

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

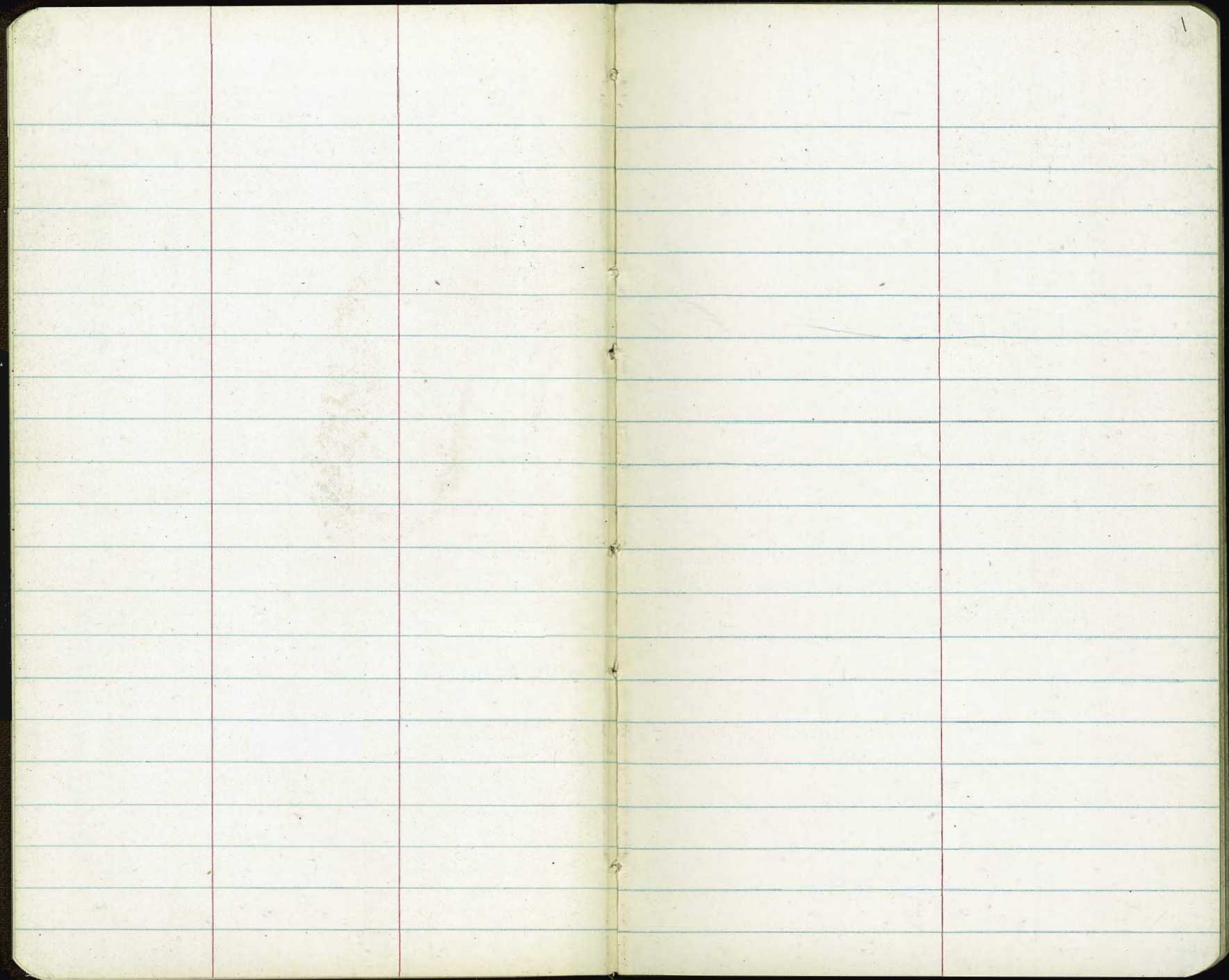
Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

G-381

MICROFILMED

APR 19 1965







Beq. Curb Stakes - Morena + weeks  
 SW. - "H" curb. - from "B" Line

1+97.01 = B.2

23.05

3

= End # on SW.  
 2+97.01 = E.C. = 44

22.24

Beq. B-2 = Island - w. side

0+00 = B.C. "B"

Marked  
 on plan.

17.04

+25 36.32

17.16

18.07

+50 37.28

17.28

18.31

+75 38.88

17.40

18.55

1+00 41.12

17.52

18.80

+25 43.12

17.71

19.07

+47.55 = E.C. =  
 B 43.73

17.94

1+50

19.36

0+00 of "C"

+75

19.70

+25 32'

18.23

2+00

20.09

+50 32'

18.52

= 1' Rad

+04.23 = W.

20.17

+75 32.03

18.82

= E

20.20

Beq. B-2 - Island. - S.W. side

1+00 32.36

19.12

20.24

+25 33.10

19.42

20.57

+50 34.23

19.74

20.93

+75 35.75

20.09

21.30

2+00 37.65

20.46

21.67

+25 39.98

20.86

22.05

+50 42.26

21.28

22.42

+75 43.62

21.78

22.77

Corb. Stake 5 - Beg. at 113 + 25

4

	S. cb = "H"		S. Island = B-2			N. Island			N. cb = "H"			
113 + 25	12.16	11.98 <sup>216</sup>	C0.18	10.41	10.41	G	10.41	10.23 <sup>41</sup>	C0.18	9.03	9.01	C0.02
+50	12.29	12.00	C0.29	10.37	10.26 <sup>37</sup>	C0.11	10.37	10.06 <sup>37</sup>	C0.31	8.79	8.66 <sup>79</sup>	C0.13
+75	12.25	12.03	C0.22	10.46	10.14 <sup>46</sup>	C0.32	10.46	9.92 <sup>46</sup>	C0.54	8.66	8.37 <sup>66</sup>	C0.29
114 ~	12.44	12.04 <sup>44</sup>	C0.40	10.39	10.03 <sup>39</sup>	C0.36	10.39	9.81 <sup>39</sup>	C0.58	8.53	8.14 <sup>53</sup>	C0.39
+25	11.97	12.03 <sup>97</sup>	F0.06	10.25	9.96 <sup>25</sup>	C0.29	10.25	9.72 <sup>25</sup>	C0.53	8.38	7.99 <sup>38</sup>	C0.39
+50	11.99	11.99	G	9.06	9.90 <sup>06</sup>	F0.84	9.06	9.66 <sup>06</sup>	F0.60	8.03	7.90 <sup>03</sup>	C0.13
+75	11.70	11.97	F0.17	9.11	9.88 <sup>17</sup>	F0.77	9.11	9.64 <sup>17</sup>	F0.53	7.98	7.82 <sup>98</sup>	C0.16
115 ~	11.73	11.97 <sup>73</sup>	F0.24	8.89	9.88 <sup>73</sup>	F0.99	8.89	9.64 <sup>73</sup>	F0.75		7.75 <sup>73</sup>	
+25	11.71	12.09 <sup>71</sup>	F0.29	9.70	9.91 <sup>70</sup>	F0.21	9.70	9.67 <sup>70</sup>	C0.03	8.06	7.84 <sup>06</sup>	C0.22
+50	11.83	12.05 <sup>83</sup>	F0.22	9.63	9.96 <sup>83</sup>	F0.33	9.63	9.72 <sup>83</sup>	F0.09	8.41	7.94 <sup>41</sup>	C0.47
+75	11.68	12.14 <sup>68</sup>	F0.46	9.29	10.05 <sup>68</sup>	F0.76	9.29	9.81 <sup>68</sup>	F0.52	8.47	8.05 <sup>47</sup>	C0.42
116 ~	11.62	12.25 <sup>62</sup>	F0.63	9.94	10.16 <sup>62</sup>	F0.22	9.94	9.92 <sup>62</sup>	C0.02	8.56	8.17 <sup>56</sup>	C0.39
+25	11.74	12.37 <sup>74</sup>	F0.63	9.66	10.29 <sup>74</sup>	F0.63	9.66	10.05 <sup>74</sup>	F0.39	8.23	8.80 <sup>23</sup>	F0.57
+50	11.79	12.50 <sup>79</sup>	F0.71	19.97	10.41 <sup>79</sup>	F0.44	19.97	10.17 <sup>79</sup>	F0.20	8.37	8.42 <sup>37</sup>	F0.05
+75	11.62	12.63 <sup>62</sup>	F1.01	9.78	10.54 <sup>62</sup>	F0.76	9.78	10.30 <sup>62</sup>	F0.52	8.01	8.55 <sup>01</sup>	F0.54
117 ~	12.25	12.75 <sup>25</sup>	F0.50	9.81	10.66 <sup>25</sup>	F0.85	9.81	10.42 <sup>25</sup>	F0.61	7.83	8.67 <sup>83</sup>	F0.84
+25	12.20	12.88 <sup>20</sup>	F0.68	9.78	10.79 <sup>20</sup>	F1.01	9.78	10.55 <sup>20</sup>	F0.77	7.21	8.80 <sup>21</sup>	F1.59
+50	12.13	13.00 <sup>13</sup>	F0.87	9.49	10.91 <sup>13</sup>	F1.44	9.49	10.67 <sup>13</sup>	F1.20	8.09	8.92 <sup>09</sup>	F0.83
+75	12.19	13.12 <sup>19</sup>	F0.93	10.20	11.03 <sup>19</sup>	F0.83	10.20	10.79 <sup>19</sup>	F0.59	8.88	9.04 <sup>88</sup>	F0.16





"H" curbs S - 125+50 - N.

Cont. on P. 26

E.C. = 125+48.85

West.

East.

125+50	9.75	10.62 <sup>9.75</sup> F 0.87	8.18	8.02	C 0.16
126 ~	9.80	10.02 <sup>9.80</sup> F 0.22	8.09	8.07	C 0.02
+50	9.00	9.42 <sup>9.00</sup> F 0.42	8.02	7.93 <sup>02</sup>	C 0.09
127 ~	8.77	8.83 <sup>8.77</sup> F 0.06	7.74	7.70	C 0.04
+50	8.10	8.23 <sup>8.10</sup> F 0.13	7.55	7.47 <sup>55</sup>	C 0.08
128 ~	7.61	7.63 F 0.02	7.57	7.25 <sup>57</sup>	C 0.32
+50	7.18	7.12 <sup>7.18</sup> C 0.06	6.57	7.02 <sup>6.57</sup>	F 0.45
129 ~	6.55 <sup>677</sup>	6.79 F 0.24	6.78	6.79 <sup>6.80</sup>	F 0.01
+50	6.73	6.56 <sup>73</sup> C 0.17	6.77	6.57 <sup>77</sup>	C 0.20
130 ~	6.62	6.33 <sup>62</sup> C 0.29	6.65	6.34 <sup>65</sup>	C 0.31
+50	6.24	6.11 <sup>24</sup> C 0.13	6.50	6.11 <sup>50</sup>	C 0.39
131 ~	6.15	5.88 <sup>6.15</sup> C 0.27	6.22	5.88 <sup>22</sup>	C 0.34
+50	5.96	5.66 <sup>96</sup> C 0.30	5.91	5.66 <sup>91</sup>	C 0.25
132 ~	5.62	5.43 <sup>62</sup> C 0.19	5.56	5.43 <sup>56</sup>	C 0.13
+50	5.35	5.20 <sup>35</sup> C 0.15	5.40	5.20	C 0.20
133 ~	5.05	5.01 C 0.04	5.12	5.01	C 0.11
+50	4.98	4.87 <sup>98</sup> C 0.11	4.93	4.87 <sup>93</sup>	C 0.06
134 ~	4.93	4.75 <sup>93</sup> C 0.18	4.90	4.78 <sup>90</sup>	C 0.12
+25	4.77	4.69 <sup>77</sup> C 0.02	4.82 <sup>4.82</sup> 4.95	4.75 <sup>82</sup>	C 0.07 C 0.20

H cb.

20' Rad. - S. Cor. Weeks + Morena.

7

West.

East.

134 +50	Top = 4.60	4.63				4.74	
+75	✓4.69	4.63	C 0.06	+76.66 = PC		4.75	4.74 C 0.01
135 +00	✓4.95	4.69 <sup>95</sup>	C 0.26	1	4.75	4.79	F 0.04
+25	4.83	4.75 <sup>83</sup>	C 0.08	2	4.99	4.90	C 0.09
+50	4.87	4.81 <sup>87</sup>	C 0.06	3	5.05	5.04	C 0.01
+75	4.75	4.87 <sup>75</sup>	F 0.12	4	4.93	5.17 <sup>93</sup>	F 0.24
136 ~	5.04	4.93 <sup>94</sup>	C 0.11	5	4.66	5.27 <sup>93</sup>	F 0.61
+25	4.76	5.01 <sup>76</sup>	F 0.25	N.E. Cor. - 100' Rad.			
+50	4.68	5.10 <sup>68</sup>	F 0.42	45+97.56 = P.C. Morena			
+75	4.96	5.20 <sup>96</sup>	F 0.24	P.C. = 0	4.45	4.77 <sup>45</sup>	F 0.32
137 ~	5.66	5.32 <sup>66</sup>	C 0.34	1	4.81	4.81	G
+25	5.55	5.45	C 0.10	2	4.84	4.86	F 0.02
+50	6.00	5.59 <sup>00</sup>	C 0.41	3	5.41	4.90 <sup>41</sup>	C 0.51
+75	6.00	5.74 <sup>00</sup>	C 0.26	4	5.47	4.95 <sup>47</sup>	C 0.52
138 ~	5.86	5.91 <sup>86</sup>	F 0.05	5	4.88	5.01 <sup>88</sup>	F 0.13
+25	6.23	6.09 <sup>23</sup>	C 0.14	6 = E.C.	4.47	5.07	F 0.60
+50	6.50	6.28 <sup>50</sup>	C 0.22	= 136 + 43.54 Weeks. - P. 21			
+75	6.89	6.48 <sup>89</sup>	C 0.41				
139 ~	6.98	6.70 <sup>98</sup>	C 0.28				

Cont. on P. 23

## B-2 Curbs - Island -

Cont. on P. 25

125+50 - 2.45

9.06

125+50 - N.  
Lt. = W.

