54 25.71 F-0.17	25.71
=w/ly end INLET #2 (NEL)	C0.27	(See pg 45 For INLET #2)				7+50					
#1=end CB LT	25.80	25.83 25.80 C-0.03									
(6+74.78) 6+75 RT				25.23 25.13 C-0.10	25.13	7+70= Sew LAT #9 LT	25.9 26.0 C4.9		25.9 19.0 C6.9		
6+63.95=ELY end CB INLET #1 RT				25.06	25.06	7+60= W/S LT	25.60 26.10 F0.50				
						7+50	25.78 26.07 F0.29	26.04 26.07 F-0.03		25.47 25.57 F-0.10	25.15 25.57 F0.42
6+59.78=C INLET #1 RT			2439=60TT.	25.04	25.04	7+25	25.93	26.00 25.93 C-0.07		25.43 25.43 C0.00	25.43
6+55.61= w/ly end CB INLET #1 RT				25.01	25.01	7+00	25.79	25.89 25.79 C-0.10		25.78 25.29 F-0.01	25.29
6+50 RT only				25.21 24.97 C-0.24	24.97	6+93.12 =ELY end inlet #2 LT	25.94 25.95 C0.01	25.75 (See pg. 45 For inlet #2)		25.08 25.25 F-0.17	25.11 25.25 F0.14

STA	P.L	CB	F	CB	P.L	STA	P.L	CB	F	CB	P.L
9+54=Sew LAT#6 RT			26.1 20.2g C5.9		26.1 21.8RT C5.3 Prop	10+86=Sew LAT#4 RT			26.0 21.0 F C5.0		26.0 22.8 prop C3.2
9+50	27.67 27.19 C0.48	27.11 27.19 F-0.08		27.22 26.69 C-0.53	27.09 26.69 C0.40	10+76=W.S RT					26.13 27.60 TPCB F1.47
9+44=W.S RT					26.65 TPCB F0.54	10+75	28.11	28.45 28.11 C-0.34		28.02 27.60 C-0.42	27.60
9+26	27.05	26.90 27.05 F-0.15		27.04 26.53 F-0.49	26.55	10+50	28.15 27.91 C0.24	28.05 27.91 C-0.14		27.86 27.40 C-0.46	27.90 27.40 C0.50
9+24=Sew LAT#7 LT	26.9 22.0 Prop C4.9		26.9 20.0 F 6.9			10+26=Sew LAT#5 RT			26.1 20.6 F C5.5		26.1 22.3 Prop C3.8
9+00	26.88 26.91 F0.03	26.18 26.91 F-0.13		26.41 26.41 C-0.00	26.68 26.41 C0.27	10+25	27.72	27.83 27.72 C-0.11		27.38 27.21 C-0.17	27.21
8+75	26.77	26.54 26.77 F0.23	Chis.X	26.43 26.27 C-0.16	26.27	10+16=W.S RT					26.19 27.15 TPCB F0.96
8+50	26.75 26.63 C0.12	26.67 26.63 C-0.04		26.18 26.13 C-0.05	26.56 26.13 C0.43	10+00	27.59 27.52 C0.07	27.46 27.52 F-0.06		27.05 27.02 C-0.03	27.60 27.02 C0.58
8+25	26.49	26.47 26.49 F-0.02		26.06 25.99 C-0.07	25.99	9+74.78=quid Brk	27.74 27.33 C0.41	27.31 27.33 F-0.02		27.15 26.83 C-0.32	27.32 26.83 C0.49



(N<sup>W</sup>) LT.

RT.

STA.	P.L.	CB	£	CB	P.L.	STA.	P.L.	CB	£	CB	P.L.
12+25	29.27	$\frac{29.70}{29.27}$ C-0.43		$\frac{28.56}{28.76}$ F-0.20	28.76						
12+02.91 Beg CB LT.	$\frac{29.39}{29.10}$ Co. 29	$\frac{29.10}{29.10}$ 0.00									
12+00 RT only				$\frac{28.51}{28.56}$ F-0.05	$\frac{29.06}{28.56}$ Co. 50						
11+75 RT only				$\frac{28.47}{28.37}$ C-0.10	28.37						
11+58 = Sew LAT #3 RT			$\frac{26.5}{21.5}$ £ C 5.0		$\frac{26.5}{23.3}$ Prop C 3.2						
11+50 RT only	$\frac{29.08}{28.70}$ Co. 34	$\frac{29.08}{28.70}$ Co. 34		$\frac{28.34}{28.18}$ C-0.16	$\frac{28.92}{28.18}$ Co. 74	13+17.91 = END CB RT.	$\frac{30.74}{30.00}$ Co. 74			$\frac{29.37}{29.50}$ F-0.13	$\frac{30.11}{29.50}$ Co. 61
11+48 = W.S. RT.					$\frac{26.5}{29.2}$ Tr. CB F 2.3	13+00 RT only				$\frac{29.31}{29.35}$ F-0.04	$\frac{29.70}{29.35}$ Co. 35
11+26.81 = CB END LT.	$\frac{28.87}{28.51}$ Co. 36	$\frac{28.87}{28.51}$ C-0.36				12+87.91 = END CB, LT.	$\frac{30.23}{29.77}$ Co. 46	$\frac{30.18}{29.77}$ C-0.41			
11+25 RT only				$\frac{28.21}{27.98}$ C-0.23	27.98	12+75	29.66	$\frac{30.35}{29.66}$ C-0.69		$\frac{29.04}{29.15}$ F-0.11	29.15
11+00	$\frac{28.54}{28.30}$ Co. 24	$\frac{28.40}{28.30}$ C-0.10		$\frac{28.07}{27.79}$ C-0.28	$\frac{28.01}{27.79}$ Co. 22	12+50	$\frac{30.01}{29.46}$ Co. 55	$\frac{29.94}{29.46}$ C-0.48		$\frac{28.75}{28.95}$ F-0.20	$\frac{29.70}{28.95}$ Co. 75

