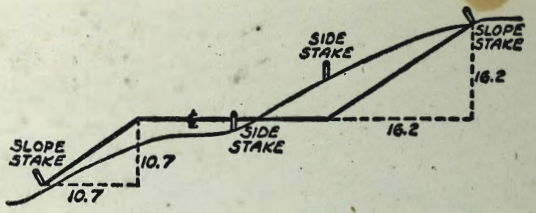


Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

M-366

IMPROVED TABLES
AND
INFORMATION

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

INDEX

Pg

CLARK
GARBER
ONEIL
ARRENILLA
5-31-56
W.O. 32458

63rd (CATOCTIN DR.)
EL CAJON to CHOCTAW

Ref: DWG: 2979-D
F.B. 1854
T.P. 29

STA.	P.L.	CB	℄	CB	P.L.
0+61.51 = Prop BC. LT.	465.49 465.33 CO.1.6	465.52 465.33 CO. 19		465.25 465.37 FO. 12	465.37
0+43.16 = CB E.C. RT. (NELY)	465.53 465.40 CO, 13	465.55 465.40 CO. 15		465.34 465.44 FO.10	465.44 chk TP CB
0+20.08 LT. only	465.55	465.49 465.55 FO.06			
0-03 = CB E.C. LT (NWLy) EXIST	465.57 465.70 FO. 13				
EXIST CB	465.73				
[0+00 = Orig. N'ly Line EL CAJON F.B 1854]					
B.M Dir. elev. Rod					463.01 = N.E B.P ROSE+ MILLAR

Approx. 150' N'ly Transferred to P.P. 7603 (SW P. Pole Rose + 63rd)

STA.	P.L	CB	℄	CB	P.L
2+75	464.92 464.56 CO.36	464.94 464.56 CO.38		464.76 464.60 CO.16	465.19 464.60 60.59
2+50	464.65	464.96 464.65 CO, 31		464.85 464.69 CO, 16	464.69
2+36.71 = E.C 63rd ST.	464.90 464.70 CO.20	464.95 464.70 CO.25		464.98 464.74 CO, 24	465.12 464.74 CO. 38
2+16.09	464.96 464.78 CO. 18	465.03 464.78 CO.25		464.98 464.82 CO.16	464.95 464.82 CO.13
1+95.47	464.91 464.85 CO.06	464.92 464.85 CO.07		464.90 464.89 CO.01	464.83 464.89 FO.06
{Curve 3 PTS E Ch = 20.61' Rad 1° [illegible]					
1+74.85 = B.C 63rd ST. Δ=3°37 LT.	464.78 464.92 FO.14	464.91 464.92 FO.01		464.81 464.96 FO.15	464.79 464.96 FO.17
1+50	465.36 465.01 CO.35	465.36 465.01 CO.35		464.33 465.05 FO.72	464.82 465.05 FO.23
1+25	465.10	465.99 465.10 CO.89		465.01 465.14 FO.13	465.14
1+00	465.64 465.19 CO.45	465.71 465.19 CO.42		464.96 465.23 FO.27	464.82 465.23 FO.41
0+75	465.28	465.49 465.28 CO. 21.		464.94 465.32 FO.38	465.32

STA	P.L	CB	℄	CB	P.L
Note: Curb on LT goes on tang	Rose &	63'rd. (does not Follow Curve From here		n.ly to S.w'ly	63'rd ST. Cor Nov 19
Curve 4 pts Ech = 25.85' def 1°25'30"					
4453.38 = BC	464.18	464.77		464.08	464.05
63'rd Δ = 11°24'	463.91	463.91		463.95	463.95
RT	Co.27	~~Co.90~~ Co.86		Co.13	Co.10
4433.27	464.29	464.66		464.29	464.15
	463.99	463.99		464.03	464.03
	Co.30	Co.67		Co.26	Co.12
4413.16	464.06	464.49		464.37	
		464.06		464.10	464.10
		Co.43		Co.27	
	464.40	464.62		464.30	464.38
3+93.05 = EC	464.13	464.13		464.17	464.17
63'rd ST.	Co.27	Co.49		Co.13	Co.21
	464.50	464.70		464.46	464.48
3+70.30	464.22	464.22		464.26	464.26
	Co.28	Co.48		Co.20	Co.22
	464.80	464.83		464.60	464.60
3+47.56	464.30	464.30		464.34	464.34
	Co.50	Co.53		Co.26	Co.26
Curve 3 pts Ech = 22.74' def 8°38'20"					
	465.04	465.08		464.64	464.65
3+34.81 = BC	464.38	464.38		464.42	464.42
63'rd Δ = 30°50' RT	Co.76	Co.70		Co.22	Co.23
3+00	464.47	464.90		464.58	
		464.47		464.51	464.51
		Co.43		Co.07	

STA.	P.L	CB	℄	CB	P.L
				463.73	
				463.42	463.42
				Co.31	
6+23.93 = CB					
BC RT.					
					463.68
6+20.18 = Prop				463.44	463.44
BC RT.					Co.24
				463.81	
6+00				463.50	463.50
				Co.31	
				463.97	
5+75				463.60	463.60
				Co.37	
					463.53
				463.87	463.64
5+56.84 = EC				463.64	Fo.11
RT. only				Co.23	
				463.88	
5+30.97 RT				463.72	463.72
only				Co.16	
				463.75	463.78
5+05.11 RT.				463.80	463.80
only				Fo.05	Fo.02
Chk:	463.80 =	TP CB	Chk:		
4483.38 ± meet	463.81	463.81			
Exist CB LT only					
				463.88	
4479.24 RT				463.87	463.87
only				Co.01	
		464.81			
4460 LT only	463.88	463.88			
		~~Co.89~~			
		Co.93			

STA.	P.L	CB	℄	CB.	P.L
#A = E.C				463.71 TREMIST CB 463.72	
#3				463.70 463.64 C0,06	
#2				463.69 463.56 C0.13	
#1				463.66 463.48 C0.18	463.48

STA.	P.L	CB	℄	CB	P.L

CJARK
GARBER
ONEIL
ABRENILLA
6-12-56
W.O. 31814

Imp's Seminole Drive - et al

Ref: F.B. 1301 - 1340 - 2254 - T.R.B 29 · 4
DWG: 11929-L to 11935A-L

SEWER: Lots 21-22 Lamesa Colony
EXIST. M.H (7743-L) to ℄ Seminole & ART.

STA.		Elev's
2+80 (Stubs 5' RT℄)	5.46% ↑	450.41 429.18 C 21.23
2+40.03 = M.H #8 = ℄ LT. 16° 53' = grid Brng. Stubs 5.06 & 10.12 RT	454.50 = Tp M.H	436.55 427.00 = F.L. C 9.55
2+00		434.36 425.66 C 8.70
1+60		433.12 424.32 C 8.80
1+20	3.33% ↑	431.89 422.99 C 8.90
0+80		428.99 421.66 C 7.33
0+40 (Stubs 5' LT℄)		426.64 420.33 C 6.31
0+00 = EXIST M.H. See DWG (7743-L)	(419.00)	
B.M. Div. Elev. Bol		458.12 = Ch□ Tp CB LT. at STA 20+00.97 F.B. 2254-29-54

STA		Elev's
6+80		453.41 445.22 C 8.19
6+40		452.74 444.20 C 8.54
6+00		452.39 443.19 C 9.20
5+60	2.52% ↓	451.97 442.18 C 9.79
5+20		451.53 441.17 C 10.36
4+81.93 = M.H #7 (Grade Brng.) P.O.T Stubs 5+10 RT℄	450.30 Tp M.H	451.32 440.22 = F.L. C 11.10
4+40		450.94 437.92 C 13.02
4+00	5.46% ↓	450.48 435.74 C 14.74
3+60		450.21 433.55 C 16.66
3+20		450.07 431.37 C 18.70

Sewer — LOTS 21 & 22 LA MESA Colony (cont.)

STA		Elev's:
	(stubs set 5.85 & 11.70 sw'ly quad)	
7+81.93 = ℄ Seminole = M.H #6 ℄ ART		456.40 447.80 C 8.60
7+60		456.64 447.24 C 9.40
7+20	1 2.52%	453.96 446.22 C 7.74

SEWER: ART. ST.
M.H #6 ℄ Seminole N'ly 33.64'

STA.		Elevs
0+33.64 = P/vg. end ℄ ART ST. (Stub 5' RT ℄)		456.75 448.81 C 7.94
0+00 = M.H #6 ℄ Seminole ℄ ART	see Pg 5 (opposite)	447.80

6-A

SEWER: Seminole DRIVE
MH #6 & Seminole & ℄ ART-N'ly 185'
to D.End

STA.		Elev's:
1+85 = Plug-end		457.27 450.15 C 7.12
Stub's Bk Prop ON℄ LAT.		
1+75 = Sew LAT #23 - RT	457.94 450.32 C 7.62	457.94 450.92 C 7.02
1+60		457.18 449.83 C 7.35
1+20		457.01 449.33 C 7.68
1.27%		
0+80		456.82 448.82 C 8.00
(Stub's RT ℄)		
0+40		456.51 448.31 C 8.26
0+00 = M.H #6 & Seminole & ART	(See pg 5)	447.80
BM		N'ly Seminole 458.12 – Ch□ CB [STA. 2+00.99 F.B (2254)

Sewer: Seminole Drive:
M.H #6 & Seminole & ART-S'wly

6B

STA.		Elev's
1+69 = Sew LAT #20 ON RT	459.39 450.5 C 8.89	459.39 451.1 8.29
1+60		457.01 450.11 C 6.90
1+20		456.18 449.53 C 6.65
1+09 = Sew LAT #21 ON RT	457.45 449.7 C 7.75	457.5 450.3 C 7.2
0+80		456.17 448.95 C 7.22
0+76 = Sew LAT #22 ON RT.	457.96 449.2 C 8.76	457.96 449.82 8.14
1.44%		
0+40		456.44 448.37 C 8.07
0+27 End ENCASE		
0+17 Beg Conc. ENCASE:		
0+00 = M.H #6 & Seminole + ART		447.80

Sewer: Seminole Dr. Sw 4Y
MH #6 (Cont.)

STA.		Elev's:
4+00 = M.H #9 stubs set	5.09 RT.	461.80
∠ LT = 21°01'00"		453.56 = F.L
		C 8.24
3+60		461.13
		452.99
		C 8.14
~~stubs set 5+10 RT~~		
~~3+50 = M.H #9~~ changed		~~452.84~~
~~∠ 8°12'48" LT.~~	As per office Cole	
= grade Brk		
3+49 = Sew Lat #17	462.29	462.29
RT	453.0	453.6
	C 9.29	C 8.69
3+20		460.39
		452.41
		C 7.98
2+80		459.69
		451.83
		C 7.86
2+77 = Sew Lat #18	461.03	461.03
RT	452.0	452.6
	C 9.03	C 8.43
2+40		458.92
		451.26
		C 7.66
2+00		457.90
		450.69
		C 7.21
2+00 Sew Lat #19	460.12	460.12
RT	450.9	451.9
	C 9.92	C 9.22

STA	Elev's:
7+70	465.39
	455.98
	C 9.41
7+35	465.24
	455.83
	C 9.41
7+00	464.88
	455.68
	C 9.20
6+65	464.70
	455.53
	C 9.17
6+30	464.51
	455.38
	C 9.13
5+95	464.16
	455.23
	C 8.93
5+60	463.64
	455.08
	C 8.56
5+25	463.10
	454.93
	C 8.17
5+00	462.52
	454.82
	C 7.70
Stubs set 5.1 & 14.2 RT	
4+82.63 = M.H #10	462.39
= ∠ LT 23°04'15"	454.75
= grade Brk	C 7.64
(stubs set 5.30 & 10.60 RT)	
4+90 = M.H #10	~~454.86~~
∠ LT 38°21'01"	changed as per office — Cole
= grade Brk	
4+40	461.99
	454.76
	C 7.81

Sewer: Seminole Dr. MH #6 - SW'ly (Cont.)

STA.			Elevs:	STA.	LT.		RT.
			465.75				
9+69.00 = Plug-END			459.70				
			C 6.05				
	466.1		466.1				
9+63.00 = Sew Lat #15	459.8 ℄		460.4 Prop				
RT	C 6.3		C 5.7				
			465.69				
9+53.00			459.28				
			C 6.41				
	466.3	466.3					
9+21.00 = Sew Lat #12	460.6 Prop	458.8 ℄					
LT.	C 5.7	C 7.5					
			465.71				
9+13.00			458.27				
			C 7.44				
1			465.60				
8+73.00 2.5%			457.25				
			C 8.35				
				10+72.4 Sew Lat #30 RT.		466.02	466.02
						457.63 ℄	458.23 Prop
						C 8.39 ℄	C 7.79
	466.3	466.3					
8+73.87 = Sew Lat #13	460.7 Prop.	457.6 ℄					
LT.	C 5.6	C 8.7					
		465.3	465.3				
8+38.87 = Sew Lat #16		456.7 ℄	460.5				
RT.		C 8.6	C 4.8				
			465.54				
8+33.00 = M.H #11 = P.O.T			456.24				
~~4 RT 2° 28' 34"~~			C 9.30				
= grid BRG (Stubs set 5' ℄ 50' RT.)				10+25 Sew Lat #29 LT.	466.10	466.10	
					458.53 Prop.	457.93 ℄	
					C 7.57	C 8.17 ℄	
			465.53				
8+05			456.12				
			C 9.41				
0.4%							
	466.3	466.3					
7+84.89 = Sew Lat #14	460.0 Prop	456.4 ℄					
LT.	C 6.3	C 9.9					

Sewer: ACORN ST. (E'ly Seminole)

From ℄ EXIST 10' EASEMENT / LOT 20 LA MESA Colony to PT. 90' E'ly ℄ Seminole DR.

STA		Elev's:
1+69.22 = M.H #4 = grid BRG	448.89 = TP	448.93 443.11 = F.L C 5.82
1+32.22 = ℄ CUT-OFF WALL		443.09 433.77 C 9.32
0+92.22 = ℄ CUT-OFF WALL		432.72 423.67 C 9.05
25.25 ℄		
0+52.22 = ℄ CUT-OFF WALL		420.80 413.57 C 7.23
0+27.22 = ℄ CUT-OFF WALL	412.77 407.25 C 5.52	~~410.78~~ ~~407.25~~ ~~C 3.53~~
0+00 = M.H #5 ℄ 10' EASEMENT LOT 20 LA MESA Colony	~~404.62~~ 405.84 = TP F 0.76 F 1.22	~~404.62~~ 400.43 = F.L ~~C 4.19~~ C 6.26
B.M.	DIR. ELEV. RD:	465.68 = SPIKE & Pk SE'ly Seminole & ACORN

STA		Elev's:	
4+16.35 = M.H. #3 = grid BRG			454.69 445.55 = F.L C 9.14
4+00			454.32 445.41 C 8.91
3+90.74 = LAT #9 LT.	456.5 446.1 P.L C 10.4	456.5 445.6 ℄ C 10.9	
3+60			453.44 445.02 C 8.42
3+48.48 = LAT #10 LT.	450.2 445.6 proj C 4.6	450.2 445.1 ℄ C 5.1	
3+20			452.64 444.62 C 8.02
2+80			451.75 444.22 C 7.53
2+40			450.70 443.82 C 6.88
2+00			449.70 443.42 C 6.28

SET TBM = 467.685 = old SE'ly corn. Conc. Porch NWly ACORN & Seminole (#4570 Seminole)

SEWER: ACORN (E/y of Seminole) (cont.)

