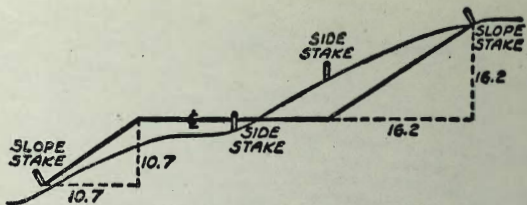


G 365



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the out or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 16 1965

DIRECTIONS FOR USE OF TABLES



TABLE No. XIV

Distance of slope stake from side or shoulder
stake for any width roadway, when 1 1/2 to 1

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve with a given L may be found
by dividing tangent (or external) opposite L by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	1.95	2.34	2.72	3.10	3.49	3.89	4.30	4.70	5.11	5.53
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

GRADES-ROANOKE ST.

from RACHEL
TO RHO DRIVE

Mulker
Taylor
Johns
Elmore
5-22-1956

WD 32538

Lt

E

Rt. 1

Cont. P. 2

0+22.07 on Lt.
Part 4 - B.C. on Rachel

160.50
159.70
F 0.60

0+04.17
0+01.51 on Lt.
Part 4 - B.C. ch. on ROANOKE

~~161.24~~ 161.20
164.65 (54.81)
C 2.41 C 2.61

0+00 = Elmore Rachel

Part 3 Lt + Rt

161.18 164.18

160.30

Part 2 Lt + Rt

161.12

160.02

Part 1 Lt + Rt

161.18 164.20

159.72

E.C. on Rachel

161.25
165.31
C 4.06

164.27 20.06
164.81 or 20.06
C 2.34

159.41 159.41
158.92 159.41
F 0.5 F 0.70

TR # 2

164.45

NE Cor. Water Box

TR # 1

155.33

147.04

B.M. NE. CP. RACHEL & WINCHESTER

CURB GRADES ~ ROANOKE ST.

from RACHEL
TO RAO DRIVE

H.

\$

Rt. 2

STATIONS

1+40

163.71
165.27
C 1.56

163.72

163.71
161.13
F 2.08

1+20

163.13

162.84

162.63

1+00 = PVC

162.66
163.58
C 0.92

162.37

162.16
159.69
F 2.47

0+60

162.07
163.38
C 1.2

161.44 161.66

161.32
160.86
F 1.26

0+35

161.70
163.14
C 1.44

160.99 161.4

160.78

.7365 cb
0+22.81 bc. Ret. on Rd

160.78

0+17
0+14.51 = bc. cb Ret. on Lt

161.20
162.81
C 0.91

160.40 = 0+10

160.50
159.21
on Road
F 1.19

0+00 = ELEV. RACHEL

160.40

160.40

0-10

Cont. from P-1

ROANOKE ST

LT

E

Pt. 3

L

$$\Delta = 33^{\circ} 26' 30''$$

STATIONS

$$L/R = 1520$$

$$T = 456.62$$

$$EL = 887.17$$

Def per foot 1/1308377

2+00

0° 33.05

171.44
175.14
C 3.7

171.15

170.94
169.85
F 1.09

2+70.80 = B.C.

0° 0'

169.88
172.85
C 2.97

169.59

169.38
167.81
F 1.57

2+460

169.30
172.31
C 3.01

169.01

168.80
167.14
F 1.66

T.P.

166.51

167.13
169.76
C 2.63

166.84

166.63
165.60
F 1.03

2+20 = E.V.C.

2+00

166.11 = 2+00

165.82

165.61

1+80

165.20
167.26
C 2.06

164.91

164.70
163.67
F 1.03

1+60

164.40

164.11

163.90

ROYNOK ST

Lt.

E

ret. 4

STATIONS

4120	2° 48.74	17891 182.61 C 3.1	17862	17841 17620 F 2.01
4100	2° 26.13	17740	17711	17711 176.90
3+80	2° 03.51	17601 179.05 C 3.04	17572	17551 175.74 C 0.23
3160	1° 40.89	17475	17446	17425
3+40 = P.N.C.	1° 18.27	17361 17649 C 2.88	17332	17311 17267 F 0.44
3+20	0° 55.66	17253	17224	17203

TP on stub 3+00 28.27 17514

2

STATIONS

5+60	5°27.04	191.23	190.94	190.73
5+40 = P.V.C.	5°04.43	189.54 192.85 C 5.3	189.25	187.04 191.26 C 2.22
5+20	4°41.81	187.73	187.44	187.23
5+00	4°19.2	185.92 190.44 C 4.52	185.63	185.42 185.89 C 0.47
4+80	3°56.58	184.11	183.82	183.61
TR #6 Nail in Fence Post West end Corral		192.85		
TR #5		182.96		
4+60 = E.V.C.	3°33.97	182.30 186.47 C 4.17	182.01	181.80 181.09 F 0.71
4+40	3°11.35	180.54	180.25	180.04

Northwest
Curb Ret.

South-
West
Curb
Ret.

Part 4 E.C. on Roanoke Hopkins

194.04
200.58
C 6.84

193.35
198.94
C 5.55

Part 2

193.95

193.44

Part 1

TR # 7 = RK in Fence Post
#1 SE Cor. Corral

200.80

5+98.24 C° 49.73 C° 10.28

5+97.77 = P.R.C. cb Ret on Rt

C° 08.81

5+96.95 = P.C. cb Ret. on Lt. ✓ OK

1937.5 19325
19976 19750
C 6.51 C 6.25
off Radios
stage

192.75 192.75
19824 19795
C 5.5 C 5.2

5+80

5° 49.66

192.51
19795
C 5.44

192.32

192.01
19631
C 4.3

North West cb Ret

SW cb Ret

ROANOKE ST

Lt.

Q.

Rt. 7

88 7°~~36.2~~ 7°37'
6+74.18 = P.C. cb Ret. North

19368
203.77
C9.09

6+72.57 = P.C. cb Ret. South ~~ck~~
7°34.38

stk 201.96

~~6+74~~

~~6+80~~

6+60 7°20.17

203.09 = stk.

