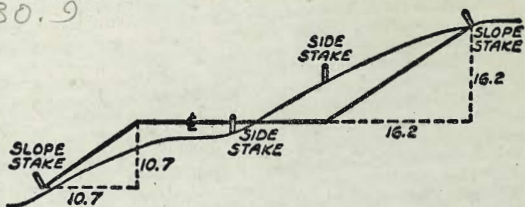


30.9



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

G-364

MICROFILMED

APR 16 1965

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at stake

IMPROVED TABLES
AND
INFORMATION

Set up stake at the point of intersection of the cut and the slope. If it does not make the slight adjustment necessary, - 0.0 -

TABLE No. XIV

To find Tangent and External for curve of any other degree, divide by degree of curve and add constant found in column of conversion. Degree of curve with a given L may be found by dividing tangent (or external) opposite L by given tangent (or external) (or L by given tangent or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

0	
1	
2	
3	
4	
5	
6	
7	
8	
9	
10	1
11	1
12	1
13	1
14	1
15	1
16	1
17	1
18	1
19	1
20	2
21	2
22	2
23	2
24	2
25	2
26	2
27	2
28	2
29	2
30	3
31	3
32	3
33	3
34	3
35	3
36	3
37	3
38	3
39	3
40	4
41	4
42	4
43	4
44	4
45	4
46	4
47	4
48	4
49	4
50	5

Distance ground is column a side stake side stake cut or fill If it does

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24-25	REVISED ALIGNMENT @ SW COR. NOYES & DIAMOND	
26	GRADES ELY SIDE 56-TH, SLY FROM MEADE AVE	8-14-56
27-	GRADES 1 1/2' : 1' QUIVERA BASIN	8-21-56
28-41	GRADES COLINA DEL SOL PARK	9-13-56
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Stampen
Huffman
Blunt
Kelley

CROSS SEC. GARNET ST. MORRELL TO QUINCY

Lt

4-16-56

Rt

W.O. 32472

Tan 9r

Elev & LIP
Tan 9r.

E.P.

E.P.

LIP.

& Rate

2+00

63.40
5.20%
C.O. 0.2

63.17

F0.32

63.38
63.06

63.69

60.55 P.I.

63.80
63.05
(M. 0.75)

63.52

F0.43

63.33
62.90

62.94

63.45
6.07%
C.O. 0.12

1+50

63.68
5.32%
C.O. 0.2

63.44

F0.34

63.66
63.32

63.97

64.85 P.I.

64.08
(63.31)
Mean 0.77

63.82

F0.38

63.60
63.22

63.19

63.72
6.26%
C.O. 0.12

1+00

63.94
5.17%
C.O. 0.2

63.71

F0.32

63.92
63.60

64.24

65.08 P.I.

64.33
(63.58)
mean
0.25

64.05

F0.42

63.85
63.43

63.45

63.97
6.15%
C.O. 0.12

0+50

64.20
4.90%
C.O. 0.2

63.98

F0.28

64.18
63.90

64.50

(75.28 P.I.)
64.56
0.72
(63.84)
Mean

64.30

F0.42

64.10
63.68

63.70

64.21
5.96%
C.O. 0.11

$\left(\frac{45}{26.5}\right)^2 = 0.0288$

0+00 = E. Line
MORRELL ST.

64.48
5.09%
C.O. 0.2

64.25
LIP
26.5

64.25

F0.29

64.46
64.17

64.75

65.60 P.I.

64.85
00.25
(64.10)
Mean

64.56

F0.48

64.36
63.88

63.95

64.48
6.22%
C.O. 0.12

$\left(\frac{85}{26.5}\right)^2 = 0.1056$

B.M.

63.17

P.K. Conc. b/w Wall NW Cor Noyes & Garnet

	T. GY. Rate	LIP	Lt EP		e		Et EP	LIP	TANGY Rate
2+20	52.83 3.96% C=0.02	52.65	F0.49 52.81 52.44	52.91	(53.70 P) 53.01 (52.32) 0.69	52.78	F0.38 52.47 52.09	51.99	52.54 6.45% C=0.07
1+80	54.01 4.26% C=0.02	53.82	F0.35 53.99 53.64	54.10	(34.95 P) 54.23 (53.51) 0.72	53.99	F0.42 53.68 53.26	53.20	53.76 6.60% C=0.08
TP. 54.34			F0.46 55.19 <u>54.73</u>	55.26	(56.13 P) 55.43 (54.77) 0.68	55.19	F0.51 54.96 54.45	54.52	55.03 6.07% C=0.07
1+40	55.21 4.18% C=0.02	55.02	F0.43 56.43 <u>56.00</u>	56.52	(57.46 P) 56.78 (56.10) 0.68	56.53	F0.37 56.36 55.99	55.95	56.43 5.69% C=0.07
1+00	56.45 4.56% C=0.02	56.25	F0.42 57.99 57.57	58.14	(59.06 P) 58.43 (57.80) 0.63	58.23	F0.39 58.13 57.74	57.80	58.20 4.75% C=0.07
0+50	58.01 4.75% C=0.02	57.80	F0.41 59.43 59.02 22	59.72 12	(60.72 P) 60.07 0 (59.42) 0.65	59.90 8	F0.57 59.92 59.35 <u>18</u>	59.65 26.5	59.99 4.04% C=0.07
0+00 = E.L. Noyes St	59.45 5.77% C=0.02	59.19 26.5							(85) ² (263) = 0.1056

Lt

R

RT

(A)

LIP

EP

EP LIP

Top Gr.
% Rate

Top Gr.
% Rate

5+00 = W.L. Olney st.	44.70 3.28% C002	44.55	F033 44.68 44.35	44.75	(4542PI) 44.81 (4420) 0.61	44.54	F044 44.29 43.85	43.85	44.35 5.92% C006
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TP 45.53 4+50	46.15 3.43% C002	46.00	F041 46.13 45.72	46.22	(4691PI) 46.28 (45.65) 0.63	46.03	F049 45.75 45.26	45.31	45.82 6.04% C007
------------------	------------------------	-------	------------------------	-------	--------------------------------------	-------	------------------------	-------	------------------------

4+00	47.60 3.43% C002	47.45	F040 47.58 47.18	47.68	(48.36PI) 47.73 (47.10) 0.63	47.49	F038 47.20 46.82	46.76	47.27 6.04% C007
------	------------------------	-------	------------------------	-------	---------------------------------------	-------	------------------------	-------	------------------------

3+50	49.06 3.85% C0.02	48.89	F035 49.04 48.69	49.18	(49.91PI) 49.23 (48.55) 0.68	48.99	F041 47.68 48.27	48.21	48.75 6.41% C007
------	-------------------------	-------	------------------------	-------	---------------------------------------	-------	------------------------	-------	------------------------

3+00	50.53 4.15% C0.02	50.34	F040 50.51 50.11	50.65	(51.44PI) 50.72 (50.00) 0.72	50.42	F045 50.16 49.71	49.67	50.29 6.68% C0.08
------	-------------------------	-------	------------------------	-------	---------------------------------------	-------	------------------------	-------	-------------------------

2+50 $(\frac{4.5}{26})^2 = 0.0288$	51.95 3.88% C0.02	51.78 26.5	F041 51.93 51.52 22	52.05 12	(52.81PI) 52.13 (51.45) 0.68	51.92 8	F036 51.59 51.23 18	51.12 26.5	51.66 6.38% C0.07 $(\frac{8.5}{26})^2 = 0.1056$
---------------------------------------	-------------------------	---------------	------------------------------	-------------	---------------------------------------	------------	------------------------------	---------------	--

	LIP		LT	EP	±	EP	LIP	ET	Tan. Gr. of Rate
	LIP								
Tan. Gr. & Rate									
				FO 12				FO 52	
2+40	41.26 2.72% C002	41.14		41.24 41.12	41.33	(41.86P) 41.28 4070 0.58	40.93	40.72 40.20	40.27 40.78 6% C0.06
				FO 13				FO 46	
2+00	41.44 2.57% C002	41.33		41.42 41.29	41.55	(42.01P) 41.47 (4093) 0.54	41.14	4094 4048	40.53 41.00 5.30% C0.06
				FO 26				FO 48	
1+50	41.68 2.68% C002	41.56		41.66 41.90	41.81	(42.27P) 41.74 (41.21) 0.53	41.43	41.25 40.77	40.86 41.31 5.32% C0.06
				FO 25				FO 47	
1+00	41.93 3.16% C002	41.79		4191 41.66	42.04	(42.63P) 42.06 (4149) 0.57	41.75	4159 41.12	41.19 41.65 5.43% C0.06
				FO 16				FO 44	
0+50	42.17 3.28% C0.02	42.02		42.15 41.99	42.31	(42.89P) 42.33 (41.77) 0.56	42.07	41.90 41.46	41.52 41.96 5.17% C0.06
				FO 21				FO 44	
0+00 = E.L. Olney St. (45) ² = 0.0288 265	4244 4.15% C0.02	42.25 2.65		4242 42.21 22	42.64 12	(43.33P) 42.70 (42.05) 0.65	4240 8	4226 41.82 18	41.85 265 (85) ² = 0.1056 265 C0.07

	LIP		LT		E		RT		②
	LIP		EP		EP		LIP		Tangr. & Rate
Tangr. & Rate									
			CO ⁰⁷				FO ²⁹		
5+00 = W. L. Pendleton St	35.96 3.69% CO.02	35.79 worked	35.94 36.01	36.21	(36.77P) 36.13 (35.49) 0.64	35.86	35.63 35.34	35.19 (worked)	35.70 5.96% CO.07
			FO ⁰⁷				FO ⁴⁸		
4+50	37.23 3.24% CO.02	37.09	37.21 37.14	37.37	(37.95P) 37.35 (36.75) 0.60	37.03	36.84 36.36	36.41	36.90 5.81% CO.06
			FO ¹⁴				FO ⁵⁷		
4+00	38.38 3.47% CO.02	38.22	38.36 38.22	38.46	(39.14P) 38.44 (37.84) 0.60	38.09	37.94 37.37	37.47	38.00 6.30% CO.06
			FO ²¹				FO ⁵⁶		
3+50	39.49 2.94% CO.02	39.36	39.47 39.26	39.56	(40.14P) 39.54 (38.94) 0.60	39.20	38.98 38.42	38.52	39.04 6.11% CO.06
TP. 39.87			FO ²⁰				FO ⁵⁹		
3+20	40.16 2.72% CO.02	40.04	40.14 39.94	40.22	(40.76P) 40.18 (39.60) 0.58	39.81	39.61 39.02	39.16	39.67 6.03% CO.06
			FO ¹⁰				FO ⁴⁸		
2+80 $(\frac{45}{265})^2 = 0.0288$	40.90 2.87% CO.02	40.77 26.5	40.88 A.97B 22	41.00 12	(41.53P) 40.92 (40.31) 0.61	40.56 8	40.33 39.85 18	39.86 26.5 $(\frac{85}{265})^2 =$	40.39 6.30% 0.1056 CO.06

	LIP		Lt				Et				Rt	
	TAD. Gr.	LIP	ER	12	0	8	ER	LIP	FAD. Gr.			
	Rate	26.5	22				18	26.5	Rate			
			CO ¹¹									
2+00	28.85 3.8490 C.022	28.68	28.83 28.94	29.22	(29.70PI) 29.19			28.68 0.51		28.91		
1+73.64=End cb on Rt.			29.48	29.84	29.96	29.85	29.63	29.65				
			FO ¹⁰									
1+50	30.42 2.83% C.0.01	30.29	30.42 30.32	30.61	(31.04PI) 30.68	30.60	30.19	30.36				
					(30.32) 0.36							
TP. 32.50			CO ⁰⁷							FO ²⁷		
1+0.5=BC. Rt	31.84 1.89% C.0.01	31.75	31.83 31.90	32.00	(32.25PI) 32.00	31.90	31.89 31.62	31.76	31.92 1.85% C.0.03			
					0.25							
0+50		33.53	33.63	33.63	33.56	33.54	33.41	33.45				
0+00=E.L. Pendleton St.		35.15 26.5	35.07 22	35.02 12	(34.91PI) 34.89	34.77 8	34.53 18	34.60 26.5				
					34.87 0.02					(85.7) 26.5 = 0.1056		

Lt

£

Rt

ⓑ

Tan. Gr.
& Rate LIP

EP

EP

Tan Gr
& Rate

2+93⁵=End Cb Lt.