STA.		Elev's:		STA.		Elev's:	
6+66.26 = LAT #24 Lt.	459 454.2 P.L C 3.1	457.9 453.7 ℄ C 4.2					
6+50			459.41 452.88 C 6.53				
6+10			458.54 451.62 C 6.92	8+31.35 = Plug-end			464.38 457.50 = F.L C 6.88
6+06.74 = LAT #25 Lt.	453.7 452.3 P.L C 1.4	453.7 451.8 ℄ C 1.9		8+24.09 = LAT #7 Rt.		465.3 457.6 ℄ C 7.9 ℄	465.5 458.1 P.Line C 7.4
5+70			457.77 450.37 C 7.40	7+90			463.86 456.60 C 7.26
5+46.74 = LAT #26 Lt.	456.5 450.4 P.L C 6.1	456.5 449.9 ℄ C 6.6		7+50			462.85 455.74 C 7.11
5+30			457.01 449.11 C 7.90	7+34.09 = LAT #6 Rt.		464.4 455.7 ℄ C 8.7	464.4 456.2 P.L C 8.2
4+90.74 = LAT #8 Lt.	459.3 448.9 P.L C 10.4	448.4 ℄		7+28.26 = LAT #11 Lt.	463.98 456.1 P.L C 7.88	463.98 455.6 ℄ C 8.38	
4+90			456.22 447.85 C 8.37	7+21.35 = M.H #12 = grd B+H			460.84 455.12 = F.L C 5.72
4+50			455.41 446.60 C 8.81	6+90			460.16 454.13 C 6.03

SEWER: ACORN - Seminole, W'ly
& 63'rd

STA	Elev's:		STA.	Elev's:	
			4+40		465.84 458.65 C 7.19
2+10		465.54 457.58 C 7.96	4+05		466.01 458.47 C 7.54
2+05 = LAT #2 RT.	465.75 457.9 ℄ C 7.85	465.75 460.3 Prop C 5.45	4+04.76 = LAT #32 RT.	465.8 458.8 ℄ C 7.0	465.8 459.3 Prop C 6.5
1+75		465.84 457.45 C 8.39	3+99.76 = LAT #3 LT.	4658 459.3 Prop C 6.5	4658 458.7 ℄ C 7.1
1+40		465.09 457.32 C 8.57	3+70	↑ 50	465.77 458.29 C 7.48
1+05	1 48	465.99 457.19 C 8.80	3+35		465.99 458.11 C 7.88
0+70	Note: Changes grade from 3.6% to 2.4%	465.83 457.06 C 8.77			
0+35		465.89 456.93 C 8.96	3+01.96 = M.H #2 (6') ∠ RT. 89°59'30" -grid brk	(Stakes set 7.07 & 14.14 RT)	466.00 457.93 C 8.07
Σ = EXIST M.H 7 0+00 = Σ Seminole & ACORN, W'ly	Chk: 456.82 = F.L Plug-W'ly Chk: 456.79 F.L M.H 456.73 = F.L		2+80		465.32 457.85 C 7.47
B.M. See Pg 9			2+45		465.40 457.71 C 7.69

Sewer: ACORN ST. ∀ 63rd
Seminole W'ly

			F. Line Elevs
5+51.16 = Plug-end			465.94 459.22 C6.72
5+40.16 = M.H #9 P.O.T.			465.96 459.17 C6.79
5+11.16 = LAT #6 RT.		465.7 459.3 ℄ C6.4	465.7 459.9 Prop C5.8
5+10			465.73 458.02 C7.71
5+06.16 = LAT # 5 LT.	465.7 459.8 Prop C5.9	465.7 459.3 C6.4	
4+75			465.62 458.83 C6.79
4+59.16 = LAT. #31 RT.		465.7 459.0 ℄ C6.1	465.7 459.6 Prop. C6.1
4+56.16 = LAT #4 LT.	465.8 459.6 Prop C6.2	465.8 459.0 ℄ C6.8	

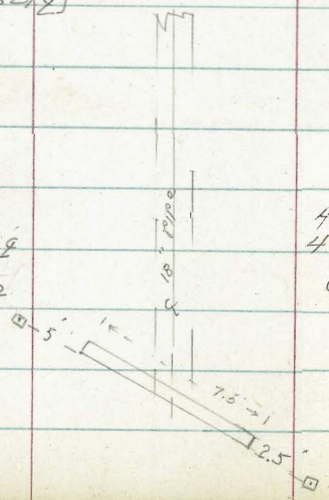
STORM-DRAIN - Seminole YART

S'Ely

Ref: DWG: 11935-L
" 6148-B
F.B 2254

13

STA	Elevs:	
W.O. 31814 = Beg Job this Contract.		
2+03.44 = ℄ Type G Cleanout. F.L = 450.81 / 447.80 / C 6.01	450.95 (Knocked out by Const) / 447.80 = F.L / C 6.15	
1+70.14 (mid-pt.)	450.60 / 441.23 / C 9.37	
1+38.34 = grid Brk	450.18 / 437.67 = F.L / C 12.51	
1+20	450.01 / 437.21 / C 12.80	
0+80	449.59 / 436.22 / C 13.37	
0+40 (Stubs 6' Lt ℄)	446.95 / 435.23 / C 11.72	
0+00 = Fc Headwall ℄ 18" Conc. Pipe on S'Ly Line Lot 22 La Mesa Colony	435.57 / 434.23 = F.L. Pipe / C 1.34	
	ON Lot Line Stubs Set on Fc H'dwall	
5+66.1 ℄ CB Inlet #1 at CB Fc (15'A-2) N'Ly CB Seminole		456.66 / 450.50 = F.L Box / C 6.16
5+16.4 = CB Fc ℄ Inlet #2 (15'A-2) S'Ly CB Seminole)		456.85 / 449.70 = F.L Box / C 7.15
4+80		454.25 / 449.17 / C 5.08
4+40		453.49 / 448.55 / C 4.94
4+00		453.02 / 447.91 / C 5.11
3+60		452.60 / 447.28 / C 5.32
3+20		451.94 / 446.65 / C 5.29
2+80		451.61 / 446.02 / C 5.59
2+40		451.28 / 445.39 / C 5.89
Bm		458.12 (See Pg 4)



Seminole Dr. (St. Grades)

ESTRELLA N'LY to CAJON

STA.	P.L	CB	℄	CB	P.L
(1+01.18)=CB EXIST B.C RT.					
1+00	464.65 462.75 C1.90	462.51 462.75 Fo.24			
0+75	462.65	462.40 462.65 Fo.25			
0+35.54=CB B.C LT.	464.03 462.57 C1.46	462.24 462.57 Fo.33			
#1	462.55	462.12 462.55 Fo.43			
#2	462.53	462.04 462.53 Fo.49			
#3 = mid-pt.	463.92 462.51 C1.41	461.95 462.51 Fo.56			
#4	462.49	461.91 462.49 Fo.58			
#5	462.47	461.91 462.47 Fo.56	(Use 5+58 at edge)		
(℄ Cross-Gutt. 92.02 461.77=Gutt. Fo.25			461.77 461.48 Co.29 ← F. Line Cross. Gutt at ℄ St.	EXIST Gutt 461.30	
#6 = END. CB.	463.88 462.44 C1.44	462.12 462.44 Fo.32			

BM (See Pg 9)

STA	P.L	CB	℄	CB	P.L
3+25	463.65	463.25 463.65 Fo.40		463.16 463.59 Fo.43	463.59
3+00	464.56 463.55 C1.01	463.11 463.55 Fo.44		462.92 463.48 Fo.56 (Fo.54	463.58 463.48 Co.10
2+75	463.45	462.98 463.45 Fo.47		462.78 463.37 Fo.59 (F.o.54)	463.37
2+60.60=Beg. (grd BRK) CB.RT	464.38 463.40 C.98	462.96 463.40 Fo.44		463.31	meet EXIST 463.31
2+50	463.35	462.91 463.35 Fo.44			
2+25	463.25	462.77 463.25 Fo.48			
2+00	464.60 463.15 C1.45	462.72 463.15 Fo.43			
1+75	463.05	462.74 463.05 Fo.31			
1+50	464.78 462.95 C1.83	462.71 462.95 Fo.24			
1+25	462.85	462.52 462.85 Fo.33			

Seminole (Cont.)

STA.	P.L	CB	℄	CB	P.L
# 3 mid-pt.				463.72 464.14 Fo. 42	465 26 464.14 C 1.12
# 2				464.20 464.20 Grade	464.20
# 1				464 06 464.19 Fo. 13	464.19
453.73 = CB BC RT S 8E'ly Acorn Seminole	465.17 464.17 C1.00	464.17	not sat. at	463.80 464.17 Fo. 37	465.14 464.17 Co. 91
4+50	464.16	463 88 464.16 Fo. 28		463.89 464.14 Fo. 25	464.14
4+25	465 03 464.06 Co. 97	463.96 464.06 Fo. 30		463.86 464.03 Fo. 17	464 96 464.03 Co. 93
4+00	463.96	463.58 463.96 Fo. 38		463 62 463.92 Fo. 30	463.92
3+75	464.91 463.86 C1.05	463.49 463.86 Fo. 37		463.52 463.81 Fo. 29	463 91 463.81 Co. 10
3+50	463.76	463.36 463.76 Fo. 40		463 44 463.70 Fo. 26	463.70
3+36.61	464.67 463.70 Co. 97	463 34 463.70 Fo 36		463 38 463.64 Fo. 26	463 38 463.64 Fo. 26

STA.	P.L	CB	℄	CB	P.L
# 6 (67° 29' 36")	464.69	464.30 464.69 Fo. 39			
# 5 (56° 14' 40")	464.62	464.34 464.62 Fo. 28			
# 4 mid. pt. (44° 59' 44")	465 51 464.55 Co. 96	464 19 464.55 Fo. 36			
# 3 (33° 44' 48")	464.48	464. 11 464.48 Fo. 37			
# 2 (22° 29' 52")	464.42	464 16 464.42 Fo. 26			
# 1 (11° 14' 56")	464.36	464 05 464.36 Fo. 31			
484.01 = = C.B., B.C., Lt. S W'ly	465 22 464.30 Co. 92	464 08 464.30 Fo. 22			
475 = Lt. only	464.26	464 29 464.26 Co. 03			
# 5 = E.C.				463 47 463.74 Fo. 27	463.74
# 4				463 36 463.95 Fo. 59	463.95

Seminole (Cont.)

STA.	P.L	CB	℄	CB	P.L
5+50				464.39 464.55 Fo. 16	464.55
#5 = E.C ACORN				463.84 463.74 C0.10	465.48 463.74 C1.74
#4				464.02 463.96 C0.06	463.96
#3				464.11 464.18 Fo.07	464.18
#2				464.20 464.35 Fo.15	464.35
#1				464.27 464.50 Fo 23	464.50
5743.73 = CB BC. RT N'ELy Seminole ACORN				464.32 464.53 Fo.21	465.42 464.53 C0.89
#8 = E.C ACORN (89°59'30")	464.83	464.70 464.83 Fo 13			
#7 (78°44'32")	464.76	464.50 464.76 Fo.26			

	LT.			RT.	
STA.	P.L	CB	℄	CB	P.L
6+50	465.83 464.96 C0.87	464.60 464.96 Fo.36		464.70 464.96 Fo.26	466.47 464.96 C1.51
6+25	464.86	464.40 464.86 Fo.46		464.54 464.86 Fo.32	464.86
#4 = E.C ON ACORN	464.72	464.49 464.72 Fo.25			
#3	464.71	464.31 464.71 Fo.40			
#2	464.70	464.32 464.70 Fo.48			
#1	464.74	464.42 464.74 Fo.32			
6+04.01 = CB BC LT. NWLy	466.15 464.78 C1.37	464.25 464.78 Fo.53		464.41 464.78 Fo.37	466.01 464.78 C1.23
6+00				464.46 464.76 Fo.30	464.76
5+75				464.43 464.66 Fo.23	464.66

Seminole (cont.)

STA.	P.L	LT. CB	℄	RT. (E'LY) CB	P.L
8+20.22 = B.V.C	465.50 465.64 Fo.14	465.24 465.64 Fo.40		465.31 465.64 Fo.33	466.38 465.64 Co.74
8+07 = W.S. — — RT.					466.42 465.50 = Tack Co.92
8+00	465.74 465.56 Co.18	465.01 465.56 Fo.55		465.15 465.56 Fo.41	466.21 465.56 Co.65
7+75	465.46	464.85 465.46 Fo.61		465.01 465.46 Fo.45	466.28 465.46
7+50	466.07 465.36 Co.71	465.00 465.36 Fo.36		464.97 465.36 Fo.39	466.29 465.36 Co.93
7+25	465.26	464.86 465.26 Fo.40		464.86 465.26 Fo.40	465.26
7+07 = W.S. — — RT.					466.07 465.20 = Tack Co.87
7+00	466.94 465.16 Co.78	464.69 465.16 Fo.47		464.81 465.16 Fo.35	466.10 465.16 Co.94
6+75	465.06	464.56 465.06 Fo.50		464.98 465.06 Fo.08	465.06
6+54 = W.S. — — LT.	465.93 465.00 = Tack Co.93				

STA	P.L	LT. CB	℄	RT. CB	P.L
10+37.93 LT. only	463.96	463.84 463.96 Fo.12			
10+12.93 = CB BC RT SELY (STANLEY) EXISTING	464.81 464.21 Co.60	463.94 464.21 Fo.27		chk: 464.21	464.20 464.21 MEAT EXIST.
10+00	464.70 464.34 Co.36	464.10 464.34 Fo.24		464.07 464.34 Fo.27	465.76 464.34 C1.42
9+75	464.61	464.49 464.61 Fo.12		464.47 464.61 Fo.14	464.61
9+50	464.66 464.87 Fo.21	464.64 464.87 Fo.23		464.72 464.87 Fo.15	466.17 464.87 C1.30
9+25	465.13	464.82 465.13 Fo.31		465.18 465.13 Co.05	465.13
9+00.22 = E.V.C	465.03 465.38 Fo.35	465.17 465.38 Fo.21		464.94 465.38 Fo.44	466.29 465.38 Co.91
8+80.22	465.56	465.28 465.56 Fo.28		464.86 465.56 Fo.70	465.56
8+60.22	465.33 465.66 Fo.33	465.44 465.66 Fo.22		465.06 465.66 Fo.60	465.92 465.66 Co.26
8+40.22	465.69	465.21 465.69 Fo.48		465.28 465.69 Fo.41	465.69

Seminole (Cont.)

STA. (Curve in 5 pts.)	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
Δ = 44° 05' 15"					
ℇR = 142.30					
T = 57.62'					
12+18.57 =	462.48	461.79		461.68	462.17
(B.C Seminole)	461.68	461.68		461.68	461.68
	C0.80	C0.11		GRADE	C0.49
12+00	461.93	461.81		461.81	461.93
		461.93		461.93	
		Fo.12		Fo.12	
11+75	463.90	462.08		462.03	463.16
	462.28	462.28		462.28	462.28
	C1.62	Fo.20		Fo25	C0.88
11+50	462.62	462.61		462.65	462.62
		462.62		462.62	
		Fo.01		C0.03	
11+42.93	464.40	462.67		462.50	463.86
= E.V.C	462.72	462.72		462.72	462.72
	C1.68	Fo.05		Fo.22	C1.14
11+22.93	463.02	463.14		462.86	463.00
		463.02		463.00	
		C0.12		Fo.14	
EXIST. 11+02.93 = CB	464.35	463.18		chk:	463.28
BC. RT (NE'LY) STANLEY	463.27	463.27			463.30
	C1.08	Fo.09			
10+82.93	463.50	463.28			
LT. only		463.50			
		Fo.22			
	465.09	463.55			
10+62.93 =	463.71	463.71			
B.V.C LT. only	C1.38	Fo.16			

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
14+75	458.30	458.02		458.29	457.96
		458.30		457.96	
		Fo.28		C0.33	
14+50	460.66	458.40		458.49	456.96
	458.62	458.62		458.33	458.33
	C2.04	Fo.22		C0.14	F1.37
14+25	458.93	458.64		458.76	458.71
		458.93		458.71	
		Fo.29		C0.05	
14+00	461.51	459.04		459.26	457.49
	459.25	459.25		459.08	459.08
	C2.26	Fo.21		C0.18	F1.59
13+75	459.56	459.41		459.68	459.46
		459.56		459.46	
		Fo.15		C0.22	
13+50	462.45	459.67		459.80	458.86
	459.88	459.88		459.83	459.83
	C2.57	Fo.21		Fo.03	F1.47
13+28.07 =	462.74	459.86		460.27	458.77
E.C. Seminole	460.16	460.16		460.16	460.16
	C2.58	Fo.30		C0.11	F1.39
13+06.17	460.46	460.33		460.62	459.57
		460.46		460.46	460.46
		Fo.13		C0.16	Fo.89
12+84.27	463.02	460.36		460.45	461.53
	460.77	460.77		460.77	460.77
	C2.25	Fo.41		Fo.32	C0.76
12+62.37	461.07	460.79		460.75	461.07
		461.07		461.07	
		Fo.28		Fo.32	
12+40.47	464.15	461.11		461.31	462.07
	461.38	461.38		461.38	461.38
	C2.77	Fo.27		Fo.07	C0.69

Seminole (cont.)

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
16+75	456.97	456.97 Not set (sea inlet)		456.46 456.55 F0.09	456.55
16+50	457.64 457.09 C0.55	456.45 457.09 F0.64		456.51 456.69 F0.18	454.15 456.69 F2.54
16+25	457.22	457.14 457.22 F0.08		456.46 456.82 F0.36	456.82
16+00	458.35 457.34 C1.01	456.86 457.34 F0.48		456.85 456.94 F0.09	454.79 456.94 F2.15
15+75	457.47	457.24 457.47 F0.23		457.24 457.07 C0.17	457.07
15+68 = W.S. — — LT.	458.98 457.5 TRCB C1.48				
15+50	459.11 457.59 C1.52	457.61 457.59 C0.02		457.30 457.20 C0.10	455.76 457.20 F1.44
15+30.01 = E.V.C	459.64 457.70 C1.94	457.78 457.70 C0.08		457.32 457.30 C0.02	456.19 457.30 F1.11
15+10.01	457.87	457.72 457.87 F0.15		457.35 457.48 F0.13	457.48
14+90.01 = (Grd Brk) B.V.C	460.29 458.10 C2.19	457.84 458.10 F0.26		457.88 457.73 C0.15	456.62 457.73 F1.11

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
18+00				456.80 456.76 C0.04	456.06 456.76 F0.70
(17+77.59 = CB BC LT EXIST.)					
17+75				456.76 456.66 C0.10	456.66
17+50				456.75 456.55 C0.20	456.40 456.55 F0.15
17+25				456.59 456.45 C0.14	456.45
17+08.37 = grd. brk RT. only Inlet RT.					456.21 456.38 F0.17
17+00 RT only				Not set sea inlet	456.43
#2 = E.C ART (N'W'ly)	456.95	456.49 456.95 F0.46			
#1	456.90	456.44 456.90 F0.96			
16+95.76 = CB. B. C. LT. (NW'ly)	457.51 456.86 C0.65	456.56 456.86 F0.30			

(Note: For CB Inlets #1 + #2 See Pg 30)

Seminole (Cont.)