193.75

stk - 201.91

6+40 6°57.55

193.90

19364 Pav.

Pav. = 19320

6+35.84 = E. Hopkins 6°52.84

6+20 6°34.93

20095 = stoke

193.70

6+00 6°12.31

193.14

BRANDKE ST

Lt.

L.

Rt.

B

7+00

8° 05.39

192.65
200.93 = st
- 8.28

192.36

192.15
200.49
- 8.34

6+80

7° 42.78

193.52

193.23

6+74.488

7° 36.2

Part 3 = PCC cb Ret. on Lt.

193.68
203.61
- 9.93

193.18

6+72.57

7° 34.38

Part 3 = PCC. cb Ret. on Rt.

193.68

193.18
202.09
- 8.91

Part 2

193.88

193.44

Part 1

194.00

193.50

BC. Ret. on Hopkins

194.04
203.21
- 9.17

193.39
202.02
- 8.63

def. Δ

8+20	10° 21.05		187.04 183.60 F 3.44	186.75	186.54 177.51 F 9.03
8+00	9° 58.43		187.56	187.27	187.06
TR #9		184.83			
7+80 PVC	9° 35.82		188.43 189.44 C 1.01	188.14	187.93 187.56 F 0.37
7+60	9° 13.21		189.48	189.20	188.99
TR #8		193.96 on Rock			
7+40	8° 50.6		190.54 196.26 = stk C 5.72	190.25	190.04 stk = 194.80 C 4.76
7+20	8° 28'		191.59	191.31	191.10

Part 1 cb Ref = Cont. P. 11

12° 29.32'
12° 29.46'
12° 29.32'
9+33.72 = P.R.C. cb Ref.

187.16 189.70

187.41

187.16
187.20

9+25

12° 19.80'

TP #10

189.30

189.37
191.09 = stk
C 1.72

189.08

188.87
stk. 192.04
C 3.17

9+00

11° 51.53
12° 19.8

188.42
188.19 = stk
F 2.23

188.13

187.92
stk 188.80
C 0.9

8+80 EVC

11° 28.91

187.67
186.00
F 1.67

187.38

187.17
185.36
F 1.81

8+60

11° 06.29

187.10
180.39
F 6.71

186.81

186.60
183.04
F 3.56

8+40

10° 43.67
10° 43.67

186.89

186.60

186.39

POHNOKE ST

Lt

Co

Rt. 11

9+75

13° 16.34

191.25
195.55 = stk
C 4.3

190.96

190.75
stk. 197.71
C 6.96

9+70.53

13° 11.27

PO.C. = E. Deouville

191.10

190.80

190.66

9+50

12° 48.09

190.31
192.73 = stk
C 2.42

190.52

189.81

Part 3 = E.C. Rd.

DEUVILLE ST.

on ~~Morningside~~

190.32

Part 2

189.93

Part Cb Rd

189.54

11+00	16° 37.69 15° 37.69		195.97 19371 = stk F 2.26	195.67	195.47 stk - 176.81 C 1.34
10+75	16° 09.42 15° 09.42		195.03 194.09 stk. F 0.94	194.73	194.53 stk - 176.17 C 1.64
10+50	14° 41.15		194.08 193.97 stk. F 0.1	193.79	193.58 stk. 197.93 C 4.35
10+25	14° 12.88'		193.14 192.7 = stk C 2.13	192.84	192.64 stk 200.21 C 7.57
T.P. R.M. MH +08.13 10+07.88 E.C. Rt. on Rt.	13° 53.5 13° 53.78	195.80	192.49	192.20	191.99
10+00	14° 44.61' 13° 44.61'		192.20 19617 = stk C 3.97	191.90	191.70 stk 197.69 C 8.0

ROANOKE ST.

Lt

L

Rt 13

11+80

$$\begin{array}{r} 198.98 \\ 197.74 \text{ stk.} \\ \hline F 1.24 \end{array}$$

198.69

$$\begin{array}{r} 198.48 \\ \text{stk. } 198.68 \\ \hline 60.2 \end{array}$$

11+59.96 = EC

16° 43.25

$$\begin{array}{r} 198.15 \\ 195.99 \text{ = stk} \\ \hline F 2.36 \end{array}$$

197.86

$$\begin{array}{r} 197.65 \\ \text{stk. } 196.57 \\ \hline F 1.08 \end{array}$$

11+40

16° 22.92

$$\begin{array}{r} 197.48 \\ 195.97 \text{ = stk} \\ \hline F 2.10 \end{array}$$

197.18

$$\begin{array}{r} 196.98 \\ \text{stk. } 196.87 \\ \hline F 0.1 \end{array}$$

11+20

16° 00.21

$$\begin{array}{r} 196.72 \\ 194.18 \text{ = stk} \\ \hline F 2.54 \end{array}$$

196.42

$$\begin{array}{r} 196.22 \\ \text{stk. } 196.79 \\ \hline 60.57 \end{array}$$

12+34

207.35
208.68 - sth
C 1.33

207.06

206.85
sth. 207.70
C 0.85

12+97

205.12
205.32 sth
C 0.2

204.83

204.62
sth. 206.04
C 1.42

TP #12

on Rock

205.03

202.89
203.02 - sth
C 0.13

202.60

202.39
sth. 202.90
C 0.5

12+60 EVC

12+40

201.78

201.76

201.25

12+20

200.72
199.33 sth
C 1.4

200.42

200.22
sth. 200.52
C 0.3

12+00

199.80

199.51

199.30

120			218.08 217.70=stk. F 0.38	217.79	217.58 218.91=stk C 1.33
15+00			217.23	216.74	216.73
14+80 NYC			216.15 216.13=stk. 00	215.86	215.65 216.88=stk C 1.23
14+45			214.04 214.40=stk C 0.36	213.75	213.54 213.97=stk C 1.85
14+08			211.86 212.67=stk C 0.86	211.52	211.31 214.04=stk C 2.73
TR 28' RT 14+08 = on cut stub		214.04			
13+71			209.58 212.25 stk C 2.67	209.29	209.08 stk= 211.20 C 2.12

ROANOKE ST

Lt.

R

Rt.