9.23 F 0.17

9.06

9.07

F 0.01

126 ~ 3.17

8.92

8.98 F 0.06

8.92

8.87<sup>97</sup>

C 0.05

+50 3.90

8.63

8.73 F 0.10

8.63

8.66

F 0.03

127 ~ 4.63

8.32

8.48<sub>32</sub> F 0.16

8.32

8.43<sub>32</sub>

F 0.11

+50 5.35

7.75

8.23<sub>75</sub> F 0.48

7.75

8.20<sub>75</sub>

F 0.45

128 ~ 6.07

7.85

7.99<sub>85</sub> F 0.14

7.85

7.98<sub>85</sub>

F 0.13

+50 6.80

7.22

7.75<sub>22</sub> F 0.53

7.22

7.75<sub>22</sub>

F 0.53

129 ~ 7.53

7.15

7.5<sup>54</sup><sub>15</sub> F 0.37

7.17

7.5<sup>56</sup><sub>15</sub> F 0.35

+50

7.61

7.30<sub>61</sub> C 0.31

7.69

7.30<sub>61</sub> C 0.39

130 ~

7.44

7.07<sup>44</sup> C 0.37

7.38

7.07<sup>38</sup> C 0.31

+50

7.19

6.84<sup>19</sup> C 0.35

7.16

6.84<sup>16</sup> C 0.32

131 ~

6.93

6.61<sup>93</sup> C 0.32

6.91

6.61<sup>91</sup> C 0.30

+50

6.81

6.39<sup>81</sup> C 0.42

6.99

6.39<sup>99</sup> C 0.60

132 ~

6.48

6.16<sup>48</sup> C 0.32

6.69

6.16<sup>69</sup> C 0.53

+50

6.26

5.93<sup>26</sup> C 0.33

6.30

5.93<sup>30</sup> C 0.37

133 ~

6.04

5.74<sup>04</sup> C 0.30

6.10

5.74<sup>10</sup> C 0.36

+50

5.69

5.60 C 0.09

5.69

5.60 C 0.09

134 ~

5.70

5.51<sup>70</sup> C 0.19

5.73

5.51<sup>73</sup> C 0.22

+25

5.10

5.48<sub>10</sub> F 0.38

5.30

5.48<sup>53</sup> F 0.18

+50

5.92

5.47<sub>92</sub> C 0.45

5.83

5.47<sup>83</sup> C 0.36

Rt. = E.

B-2

- Island.

Lt = W.

Rt = E.

9

134 + 75	5.59	<sup>59</sup> 5.47	C 0.12	5.23	5.47	F 0.24
135 ~	5.32	5.48	F 0.16	5.60	5.48	C 0.12
+ 25	5.57	<sup>32</sup> 5.51	C 0.06	5.69	5.51	C 0.18
+ 50	5.44	5.55	F 0.11	5.55	5.55	G
4' Lt. of E = + 74 6' R.	5.30	5.60	F 0.30	5.30	5.60	F 0.30

136 + 40	3.77	<sup>59</sup> 5.85	F 2.09	3.77	5.83	F 2.06
+ 50	3.41	<sup>377</sup> 5.90	F 2.49	3.41	5.83	F 2.42
+ 75	3.41	<sup>341</sup> 6.02	F 2.61	3.41	5.93	F 2.52
137 ~	3.79	<sup>341</sup> 6.16	F 2.37	3.79	6.05	F 2.26
+ 25	4.00	<sup>379</sup> 6.28	F 2.28	4.00	6.18	F 2.18
+ 50	4.28	<sup>400</sup> 6.42	F 2.14	4.28	6.32	F 2.04
+ 75	4.66	<sup>428</sup> 6.57	F 1.91	4.66	6.47	F 1.81
138 ~ 5' Rt	4.98	<sup>466</sup> 6.74	F 1.76	4.98	6.64	F 1.66
+ 25 - 3.24 Rt	5.17	<sup>498</sup> 6.89	F 1.72	5.17	6.82	F 1.65
+ 50 - 2.02 Rt	5.52	<sup>517</sup> 7.06	F 1.54	5.68	7.01	F 1.33
+ 75 - 7.20 Lt	5.90	<sup>552</sup> 7.24	F 1.34	5.89	7.21	F 1.32
Dist from E = 1.1		<sup>590</sup> 7.24			7.21	
139 ~ 8.66 Lt	6.22	<sup>590</sup> 7.43	F 1.21	6.06	7.43	F 1.37
+ 25 - 3.24 Rt	6.48	<sup>622</sup> 7.66	F 1.18	6.14	7.66	F 1.52
		<sup>648</sup> 7.66			7.66	

Lt.

139 +50	7.29	7.9 <sub>9</sub>	F 0.61
+75	7.86	8.1 <sub>6</sub>	F 0.30
140 ~	8.21	8.4 <sub>21</sub>	F 0.22
+25	8.51	8.7 <sub>51</sub>	F 0.20
+50	8.88	9.0 <sub>88</sub>	F 0.13
+75	9.19	9.3 <sub>19</sub>	F 0.13
141 ~	9.41	9.6 <sub>41</sub>	F 0.23
+25	9.99	9.97	C 0.02
+50	10.23	10.3 <sub>23</sub>	F 0.09
+75	10.66	10.68	F 0.02
142 ~ = 4BK - Pathways	11.05	11.05	G
+25	11.36	11.4 <sub>36</sub>	F 0.07
+50	11.68	11.8 <sub>68</sub>	F 0.15
+75	12.21	12.23	F 0.02
143 ~ = Beq. Taper	12.64	12.62	C 0.02
+25	13.25	13.0 <sub>25</sub>	C 0.23
+50	13.42	13.42	G
+65 = 1 Red.	13.32	13.6 <sub>32</sub>	F 0.34
144 ~			

Rt.

6.42	7.90	F 1.48
6.75	8.1 <sub>6</sub>	F 1.41
7.08	8.4 <sub>3</sub>	F 1.35
7.60	8.7 <sub>1</sub>	F 1.11
8.48	9.0 <sub>1</sub>	F 0.53
8.91	9.3 <sub>2</sub>	F 0.41
9.48	9.6 <sub>4</sub>	F 0.16
9.91	9.97	F 0.06
10.21	10.3 <sub>2</sub>	F 0.11
	10.68	
	11.05	
	11.43	

B-2

Island

11

Lt

Rt.

144 + 35 <sup>s Rt</sup> = 1' Rad.	15.04	<sup>504</sup> 14.75	C 0.29
+ 65 = Bag. Taper	15.35	<sup>35</sup> 15.18	C 0.17
+ 75	15.50	<sup>50</sup> 15.32	C 0.18
145 ~	15.78	<sup>78</sup> 15.65	C 0.13
+ 25	16.02	<sup>02</sup> 15.95	C 0.07
+ 50	16.04	<sub>04</sub> 16.23	F 0.19
+ 75	16.33	<sub>33</sub> 16.49	F 0.16
146 ~	16.53	<sub>53</sub> 16.73	F 0.20
+ 25	16.52	<sub>52</sub> 16.96	F 0.44
+ 50	16.74	<sub>74</sub> 17.15	F 0.41
+ 75	16.89	<sub>89</sub> 17.33	F 0.44
147 ~	17.12	<sub>12</sub> 17.49	F 0.37
+ 25	17.45	<sub>45</sub> 17.63	F 0.18
+ 50	17.62	17.74	F 0.12
+ 75	17.87	<sup>87</sup> 17.83	C 0.04
148 ~	17.90	17.91	F 0.01
+ 25	17.20	17.96	F 0.76
+ 50	17.78	17.99	F 0.21
+ 75	17.62	<sub>62</sub> 18.00	F 0.38

Level

Lt.

Rt. = E.

149 ~		17.70	17.99	F 0.29			
+25'		17.40	17.96	F 0.56			
+50		17.78	17.91	F 0.13			
+75'		17.05	17.83	F 0.78			
150 ~		17.59	17.73	F 0.14			
+25'		17.57	17.63	F 0.06			
+50		17.72	17.52	C 0.20			
+75' - 4' both ways		16.43	17.42	F 0.99			
Deq. - w. cb. Tang							
151 ~	3.67	17.38	17.31	C 0.07			
+25'	2.88	17.20	17.21	F 0.01			
+50	2.16	16.84	17.10	F 0.26			
+75'	1.61	16.69	16.99	F 0.30			
152 ~	1.18	16.61	16.89	F 0.28			
stake - S Rt.							
+25'	2.78	16.21	16.50	F 0.59	16.21	16.79	F 0.58
- 7' Rt.							
+50	2.52	16.16	16.70	F 0.54	16.16	16.68	F 0.52
+75'	2.32	16.12	16.61	F 0.49	16.12	16.58	F 0.46
153 ~	2.16	15.48	16.52	F 1.04	15.48	16.47	F 0.99
+25'	2.07	15.09	16.42	F 1.33	15.09	16.37	F 1.28
+50	2.05	15.20	16.33	F 1.13	15.20	16.26	F 1.06
+75'	2.01	15.00	16.23	F 1.23	15.00	16.15	F 1.15
154 ~	2.16	14.49	16.14	F 1.65	14.49	16.04	F 1.55
w. cb. Tang							

W. curb. Stakes - 3 BK.  
 See P. 24 - for S.

151~	17.07	16. <sup>04</sup> <sub>88</sub>	C 0.16
+50	16.72	16. <sup>72</sup> <sub>44</sub>	C 0.28
152-	16.21	16. <sup>21</sup> <sub>16</sub>	C 0.05
+50	15.94	15. <sup>98</sup> <sub>92</sub>	C 0.06
153-	15.84	15. <sup>88</sup> <sub>68</sub>	C 0.20
+50	15.54	15. <sup>54</sup> <sub>44</sub>	C 0.10
154~	15.37	15. <sup>37</sup> <sub>19</sub>	C 0.18
+50	15.34	14. <sup>34</sup> <sub>98</sub>	C 0.39
+75	15.02	14. <sup>50</sup> <sub>83</sub>	C 0.19
155~		14.71	
+25	14.89	14. <sup>89</sup> <sub>60</sub>	C 0.29
+50	14.60	14. <sup>60</sup> <sub>49</sub>	C 0.11
156~	14.45	14. <sup>45</sup> <sub>24</sub>	C 0.21
+50	13.80	13.97	F 0.17
157-	13.52	13. <sup>52</sup> <sub>67</sub>	F 0.15
+50	13.30	13.36	F 0.06
158~	12.55	13. <sup>55</sup> <sub>05</sub>	F 0.50
+50	12.36	12. <sup>36</sup> <sub>74</sub>	F 0.38
159~	12.35	12. <sup>35</sup> <sub>44</sub>	F 0.09
+50	11.88	12. <sup>88</sup> <sub>13</sub>	F 0.25.



160~	12.01	<sup>2</sup> 11.82 <sup>01</sup>	C 0.19	166+50 F 0.15	12.10	11.95	<del>12.04</del> <sub>15</sub>	F 0.09	
+50	11.62	<sup>62</sup> 11.55 <sup>62</sup>	C 0.07	167~	F 0.20	12.24	12.04	<del>12.20</del> <sub>04</sub>	F 0.16
161~	11.06	11.33	F 0.27	+50		12.43	12.37 <sup>+2</sup>	C 0.06	
+25	<del>10.84</del> 9.84	<sup>06</sup> 11.24 <sup>06</sup>	F 0.40	+75		12.46	12.44	C 0.02	
+50	<del>10.24</del> 10.25	<sup>84</sup> 11.16 <sup>84</sup>	F 0.92	168~		12.48	12.49	F 0.01	
+75	<del>10.59</del> 9.00	<sup>24</sup> 11.12 <sup>24</sup>	F 0.53	+25		12.45	12.51 <sub>45</sub>	F 0.06	
162~	<del>10.64</del> 9.43	<sup>89</sup> 11.10 <sup>89</sup>	F 0.42	+50		12.58	12.52	C 0.06	
+25	<del>10.71</del> 9.86	<sup>68</sup> 11.12 <sup>68</sup>	F 0.41	+75		12.59	12.51	C 0.08	
+50	<del>10.57</del> 10.54	<sup>71</sup> 11.15 <sup>71</sup>	F 0.58	169~		12.46	12.47	F 0.01	
+75	<del>10.82</del>	<sup>57</sup> 11.18 <sup>57</sup>	F 0.36	+25		12.25	12.41 <sub>25</sub>	F 0.16	
163~	<del>10.99</del>	<sup>82</sup> 11.22 <sup>82</sup>	F 0.23	+50		12.15	12.34 <sub>15</sub>	F 0.19	
+25	11.21	<sup>99</sup> 11.26 <sup>99</sup>	F 0.05	170~		12.19	12.16	C 0.03	
+50	11.26	11.30	F 0.04	+50		2.02	<sup>21</sup> 11.99 <sup>21</sup>	C 0.03	
+75	11.19	<sup>21</sup> 11.35 <sup>21</sup>	F 0.16	171~		11.89	11.81	C 0.08	
164~	11.15	11.42	F 0.27	+50		11.77	11.64 <sup>22</sup>	C 0.13	
+50	F 0.12	11.56	11.44	11.40	C 0.04	172~	11.43	11.46	F 0.03
165~	F 0.19	11.70	11.51	11.56	F 0.05	+50	11.09	11.29	F 0.20
+50	F 0.24	11.83	11.59	11.72	F 0.13	173~	11.23	11.11 <sup>23</sup>	C 0.12
166~	F 0.32	11.97	11.65	11.88	F 0.23	+50	10.97	10.94	C 0.03

Cont.