STA.	P.L	CB	℄	CB	P.L
				457.38	
20+00.97 = B.C (See Pg 21)				457.60	
Seminole				Fo.22	
				457.28	
19+75				457.50	
				Fo.22	
				457.21	457.81
19+50				457.40	457.40
				Fo.19	Co.41
				457.22	
19+25				457.29	
				Fo.07	
				457.02	458.24
19+00				457.19	457.19
				Fo.17	C 1.05
				456.97	
18+75				457.08	
				Fo.31	
				456.83	
18+71.58 =				457.06	
= P.T. 90° to Prop. Conn (± Sub-Line)				Fo. 23	
(Lot 24 La Mesa Colony)					
				456.76	
18+14.78 = CB				456.83	
BC. RT				Fo.07	
(SOLITA)					
= End CB Const. W'ly side SoLITA (Cont. Ely side)					

STA	P.L	CB	℄	CB	P.L

Seminole (Cont.)

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
20+97.47	458.48			457.82 458.00 Fo.18	457.80 458.00 Fo.20
20+73.34	458.38			457.58 457.90 Fo.32	457.90
20+49.22	458.29			457.52 457.80 Fo.28	457.06 457.80 Fo.74
20+25.09 (EXIST. C&B LT. Δ = 43° 18' 45" ΣR = 549.74)	458.19			457.50 457.70 Fo.20	457.70
20+00.97 = BC. Seminole	458.10	458.10		457.38 457.60 Fo.22	456.88 457.60 Fo.72

STA.	LT. P.L	LT. CB	℄	RT. CB	RT. P.L
23+38.72	459.45 459.43 Co.02	459.28 459.38 Fo.10		458.85 459.04 Fo.19	460.13 459.04 C1.09
23+14.59	459.33	459.15 459.26 Fo.11		458.78 458.94 Fo.16	458.94
22+90.47	459.29 459.24 Co.05	458.98 459.15 Fo.17		458.74 458.83 Fo.09	459.77 458.83 C0.94
22+66.34	459.14	458.92 459.04 Fo.12		458.40 458.73 Fo.33	458.73
22+42.22	458.76 459.05 Fo.29	459.81 458.93 Fo.12		458.34 458.63 Fo.29	459.13 458.63 C0.50
22+18.09	458.95	458.81 458.81 Grade		458.14 458.52 Fo.38	458.52
21+93.97	458.29 458.86 Fo.57	458.70 458.70 Grade		458.04 458.42 Fo.38	458.59 458.42 C0.17
21+69.84	458.76	458.84 458.59 Fo.25		458.02 458.32 Fo.30	458.32
21+58 = SOW LAT #28 RT.			458.23 452.10 ℄ C6.13		458.23 452.75 Prop C5.48
21+45.72 (END EXIST. C&B LT. Beg. NOW C&B W.S RT.)	chk = 458.45 (Meet EXIST.) 458.67			457.97 458.21 Fo.24	458.22 458.21 Grade 458.15 458.2 = TPCP Fo.05
21+43 = W.S RT.					
21+21.59	458.57	458.57		457.83 458.11 Fo.28	458.11

STA.	P.L	C.B.	℄	C.B.	P.L
25+00 = B.V.C.	460.64 460.14 C0.50	459.92 460.14 Fo.22		459.38 459.61 Fo.23	460.18 459.61 C0.57
24+95 = Sew LAT #27 LT.	460.70 452.24 prop C8.36		460.70 451.64 C9.06		
24+90 = W.S LT.	460.77 460.10 = To C.B. C0.67				
24+75	460.02	459.70 460.02 Fo.32		459.39 459.54 Fo.15	459.54
24+50	460.74 459.90 C0.84	459.45 459.90 Fo.45		459.30 459.47 Fo.17	460.50 459.47 C1.03
24+25	459.78	459.65 459.78 Fo.13		459.18 459.40 Fo.22	459.40
24+16.54 = E.C. Seminole	460.22 459.74 C0.48	459.66 459.74 Fo.08		459.21 459.37 Fo.16	460.19 459.37 C0.82
24+11.09	459.72	459.74 459.72 C0.02		459.02 459.35 Fo.33	459.35
23+86.97	459.82 459.63 C0.19	459.54 459.60 Fo.06		459.22 459.25 Fo.03	460.48 459.25 C1.23
23+62.84	459.52	459.51 459.49 C0.02		459.17 459.14 C0.03	459.14

STA.	P.L	C.B.	℄
27+15 = C.B. B.C. R.T. (SE'LY Filipo)	459.80 458.70 C1.10	458.38 458.70 Fo.32	
27+00	458.83	458.61 458.83 Fo.22	
26+75	459.06	458.75 459.06 Fo.31	
26+50	460.60 459.28 C1.32	459.22 459.28 Fo.06	
26+25	459.51	459.31 459.51 Fo.20	
26+00	460.77 459.73 C1.04	459.46 459.73 Fo.27	
25+80 = E.V.C.	460.59 459.91 C0.68	459.53 459.91 Fo.38	
25+60	460.08	460.28 460.08 C0.20	
25+40	460.60 460.16 C0.44	460.03 460.16 Fo.13	
25+20	460.18	459.95 460.18 Fo.23	

℄		
	457.63 457.88 Fo.25	457.96 457.88 C0.08
	457.53 458.06 Fo.53	458.06
	458.21 458.35 Fo.14	458.35
	458.50 458.63 Fo.13	459.83 458.63 C1.20
	458.77 458.92 Fo.15	458.92
	458.99 459.20 Fo.21	460.00 459.20 C0.80
	459.26 459.43 Fo.17	460.10 459.43 C0.67
	459.22 459.58 Fo.36	459.58
	459.27 459.66 Fo.39	460.29 459.66 C0.63
	459.16 459.67 Fo.51	459.67

Seminole (Cont.)

STA	P.L	CB	E	CB	P.L
27+50 Lt. only	458.18	458.00 458.18 Fo.18			
27+25 Lt. only	458.55	458 33 458.55 Fo, 22			
#7 = EC on Filipo				456.24	EXIST
#6				456 28 456.30 Fo.02	
#5				456 45 456.40 Co.05	
#4				456 48 456.60 Fo.12	
#3				455.75 456.90 Fo.15	
#2				45664 457.25 Fo.61	
#1				457.06 457.60 Fo.54	

STA.	P.L	CB	E	CB	P.L
#3 = EC on Carson	EXIST.	CHK 457.61 457.62			
#2		457 68 457.45 Co.23			
#1		457 86 457.50 Co, 36			
27+84.85 = CB Bc Lt. (SW'ly)	458 14 457.65 Co.49	457.25 457.65 Fo,40			
27+75 Lt. only	457.79	457.65 457.79 Fo,14			

ACORN - E'ly of Seminole

STA.	(N'ly) LT P.L	CB	℄	RT CB	RT P.L
1+52 = W.S.LT.	464.45 461.20 TP CB C3.25				
	461.28	461.28		461.38	
1+50	461.20	461.20		461.20	461.20
	C0.08	C0.08		C0.18	
	464.60	461.57		461.67	465.20
1+25	461.71	461.71		461.71	461.71
	C2.89	F0.14		F0.04	C3.49
		462.04		462.30	
1+00	462.22	462.22		462.22	462.22
		F0.18		C0.08	
	465.46	462.82		462.42	464.78
0+75	462.73	462.73		462.73	462.73
	C1.73	C0.09		F0.31	C2.05
	465.53				
0+72.26 = W.S.LT.	462.70 TP CB C2.83				
	465.54	463.16		463.19	
0+50	463.24	463.24		463.24	463.24
	C2.30	F0.08		F0.05	
		463.45		463.32	465.25
0+40	463.44	463.44		463.44	463.44
		C0.01		F0.12	C1.81
					465.30
0+20 = CB.EC	463.74	463.74		463.74	463.74
(For Ref's See Pg 15&16)					C1.56
(0+00 = E.LINE Seminole)					
B.M (See Pg 9)					

STA.	P.L	CB	℄	CB	P.L
3+00				458.06 458.20	457.30 458.21
				F0.14	F0.91
2+80 = W.S.RT.				458.50	453.10 458.50 = TP CB F5.40
2+75				459.41 458.71 F0.30	458.71
2+60.07 (OPP. CB BC LT.)	459.01			458.98 459.01 F0.03	459.98 459.01 F5.03
2+35				459.60 459.50 C0.10	459.50
2+20 = W.S.RT					459.2 459.70 = TP CB F0.5
2+10				460.23 460.00 C0.23	460.00 460.00 grade
1+85 (CB CONST. ON RT. ONLY HERE-ON)				461.11 460.50 C0.61	460.50
END CB CT. (MEET) 1+72.26 = EXIST. CB CT. & EXIST. PROP. N'ly ½ ST.	460.76			461.21 460.76 C0.45	463.46 460.76 C2.70
1+67.26 = W.S. RT.					464.36 460.8 TP CB C3.56

ACORN-E4- (CONT.)

STA.	P.L	CB	℄	CB	P.L
5+00				454.45 454.25 C0.20	454.25
4+75				454.95 454.74 C0.21	459.93 454.74 C5.19
4+50				44529 455.25 C0.04	455.25
4+30 =grd BRK 4 SUB. LINE	455.62			455.98 455.62 C0.36	457.39 455.62 C1.77
4+25				456.04 455.72 C0.32	455.72
4+00				456.32 456.22 C0.10	459.49 456.22 C3.27
3+75				456.81 456.72 C0.09	456.72
3+50.07 (OPP. CB BC LT.)	457.22			457.07 457.22 F0.15	456.92 457.22 F0.30
3+40= W.S.RT					456.5 457.40=TP CB. F0.9
3+25				457.63 457.71 F0.08	457.71

STA	P.L	CB	℄	CB	P.L
(At end RT. CB. CUT-OFF WALL) 6+27.78 =END CONST.				451.53 451.33 C0.20	452.47 451.33 C1.14
6+15				451.60 451.64 F0.04	451.64
6+00.81 (OPP. CB BC. LT.)	chk: 452.04 452.02			452.05 452.02 C0.03	452.42 452.02 C0.40
5+75				452.84 452.62 C0.22	452.62
5+55.74 o.k.				453.07 453.10 F0.03	450.35 453.10 F2.75
5+30				453.84 453.64 C0.20	453.64
5+10.81 (OPP. CB BC LT.)	454.06			454.22 454.06 C0.16	454.63 454.06 C0.57

ACORN – W/L of Seminole

to 62'nd

STA	LT P.L	LT CB	E	RT (N'LY) CB	RT (N'LY) P.L
1+48 = W.S. RT					466.16 465.20=TP CB C0.96
1+25	465.67 465.13 C0.54	465.16 465.13 C0.03		464.81 465.14 F0.33	465.73 465.14 C0.59
1+00	465.03	465.01 465.03 F0.02		464.76 465.04 F0.28	465.04
0+75	465.83 464.94 C0.89	464.84 464.94 F0.10		464.56 464.94 F0.38	466.18 464.94 C1.24
0+60	464.88	464.66 464.88 F0.22		464.61 464.88 F0.27	464.88
0+47 = CB EC LT 0+32, RT only	465.78 464.83 C0.95	464.83		464.51 464.83 F0.32 464.47 ~~464.78~~ F0.31	466.37 464.83 C1.54 ~~464.78~~
0+17 = CB EC RT (For Ret's see Pg 15+16)				464.72	466.12 464.72 C1.40
(0+00 = W. Line Seminole)					

BM (See Pg 9)

Ref: F.B 2344-38

STA	P.L	CB	E	CB	P.L
2+50 LT. only	465.60	465.44 465.60 F0.16			
2+25 LT. only	465.41 465.51 F0.10	465.30 465.51 F0.21			
#4 = E.C ON 63'nd				465.37 465.88 F0.51	465.88
#3				465.12 465.79 F0.67	465.79
#2				465.02 465.70 F0.68	465.70
#1				464.93 465.61 F0.68	465.61
(map) 2+23.76 = CB BC RT N'ELY RT. only				464.86 465.52 F0.66	465.54 465.52 C0.02
2+00	465.41	465.36 465.47 F0.05		465.02 465.43 F0.41	465.43
1+75	465.41 465.32 C0.09	465.28 465.32 F0.04		464.95 465.34 F0.39	465.78 465.34 C0.44
1+50	465.22	465.15 465.22 F0.07		464.97 465.24 F0.27	465.24

ACORN – N'Ly (Cont.)

STA	P.L	CB	℄	CB	P.L
3+79.76	466.09	466.06 466.09 Fo.03		455.80 466.09 Fo.29	466.09
3+59.76 = B.V.C.	465.73 466.04 Fo.31	466.11 466.04 Co.07		465.64 466.04 Fo.40	466.09 466.04 Co.05
3+39.76	465.96	465.95 465.96 Fo.01		465.71 465.97 Fo.26	465.97
#4 – E.C. on 63' rd				465.58 466.00 Fo.42	466.00
#3 Line only				465.34 465.92 Fo.58	
#2				465.38 465.85 Fo.47	465.85
#1 Line only				465.45 465.87 Fo.42	
3+19.76 = CB BC. RT NW'Ly	465.57 465.87 Fo.30	465.33 465.87 Fo.54		465.32 465.89 Fo.57	465.93 465.89 Co.04
3+00 LT only	465.79	465.52 465.79 Fo.27			
2+75 LT only	465.49 465.70 Fo.21	465.39 465.70 Fo.31			

STA	P.L	CB	℄	CB	P.L
5+25	465.57	465.52 465.57 Fo.05			
5+00	466.82 465.69 C1.13	465.70 465.69 Co.01			
4+75	465.82	465.91 465.82 Co.09			
4+50	466.71 465.95 Co.76	466.12 465.95 Co.17			
4+39.76 = E.V.C	466.70 466.00 Co.70	466.15 466.00 Co.15			
4+19.76 (Cont. CB Lt. only =)	466.08	466.07 466.08 Fo.01			
(4½ PAV. ST (End CB RT.)					
3+99.76 = E. Line Alley Prop. RT.	466.18 T.P. 466.11 Co.07	466.02 466.11 Fo.09		466.55 466.31 Co.24	466.44 Rod 466.31 grade Co.13
(3+99.76) Alley E.C. RT.				466.19 466.19 Grade	466.19
3+95.76 = Alley B.C. RT. (4' CB Rad.) RT. only				466.12 466.11 Co.01	466.11

ACORN - W'LY (CONT.)

STA	P.L	CB	℄	CB	P.L
7+75	464.30	464.22 464.30 F0.08			
7+50	465 71' 464.43 C1.28	464 39 464.43 F0.04			
7+25	464.56	464 51 464.56 F0.05			
7+00	466 22 464.68 C1.54	464.69 464.68 C0.01			
6+75	464.81	464.97 464.81 C0.16			
6+50	466 59 464.94 C1.65	465.05 464.94 C0.11			
6+25	465.06	465 16 465.06 C0.10			
6+00	466 44 465.19 C1.25	465 23 465.19 C0.04			
5+75	465.31	465.35 465.31 C0.04			
5+50	466 59 465.44 C1.15	465 36 465.44 F0.08			

STA	P.L	CB	℄	CB	P.L
(per plan) end CB					
#2 =	464.90 463.82 C1.08	463.70 463.82 F0.12			
#1	463.87	463 90 463.87 C0.03			
8+36.23 = CB, BC, LT. SW'LY	464 93 463.98 C0.95	464 03 463.98 C0.05			
8+25	464.05	464.12 464.05 C0.07			
8+00	465.53 464.18 C1.35	464 06 464.18 F0.12			

Note: DATA IN F.B 2344 - 38 USED IN SETTING CB BC AT SE'LY R.T.Y. OPENING SHEET 8-83 (NOTTIES SHOWN ON PLANS!)