17

16+40

218.28
218.18 = stk
70.1

217.99

217.78
218.16 = stk
C 0.7

+20

218.83

218.54

218.33

16+00

219.15
219.24 = stk
C 0.1

218.86

218.65
220.09 = stk
C 1.44

15+80

219.23

218.94

218.73

DOT.

= 15 + 65.95 = TP 50' RP Hub on Rt.

219.00 = Hub 75' Rt.

219.22 = 50' Rt off

15+60

219.00
219.22 = stk
C 0.2

218.79

218.58
219.90 = stk
C 1.32

15+40

218.70

218.41

218.20

17+60

211.05
212.66 stk.
C 1.6

210.76

210.55
213.66 stk.
C 3.1

17+40

212.27

211.98

211.77

17+20

213.75
215.02 = stk.
C 1.27

213.46

213.25
stk. 215.97
C 2.72

17+00

215.23

214.54

214.73

16+80

216.48
217.54 = stk.
C 1.1

216.19

215.98
217.38 = stk.
C 1.4

16+60

217.50

217.21

217.00

18+20

20856

18+17.72 = $\frac{1}{2}$ Morningside

20910 = Pav. Grade
38' ct.

38' Rt. = ^{Part} 207.70

17+99.77

Part 3 = FC, on Morningside

20984 = NE Rd.

20904

SE Rd. = 208.00

Part 2

Part 1

N.W. x S.W. Return

17+79.72 = BC 20' cb Ret.

C
210.07
211.16 = stk Rods
0109

20978

209.57
Rad = 212.52
stk

TP. on 20' Rods ^{cb} 38' Rt. 17+79.72 = 212.52

ROANOKE ST

4

RT 20

see page vi

19 + 00.88 = BK

208.28
209.461K
C 1.18

207.99

207.78
206.52
F 1.22

18 + 80

18 + 55.72

Part 3 = F.C. Ch Ret. on Roanoke St

208.53
209.87
C 1.34

207.90
208.67

Part 2

208.58

207.83

Part 1

208.65

207.78

18 + 35.72 = BC. 20 Ch Ret. on Martinsburg Rd

209.00

207.60

ROANOKE ST

Lt

E

Rt. 21

19+75

3°31.89

207.95
207.29
F0.66

207.65

207.45
200.28
F1.17

19+69.88 = opp sw cor Alley 3°17.29

Alley Prop.
C6 67 Prop.
= 207.65

19+68.09 = BC. 2nd Alley R 3°12.13

$\Delta 19^{\circ}45'45''$

R = 601.31

L = 207.41

T = 169.74'

def. perf. = 2.858547

207.48

19+50

2°20.42

208.06
208.19
C0.13

207.76

207.56
203.98
F4.58

19+25

1°08.95

208.17
208.81
C0.70

207.57

207.67
205.50
F2.17

19+00.88 = BC. Rt.

208.27
209.43
C1.15

207.98

207.77
206.54

ROANOKE ST

111115 S' WLY

20+77.13

25cb R on Lt. Red. Cont. P. 24

20+82.13 - BC. 8° 38.11 on Lt.

20 V 1

+75

8° 17.7

20 69.52

15 67

20+70 Bk.

8° 02.03

55.80

+50

7° 06.23

+25

5° 54.76

20+00

4° 43.39

4° 23.74

19+93.14 = 2' 16 Rad. E. side Alley

opp. SE Cor Alley

19+91.84

4° 20' 03

Lt

E

Rt. 22

207.60

207.18

207.21

207.05
206.37
F 0.74

207.53 - Bk.

207.27

207.81

F 3.72

207.24

207.08

207.62

207.97

201.11

F 6.51

207.32

207.16

205.55

205.45

F 1.71

207.73

201.45

F 6.28

207.43

207.27

204.19

F 3.08

207.84

203.07

F 4.72

207.54

207.38

199.84

F 7.54

207.40

207.55

ROANOKE - 57

23

TR. Set Temp BM 100' W 21+08.29 = 209.97

Part 2 = cb EC. on Rec Dr on Rt. SW Cor.

206.77

Part 1 on SW cb Ret

cb
SW Ret

206.81

21+15.07 = B.C. - 20' cb R on Rt.

on 20' R = 38' R
206.76

206.86

21+08.29^{.28} = F.C. 9° 52' 86

206.88
206.97
C 0.09

21+00

9° 29' 17

207.11

206.91
206.64
F 0.27

Roanoke St

Lt

2

Rt

2A

Part 4 = cb EC. on • REG DR N.W. Cor.