174~	10.89	10.76 <sup>89</sup>	C 0.13	182~	10.43	10.83 <sub>43</sub>	F 0.40
+50	10.54	10.59	F 0.05	+50	11.08	11.13 <sub>8</sub>	F 0.05
175~	10.35	10.41	F 0.06	183~	11.26	11.43 <sub>26</sub>	F 0.17
+50	10.24	10.24	G	+50	11.62	11.73 <sub>62</sub>	F 0.11
176~	10.05	10.06	F 0.01	184~	12.13	12.02 <sub>13</sub>	C 0.11
+50	9.90	9.89	C 0.01	+50	12.64	12.36 <sub>64</sub>	C 0.28
177~	9.85	9.71 <sup>85</sup>	C 0.14	185~	12.33	12.69 <sub>33</sub>	F 0.36
+50	10.02	9.56 <sup>02</sup>	C 0.46	+50	12.56	13.03 <sub>56</sub>	F 0.47
178~	9.57	9.44 <sup>57</sup>	C 0.13	186~	13.75	13.36 <sub>75</sub>	C 0.39
+50	9.46	9.32 <sup>46</sup>	C 0.14	+50	13.65	13.70	F 0.05
+75	9.04	9.31 <sub>04</sub>	F 0.27	187~	14.24	14.04 <sup>24</sup>	C 0.20
179~	9.17	9.37 <sub>17</sub>	F 0.20	+50	14.30	14.38	F 0.08
+25	9.18	9.43 <sub>18</sub>	F 0.25	188~	15.17	14.71 <sup>517</sup>	C 0.46
+50	9.30	9.49 <sub>30</sub>	F 0.19	+50	15.26	15.05 <sub>26</sub>	C 0.21
+75	9.56	9.55 <sup>56</sup>	C 0.01	189~	14.85	15.39 <sub>85</sub>	F 0.53
180~	9.70	9.64 <sup>70</sup>	C 0.06	+50	15.68	15.72 <sub>68</sub>	F 0.04
+50	9.89	9.86	C 0.03	190	16.14	16.06 <sub>14</sub>	C 0.08
181~	10.04	10.16 <sub>04</sub>	F 0.12	+50	16.15	16.43 <sub>15</sub>	F 0.28
+50	10.35	10.49 <sub>35</sub>	F 0.14	191~	16.56	16.88 <sub>56</sub>	F 0.32

Cont. on P. 29

Begin Island B-2 Curbs - 164+00

Cont. on P. 27 = To S.

W

E.

164 -		12.37	12.25 <sup>37</sup> C 0.12	12.37	12.15	
+50		12.34	12.41 <sub>34</sub> F 0.07		12.31 <sup>34</sup>	C 0.03
165 ~	5' Rt	12.04	12.57 <sub>04</sub> F 0.53	11.75	12.47 <sup>251=59</sup> <sub>75</sub>	F 0.72
Dist. -# to Lt. 190 +						
+25	3.83 Rt.	12.24	12.59 <sub>24</sub> F 0.35			
+50	0.33 Rt.	12.59	12.61 F 0.02	12.00	12.63	F 0.63
+75	4.29 Lt.	12.38	12.64 <sub>38</sub> F 0.26			
166 -	7.83 "	12.46	12.66 <sub>46</sub> F 0.20	12.11	12.79 <sub>11</sub>	F 0.68
+25	9 "	12.26	12.69 <sub>26</sub> F 0.43			
+50	wide "	12.23	12.77 <sub>23</sub> F 0.54	12.45	12.95	F 0.50
167 ~	"	12.68	12.93 <sub>68</sub> F 0.85	12.38	13.11 <sub>38</sub>	F 0.73
+50	"	12.58	13.10 <sub>58</sub> F 0.52	12.49	13.28 <sub>49</sub>	F 0.79
+75	"	12.84	13.17 <sub>84</sub> F 0.33	12.57	13.35 <sub>57</sub>	F 0.78
168 ~	9' Lt.	12.84	13.22 <sub>84</sub> F 0.38	12.59	13.40 <sub>59</sub>	F 0.81
+25	8.56 "	13.00	13.24 F 0.24	12.86	13.42 <sub>86</sub>	F 0.56
+50	7.25 Lt.	13.26	13.21 C 0.05	12.86	13.43 <sub>86</sub>	F 0.57
+75	5.50	13.12	13.18 F 0.06	12.91	13.42 <sub>91</sub>	F 0.51
169 ~	3.75	13.35	13.15 <sup>35</sup> C 0.20	12.63	13.38 <sub>63</sub>	F 0.75
+25	2.00	13.13	13.12 C 0.01	12.59	13.32 <sub>59</sub>	F 0.73
+50	0.25 Lt.	13.06	13.09 F 0.03	12.47	13.25 <sub>47</sub>	F 0.78
+75	1.50 Rt.	13.05	13.07 F 0.02			

## Island curbs.

17

W

E.

wide

170 - 3.25 RT	12.90	13.06 <sub>90</sub>	F 0.16		12.66	13.07 <sub>66</sub>	F 0.41
+25 - 4.56"	12.84	13.03 <sub>84</sub>	F 0.19				
+50 = 5 RT.	12.68	13.00 <sub>68</sub>	F 0.32		12.08	12.90 <sub>08</sub>	F 0.82
171 -	12.53	12.82 <sub>53</sub>	F 0.29		12.35	12.72 <sub>35</sub>	F 0.37
+50	12.55	12.65	F 0.60		12.08	12.55 <sub>08</sub>	F 0.47
+60	12.00	12.62	F 0.62		12.17	12.52 <sub>17</sub>	F 0.35
+70 = 1 Rad. E.	11.64	12.53 <sub>64</sub>	F 0.89	11.64	<del>11.98</del>	12.48 <sub>64</sub>	F 0.84
Milton							
172 +50 = 1 Rad E	10.68	12.25 <sub>68</sub>	F 1.57		10.68	12.20 <sub>68</sub>	F 1.52
+60	11.69	12.26 <sub>69</sub>	F 0.57		11.64	12.16 <sub>64</sub>	F 0.52
173 -	11.48	12.12 <sub>48</sub>	F 0.64		11.44	12.02 <sub>44</sub>	F 0.58
+50	11.24	11.95 <sub>24</sub>	F 0.71		11.19	11.85 <sub>19</sub>	F 0.66
174 -	11.11	11.77 <sub>11</sub>	F 0.66		11.02	11.67 <sub>02</sub>	F 0.65
+35 3.5 RT + E	11.38	11.65 <sub>38</sub>	F 0.27	+50	10.80	11.50 <sub>80</sub>	F 0.70
+60 3.25 RT	11.38	11.50 <sub>38</sub>	F 0.12	175 -	10.74	11.32 <sub>74</sub>	F 0.58
+85 2 H	11.46	11.34 <sub>46</sub>	C 0.12	+50	10.44	11.15 <sub>44</sub>	F 0.71
175 +10 7.25	10.99	11.18 <sub>99</sub>	F 0.19	176 -	10.23	10.97 <sub>23</sub>	F 0.74
+35 9	10.19	11.02 <sub>19</sub>	F 0.83				
+55 8.12 H	10.31	10.95 <sub>31</sub>	F 0.64				

## Island Curbs

18

	wide		W.		E.	
175+75	5.50	Lt.	10.72	10.95 <sub>72</sub>	F 0.23	
+95	1.12	Lt.	10.47	10.96 <sub>47</sub>	F 0.49	
176+15 = R. 1	8' Rt.		9.29	10.97 <sub>929</sub>	F 1.68	9.29 10.92 <sub>929</sub> F 1.63
176+80 = 1	E. Rad.		10.12	10.74 <sub>12</sub>	F 0.62	10.12 10.69 <sub>12</sub> F 0.57
+90			10.08	10.75 <sub>08</sub>	F 0.67	10.08 10.65 <sub>08</sub> F 0.57
177~			9.98	10.72 <sub>98</sub>	F 0.74	9.98 10.62 <sub>98</sub> F 0.64
+50			9.57	10.57	F 1.00	9.57 10.47 <sub>57</sub> F 0.90
178~			9.41	10.47 <sub>41</sub>	F 1.06	9.41 10.37 <sub>41</sub> F 0.96
+25			9.46	10.44 <sub>46</sub>	F 0.98	9.46 10.34 <sub>46</sub> F 0.88
+50			9.41	10.43 <sub>41</sub>	F 1.02	9.41 10.33 <sub>41</sub> F 0.92
177+75			9.23	10.43	F 1.20	9.23 10.33 <sub>23</sub> F 1.10
179~			9.39	10.44 <sub>39</sub>	F 1.05	9.39 10.34 <sub>39</sub> F 0.95
+25			9.45	10.46 <sub>45</sub>	F 1.01	9.45 10.36 <sub>45</sub> F 0.91
+50			9.46	10.50 <sub>46</sub>	F 1.04	9.46 10.40 <sub>46</sub> F 0.94
+75			9.63	10.56 <sub>63</sub>	F 0.93	9.63 10.46 <sub>63</sub> F 0.83
180~			9.62	10.65 <sub>62</sub>	F 1.03	9.62 10.55 <sub>62</sub> F 0.93
+30			9.57	10.77 <sub>57</sub>	F 1.20	9.57 10.67 <sub>57</sub> F 1.10
+40 = 1	E. Rad.		9.63	10.77 <sub>63</sub>	F 1.14	9.63 10.72 <sub>63</sub> F 1.09

Req. at	182+50	Lt. cb. is .12 lower Than Rt.	W.	Island curbs.	E.	19
181+20 = 1 <sup>w.</sup> Rad.	✓ 9.90	11.32 <sub>90</sub>	F 1.42	9.90	11.27 <sub>990</sub>	F 1.37
+30	✓ 9.89	11.40 <sub>89</sub>	F 1.51	9.89	11.30 <sub>89</sub>	F 1.41
+50	✓ 10.02	11.50 <sub>02</sub>	F 1.48	10.02	11.45 <sub>02</sub>	F 1.43
182 -	10.23	11.86 <sub>023</sub>	F 1.63	10.23	11.86 <sub>023</sub>	F 1.63
+50	10.24	12.22 <sub>024</sub>	F 1.98	10.24	12.28 <sub>024</sub>	F 2.04
183 -	10.97	12.58 <sub>097</sub>	F 1.61	10.97	12.70 <sub>097</sub>	F 1.73
+50	11.91	13.00 <sub>091</sub>	F 1.09	11.91	13.12 <sub>091</sub>	F 1.21
184 -	12.58	13.39 <sub>258</sub>	F 0.81	12.58	13.51 <sub>258</sub>	F 0.93
+50	12.76	13.75 <sub>276</sub>	F 1.00	12.75	13.87 <sub>275</sub>	F 1.12
+70	13.08	13.89 <sub>08</sub>	F 0.81	13.08	14.01 <sub>08</sub>	F 0.93
+80 - 1 <sup>Rt.</sup>	13.19	14.01 <sub>319</sub>	F 0.82	13.19	14.07 <sub>319</sub>	F 0.88
Jellette					14.59	
185+60 = 1 <sup>Lt.</sup>	13.49	14.49 <sub>349</sub>	F 1.00	13.49	14.55 <sub>349</sub>	F 1.06
+70	13.53	14.56 <sub>353</sub>	F 1.03	13.53	14.68 <sub>353</sub>	F 1.15
186 -	13.69	14.76 <sub>369</sub>	F 1.07	13.69	14.88 <sub>369</sub>	F 1.19
+50	14.08	15.09 <sub>408</sub>	F 1.01	14.08	15.21 <sub>408</sub>	F 1.13
187 -	14.42	15.42 <sub>442</sub>	F 1.01	14.42	15.55 <sub>442</sub>	F 1.13
+50	14.95	15.77 <sub>495</sub>	F 0.82	14.95	15.89 <sub>495</sub>	F 0.94
188 -	15.28	16.10 <sub>528</sub>	F 0.82	15.28	16.22 <sub>528</sub>	F 0.94
Cont. P. 31						

Curbs - S.E. Cor. Morena + Clairemont

= 191 + 31.62 = P.O.C.  $\pm$  - Rad.

		Top cb	
B.C. = 0+00	17.68	18.63 <sub>7 68</sub>	F 0.95
+25	18.35	18.56 <sub>35</sub>	F 0.21
+50	17.97	18.43 <sub>7 97</sub>	F 0.46
+75	18.40	18.43 = Inlet	
1+00 = P.C.C.	19.34	18.88 <sub>9 34</sub>	C 0.46
+25.92	19.96	19.77 <sub>9 6</sub>	C 0.19
+51.84	21.32	21.06 <sub>32</sub>	C 0.26
+77.76	22.85	22.74 <sub>85</sub>	C 0.11
2+03.68	24.98	24.76 <sub>98</sub>	C 0.22
+29.60	27.69	26.91 <sub>7 69</sub>	C 0.78
+55.53 = P.C.C.	29.28	28.78 <sub>9 28</sub>	C 0.50
2+85.37	30.70	30.63 <sub>70</sub>	C 0.07
3+15.21 = E.C.	32.18 = Top	32.25	
= Mect.			

3' Bk.