25.65

26.01

26.36

(27.45P)

26.50

26.48

26.26

(0.95)

2+50

27.06

27.35

27.69

(28.44P)

27.75

0.69

2+21=BC Lt. Cb.

28.00

28.27

28.57

(29.08P)

28.54

0
(0.59)

8

18

28.37

$\left(\frac{4.5}{26.5}\right)^2 = 0.0288$
0.02

26.5

$\left(\frac{8.5}{26.5}\right)^2 = 0.1056$

54" STORM DRAIN NOYES ST.; GRAND
AVE TO DIAMOND ST. W.O. 32103

1+18

NOTE: Offset stakes ave
= set 6' W. of pipe
or as noted

1+00

0+75

0+50

2.26 92

0+25

Make Connection
0+00 = N.L. Grand Ave

B.M.

44.78

TBM. P.K. of Noyes & Grand,

36.10

LT.

E

RT

(9)

Ref DW 95.11961-62-56-L

C 12.47

42.38

29.91

C 12.50

42.00

29.50

C 12.78

41.71 ✓

28.93

C 12.09

40.46 ✓

28.37

C 11.84 ✓

38.84

27.80

C 10.50 ✓

37.74

27.24

R.P. Disk 50' W. of N.Y. 7' Mort. Balloon &
E Noyes St.

STORM DRAIN NOYES ST.

2+25

2+00

1+75

1+54.86

1+41⁸⁶ & CONC. ETC.

1+34.86

5.5706

lt. & et (10)

C 11 22
44.38
33.16

C 11.83
44.15 ✓
32.32 ✓

C 11 78
43.26 ✓
31.48

C 12.07
42.88 ✓
30.81

C 12.57
43.12 ✓
30.55

C 12.56
42.85 ✓
30.29

STORM DRAIN NOYES ST.

3+40

6.48 90

C 10.91

49.68
38.77

3+15

Y

C 10.19

47.34 ✓
37.15

2+95

C 10.54

TR 46.50 ✓
35.96

2+75

C 10.41

45.37 ✓
34.96

2+55

C 10.29

44.47 ✓
34.18

2+46⁷⁸ -18⁵⁴ ft.
Type "H" Cb. Inlet N=1

3.37 90

R.P. 12' R.P. 6' 6" Inlet
be. Cb. cb. face on
Line Only Type H. Inlet

C 0.31 C 0.97

44.77 44.77
44.46 43.80

Cb. Gut

R.P. 6' 6" Inlet

C 9.27 C 9.02 C 10.15

44.77 C 44.00 44.00 ✓
35.50 35.00 33.89

18" Inlet

F. 6. Inlet

18" W/W
R.P. 6' 6"

Lt.

±

Rt

(12)

STORM DRAIN NOYES ST.

4+75

C 10. 66

56. 94 ✓

46. 28

4+55

C 10. 74

56. 33 ✓

45. 59

4+35

C 10. 61

55. 32 ✓

44. 71

4+15

C 12. 73

56. 36 ✓

43. 63

3+90

C 13. 41

TR. 55. 42 ✓

42. 01

3+65

64.8 5/0

C 14. 16

54. 55

40. 39

STORM DRAIN NOYES ST.

C 12.77
60.58
47.81

5490

C 12.35
59.91 ✓
47.56 ✓

5465

0.986.90

C 11.64
58.96 ✓
47.32 ✓

5440

C 11.33
58.40 ✓
47.07

5415

Y

C 11.27
58.04 ✓
46.77 ✓

4795

C 11.18
57.75 ✓
46.57 ✓

4787 \$ CONC. ETC.

LT. 4-23-56 & RT (7A)
 NOTE: Stakes from 7+15 N/4
 = offsets are 6° Lt. Or as Noted

STORM DRAIN NOYES ST.

7+40

C 12 60
 61.89
 49.29

7+15

C 12 55
 61.60
 49.05
 6° Lt.

6+89⁰⁹ & Type C^u C.O. N°1

14° S/4 of N.L. Garnet.

Line Chs/⊕
 6' Lt.

C 11 90 F 0 11
 60.69 60.69
 48.79 60.80
 F.L. 0
 6' Rt. Top C.O.
 C 12. 09 Chs/⊕
 61.64_v 6' Rt.
 48.55

6+65

C 12. 76
 61.66_v
 48.30

6+40

6+15

C 12 64.
 60.70_v
 48.06

TR M.

63.17-26317 P.K. CONC. b/k, Wall NW. Cor Noyes & Garnet

STORM DRAIN NOYES ST.

8+65

2.3890

8+39⁸⁶

X

8+37⁹ & CONC. ETC.

8+15

0.59070

7+90

7+65

lt.

£

rt

(15)

C 12.62 ✓
63.49
50.87

C 12.19 ✓
62.47
50.28

C 12.19 ✓
62.45
50.26

C 12.92
62.96
50.04

C 13.06 ✓
62.83
49.79

C 12.75
62.29
49.54

STORM DRAIN NOYES ST.

10+15

9+90

9+65

9+40

9+15

8+90

2.38%

LT

±

RT

(16)

C11 00 V

65.44

54.44

C11 21

65.06

53.85

C12 46

65.71

53.25

C12 09 V

64.75

52.66

C12 20 V

64.26

52.06

C12 57 V

64.04

51.47

STORM DRAIN NOYES ST.

11+65

LT. E RT (17)
C12 68 ✓
70 69
58.01

11+40

C12 69 ✓
70 11
57.42

11+15

C12 86 ✓
69 68
56.82

10+90

2.38%

C12 97 ✓
69 20
56.23

10+65

C13 01 ✓
68 64
55.63

TP

66.52

C11 48
66 52
55.04

10+40

STORM DRAIN NOYES ST.

12+90

12+65

12+40

12+15

11+8986

11+87⁶¹ & CORR. ENC

3.09390

X

2.3896

Lt

€

Rt

(10)

C11.94 ✓
72.67
61.73

C11 31 ✓
72.27
60.96

C11 35 ✓
71.53
60.18

C11.34 ✓
70.75
59.41

C11 47 ✓
70.08
58.61

C11 59 ✓
70.14
58.55

STORM DRAIN NOYES ST.

C 11 39

14+00

7.77
65.18

C 11 18

13+75

7.561
64.43

C 10 71

13+50

7.444
63.73

C 10.73

13+25

7.374
63.01

TP. Ch. Ctr. BC Rt. SE Emerald St.

75.35 - 65.19

F0.55 F1.38 C016

F0.67

C549

F1.52 F0.69 F1.77 F0.94

12+98⁷⁸ 4" Type B-2 (16")
Cb. Inlets Lt. & Rt.
N° 2 Rt.; N° 3 Lt.

73.17 73.17 4.34
73.72 74.55 74.18
G+S → Cb G+N
~~BC Cb Ret.~~ ~~BC 16'~~
3' brcb

74.34
75.01
→ Cb
3' brcb

62.25
F.L.
5 1/2"

72.99
67.50
30E
F.L. Inlet

2.97 2.97 3.24 3.24
74.49 73.66 75.01 74.18
G+S → G Cb+N → G
BC-16' BC. Cb. Ret

23.75 5/4 of S.W. Emerald St.

12+98⁷⁸ 4" Type "C"

C.O. N° 2

F1.25
73.36
74.62
Cb. @
4" Inlet
3' brcb.

C636
73.36
67.00
F.L.
B-2 Inlet
Lt.

C1084
72.84
62.00
0
F.L.
54"

F1.46
72.84
74.30
0
Top C.O.

C684
72.84
66.00 →
Inlet
18" Rt.

3.093 90

STORM DRAIN NOYES ST.

15+37⁵⁵ = ϵ CONC. ETC.

15+25

15+00

14+75

14+50

14+25

2.9 90

47.

ϵ

RT

(20)

C12 39
81 56
69.17

C13 17
81 97
68.80

C13 10
81 18
68.08

C12 98
80 33
67.35

C12 76
79 39
66.63

C12 77
78 67
65.90

STORM DRAIN NOYES ST.

16+72.19
P.O.C. $\Delta = 26^\circ$

9.30'

16+62.89
P.O.C. $\Delta = 13^\circ$

9.30'

Δ @ Ctr.
 $\Delta = 65^\circ R = 41' L = 46.51'$
 $16+53.59 = B.C. \& Pipe$
 $= 19^\circ 51' 4$ of S.L. Diamond

TP

90.78

16+27

16+00

TP

84.63

15+75

15+50

2.5489%

2.9%

REVISED
SEE PG 24



C 15.18
88.18
73.00

C 14.75
87.31
72.56

C 14.36
86.88
72.52

C 14.29
86.05
71.76

C 14.10
85.08
70.98

C 12.92
83.17
70.25

C 13.17
82.70
69.53

STORM DRAIN NOYES ST.

17+23.12 = END Plug

P.O.C. $\Delta = 10^\circ$

C 13.73

87.93 ✓

74.20 ✓

7.15

A @ Ctr.

$\Delta = 20^\circ R = 41' L = 14.31'$

B.C. 17+15.97

C 13.95

87.98 ✓

74.03

14.12 Tan

17+01.85

Δ Box $35^\circ \times 5^\circ$ Wide $L = 14.31'$

11.75 Tan

C 0.68 C 14.43

C 10.48

88.18 88.18

88.18

87.50 73.75 ✓

77.70 ✓

03 F.L. BOX

25

face Ch.

Inlet 18"

To N.

17+00.10

E.C. $\Delta = 65^\circ$

73.70

9.31'

16+90.79

P.O.C. $\Delta = 52^\circ$

C 14.87

88.31 ✓

73.47

9.30'

16+81.49

P.O.C. $\Delta = 39^\circ$

C 15.10

88.33 ✓

73.23 ✓

9.30'

REVISED

LT E RT

Lt.

±

rt.

(23)

STORM DRAIN NOYES ST.

B.M.

87.65

87.69 ± L&T, Diamond & Noyes

C 10.70

89.50

78.80

C 0.55

C 1.38

C 10.27

C 2.38

C 1.55

862

8862

897

89.60

89.60

88.07

87.24

78.70

87.22

88.05

cb

G

Outlet

G

cb.

R.P. 5' 6k cb.

C 9.41

87.61

78.20

R.P. 6' Lt.

0+11.20³⁶0+39³⁶ ± Type 'G' Inlet @ N.W. Ret.
Diamond & Noyes.0+20⁶
0+19⁶⁸0+00 = Inside face of Inlet N^o 4
= 17+01.85-51" Pipe (see P. 22)

77.70

Inlet.