63rd ST. N'ly of ACORN

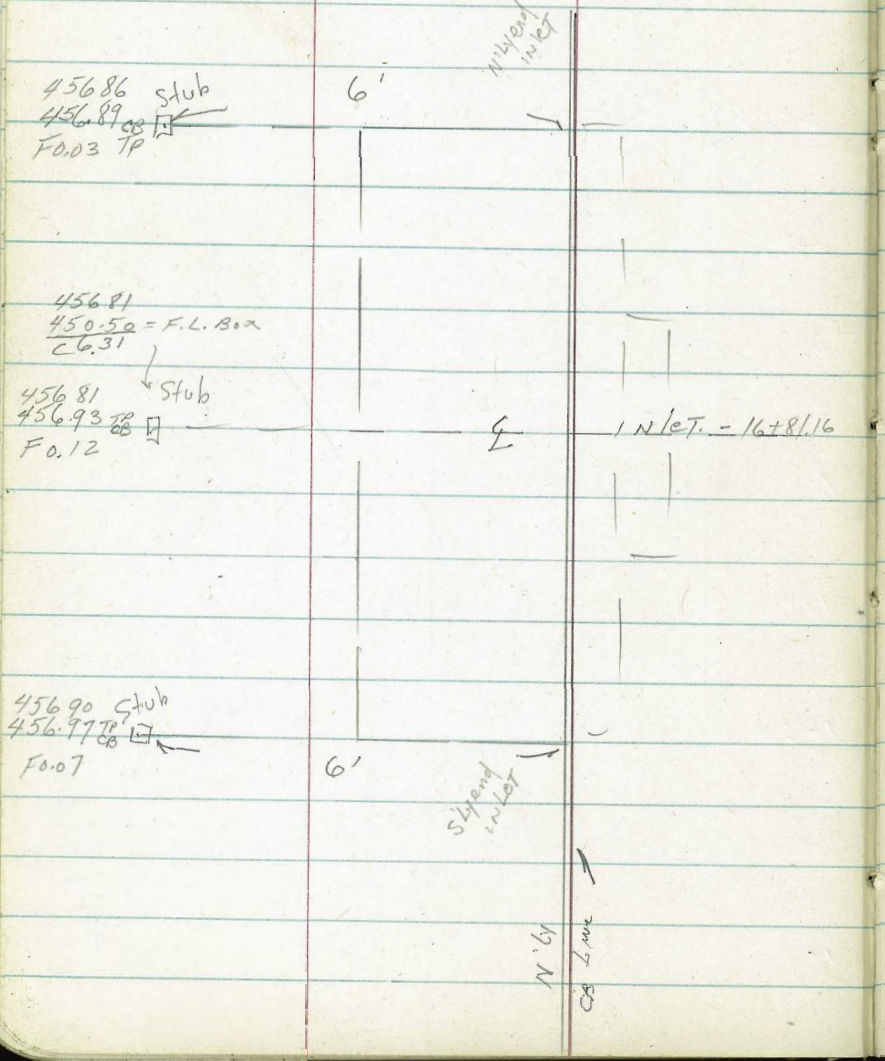
STA	P.L	CB	℄	CB	P.L
1+25	466.26	465.81 466.26 Fo.45		465.81 466.26 Fo.45	466.26
1+00	465.68 466.20 Fo.52	465.77 466.20 Fo.43		465.75 466.20 Fo.43	465.47 466.20 Fo.73
0+80=N.S RT.					465.77 466.15=CB Fo.38
0+77= W.S. LT	466.00 466.14=CB Fo.14				
0+75	466.14	465.95 466.14 Fo.19		465.81 466.14 Fo.33	466.14
0+50	466.08	465.80 466.08 Fo.28		465.73 466.08 Fo.35	466.08
0+40	465.90 466.05 Fo.15	465.73 466.05 Fo.32		465.54 466.05 Fo.51	465.84 466.05 Fo.21
0+20=CB EC'S: (For POT'S See Pg 26+27)	466.11 466.00 Co.11	466.00		465.88	465.76 465.88 Fo.12
0+00=N'ly Line ACORN)					

STA	P.L	CB	℄	CB	P.L
2+21.4 =End Const.	465.40 466.50 Fo.10	465.61 466.50 Fo.89		465.96 466.50 Fo.54	465.88 466.50 Fo.62
2+00	465.67 466.44 Fo.77	465.81 466.44 Fo.63		466.07 466.44 Fo.37	465.57 466.44 Fo.87
1+86.4= W.S.RT.				~~466.41~~	466.05 466.41=CB Fo.36
1+83.4= W.S.LT	465.75 466.40=CB Fo.65	~~466.40~~			
1+75	466.38	465.90 466.38 Fo.48		465.99 466.38 Fo.39	466.38
1+50	465.56 466.32 Fo.76	465.80 466.32 Fo.52		465.89 466.32 F 0.43	465.76 466.32 Fo.56
1+34.4= W.S.RT.				~~466.28~~	465.88 466.28=CB Fo.40
1+31.4= W.S.LT.	465.75 466.28=CB Fo.53	466.28			

CB INLETS Seminole & ART
TYPE A-2

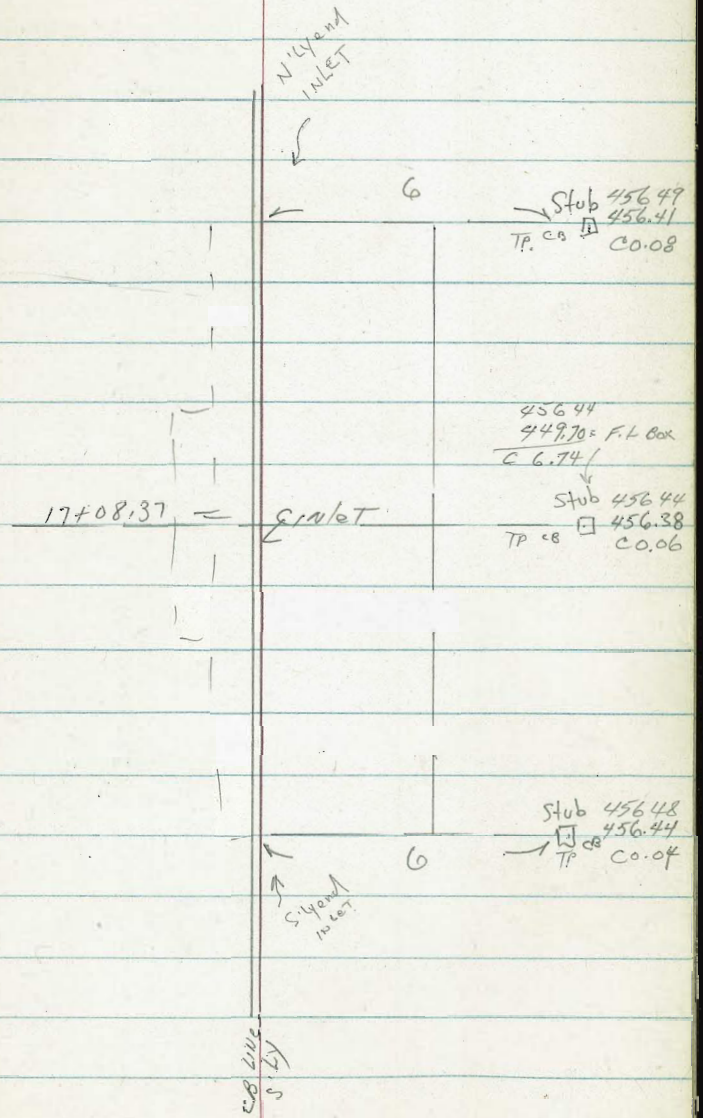
1 N'ly CB Line Seminole

℄ Sta = 16+81.16 (on LT)



2 Type A-2

℄ STA = 17+08.37



Garber
O'Niel
Abrenilla

Stake Alley Blk 61 Park Villa
Bdry. - Felton - Upas & Myrtle

W.O. 32456
10-3-56

	Lt		Rt	
+40	(313.83)	313.49 313.52 F-0.03	(314.13)	313.90 313.83 C-0.07
+20	(313.00)	313.48 312.74 C-0.74	(313.30)	313.42 313.05 C-0.37
1+00	(312.00)	313.05 311.78 C-1.27	(312.30)	312.48 312.11 C-0.37
+75	(310.76)	311.50 310.59 C-0.91	(311.05)	310.99 310.93 C-0.06
+50	(309.51)	310.26 309.41 C-0.85	(309.80)	310.43 309.75 C-0.68
+30	(308.51)	308.84 308.45 C-0.39		309.34 308.80 C-0.54
+20	(308.02)	308.62 307.97 C-0.65		308.78 308.18 C-0.60
+10 BVC Rt				308.57 307.46 C-1.11
0+00	307.05 307.02 Gutter C-0.03		306.65 306.63 C-0.02	
			312.35 NWBP Upas & Felton	

	Lt.	Rt.
Note - Grade change by Gabrielson. Original grades shown in parenthesis. ( )		
3+00.20 Exist Cb	315.28 315.30 F-0.02	Existing 315.34 315.36 F-0.02
+90	315.92 315.55 C-0.37	316.12 315.85 C-0.27
+70	315.79 315.81 F-0.02	316.22 316.11 C-0.11
+50	315.21 315.69 F-0.48	(? 316.07 315.99 C-0.08
+25	(315.30) 315.06 315.25 F-0.19	(315.60) 315.57 315.54 C-0.03
2+00	(314.92) 314.76 314.79 F-0.03	(315.22) 315.40 315.08 C-0.32
+75	(314.54) 314.58 314.34 C-0.24	(314.84) 314.78 314.63 C-0.15
1+60	(314.31) 314.13 314.06 C-0.07	(314.61) 314.41 314.36 C-0.05

CLARK
GARBER
O'NEIL
ABRENILLA

STORM DRAIN - MARKET - Columbia to STATE

Ref: City Eng's. Notes: File G-21
DWG: 3601-D, 3602-D

1+40
7.16
2.02
C5.14

1+05
7.19
1.72
C5.47

0+70
6.61
1.42
C5.19

0+35
6.10
1.13
4.97
0.85-9

0+06 = ℄ 4' Type "K-1" Inlet #1
5.64
0.88 = F.L. E'ly Pipe
4.76

5.64
0.38 = F.L. W'ly Pipe & F.L. Box
5.26

0+00 = E. Line Columbia
(Stubs 5' Lt. ℄)

B.M.: Div. Elev. Walk
4.91 = S.W.B.P. Market & Columbia

Inlet #3 4' Type "K-1"
9.14
6.00 = F.L. Box
C3.14

2+84 = ℄ Inlet #2 - 7' "K-1"
9.17
4.50 = F.L. Box
C4.67

9.11
5.50 = F.L. N'ly Pipe
C3.61

9.11
4.00 = F.L. Pipe E'ly
C5.11

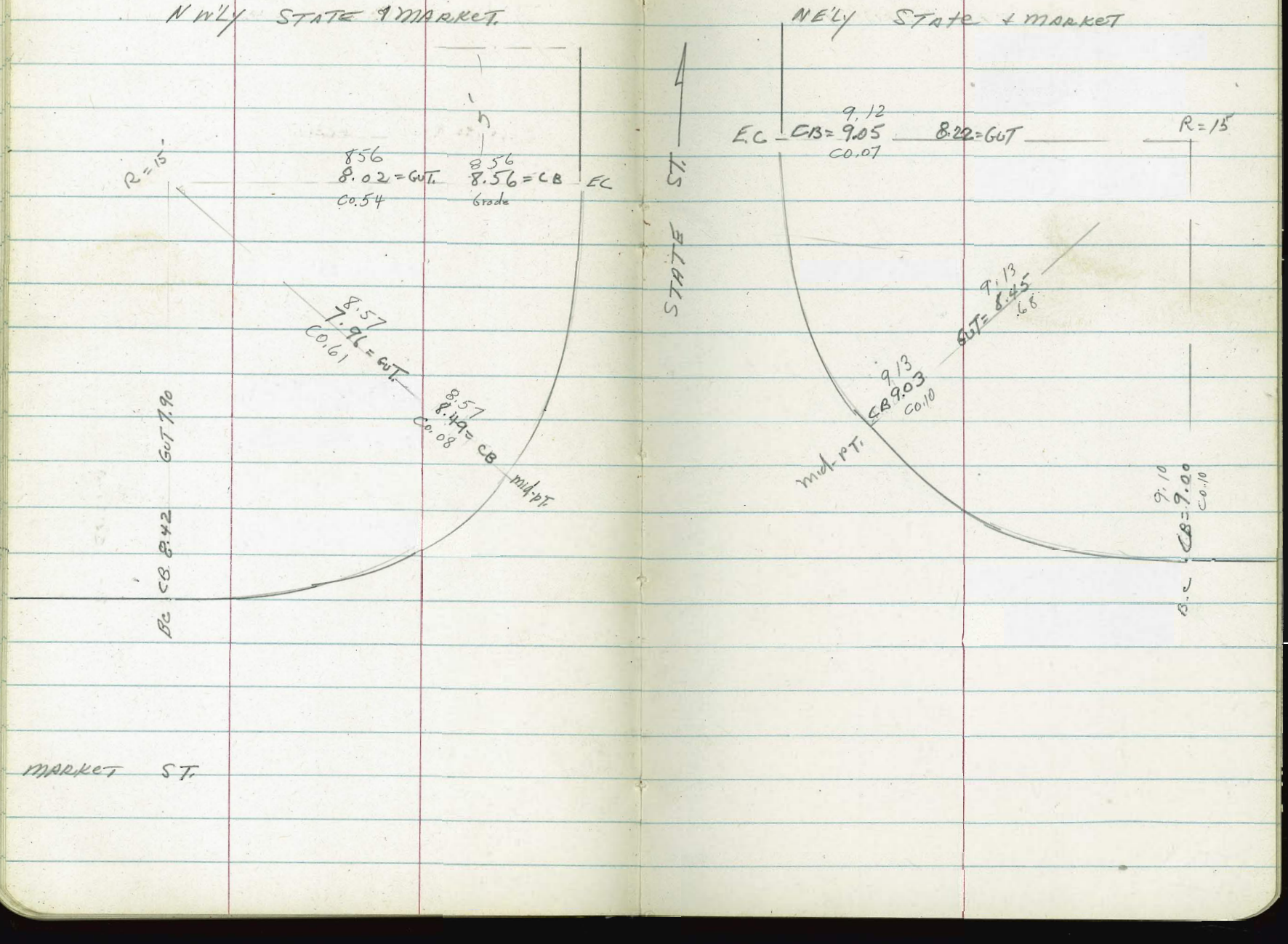
2+61 = ℄ Type "G" Cleanout = 4 Lt 90° For 15.5' 18' pipe
9.11
3.05 = F.L. Box
C6.06

2+45
8.90
2.92
C5.98

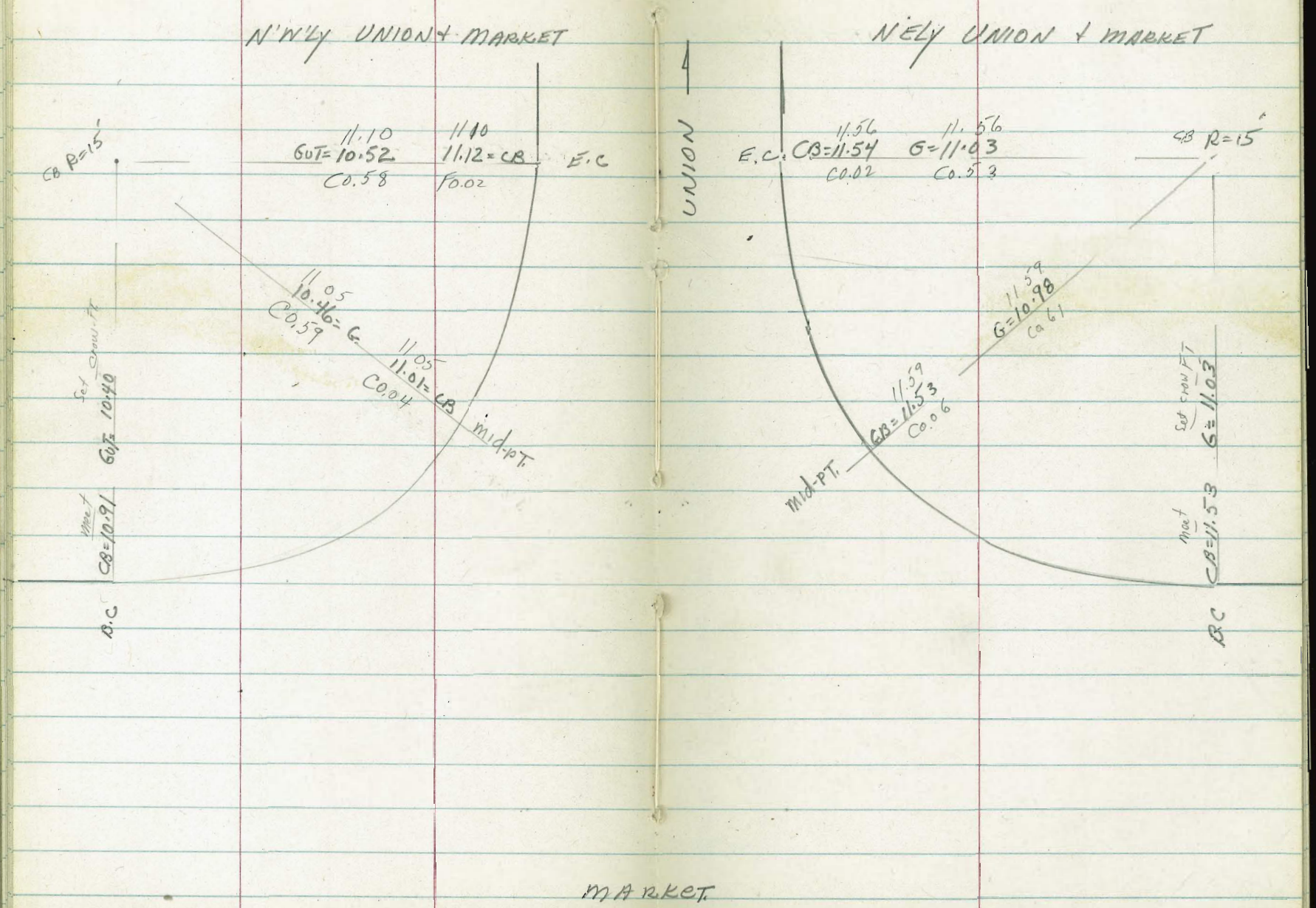
2+10
8.50
2.62
C5.88

1+75
7.73
2.32
C5.41

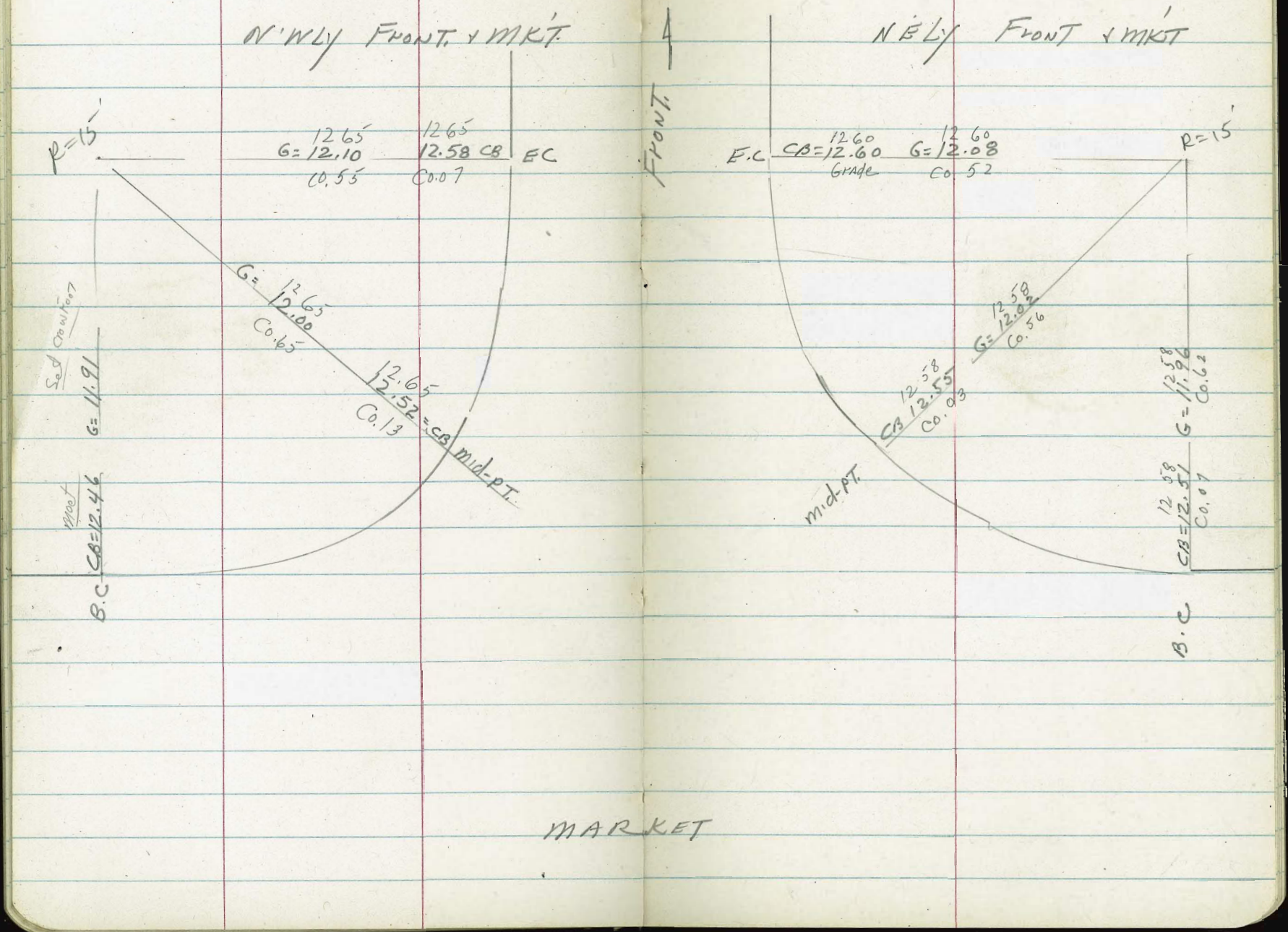
C.B. Returns (Mkt St. Drain) cont.