P. 7 for Return				140 + 75	7.99	8.31	F 0.32
				141 -	7.60	8.48 <sup>99</sup>	F 0.88
136 + 43.54 = P.C.	4.47	5.07 <sup>+47</sup>	F 0.60	+ 25	7.98	8.65 <sup>15</sup>	F 0.67
+ 75	5.13	5.20 <sup>13</sup>	F 0.07	+ 50	8.95	8.84	C 0.11
137 -	5.22	5.32	F 0.10	+ 75	8.81	9.08 <sup>81</sup>	F 0.27
+ 25	5.45	5.45	G	142 -	9.62	9.37 <sup>62</sup>	C 0.25
+ 50	5.67	5.59 <sup>67</sup>	C 0.08	+ 25	9.51	9.69 <sup>51</sup>	F 0.18
+ 75	5.84	5.74 <sup>84</sup>	C 0.10	+ 50	10.29	10.08 <sup>29</sup>	C 0.21
138 -	5.93	5.91	C 0.02	+ 75	11.06	10.48 <sup>06</sup>	C 0.58
+ 25	6.39	6.09 <sup>39</sup>	C 0.30	143 -	11.62	10.87 <sup>62</sup>	C 0.75
+ 50	6.59	6.28 <sup>59</sup>	C 0.31	+ 25	11.68	11.29 <sup>68</sup>	C 0.41
+ 75	6.86	6.48 <sup>86</sup>	C 0.38	+ 50	12.11	11.67 <sup>11</sup>	C 0.44
139 -	6.60	6.70	F 0.10	+ 75	12.14	12.07 <sup>14</sup>	C 0.07
+ 25	7.14	6.93 <sup>14</sup>	C 0.21	144 -	12.57	12.47 <sup>57</sup>	C 0.10
+ 50	7.22	7.17 <sup>22</sup>	C 0.05	+ 25	12.39	12.86 <sup>39</sup>	F 0.47
+ 75	7.06	7.43 <sup>06</sup>	F 0.37	+ 50	13.45	13.22 <sup>45</sup>	C 0.23
140 -	7.57	7.68 <sup>57</sup>	F 0.11	+ 75	13.46	13.57 <sup>46</sup>	F 0.11
+ 25	7.93	7.91 <sup>93</sup>	C 0.02	145 -	13.98	13.90	C 0.08
+ 50	8.21	8.12 <sup>21</sup>	C 0.09	+ 25	14.44	14.20 <sup>44</sup>	C 0.24



"H" curb- E. Side

22

17.19 = B.M. -  
S.E. Pole Asher

145 + 50	14.95	14.95 <sup>95</sup>	C 0.47	150 + 25 = inlet		15.98 <sup>✓</sup>	
+ 75	15.38	14.74 <sup>38</sup>	C 0.64	+ 34 = P.C.	16.80	15.99 <sup>80</sup>	C 0.81
146 ~	15.62	14.98 <sup>62</sup>	C 0.64	1/2	16.74	16.12 <sup>74</sup>	C 0.62
+ 25	15.50	15.21 <sup>50</sup>	C 0.29	3/4	17.54	16.36 <sup>54</sup>	C 1.18
+ 50	15.58	15.40 <sup>58</sup>	C 0.18	E.C.	17.80	16.70 <sup>80</sup>	C 1.10
+ 75	15.78	15.58 <sup>78</sup>	C 0.20	See Below for NE Cor.	15.50	15.69 <sup>50</sup>	F 0.19
				+ 50	15.67		F 0.07
147 ~	15.71	15.74	F 0.03	+ 75	15.71	15.64 <sup>71</sup>	C 0.07
+ 25	16.07	15.88 <sup>07</sup>	C 0.19	152 ~	15.45	15.58 <sup>45</sup>	F 0.13
+ 50	16.00	15.99	C 0.01	+ 25	15.45	15.52 <sup>50</sup>	F 0.07
+ 75	15.92	16.08 <sup>92</sup>	F 0.16	+ 50	15.17	15.46 <sup>92</sup>	F 0.29
148 ~	15.71	16.16 <sup>71</sup>	F 0.45	+ 75 ✓	15.20	15.41 <sup>71</sup>	F 0.21
+ 25	15.84	16.21 <sup>84</sup>	F 0.37	153 ~	15.26	15.41 <sup>84</sup>	F 0.05
+ 50	15.80	16.24 <sup>80</sup>	F 0.44	+ 25	15.21	15.35 <sup>80</sup>	F 0.14
+ 75	16.42	16.25 <sup>42</sup>	C 0.17	+ 50	15.13	15.29 <sup>42</sup>	F 0.16
149 ~	17.39	16.24 <sup>39</sup>	C 1.15	+ 75	14.93	15.23 <sup>39</sup>	F 0.30
+ 25	16.28	16.28 <sup>28</sup>	C 0.07	154 ~	15.01	15.18 <sup>28</sup>	F 0.17
+ 50	16.28	16.16 <sup>28</sup>	C 0.12	Ret. - Asher.	15.10	15.12	F 0.02
+ 75	16.62	16.10 <sup>62</sup>	C 0.52	P.C. = 151 + 26	15.69	15.75 <sup>69</sup>	F 0.06
150 ~	16.42	16.04 <sup>42</sup>	C 0.38	1/3	15.75	15.79	F 0.04
				2/3	15.73	15.86 <sup>73</sup>	F 0.13
				E.C.	15.94	15.95	F 0.01

Cont. from P. 17  
 "H" Curb on W.

23

139 +25'	7.24	6. <sup>24</sup> <sub>93</sub>	C 0.31	144 +25'	16.34	16. <sup>70</sup> <sub>39</sub>	F 0.36
+50	7.47	7. <sup>47</sup> <sub>19</sub>	C 0.28	+50	16.94	17. <sup>06</sup> <sub>94</sub>	F 0.12
+75'	7.90	7. <sup>90</sup> <sub>51</sub>	C 0.39	+75'	17.40	17.41	F 0.01
140 -	8.18	7. <sup>18</sup> <sub>89</sub>	C 0.29	145 ~	17.91	17. <sup>91</sup> <sub>74</sub>	C 0.17
+25'	8.54	8. <sup>54</sup> <sub>33</sub>	C 0.21	+25'	18.18	18. <sup>18</sup> <sub>04</sub>	C 0.14
+50	8.89	8. <sup>89</sup> <sub>82</sub>	C 0.07	+50	18.79	18. <sup>79</sup> <sub>32</sub>	C 0.47
+75'	9.38	9. <sup>38</sup> <sub>32</sub>	C 0.06	+75'	19.20	18. <sup>20</sup> <sub>58</sub>	C 0.62
141 ~	10.10	9. <sup>10</sup> <sub>83</sub>	C 0.27	146 -	19.45	18. <sup>45</sup> <sub>92</sub>	C 0.63
+25'	10.54	10. <sup>54</sup> <sub>35</sub>	C 0.19	+25'	19.41	19. <sup>41</sup> <sub>05</sub>	C 0.36
+50	11.27	10. <sup>27</sup> <sub>89</sub>	C 0.38	+50	19.54	19. <sup>54</sup> <sub>24</sub>	C 0.30
+75'	11.70	11. <sup>70</sup> <sub>44</sub>	C 0.26	+75'	19.59	19. <sup>59</sup> <sub>42</sub>	C 0.17
142 ~	12.22	12.00	C 0.22	147 ~	19.50	19. <sup>50</sup> <sub>58</sub>	F 0.08
+25'	12.78	12. <sup>78</sup> <sub>57</sub>	C 0.21	+25'	18.61	19. <sup>61</sup> <sub>70</sub>	F 1.09
+50	13.44	13. <sup>44</sup> <sub>15</sub>	C 0.29	+50	18.43	19. <sup>43</sup> <sub>78</sub>	F 1.35
+75'	13.85	13. <sup>85</sup> <sub>74</sub>	C 0.11	+75'	18.77	19. <sup>77</sup> <sub>78</sub>	F 1.01
143 ~	14.29	14. <sup>29</sup> <sub>33</sub>	F 0.04	148 ~	19.17	19. <sup>17</sup> <sub>72</sub>	F 0.55
+25'	14.75	14. <sup>75</sup> <sub>90</sub>	F 0.15	+25'	19.29	19. <sup>29</sup> <sub>60</sub>	F 0.31
+50	15.02	15. <sup>02</sup> <sub>42</sub>	F 0.40	+50	18.77	19. <sup>77</sup> <sub>44</sub>	F 0.67
+75'	15.42	15. <sup>42</sup> <sub>89</sub>	F 0.47	+75'	19.17	19. <sup>17</sup> <sub>26</sub>	F 0.09
144 -	15.73	16. <sup>73</sup> <sub>31</sub>	F 0.58	149 ~	19.12	19. <sup>12</sup> <sub>06</sub>	C 0.06

149 + 25'	18.93	18.84 <sup>93</sup>	C 0.09
+ 50	18.66	18.60	C 0.06
+ 75'	18.24	18.33 <sub>24</sub>	F 0.09
150 ~	17.97	18.04 <sup>97</sup>	F 0.07
+ 25'	17.72	17.75'	F 0.03
+ 50	17.50	17.45'	C 0.05
+ 75'	17.21	17.26	C 0.05
151 ~ - See P. 13	17.07	16.88	C 0.16

Cont. from P. 8

25

## B-2 Island Curve - Bridge - N.

H = W.

R = E.

121 + 37.4 = Meet E	11.16	11.14		10.94	10.91	
+50	11.07	11.09	F 0.02	11.07	10.85 <sup>07</sup>	C 0.22
+75	10.70	10.98	F 0.28	10.70	10.74	F 0.07
122 ~	10.50	10.87 <sub>50</sub>	F 0.37	10.50	10.63	F 0.13
+25	10.45	10.75 <sub>45</sub>	F 0.30	10.45	10.51	F 0.06
+50	10.48	10.64 <sub>48</sub>	F 0.16	10.48	10.40	C 0.08
+75	10.49	10.53 <sub>49</sub>	F 0.04	10.49	10.29	C 0.20
123 ~	10.18	10.41 <sub>18</sub>	F 0.23	10.18	10.17	C 0.01
+25	10.10	10.30 <sub>10</sub>	F 0.20	10.10	10.06	C 0.04
+50	9.77	10.19 <sub>77</sub>	F 0.42	9.77	9.95 <sub>77</sub>	F 0.18
+75	9.64	10.07 <sub>64</sub>	F 0.43	9.64	9.83 <sub>64</sub>	F 0.19
124 ~	9.84	9.96 <sub>84</sub>	F 0.12	9.84	9.72 <sub>84</sub>	C 0.12
+25	9.78	9.84 <sub>78</sub>	F 0.06	9.78	9.60	C 0.18
+50	9.76	9.72	C 0.04	9.76	9.50	C 0.26
+75	9.42	9.61 <sub>42</sub>	F 0.19	9.42	9.39	C 0.03
125 ~ 2'	9.08	9.48 <sub>08</sub>	F 0.40	9.08	9.28	F 0.20
+25 2.08	9.18	9.36 <sub>18</sub>	F 0.18	9.18	9.18	G
+50 - See P. 8	9.06	9.23 <sub>06</sub>	F 0.17	9.06	9.07	F 0.01

"H" Curbs - N. of Bridge - Weeks.  
Cont. from P. 6

	H. - W.			Rt. - E.	
121+24.4			Meet.	9.38	9.36
+50				9.17	9.18 F 0.01
+52.08 = Meet.	13.37	13.33			
+75	13.29	13.29 <sup>29</sup>	C 0.15	9.12	8.99 <sup>12</sup> C 0.13
122 -	13.06	12.96 <sup>3</sup>	C 0.10	8.90	8.89 C 0.03
+25	12.90	12.84 <sup>9</sup>	C 0.06	8.70	8.76 F 0.06
+50	12.62	12.73 <sup>62</sup>	F 0.11	8.74	8.64 C 0.10
+75	12.18	12.62 <sup>18</sup>	F 0.44	8.71	8.53 <sup>71</sup> C 0.18
123 -	12.11	12.50 <sup>11</sup>	F 0.39	8.57	8.42 <sup>57</sup> C 0.15
+25	11.95	12.39 <sup>95</sup>	F 0.44	8.33	8.30 C 0.03
+50	11.78	12.28 <sup>78</sup>	F 0.50	8.37	8.19 <sup>37</sup> C 0.18
+75	11.64	12.16 <sup>64</sup>	F 0.52	8.44	8.07 <sup>44</sup> C 0.37
124 -	11.85	12.05 <sup>85</sup>	F 0.20	8.08	7.96 <sup>08</sup> C 0.12
+25	11.60	11.91 <sup>60</sup>	F 0.31	7.72	7.87 <sup>72</sup> F 0.15
+50	11.50	11.73 <sup>50</sup>	F 0.23	7.74	7.83 <sup>74</sup> F 0.09
+75	11.15	11.50 <sup>15</sup>	F 0.35	8.02	7.84 <sup>15</sup> C 0.18
125 -	11.13	11.22 <sup>13</sup>	F 0.09	8.02	7.88 <sup>02</sup> C 0.14
+25	10.81	10.92 <sup>81</sup>	F 0.11	7.95	7.95 G
+50 - See P. 6	9.75	10.62 <sup>75</sup>	F 0.87	8.18	8.02 <sup>18</sup> C 0.16

Island Curb. - B-2 - 154+00 - N.

27

	2' Bk. Stake	E. cb. Top of cb. Grade	+ .10 for W. cb.						
154+25		14.37	15.94 + .57	F 1.57	1' Lt. 161+10 = 1' Rad.	10.67	12.25 + .05 0.67 + .10	F 1.58	1.63
+50		14.11	15.83 + .11	F 1.72	+20	11.14	12.17	F 1.03	1.13
+75		14.08	15.73 + .58	F 1.65	+50	11.42	12.07 + .42	F 0.65	
155 ~		13.99	15.62 + .99	F 1.63	+75	11.45	12.01 + .45	F 0.56	
+25		13.89	15.51 + .89	F 1.62	162 ~	11.31	11.97	F 0.66	
+35 = 1' Rad.		13.81	15.47 + .81	F 1.66	+25	11.62	11.94 + .31	F 0.32	
Littlefield					+40	11.67	11.93 + .05	F 0.26	
156+17 = 1' Rad.		13.55	15.10 + .55	F 1.55	= 1' Rt. +50 = 1' Rad.	11.49	11.93 + .49	F 0.44	0.49
+27		14.10	15.01 + .10	F 0.91	Napiev 1' Lt.				
+50		13.88	14.88 + .88	F 1.00	163+30 = 1' Rad.	10.72	12.01 + .05 0.72	F 1.29	1.34
157 ~		13.86	14.58 + .86	F 0.72	+40	10.90	12.00 + .90	F 1.10	1.20
+50		13.59	14.27 + .59	F 0.68	+75	11.78	12.07 + .37	F 0.29	F 0.39
158 ~		13.30	13.94 + .30	F 0.66	164 - See P. 16	12.37	12.15	F 0.22	0.12
+50		12.95	13.66 + .95	F 0.71					
159 ~		13.13	13.35 + .13	F 0.22					
+50		12.36	13.04 + .36	F 0.68					
160 ~		11.98	12.73 + .98	F 0.75					
+20		11.69	12.62 + .69	F 0.93					
+30 = 1' Rad.		11.43	12.56 + .43	F 1.13					1.18
Ashton			1.43						