20872

Part 3

20840

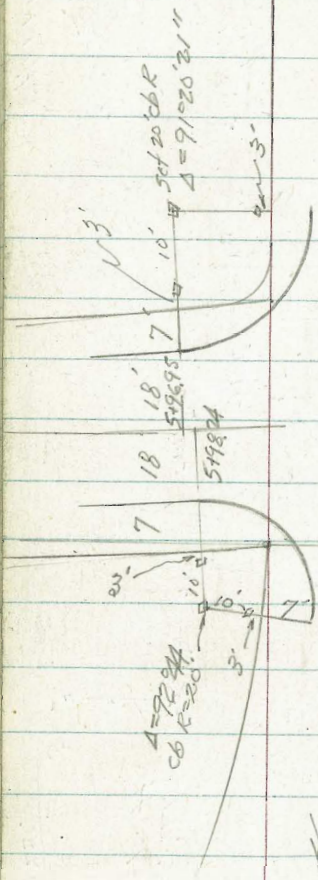
Part 2

20812

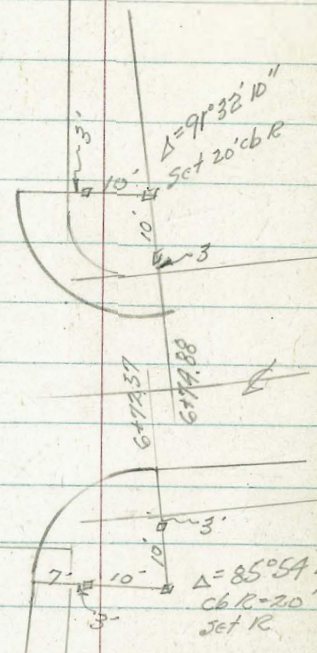
Part 1

20780

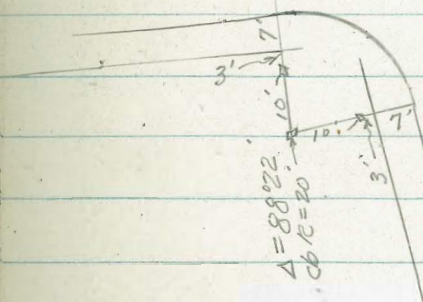
57



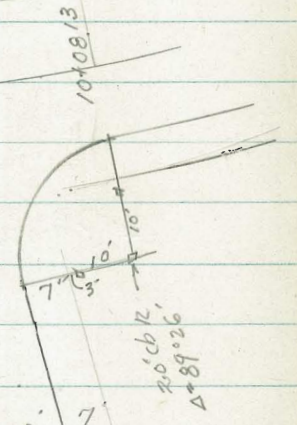
HOPKINS



ROANOKE
R=1520'



DEKUNVILLE ST



TURKEY PINES PARK

From SLY From Cor. #25

Station	From Line	V.A.	Corr.	Horiz.	Total	Cor #
244	150°45'	1°30'	0	244	244	
417		3°0'	-1	416	416	
					660	#24

From 24 SLY

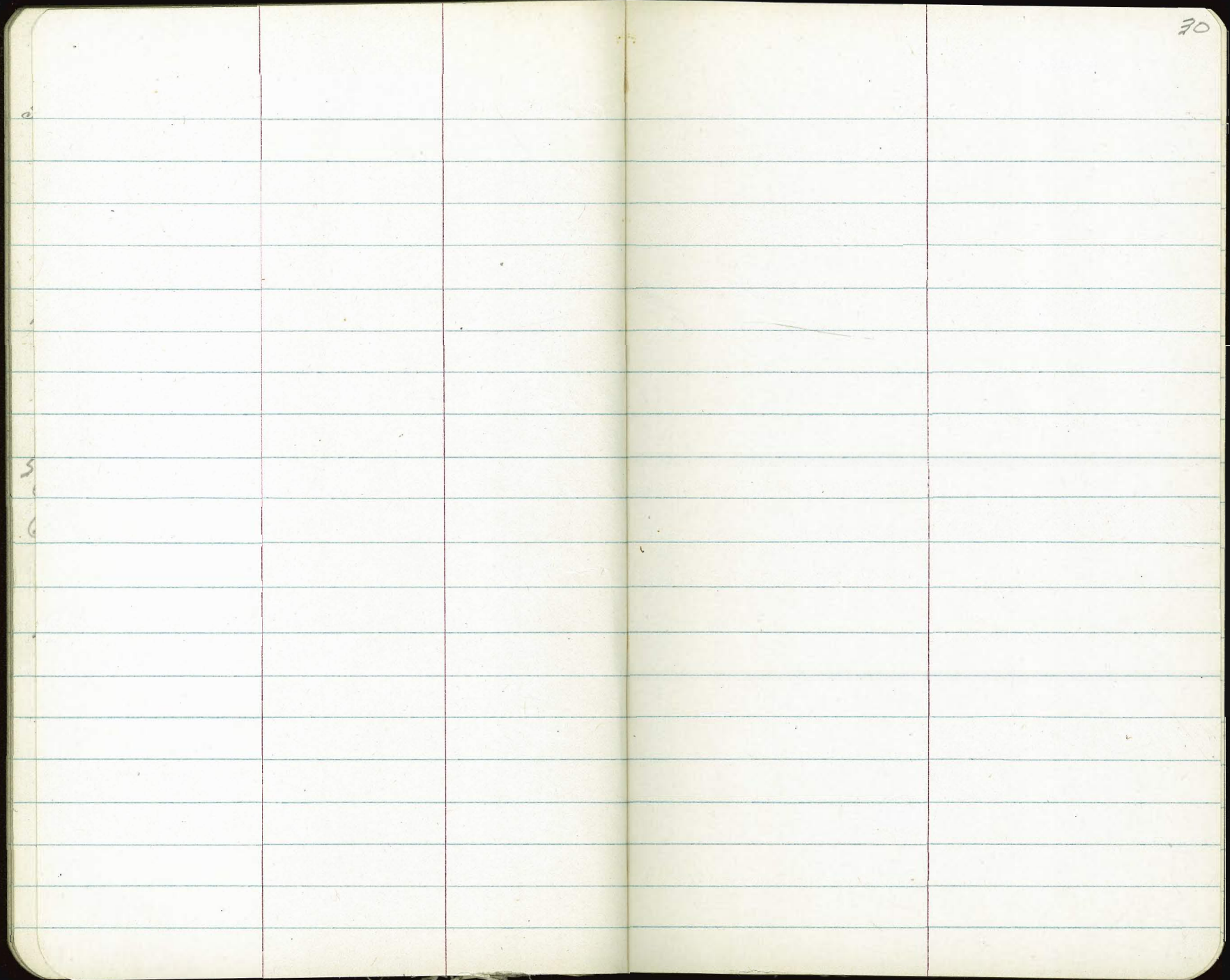
213	195°27'	3°35'	-1	212	212	
				25	25	
					237.0	#23