Clark  
O'Neil  
ABRENILLA  
9-20-56  
W.O. 62484

Imp's: HOWARD AVE - UNIV. HTS.  
Sewer - Alley BIK 126 to E  
ALLEY BIK 125

REF: CITY ENG Notes: H-18 - Hatch 51  
DWG: 3832-D

STA	Elev's	CR's	Elev's
1+75	316.85 310.90 C5.95		306.17 = 306.18 = FL M.H. 0700 (= 4730 Notes & H-18)
1+40	315.73 310.73 C5.00	3+80 = EXIST M.H. 3+75 { 2' each side 4" 90s main ENCASE SEWER MAIN	320.18 = FL EXIST
1+05	315.10 310.55 C4.55	3+40	322.12 317.78 C4.34
0+70	314.92 310.38 C4.54	3+00	320.54 315.38 C5.16
0+35	315.44 310.20 C5.24	2+70 = E.V.C.	319.34 313.58 C5.76
0+12 = END CON. ENC.		2+50	318.67 312.60 C6.07
(stubs set 5' RT E)		2+30	318.24 311.90 C6.34
0+00 = Alley BIK 126 = EXIST MAIN Rebuild. to drip- m.H. (stubs set 2' 8' RT E) m.H.	F.L. Ely = 317.20 310.03 C7.17	2+10	317.87 311.30 C6.57
	F.L. M.H. = 306.18	1+90 = B.P.C.	317.34 310.98 C6.36
BM: Dir. Elev Rod:	318.04 = S.E. B.P.	TEXAS ST - HOWARD AVE.	

CLARK  
 GARBER-ONEIL  
 ABRENNIA  
 9-21-56  
 W.O. 32646  
 STA.

52nd ST. Polk to ORANGE  
 Water-Line

REF: DWG: 3554-D sheet #1  
 City ENG: Notes: K-16 & K-18 - ALLEN  
 52

STA.	Elev. FIN. Pav.	STA	Elev's FIN. Pav.
240	339.44 337.40 C 2.04	4+87 = EVC	361.86 360.50 C 1.36
2+00	336.24 334.27 C 1.97	4+67	359.41 357.30 C 2.11
1+60	332.33 331.14 C 1.19	4+47	356.91 354.50 C 2.41
1+20	328.58 328.01 C 0.57	4+27	354.43 352.30 C 2.13
0+80	325.28 324.88 C 0.40	4+07 = BVC	353.28 350.50 C 2.78
0+40	322.36 321.76 C 0.60		
0+15	320.66 319.81 C 0.85	3+60	350.67 346.78 C 3.89
(Stake set 5 RT E)		3+20	346.81 343.65 C 3.16
0+00 = N Line Polk	317.54 319.44 meet	2+80	343.02 340.52 C 2.50

Note: Cut stakes to refer to grade prop. Pav.  
 As per Water-Dept (City-Forces) Request - C. ELDER

B.M. 315.32 = NW BP 52nd & UNIV.

STA.

Elev Fin. Pat.

CHK:

377.56 - 377.51 = SN/AP 52 in 1 ORANGE

5778.57 = S. LINE ORANGE

376.30  
376.40  
Fo.10

5767

374.79  
375.85  
F1.06

5757

373.24  
374.46  
F1.22

5747 B.V.C

371.75  
372.70  
Fo.95

5717

366.66  
366.60  
CO.06

Clark  
GARDNER  
O'Neil  
ABERNILLA  
7-24-56  
W.O. 2/285

DRAIN - TUBEROSE & Poplar  
B/K 25 - LEXINGTON PK.

Ref. DWG: 5489-B

54

(No Field-Book  
No Right-of-Way DWG)!

STA.

Elev's

0+88 = END EXIST. 18" Pipe

274.83 = EXIST  
F.L  
(meet)

0+66

273.25  
272.96  
C.O. 29

0+44

270.25  
271.09  
F.O. 84

0+22

268.77  
269.22  
F.O. 45

0+00

268.16  
267.35  
C.O. 81 F.L

B.M. (Dir. Elev. Rod) used F.L. LINE  
EXIST. PIPE 284.02 = SPIKE SN P. TUBEROSE & Pepper (OUT)

CLARK  
GARBER  
O'NEIL  
ABRENTA

EXTEND DRAIN - WARRINGTON  
WHITTIER

REF: city notes: File C-19 (CLARK) (Survey to EXTEND DRAIN) 55  
DING: 6187-B

CHK:

41.02 = 41.02 = B.M

1+35.68 = E.C

38.84 = F.L <sup>Meet EXIST</sup>

(A = 19° 06'  
R = 22'  
T = 3.70  
L = 7.34)

1+28.34 = B.C

39.37  
38.43 = F.L  
C 0.94

1+20

38.72  
38.10  
C 0.62

0+80

38.52  
36.50  
C 2.02

(Hubs set 8' L&E)

0+40

39.24  
34.90  
C 4.34

0+00 = Fc. Curtain -  
- WALL

36.85  
33.30 = F.LINE  
C 3.55

B.M DIR. Elev. Rod:

41.02 = C&D ELY CORN - to EXIST H'dwall  
(Notes C-19-P92)



CLARK  
GARBER  
ABRENILLA

Storm-Drain  
LIVERPOOL CT.  
(BAYSIDE Lane to BOYSIDE-WALK)

Ref: DWG: 5956-B

57

NO F.B. AVAILABLE!

10-16-56  
W.O.: 20361

STA.