C 13.87

88.32 ✓

74.45

17+34.28 = End Plug

4'

17+30.28

E.C. 4 = 20°

C 13.70

88.06 ✓

74.36

7.16

REUSED

ct. ± et.

REVISED ALIGNMENT @ SW COR. NOYES #

DIAMOND STS.
17+13.88
P.O.C. Δ = 78° 23'

C13.44
87.71 ✓
74.27

18.50'
17+05.38
P.O.C. Δ = 4 = 66° 40' = ± LUG. 37.33' Pipe

C13.82 C9.87
87.84 ✓ 87.84
74.02 77.97 ✓
Inlet 18"
N.Y.

1208
16+93.30
P.O.C. Δ = 50° 00'

C14.57
88.24
73.67 ✓

12107
16+81.23
P.O.C. Δ = 33° 20'

2.90578

C14.92
88.24 ✓
73.32

12107
16+67.16
P.O.C. Δ = 1641' 30"

C15.17
88.14 ✓
72.97
8' 4.

12107
Δ = 90° 06' R = 415' L = 65.26'
16+57.02 BC. ± Pipe

C14.48 ✓
87.10
72.62

cont'd from p 21

lt € et

0+37.35 = 5ly Inside face Type 'G' Inlet

78.70

0+18.67 = Mid Pt. 18' Pipe

C 19.29
87.62
78.33
6' Lt Wly

0+00 = 17+05.38 18" Pipe Nly

77.97
Inlet

17+30.35
End of Pipe

C 13.10
87.85 ✓
74.75

P.O.T. 8'
17+22.35
EG. 4 = 90° 06'

C 13.26
87.78 ✓
74.52

8.17

Ref DW9 12834-4 8-14-56

(26)

GRADES ELY SIDE 56-TH ST; SLY FROM.

SOUTH LINE MEADE AVE W.O. 32708

B.M.

NOTE: Stakes Set 5th bk of
Cb. face

Stamped
Huffman
Taylor
Blunt
Johns

0+91.69

C 2.42 ✓
3.51
421.09

0+71.69 - Set chis / Cross

C 2.49 ✓
3.91
421.42

0+51.69 - Set chis / (A)

C 2.98 ✓
4.50
421.52

0+31.69

C 2.75
24.37
421.62

0+00 = S.L. Meade

B.M.

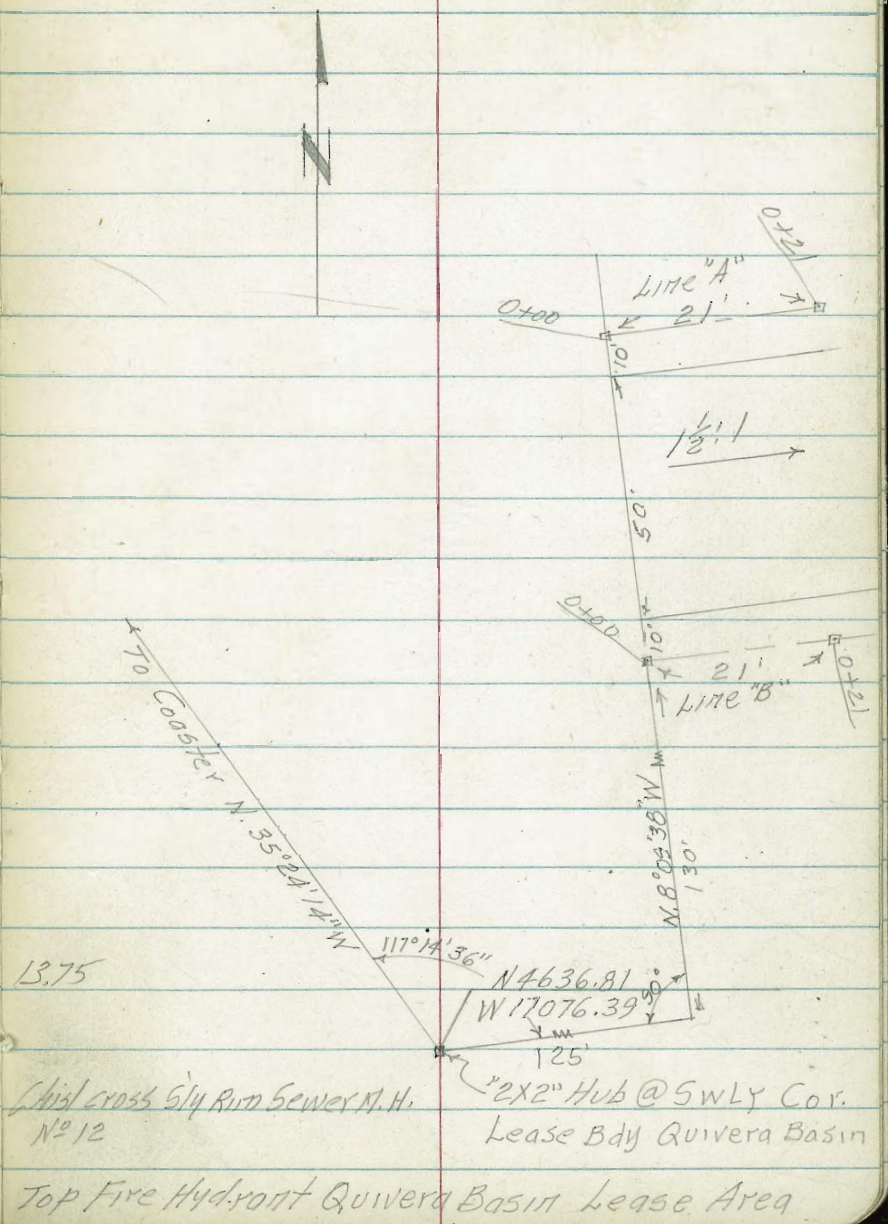
423.43

P.K. Nail face Conc. Blk Wall 5+73-25' Lt
orig. X-sec (File K-17)

GRADES FOR PROPOSED CONC. SLAB

QUIVERA BASIN. W.O. 64010

Sta	+	H.I.	-	Elev	Grade
					C11 ³⁴
"A" Line					7.34
0+21			8.64	7.34	-4.00
					C1 ⁰⁰
"A" Line					11.00
0+00			4.98	11.00	10.00
					C11 ⁰⁶
"B" Line					7.06
0+21			8.92	7.06	-4.00
					C0 ⁷⁹
"B" Line					10.79
0+00			5.19	10.79	10.00
	3.68	15.98			
T.B.M.				12.30	
B.M.			3.20	13.75	13.75
	4.65	16.95			
T.B.M.			5.20	12.30	
	3.75	17.50			
B.M.				13.75	

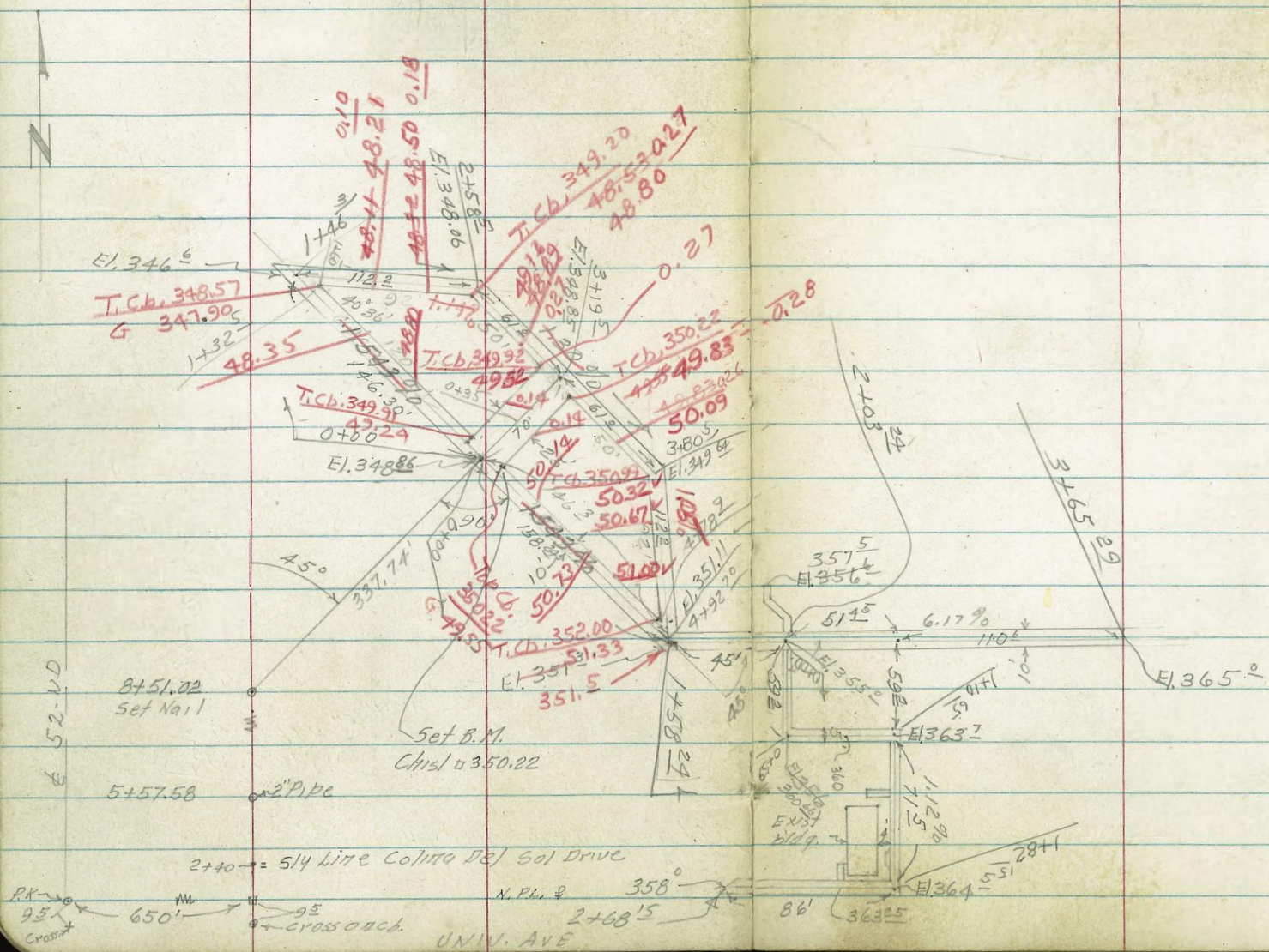


GRADING, WALKS & PAVING COLINA DEL SOL PARK

W.O. 21409

Ref DWG 3011-AD 9-6-56
 " " 2162-D
 " FB. 2148
 65

Stampen (28)
 Schelitt
 Blunt
 Kelley



GRADES COLINA DEL SOL PARK. See Sketch Pg. 28

1+46³ = E.P.I.

346.60

138

1+32⁵

346.81

40

0+92⁵

347.43

40

0+52⁵

348.05

40

0+12⁵

348.67

0+00 N.W. Loop

348.86

B.M.

363.11

P.K. Nail Core Base Flagpole Rec. Bldg.

REVISED

-1.543%

3+07

348.69

25'

2+82

348.36

235

2+58⁵ ~~4~~ P.I.

348.06

6⁴

REVISED

2+52^L

347.97

30'

2+22^L

347.58

31'

+ 1.3 % ↑

1+91^L

347.18

44.80

0+35 & 25' Walk (see Sketch)

4+78²

30'

4+48²

31'

4+17²

37[±]

3+80[±] & Pl.