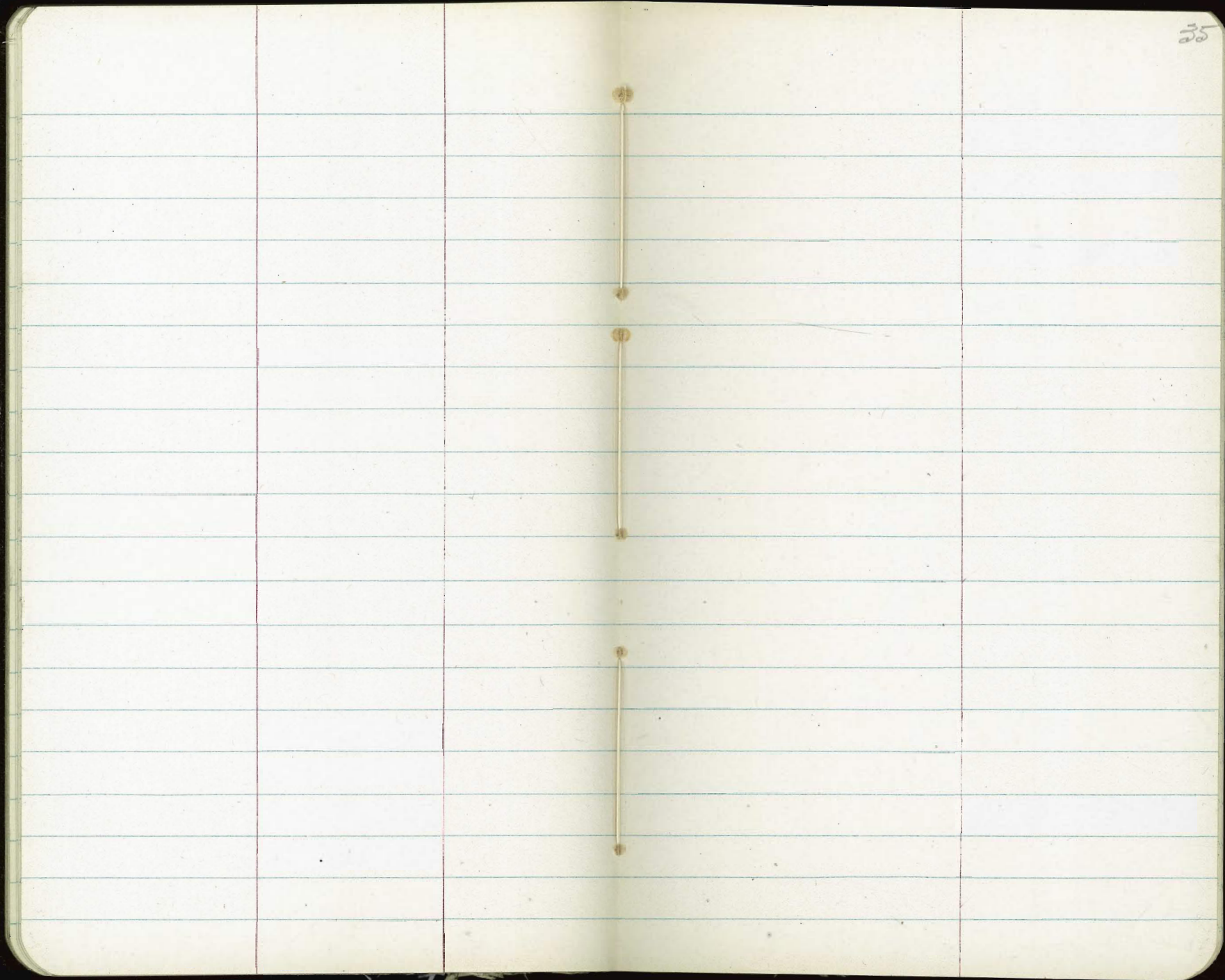
From 23

555	64°30'	5°50'	-6'	549	549	POT. Hub
668		2°55'	-1	667	667	
					1216	POT HUB
394		0		394	394	

From Int. Line 22-23-20-21

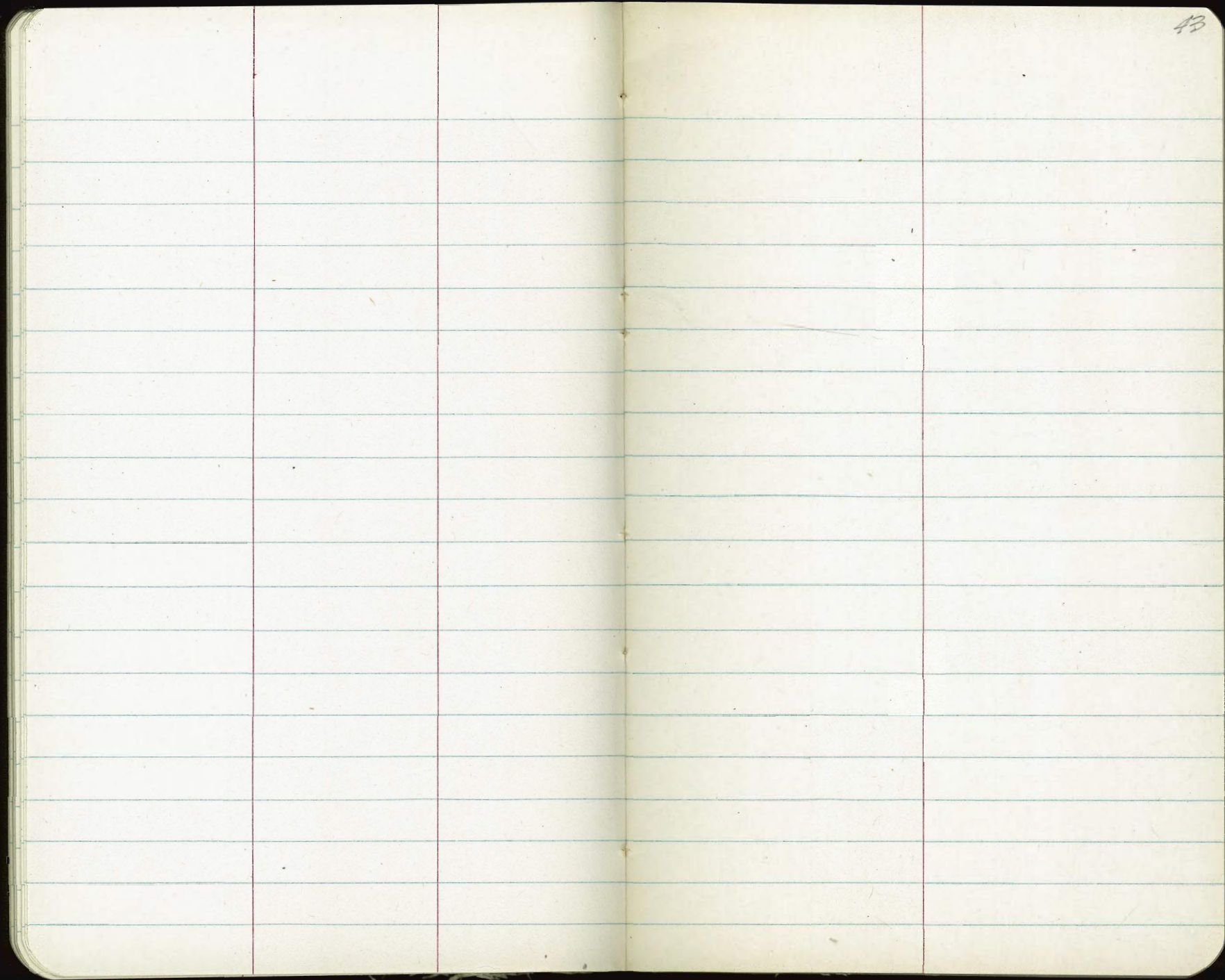
					1610	POT. on Line = Int. Line from (23-22 + 21-20)
					225	
					1385	Cor #22
525	279°				525	POT
				140	-140	Cor #21
					385	
					90	
					480	