CB Ret's (Market St. Drain Cont.)



CB Ret's (Market St. Drain (Cont.)



Garber
O'Niel
Abrenilla
Talamantez

11-13-56

Storm Drain - Island 27th to 28th

W.O. 21190

Ref:- Field Bk. 2237-P 54
Drwg. 12707-L

		+75	110.07 97.76 C-12.31 1X1
2+00	102.58 93.80 C-8.78 1X1		
		+50	107.48 97.04 C-10.44 1X1
+75	102.01 93.68 C-8.33 1X1		
		+25	105.48 96.32 C-9.16 1X1
+50	101.43 93.55 C-7.88 X on Walk		
		Clean-out, Gr. Brk +16.16	104.76 96.05 C-8.71 1X1
+25	100.97 93.43 C-7.54 X on Walk		
		3+00	104.19 95.74 C-8.45 1X1
1+00	100.41 93.30 C-7.11 1X1		
		+75	103.89 95.24 C-8.65 1X1
+75	99.98 93.18 C-6.80 1X1		
		+50	104.21 94.74 C-9.47 1X1
+50	99.67 93.05 C-6.62 X on Walk		
		+25	103.52 94.24 C-9.28 1X1
+25	99.33 92.93 C-6.40 X on Walk		
		Gr. Brk 2+04.05	102.64 93.82 C-8.82 1X1
0+00 =Sta. 5+54.05 Drwg. No. 12707-L	98.77 92.80 C-5.97 Nail in st.		
Note - All points 6' Rt		98.06 SWBP 28th & Island	

End of Work +54.05	102.91 - Existing Pipe
+36.05	108.89 102.39 C-6.50 1X1
E.C. 5+18.05	109.01 101.87 C-7.14 1X1
M.d. Pt. +94.22	110.77 101.18 C-9.59 1X1
B.C +70.40	114.57 100.50 C-14.07 1X1
E.C +54.99	117.53 100.06 C-17.47 1X1
M.d. Pt. +42.75	117.15 99.71 C-17.44 1X1
B.C. +30.51	116.12 99.36 C-16.76 1X1
4+00	112.85 98.48 C-14.37 1X1

CLARK
GARBER
O'NEIL
ABRENILLA
3-20-57
21303

Chocolate Canyon Sewer
(Pennell to Nutmeg

Ref: DWGS: 3870-D & 3871-D
Field Notes I-20 & I-21 (C.H.S.)

STA.		Elev's	STA	Elev's:	
			4+89.42	87.03 79.14 C 7.89	
2+10		80.79 73.17 C7.62			
			4+54.42	85.95 78.27 C7.68	
1+75		79.60 72.75 C6.85			
			4+19.42	84.97 77.42 C7.35	
1+40		78.06 72.33 C5.73			
			3+84.42	83.45 76.56 C6.89	
1+05	1.2%	76.41 71.91 C4.50	2.4% TG		
			3+49.42	82.55 75.71 C6.84	
0+70		75.58 71.49 C4.09			
			3+14.42	81.80 74.85 C6.95	
0+35	(Stubs 5' RT)	76.29 71.07 C5.22			
			(Abandon Exist. M.H 1-X) 2+79.42 = M.H #1 Δ = 69° 37' RT	83.20 77.00 C 9.20	83.2 83.0 = TP C0.20
0+00 = EXIST M.H. Pennell ST		79.30 70.65 C 8.65			
Chk: Rim M.H 0+00 =	79.30		2+45	81.47 73.59 C7.88	
B.M Dir. Elev. Rod:		80.86 = 2" Pipe W/4 18' Line 35 4L 4ASH			

STA:	Elev's:
7+57.26 (2.56 / 2.58)	94.07 85.78 C 8.29
7+22.26	92.42 84.89 C 7.53
(Abandon ∈ xist MH 3-x) & 2-x 6+87.26 = MH #2 ∠ LT.	93.55 83.99 FL C 9.56
6+64.42	90.63 83.43 C 7.20
6+29.42 (2.45-3)	89.71 82.57 C 7.14
5+94.42	89.08 81.71 C 7.37
5+59.42	88.39 80.85 C 7.54
5+24.42	87.80 80.00 C 7.80
10+14.19	100.34 92.46 C 7.88
9+79.19	99.08 91.55 C 7.53
9+44.19	97.84 90.63 C 7.21
9+09.19 (2.60-3 / 2.6 1-2)	96.28 89.72 C 6.56
8+74.19	95.58 88.81 C 6.77
8+39.19	95.91 87.89 C 8.02
(Abandon MH 4-x) 8+04.19 = MH #3 ∠ RT.	98.97 86.98 = FL C 11.99
7+92.26	96.02 86.68 C 9.34

98.97 tp
99.0a tp
3

STA.	Elev's:	
0+00 Whaley = (11+96.69 Canyon-Line = M.H #4)	104.71 97.71 = F.L C 7.00	
Note: Beg. Whaley St. Line (CONT. CANYON LINE Pg 40)		
CLK: 107.03 = RIM EXIST (5-X) = 107.00 (Abandon M.H 5-X)		
11+96.69 = M.H #4	104.71 97.24 F.L C 7.47	104.7 107.0 T.P. F 2.3
11+89.19	97.03	
11+54.19	103.20 96.12 C 7.08	
11+19.19	102.70 95.20 C 7.50	
(stubs 5' RT.)		
10+84.19	101.86 94.29 C 7.57	
10+49.19	101.11 93.37 C 7.74	

(Retain) WHALEY 2+37.25 = EXIST M.H	137.14	143.26 chk: 143.28 = Rim
2+85 = ℄ CUT-OFF WALL		
2+01.97	134.10 127.07 C 7.03	
1+66.70	124.97 117.00 C 7.97	
1+65 = ℄ CUT-OFF WALL		
1+41.70	119.65 111.33 C 8.32	
1+25 = ℄ CUT-OFF WALL		
1+16.70 = E.V.C	113.58 105.67 C 7.91	
1+04.20	110.50 103.14 C 7.36	
0+91.70	107.86 101.26 C 6.60	
0+90 ℄ CUT-OFF WALL		
0+79.20	106.73 100.00 C 6.73	
0+66.70 = B.V.C (Stubs 5' LT (0+00 to 2+37.25))	106.40 99.38 C 7.02	
0+33.35	105.40 98.55 C 6.85	

CONT. CANYON LINE

STA	Elevs	
L.RT.		
= M.H #5	112.7	112.68
14+23.89	115.0 = T.P. M.H	103.98 F. LINE
Stubs on split (5.03 RT)	F. 3.7	8.70
14+08.39		112.32
		103.51
		8.81
13+73.39		111.15
		102.47
		8.68
(30.0)		
13+38.39		109.47
		101.42
		8.05
13+03.39		108.28
		100.38
		7.90
12+68.39		106.82
		99.34
		7.48
12+33.39		105.41
		98.29
		7.12
= 11+98.39 — Ahead		
11+96.69 = M.H #4 } EQ. (See Pg. 39)		97.24 F.L.N.W.ly
(Note: CONTINUE CANYON LINE)		

STA.	Elev's:
17+38.89 (Not set)	111.93
17+03.89	120.26
	111.93
	C 8.33
16+68.89	119.22
	110.94
	C 8.28
16+33.89	118 42.
	109.94
	C 8.48
15+98.89	117.50
	108.95
	C 8.55
(28.45)	
15+63.89	116 41
	107.96
	C 8.45
15+28.89	115 59
	106.96
	C 8.63
14+93.89	114 57
	105.97
	C 8.60
14+58.89	113 90
	104.97
	C 8.93

CHOCOLATE CANYON (CONT.)

STA.	Elev's	
20+21.56	125 49 119.95 C 5.54	
19+86.56	125 00 119.09 C 5.91	
19+51.56	124 28 118.22 C 6.06	
19+16.56	123.87 117.35 C 6.52	
18+81.56	123.72 116.48 C 7.24	2.486 →
18+46.56	124 09 115.61 C 8.48	
18+11.56	124 15 114.75 C 9.40	
17+76.56	123 64 113.88 C 9.76	
17+41.56 = M.H #6 ∠ RT (stubs on split 5.05 RT)	121.9 124.0 Tp. M.H F 2.1	121.91 113.01 F.L. C 8.90

STA.	Elev's:		
22+89.65	135 74 127.07 C 8.67		
22+54.65 (2.986 ↑)	134 38 126.05 C 8.33		
22+19.65	132 31 125.02 C 7.29		
chis: 132.76 + F.M EXIST: = 132.73			
(ABANDON EXIST M.H 9-X) + CONNECT SEWER	130.7 132.0 = Tp M.H F 2.7	130.65 124.00 F. Line 6.65	
21+84.65 M.H. #7 ∠ RT (stubs on split 5.02)			
21+61.56	129 96 123.43 C 6.53		
21+26.56 (2.486 ↑)	128 62 122.56 C 6.06		
20+91.56	127.16 121.69 C 5.47		
20+56.56	126 36 120.82 C 5.54		

CHOCOLATE CANYON (CONT.)

STA.	Elev's:
26+04.65	144.00 136.30 C 7.70
25+69.65	142.67 135.27 C 7.40
25+34.65	141.29 134.25 C 7.04
24+99.65	140.84 133.22 C 7.62
2.936	
24+64.65	140.45 132.20 C 8.25
24+29.65	139.08 131.17 C 7.91
23+94.65	137.40 130.15 C 7.25
(ABANDON M.H. 10-X)	
23+59.65	136.35 129.12 C 7.23
23+24.65	135.84 128.10 C 7.74

(ABANDON EXIST M.H 11-X)

M.H #9
28+70.00
= P.O.T.
chk. on RIM EXIST 5.0' RT
STUB 10' RT (LINE ONLY)

153.6
153.6 = Tp M.H
grade

153.63
144.40 = FL.
C 9.23

28+36.42

15" / 50
143.39
C 8.11

28+01.42

150.28
142.32
C 7.96

27+66.42

30 x 66

148.82
141.26
C 7.56

27+31.42

146.93
140.19
C 6.74

26+96.42

145.77
139.13
C 6.64

26+61.42

145.10
138.06
C 7.04

chk: 147.76 = EXIST RIM = 147.72
(RETAIN EXIST M.H - CONNECT.)

EQ { 26+26.42 Ahead
26+28.33
= M.H #8
L.CT. (STUBS SET ON SPLIT 5.39' RT)

144.99
146.0 = Tp M.H
F 1.01

144.99
137.00 FL
7.99

CHOCOLATE CANYON - (CONT.)

STA	Elev's.		STA	Elev's.	
				168 53 159.81 C 8.72	
(CHK: 161.94 = 161.90 = RIM EXIST)			CHK = RIM EXIST = 167.79		
(ABANDON EXIST M.H 12-X)			(ABANDON EXIST M.H 13-X) (CONNECT EXIST 6" E'LY, W'LY Sewer)	167.8	167.80
31+55.50 = M.H. #10 L.RT (Stubs on split 8.14' R.T. (NAIL IN CONC. EXIST. M.H)	161.8 163.0 = Tp M.H F1.2	161.82 151.48 = F. LINE C 10.34	34+31.08 = M.H #11 L.RT Stubs on SPLIT 5.02' R.T. (NAIL CONC EXIST. M.H)	167.8 = Tp.M.H Grade	158.48 F.L C 9.32
31+15		159.50 150.48 C 9.02	34+00.5		166 12 157.70 C 8.42
30+80		158 23 149.61 C 8.62	33+65.5		165.37 156.81 C 8.56
30+45		156.83 148.74 C 8.09	33+30.5		164.36 155.93 C 8.43
30+10 (1" = 80', V: 1" = 8')		155.53 147.87 C 7.66	32+95.5 (1" = 80', V: 1" = 8')		162.53 155.04 C 8.49
29+75		154.91 147.0 C 7.91	32+60.5		162 36 154.15 C 8.21
29+40		154.75 146.14 C 8.61	32+25.5		161 74 153.26 C 8.48
29+05		154.31 145.27 C 9.04	31+90.50		161 65 152.37 C 9.28

CHOCOLATE CANYON - (CONT.)

STA	Elevs:
37+78	178.67 169.65 C 9.02
37+43	177.99 168.72 C 9.27
37+08	177.43 167.79 C 9.64
36+73	176.15 166.87 C 9.28
36+38	174.10 165.94 C 8.16
(ABANDON EXIST M.H 14-X) CONNECT TO EXIST 6" SEWER 36+03 = M.H #12 (STUBS 90° RT 5'+10')	172.2 174.5 = T/P M.H F 2.3 172.19 165.01 = F.L. C 7.18
35+71.08	171.52 163.80 C 7.72
35+36.08	171.47 162.47 C 9.00
35+01.08	170.08 161.14 C 8.94

2.6 SLOPE

3.8 SLOPE

STA	Elevs:
40+40 END CONC. ENCASE CHK: 197.81 = RIM EXIST. M.H. = 197.77 (RETAIN EXIST. M.H - CONNECT)	197.7 198.5 = T/P M.H F 0.8
40+18.07 = M.H #13 ∠ LT 18°19 (M.H MOVED S'LY 1.8 TO AVOID 6" SEWER) (STUBS ON SPLIT 5.07 RT)	197.72 176.01 F.L. C 21.71
39+99 = N'LY CB	204.33 175.48 C 28.85
39+82 APPROX ℄ PAVE(±)	204.40 175.03 C 29.37
39+68 ±FC S'LY CB CHK: 205.00 = X S'LY CB (ON ℄) = 204.96	205.14 174.66 C 30.48
39+53	199.11 174.29 C 24.82
39+18	190.96 173.36 C 17.60
38+83	187.30 172.43 C 14.87
38+75 Beg CONC. ENCASEMENT 38+48	182.93 171.50 C 11.43
38+13	180.08 170.58 C 9.50

2.6 SLOPE

CHOCOLATE CANYON - (CONT.)

STA:	Elev's:
43+33.07	202.97 192.39 C 10.58
42+98.07	201.07 190.57 C 10.50
42+63.07	198 50 188.77 C 9.73
42+28.07	196 11 186.96 C 9.15
41+93.07	194 66 185.15 C 9.51
41+58.07	193 04 183.34 C 9.70
41+23.07	192 10 181.53 C 10.57
40+88.07	191.44 179.72 C 11.72
40+53.07	190 82 177.91 C 12.91

S: 20.0 ↓

↓ 37

STA	Elev's
45+93.72	214.99 206.15 C 8.84
45+58.72	212 97 204.29 C 8.68
45+23.72	210 19 202.44 C 7.75
44+88.72	207 81 200.58 C 7.23
44+53.72	206 33 198.73 C 7.60
44+18.72	205 08 196.87 C 8.21

S: 3.96 ↑

Chk: (EXIST M.H HIT) = RIM EXIST M.H=202.60
(ABANDON EXIST M.H 16-X)

43+83.72
= M.H #14
L.LT (Set clr X 5.01 RT Rim EXIST.) (STUBS ON SPLIT) 5.01 RT

202.8
204.0 TP M.H
F 1.2

20276
195.02 FL
C 7.74

43+68.07

20394
19720
C 9.74

CHOCOLATE CANYON (CONT.)