23[±]

3+57

25'

3+32

25'

Lt

±

et

(31)

348.68

349.03

350.92

350.53

350.13

349.64

349.34

349.01

REVISED

↑
+1.390

1+80⁷⁴

22⁵

1+58²⁴ P.I. $\Delta = 45^\circ$ Lt. Offsets 3' Lt. E.P.

25⁷⁴

1+32⁵ = End Curb.

40'

0+92⁵

40'

0+52⁵

40'

0+12⁵ E/4

C 1. ³³
~~62.08~~
5 ³³
~~353.25~~
354.00

60.19
51.69
~~351.30~~
⁵⁰

~~350.90~~

~~350.29~~

↑
+ 1.543%

~~349.67~~

~~349.05~~

3+25

C 1. 23
3 74
362.51

25'

3+00

C 1. 52
2 49 ✓
360.97

25'

2+75

C 2. 05
61.48 ✓
359.43

7P.

359.95

25'

2+50

C 2. 49
60.37 ✓
357.88

25'

2+25

+ 6.17%

0.50
C 2. 71 ✓
59.05 ✓
356.34

2176

2+03²⁴ = 0

1.00
C 2. 52 ✓
57.50 o.k.
355.00
356.50

22 5

0+84² Offsets 3' Lt. EP 5' ahead

F 0.50
~~C 1.65~~
61.65 ✓
~~360.00~~
362.15

257

0+59² = P.I. 4 = 90 Lt. bk. Tan.

Grade
~~C 4.66~~
60.66
~~356.00~~
360.66

29⁶

0+29⁶

F 0.29
~~C 3.29~~
58.79
~~355.50~~
359.08

29⁶

2+03²⁹ = 0+00 - 5' walk 5/4, Offsets 3' Rt EP

1.00
~~C 2.50~~
57.50
~~355.00~~
356.50

3+65²⁹ = End 10' walk

C 1.05
6.05
365.00

↑

15²⁹

C 1.23
5.28
364.05

6.17 90

3+50

25'

2+25 15

Grade
FO ~~24~~
63.76
364.00

21 5

Grade
FO ~~19~~
64.01
364.20

2+03 65

T.P. on P.K. 1+82 15 for Tan — 364.41

21 5

C.O. 65
5.15
364.50

1+82 15 P.I. $\angle = 90^\circ$ Rt. bk. Tan

23 80

C.O. 11 V
4 34
364.23

1+58 35

23 85

Grade
3 97
363.97

1+34 5

+ 11290

23.85

F1.36
~~F1.31~~
~~2.39~~
363.70
2.34

1+10 65 P.I. $\angle = 90^\circ$ Rt. bk. Tan

2+68¹⁵ = End walk

21 5

2+46⁶⁵

21 5

Grade
~~67.60~~
1.60
360.00

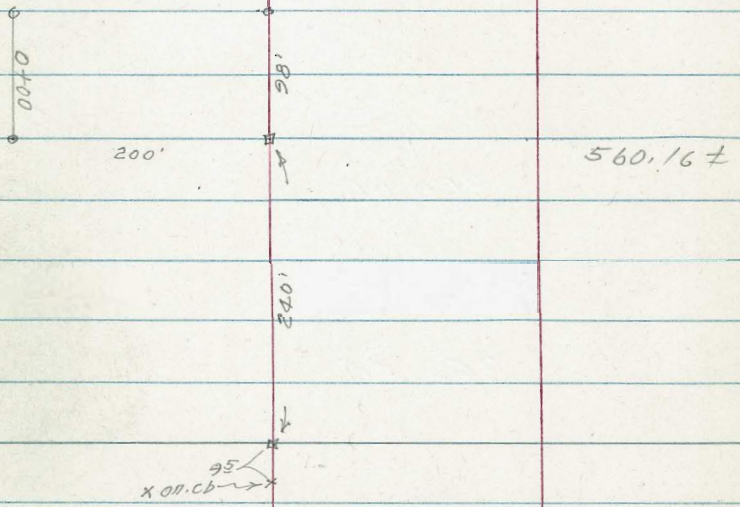
Grade
~~67.05~~
3.05
362.00

9-11-56

(57)

Stampex
Blunt
Kelley

ALIGNMENT DEL SOL RD



560.16 ±

7460.16

GRADES COLINA DEL SOL RD.

2+60

2+00

TP

1+50

1+00

0+50

0+00

TP

B.M.

334.28

361.28

363.11

(see pg. 29)

Lt.

±

Rt

(38)

9-12-56

C4^o

36.85
332.8

C3^o

32.9
329.0

F05

9.30
329.80

F0²

25.82
326.0

L

L

R

(39)

5+60

C4⁶58.63
354.0F1⁸49.23
351.0

7P

342.67

C2⁰55.95
353.9C0²51.13
350.9

5+10

7P

346.55

C0⁹51.37
350.5C1⁰48.55
347.5

4+60

C0³46.03
345.7

Grade

42.67
342.7

4+10

C0⁹19
341.0F0²⁰37.80
338.0

3+60

C1⁵39.19
337.7F1⁵33.2
334.7

3+10

B.M. 363.10 — 363.11 (Starting Bench)

TP. 361.59

TP. 252.73

TP. 343.73

TP. 334.42

7+60

346.45

7+10

F29
51.63
354.5

F2^o
340.3
342.3

TP.

352.30

C 7.2
55.52
348.3

F 1.7
43.6
345.3

6+60

6+10

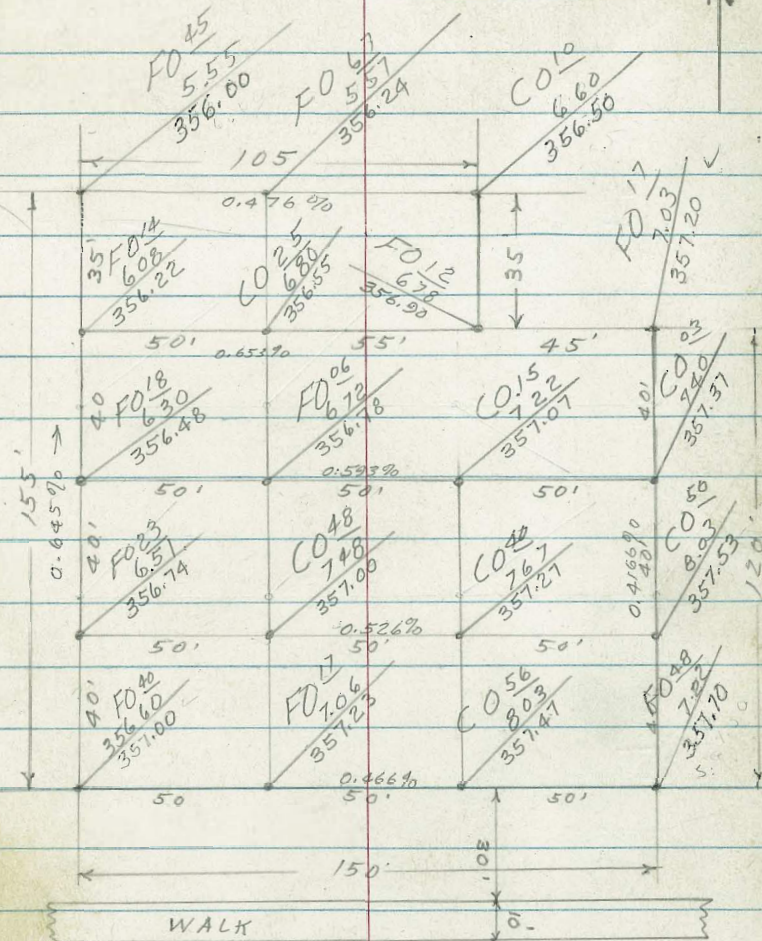
C 7.4
58.50
351.1

F 1.7
46.4
348.1

SUBGRADES VOLLEY BALL & BASKETBALL
COURT COLINA DEL SOL PARK W.O. 21409

9-13-56
NOTE: Denominators Indicate
Subgrades; Numerators
denote Top of Stub Elev's.

Stamper
Blunt
Kelley (A)



B.M.

363.11

P.K. Nail Base Flagpole

L

Ref Fb 2253 ϕ
" DWG 3153-D
Curb
Rough Curb 9-19-56

RT (22)
Curb
Rough

GRADES ROSEFIELD ST. 67TH TO 68TH

W.O. 32533

B.C. $\Delta = 54^{\circ}28'$ Lt
P.O.C def $\Delta = 8^{\circ}48'12''$ Rt

Meet.
444.85
4.98

F0.28
717
447.45

C-3° bk. Cb = 8.264'

9.73 Lt

9.21'

Set Hub 47 (60)
0+48 $\frac{3}{2}$ = E.C.
SEC. Cb Ref Cb R = 30'
 $\Delta = 88^{\circ}02'$

- 44.40 51' P.O.C

~~C0 02~~ ~~F0 30~~
5.32 6.34
445.30 446.69

F0.26 C2.50
747 50.23
447.73 447.73

9.73 Lt

C3.88 F0 21
9.51 5.92
445.63 445.63 445.70

P.O.C. $\Delta = 27^{\circ}14'$

9.73'

F0 23
5.62
445.85

P.O.C. $\Delta = 13^{\circ}37'00''$

9.73'

C1 19 F0 24
7.24 5.86
446.10 446.10

27 $\frac{72}{2}$
0+26 $\frac{72}{2}$ = E.C. NE Set chis. 1 @ ctr.
Cb. Ref. Cb. R = 41.28'
 $\Delta = 27^{\circ}58'58''$

Set Chis. + RR 0 - 33 $\frac{25}{2}$ W. Walk. 67th St.

0+00 = P.K. Nail 25' W. E.L. 67th St.

B.M.

445.70

P.K. Nail 0+00

ROSEFIELD

LT
Curb
Earth

±

RT (43)
Curb
Earth

C2⁶⁵FO³⁰

0.65

7.70

448.00

448.00

448.50

FO.46

C1.38

8.57

50.41

449.03

449.03

FO³⁸

6.96

447.34

447.86

FO⁴⁰

8.00

448.40

C3.15

C3²⁴

50.65

50.74

447.50

447.50

B.C. 67+11 def 4 = 44°01'

9.22

P.O.C. def 4 = 35°12'48"

C0.28

7.53

447.25

9.22

P.O.C. def 4 = 26°24'36"

FO⁰⁵

7.15

447.20

9.22

P.O.C. def 4 = 17°36'24"

FO¹⁴

7.14

447.28

9.22

ROSEFIELD

3+13⁶⁶Curb
Rough

Curb

FO 25
3 19
453.44 453.44

453.81

FO 47

3 80
454.27

2+93^{66v}

CO 68

FO 29

3 72 2 75
453.04 453.04

453.41

FO 28 C O. 87

3 59 4 74
453.87 453.87

2+73⁶⁶

FO. 18

2 39
452.57

452.94

FO. 23

3 17
453.40

TP.

453.06

2+50^v

CO 6

FO 15

2 5 1 80
451.95 451.95

452.33

FO 28 C 1 17

2 52 3 97
452.80 452.80

TP.