H cb. on E. N. of Jelletta

28

186 + 58.80 = end cb.	6.58	16.63	
+ 75	16.61	16.73	F 0.12
187 ~	17.53	16.88 <sup>50</sup>	C 0.65
+ 25	17.90	17.04 <sup>90</sup>	C 0.86
+ 50 = from E	17.80	17.20 <sup>80</sup>	C 0.60
+ 75 = on Tang.	17.69	17.36 <sup>69</sup>	C 0.33
188 ~	17.77	17.54 <sup>77</sup>	C 0.23
25.15 = Dist.			
+ 25	18.22	17.72 <sup>22</sup>	C 0.50
+ 50	18.66	17.90 <sup>66</sup>	C 0.76
+ 75	19.18	18.09 <sup>18</sup>	C 1.09
189 ~	18.16	18.29 <sup>16</sup>	F 0.13
+ 25	17.58	18.49 <sup>58</sup>	F 0.91
+ 50	17.76	18.65 <sup>76</sup>	F 0.89
+ 75	17.68	18.78 <sup>68</sup>	F 1.10
190 ~	17.55	18.85 <sup>55</sup>	F 1.30
+ 25	17.74	18.83 <sup>74</sup>	F 1.09
+ 50	18.13	18.80 <sup>13</sup>	F 0.67
+ 75	18.13	18.76 <sup>13</sup>	F 0.63
191 ~	18.29	18.71 <sup>29</sup>	F 0.42
+ 25	18.47	18.66 <sup>47</sup>	F 0.19

'H' curbs on W. - Jollette  
Cont. from P. 15

29

191+50	17.28 17.41 <sub>28</sub>	F 0.13
192~	18.04 18.01	C 0.03
+50	18.79 18.65 <sup>79</sup>	C 0.14
193~	19.34 19.29 <sup>34</sup>	C 0.05
+50	19.80 19.93	F 0.13
194~	20.53 20.57	F 0.04
+50	21.22 21.21	C 0.01
195~	22.00 21.85 <sup>2.00</sup>	C 0.15
+25=end	22.43 22.17 <sup>43</sup>	C 0.26



## Curbs - N.E. Cor. Clairemont + Morena

30

Meet cb = 2+16.3	27.54	27. <sup>57</sup> 49	
2+00	26.80	26.85	F 0.05
1+75	25.67	25. <sup>67</sup> 85	F 0.18
+50	24.34	25. <sup>4</sup> 05	F 0.71
<sup>0+00 on curve</sup> 1+26.10 =	24.15	24. <sup>15</sup> 44	F 0.29
0+22.24	23.78	23. <sup>78</sup> 84	F 0.06
+44.48	23.22	23.26	F 0.04
+66.72	22.92	22.89	C 0.03
+88.96	Top	22.84	
1+11.21 = PCC	23.61	23. <sup>61</sup> 13	C 0.48
1+42.59 = end cb.	23.68	23. <sup>68</sup> 91	F 0.23

Cont. from P. 19

Island Corbs. Jéllette - N.

Lt.

188+50	14.98	16.44 4.98	F 1.46
189 ~	15.24	16.76 5.24	F 1.52
+05 = Cross	16.02	16.79 6.02	F 0.77
+15 = 1' Rt.	15.50	16.94 5.50	F 1.44

Inqulf

189+80 = 1' Lt.	15.68	17.31 5.68	F 1.63
+90 = 1' Lt.	15.88	17.38 5.88	F 1.50
190 ~	15.86	17.45 8.6	F 1.59
+50	16.42	17.82 6.42	F 1.40
191 ~	16.76	18.27 6.76	F 1.51
+50	17.08	18.80 7.08	F 1.72
192	17.45	19.40 7.45	F 1.95
+50	17.96	20.04 7.96	F 2.08
+80	18.81	20.42 8.81	F 1.61
+90 = 1' Rt.	19.21	20.61 9.21	F 1.40

Clairemont

193+90 = 1' Lt.	20.26	21.84 0.26	F 1.58
194 -	20.40	21.96 0.40	F 1.56
+50 = inlet	22.29	22.60 2.29	F 0.31

Lt. cb. 15 .12 lower than Rt.

Rt.

31

14.98	16.56 4.98	F 1.58
15.24	16.88 5.24	F 1.64
16.02	16.91 6.02	F 0.89
15.50	17.00 5.50	F 1.50

15.68	17.37 5.68	F 1.69
15.88	17.50 5.88	F 1.62
15.86	17.57 5.86	F 1.71
16.42	17.94 6.42	F 1.52
16.76	18.39 6.76	F 1.63
17.08	18.92 7.08	F 1.84
17.45	19.52 7.45	F 2.07
17.96	20.16 7.96	F 2.20
18.81	20.54 8.81	F 1.73
19.21	20.67 9.21	F 1.46

20.26	21.90 0.26	F 1.64
20.40	22.08 0.40	F 1.68
22.29	22.72 2.29	F 0.43

Island cb. - Clairemount

32

Lt.

Rt.

195 + 00	21.72	23.24 <sub>1.72</sub>	F 1.52	7'	21.72	23.36 <sub>1.72</sub>	F 1.64
+25	22.16	23.56 <sub>2.16</sub>	F 1.40	7'	22.16	23.68 <sub>2.16</sub>	F 1.52
+37.5 - 3.25 Rt. 2' Bk	22.37	23.67 <sub>2.37</sub>	F 1.30				
+50 2' Lt. "	22.35	23.67 <sub>2.35</sub>	F 1.32	7'-2'	22.59	24.00 <sub>2.59</sub>	F 1.41
+62.5 7.25 Lt. "	22.46	23.67 <sub>2.46</sub>	F 1.21	8.31 Rt. - 2' Bk	22.83	24.14 <sub>2.83</sub>	F 1.31
+75 9' Lt. "	22.50	23.78 <sub>2.50</sub>	F 1.28	6.25 Rt. - 2' Bk	22.98	24.24 <sub>2.98</sub>	F 1.26
+87.5 7.75 Lt. "	22.68	23.98 <sub>2.68</sub>	F 1.30	2.81 Rt.	23.00	24.29 <sub>3.00</sub>	F 1.29
196 + 00 = 1' Rad. 3' Lt.	22.93	24.25 <sub>2.93</sub>	F 1.32		22.93	24.31 <sub>2.93</sub>	F 1.38

End cb. = BC		Meet					
				-3+25	20.35	20.56 <sub>35</sub>	F 0.21
# 1	13.51	14.59	F 1.08	-3+57.41 = PC.	20.49	21.02 <sub>49</sub>	F 0.53
2	14.36	14.66	F 0.30	End.	20.55	21.17 <sub>55</sub>	F 0.62
3	14.40	14.72	F 0.32	Cushman			
= 4+15.70	14.29	14.79	F 0.50				
4 = E.C. 4+00	14.37	14.85	F 0.48	End.	21.30	21.50 <sub>30</sub>	F 0.20
+50	14.23	15.12	F 0.89	-3+99.73 = PC.	21.25	21.52 <sub>25</sub>	F 0.27
3 ~	14.59	15.52	F 0.93	-4+36.61 = Bk = +10+71.52 - Ah.	21.71	21.78 <sub>71</sub>	F 0.07
+50	15.15	15.98 <sub>15</sub>	F 0.83	11+00	22.12	21.88 <sub>12</sub>	C 0.24
2 ~	15.39	16.42 <sub>39</sub>	F 1.03	+50	22.23	22.08 <sub>23</sub>	C 0.15
+50	16.13	16.87 <sub>13</sub>	F 0.74	11+79.34 = PC	22.05	22.21 <sub>05</sub>	F 0.16
1 ~	17.50	17.32 <sub>50</sub>	C 0.18	1	22.07	22.34 <sub>07</sub>	F 0.27
+50	16.97	17.77 <sub>97</sub>	F 0.80	2	22.30	22.49 <sub>30</sub>	F 0.19
Both ways 0+00	16.71	18.16 <sub>71</sub>	F 1.45	3	22.49	22.64 <sub>49</sub>	F 0.15
- +50	17.27	18.48 <sub>27</sub>	F 1.21	4	22.69	22.76 <sub>69</sub>	F 0.07
- 1+00	18.09	18.73 <sub>09</sub>	F 0.64	5 = E.C. = End.	22.86	22.87	F 0.01
- +50	18.26	18.96 <sub>26</sub>	F 0.70	Naples Place			
- 2+00	19.17	19.24 <sub>17</sub>	F 0.07				
- +50	19.11	19.64 <sub>11</sub>	F 0.53				
- 3+00	20.10	20.21 <sub>10</sub>	F 0.11				

Bed. "H" on N. Side Morena - Naples Pl.

11+69.86 = Bcg.	23.75	23.43 <sup>75</sup>	C 0.32	16+50	20.78	20.40 <sup>78</sup>	C 0.38
12 -	23.25	23.32 <sup>25</sup>	F 0.07	17 -	19.27	20.00 <sup>27</sup>	F 0.73
+50	22.59	23.14 <sup>59</sup>	F 0.55	+50	19.75	19.60 <sup>75</sup>	C 0.15
13 -	22.46	22.98 <sup>46</sup>	F 0.52	18 -	19.18	19.20	F 0.02
+50	22.69	22.73 <sup>69</sup>	F 0.04	+50	19.06	18.84 <sup>06</sup>	C 0.22
14 -	22.42	22.40	C 0.02	+81.87 = B.C.	18.41	18.67 <sup>41</sup>	F 0.26
+50	22.43	22.00	C 0.43	19+00	18.29	18.52 <sup>29</sup>	F 0.23
14+88.40 = P.C.	22.10	21.69 <sup>10</sup>	C 0.41	+25	18.96	18.41 <sup>96</sup>	C 0.45
1/4	22.10	21.66 <sup>10</sup>	C 0.44	+50	19.14	18.34 <sup>14</sup>	C 0.80
1/2	22.09	21.68 <sup>09</sup>	C 0.41	+ = P.C. 4 Rad	17.21	18.27 <sup>09</sup>	F 1.06
3/4	22.19	21.74 <sup>19</sup>	C 0.45	EC. = Dorcas	17.21	18.23 <sup>19</sup>	F 1.02
end = EC.	22.27	21.85 <sup>27</sup>	C 0.42	End. = E.	17.13	18.19 <sup>27</sup>	F 1.06
Buenos				Dorcas			
End = EC.	20.60	21.50	F 0.90	End = W.	17.44	18.30 <sup>60</sup>	F 0.76
1/4	22.77	21.38 <sup>77</sup>	C 1.39	+ = P.C. 4 Rad	17.37	18.41 <sup>77</sup>	F 1.04
1/2	21.93	21.26 <sup>93</sup>	C 0.67	20+25	18.88	18.45 <sup>93</sup>	C 0.43
3/4	21.03	21.16 <sup>03</sup>	F 0.13	+26.62 = EC.			
PC = 15+68.40	20.88	21.06 <sup>88</sup>	F 0.18				
16 -	21.09	20.80 <sup>09</sup>	C 0.29				

Cont. on P. 59

GRADES ELY SIDE OF MORENA  
BLVD LISTER TO JELWETT

Rough Lt  
Curb Curb

Stamp  
Blint  
Stuckey  
Wentworth  
8-7-57

RT 35  
Rough  
Curb

NOTE: Grades for drain @ NE Cor. Curb  
Napier & Morena; Thence Nly.  
250' are in G-385

+75						9.85	
+50				Fo.36	9.59	9.95 59	CO <sup>10</sup> 10.85 9.95
+25						10.04	
177				Co.19	10.32	10.13 <sup>32</sup>	CO <sup>24</sup> 10.37 10.13
ROC Pt. 11.79'	= End.			Exist	10.42	10.46	
P.O.C. 4 = 22°30'22" = 1/2					10.99	10.26 <sup>99</sup>	Co.73
11.78'							
+90.20 = EC. N.E. Cb. Ref. Lister St. Cb. R = 30' $\Delta = 90^\circ 01' 30''$ $L = 47.14'$				Fo.47	9.69	10.16 9.69	10.16
(Cont'd 5/9 P. 55)							
176 + 42.20 = E Lister St							
B.M.		12.64		High Pt. on Rock Curbing Front of Bernies Chalet			

L+

E.

R+

Curb

36  
Rough  
Curb

MORENA BLVD

+25

9.61

179

F0.36

9.19

9.55

1002

9.55

Top inlet

9.60

+75

9.56

+50

F0.35

9.27

9.62

939

9.62

+25

9.63

178

F0.14

9.62

9.76

10.04

9.76

Lt

E

Rt

MORENA BLVD

Curb

37  
Rough  
CurbP.C.  $\Delta = 44^{\circ}59'34''$  = end cb.

C0.05

10.20

10.15

11.78

P.O.C.  $\Delta = 22^{\circ}29'37''$  1/2

C0.10

10.15

10.05

11.78

Cb. R = 30'  $\Delta = 89^{\circ}58'30''$   
+34.13 = B.C. SE Cb. Ret Home St.  
33

C0.11

10.07

10.07  
9.9610.33  
9.96C0<sup>37</sup>

+25

9.92

180

C0.01

9.83

9.82

10.36  
9.82C0<sup>34</sup>

+75

9.73

+50

P0.17

9.50

9.67  
53

9.67

C0<sup>32</sup>



L+

E

R+

Curb

38  
Rough  
Curb

MORENA BLVD

+75

11.14

181+50

C0.01

10.84

10.83

C0.71

11.54

10.83

POC.  $\beta = 45^{\circ}00'45''$  (North) = end

C0.24

10.66

10.42<sup>66</sup>

11.78'

POC.  $\beta = 22^{\circ}30'22'' = 1/2$ 

C0.61

11.11

10.50<sup>11</sup>

11.78'

Cb. R = 30'  $\beta = 90^{\circ}01'30''$ 

181+30.73 = E.C. NE Ch. Ref Kane St.

33

C0.17

10.84

10.67<sup>84</sup>C0.60  
11.27  
10.67180+82.73 = Kane St  
33

MORENA BLVD

Lt

E

Rt

curb

39  
Rough  
Curb

B.M.

12.79

"X" in NE Cor. Conc. base  
of RR. 519. 5 W. Sellett & N...

183+57.35 = Meet.

d = .42365583

R = 4057.24' T = 540.40 L = 1074.46

183+15.50 = B.C. Lt. A = 15°10' 24.6"

183

+75

+50

+25

182

8.81  
67  
9.48

12.89  
67  
13.56

12.87  
67  
13.54

12.83  
67  
13.50

11.70  
4.93  
16.63  
5.45  
11.18

74  
3.27  
41

70  
18  
52

14+05.5

13+68

13+05

16.63  
5.90  
10.73

12+35.5

1.95

6.12  
6.17

8.0

12.23  
1196

89 FO.27  
14  
8 | 75.0  
   .094

16.14  
   .094  
-----  
16.234  
16.328  
   .094

12.62  
   .40

-----  
13.02

13.42  
   .24

-----  
13.66

   .56

-----  
14.22

16.422  
16.516  
   .094

-----  
16.610

16.704  
   .094

-----  
16.798

16.892

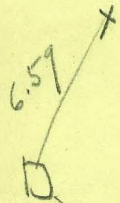
1248

   521

-----  
1769 Hi.