Elev's

0+94.5 = Ely edge (-4.78 = FL DRAIN EST.) - (3) 4.90 - 4.10 = F.L.  
EXIST. 2'x2' DRAIN  
E BAYSIDE-LANE

0+63.5 - 5.01 - 1.25 - 4.29  
C 3.04

(5' RT) (PLAN)  
0+31.5 - 5.12 - 0.98 - 4.48  
C 3.50

0+00 = W/edge (-4.95 = FL cleanout) - (3) 5.23 - 4.67 = F.L.  
EXIST. CLEANOUT  
BAYSIDE-WALK

B.M. DIV. Elev. Rod:

6.98 = S.W.B.P

SAN LUIS OBISPO - PLACE & MISSION BEACH - SEA WALL



CLARK  
GABER  
ABRENILLA  
10-16-56  
No. 20361

STORM-DRAIN: NANTASKET  
CT. (Bayside-Lane to Bayside-  
-walk

REF: DWG: 5953-B

58

No F.B. available!

0+92.14# = Ely  
edge EXIST DRAIN  
E Bayside - Lane

- 4.90 - 5.11

~~0+60.4~~

- 1.31  
- 5.32  
C 4.01

0+48

~~0+30.7~~

0+00 = Wly edge  
EXIST. CLEANOUT

- 5.26 - 5.52

D.M.: DIV. E/OK ROD:

7.07 = S.W.B.P  
SAN JUAN Y MISSION BEACH  
SEA-WALL

CLARK  
GARBER  
DINCEL  
ABREVILO  
10-25-56  
W.O. 32498

SEWER: EL CAJON Blvd -  
PEARSON DRIVE - ROLANDO +  
CAMPO

REF: F.B. 2275  
DWG: 2915-D  
2916-D

59

(= 0+00 S'LY EL CAJON) see pg 62

4+56.45 = M.H. #3 = P.O.T.  
 $\Delta = 113^{\circ} 11' 18''$  RT (W.I.L.)  
Stubs set 9.58' + 19.16' RT  
ON SPLIT

409.85  
406.51  
C 3.34

STA:

#/ers:

1+55

403.77  
396.85  
C 6.92

4+25

410.09  
405.51  
C 4.58

1+20

403.06  
395.72  
C 7.34

3+90

408.87  
404.40  
C 4.47

0+85

402.55  
394.59  
C 7.96

3+55

409.86  
403.28  
C 6.58

3+20

407.33  
402.17  
C 5.16

0+50.22 = M.H. #1

$\angle$  LT  $32^{\circ} 34' 30''$

[Stubs set 8.34'  
+ 16.68' ON SPLIT]

400.43  
393.47  
C 6.96

2+85

405.78  
401.06  
C 4.72

CHK: Hub  $\phi$  2+52.10 = 405.04

0+25.11

412.38  
392.97  
C 19.41

2+52.10 = M.H. #2

$\angle$  LT  $37^{\circ} 12'$

[Stubs set 8.44' + 16.88 RT.  
ON SPLIT]

405.30  
400.01  
C 5.29

0+00 = EXIST D-END

AS PER DWG: 1421-B-D Pg 9  
(EXACT LOC. UNKNOWN)  
S'LY MONTEZUMA Rd

392.47 (DWG)

2+25

404.44  
399.12  
C 5.32

B.M. DIR. Elev. ROD:

453.73 = S.W. B.P.  
6744 EL CAJON

1+90

404.00  
397.99  
C 6.01

↑  
3.248

↑  
3.8

(Stubs set 8.34'  
+ 16.68' ON SPLIT)

MONTEZUMA-PEARSON DRIVE Senr. (CONT)

CHK: 2x2 HUB  $\angle 3^{\circ} 26' 07''$  449.94 = 449.96  
 (F.B. 2275-26-35)  
 (6+38.56)

STA:	Elev's:	STA.	Elev's:
5+71.45 } Beg grade } end encase. = E.V.C. 5+62.45	430.70 417.25 C 13.45	7+76.61 = $\angle$ RT $3^{\circ} 26' 07''$ (No. m.H. here) stubs set 8' LT + 8' RT on split	450.05 436.95 C 13.10
5+52.45 = $\epsilon$ C <sub>0</sub> T <sub>0</sub> FF WALL	423.76 414.96 F.L. C 8.80	7+60	449.35 436.88 C 12.47
5+42.45	417.79 412.95 C 4.84	7+25	447.67 436.74 C 10.93
5+32.45	415.16 411.23 C 3.93	6+90	446.70 436.60 C 10.10
5+22.45	412.41 409.80 C 2.61	6+55 (stubs set 8' LT - here - on)	445.78 436.46 C 9.32
5+12.45	410.77 408.65 C 2.12	6+39.71 = m.H. #4 = P.O.T w/ly stubs set 8' + 16' RT of 70'	444.77 436.40 = F.L. C 8.37
5+02.45	409.55 407.79 C 1.76	6+12.45 = $\epsilon$ C <sub>0</sub> T <sub>0</sub> FF WALL	443.84 435.00 = TP C 8.84 WALL 429.64 F.L. C 14.20
4+92.45	409.40 407.22 C 2.18		
4+82.45 B.V.C.	409.58 406.93 C 2.65	5+82.45 = $\epsilon$ C <sub>0</sub> T <sub>0</sub> FF WALL	442.43 422.20 F.L. C 20.23

↑  
5  
0.4  
10.10

MONTEZUMA - PEARSON DV - (CONT)

STA.	Elev's:
10+75	450.44 438.14 C12.30
10+40	450.74 438.00 C12.74
10+05	451.67 437.86 C13.81
9+70	451.38 437.72 C13.66
9+35	451.26 437.58 C13.68
9+00.66 = M.H #5 = P.O.T.	449.08 437.44 F.L. C11.64
8+65	448.99 437.30 C11.69
8+30	449.27 437.16 C12.11
7+95	449.67 437.02 C12.65