47+92.00 = EXIST M.H (RETAIN)
22554
214.35
C11.19

47+82.44
22510
214.12
C10.98

47+47.44
245'
22415
213.28
C10.87

(ABANDON EXIST M.H #17X)

47+12.44 = M.H #15
(2 @ STUBS 5.13' & 10.26 RT)
Tp = 222.09 222. Grade
222.09
212.44 F.L.
C9.65

46+98.72
220.47
211.71
C8.76

46+63.72
217.76
209.86
C7.90

46+28.72
216.53
208.00
C8.53

(RETAIN EXIST M.H & CONNECT)

50+79.90 = M.H #16
(STUBS SET 5.72' & 11.44' RT)
SET CHX 5.72' RT ON RIM
232.6 = Tp. Grade
232.81
220.97 F.L.
C11.84

50+72
231.72
220.79
C10.93

50+37
230.08
219.98
C10.10

50+02
228.49
219.18
C9.31

49+67
227.61
218.37
C9.24

233'

49+32
226.91
217.57
C9.34

48+97
226.04
216.76
C9.28

48+62
225.42
215.96
C9.46

48+27
225.66
215.15
C10.51

Chocolate Canyon (Cont.)

		261 88 247.93 C 13.95
53+51.61		
		259 48 246.28 C 13.20
53+16.61		
53+10 Beg Conc. Cradle		
		256 69 244.63 C 12.06
52+81.61		
	=253.43= Rim Exist M.H	
(Abandon Exist M.H #18-X) (Connect 6" Sewer)		
52+46.61 = M.H #17 Stubs Set 7.35' RT	252.5 254.0 = TP F 2.5	252.45 242.98 = F.L C 9.47
		243 39 236.97 C 6.42
52+13.25		
51+79.90 = grd Brk		238 24 230.97 C 7.27
		234 49 227.63 C 6.86
51+46.56		
		232 57 224.30 C 8.27
51+13.23		

Intx	288.49 =	288.45 = SE Disc Nutmeg Teresita
(Connect.)		
55+58.20 = Exist M.H.		257.69 (Meas)
		268 39 256.13 C 12.26
55+26.61		
		267 09 254.51 C 12.58
54+91.61		
54+60 End Conc. Cradle		
		266 45 252.86 C 13.59
54+56.61		
		265 27 251.22 C 14.05
54+21.61		
		263 81 249.58 C 14.23
53+86.61		

CLARK
GARBER
ONEIL
ABRENILLA
T-9-57
W.O. 32183

Imp's Santa Margarita 5542 to San Jacinto

Ref: F.B 1712 & 2295
T.P.S & Sub-maps
Dwgs: 3975-D & 3976-D

STA	Prop	CB	℄	CB	Prop
~~#~~ 2 = End CB.				168 74 168.23 Co. 51	168.23
# 1				168 43 168.32 Co. 11	168.32
0+28.72 = C.B.B.C RT (N.W.ReT.	168.92	169 06 168.92 Co.14		168 41 168.31 Co.10	168 66 168.31 Co. 35
0+25					
0+18.88 = NW Corn					
0+05.10 = SE Corn (Tp CO)	169 98 169.11 Co.87	169.34 169.11 Co.23			
0+00 = ℄ Santa Margarita y E, Line Las Altoras					
0-07.10 = NE Corn (PAY. only)					168 28. 168.05 Co.23
B.M. (Dir. Elev. R.D.)				189.45 - ECHT	

STA	Prop	CB	℄	CB	Prop
1451.5 = W.S LT.	1689 167.8 tpCB C1.1				
1450	168 73 167.81 Co.92	167.95 167.81 Co.14		167.23 167.20 Co.03	166 57 167.20 Fo.63
1425	168.04	168.21 168.04 Co.17		167.35 167.43 Fo.08	167.43
1416.7 = W.S.RT					167 38 167.5 tpCB Fo.12
1400	169 20 168.27 Co.93	168 34 168.27 Co.07		167.40 167.66 Fo. 26	167 34 167.66 Fo.32
0+97.5 = W.S LT.	1697 168.3 tpCB C1.4				
0+75	168.50	168 48 168.50 Fo.02		167.94 167.89 Co.05	167.89
0+50	169 88 168.73 C1.15	168 75 168.73 Co.02		168 26 168.12 Co.14	168 42 168.12 Co.30
0+44.5 = W.S. LT	170.29 168.7 C1.58				
℄ Church Ward ℄E-Tang of San Jacinto					

STA	prop	CB	E	CB	Prop
3+25	166.21	165.96 166.21 Fo.25		164.26 165.60 Fo.34	165.60
3+00	16726 166.44 Co,82	166.08 166.44 Fo.36		16555 165.83 Fo.28	165.76 ~~166.77~~ ? 165.83 ~~Co.94~~ Fo.07
2+75	166.67	16637 166.67 Fo.33		16582 166.05 Fo.23	166.05
2+50	16761 166.90 Co.71	16647 166.90 Fo.43		16601 166.28 Fo.27	166.27 166.28 Fo.01
2+25	167.13	16676 167.13 Fo.37		16623 166.51 Fo.28	166.51
2+00	16832 167.36 Co.96	167.04 167.36 Fo.32		16646 166.74 Fo.28	16635 166.74 Fo.39
1+75	167.59	167.40 167.59 Fo.19		16694 166.97 Fo.03	166.97
166.7=Sew LAT 12 RT.			166.43 160.2 E C6.23		16643 162.0 P.L C4.43
156.7=WS RT					1666 167.1 tp CB Fo.5

STA	Prop	CB	E	CB	Prop
	1678		1678		
5+12=Sew LAT 7 LT	159.6 P.L C8.2		157.8 E C1.0		
5+02=WS LT	1679 164.6 tp CB C3.3				
5+00	167 04 164.61 C2.43	16479 164.61 Co.18		164.08 163.99 Co.09	164 63 163.99 Co.64
4+75	164.84	164.80 164.84 Fo.04		164.14 164.22 Fo.08	164.22
4+50	166.95 165.07 C1.88	164.95 165.07 Fo.12		164.37 164.45 Fo.08	164 71 164.45 Co.26
4+25	165.30	165.12 165.30 Fo.18		16438 164.68 Fo.30	164.68
4+00	166.50 165.52 Co.98	16505 165.52 Fo.47		164.51 164.91 Fo.40	165.00 164.91 Co.09
3+75	165.75	165.51 165.75 Fo.24		16468 165.14 Fo.46	165.14
3+50	167 02 165.98 C1.04	16565 165.98 Fo.33		164.90 165.37 Fo.47	164 97 165.37 Fo.40

STA	Prop	CB	℄	CB	Prop
6+36.93 LT ONLY	163.61	16335 163.61 Fo.26			
6+16.93 LT ONLY	163.66	163.29 163.66 Fo.37			
5+96.93 grd Bik LT only (=E.L. 54'th Proj.)	165.10 163.71 C1.39	16366 163.71 Fo.05			
#2				16269 163.00 Fo.31	163.00
#1				163.11 163.09 Co.02	163.09
5+88.93= CB BC R.T. only NE ReT 54'h				16324 163.18 Co.06	16372 163.18 Co.54
5+75	163.92	16404 163.92 Co.12		163.35 163.31 Co.04	163.31
5+50	16621 164.15 2.06	16417 164.15 Co.02		16353 163.54 Fo.01	16426 163.54 Co.72
5+25	164.38	16430 164.38 Fo.08		163.74 163.76 Fo.02	163.76

STA	Prop	CB	℄	CB	Prop
7+75	162.70	162.90 162.70 Co.20		16212 162.10 Co.02	162.10
7+50	164.45 162.88 C1.57	16285 162.88 Fo.03		16227 162.28 Fo.01	16277 162.28 Co.49
7+25	163.07	163.17 163.07 Co.10		16246 162.46 Grade	162.46
7+00	165.96 163.25 C2.71	163.22 163.25 Fo.03		16261 162.65 Fo.04	16373 162.65 C1.08
6+75	163.43	163.22 163.43 Fo.21		16286 162.83 Co.03	162.83
#2 End CB				162.96 162.94 Co.02	162.94
#1				16287 162.93 Fo.06	162.93
6+64.93=CB BC RT. only N.W. ReT.				162.87 162.90 Fo.03	16317 162.90 0.27
6+56.93=grd Bik LT. only (=W.L. 54'th Proj.)	164.53 163.56 Co.97	163.37 163.56 Fo.19			

STA	Prop	CB	℄	CB	Prop
	161.66	161.50		160.77	160.61
9+50	161.43	161.43		160.82	160.82
	Co. 23	Co.07		Fo.05	Fo. 21
		161.55		161.03	
9+25	161.61	161.61		161.00	161.00
		Fo.06		Co.03	
	162.42	161.89		160.80	161.05
9+00	161.79	161.79		161.18	161.18
	Co 63	Co.10		Fo.38	Fo.13
		161.97		160.95	
8+75	161.97	161.97		161.37	161.37
		Grade		Fo.42	
	163.02	162.05		161.39	161.38
8+50	162.16	162.16		161.55	161.55
	Co.86	Fo.11		Fo.16	Fo.17
8+36.9=Sew. LAT #11 RT			161.5 156.7 ℄ C4.8		161.5 157.5 P.L C4.0
8+26.9= W.S. RT					161.6 161.7 tp cb Fo.1
		162.28		161.56	
8+25	162.34	162.34		161.73	161.73
		Fo.06		Fo.17	
	163.77	162.64		161.66	162.33
8+00	162.52	162.52		161.92	161.92
	C1.25	Co. 12		Fo. 26	Co.41

STA	Prop	CB	℄	CB	Prop
	161.34	160.27		159.61	159.18
11+00	160.34	160.34		159.72	159.72
	C1.00	Fo.07		Fo. 11	Fo.54
10+86.9=Sew LAT #9 RT omit			159.2 154.3 ℄ C4.9		159.2 155.1 P.L C4.1
10+76.9= W.S. RT					159.4 159.9 tp cb Fo.5
		160.69		159.82	
10+75	160.52	160.52		159.90	159.90
		Co.17		Fo.08	
	161.57	160.76		159.94	159.43
10+50	160.70	160.70		160.09	160.09
	Co.87	Co.06		Fo.15	Fo.66
10+36.9=Sew LAT #10 RT omit			159.4 154.7 ℄ C4.7		159.4 155.5 P.L C3.9
10+26.9= W.S. RT				160	159.6 160.3 tp cb Fo.7
		161.00		160.19	
10+25	160.88	160.88		160.27	160.27
		Co.12		Fo.08	
	161.46	161.12		160.38	160.03
10+00	161.06	161.06		160.45	160.45
	Co.40	Co.06		Fo.07	Fo. 42
		161.31		160.68	160.03
9+75	161.25	161.25		160.63	160.63
		Co.06		Co.05	Fo.60

STA	P.L	CB	℄	CB	P.L
12+24 = W.S LT.	160.5 159.4 TPCB C1.1				
12+22.29	160.41 159.46 C0.95	158.96 159.46 F0.50		158.80 158.91 F0.11	158.65 158.86 F0.21
12+15 = Sew LAT #5 RT.			158.7 152.8 ℄ C5.9		158.7 154.0 P.L C4.7
12+00.46	160.45 159.61 C0.84	159.59 159.61 F0.02		158.95 159.04 F0.09	158.90 159.01 F0.11
11+78.64	161.21 159.76 C1.45	159.72 159.76 F0.04		159.03 159.18 F0.15	158.84 159.16 F0.32
11+56.81 = ℄ Sta. marg.	161.67 159.91 C1.76	159.76 159.91 F0.15		159.09 159.31 F0.22	158.47 159.31 F0.84
11+50	159.96	159.85 159.96 F0.11		159.18 159.36 F0.18	159.36
11+26.9 = Sew LAT #6 RT omit			158.9 153.8 ℄ C5.1		158.9 154.7 P.L C4.2
11+25	160.15	160.26 160.15 C0.11		159.50 159.54 F0.04	159.54
11+11.93 = W.S. RT omit					158.8 159.6 tp cb F0.8

STA	P.L	CB	℄	CB	P.L
13+15.01	158.52 158.80 F0.28	158.52 158.80 F0.28			
13+08.11 Sew LAT #3 LT.	160.0 154.2 P.L C6.8		161.00 152.00 ℄ C9.0		
12+98.87 = B.C LT 5'ly CB (CONST.) Note: Beg STA's here For 5'ly CB Prop-Line STA's only 11.10 -		158.71 158.93 F0.22			
12+87.77 = P.R.C F/B (E.C DWG CONST) = 6.44' Ahead	160.20 159.01 C1.19	158.74 159.01 F0.27		158.51	(meet EXIST) 158.51 Chk 158.41 = EXIST CB RT
12+74.8 = W.T.S. LT. omit	160.8 159.1 tp CB C1.7				
12+65.94	160.41 159.16 C1.25	159.04 159.16 F0.12		158.70 158.65 C0.05	158.62 158.56 C0.06
12+62 = Sew LAT #8 LT. omit	160.9 154.2 P.L C6.7		160.9 152.4 LT. C8.5		
12+44.11	160.68 159.31 C1.37	159.77 159.31 C0.46		158.93 158.77 C0.06	158.75 158.71 C0.04
12+32 Sew LAT #4 LT	161.0 154.6 P.L C6.4		161.0 152.8 ℄ C8.2		

STA	P.L	CB	℄	CB	P.L
14+17.92 = EXIST CB END	RT=				161.39 chk: 161.35
14+07.82	164.35 161.24 C3.11	161.30 161.24 C0.06			
℄ Arc=20'					
13+87.82	163.30 160.03 C3.27	160.33 160.03 C0.30			
End Prop. STA ℄					
Note: Beg ℄ STA.					
13+69.75=P.C.C. LINE only					
13+63.35 LT only (=13+67.82 ℄ STA)	161.88 159.20 C2.68	159.18 159.20 F0.02			
13+46.27 LT only	161.07 158.78 C2.29	158.81 158.78 C0.03			
13+31.15=℄ 8' CMP Cross-Gutt LT only	160.36 158.68 C1.68	158.71 158.68 C0.03			

STA	P.L	CB	℄	CB	P.L
15+37.05	176.43 173.52 C2.91	173.45 173.52 F0.07		173.03 172.92 C0.11	176.70 172.92 C3.78
15+11.66	171.25	171.51 171.25 C0.12		170.61 170.65 F0.04	170.65
~~STA = 14+23'~~					
14+86.28= P.C.C.	170.63 168.98 C1.65	169.03 168.98 C0.05		168.28 168.38 F0.10	171.63 168.38 C3.25
℄ Arc = 19.23' dcf = 3°07'35" Rch = 1922					
14+67.05	166.90	166.94 166.90 C0.04		166.15 166.30 F0.15	166.30
3' BK SW CB Ch = 16.71' ℄ Arc = 19.23'					
14+47.82	167.00 164.81 C2.19	164.65 164.81 F0.16		164.08 164.21 F0.13	168.84 164.21 C4.63
℄ Arc=20'					
14+27.82	165.80 162.83 C2.97	162.73 162.83 F0.10		162.24 162.23 C0.01	166.88 162.23 C4.65
℄ Arc=20'					

STA.	P.L	CB	℄	CB	P.L
16+67.82	186.56 181.35 C5.21	181.37 181.35 C0.02		180.35 180.75 Fo.40	180.37 180.75 Fo.38
16+47.82	181.34	181.03 181.34 Fo.31		180.88 180.64 C0.24	180.64
16+27.82	183.14 180.65 C2.49	180.51 180.65 Fo.14		180.10 180.05 C0.05	178.59 180.05 F1.46
16+07.82	179.59	179.53 179.59 Fo.06		178.80 178.99 Fo.19	178.99
15+87.82 B.V.C	182.88 178.06 C4.82	178.08 178.06 C0.02		177.34 177.46 Fo.12	178.53 177.46 C1.07
15+62.43	175.79	176.06 175.79 C0.27		175.27 175.19 C0.08	175.19

STA	P.L	CB	℄	CB
				176.81 177.03 Fo.22
#1 def = 10°35'21 ch = 9.93 (3 BK) 17+63.61 = CB BC RT				176.94 177.40 Fo.46
17+55.9 = SeW LAT #1 LT	1843 173.6 P.L C10.7		1843 169.6 ℄ C14.7	
17+47.82 = E.C MARGARITA	183.58 178.40 C5.18	17839 178.40 Fo.01		17808 177.80 Co.28
17+40 = W.S. LT.	186.4 +P 178.7 = CB. C7.7			
17+27.82	179.27	17926 179.27 Fo.01		17895 178.67 Co.28
17+16 = SeW LAT #2 LT.	187.1 175.1 P.L C12.0		187.1 170.9 ℄ C16.2	
17+07.82	186.86 180.15 C6.71	18023 180.15 Co.08		179.53 179.55 Fo.02
17+00 = W.S LT.	187.5 180.3 = T.P. CB C7.2			
16+87.82	180.98	18090 180.98 F0.08		18008 180.38 F0.30

STA	P.L
	177.03
	177.40
	177.83 177.80 Co.03
	178.67
	179.63 179.55 Fo.92
	180.38

STA	P.L	CB	℄	CB	P.L
18+07.59 = EXIST CB LT.	176.71 = EXIST	CLK 176.87			
17487.67 LT. only		177.43 177.37 Co.06			
17467.74 LT only	177.84	177.87 177.89 F0.02			
#2 = EXIST CB RT Δ = 21° 10' 42" ch: 9.93' (3 BK)				176.41	176.45 CHK: 176.41

STA

CLARK
GARBER
ABREWILLA
7-16-57
W.O. 32605

Imp's ALLEY BLK 29
FORTUNA PK

REF: City Notes C-15 (Robarts)
DWG: 12999-L

STA	LT.			RT (E'LY)
0+75	21.50 21.06 C0.44			20.40 20.75 Fo.35
0+50	20.49 20.69 Fo.20			20.23 20.39 Fo.16 (1' BK edge)
0+24	20.54 20.30 C0.24			19.48 20.00 Fo.52
0+14	20.55 19.98 C0.57		20.55 19.48 C1.07	19.31 19.68 Fo.37
0+04				19.17 19.02 C0.15
0+00 = ℄ alley at N'ly line crown Pt.	19.72 19.18 C0.54	off stub 2' BK LT	19.72 18.80 C0.90	

B.M

22.34 = 7'x7' LT DISC N.E Corner Sequoia & Roosevelt

2+32.3 = EXIST Chk.	23.29 23.28 PAV.		chk. 23.27 23.26
2+30	23.48 23.40		23.21 23.10
2+25	23.44 23.31 C0.13	(to meet EXIST PAV at 2+32.3 C0.23)	(F1.10) 22.02 23.02 F1.00
2+00	23.24 22.94 C0.30		21.85 22.62 F0.77
1+75	22.83 22.56 C0.27		21.87 22.25 F0.38
1+50 = Saw Cut #1 RT		21.47 10.40 & C1.07	21.47 18.90 P.L C2.57
1+50	22.27 22.19 C0.08		21.53 21.89 F0.36
1+25	21.92 21.81 C0.11		21.23 21.50 F0.27
1+00	21.62 21.44 C0.18		20.80 21.12 F0.32

CLARK GARBER ARRENILLA
7-16-57
W.O. 32653

IMP'S ALLEY BLK 15
LA JOLLA PK.