450.66

2+00^v

C 1.24

CO 03

1 87 0 66
450.63 450.63

451.06

FO 13 C O. 84

1 42 2 39
451.55 451.55

chis 1 ⊕

1+50^v

C 1.71

FO 05

1 03 9 27
449.32 449.32

449.78

FO 49 C 1.1

9 80 1 4
450.29 450.29

ROSEFIELD

LT
Curb
Rough

E

RT (25)
Curb
Rough

4+39 $\frac{46}{19}$ = W. Lat
19' RT

454.95

C0.15
5.58
455.43
RR 3'E

14 B

C0.36 F0.29

C5.18 F0.18 C1.82

4+24 $\frac{64^v}{N \ 1. R + 30}$ = S. Lat

4.83 4.18
454.97 454.47

454.87

7.18 5.17 7.18
452.00 455.35 455.36
S. Lat
5. BR R

31'

F0.31

F0.18

3+93 $\frac{6.6}{}$

3.99
454.30

454.71

5.02
455.20

C0.41 F0.46

F0.4L C1.70

3+73 $\frac{6.6^v}{}$

4.60 3.73
454.19 454.19

454.59

4.66 6.77
455.07 455.07

F0.39

F0.36

3+53 $\frac{6.6}{}$

3.63
454.02

454.40

4.51
454.87 454.67

C1.38 F0.26

F0.42 C1.25

3+33 $\frac{6.6^v}{}$

5.15 3.51
453.77 453.77

454.14

4.11 5.85
454.60 454.60

ROSEFIELD

$\Delta = 38^\circ 40' 52''$
P.O.C. P.

10.62'
 $\Delta = 18^\circ 23' 31''$
P.O.C.

9.63

$6 + 28 \frac{73}{100} = BC.SW.$
Cb. Ret Cb. R = 30'
 $\Delta = 38^\circ 40' 52''$ L = 20.25'

6+00'

5+50'

5+00'

4+50'

TR

10 59

LT
Curb
Rough Curb

FO³⁹ FO⁰¹
5.03 5.41
455.42 455.42

FO⁴⁹ FO²⁸
4.66 4.87
455.15 455.15

FO⁰⁸ FO⁴⁰
4.80 4.48
454.88 454.88

FO²² FO³⁵
4.39 4.26
454.61 454.61

454.86

E

455.94

455.79

455.53

455.27

455.00

ET (8)

Curb. Curb
FO²⁸ FO⁸²
6.83 7.37
456.55 456.55

CO⁰⁵
6.47
456.42 456.42

FO¹³ CO⁸¹
6.27 7.21
456.40 456.40

156.10 156.10

FO²⁰ CO⁹⁰
6.05 7.15
456.25 456.25

FO¹⁶ CO⁴³
5.84 6.43
456.00 456.00

FO¹⁴ C1.64
5.60 7.38
455.74 455.74

FO²⁶ C1.68
5.23 7.42
455.49 455.74

ROSEFIELD ST.

lt
Curb
Rough

Curb

E

rt
Curb
Rough

Set R.P. 31.97' E. of W.L. 68-4454 of $\frac{1}{4}$
Rosefield Produced Ely.

$\angle = 34^{\circ} 52' 12''$
P.O.C. $\frac{1}{4}$.

FO⁰⁷ CO³⁰
5.60 5.97
455.67 455.67

9.05"
 $\angle = 17^{\circ} 35' 24''$
P.O.C.

CO.31
5.96
455.65

9.21'
 $d = 57.29578$
 $b + 32^{\circ} 02' = B.C.N.W.Cb.$
Ref. Cb. R = 30' L = 18.26'
 $\angle = 34^{\circ} 52' 12''$

FO²⁰ CO²⁷
5.46 5.87
455.60 455.60

18"
GRADES STORM DRAIN NLY UNIV. AVE, ELY 54TH

W.O. 20556

1+25

T.P. Nail in Tree

33 2.43

1+00

0+75

0+50

0+19⁸⁸ = E.C.

B.M.

323.00

Ref DWG 6178-B
NOTE: Offsets 7' ET

9-20-56 (48)

Stampen
Bluff
Kelley

C 3.50
35.37
331.87

C 0.34
30.44
330.10

C 0.86
9.18
328.32

C 1.54
8.09
326.55

C 2.26
26.67
324.41

= F.L. End Pipe

9-20-56

18" DRAIN

B.M. 323.00 - 323.00

T.P. 332.43

2+09⁸⁸ - Set stake for End of Pipe 2' Ahead of 7' Rt.

To Avoid Rubbish Pipe

2+07⁸⁸ = End Drain

1.90
4.66
337.76

2+00

1.65
8.85
337.20

1+75

1.88
7.30
335.42

1+50

4.00
7.65
333.65

GRADES 18" DRAIN PARK ROAD MISSION BAY

0+59.27 E.C.A = 50°

C10.72
14.07
3.35

13.27

C10.06

13.29
3.23

0+46 P.O.C.A = 33°06'15"

13

C10.34

13.45
3.11

0+33 P.O.C.A = 16°33'08"

13

X@Ct.

2d = 76.39438

A = 50° R = 45'

0+20 = B.C.Lt

F5.59

C10.75

13.74
2.99

821
13.80

Grade C10.86

F0.14

0+00 = E Type C C.O. 13.80

13.66
2.80

13.66
13.80

P.O.C. def'd = 7°45'

Rk.R.P.

F.L.

TOP

C =

R = 87' A = 15°30'

B.C. Existing Drain 15'

C =

T.B.M.

0-27¹ R.P. P.K.

13.80

B.M.

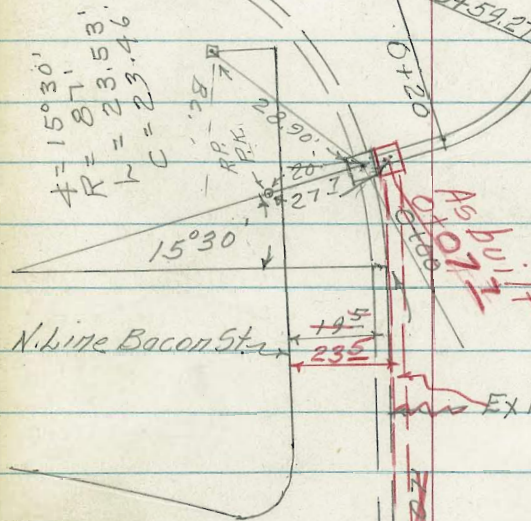
14.04

NOTE: For Additional
Grades See G-34A

Ref. Dwg 3157-D

Sheet 2

Stakes 10' Int.



cont'd Pg. 52
B.C. (50)
2+19.27

160'

A = 50°
R = 45'
V = 15.92'
T = 20.98'

0+59.27

0+20

0+00

0+20

0+00

0+20

0+00

0+20

0+00

0+20

0+00

0+20

0+00

0+20

0+00

0+20

0+00

Existing 60" RCP Drain

WEST PT. LOMA

BLVD

18" DRAIN CONTD

2+00

C 6 76
1295
6.19

~~C 8 89
1295
4.66~~

1+95 New F.L.

6.15

6.15
C 7 67
13.27
5.60

~~C 8 83
13.26
4.43~~

1+75

↑

C 8 42
1333
4.91

~~C 9 15
1335
4.20~~

1+50

2.74 %

C 9 42
1365
4.23

~~C 9 72
1368
3.96~~

1+25

1+06 = End Laid Pipe

1+00

3.71
F.L.

~~C 10 23
1396
3.73~~

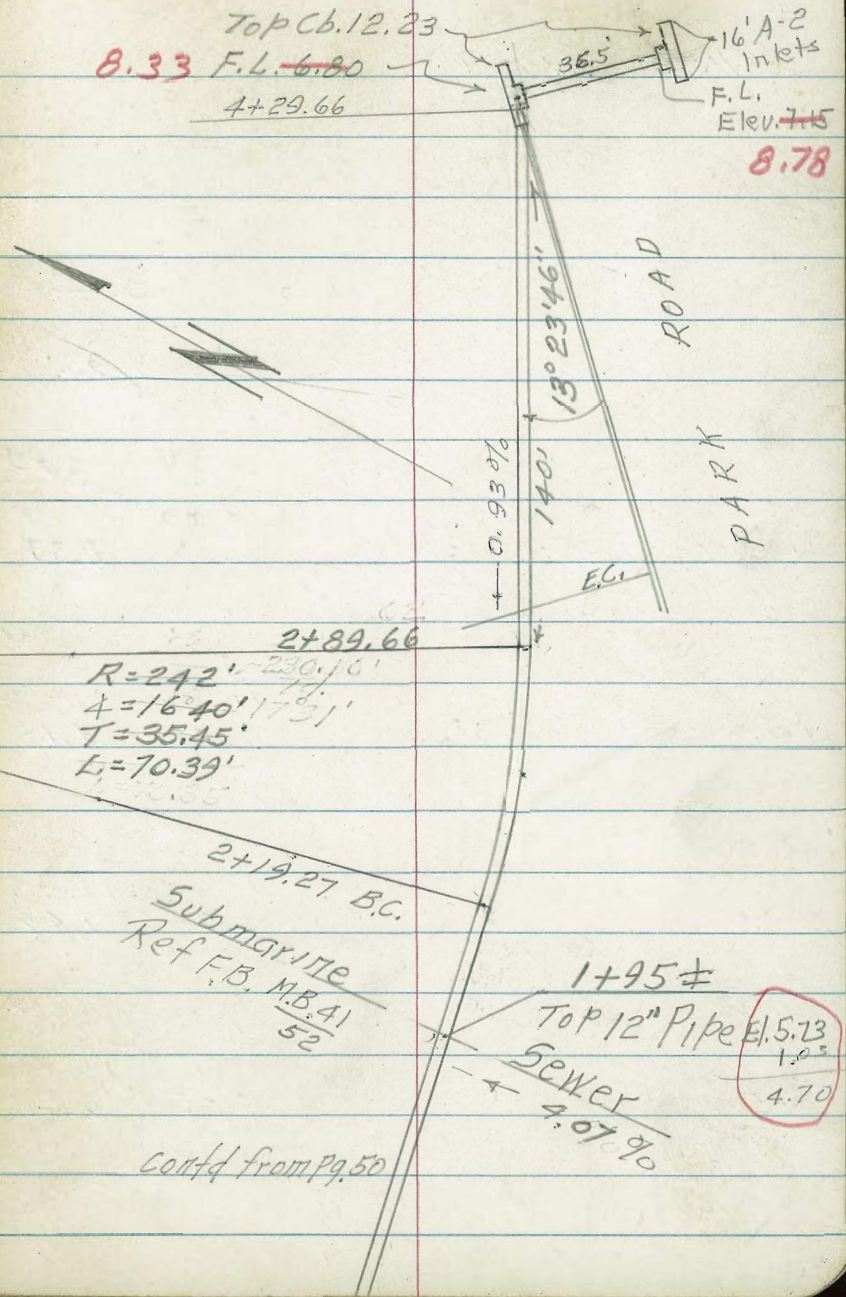
0+75

~~C 10 69
1419
3.50~~

15.73

18" DRAIN CONTD

3+25	C6²²	C5²⁴
	12.04	12.05
	5.82	6.81
3+00	C6⁵⁶	C5⁴⁸
	12.15	12.17
	5.59	6.69
10.34	C6⁷¹	C5⁵⁸
	12.20	12.22
	5.49	6.64
E.C. 2+89.66 EC, def Δ =		
22.39 C =	C7²⁵	C6⁰²
	12.53	12.55
	5.28	6.53
2+67.27 POC, def Δ = 5° 40' 56"		
24 C =	C7⁵⁹	C6²⁵
	12.65	12.66
	5.06	6.41
2+43.27 POC, def Δ = 2° 50' 28"		
24' C = 23.99	C8⁰²	C6⁵⁴
d = 7.102782	12.86	12.83
2+19.27 = B.C. Lt.	4.84	6.29



contd from pg. 50

Lt

Rt

18" DRAIN CONTD.