0.48  
↑

chk: → 449.94 = 449.96 (see pg. 60) <sup>TP.</sup>

STA	Elev's:
13+15.66 = Plug-End	449.08 439.10 F.L. C 9.98
12+90 (Sub 8' RT)	449.49 439.00 C 10.49
12+65	439.76 438.90 C 0.86
12+40.66 = M.H #6 = P.O.T.	442.25 438.80 F.L. C 3.45
12+15	444.38 438.70 C 5.68
11+80	446.76 438.56 C 8.20
11+45	450.82 438.42 C 12.40
11+10	450.83 438.28 C 12.55

Sly EL CANYON (CONT) (See Pg 59)

0+00 = (4+56.45 M.H. #3 w'ly line)

STA.	Elev's:		
1+75	419.99	4+07.38 = M.H. #8	438.39 431.00
1+45 & C&F	435.59 417.69 C17.90	chk & stob. F.R.T. split 10.45' LT	C 7.39
1+40	417.29	3+75	437.24 429.52 C 7.72
1+32 & C&F	435.54 416.69 C18.85	3+40	435.81 427.92 C 7.89
1+05	414.60	3+05	434.74 426.32 C 8.42
0+95 & C&F	434.35 413.83 C 20.52	2+70	434.03 424.72 C 9.31
0+70	427.97 411.90 C16.07	2+35	433.67 423.12 C10.55
0+35	409.76 409.21 C0.55	2+00	433.59 421.52 12.07
0+00 = M.H. #3 (= 4+56.45 w'ly line) See pg 59	406.51	1+87.38 = M.H. #7 A = 72° 06' LT stubs set	433.75 420.94 F.L. C12.81
B.M.	453.93 = SW B.P. EL CANYON + 6714W	[chk set on 6' BK M.H. ON BK TANG (FOR tunneling)]	

7.78

7.5732

Sly, EL CAJON - (CONT.)

5779.18 = plog. end

443.49  
439.00  
C 4.49

5460

↑  
7.06%

442.54  
437.65  
C 4.89

5425

440.82  
435.17  
C 5.65

4494.18 = M.H. #9

Sec Nail 10' 20' pt  
on split

439.63  
433.00  
C 6.63

4470

439.34  
432.48  
C 6.86

4458 CB Fc

↑  
0%

440.58  
432.16  
8.42

4447 = CB Fc

440.65  
431.91  
C 8.74

4435

439.53  
431.63  
C 7.90

CLARK  
GARBER  
O'NEIL  
ABRENILLA  
12-22-56  
M.O. 31674

Imp's. Alley BIK "J" (MONTE ELLO)  
EL CAJON to MONROE

REF: DWG: 12843-L  
Field Notes: J-18

64

Note: 0.50 Pav. Exception  
each side alley = 19' pav. width.

	LT.	RT.	LT.	RT.
1+61.70 = EVC	372.62 373.10 Fo.48	374.13 373.40 Co.73		
1+41.70	372.17 372.26 Fo.09	373.01 372.56 Co.45	3+61.70 = BVC	378.81 379.64 Fo.83
1+21.70	371.09 371.33 Fo.24	373.43 371.63 Co.180	3+36.70	378.16 378.94 Fo.78
1+01.70	370.32 370.35 Fo.03	372.97 370.65 Co.232	3+11.70 (25')	378.20 378.25 Fo.05
0+81.70	369.70 369.37 Co.33	369.81 369.67 Co.14	2+86.70	377.69 377.55 Co.14
0+61.70	368.79 368.37 Co.42	368.76 368.67 Co.09	2+61.70 EVC	376.49 376.86 Fo.37
0+41.70 = BVC	367.82 367.32 Co.50	367.50 367.61 Fo.11	2+41.70	376.21 376.24 Fo.03
0+28.85	365.60 366.14 Fo.54	366.59 366.52 Co.07	2+21.70 = B.V.C	375.38 375.50 Fo.12
0+00 (0+01.7 LT.) (0+01.7 RT.)	364.94 (set cross Ft)	365.43 (set cross Ft)	2+01.70	375.61 374.70 Co.91
(E ST. 5)			1+81.70	374.23 373.90 Co.33
B.M. Dir. Elev. Rod:		355.37 = S.W. B.P		375.23 374.20 Co.03
		EL CAJON 49.45		

## ALLEY BIK "J" (CONT)

5+61.70	380.15 380.00 Co.15	381.27 380.30 Co.97	7+58.36 RT. only		376.91 376.34 Co.57
5+41.70 = EVC	380.15 380.25 Fo.10	381.00 380.55 Co.45	7+35.03 RT. only		377.04 376.60 Co.44
5+21.70	380.21 380.45 Fo.24	381.15 380.75 Co.40	(7+24.F.B) 7+11.70 = 1309 PAY. LT.	376.29 CHK 376.30 = EXIST. PAY.	376.43 = E.PAY. 377.10 376.85 Co.25
5+01.70 = BVC	380.90 380.55 Co.35	381.01 380.85 Co.16	6+91.70	377.59 376.88 Co.71	378.18 377.18 C 1.00
4+81.70	380.33 380.60 Fo.27	381.11 380.90 Co.21	6+68.36	378.06 377.56 Co.50	379.05 377.86 C1.19
4+61.70 EVC	380.85 380.65 Co.20	381.42 380.95 Co.47	6+45.03	380.08 378.24 C1.84	379.85 378.54 C1.31
4+41.70	380.75 380.65 Co.10	381.20 380.95 Co.25	(23.23) 6+21.70 EVC	380.77 378.92 C1.85	380.36 379.22 C1.14
4+21.70	380.66 380.53 Co.13	381.42 380.83 Co.59	6+01.70	379.71 378.42 Co.29	380.66 378.72 C1.94
4+01.70	380.59 380.37 Co.22	380.50 380.67 Fo.17	5+81.70 BVC	379.97 379.75 Co.22	381.10 380.05 C1.05
3+81.70 = BVC	380.46 380.10 Co.36	380.48 380.40 Co.08			



AL/EX BIK "J" (CONT)

LT.