Ref: F.B 2232-29
DWG. 13080-L

	LT.	RT.
1+20	128.86 127.30 C 1.56	126.61 127.00 F0.39
1+00	129.24 126.88 C 2.36	126.59 126.58 C0.01
0+80	129.33 126.45 C 2.88	125.99 126.15 F0.16
0+60 E.V.C	126.70 126.03 C0.67	125.13 125.73 F0.60
0+40	126.58 125.29 C 1.29	124.89 124.99 F0.10
0+20	125.16 123.93 C 1.23	124.26 123.63 C0.63
0+10	124.78 123.10 1.68	123.71 122.80 C0.91
0+00 (Meas)	122.70	121.81
B.M. Coil Elev. Rod:		127.130 S.W. BP HIGH PEARL

	LT.	RT.
3+20=E.V.C	132.40 131.72 C0.68	130.54 131.42 F0.88
3+00	131.96 131.54 C0.42	131.19 131.24 F0.05
2+80=B.V.C	131.50 131.22 C0.28	131.00 130.92 C0.08
2+60	130.95 130.84 C0.11	130.74 130.54 C0.20
2+40	131.01 130.46 C0.55	130.37 130.16 C0.21
2+20	130.62 130.08 C0.54	130.01 129.78 C0.23
2+00	130.06 129.70 C0.36	129.46 129.40 C0.06
1+80	129.95 129.10 C0.85	128.08 128.80 F0.72
1+60	129.62 128.50 C1.12	127.44 128.20 F0.76
1+40	128.42 127.90 C0.52	127.23 127.60 F0.37

Jimp's ALLEY BLK 15 (CONT.)

STA	LT.		RT
CLK:			
CLK:	3+ 26.5 - 9	RT & Con steps & RT. Wall	132.14 = 132.14 = TP step.
4+00 (3+99.87)	132 67 132.20 Co. 47		133 23 131.90 C 1.33
3+80	132 41 132.08 Co.33		130 47 131.78 F 1.31
3+60	132 48 131.96 Co.52		130 45 131.66 F 1.21
3+40	132 48 131.84 Co.64		132 00 131.54 Co.46

CLARK
GARBER
O'NEIL
ABRENILLA
7-29-57
W.O. 62501

Imp's: ARISTA ST.
Pine to S'Ly Line Cherry

Ref: City Notes "E-18
DWG: 13133-L

STA	P.L	LT. Elev. CB	℄	RT.-(E'Ly) Elev GUTT ~~CB~~	P.L
0+50		247.98 248.42 FO. 44			
0+40 =BVC LT.		247.52 247.83 FO. 31			
0+25		246.69 246.91 FO. 22			
0+10=CB BC. LT (NW'Ly)		246.04 246.00 CO. 04			
[0+00=N'Ly Line Pine]					
# 2 mid-pt.		245.10 245.15 FO. 05			
# 4 EC. CB (Pine)		244.55 ~~244.60~~ FO. 05			
0+00=CB BC. ARISTA , E'Ly				245.52=GUTT.	
B.M				245.94=T'L+T NE Pine + ARISTA	

STA	P.L	CB	℄	GUTT ~~CB~~	P.L
1+40=GUTT RT.				253.17	
1+35		251.93 252.59 FO. 66			
1+30=GUTT RT				252.61	
1+25=BVC LT		251.62 252.15 FO. 53			
1+02.5		250.45 251.07 FO. 62			
0+99=GUTT RT.				250.79 =GUTT	
0+80=EVC		249.54 250.00 FO. 46			
~~0+78~~					
0+78=GUTT ON RT				250.45 =GUTT (BrK) (SET CROWN FT ON EXIST CB RT)	
0+70		248.93 249.51 FO. 58		249.98 GUTT (Plate 1 of 2)	
0+60		248.44 248.98 FO. 54			

ARISTA (Cont.)

STA.	P.L	CB	℄	GUTT	P.L
2+20 = GUTT. RT.				255.12	
2+15		25470 254.74 F0.04			
2+05 = B.V.C. LT		254.54 254.52 C0.02			
1+91.5 = GUTT. RT				254.31	
1+85		25436 254.05 C0.31			
1+77 = GUTT RT.				253.90	
1+65 = E.V.C. LT		25393 253.58 C0.35			
1+55		25361 253.31 C0.30			
1+50 = GUTT. RT				253.48	
1+45		252.85 252.98 F0.13			

STA	P.L	CB	℄	GUTT	CB
2+95.96 = CB BC LT		25552 255.28 C0.24			
2+81.46 up CBU EN RT, 25' RT ℄ mid-pt					25454 255.12 - up Correx F0.58
2+70.5 LT only		254.27 255.28 F 1.01			
2+62.96 = END CB AT PROP RT.			(AS Per plan)	25741 255.33 C2.08	25741 256.00 C1.41
2+62.96 = CB E.C RT			GUTT.	25634 255.50 C0.84	25634 255.93 = CB C0.41
2+60 = GUTT. RT. = (2+58.96 = CB BC RT)			GUTT.	255.37 cut crow-Ft.	255.87 = CB matEXIST
2+50 = GUTT RT.				255.34	
2+45 = EVC LT.		25489 255.08 F0.19			
2+35		25492 255.02 F0.10			
2+30 = GUTT RT.				255.27	
2+25		25482 254.90 F0.08			

ARISTA (CONT.)

STA	P.L	CB	℄	GUTT	CB
2+99.96=CB RT AT PROP L				25514 254.90=GUTT. CO. 24	25514 CB 255.50 (AS PER PLAN) FO. 36
2+99.96=CB 18' RT OF ℄ ST.			G=	25563 255.25 CO. 38	25563 255.67=TP CB FO.04
2+99.96=CB ELEV 14' RT ℄			G=	25562 255.17 CO.45	25562 TP 255.67=CB FO.05
2+99.96 CB EL. EST		25610 254.98=G C1.12	25610 255.48=TP CB CO.62		
2+99.96= CB EC LT.		25562 255.34 CO.38			

CLARK
GARBER
ABRENILLA
8-2-57
W.O. 32728

SEWER: SOLEDAD RD

EXIST M.H 110.82' S'Ly & Soledad-Way
N'Ly to (S'Ly & N'Ly Line) P.L. II 1779

Ref: City Notes: C-13 (HATCH)
Dwg: 3941-2-D

STA		E/ev's
1+90		368.96 358.59 C 10.37
1+50	40' @ 8.01°	364.74 355.07 C 9.67
= M.H #1 1+10.82 (Δ=0°0')	39.18'	360.80 351.60 C 9.20
0+73.88	36.94'	357.85 349.66 C 8.19
0+36.94	36.94' @ 5.25°	355.27 347.72 C 7.55
Ck: cross N'Ly Rim	EXIST M.H 353.00	= 353.00
0+00 = ℄ EXIST M.H (Dwg 3191-D) 110± S'Ly ℄ Soledad-Way		345.78
B.M (Dist. Elev. Rod.)		362.87 = N.E. Spike

STA.	E/ev's:
4+80	397.17 383.03 C 14.14
4+40	392.81 379.87 C 12.94
4+00 (7.90° @ 40.63') (Note checked Back to B.M O.K!)	390.28 376.70 C 13.58
Chk 40.63' 387.62 = 387.47 = 2x2 (℄ = City Notes 3+59.37) C-13 (Hatch-Smith)	
= M.H #2 3+59.37 [Δ = 20° 41' 30" RT]	386.42 373.50 = F.L C 12.92
9.37'	
3+50	385.29 372.67 C 12.62
3+10	381.13 369.15 C 11.98
2+70	378.62 365.63 C 12.99
2+30	372.75 362.11 C 10.64

IN Pole Soledad Rd & Soledad-Way (No Number)

SEWER: Soledad Rd (Cont.)

Sta.	Elev's:
8+20	427.89 411.94 C 15.95
7+80	424.17 408.07 C 16.10
7+40	420.53 404.21 C 16.32
(37.40') Chk: 414.78 = 414.63 = 2x2 ℄ 702.60 ! See chk at 3+59.37	
=#3 7+02.60 [Δ = 24° 40' RT.]	416.15 400.60 C 15.55
6+80	413.34 398.81 C 14.53
6+40	409.48 395.66 C 13.82
6+00	406.69 392.51 C 14.18
5+60	402.98 389.35 C 13.63
5+20	399.05 386.19 C 12.86

Sta.	Elev's:
11+70	456.40 443.72 C 12.68
11+30	452.65 440.55 C 12.10
10+90	449.04 437.37 C 11.67
(-37.42')	
=M.H #4 10+52.60 [Δ = 0° 0']	446.42 434.40 C 12.00
(32.60')	
10+20	442.66 431.26 C 11.40
9+80	440.32 427.39 C 12.93
9+40	437.50 423.53 C 13.97
9+00	433.23 419.67 C 14.56
8+60	431.39 415.80 C 15.59

Sewer: Soledad Rd - (Cont.)

STA		Elev's:
15+20		481.43 467.58 C 13.85
	43.80'	
14+80		479.32 465.74 C 13.58
		477.38 463.91 C 13.47
14+40		
	(37.40')	
= M.H #5 14+02.60		475.28 462.20 C 13.08
	194.8'	
	(32.60')	
13+70		473.71 459.60 C 14.11
13+30		471.36 456.43 C 14.93
12+90		467.71 453.25 C 14.46
12+50		462.82 450.07 C 12.75
12+10		460.51 446.90 C 13.61

STA.	Elev's:
Chk: 482.93 =	482.78 = 2x2¢ 15+46.66
	City Notes C-13 (note: Same 0.15' we Picked up At 3+59.37)
{D. END = Plug end 15+46.66 (= PT int. w'ly Line P.L #1779)	482.98 468.80 = F.L. C 14.18
(26.66')	

CLARK GAMBER ARRENIUS

8-13-57
W.O. 21631

STORM-DRAIN - LOT 14
LA JOLLA CORONA ESTATES

Ref. DWG: 6639-B
Notes B-12

(0+26)
0424

424.22
417.20
C 7.02 F.L

end Pipe
on Line Fc. hdwall

Pipe
24" RCP

0700 E Type "G" 431.63 431.63
437 425 FL
F 5.37 Tp C 6.63
C/L RCP NO 1 Box
PT 2.67 Beyond Fc EXIST
hdwall
CLEAN OUT

B.M. 449.18 = Ch □ TP CB E EXIST CB INLT

CLARK
GARBER
Moore
ABRENILLA
9-6-57
W.O. 32667

IMP's: LAURETTA ST.

Mollie to AZUSA

REF: DWG: 4042-D & 4042-A-D
: City Notes: E-17

(Note: W. Services set by Water Dept. Survey Crew 9-6-57)

STA	P.L	CB	℄	CB	P.L
		(LT'LY)		RT.	
	32 67	32 24		31 53	32 57
0+70=B.V.C	32.34	32.34		31.92	31.92
	Co.33	Fo.10		Fo.39	Co.65
0+68=W.S RT.					
	32 85	32 12		31 46	
0+50	32.18	32.18		31.84	31.84
	Co.67	Fo.06		Fo.38	
0+38=W.S LT.					
		31 86		31 62	
0+25	31.98	31.98		31.74	31.74
		Fo.12		Fo.12	
	32 25	31 65		32 24	32 31
0+08=CB	31.84	31.84		31.67	31.67
BC'S:	Co.41	Fo.19		Co.57	Co.64
		31 84		31 83	
#1=END CB	31.86	31.86		31.60	31.60
		Fo.02		Co.23	
(R. Grade only)					
0+00=E.L.	31.85	31 55		31.64	31.64
AZUSA					
B.M. (Dir. Elev. Rod):				31.61= Con Mon	
				℄ Lauretta & W. Line	
				Mollie	

STA	P.L	CB	℄	CB	P.L
	35 49	34 90		34 62	34 53
2+60=BVC	35.33	35.33		34.83	34.83
	Co.16	Fo.43		Fo.21	Fo.30
		34 57		34.23	
2+35	34.91	34.91		34.41	34.41
		Fo.34		Fo.18	
	35 17	34.13		33 68	34.20
2+10	34.49	34.49		33.99	33.99
	Co.68	Fo.36		Fo.31	Co.21
		33 91		33 34	
1+85	34.08	34.08		33.58	33.58
		Fo.17		Fo.24	
	34 14	33 47		32 94	33 42
1+60	33.66	33.66		33.16	33.16
	Co.48	Fo.19		Fo.22	Co.26
		33 00		33 03	
1+35	33.25	33.25		32.75	32.75
		Fo.25		Co.28	
	33 30	32 62		32 07	32 75
1+10=E.V.C	32.83	32.83		32.33	32.33
	Co.47	Fo.21		Fo.26	Co.42
		32 36		31 70	
0+90	32.54	32.54		32.06	32.06
		Fo.18		Fo.36	
			33 65		33.65
0+83=Sew			26.43 ℄		26.97 Ap.
LAT=10 RT.			C7.22		C 6.68 F. Line

Note: Set TBM on Con Mon 144± S'ly on W'ly Line Mollie = 30.705

STA	P.L	LT. CB	℄	RT CB	P.L
3+96= W.S RT					
3+88 =W.S. LT.					
3+84.48	33 63 33.40 C0.23	33 32 33.40 F0.08		32 71 32.90 F0.19	32 83 32.90 F0.07
3+62.24	34.01	33 88 34.01 Fo.13		33 45 33 51 F0.06	33.51
3+40=EVC	37.34 34.61 C 2.73	34.44 34.61 Fo.17		33 84 34.11 Fo.27	33 36 34.11 Fo.75
3+38 = SeW LAT #1 RT			3292 27.45 C 5.47	℄	32 92 28.00 F.L Prop C 4.92
3+20	35.18	35 10 35.18 F0.08		33 85 34.68 Fo.83	34.68
3+00	36 70 35.48 C1.22	35 31 35.48 Fo.17		35 18 34.98 C0.20	35 59 34.98 C0.61
2+80	35.54	35 17 35.54 Fo.37		35 57 35.04 Co.53	35.04
2+73=W.S LT.					