   593

-----  
1196



5.06

MORENA BLVD

Lt

±

Rt

Curb

39  
Rough  
Curb

B.M.

12.79

"X" in NE Cor. Conc. base  
of RR. 59. SW. Jellott & Morena

13.73 ✓

C / 95

15.12

13.17

13.17  
12

F 0.05

13.12

183 + 57.35 = Meet.

d = .42365583

R = 4057.24 T = 540.40 L = 1074.46

183 + 15.50 = B.C. Lt. A = 15° 10' 24.6"

183

F 0.05

12.90

12.95

C / 70

14.65

12.95

+75

12.59

+50

F 0.13

12.10

12.23

F 0.15

12.08

12.23

10

+25

11.86

182

F 0.75

1074

11.49

C 0.93

12.42

11.49

0.74

GRADES ELY SIDE OF MORENA  
 NLY FROM STA. 154+13.86

Lt

8-9-57

Stamper  
 Bluff  
 Stuckey  
 Wentworth

Rt

Curb  
 40  
 Rough  
 Curb

P.O.C. # =

Meet.

15.19

15.14

12.01'

P.O.C. # =

F 0.24

14.68

14.92  
 64

12.01'

Cb. R = 27'

155+06.34 = B.C. S.E. Cb. Ret. Littlefield

Top inlet

14.92

14.86  
 2' 11"

CO 17

15.03  
 14.86  
 2' 11"

+75

F 0.08

14.87

14.95  
 87

+50

F 0.24

14.76

15.00  
 4 76

FO 07

1493  
 15.00  
 2' 11"

+25

F 0.25

14.81

15.06  
 4 81

CO 29

39  
 15.10

154+13.86

B.M.

12.00

Chisler SE Cor. Conc. base RR. Signal - 85' Lt @  
 156+40 Littlefield St.

MORENA BLVD

LT

E

RT

Curb

(41)  
Rough  
Curb

(235)

+50

C 0.20

14.38

<sup>38</sup>  
14.18

<sup>1653</sup>  
14.18

156+25

14.30

Meet.

15.09 ✓

E.C.  $\Delta = 62^{\circ}28'$

C 0.02

15.04

15.02

10.83

P.O.C.  $\Delta = 41^{\circ}38'40''$

C 0.08

14.80

<sup>80</sup>  
14.72

10.83'

P.O.C.  $\Delta = 20^{\circ}49'20''$

F 0.05

14.45

14.50  
<sub>45</sub>

10.83'

Cb. R =  $30' \Delta = 62^{\circ}28' L = 32.49$   
 $156 + 09.76 = E.C. NE Cb. Ret.$   
Lilfield st

C 0.26

14.63

<sup>63</sup>  
14.37

(201)

<sup>1638</sup>  
14.37

MORENA BLVD

Lt

E

Rt curb

Rough  
Curb

(2)

(289)

158

C0.37

13.73

73  
13.36

1625  
13.36

+75

13.50

(239)

+50

C0.49

14.13

413  
13.64

1603  
13.64

+25

13.77

(251)

157

C0.49

14.40

440  
13.91

1640  
13.91

+75

14.04

MORENA BLVD

48

+50

Alley & R. = N. Side

+4'

B.C. Alley

± Alley = 159 + 02.22  
Cb. R = 6'

159 + 18<sup>22</sup> ± = E.C. NE Alley Ret

159

Alley & R. = S. Side

+4'

E.C. Alley

+75  
Cb. R = 6'

+86<sup>22</sup> ± = B.C. SE Alley Ret

158

+50

+25

20.15  
67  
20.82

20.45  
67  
21.12

20

20.78  
67  
21.45

20.80  
67  
21.47

20.53  
67  
21.50

20.78  
67  
21.45

20.67  
67  
21.34

20.51  
67  
21.18

23  
Rough  
b32  
56



$$\begin{array}{r} 20.15 \\ 67 \\ \hline 20.82 \end{array}$$

$$\begin{array}{r} 20.45 \\ 67 \\ \hline 21.12 \end{array}$$

20

$$\begin{array}{r} 20.78 \\ 67 \\ \hline 21.45 \end{array}$$

$$\begin{array}{r} 20.80 \\ 67 \\ \hline 21.47 \end{array}$$

$$\begin{array}{r} 20.53 \\ 67 \\ \hline 21.50 \end{array}$$

$$\begin{array}{r} 20.78 \\ 67 \\ \hline 21.45 \end{array}$$

$$\begin{array}{r} 20.67 \\ 67 \\ \hline 21.34 \end{array}$$

$$\begin{array}{r} 20.51 \\ 67 \\ \hline 21.18 \end{array}$$

$$\begin{array}{r} 6.60 \\ 67 \\ \hline 7.27 \end{array}$$

$$\begin{array}{r} 8.31 \\ 67 \\ \hline 18.98 \end{array}$$

$$\begin{array}{r} 9.16 \\ 67 \\ \hline 4.91 \end{array}$$

$$\begin{array}{r} 20.81 \\ 67 \\ \hline 21.54 \end{array}$$

$$\begin{array}{r} 21.64 \\ 67 \\ \hline 22.31 \end{array}$$

$$\begin{array}{r} 22.25 \\ 67 \\ \hline 22.92 \end{array}$$

$$\begin{array}{r} 22.67 \\ 67 \\ \hline 23.34 \end{array}$$

$$\begin{array}{r} 22.92 \\ 67 \\ \hline 23.59 \end{array}$$

$$\begin{array}{r} 22.72 \\ 67 \\ \hline 23.39 \end{array}$$

$$\begin{array}{r} 22.60 \\ 67 \\ \hline 23.27 \end{array}$$

$$\begin{array}{r} 22.07 \\ 67 \\ \hline 22.74 \end{array}$$

$$\begin{array}{r} 21.89 \\ 67 \\ \hline 22.56 \end{array}$$

$$\begin{array}{r} 21.53 \\ 67 \\ \hline 22.20 \end{array}$$

$$\begin{array}{r} 21.17 \\ 67 \\ \hline 21.84 \end{array}$$

$$\begin{array}{r} 20.81 \\ 67 \\ \hline 21.48 \end{array}$$

$$\begin{array}{r} 20.45 \\ 67 \\ \hline 21.12 \end{array}$$

$$\begin{array}{r} 20.09 \\ 67 \\ \hline 20.76 \end{array}$$

$$\begin{array}{r} 19.73 \\ 67 \\ \hline 20.40 \end{array}$$

$$\begin{array}{r} 19.37 \\ 67 \\ \hline 20.04 \end{array}$$

$$\begin{array}{r} 18.65 \\ 67 \\ \hline 19.32 \end{array}$$

$$\begin{array}{r} 18.29 \\ 67 \\ \hline 18.96 \end{array}$$

$$\begin{array}{r} 17.93 \\ 67 \\ \hline 18.60 \end{array}$$

$$\begin{array}{r} 17.74 \\ 67 \\ \hline 18.45 \end{array}$$

$$\begin{array}{r} 9.43 \\ 75 \\ \hline 8.68 \end{array}$$

$$\begin{array}{r} 9.14 \\ 75 \\ \hline 8.39 \end{array}$$

$$\begin{array}{r} 9.23 \\ 75 \\ \hline 8.48 \end{array}$$

$$\begin{array}{r} 8.86 \\ 75 \\ \hline 8.11 \end{array}$$

$$\begin{array}{r} 8.8 \\ 75 \\ \hline 8.13 \end{array}$$

$$\begin{array}{r} 8.61 \\ 75 \\ \hline 7.86 \end{array}$$

$$\begin{array}{r} 8.63 \\ 75 \\ \hline 7.88 \end{array}$$

$$\begin{array}{r} 8.38 \\ 75 \\ \hline 7.63 \end{array}$$

$$\begin{array}{r} 8.16 \\ 75 \\ \hline 7.41 \end{array}$$

$$\begin{array}{r} 8.27 \\ 75 \\ \hline 7.52 \end{array}$$

$$\begin{array}{r} 7.97 \\ 75 \\ \hline 7.22 \end{array}$$

$$\begin{array}{r} 8.15 \\ 75 \\ \hline 7.40 \end{array}$$

$$\begin{array}{r} 7.79 \\ 75 \\ \hline 7.04 \end{array}$$

$$\begin{array}{r} 7.62 \\ 75 \\ \hline 6.87 \end{array}$$

$$\begin{array}{r} 7.99 \\ 75 \\ \hline 7.24 \end{array}$$

$$\begin{array}{r} 7.80 \\ 75 \\ \hline 7.05 \end{array}$$

$$\begin{array}{r} 7.59 \\ 75 \\ \hline 6.84 \end{array}$$

MORENA BLVD

Lt

±

Rt

curb

Rough  
Curb  
CO<sup>32</sup>  
12.86  
12.54  
4' in

+50

CO.25

12.79

12.54<sup>79</sup>

Alley & R.

= N. Side

CO.10

13.04

12.94<sup>04</sup>

+4'

B.C. Alley

CO.26

13.12

12.86<sup>12</sup>

± Alley = 159 + 02.22

CB. R = 6'

159 + 18.22 ± = E.C. NE Alley Ret

CO.24

12.95

12.71<sup>95</sup>

CO<sup>35</sup>  
13.16  
12.81

159

Alley & R.

= S. Side

CO.74

13.79

13.05<sup>79</sup>

+4'

E.C. Alley

CO.08

13.05

12.97<sup>05</sup>

+75

CB R = 6'

+86.22 ± = B.C. SE Alley Ret

CO.02

12.91

12.89<sup>91</sup>

C313

58

+50

CO.18

13.27

13.09<sup>27</sup>

16.22  
13.09

+25

13.22

MORENA BLVD

LT

±

RT

Curb

④  
Rough  
Curb

EC. 4 = 89°58'30" = Meet.

12.36 12.38

11.77'

POC 4 = 67°28'52" = 3/4

C 0.14

12.30 12.16<sup>30</sup>

11.78'

POC 4 = 44°59'15" 1/2

C 0.16

12.25 12.09<sup>25</sup>

11.78

POC 4 = 22°29'37" 1/4

C 0.02

12.15 12.13

11.78'

Top 12.15

cb. R = 30' 4 = 89°58'30" L = 47.11'  
160 + 14.52 = B.C. SE cb. Ashford  
.05

F 0.17

12.01 12.18

C 0.25  
12.43  
12.18  
4'in.

160 + 00

C 0.14

12.40 12.26<sup>40</sup>

+75

12.40

MORENA BLVD

Lt

E

Rt

Corb

(45)  
ROUGH  
CORB

B.P. 11.118

Top Inlet 11.44

+50

F 0.21

11.24

11.45  
24

FO<sup>15</sup>  
11.30  
11.45

Ashton  
BC  $\angle = 90^{\circ} 01' 30'' = \text{Meet.}$

F 0.21 12.07

12.28  
27

12.22

11.79'

POC  $\angle = 67^{\circ} 31' 07'' = 3/4$

F 0.61

11.32

11.93  
32

11.78'

POC  $\angle = 45^{\circ} 00' 45'' = 1/2$

F 0.01

11.70

11.71

11.79'

POC  $\angle = 22^{\circ} 30' 22'' = 1/4$

F 0.39

11.18

11.57  
18

11.78'

cb. R = 30.  $\angle = 90^{\circ} 01' 30'' L = 47.14'$   
161 + 30.55 = E.C. NE Ch. Ret Ashton

F 0.77

10.73  
11.14

11.50  
0.73

FO<sup>20</sup>  
11.30  
11.50

MORENA BLVD

Lt

E

Rt

Curb

Ⓟ  
Rough  
Curb

Cont. P. 47

11.77'

POC  $\phi = 67^{\circ}28'52''$   $\frac{3}{4}$

F 0.11 11.51 11.62  
51

11.78

POC  $\phi = 44^{\circ}59'15''$   $\frac{1}{2}$

F 0.20 11.18 11.38  
1.18

11.78

POC  $\phi = 22^{\circ}29'37''$   $\frac{1}{4}$

F 0.31 10.93 11.24  
0.93

11.78'

cb.  $R = 30' \phi = 89^{\circ}58'30'' L = 47.11'$   
+ 34.00 = BC. SE Ch Ref Napier St.

Top Inlet 11.19  
on Inlet. 11.19

11.19 11.21

CO  $\frac{05}{1126}$   
11.21

162

F 0.15 11.16 11.31  
16

CO  $\frac{08}{1139}$   
11.31

+75

11.38

MORENA BLVD

Lt

±

Rt

Curb

④7  
Rough  
Curb

Napier  
B.C.  $\angle = 90^{\circ}01'30''$  = Meet.

F 0.04 11.87 11.91  
87

11.79'

P.O.C.  $\angle = 67^{\circ}31'07''$   $\frac{3}{4}$

F 0.05 11.62 11.67  
62

11.78'

P.O.C.  $\angle = 45^{\circ}00'45''$   $\frac{1}{2}$

C 0.21 11.74 11.53  
74

11.79'

Top Inlet: 11.45

P.O.C.  $\angle = 22^{\circ}30'22''$   $\frac{1}{4}$

F 0.03 11.45 11.48

11.78'

Ch. R =  $30'4'' = 90^{\circ}01'30''$  L = 47.14'  
163+50 = E.C. N.E. Ch. Ret Napier St.

7' Bk.

C 0.46 11.96 11.50  
96

EO 55  
1205  
11.50

EC  $\angle = 89^{\circ}58'30''$  = End = Meet - S. Ret.