~~C 4²⁵~~ C 3⁷³
 10' Lt. 11.05 11.07
 0+00- 6.80 0+00- 7.34

~~C 5⁰³~~
 11.23
 10' Lt. 6.80

~~C 4⁴⁵~~ C 3⁸³
 RR Rt → 11.25 11.27
 6.80 7.34
 F.L. Top cb.

~~C 4³⁹~~
 11.36
 6.97
 F.L.
 & Rd

~~C 4⁰²~~
 11.17
 7.15
 F.L.
 0+365

4+29.66 = & Rd Sta. 5+73.88
 = 514. Inside face type A-2 1/2 let
 35x35 Inside.

~~C 4⁷⁰~~ C 4⁰⁴
 11.22 11.23
 6.52 7.19

~~0+825~~
 10' Lt
 C 3⁸²
 11.38
 7.56

~~C 3⁴⁰~~
 11.19
 7.79

4+00

~~C 5⁶⁶~~ C 4⁸⁹
 11.94 11.95
 6.28 7.06

3+75

~~C 6⁰⁵~~ C 5¹⁸
 12.10 12.12
 6.05 6.94

3+50

Ref. Dwg. 3757-D
sheet 2

4-30-57

Stampel (54)
Blunt
Kelley
Wentworth

NOTE: Offsets
= 5' RT.

C 2 87
12 80
9.93

10" H₂O MAIN PARK ROAD F.L. GRADES

2+50

C 2 67
12 99
10.32

2+00

C 2 30
13 00
10.70

1+50

C 2 41
13 51
11.70

1+00

.783 5/16

C 2 60
14 10
11.50

0+50

0-10- Make Connection W. Pt. Loma & Bacon St

0+00 = E. W. Pt. Loma & Bacon

T.B.M.

13.80

20' R.P. Sewer

B.M.

GRADES H₂O MAIN PARK ROAD

5+00

4+50.40 = \pm E.C. def $\Delta = 16^{\circ}37'45''$

50.10

$c = 52.32'$

4+00 P.O.C. def $\Delta = 10^{\circ}51'15''$

23.16

$c = 23.04'$

\pm Sta. 6" Lat. 50' Pt. Radial
3+77.84 P.O.C. def $\Delta = 8^{\circ}18'52''$
End 8" Begin 6"

28.94

$c = 28.94'$

\pm Sta 9
3+50 P.O.C. def $\Delta = 5^{\circ}07'28''$

46.45

$c = 46.45'$

$d = 6.611051$

$L = 150.92$

$R = 260' \Delta = 33^{\circ}15'30''$

3+05.28 = B.C. Lt

3+03 \pm = \pm Pressure Sewer Crossing

C 2 92

11 42

8.50

C 2 95

11 55

8.60

C 2 86

11 76

8 90

C 3 00

12 00

9.00

C 2 69

12 69

10.00

50'

C 2 96

12 16

9.20

C 2 82

12 32

9.50

8.60 \neq = Elev. Top Pipe

GRADES H₂O MAIN PARK ROAD

2+00 = End 2" Line

1+50

1+00

0+50

0+00 2" Line

5+62.63 = 2" Copper Service 200' Rht

5+50

TP 5+56

11.18

€
C 2 53

12 53

10.00

C 3 27

12 52

9.25

C 4 08

12 58

8.50

C 4 45

12 20

7.75

7.00

C 2 58

11 18

8.60

GRADES H₂O MAIN PARK ROAD

B. M. 14.04 — 14.03

8+35.63 = End 6" Line

40'

7+95.63

40'

7+55.63

40

7+15.63 = P.I. & Pt. = 59°27'11"

6+78

6+40.63 = 65'-1" Copper Service Lt.

6+00

C 2 86
12 86
10.00

C 3 08
12 78
9.70

C 2 70
12 05
9.35

C 2 40
11.40
9.00 RP, 5' RT BR. TAN

C 2 55
11.25
8.70

C 2 66
12 66
10.00
65'

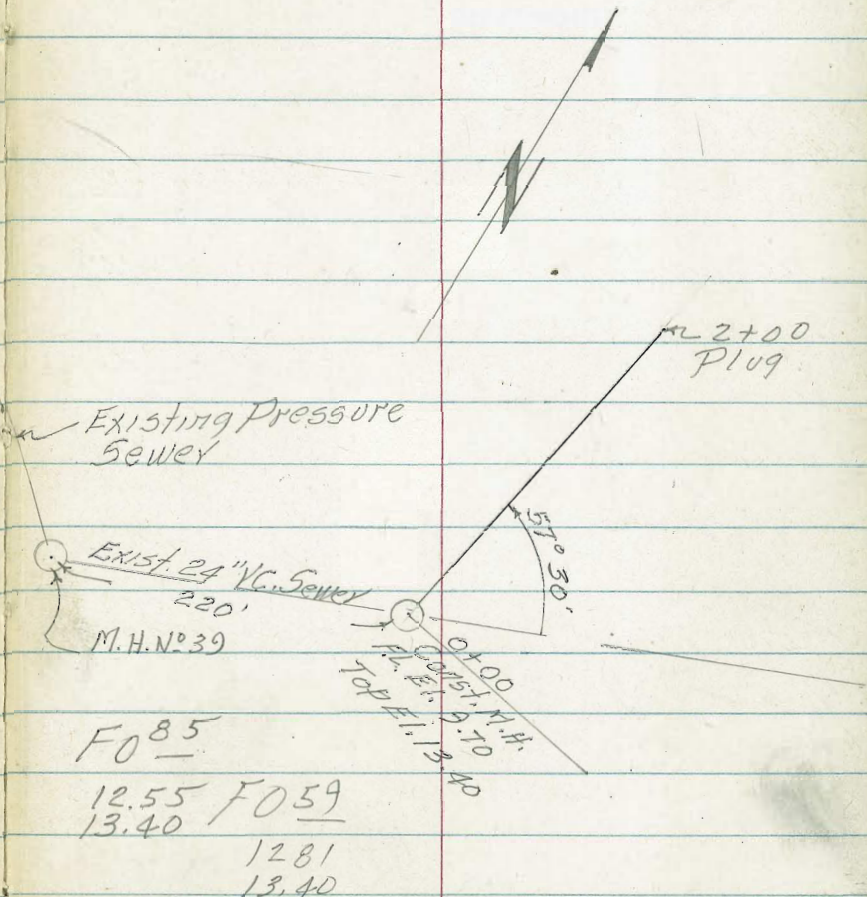
C 4 25
11 25
7.00

8" V.C.P. SEWER OCEAN BEACH REC. AREA

Ref Dwg. 3759-D Sheet 4

Stakes Set 10' RT.

1+00		C 2 <u>27</u>	
		12.32	
		10.05	
0+75		C 2 <u>37</u>	
		12.33	
		9.96	
0+50		C 2 <u>59</u>	
		12.46	
		9.87	
0+25	0.35 20	C 2 <u>74</u>	
		12.53	
		9.79	
0+00		C 2 <u>94</u>	F 0 <u>76</u>
		12.64	12.64
		9.70	13.40
		FL	TOP
B.M.			04 14.70



8" SEWER CONTD.

B.M.

14.04

C 1 80
1220
10.40

2+00 = END P119

C 1 93
1224
10.31

1+75

C 2 06
1228
(10.22)

1+50

C 2 06
1220
10.14

1+25

18" STORM DRAIN LAJOLLA MESA DRIVE &

P.L. 1781,

W.O. 20006

0+39.13 = E.C. = ~~+~~ Cut-off Wall

$\Delta = 50^\circ$ R = 22.5'

0+19.5 = B.C. Pt = ~~+~~ Cut-off Wall

L = 19.63' T = 10.5'

4'

0+15.5

4'

0+11.5

0+00 Curtain Wall

B.M.

4-20-28

Ref DWg 6486-B
Loose Leaf Notes B-12

Ref Pts 5' Lt.

4-19-57

(60)
Stampey
Bluff
Kelley
Wentworth

C 3 70 ✓

22.13
418.43

C 5.79

16.43
410.64

C 5 68

14.73
409.05

C 4 50

11.71 TP
407.21

C 2 73

03.73
401.00

P.I. Hub Orig Notes B-12

18" DRAIN

TBM, 0+90 (Orig. Notes)

430.61

0+93.13

C 6 35
3243
426.08

20

TP

27.90

0+73.13

C 3 03
7.89
424.86

4'

0+69.13

C 2 41
703
424.62

18'

0+51.13

C 1 87
3.97
422.10

4'

0+47.13

C 2 04
23.26
421.22

4'

0+43.13

C C 2 85
22.87
420.02

4'

18" DRAIN

30.13'
1+32.86 = End = ϕ Type I Inlet } 3.46x4'
 } outside
 } 6" walls

+9.73'

17'

1+13.13

20'

TBM. 1+15 ϕ P.A. (Orig Notes)

432.12

C063

28.97

428.34

F.L.

F203

28.97

431.00

GUT

~~X 1.41~~

~~29.95~~

~~428.34~~

~~PP/F.L.~~

F105

9.95

431.00

GUT

C431

31.61

427.30

CONC GUTTER GRADES 11-TH & K-STS.
WO 21623

Ref DWG 13333-L
Loose leaf G-23
Gutter

8-23-57

(64)

Stampel
BLUMT
E/more
Wentworth

1+14 End Drive

Gd
23.49

14

1+00

Gd
23.81

26

0+74 Begin Drive

Gd
24.41

26

0+48

Gd
25.01

16

0+32 End Drive

Gd
25.51

0+16 = Begin Drive

C-0.63
26.49
25.86
C-0.77
26.90
26.13

0+00 = E. Cb. Line 200' N. of N. Line K St.

B.M.

28.54

SWBP J & 11-th Sts.

GUTTER 11-JH & K

17'

2+41 Begin Drive

17'

2+23 60

23 6

2+00

17

1+83

17

1+66 End Drive

28

1+38 Begin Drive

24

0.20390

2.30290

LH

E

RT

(65)

Gutter

Gd
21.14

Gd
21.31

Gd
21.51

Gd
21.90

Gd
22.29

Gd
22.94

GUTTER 11-74. 8/15

LT

E

RT 66

Gutter

3+90 End Drive

GD
20.82

3+70

C-0.32
21.18
20.86

3+50

C-0.34
21.25
20.91

3+25

C-0.32
21.28
20.96

3+00

C-0.26
21.28
21.02

2+75

C-0.22
21.29
21.07

17

C-0.24
21.34
21.10

2+58

17

0.222%

0.203%

GUTTER 11-TH FK

LT

RT

RT

67

B.M.

28.54

(Starting Bench)

T.P.