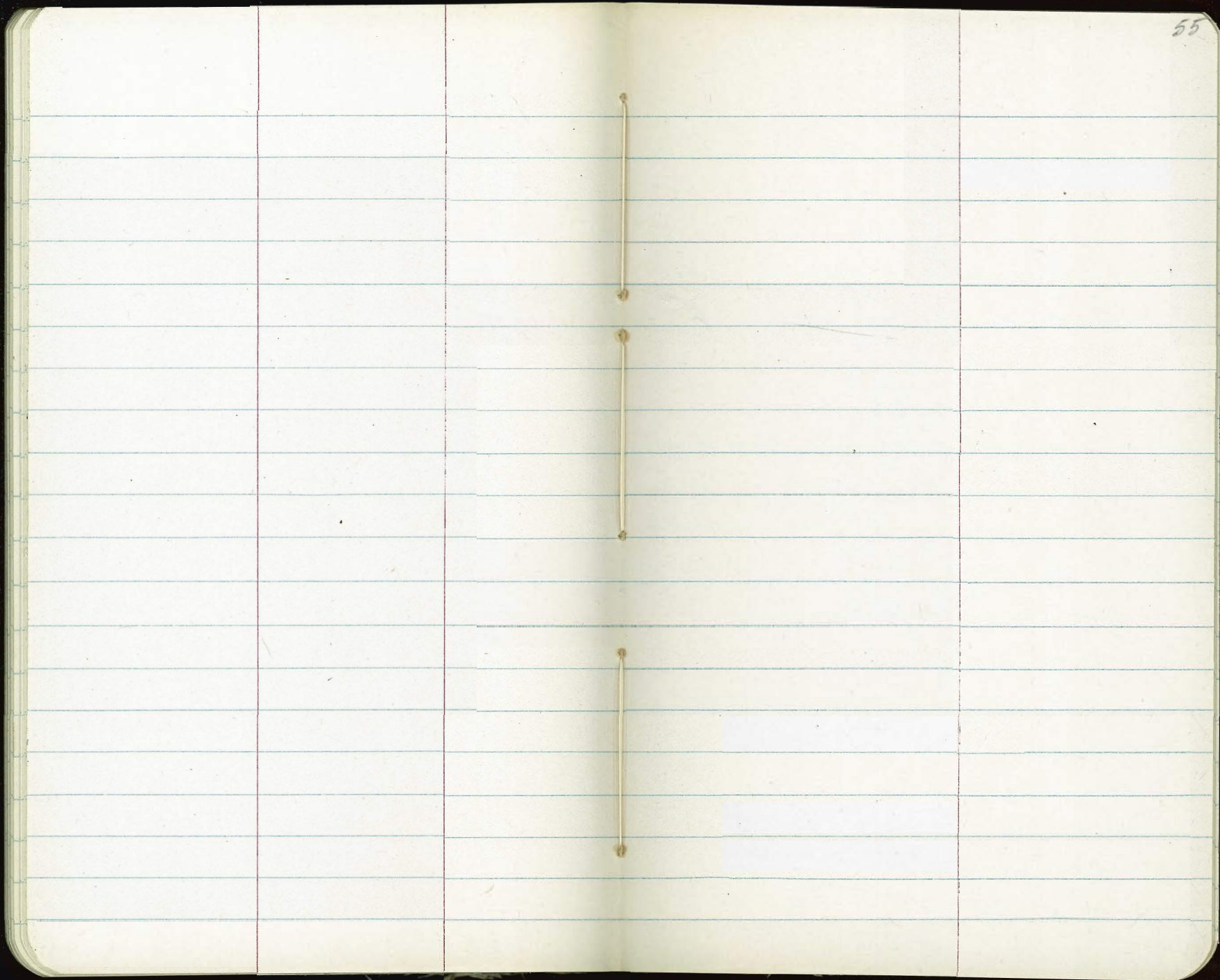


The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. The notebook is bound in the center, and the pages have rounded corners. The number '38' is handwritten in the top right corner of the right page. The notebook is set against a dark, possibly black, background.