✓ 11.90 11.90

11.77



Cont. P. 46

MORENA BLVD

2+

±

Rt

Curb

②  
Rough  
Curb

Alley & R. - S. side

F 0.19 11.84 12.03  
1.84

+4'

E.C. Alley

F 0.03 11.92 11.95

Ch. R = 6'  
164 + 46' = BC. SE Alley Ret

C 0.10 11.91 11.81<sup>91</sup>

+25

11.74

164

C 0.25 11.91 11.66<sup>91</sup> 12.09  
11.66

+75

11.58



MORENA BLVD

Lt

±

Rt

curb

<sup>49</sup>  
Rough  
Curb

+50

C 0.57

12.71

12.14

FD<sup>69</sup>

11.50

12.14

165

C 0.57

12.55

<sup>255</sup>  
11.98

FD<sup>14</sup>

11.84  
11.98

Alley & ~~±~~ = N. side

F 0.25

11.84

12.09  
1.84

+4'

C 0.17

12.18

<sup>18</sup>  
12.01

B.G. Alley

Ch. R = 6'  
164 + 78' = E.G. NE Alley Ret

C 0.35

12.26

<sup>226</sup>  
11.91

-164 + 62.13 = ~~±~~ Alley

+50

11.82

CO<sup>08</sup>

11.90

11.82

MORENA BLVD

Lt

t

Rt Curb

Rough  
Curb

168

C0.01

12.92

12.91

C0<sup>93</sup>

13.84

12.91

+75

12.86

+50

C0.01

12.80

12.79

C1<sup>58</sup>

14.37

12.79

167

C0.02

12.64

12.62

C0<sup>30</sup>

92

12.62

+50

F0.39

12.09

12.46

F0<sup>59</sup>

11.87

12.46

166

F0.09

12.22

12.30

F0<sup>56</sup>

11.74

12.30

22

MORENA BLVD

Lt

E

Rt

Curb

⑤  
Rough  
Curb

+50

F 0.04

12.72

12.76

FD 08

268

12.76

72

+25

12.83

169

C 0.03

12.92

12.89

CO 14

1303

12.89

+75

12.93

+50

G

12.94

12.94

FO 09

1285

12.94

+25

12.93

MORENA BLVD

Lt

E

Rt

Curb

53  
Rough  
Curb

POC  $\Delta = 22^\circ 29' 37'' = 1/4$

F 0.10 11.91 12.01  
1.91

11.78

11.97

CO<sup>30</sup>

Ch. R = 30'  $\Delta = 89^\circ 58' 30''$  L = 47.11  
+ 62.13 = BC. SEC. R. of Milton St.

F 0.29 11.73 12.02  
1.73

1232  
12.02

+50<sup>v</sup>

F 0.10 11.96 12.06  
1.96 12.06

CO<sup>24</sup>

171

F 0.27 11.96 32 12.47  
CO. 0.29 ~~12.32~~ 12.23 12.23

+50

C 0.07 12.48 48 12.41  
51 12.41

CO<sup>10</sup>

170

C 0.15 17.73 73 12.58  
12.58

CO<sup>18</sup>

MORENA BLVD

Lt

E

Rt

Curb

Rough  
Curb <sup>(53)</sup>

P.P.  
POC  $\angle = 45^{\circ} 00' 45''$  End:

Exist

11.99

12.03

11.79

POC  $\angle = 22^{\circ} 30' 22'' = 1/2$

11.29

11.78  
29

Fo. 49

11.78'

Ch. R = 30'  $\angle = 90^{\circ} 01' 30''$  L = 47.14'  
172 + 62.13 = E.C. NE. Ch. Ret. Milton St.

Fo. 82

10.85

11.67  
0.85

C053

12.20

11.67

E.C.  $\angle = 89^{\circ} 58' 30'' =$  Meet.

12.43 ✓

11.77'

POC  $\angle = 67^{\circ} 28' 52'' = 3/4$

Fo. 19

12.06

12.20  
<sup>43</sup>  
<sub>01</sub>

11.78'

POC  $\angle = 44^{\circ} 59' 15'' = 1/2$

GT

12.05

12.05

11.78'

MORENA BLVD

L+

E

Rt

curb

(59)  
Rough  
curb

+50

Fo. 37

10.29

10.66  
29

FO<sup>32</sup>  
1034  
10.66

175

Fo. 06

10.77

10.83  
77

CO<sup>91</sup>  
1174  
10.83

+50

Fo. 50

10.51

11.01  
0.51

CO<sup>54</sup>  
1155  
11.01

174

Fo. 47

10.71

11.18  
0.71

CO<sup>48</sup>  
1166  
11.18

+50

Fo. 40

10.96

11.36  
0.96

CO<sup>42</sup>  
1178  
11.36

173

Fo. 53

11.00

11.53

CO<sup>69</sup>  
1222  
11.53

MORENA BLVD

Lt

E

Rt

Curb

Right  
Curb

(55)

B.M.

12.64

(see pg. 35)

N.E. Ret - Jelllette

P.C. = Jelllette = on Inlet.

16.36

1/4

15.98

15.98

G

1/2

15.40

15.87

F 0.47

3/4

16.02

15.91<sup>02</sup>

C 0.11

= Meet.

15.91

E.C. - Exist. cb

15.98

15.99

(Contd N14 P9 35)

P.O.C.  $\phi = 44^{\circ} 59' 15'' = \text{end}$

Meet.

10.50

10.52

11.78

P.O.C.  $\phi = 22^{\circ} 29' 37'' = 1/2$

10.45

10.51

11.78'

cb. R = 30'  $\phi = 89^{\circ} 58' 30'' L = 47.11'$

175 + 94.20 = B.C. SE cb Ref Lister St.

F 0.30

10.14

10.50

C 0.13

1063

10.50

14

## Beg. curb. Stakes - Sly. Side of Morena - Knoxville - W.

56

P.K.s - 5' out. - Cb. Moved Back 2'

End cb. - 3' Bk	8.95	9.62 <sub>95</sub>	F 0.67	43 ~	5.63	6.49 <sub>63</sub>	F 0.86
1/2 - 3' Bk 20' R.	8.87	9.72 <sub>87</sub>	F 0.85	+50	5.45	6.27 <sub>45</sub>	F 0.82
35 + 38.21 = P.C.	9.21	9.82 <sub>21</sub>	F 0.61	44 ~	5.29	6.06 <sub>29</sub>	F 0.77
+50	9.26	9.85 <sub>26</sub>	F 0.59	+50	5.12	5.76 <sub>12</sub>	F 0.64
36 ~	9.41	10.05 <sub>41</sub>	F 0.64	45 ~	4.54	5.37 <sub>45</sub>	F 0.83
+50	9.60	10.26 <sub>60</sub>	F 0.66				
37 ~	9.85	10.46 <sub>85</sub>	F 0.61				
+50	9.95	10.67 <sub>95</sub>	F 0.72				
38 ~	10.03	10.88 <sub>03</sub>	F 0.85				
+25 r.p.	10.11	10.91 <sub>11</sub>	F 0.80				
+50	10.01	10.80 <sub>01</sub>	F 0.79				
39 ~	9.41	10.26 <sub>41</sub>	F 0.85				
+50	8.80	9.66 <sub>80</sub>	F 0.86				
40 ~	8.22	9.07 <sub>22</sub>	F 0.85				
+50	7.64	8.48 <sub>64</sub>	F 0.84				
41 ~	7.02	7.88 <sub>02</sub>	F 0.86				
+50	6.54	7.36 <sub>54</sub>	F 0.82				
42 ~	6.15	6.98 <sub>15</sub>	F 0.83				
+50	5.87	6.71 <sub>87</sub>	F 0.84				



Curb stakes - Nly. Side Morena - Knoxville - W.

Cont. on P. 60

7.40  
7.57  
56  
8.13

57

Knoxville

End. cb.	8.71	9.12 <sub>71</sub>	F 0.41	40+25	7.90	8.13	F 0.23
1/2 15' Rad.	9.28	9.27 <sub>07</sub>	C 0.21	R=15' +52.19=PC.	7.28	7.57 <sub>28</sub>	F 0.29
35+35.31=PC.	9.22	9.10 <sub>22</sub>	C 0.12	Nashville Meet. 7.40			
+50	9.21	9.19 <sub>21</sub>	C 0.02	7.34			
36~	9.07	9.49 <sub>07</sub>	F 0.42	Frankfort			
+50	9.15	9.78 <sub>15</sub>	F 0.63	44+08.41=PC=Meat.	5.41		
37-	9.12	10.07 <sub>12</sub>	F 0.95	+50	4.89	5.14 <sub>89</sub>	F 0.26
+50	8.66	10.37 <sub>66</sub>	F 1.71	45~	4.92	4.95	F 0.03
R=15 +62.13=PC.	8.68	10.44 <sub>68</sub>	F 1.76	+25	5.10	4.84 <sub>10</sub>	C 0.26
1/2	8.66	10.37 <sub>66</sub>	F 1.71	+50 = F inlet.	4.71	4.74	
End. = NL.	8.84	10.20 <sub>84</sub>	F 1.36	Inlet = w. "		4.71 = Top	
Lehigh							
End = NL.	9.35	10.43 <sub>35</sub>	F 1.08	45+97.56=PC=Meat	4.66		
1/2	9.27	10.63 <sub>27</sub>	F 1.36				
PC = 38+28.13	9.13	10.72 <sub>13</sub>	F 1.59				
+50	7.80	10.59 <sub>80</sub>	F 2.79				
39~	7.85	9.93 <sub>85</sub>	F 2.08				
+50	8.61	9.21 <sub>61</sub>	F 0.60				
40~	8.31	8.49 <sub>31</sub>	F 0.18				

10 + 62.67 = N. end inlet	.59	20.57	
11 ~	20.78	20.82	F 0.04
+ 50	20.70	21.12 <sub>10</sub>	F 0.42
12 ~	21.24	21.35 <sub>24</sub>	F 0.11
+ 38.89 = B.C.	20.57	21.45 <sub>57</sub>	F 0.88
+ 50	20.55	21.47 <sub>55</sub>	F 0.92
+ 75	20.70	21.50 <sub>70</sub>	F 0.80
13 ~	20.97	21.52 <sub>97</sub>	F 0.55
+ 25	20.80	21.49 <sub>80</sub>	F 0.69
+ 49.81 = E.C.	20.89	21.45 <sub>89</sub>	F 0.56
14 ~	21.59	21.34 <sub>59</sub>	C 0.25
+ 50	21.53	21.18 <sub>53</sub>	C 0.35
+ 75	21.54	21.10 <sub>54</sub>	C 0.44
20' R. + 88.40 = P.C.	21.53	21.06 <sub>53</sub>	C 0.47
1/4	21.66	21.07 <sub>66</sub>	C 0.59
1/2 on Inlet	21.07	21.12 <sub>84</sub>	
3/4	21.84	21.21 <sub>84</sub>	C 0.63
E.C.	21.90	21.35 <sub>90</sub>	C 0.55

Buenos

cont. on P. 61

= 1' Rad.	...	w	E. cb.		
- 0 + 82.37	A	E.	18.75	19.65	F 0.90
				19.61	F 0.86
- 1 + 00			18.81	19.71	F 0.90
+ 25			18.86	19.79	F 0.93
+ 50			18.91	19.85	F 0.94
- 2 + 00			19.29	19.96	F 0.67
+ 50			19.56	20.12 <sub>56</sub>	F 0.56
- 3 + 00			19.82	20.46 <sub>82</sub>	F 0.64
+ 50			20.25	20.96 <sub>25</sub>	F 0.71
- 4 + 00			20.52	21.36 <sub>52</sub>	F 0.84
E.C. "B"					
+ 36.61 = opp			20.69	21.55 <sub>69</sub>	F 0.86
Beq. 2' Both ways - level.					
= 10 + 71.52 ahead.					
11 ~			20.48	21.67 <sub>48</sub>	F 1.19
+ 50			20.90	21.84 <sub>90</sub>	F 0.94
+ 69 = Taper			21.02	21.90 <sub>02</sub>	F 0.88
+ 79 = 1' Rad.			21.10	21.93 <sub>10</sub>	F 0.83

H' eb. - E. Side Morenci - Dorcas - W.

cont. from P. 34

27  
19  
46  
23

59

20 + 26.62 = E.C.	18.82	18.45	C 0.37	1/2 ?	22.49	23.23	F 0.74
+ 50	18.72	18.60	C 0.22	27 + 22.60 = P.C.	22.52	23.19	F 0.67
21 ~	18.71	18.96	F 0.25	+ 50	22.79	23.39	F 0.60
+ 50	18.74	19.32	F 0.58	+ 98.33 = P.C.	23.12	23.64	F 0.52
22 ~	19.40	19.68	F 0.28	28 -	23.16	23.65	F 0.49
+ 50	20.10	20.04	C 0.06	28 + 25'	23.24	23.59	F 0.35
23 -	20.55	20.40	C 0.15	+ 50	22.38	23.34	F 0.96
+ 50	20.44	20.76	C 0.32	+ 75'	22.55	22.92	F 0.37
24 ~	21.25	21.12	C 0.13	29 ~	22.48	22.31	C 0.17
+ 50	21.09	21.48	F 0.39	+ 25'	22.10	21.54	C 0.56
25 ~	21.56	21.84	F 0.28	+ 50	21.54	20.69	C 0.85
+ 50	22.04	22.20	F 0.16	+ 75'	19.00	19.83	F 0.83
26 ~	22.57	22.56	C 0.01	= E.C.	18.18	19.13	F 0.95
+ 25'	22.88	22.74	C 0.14	30 ~ not in		<del>18.98</del>	
+ 56.60 = P.C.	22.82	22.97	F 0.15	+ 50	16.70	17.27	F 0.57
1/2 ?	22.62	23.17	F 0.55	31 -	14.50	15.68	F 1.18
end	22.66	23.37	F 0.71	+ 50	12.99	14.45	F 1.46
Viola St.				+ 75'		<del>13.89</del>	
End.	22.87	23.27	F 0.40	= Bridge	13.78	13.77	

Nly Side Morena  
H cbs.

Bridge	12.35	12.31	
32+50 - Not in		11.79	
+68 = PC.	10.31	11.15	F 0.84
1/3	9.97	10.72	F 0.75
2/3	9.45	10.25	F 0.80
End.	9.34	9.95	F 0.61
Drive - 30'			
End.	9.44	9.45	F 0.01
1/3	8.89	9.37	F 0.48
2/3	8.93	9.32	F 0.39
33+38 = PC	9.10	9.23	F 0.13
+50	8.73	9.05	F 0.32
+75	8.63	8.79	F 0.16
+87 = PC	8.57	8.71	F 0.14
1/3 = inlet	8.60	8.63	F 0.03
2/3	8.57	8.62	F 0.25
End.	8.65	8.70	F 0.05
Drive = 30'			
End.	8.23	8.75	F 0.52

1/3	8.47	8.68	F 0.21
2/3	8.47	8.67	F 0.20
34+57 = PC.	8.36	8.71	F 0.35
34+65.31 = PC.	8.75	8.73	C 0.02
1/2	8.44	8.79	F 0.35
End.	8.47	8.88	F 0.41

Knoxville

Cont. from P. 57

Cont. from P. 58

"H" cb. Sly. + wly. Morena - Buenos - W.