23.86

4+28⁵⁰ = POC @ Inlet

21.50

C-1.00

21.62

20.62

11'

4+17⁵ = B.C. cb. Ret

21.50

Gd

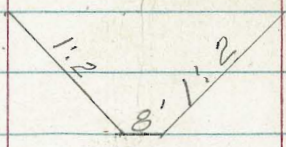
20.75

cb

TEMPORARY DRAINAGE EAST SHORE
MISSION BAY W0 6414

Ref DW9 3799-D 8-26-57
Lt Lt Rt (68)

2+50



2+00

Typical Sec

1+50

0.088%
N 64° 49' 25" E
~~N 60° 13' 50" E~~

1+00

Slopes 1:2

0+50

C3^L C4^S
8.6 9.8
5.5 5.5
8.6 8.6

C11 ⁹	C9 ⁰	C9 ²	C9 ⁷	C9 ³	C12 ⁵
14.98	14.73	14.9	15.4	15.03	15.58
3.1	5.73	5.72	5.72	5.75	3.1
26 ²	17 ⁰	18 ⁴	19 ⁴	17 ⁶	25 ⁰
C11 ³	C8 ⁶	C8 ⁸	C8 ⁹	C8 ⁷	C12 ²
14.43	14.30	14.5	14.6	14.40	15.31
3.1	5.70	5.67	5.67	5.70	3.1
27 ⁴	16 ²	17 ⁶	17 ⁸	16 ⁴	25 ⁶
C10 ⁵	C7 ⁹	C7 ⁸	C7 ⁶	C7 ⁶	C10 ⁹
13.63	13.55	13.4	13.2	13.25	13.97
3.1	5.65	5.63	5.63	5.65	3.1
29 ⁰	14 ⁸	15 ⁶	15 ²	14 ²	28 ²
C10 ⁴	C6 ⁵	C6 ⁵	C7 ¹	C6 ⁹	C10 ⁰
13.51	12.10	12.1	12.7	12.50	13.07
3.1	5.60	5.59	5.59	5.60	3.1
29 ²	12 ⁰	13 ⁰	14 ²	12 ⁸	30 ⁰
C8 ²	C3 ⁵	C4 ⁷	C3 ²	C4 ³	C7 ⁹
11.34	9.05	10.24	8.74	9.83	11.01
3.1	5.55	5.54	5.54	5.55	3.1
33 ⁶	6 ⁰	9 ⁴	6 ⁴	7 ⁶	34 ²
C2 ⁹	C0 ⁷	C0 ⁴	C0 ⁵	C0 ⁷	C2 ⁴
15.98	6.20	5.9	6.0	6.20	5.49
3.1	5.50	5.50	5.50	5.50	3.1
44 ²	0 ⁴	0 ⁸	1 ⁰	0 ⁴	45 ²

N. 9573.08
W 7696.74
0+00 = Wiy End of Ditch

N 9573.08
W 7696.74

B.M.

42
12.58

Top Hub N 10200 W 7066.71 (MB 90 Pa 14)

TEMPORARY DRAINAGE

Lt

±

Rt

(69)

5+50

C102	C74	C62	C69	C73	C100
1377 3.1	13.43 6.05	127 5.98	12.9 5.98	13.35 6.05	13.13 3.1
286	138	134	138	136	300

5+00

C112	C70	C73	C84	C72	C111
1430 3.1	13.00 6.00	13.2 5.94	14.3 5.94	13.20 6.00	14.21 3.1
276	130	146	168	134	270

4+50

C115	C85	C82	C78	C83	C111
1464 3.1	14.45 5.95	14.6 5.90	137 5.90	14.75 5.95	14.17 3.1
270	160	174	156	166	278

4+00

C103	C80	C86	C82	C88	C117
1344 3.1	13.90 5.90	14.45 5.85	14.55 5.85	14.70 5.90	14.81 3.1
294	150	172	174	166	266

3+50

C122	C93	C88	C94	C92	C121
1584 3.1	15.15 5.85	14.6 5.81	15.2 5.81	15.05 5.85	15.16 3.1
246	176	176	188	174	258

3+00

C122	C96	C94	C95	C96	C123
1598 3.1	15.40 5.80	15.16 5.76	15.26 5.76	15.40 5.80	15.43 3.1
242	182	188	190	182	254

~~N60°13'50"E~~
 N64°49'25"E

TEMPORARY DRAINAGE

LT E RT (2)

NOTE: Red Elev's Indicate
as built Grades

REVISED

REVISED

~~7+18.35 = W/4 END of Existing Culvert~~

7+04.76
~~7+00~~

588° 23' E
N 64° 49' 25" E
Slopes 1:3

6+50

6+00 = ~~RT~~

~~N 60° 35' E~~

3.11
F.L.

C 9 ^L	C 5 ⁸	C 5 ⁴	C 6 ⁶	C 5 ⁹	C 9 ²
12.24	11.9	11.5	12.7	12.0	12.33
3.1	6.12	6.12	6.12	6.12	3.1
@ 22 ^L	16 ⁴	@ 10 ⁸	@ 13 ²	16 ⁷	@ 22 ⁴
C 10 ³⁰	C 7 ⁷	C 7 ⁰	C -6 ⁹	C 7 ²	C 10 ⁵⁰
13.40	13.8	13.1	13.0	13.3	13.60
3.1	6.12	6.07	6.07	6.12	3.1
19 ^L	22 ^L	14 ⁰	13.8	20 ⁶	18 ⁵
C 10 ⁶	C 7 ⁶	C 7 ¹	C 7 ⁰	C 7 ⁰	C 9 ⁵
13.68	13.7	13.1	13.0	13.1	12.65
3.1	6.12	6.03	6.03	6.12	3.1
18 ²	21 ⁸	14 ²	14.0	20 ²	21 ⁵
For Tan					For Tan

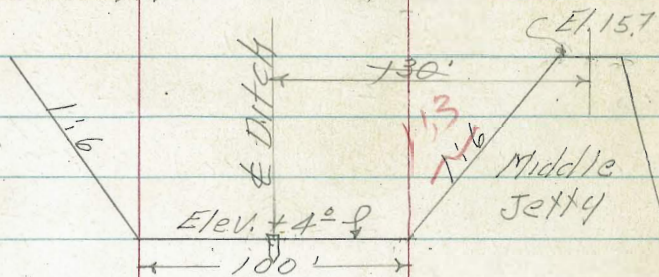
TEMPORARY DRAINAGE DITCHES ELY
SIDE HI-WAY 101 - MISSION BAY PARK
W.O. 64141

NOTE: Stakes set 5' Lt
or Wly.
9-16-57

		C-25		C-29	+63 = EMD	C-04 ⁽⁷⁾
		10.55		10.06		6.56
4		8.09	9	7.20	14	6.20
		C-18		C-30		C-06
		10.01		10.34		6.69
+50		8.18	+50	7.29	+50	6.31
		C-09		C-26		C-06
		9.17		9.84		6.98
3		8.27	8	7.37	13	6.40
		C-16		C-27		C-48
		10.02		10.13		11.25
+50		8.36	+50	7.46	+50	6.49
		C-19		C-19		C-42
		10.35		9.43		10.77
2		8.44	7	7.55	12	6.58
		C-17		C-12		C-49
		10.24		8.78		11.56
+50		8.53	+50	7.64	+50	6.66
		C-21		C-24		C-35
		10.74		10.09		10.29
1+00	0.178	8.62	6	7.73	11	6.75
		C-19		C-26		C-49
		10.63		10.40		11.26
0+50		8.71	+50	7.82	+50	6.93
		C-03		C-29		C-35
		9.15		10.76		10.46
0+00 =	N. 8465.05 W. 6596.00	8.80	5	7.91	10	7.02
				C-26		C-31
				10.58		10.16
B.M. P.K. Nail	N. 9400.00 W. 6980.00	13.01	+50	8.00	+50	7.11
		M.B. 90				
		7				

GRADES CHANNEL 100' SWY OF
MIDDLE JETTY FLOOD CHANNEL

MISSION BAY W.O. 64010



Typical Sec.

	C5 ¹⁸	
31+00	9.18 4.00	
	C5 ⁷¹	
30+00	9.71 4.00	
	C6 ⁹⁴	
29+00	10.94 4.00	
	C2 ⁸⁵	
28+00	6.85 4.00	
	C2 ⁸⁵	
27+00 Middle Jetty	6.85 4.00	
TBM.	12.18.	
B.M.	13.80	

9-19-57

Set Stakes & Ditch

Sta. 31+00	
TBM. Top. Drift Pin & Jetty	15.67
TBM Sta 28+00	16.49

Stamper
Bluff
Elmore
Wentworth

(73)

	C0 ⁵⁷
37+00	4.57 4.00
	C1 ⁵⁸
36+00	5.58 4.00
	C1 ⁷⁴
35+00	5.74 4.00
	C2 ⁹⁶
34+00	6.96 4.00
	C3 ¹¹
33+00	7.11 4.00
	C3 ⁶⁴
32+00	7.64 4.00

on Rock
R.P. PK. (see Pg. 50)

LT E RT 74
9-24-57

TEMPORARY DRAINAGE DITCH

0+00 = N 15361.45 S 75° E 7+00 = N. 5180.27
W. 7188.52 W. 6512.37

	LT	E	RT				
	C-59		C-60				
+50	13.0 7.07 118 C-65	7.07	13.1 7.07 120 C-72				
3	13.6 7.06 130 C-59	7.06	14.3 7.06 144 C-65				
+50	12.95 7.05 118 C-65	7.05	13.55 7.05 130 C-54	END 7+00	C-59 13.05 7.15 118 C-40	7.15	C-54 12.55 7.15 108 C-36
2	13.5 7.04 130 C-53	7.04	12.4 7.04 108 C-54	+50	11.14 7.14 8.0 C-36	7.14	10.74 7.14 7.2 C-35
+50	12.3 7.03 108 C-48	7.03	12.4 7.03 108 C-51	6	10.72 7.12 7.2 C-34	7.12	11.62 7.12 110 C-32
1	11.8 7.02 96 C-52	7.02	12.13 7.02 102 C-43	+50	10.51 7.11 88 C-38	7.11	10.81 7.11 7.4 C-40
+50	12.2 7.01 102 F-32	7.01	11.3 7.01 86 F-32	5	10.90 7.10 76 C-49	7.10	11.10 7.10 80 C-44
0+00	3.8 7.00	7.00	3.8 7.00	+50	12.0 7.09 98 C-50	7.09	11.5 7.09 88 C-51
					12.1 7.08 100	7.08	12.2 7.08 102

Hi-way Sta. 182+25
B. M. Chris + E. Colv. Adwall 13.50

4+00 7.08 7.08 7.08

LT

E

RT

GRADES STORM DRAIN BLK 4

BUNGALOW PARK W.O. 21613 J-19

TBM. 0+83³⁰ E.L. Aikay
Orig. Survey (Hub) 303.12

NOTE: Stakes Set 15' LT.

0+95³⁰ = End.

12'

0+83³⁰ = E.C. $\Delta = 30^\circ$

11.65

0+71.65 POC $\Delta = 15^\circ$

11.65 C = 11.62'

0+60 = B.C. RT, $\Delta = 30^\circ$ R = 44.50 L = 23.30' T = 11.92'

0+40

0+20

Chislt +.

0+00 = End Existing Pipe (Make Connection)

B.M.