RT

8108.1 = S. Line.  
MONROE  
RT only

375.49 CHX?  
375.51 - TP c13

375.40 = EXIST

375.34 = EXIST

7+81.70  
RT only

377.66  
376.09  
C1.57

CLARK  
GARDEN  
CIVIL  
ARIZONA  
1-2-57  
W.O. 62939

Imp's: SOLITA AVE.

SEMINOLE ELY

LT. (NWLY)

P.L.

CB

E

CB

P.L.

STA.

P.L.

CB

E

RT.

CB

P.L.

REF: DWG: 3952-D

CITY NOTES: L-17 (Sommermejer)

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
						2+75				457.97 458.20 Fo.23	458.20
0+25				456.88 457.14 Fo.26	457.14					457.71 458.09 Fo.38	458.38 458.09 C 0.27
0+10 = EXIST Prop P.L. LT (NWLY)				456.57 457.03 Fo.46	457.13 457.03 C 0.10	2+50				457.69 457.98 Fo.38	457.59 457.98 Fo.39
0-21.20 = P.L. B.C				456.63 456.94 Fo.31	456.94	2+00				457.53 457.88 Fo.35	458.04 457.88 C 0.16
						1+75				457.35 457.77 Fo.42	457.77
0-25.64 = CB, BC RT				456.61 456.92 Fo.31	456.79 456.92 Fo.13					457.36 457.67 Fo.31	457.71 457.67 C 0.04
# 1					456.68 456.89 Fo.21					457.28 457.56 Fo.28	457.56
# 2					456.73 456.86 Fo.13					457.02 457.45 Fo.43	457.70 457.45 C 0.25
# 3 = CB, E.C SEMINOLE (EXIST)				456.83 = EXIST. CB.		1+00				457.06 457.35 Fo.29	457.35
						0+75				457.10 457.42 Fo.37	457.48 457.42 C 0.06

B.M.

458.12 = CH II NWLY CB AT BC  
SEMINOLE (STA 20+00.97 FB.2254)

END - SOLITA AVE. (CONT.) (Seminole Ely to Filipo)

SOLITA: (Ely Line Lot 22 N'Wly to Filipo) 68

STA	LT. (N'ly)			RT.	
	P.L.	CB	E	CB	P.L.
(See Pg 69)					
4+78 = CB EC. RT				458.81 459.06 Fo. 19	458.97 459.06 Fo. 09
4+73.92 = Prop. BC RT				458.88 459.04 Fo. 16	459.04
4+62.88 = EXIST. Pk. LT. Filipo				458.80 458.94 Fo. 14	459.19 458.94 Co. 25
4+50				458.75 458.83 Fo. 08	458.83
4+25				458.54 458.73 Fo. 19	459.38 458.73 Co. 65
4+00				458.43 458.62 Fo. 19	458.62
3+75				458.26 458.57 Fo. 25	458.90 458.57 Co. 39
3+50				458.46 458.41 Co. 05	458.41
3+00				458.10 458.30 Fo. 20	458.74 458.30 Co. 44

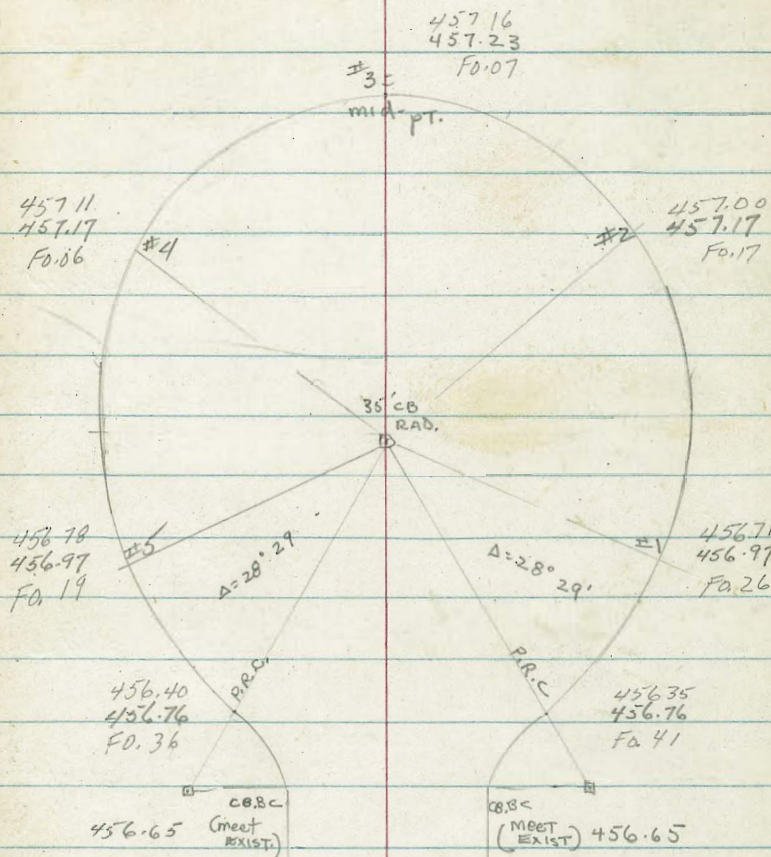
STA	LT. (N'ly)			RT.	
	P.L.	CB	E	CB	P.L.
1+50	457.96 458.29 Fo. 33	458.12 458.29 Fo. 17		457.97 458.21 Fo. 24	457.62 458.21 Fo. 59
1+25	457.72	457.57 457.72 Fo. 15		457.25 457.57 Fo. 32	457.57
1+00	456.27 457.16 Fo. 89	456.88 457.16 Fo. 28		456.62 456.94 Fo. 32	456.23 456.94 Fo. 71
0+75	456.59	456.37 456.59 Fo. 22		456.10 456.30 Fo. 28	456.30
0+50	455.32 456.03 Fo. 71	455.82 456.03 Fo. 21		455.43 455.67 Fo. 24	455.58 455.67 Fo. 09
0+35.35 = E.C. Solita	455.24 455.70 Fo. 46	455.33 455.70 Fo. 37		454.94 455.30 Fo. 36	455.32 455.30 Co. 02
2 UNDERDRAIN =	455.36 455.54 Fo. 18	455.54 455.77 Fo. 34		454.28 454.89 Fo. 61	455.30 454.89 Co. 41
0+17.67 = mid-pt. curve	457.64 455.17 Co. 247	454.83 455.17 Fo. 34			
0+00 = Ely Line Lot 22 = B.C. Solita	454.44	454.44		454.44	454.44