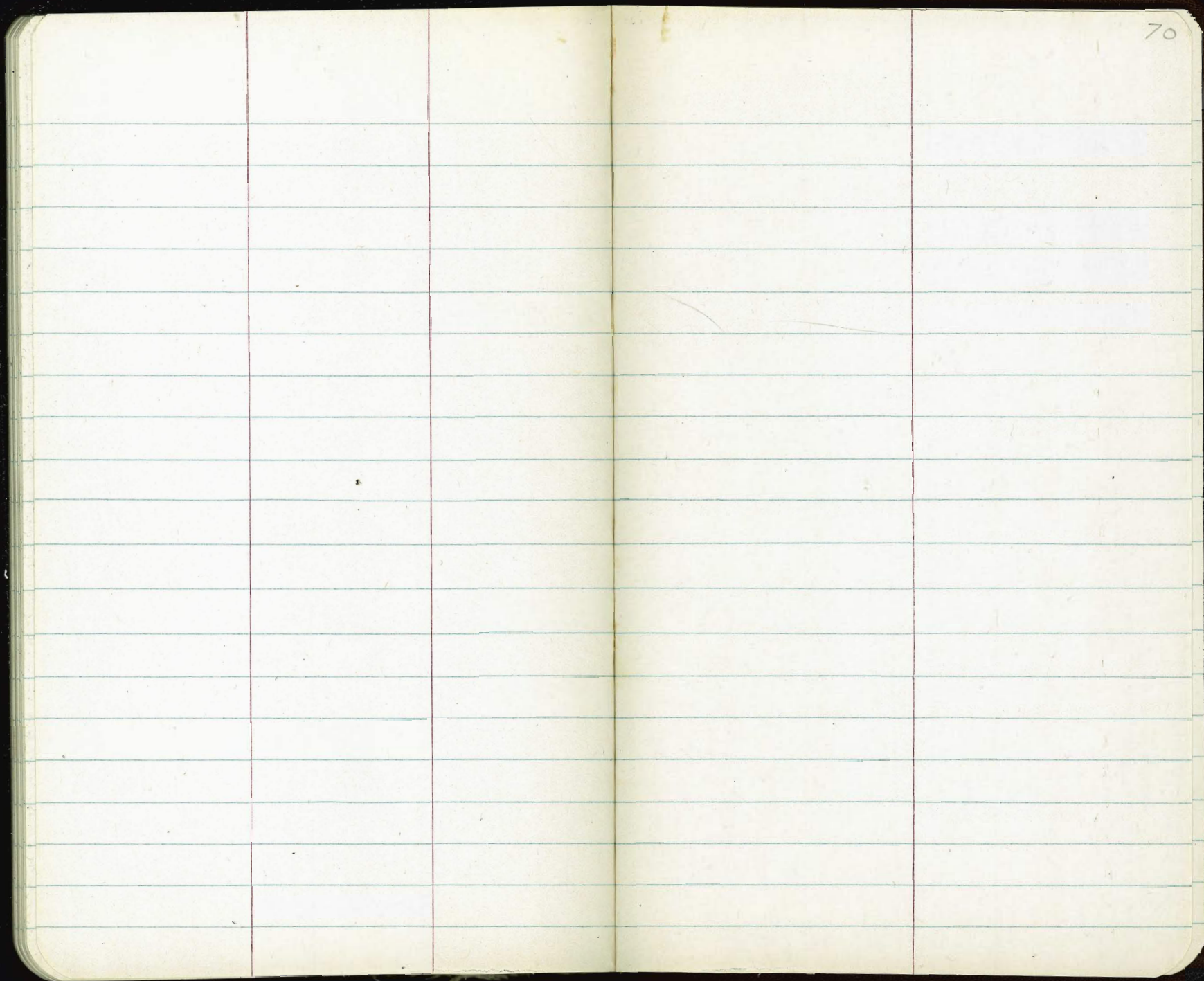
An open notebook with two blank, lined pages. The pages are cream-colored with light blue horizontal ruling. The notebook has rounded corners and a dark cover visible around the edges. The right page has the number '40' written in the top right corner. The pages are otherwise empty of any text or drawings.