61

E.C.	21.07	20.92 <sup>107</sup>	C 0.15	1/2	17.53	17.62 <sup>3</sup>	F 0.09
1/4	20.93	20.89 <sup>93</sup>	C 0.04	Wly. End.	17.52	17.58	F 0.06
1/2	20.90	20.87 <sup>90</sup>	C 0.03	Beq. 25' R. Naples.			
3/4	20.05	20.85 <sup>05</sup>	F 0.80	End - Naples.	17.50	17.30 <sup>50</sup>	C 0.20
PC = 15 + 68.40	19.65	20.82 <sup>965</sup>	F 1.17	1	17.50	17.42 <sup>50</sup>	C 0.08
16 ~	19.58	20.72 <sup>958</sup>	F 1.14	2	17.60	17.70	F 0.10
+50	19.65	20.57 <sup>965</sup>	F 0.92	3	17.89	18.11 <sup>89</sup>	F 0.22
17 ~	20.47	20.42	C 0.05	4	18.14	18.53 <sup>14</sup>	F 0.39
+50	20.27	20.27	G	5	18.44	18.76 <sup>44</sup>	F 0.32
18 ~	19.32	20.12 <sup>932</sup>	F 0.80	6 = PC = 20 + 61.50	18.53	18.80 <sup>53</sup>	F 0.27
+50	19.04	19.88 <sup>04</sup>	F 0.84	21 ~ = Inlet.	18.71/18.74		F 0.03
19 ~	18.84	19.58 <sup>84</sup>	F 0.74	+50	17.69/18.75		F 1.06
+25	18.71	19.30 <sup>71</sup>	F 0.59	22 ~	18.48/18.84		F 0.36
+49.54 = BC 15' R.	17.91	18.82 <sup>91</sup>	F 0.91	+50	18.79/18.98		F 0.19
1/2	18.05	18.46 <sup>05</sup>	F 0.41	23 ~	18.59/19.17		F 0.58
End = E.C.	17.28	18.15 <sup>28</sup>	F 0.87	+50	18.74/19.36		F 0.62
Dorcas				+98.33 = PC.	18.96/19.54		F 0.58
10' R on SW Cor.				1/2	19.48/19.55		F 0.07
sly. end	17.56	17.62	F 0.06	End	19.25/19.52		F 0.27
				Savannah			

H. cb. = wly. Morena.

62

Savannah

End = E.C. on Savannah	19.56	18.70	C0.86	30 ~	16.74	17.96	F 1.22
1/4	19.95	19.07	C0.91	+50	14.90	16.81	F 1.91
1/2	20.31 <sup>54</sup>	19.46	C0.85	31 ~	13.43	15.66 <sub>343</sub>	F 2.23
3/4	20.97 <sup>19</sup>	19.81	C0.66	+50	12.87	14.61 <sub>287</sub>	F 1.74
P.C. = 25 + 16.81	20.84	20.61	C0.83	+ = Bridge	14.03 <sup>5</sup>	14.01	
+50	20.67	20.14	C0.53	Bridge.	12.59	12.55	
26 -	20.15	20.33	F0.18	32 +50	10.84	12.09 <sub>684</sub>	F 1.25
+50	20.24	20.53	F0.29	+75	9.92	11.35 <sub>992</sub>	F 1.43
27 ~	20.60	20.73	C0.11	33 ~	9.18	10.70 <sub>918</sub>	F 1.52
+25	20.73	21.13	C0.32				
+50	20.76	20.89	C0.06	+25	8.60	10.20 <sub>860</sub>	F 1.60
+75	20.80	20.81	F0.01				
+98.33 = B.C.	20.71	20.75	F0.04	+50	8.23	9.82 <sub>823</sub>	F 1.59
28 -	20.71	20.74	F0.03	+75	8.20	9.57 <sub>820</sub>	F 1.37
+25	20.77	20.59 <sup>77</sup>	C0.18	34 -	8.34	9.44 <sub>834</sub>	F 1.10
+50	20.41	20.39 <sup>41</sup>	C0.02	+25 = inlet	8.05	9.42 <sub>805</sub>	F 1.37
+75	19.88	20.13 <sup>88</sup>	F0.25	+50	8.58	9.46 <sub>858</sub>	F 0.88
29 -	19.27	19.81	F0.54	+62.31 = P.C.	8.50	9.56 <sub>850</sub>	F 1.06
+25	18.64	19.43 <sup>64</sup>	F0.79	1/2	8.51	9.46 <sub>851</sub>	F 0.95
+50	17.94	18.98 <sup>94</sup>	F1.04	End	8.24	9.36 <sub>824</sub>	F 1.12
+64.25 = E.C.	17.82	18.77 <sup>82</sup>	F0.95				

Curb. Stakes w. Side - Sherman - South

63

1 Sherman E.C. = end at	13.43	14.46 <sub>3 43</sub>	F 1.03	9+50	14.50	14.24 <sup>50</sup>	C 0.26
3/4	14.09	14.64 <sub>0 9</sub>	F 0.55	+75	14.58	14.33 <sup>58</sup>	C 0.25
1/2	14.44	14.82 <sub>4 4</sub>	F 0.38	0 ~	14.38	14.34 <sup>38</sup>	C 0.04
1/4	13.82	15.00 <sub>3 82</sub>	F 1.18	+25	14.31	14.39 <sub>31</sub>	F 0.08
PC. = 5+54.79	13.88	15.17 <sub>3 88</sub>	F 1.29	+50	14.41	14.44 <sub>41</sub>	F 0.03
+75	13.96	15.19 <sub>3 96</sub>	F 1.23	+75	14.40	14.53 <sub>40</sub>	F 0.13
6 ~	14.93	15.17 <sub>9 3</sub>	F 0.24	+96.79 = EC.	14.00	14.70	F 0.70
+2756 = Bk +50.51 ah = BC.	15.06	15.15 <sub>0 6</sub>	F 0.09	11 ~	14.98	15.05 <sub>9 8</sub>	F 0.07
+75	15.00	15.11	F 0.11	+50	15.42	15.56 <sub>4 2</sub>	F 0.14
7 ~	14.89	15.04 <sub>8 9</sub>	F 0.15	+75	15.52	16.15 <sub>5 5 2</sub>	F 0.63
+25	15.02	14.99	C 0.03	12 ~	16.72	16.81 <sub>7 2</sub>	F 0.09
+50	15.07	14.93 <sub>0 7</sub>	C 0.14	+25	17.38	17.52 <sub>3 8</sub>	F 0.14
+75	14.92	14.87 <sub>9 2</sub>	C 0.05	+50	18.09	18.27 <sub>0 9</sub>	F 0.18
8 ~	14.90	14.81 <sub>9 0</sub>	C 0.09	+75	18.78	19.06 <sub>7 8</sub>	F 0.28
+25	14.76	14.75 <sub>7 6</sub>	C 0.01	13 ~	19.27	19.86 <sub>2 7</sub>	F 0.59
+50	14.87	14.69 <sub>8 7</sub>	C 0.18	+25	19.84	20.63 <sub>8 4</sub>	F 0.79
+75	14.71	14.63 <sub>7 1</sub>	C 0.08	+50	19.98	21.35 <sub>9 9 8</sub>	F 1.37
9 ~	14.66	14.52 <sub>6 6</sub>	C 0.14	+75	20.69	22.04 <sub>0 6 9</sub>	F 1.35
+25	14.38	14.19 <sub>3 8</sub>	C 0.15	14 ~	21.41	22.67 <sub>1 4 1</sub>	F 1.26

+ = Bridge

23.40 = Top.

Curb Stakes - Buenos

0+00 = Prop Line to E

E.

W.

0+04 = P.C. = E <sup>Top</sup> 27.09 27.15

+19 = P.C. - W. 27.14 26.85<sup>7 14</sup> C 0.29

+44 26.25 26.32<sup>3</sup> F 0.07

+69 25.34 25.73<sup>34</sup> F 0.39

+94 25.06 26.13<sup>5 06</sup> F 1.07

1+14.88 = PC <sup>10' Rad</sup> 24.78 24.67<sup>2 8</sup> C 0.11

end - S. at Alley 24.01 24.68<sup>0 1</sup> F 0.67

end - N. at Alley 23.96 24.30<sup>3 96</sup> F 0.34

+54.88 = PC. 23.65 23.76<sup>6 5</sup> F 0.11

1+75 23.21 22.89<sup>3 21</sup> C 0.32

2+00 22.86 22.69<sup>8 6</sup> C 0.17

+25 22.24 22.09<sup>2 4</sup> C 0.15

+55.22 = PC. <sup>20' Rad.</sup> 21.90 21.35<sup>9 0</sup> C 0.55

4' Rad. 1+20.88 = PC. 24.23 24.02<sup>2 3</sup> C 0.21

EC = 4' Rad. 24.23 24.06<sup>2 3</sup> C 0.18

end at Alley <sup>S</sup> 24.67 24.18<sup>6 7</sup> C 0.49

end at Alley <sup>N</sup> 24.50 23.70<sup>4 50</sup> C 0.80

EC = 4' Rad. 23.97 23.57<sup>9 7</sup> C 0.40

+48.88 = PC. 23.97 23.39<sup>9 7</sup> C 0.58

23.11 22.77<sup>3 11</sup> C 0.34

22.61 22.17<sup>6 1</sup> C 0.44

22.02 21.57<sup>2 0 2</sup> C 0.45

21.07 20.92<sup>1 0 7</sup> C 0.15





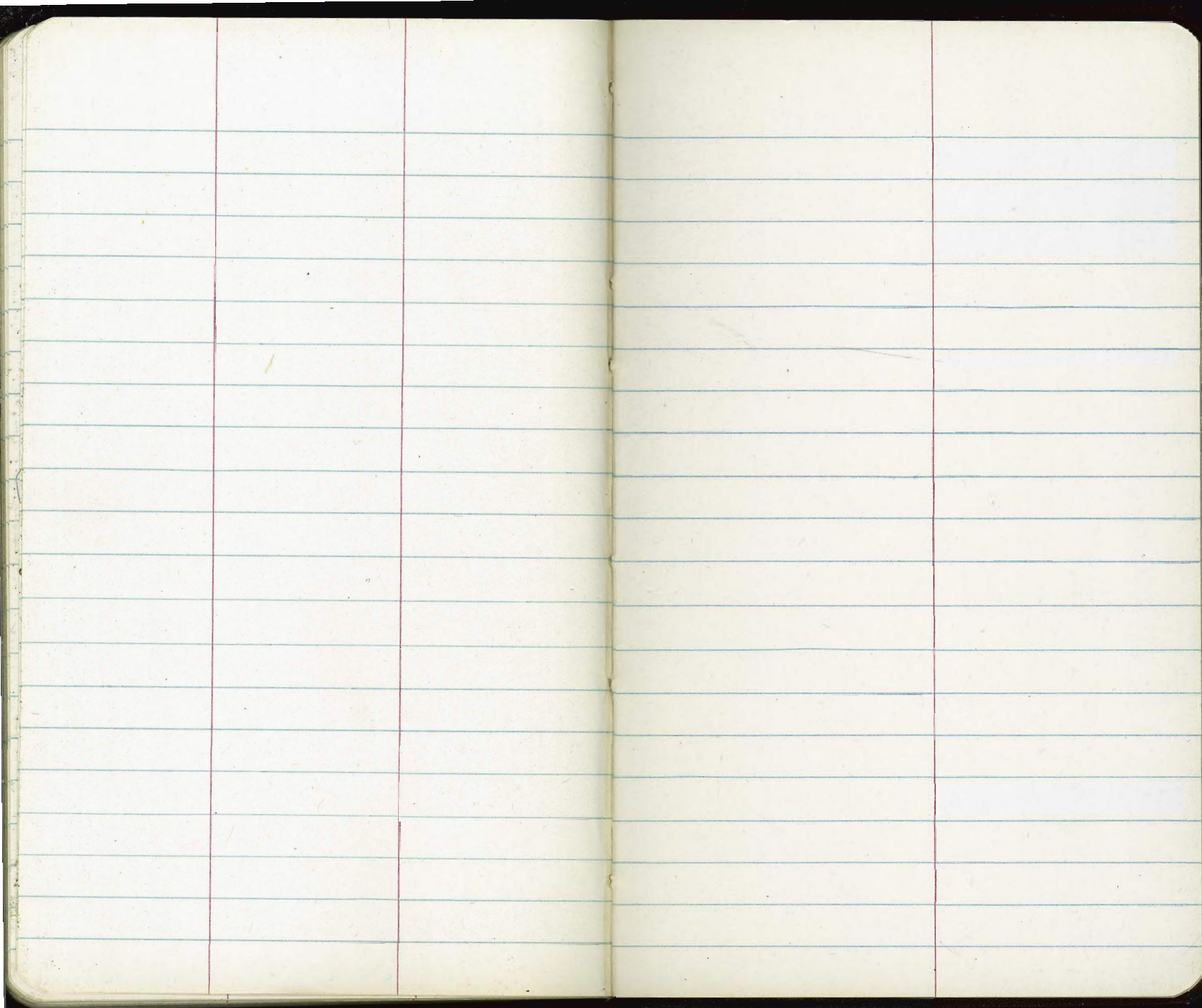


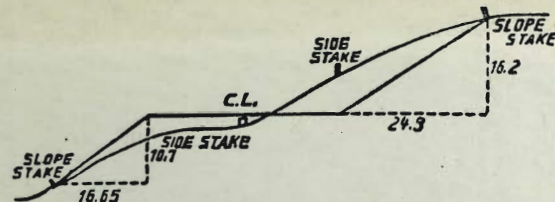






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**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**

SLOPE  $1\frac{1}{2}$  TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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