B.M. See Pg 67.

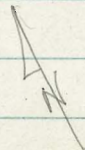
SOLITA { Ely Line Lot 22  
N'Wly to Filipo

STA	P.L	CB	E	CB	P.L
#3 (see pg 68) (= 4478 RT) A=47°48'	459.06	459.06			
#2 A=29°38'	459.15	458.99 459.15 Fo. 16			
#1 - P.L. A=11°28'	459.12	458.91 459.12 Fo. 21			
1+86.10 = C.B.B.C. LT.	458.55 459.07 Fo. 52	458.67 459.07 Fo. 40			
#3 = EXIST. E.C. RT (Filipo)			459.18	459.18	
#2 =					
mid-pt.			458.79 459.04 Fo. 25		
#1 =					
1+76.75 = B.C. SOLITA RT	458.40 458.90 Fo. 58	458.65 458.90 Fo. 25	458.59 458.90 Fo. 31	458.94 458.90 Co. 04	

MATARO Drive Cul-De-Sac 69  
DWG: 3952-D



(L.T.)



(R.T.)

CLARK

GARBER  
O'NEIL

SOUTH CLAREMONT PK

REF: DWG: 4061-D

70

2-18-57

NO. 21175

C.B.

GUTT,  
PAR.

1+44.88 mid-pt.

295.11  
294.17  
C 0.94

1+33.71 = CB BC

296.24  
294.64 294.14  
C 1.60

1+09.71

296.13  
294.88 294.38  
C 1.25

0+85.71

296.08  
295.12 294.62  
C 0.96

0+66.71

296.20  
295.36 294.86  
C 0.84

0+37.71 = E.C

296.02  
295.60 295.10  
C 0.42E. Line Cl'mont Drive  
1+85.27 = END CB287.67  
290.12  
F 0.45

1+78.39 = E.C

290.43  
290.80  
F 0.3710' Rod PT.  
0+21 = CB BC295.82  
295.70 295.20  
C 0.12

1+67.22 mid-pt

292.19  
292.35  
F 0.16

0+0

(Front Porch) 295.86 295.40

1+56.05 = P.R.G.

293.42  
293.49  
F 0.07(Claremont Drive)  
BM = Ld Plug CB N'ly Line Park 289.61

OM = Pl. EXIST. Bldg. = 296.00

CLARK  
GAMBAY  
O'NEIL  
2-19-57  
W.O. 32259  
STA.

ALLEY BIK - 215  
PACIFIC BEACH  
-Rendall to LAMONT-

REF: (Field notes: C-14  
DWG: 3808-D)

71

STA.	LT.	RT (S'LY)	STA.	LT.	RT (S'LY)
2+00	59.78 60.20 Fo.42	59.12 60.20 F1.08	4+00	SEN LAT 4415 RT.	59.77 50.39 C9.38 60.43 60.74 Fo.31
1+75	59.73 60.15 Fo.42	59.06 60.15 F1.09	3+80=ARC	60.68 60.56 Co.12	60.30 60.56 Fo.26
1+50	59.64 60.10 Fo.46	59.03 60.10 F1.07	3+65	60.71 60.53 Co.18	61.60 60.53 C1.07
1+30 = Sen LAT LT.	59.84 55.00 Pr. C4.84	59.84 51.50 Pr. C8.34			
1+25	59.77 60.05 Fo.28	58.67 60.05 F1.38	3+50	60.77 60.50 Co.27	61.51 60.50 C1.01
1+00 = grid BIK	60.31 60.00 Co.31	60.31 on stub LT. 59.60 Co.71	3+25	60.97 60.45 Co.52	60.76 60.45 Co.31
0+75	60.12 60.05 Co.07	58.93 59.95 F1.02	3+00	60.80 60.40 Co.40	59.39 60.40 F1.01
0+50	60.57 60.10 Co.47	59.14 59.90 Fo.76	2+75	60.02 60.35 Fo.33	59.48 60.35 Fo.87
0+25	60.99 60.15 Co.84	59.58 59.85 Fo.27	2+50	59.93 60.30 Fo.37	5981 60.30 Fo.49
0+00 = E. Line Rendall	60.68 60.20 Co.48	60.68 59.40 C1.28	2+25	59.67 60.25 Fo.58	58.71 60.25 F1.54
T.A.M.		59.57 = CLK 0-078A 1/4			
B.M.		40.37 = Sely LT. Reed & Lamont			

RIKY BIK 215 (Cont.)