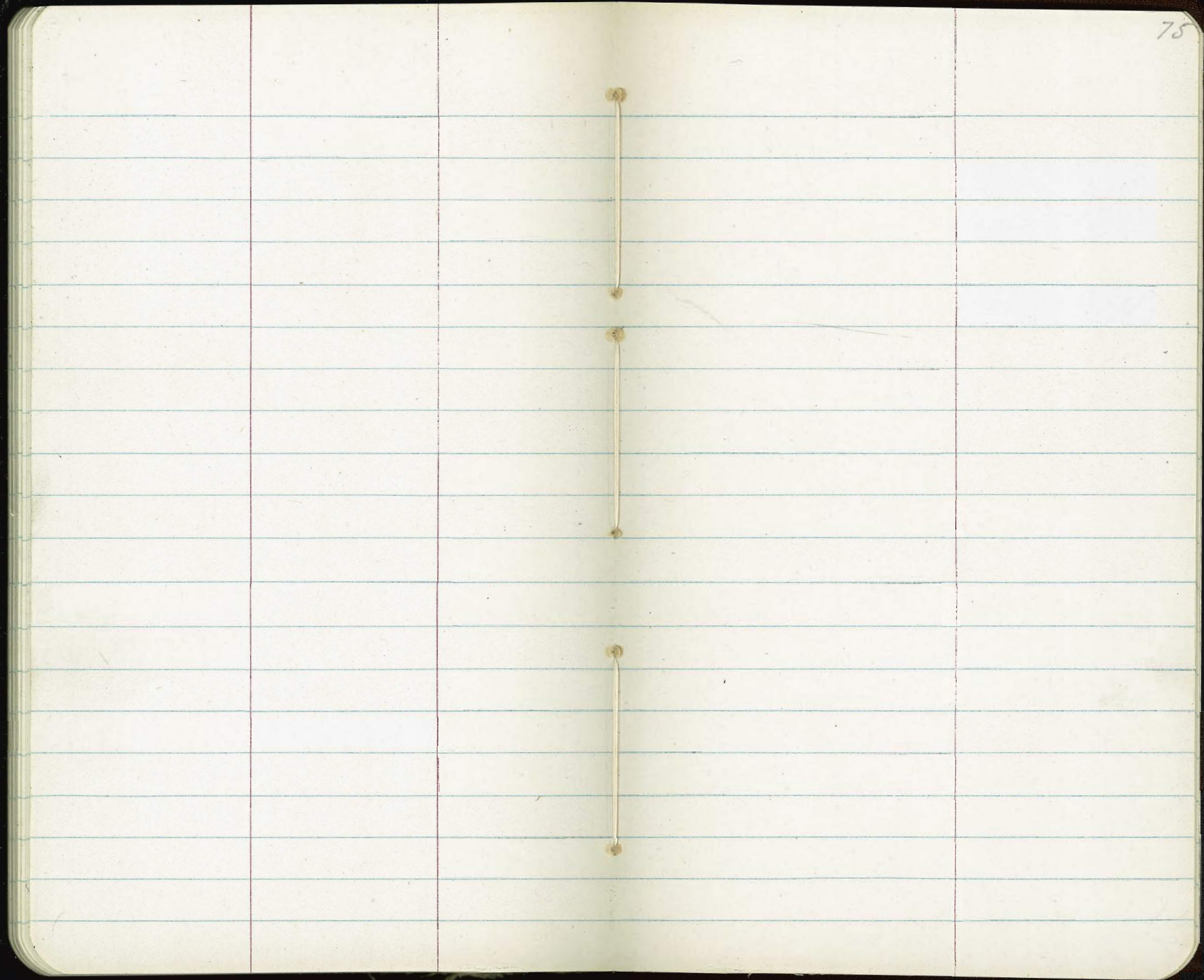


The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. The notebook is bound in the center, and the pages are otherwise blank. The right page has the number '44' written in the top right corner. The notebook's dark cover is visible at the edges.



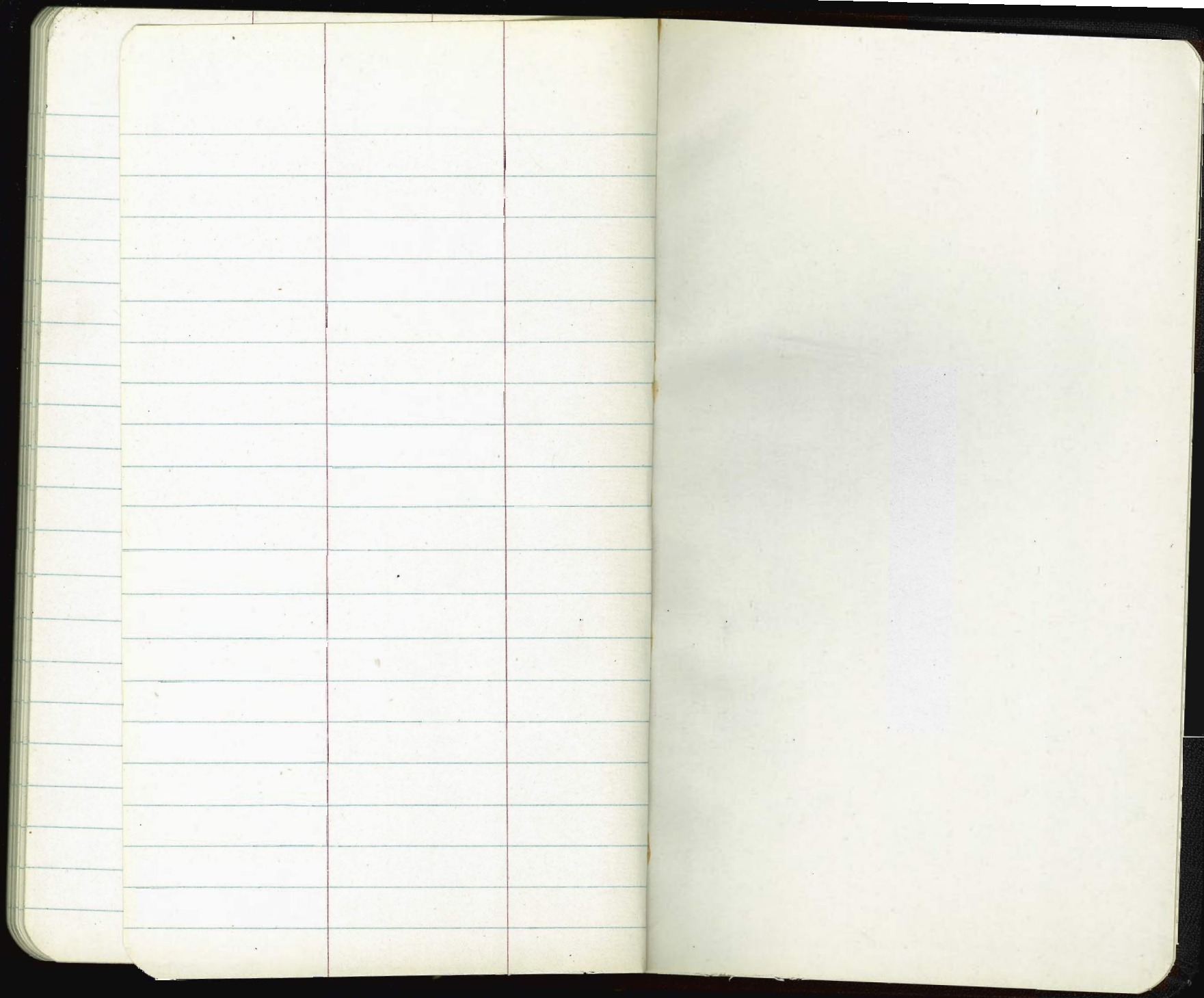
The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. A vertical red margin line is present on the left side of each page. The right page has the number '67' written in the top right corner. The notebook is placed on a dark, possibly black, background.





The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page is divided into three vertical columns by two faint red lines. The leftmost column is the narrowest, the middle column is the widest, and the rightmost column is of medium width. The pages are otherwise blank, with no handwriting or printed text. The notebook's dark cover is visible at the very edges. In the top right corner of the right page, the number '76' is handwritten in a small, dark ink.

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature horizontal light blue ruling. The left page is divided into three vertical columns by a red margin line on the left and a blue margin line on the right. The right page is divided into two vertical columns by a blue margin line on the left. The notebook is bound in the center, and the pages are otherwise blank.

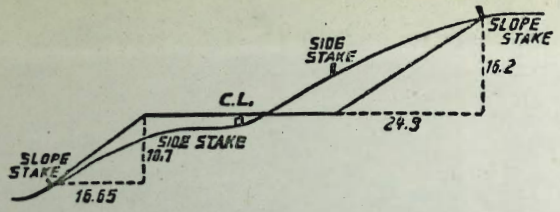


2596
25

1428
50
450.8

1910080
195572
4508

1816
4079
855



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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