299.15

Chislt Top Pipe 0+00

C 5 0706 07
301.00C 4 7405 14
300.40C 6 806 63
299.83C 4 5403 79
299.25 ✓C 1 87300 13 ✓
298.26C 2 73300 00
297.27C A 82301 10 ✓
296.28

Ref DW9 3800-D 10-14-57

RT 76

TEMPORARY DRAINAGE DITCH WLY SIDE
HIGHWAY 101 - MISSION BAY W.O. 64141

Stamper
Blunt
Elmore
Westworth
Maker

	3 rd BK Top	1 st h.c. @ Top	RT
	C-97		
+50	14.83 5.11 @ 194	14.0 5.11 17.8	
	C-102		
3	15.81 5.09 21± C-95	14.7 5.09 19±	5.6
	14.60 5.08 19± C-73	12.4 5.08 14±	
+50			
	12.39 5.06 14± C-89	12.0 5.06 13±	5.3
2			
	12.95 5.04 16± C-72	12.4 5.04 14±	
+50			
	12.25 5.03 14± C-86	12.0 5.03 14±	4.9
1+00			
	13.59 5.02 17± C-03	13.0 5.02 16±	
0+50			
	5.30 5.00 0±	5.3 5.00 0±	4.1
0+10			
0+00			

	Stubs 3 rd BK Top		RT
	C-92		
+50	14.21 5.23 18±		
	C-94		
7+00	14.62 5.21 18±	6.2	
	C-102		
+50	15.17 5.20 20±		
	C-99		
6	15.13 5.18 19±	6.1	
	C-103		
+50	15.49 5.17 20±		
	C-108		
5	15.92 5.15 21±	6.0	
	C-109		
+50	15.11 5.14 20±		
	C-90		
4+00	14.07 5.12 18±	5.9	

Kathe only 3' RT
Top Slope

0.03044 %

NOTE (See Sketch Pg 77)

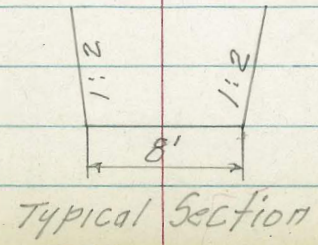
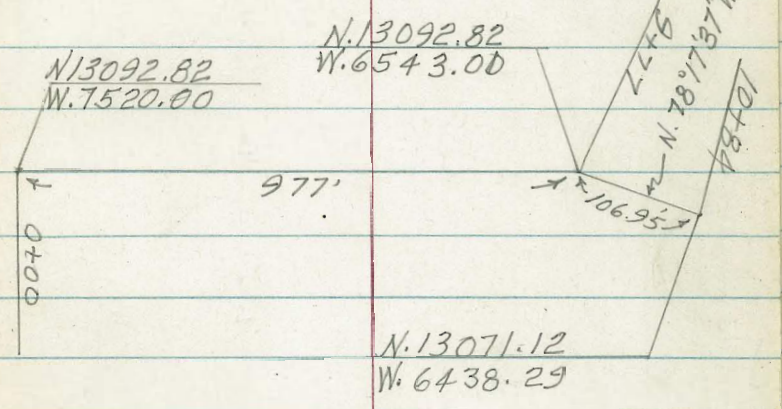
B.M.

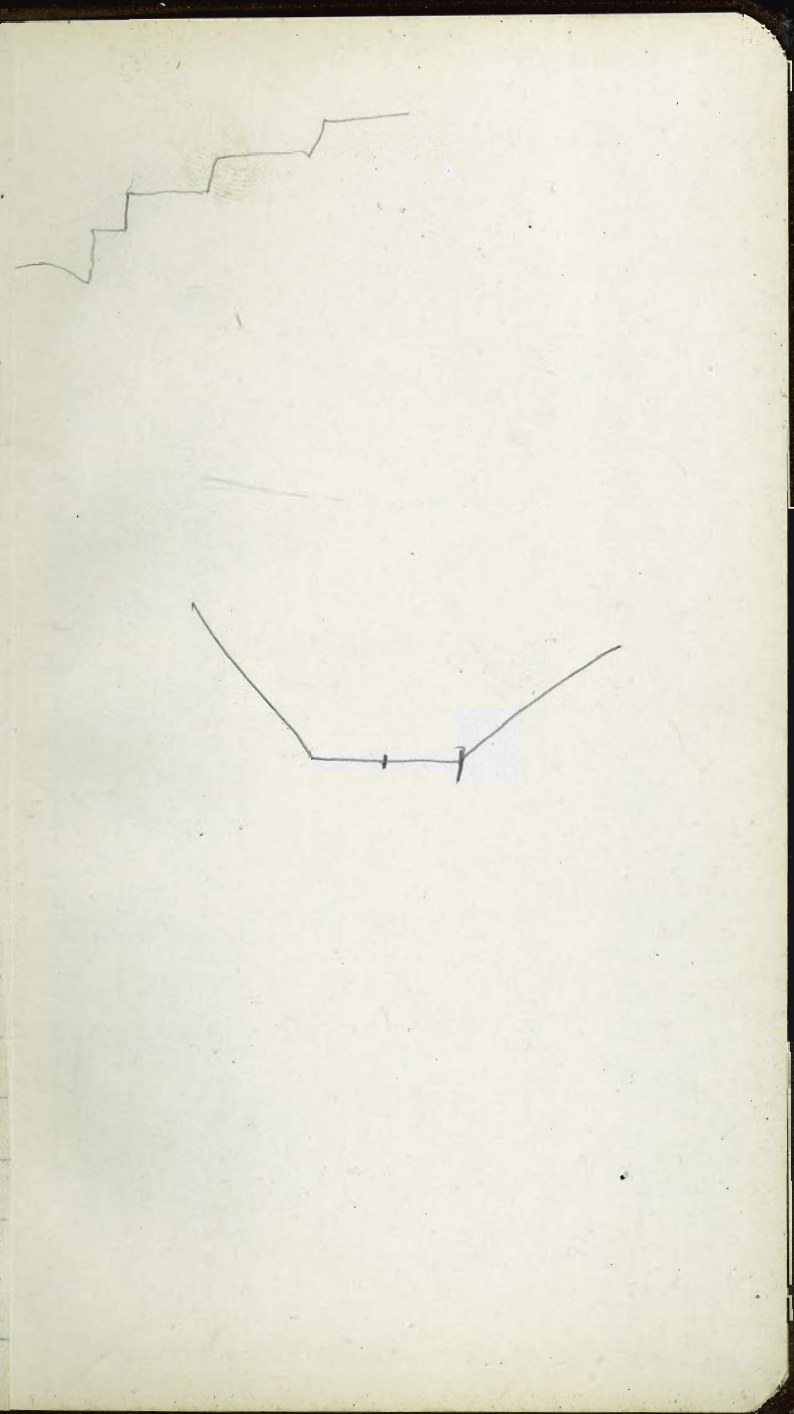
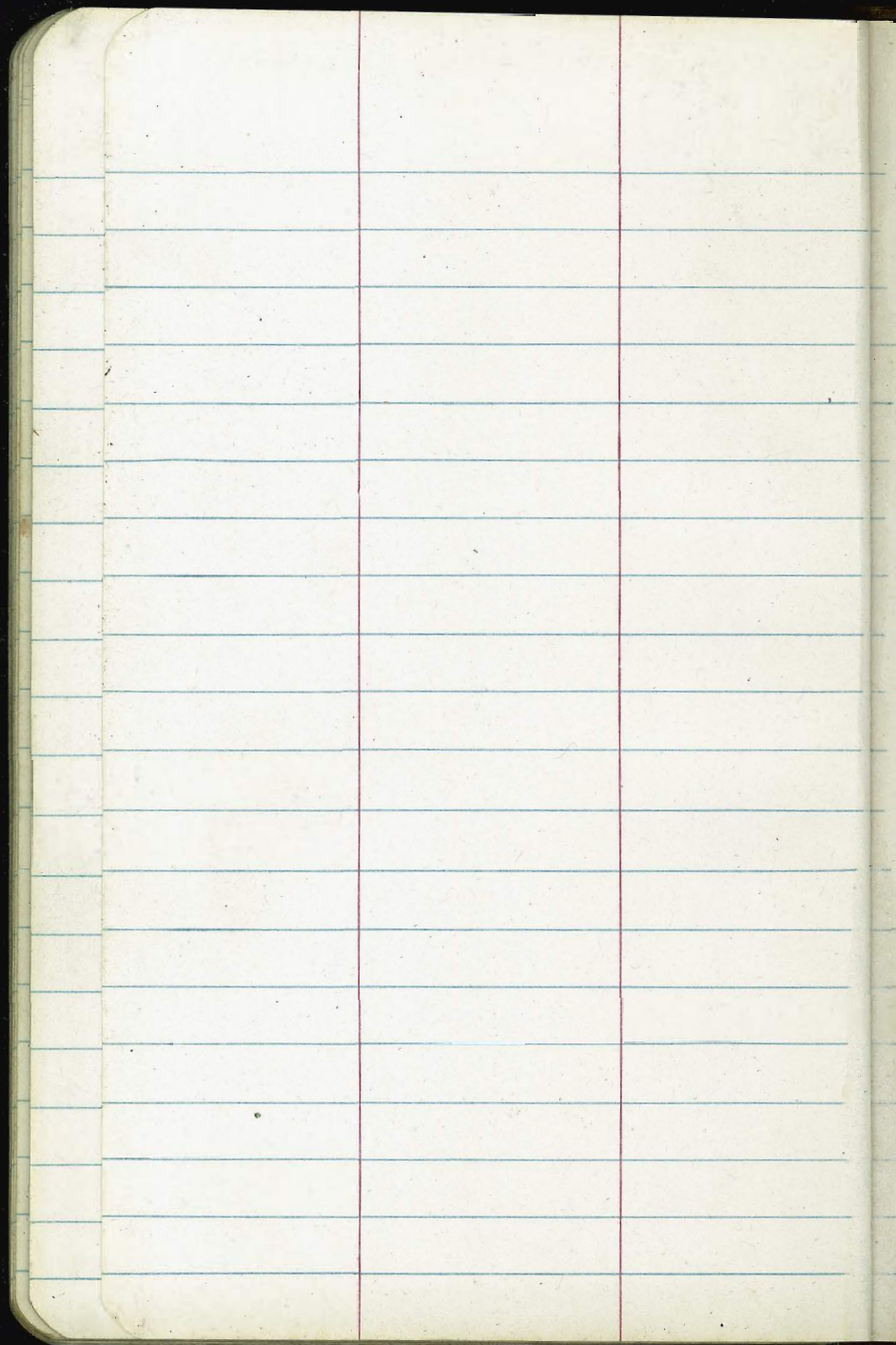
11.64

Boff & Wasker B.M. No. 19 - A State Hi-Way E. & Br. Hi-Way
Hi-Way Sta. 5D.160+75

NOTE: Elev's shown in Red indicate as built Grades

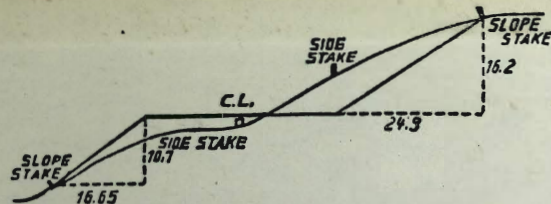
	LT	#	RT
		stubs 3' BK Slope	Lathe only Top Slope
+84 = End	6.8	C567 11.00 5.33	5.33
+50	7.6	C53 10.62 5.32 @10.5	C56 10.92 5.32 @11.2
10+00	6.6	C52 10.50 5.30 @10.4	C48 10.10 5.30 @9.6
+77 deflet = 11°42'23"		C57 11.00 5.29 @11.4	C51 10.39 5.29 @10.2
+50		C-7 12.28 5.28 14.2	12.5 5.28 14.4
9+00	6.5	C-7.8 13.10 5.27 15.5	12.3 5.27 14.0
+50		C-8.8 14.06 5.26 17.5	13.5 5.26 16.5
8+00	6.3	C-9.8 14.98 5.24 @19.5	14.9 5.24 @19.5
BM	2.10	13.10	11.00





935 1 1000
 905 2 103
 915 102
 915 102
 965 97
 480

935 1000
 480 455
 455 545



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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