STA	LT.	RT.
5719.22 = CB. BC	RT	
CHK: 5716.22 = CB BC	LT	62.82 = 62.80 (C-14)
5720 = GOTT Line LAMONT	62.34 = GOTT P1	61.99
		61.74 = GOTT P1
5700.22 = W Line LAMONT	63.01 62.80 Co. 21	62.51 62.50
4780 = BYC	63.92 62.60 C1.32	62.88 62.60 Co. 28
4760 <del>marked out</del>	<del>63.74</del> <del>62.10</del> <del>C1.64</del>	62.50 62.10 Co. 40
4740	63.61 61.60 C2.01	61.07 61.60 Fo. 53
4720 = EVC	62.28 61.10 C1.18	60.81 61.10 Fo. 29

CLARK  
GARBER  
ONCIL  
ABRENNILA  
4-12-57  
W.O. 31884

Imp's: ALLEY BJK 58  
UNIVERSITY HT'S

Ref: Field Notes. 4-18  
DWG: 3833-D

73

Note: { 0.25 Po V. Exceptance HT+RT

STA:	LT.	E	RT	STA	LT.	E	RT
				3+50	379.39 379.54 Fo. 15		379.52 379.54 Fo. 02
1+50	376.64 377.27 Fo. 63		377.78 377.27 Co. 51	3+25	380.81 379.26 C 1.55		379.30 379.26 Co. 04
1+25	377.84 376.99 Co. 85		377.21 376.99 Co. 22	3+00	379.08 378.97 Co. 11		378.98 378.97 Co. 01
1+00 = E.V.C	377.60 376.71 Co. 89		377.04 376.71 Co. 33	2+75	378.88 378.69 Co. 19		379.16 378.69 Co. 47
0+80	377.50 376.48 C 1.02		376.98 376.50 Co. 48	2+50	378.46 378.41 Co. 05		378.89 378.41 Co. 48
0+60	376.45 376.32 Co. 13		376.84 376.35 Co. 49	2+25	378.17 378.12 Co. 05		378.31 378.12 Co. 19
0+40	375.82 376.10 Fo. 28	376.53 ← off RT. 375.76 Co. 77	376.53 376.22 Co. 31	2+20 = E. S. W. LAT. (#1) RT		378.58 370.44 ← C 8.14	378.58 373.07 ← PL C 5.51
0+20	375.80 375.94 Fo. 14	376.35 ← off stub RT 375.72 Co. 63	376.35 376.14 Co. 21	2+00	378.28 377.84 Co. 44		378.09 377.84 Co. 25
0+00 = N. Line MONROE = BYC	375.78 (meet)		376.08 (meet)				
B.M.	Dir. Elev. Rod:		389.38 = S.E. 304h +	1+75	376.97 377.56 Fo. 59		378.17 377.56 Co. 61

B. P.  
ADAMS



NLEY BLK 58 (CONT.)

74

STA	LT.	E	RST	STA	LT.	RT.
5+80	381.61 381.03 Co.58	381.61 OFF 380.78 AT J <sup>th</sup> Co.83	382.02 381.33 Co.69			
5+60	381.50 381.17 Co.33		381.95 381.47 Co.48	chk:		381.51 = 381.49 = CB END Rt STA 5+99.21
5+40	381.34 381.22 Co.12		381.53 381.50 Co.03			
5+20	381.26 381.17 Co.09		381.88 381.43 Co.45			
5+00 = B.V.C.	381.55 381.03 Co.52		381.32 381.25 Co.07			
4+75	380.43 380.80 Fo.37		382.41 380.96 C1.45			
4+50	380.40 380.57 Fo.17		381.61 380.68 Co.93			
4+25	380.25 380.34 Fo.09		380.60 380.39 Co.21			
4+00 = grid B.V.C.	379.89 380.11 Fo.22		380.29 380.11 Co.18	= 5+99.21 = S. Line (6+00) { MADISON = E.V.C.	380.60 (meat)	380.73 (meat)
3+75	379.56 379.82 Fo.26		379.57 379.82 Fo.25			381.15 (meat)

CLARK  
GARBER  
O'NEIL  
ABRENILLA  
6-7-57  
W.O. 62921

STORM DRAIN: AUBURN DR ELY  
(FAITHAVEN ACRES) TO EXIST 21" CURVET

Ref: DWG: 6401-B  
Field Notes J-19

75

STA.	Elev's	chk:	
			266.71 = 266.71 = P.K. - TP 2 Hdwall
1+90	249.21 245.84 C 3.37		
1+40	244.30 241.83 C 2.47		
0+90.40 = E.C.	240.07 237.85 C 2.22		
		(make collar connection) EXIST 21" Pipe 3+50.37 = Hd wall	chk: 263.29 263.28 = F.L
0+67.48 = B.C. = g'd B.M. D = 140.26 LT. R = 91' T = 11.52' L = 22.92'	238.42 236.00 C 2.42 F.L.	3+17.32	262.33 259.33 C 3.00
0+33.74	237.48 235.60 C 1.88	2+83.66 = E.C.	260.00 255.38 C 4.62
(CURTAIN-WALL) 0+00 = PT on Ely 12' LINE AUBURN DR +83.67 N'ly OF S. LINE FAITHAVEN ACRES MEAS. along W'ly 7' LINE AUBURN DR	234.79 235.20 = F.LINE FO. #1	2+56.60 = mid-pt	255.74 252.19 C 3.55
B.M. { = 238.38 SPIKE IN Pole W'ly MON (W'ly 7' LINE AUBURN DR (Dir. Elev. Rod) #5500 (4 S'ly LINE FAITHAVEN ACRES)		2+29.54 = B.C. = g'd B.M. A = 34° 04' 30" LT R = 91' T = 27.89' L = 54.12' E = 4.18'	251.33 249.00 = F.L C 2.33

CLARK  
GARBER  
MOORE  
ABRENILLA  
10-1-57  
W.O. 21643

STORM-DRAIN  
6th ST. EXTENSION  
(36" on plan, changed by  
office to 30")

Ref: city notes G-19 (do not apply this job) <sup>76</sup>  
DWG: 5202-D  
(shows 36" R.C.P.  
changed to 30" [Red line]  
[data on plan])

END CONST.  
0+96

190.25

189.00 - F.L.  
C1.25

0+64

↑  
4.178

189.81  
190.33  
F0.52

0+32

191.60  
191.66  
F0.06

(MAKE COLLAR CONNECTION)

0+00 = END EXIST  
30" R.C.P.