STA	P.L	CB	℄	CB	P.L
Chk:	32.64	=32.67=	ENAIL	LAURETTA & AZUSA	
(R. grade only) 4+16.72=W. Line AZUSA	33 06 32.7 C0.36				32 83 31.8 C 1.03
#1 END CB	32.70	33 36 32.70 Co.66		32 92 31.85 C1.07	31.85 #1 END CB
(NW'LY) Ret Δ=48°11'23"					(S.W'LY Ret)
4+06.72 CB Bc's	33 05 32.80 C0.25	33 60 32.80 F0.20		31 95 32.30 Fo.35	32 80 32.30 C0.50

LAURETTA ST. (Cont.
AZUSA to BENICIA

STA.	P.L	CB	℄	CB	P.L
1+25	34.90	34 33 34.90 Fo.57		34 10 34.41 Fo.30	34.41
1+00	34 36 34.27 Co.09	33.94 34.27 Fo.33		33 39 33.78 Fo.39	32 03 33.78 F1.75
0+75	33.63	33 28 33.63 Fo.35		32 69 33.15 Fo.46	33.15
0+50 =grd Brk Lt.	33 07 33.00 Co.07	32 51 33.00 Fo.49		32 22 32.51 Fo.29	31 98 32.51 Fo.53
0+38=W.S RT					
0+25	32.69	32 10 32.69 Fo.59		31.08 31.88 Fo.80	31.88
0+10=CB 12C's	32 67 32.50 Co.17	31 86 32.50 Fo.64		30 95 31.50 Fo.55	30 72 31.50 Fo.78
#1=END CB Δ=48° 11' 23"	32.40	32 96 32.40 Co.56		31 34 31.20 Co.14	31.20 #1
0+00=E.Line AZUSA	32 7 32.4 Co.3	(R.Grade only)			30 64 31.2 Fo.56

STA.	P.L	CB	℄	CB	P.H
3+13.5= BrC	49 18 48.36 Co.82	48 15 48.36 Fo.21		47 65 47.86 Fo.21	48 82 47.86 Co.96
2+88.5	45.31	45 76 45.31 Co.45		45 35 44.81 Co.54	44.81
2+63.5= E.V.C	40 30 42.27 F1.97	42 50 42.27 Co.23		42 16 41.77 Co.39	44 52 41.77 C2.75
2+43.5	40.08	40 17 40.08 Co.09		40 30 39.58 Co.72	39.58
2+28=W.S RT.					
2+23.5	39 20 38.37 Co.83	38 23 38.37 Fo.14		38 32 37.87 Co.45	39 49 37.87 C1.53
2+03.5	37.14	36 85 37.14 Fo.29		36 23 36.64 Fo.41	36.64
1+83.5= B.V.C.	36 64 36.39 Co.25	36 07 36.39 Fo.32		35 59 35.89 Fo.30	35 65 35.89 Fo.24
1+75	36.17	35 80 36.17 Fo.37		35 27 35.68 Fo.41	35.68
1+50	35 52 35.53 Fo.01	35.03 35.53 Fo.50		34 64 35.04 Fo.40	34 51 35.04 Fo.53

Set T.B.M. - swly CB R - 52.95 Elk: 1X1
At Lauretta & Benicia

STA	P.L	CB	E	CB	P.L
	55.9				533
4+16.86 =	55.2	Rough - Grade only			54.2
W. Line	C0.7				F0.9
BENICIA					
#2 = End CB	55.23	5621		5331	54.20 #2
Δ = 48° 11' 23"		55.23		54.20	
		C0.98		F0.89	
#1		5467		5364	54.20 #1
	55.00	55.00		54.20	
Δ = 32° 07' 40"		F0.33		F0.56	
4+08.86 =	5625	5425		5373	5302
CB BC's:	54.55	54.55		54.05	54.05
	C1.70	F0.30		F0.32	F1.03
3+90.4	5556	5346		5274	5252
	53.63	53.63		53.13	53.13
	C1.93	F0.17		F0.39	F0.61
3+89 = Sew	5583		5583		
LAT #2 - LT	48.54 F.L.		45.51 E		
	7.29 Prop		C10.32		
3+71.95	52.72	5230		5203	52.22
		52.72		52.22	
		F0.42		F0.19	
3+535 =	5210	5136		5091	5148
E.V.C	51.80	51.80		51.30	51.30
	C0.30	F0.44		F0.39	C0.18
3+335	50.44	5003		4922	49.94
		50.44		49.94	
		F0.41		F0.72	

LAURETTA (CONT.
BENICIA to COLUSA

Ref: City Notes: E-17 (CLIFF ALLEN) (INCOMPLETE!)

STA	P.L	CB	E	CB	P.L
1+26.5 = W.S.					
RT.					
	61.93		6193		
1+06.5 =	55.37 P.L		51.61 E		
Sew LAT #3	C6.56		10.32		
LT.					
		60.00		5856	
1+03	60.22	60.22		59.22	59.22
		F0.22		F0.66	
	60.70	58.92		5766	58 15
0+78	59.24	59.24		58.24	58.24
	C1.46	F0.32		F0.58	F0.09
		5775		5678	
0+53	58.26	58.26		57.26	57.26
		F0.51		F0.48	
	5861	5695		5588	5627
0+28	57.28	57.28		56.26	56.26
	C1.33	F0.33		F0.38	C0.01
	5775	5607		5570	5558
0+08 - CB BC's	56.50	56.50		55.50	55.50
	C1.25	F0.43		C0.20	C0.08
		5604		5546	
#1	56.20	56.20		55.14	55.14
Δ = 32° 07' 40"		F0.16		C0.32	
		5761		5537	
#2 CB end	56.13	56.13		54.97	54.97 CB END
Δ = 48° 11' 23"		C1.48		C0.40	
	575				5545
0+00 = E. Line	56.1				55.0
BENICIA	C1.4				C0.45

Note: W.S.s set by city Water Dept. Survey Party

STA	P.L	CB	℄	CB	P.L
2+75	65.52	6525 65.52 Fo. 27		6474 64.52 Co.22	64.52
2+50	6694 64.82 C2.12	6455 64.82 Fo. 27		6413 63.82 Co. 31	6364 63.82 Fo.18
2+25	64.13	6381 64.13 Fo. 32		6315 63.13 Co.02	63.13
2+00	6536 63.43 C1.93	6313 63.43 Fo.30		62.17 62.43 Fo.26	6112 62.43 F1.31
1+76.5= Sew LAT #5 LT	6582 57.78=P.L C8.04		6582 53.91 ℄ C11.91		
1+75	62.74	6212 62.74 Fo. 62		61.68 61.74 Fo.06	61.74
1+68=E.V.C	6509 62.55 C2.54	6202 62.55 Fo. 53		6155 61.55 grade	6075 61.55 Fo.80
1+48	61.94	6145 61.94 Fo.49		6055 60.94 Fo. 39	60.94
1+46.5=Sew LAT #4 RT.			60.60 52.93 ℄ C7.67		60.60 53.43=P.L. C7.17
1+28=B.V.C	6288 61.21 C1.67	6074 61.21 Fo.47		5961 60.21 Fo.60	6046 60.21 Co.25

STA	P.L	CB	℄	CB	P.L
4+13.08=W.Line Colusa	70.9 70.0 Co.9	(R. Grade only)			6736 68.2 Fo. 84
#2-end CB	70.03	7145 70.03 C1.42		6700 68.25 F1.25	68.25
#1	69.60	6940 69.60 Fo.20		6764 68.23 Fo.59	68.23
4+05.08=CB Bc's:	7094 69.10 C1.84	6881 69.10 Fo.29		6771 68.10 Fo.39	6700 68.10 F1.10
4+00	68.98	6874 68.98 Fo.24		6763 67.98 Fo.35	67.98
3+75	68.29	6785 68.29 Fo.44		6699 67.29 Fo.30	67.29
3+51.5= Sew LAT #7 RT.			6499 59.53 ℄ C5.46		64.99 60.03 P.L C4.96
3+50	6979 67.60 C2.19	67.27 67.60 Fo.33		6632 66.60 Fo.28	6548 66.60 F1.12
3+25	66.90	6655 66.90 Fo.35		6572 65.90 Fo.18	65.90
3+00	7055 66.20 C4.35	5594 66.20 Fo.26		6525 65.20 Co.05	6454 65.20 Fo.66

LAURETTA ST. Colusa to Brunner

Set T.B.M. = SWly Rod. PT = 66.25

STA.	P.L	CB	℄	CB	P.L
0+78 = EVC	79.50 76.13 C 3.37	75.82 76.13 Fo. 31		74.78 75.13 Fo. 35	74.78 75.13 Fo. 35
0+58	75.00	74.54 75.00 Fo. 46		73.54 74.00 Fo. 46	74.00
0+38 = B.V.C	76.64 73.66 C 2.98	73.23 73.66 Fo. 43		72.52 72.66 Fo. 14	72.59 72.66 Fo. 07
0+23	72.58	72.20 72.58 Fo. 38		71.27 71.58 Fo. 31	71.58
0+20 = Sew-LAT #8 LT.	76.06 67.36 P.L C 0.70		76.06 64.03 ℄ C 1.203		
0+08 = CB BC's	74.85 71.50 C 3.35	71.35 71.50 Fo. 15		70.31 70.50 Fo. 19	70.35 70.50 Fo. 15
#1	71.21	74.43 71.21 C 3.22		70.05 69.78 C 0.27	69.78
#1 End CB	71.28	74.56 71.28 C 3.28		69.84 69.43 C 0.41	69.43
0+00 = E. LINE Colusa	74.24 71.3 C 2.94				69.32 69.4 Fo. 08

STA. (NELy Ret)	P.L	CB	℄	CB	P.L
	81.90	- chk		cont next Pg.	
2+14.92 = CB BC LT only	81.94 = EXIST CB BC				
2+01.06 = END EXIST. CB. RT				chk:	80.69
1+90.34 LT only = Con. Gutt.	81.00 = Gut. grade				
1+76.19 RT only				79.35 79.76 Fo. 41	79.76
1+71.94 LT. only = Con Gut.	80.60 = Gut grade				
1+53.54 LT only = Con. Gutter	79.60 = Gut. grade				
1+51.32 RT only				78.52 78.84 Fo. 32	78.24 78.84 Fo. 60
1+45.30 = Prop Conc LT	83.3 80.0 C 3.3	(R. Grade only)			
#1 end CB. LT. (NWly Ret)	80.05	83.73 80.05 C 3.68			
1+41.32 = CB B.C LT only	83.21 79.40 C 3.81	79.44 79.40 C 0.04		78.08 78.40 Fo. 32	78.40
1+25	82.36 78.57 C 3.79	78.63 78.57 C 0.06		77.45 77.57 Fo. 12	77.42 77.57 Fo. 15
1+05 = Sew-LAT #9 LT	82.43 72.53 P.L C 9.90		82.43 66.84 ℄ 15.59		
1+00	77.27	77.40 77.27 C 0.13		76.59 76.27 C 0.32	76.27

STA.	P.L	CB	℄	CB.	P.L	STA.	P.L	CB	℄	CB	P.L
#1 end co	82.35	82.41 82.35 Co.06									

CLARK
GARBER
MOORE
ABBENILLA
10-10-57
W.O. 31678

ALLEY: JEWELL to KENDALL
CONGRESS HT'S ADD:
(bet. MONMOUTH + BERYL)

REF: DWG: 3897-D
City Notes C-13 (HATCH)

STA	LT.	℄	RT (S'ly)
1+40	178 84 178.11 C0.73		179 26 177.81 ch-wall 0.21' BK C1.45
1+20 = BVC	178 55 178.18 C0.37		177 43 177.88 F0.45
1+00 ch-wall 0.25' BK	179.67 178.11 C1.56		179 32 177.81 ch-wall 0.10' BK C1.51
0+75 ch-wall 0.28' BK	179.00 178.02 C0.98		178 99 177.72 ch-wall 0.07' BK C1.27
0+50 ch-wall 0.25' BK	178 99 177.93 C1.06		178 54 177.63 ch-wall 0.09' BK Pair C0.91
0+25 ch-wall 0.25' BK	179.05 177.84 C1.21		178 55 177.54 ch-wall 0.10' IN C1.01
0+10 ch-wall 0.25' BK	179 37 177.79 C1.58		178 13 177.49 ch-wall 0.71' BK C0.64
0+00 = E. Line JEWEL	179.16 177.80 C1.36		177 84 177.40 ch-wall 0.50' BK C0.44
Notes: [All outs refer to edge PAV.			
B.M. DIR. ELEV. ROD:			160.15 = N.E. BP BERYL + JEWELL

STA.	LT.	℄	RT
2+70	175 17 175.20 C0.57		174 13 174.90 F0.77
2+50 = grid Brk	176 37 175.50 C0.87		174 45 175.20 F0.75
2+30 = W.S LT.	176 82 176.25 = PAV. C0.57	176 82 172.75 = F.L Pipe At prop C4.07	
2+25	176.97 176.13 C0.84		175 50 175.83 F0.33
2+20 = Sew. LAT #1 LT	177.20 171.00 Prop C6.20 F. Line	177.20 169.77 ℄ C7.43	
2+00 Nail Fence 0.50' BK	178 61 176.75 C1.86		176 10 176.45 F0.35
1+75	178 78 177.38 C1.40		176 46 177.30 F0.84
1+60 = EYC Stub 0.50' BK	179 17 177.75 C1.42		176 90 177.45 F0.55

[For Storm-Drain See Pg 75]

Chk: 184.59 = 184.58 = clx w Rim M.H 5+25 Notes C-13 Pg5

STA.	LT.	℄	RT.
3+70	179.35 179.50 F0.15		177.50 179.20 F1.70
3+60	179.10 178.90 C0.20		176 83 178.60 F1.77
3+50	177.74 178.12 F0.38		175 66 177.82 F2.16 cl-wall 1'BK
3+30	176 77 176.36 C0.41		174 96 176.06 F1.10 cl-wall 1'BK
3+10 = 9+4 BK	175 82 175.12 C0.70		174 55 174.82 F0.27 cl-wall 1'BK
2+93.15 = ℄ Type "J" Catch Basin stub 9'S 24 ℄ BASIN		17361 174.25 = Grate F0.58	17367 172.00: F.L. Box C1.67
2+90	175 66 174.90 C0.76		174 01 174.60 F0.59

STA.	LT.	℄	RT
			184 52
5+00.55 = N.	186 52 186.26		184.75
LINE KENDALL	C0.26		F0.23
NAIL Fence 0.60 BK			stub 1'BK
	186.10		184.11
4+90	185.50		184.90
NAIL Fence 0.60 BK	C0.60		F0.79
	186 07		183 90
4+80	185.00		184.70
NAIL Fence 0.60 BK	C1.07		F0.80
	185 49		183.55
4+65	184.25		183.95
NAIL Fence 0.60 BK	C1.24		F0.40
	184 09		182.57
4+40	183.00		182.70
	C1.09		F0.13 stub 1'BK
	182.23		180 95
4+15	181.75		181.45
stub 1'BK	C0.48		F0.50
3+90	181.53 180.50		178 55 180.20
NAIL Fence 1' BK	C1.03		F1.65

STORM DRAIN (Alley Contract) See Pg 73
ALLEY: JEWELL to KENDALL

REF: City Notes: C-13 (Sommermeyer)
DWG: 3897-D

STA. [℄R = 22.50' Δ = 30°]	Elev's	STA.	Elev's:
1+29.36 = B.C	172.85 169.73 C 3.12	CLK: (Ck + Ely Rim M.H) C-13 Pg 3	175.34 = 175.32
1+00 - grid Blk	171.06 167.00 F.L C 4.06		
0+80 = grid Blk	169.90 166.00 = F.L Pipe C 3.90		
0+47.5 (Stubs Set 4' RT. ℄)	168.20 164.90 C 3.30		
- Beg 15" Pipe 0+15 = END CB outlet Box	166.02 163.80 = F.L Box + Pipe C 2.22	1+53.64 = INside (5'4) edge CATCH BASIN	For grade on BASIN See Pg 74 (STA 2+93.15 Alley)
0+10	164.91 164.60 = Top WALK C 0.31 - Top Box	1+41.14 = E.C	173.39 170.83 C 2.56
0+00 = CB LINE	164.17 = CB	163.55 = Gutt.	
BM: Dir. Elev. Rod:	170.39 = NEBP Beryl + KENDALL		

CLARK
GARBER
MOORE
ARRENILLA
12-23-57
W.O 20945
CLK:

Storm Dr. Lot 14, Blk 127
CHONTES ADD.

REF: F.B 2060-74
DWG: 6838-B
6838-A-B

69.18 - 69.15 = F.L EXIST T 48" C.M. Pipe

Box #2

68 43
67.80
C0 63 F.L Box

0+88 = S'ly inside edge Box #1

69 88
67.65
C2.23 F.L Box

69.88
x 68.55 = F.L 12'45" Pipe to N'ly
C1.33

0+66

68 03
67.11
C0.92

0+44

68 20
66.56
C1.64

0+22

66 96
66.01
C0.95

Stubs set 5' RT (E'ly)

0+00

65.47 F.L 45"

Note: F.L N'ly end EXIST 60" = 65.07 not as shown on Dwg 64.44!

T.B.M. = F.L EXIST 30" CON. Pipe = 67.77 F.B 2060 Pg 77

CLARK
GARBER
MOORE
ABRENILLA
2-21-58
W.O. 20006

CB Grades (For Grade-Study)

RIGEL ST. MAIN — to DALBERGIA

REF: PROJ. DWG: No number
F.B 2196-1

LT. STA.	LT. Prop	CB	E	CB	RT Prop
		6.41			6.13
1+50		5.54			5.64
		Co.87			Co.49
(1+28) CB	6.57				
	5.65				
	Co.92				
		5.75			
1+25		5.67	5.62		
		Co.08			
(1+15) CB	6.58				
	5.72				
	Co.86				
		6.45			6.24
1+00		5.79			5.89
		Co.66			C.35
		6.37			
0+75		5.92			
		Co.45			
		6.45			6.37
0+50		6.04			6.14
		Co.41			Co.23
		6.55			
0+25		6.17			6.27
		Co.38			
		6.33			6.57
0+08=CB BC		6.25			6.35
		Co.08			Co.22
0+00=N.L MAIN		6.41			Stubs on Prop

Stubs 3' BK CB FC

MAIN & RIGEL
TP NE CBEND (0+00 21.7 RT) = 6.53

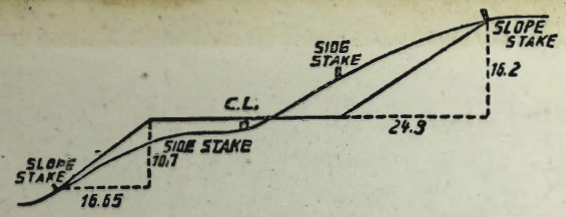
B.M DIM. Elev RD.

5.21 = L+T N'ly 7' Line MAIN + W Line SIVA

STA.	Prop.	CB	E	CB	Prop
	6.03				6.05
2+68=E.V.C	5.15	5.35			5.45
	C.88				Co.60
	6.29				6.19
2+48	5.15	5.15			5.25
	1.14				Co.94
	6.75				6.27
2+28=BVC	5.15	5.15			5.25
	C1.60				C1.02
2+25	5.17	5.17	℄ not set		
	6.89				6.22
2+00	5.29	5.29			5.39
	C1.60				Co.83
1+70	5.42	5.42			

Stubs on Prop.

Stubs on Prop



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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