CHK: 193.00 F.L

B.M. F.L. EXIST 30" = 193.00

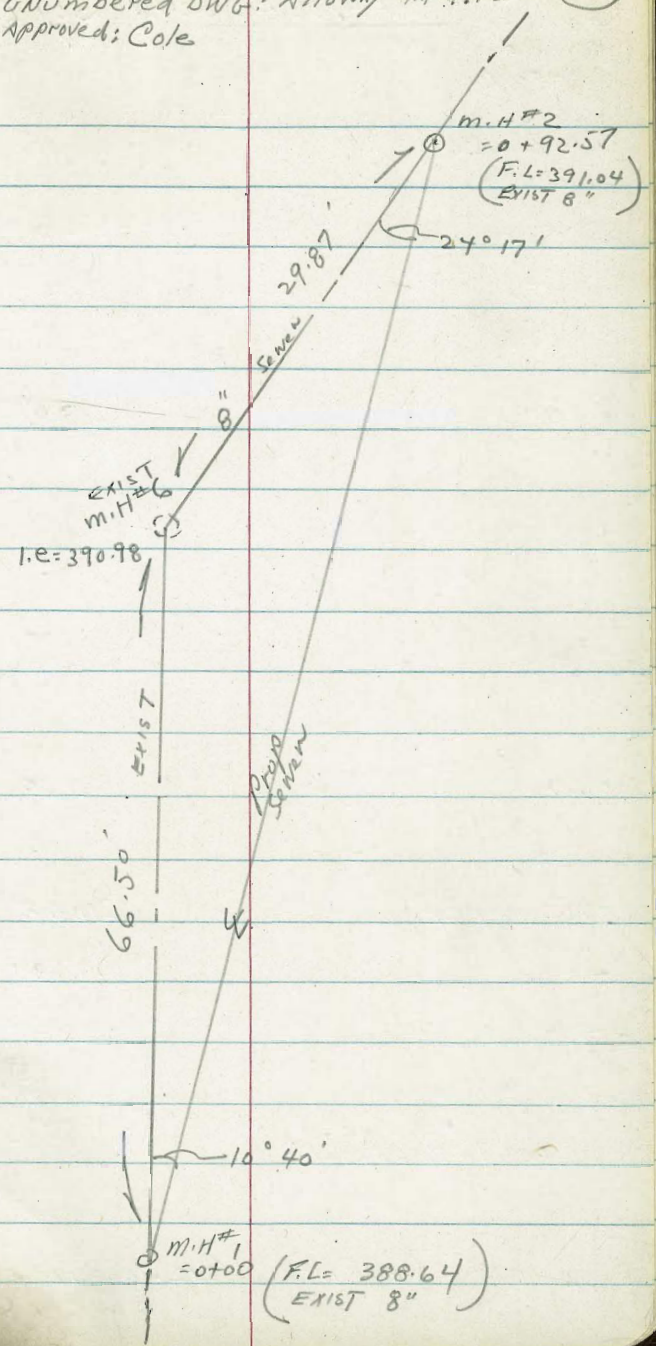
Clark  
Garber  
Moore  
ABTENILLA  
10-1-57  
W.O. 20413

Sewer Line: N/4 AERO DR  
By-PASS W/4 AFTON Rd  
ABANDON Septic-TANK

Ref: unnumbered DWG: Alloway dated: 9-3-57 (77)  
Approved: Cole

0+92.57 m.H.#2	390.04 meet F.L. EXIST 8"
0+75	395.05 390.59 C 4.46
0+50	395.46 389.94 C 5.52
0+25	394.58 389.29 C 5.29
0+00 m.H.#1	388.64 meet F.L. line EXIST 8"

BM = F.L. line EXIST M.H.#6 = 390.98



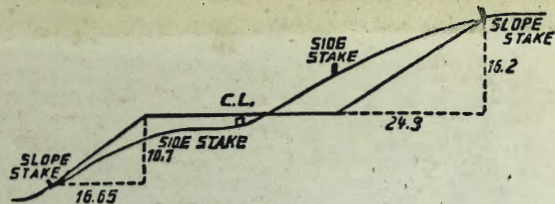
CLARK  
GARBER  
MOORE  
ABRENILLA  
3-19-58  
W.O. 20020

Ely CB: 63rd SLY IMPERIAL

REF: DWG: 5383-D  
(No tie-sheets, No city notes?)

STA	CB	STA	CB (Ely)
	(Ely-63rd)		
0+75	215.67 215.42 Co. 25		
0+50	213.78 213.47 Co. 31		
0+35.13	213.01 212.30 Co. 71		
0+30	212.57 211.90 Co. 67		
0+20	211.70 211.30 Co. 40		
0+15 = End Berm Beg CB	211.29 211.08 Co. 21		
0+10	210.98 210.85 Co. 13		
0+0.0 = END EXIST CB, S Ely 63rd + IMPERIAL	210.47 CHK = CB.EC	1+02.12 = (END CONST. 90° to Lot-Line)	217.80 217.52 Co. 28
B.M. (Dir. Elev. Rod:)	212.70 = TP EXIST. F.H.Y.D. S Ely 63rd + IMPERIAL		





**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**

**SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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 HOLYOKE MASSACHUSETTS  
 NEW YORK CHICAGO BOSTON SAN FRANCISCO