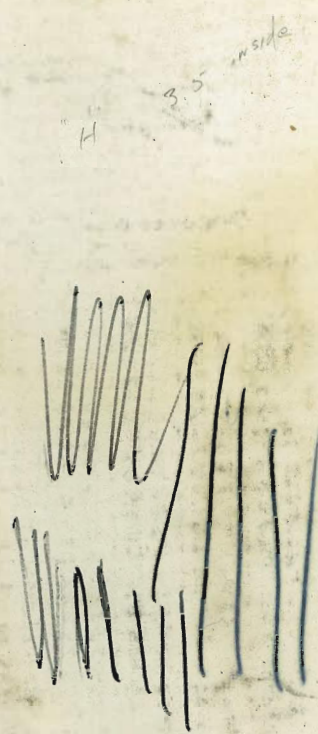


DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING  
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

G-384



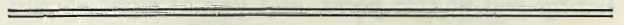
DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Contents of this table have also been printed in the form of a separate sheet for use with roadway tables 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50.



# IMPROVED TABLES AND INFORMATION



The object of this table is to give the user a ready means of determining the amount of earth to be excavated or filled in any given case.

TABLE No. VII

To find the amount of earth to be excavated or filled in any given case, the user should refer to the appropriate table in this book, and then to the appropriate column in this table. The amount of earth to be excavated or filled will be given in the appropriate row of the table.

- 0
- 1
- 2
- 3
- 4
- 5
- 6
- 7
- 8
- 9
- 10
- 11
- 12
- 13
- 14
- 15
- 16
- 17
- 18
- 19
- 20
- 21
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- 36
- 37
- 38
- 39
- 40
- 41
- 42
- 43
- 44
- 45
- 46
- 47
- 48
- 49
- 50

Distance  
ground  
column  
side of  
side of  
cut or fill  
If it does

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.95	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.265	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX:

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CLARK  
GARBER  
ONEIL  
ABERNILLA  
3-26-57  
W.O. 62510

LOCUST ST. - UDALL - WLY  
ADJ. LOT 12, BLK 169 Roseville

STA.	AL	CB	E	RT	P.L.
0+23.5 = Beg. 16 Drive	92.7 104.72 F12.0 ch 18.5 BK hinge-pt	104.72			
0+21.5 (end set)	105.03	104.71 105.03 F0.32			
0+15 = W. Line UDALL	106.00	105.19 106.00 F0.81	106.40		106.40
0+10	106.75	105.60 106.75 F1.15	107.15		
0+06.5 ± = Edge EXIST C&G, 7' RT E ST				meat EXIST Pave	
0+05	107.34	105.96 107.34 F1.38			
0+00 = END EXIST C.B. LT (54)	107.60	107.60		Remove EXIST. Berm AT edge Pav.	

Note: AT Contractor's  
request ch's were set on  
F. bid's rather than  
stakes.

B.M. Dir. Elev. Rod:

187.16 = SW plug  
UDALL + willow

NO TE. No B.M. given on DWG: 6345-B

Ref: Field Notes D-20  
DWG: 6345-B

STA.	P.L.	CB	E ST.	Rough - (grader limit 17' NLY E ST.)
0+85 = Brow Fill	83.5 95.45 F12.0 ch - wall 18' BK hinge - PT.		95.89	98.9 95.9 E 2.5 4' BK Brow cut
(0+80 ± 2' conc. chute)				
0+79.0 = End C.B. LT	84.40 96.39 F12.0 ch - wall 18.5' BK hinge - PT.	97.56 96.39 C1.17	96.79	99.5 96.8 C2.1 4' BK Brow cut
0+60.25		101.09 99.21 C1.88		
0+47 ± only			101.60	101.60 101.60 Grade 4' BK Toe Fill
0+41.5 LT only	102.02	103.02 102.02 C1.00		(No slope ratio on NLY side)
0+39.5 = End Drive	96.30 102.32 F12.0 ch on wall 18.5 BK hinge - PT.	102.32		

CLARK  
GARBER  
ONEIL  
ABRENILLA  
4-26-57  
W.O. 32474

EMERALD ST.  
OLNEY to PENDLETON

REF: JNG: 3005.A.D  
FB 2405-1

STA	P.L	CB	±	CB	P.L	STA	P.L	CB	±	CB	P.L
						1+00	68.66	68.50 68.66 Fo.16		68.24 68.16 Co.08	68.16
#2	71.70	71.68 71.70 Fo.02		70.14 70.98 Fo.84	70.98						
#3	71.85	72.01 71.85 Co.16		70.85 71.00 Fo.15	71.00	0+90 = W.S LT	68.60 69.83 = T.P.C.B F1.23				
#4	71.52 72.00 Fo.48	72.33 72.00 Co.33	chk	70.92 70.94	70.94	0+80	68.94 69.00 Fo.06	69.02 69.00 Co.02		68.69 68.41 Co.28	68.12 68.41 Fo.29
						0+60	69.60	69.75 69.60 Co.15		69.12 69.00 Co.12	69.00
#2 = CB END = P.L INC OLNEY ST	73.68 73.10 Co.58	73.08 73.10 Fo.02				0+40 = W.S LT	70.00 70.55 = T.P.C.B Fo.55				
#1	73.36	72.95 73.36 Fo.41				0+40	69.99 70.55 Fo.58	70.37 70.55 Fo.18		69.80 69.80 Grade	68.43 69.80 F1.37
<del>#1</del> = END EXIST. CB	73.77	chk: 73.76 73.77				0+25	71.10	70.83 71.10 Fo.27		70.03 70.35 Fo.32	70.35
(EMERALD) B.C	74.00					0+10 = B.Y.C = B.C EMERALD	70.93 71.45 Fo.52	71.16 71.45 Fo.29		69.80 70.75 Fo.95	69.36 70.75 F1.39
<u>N.W. Co.T.</u> (EMERALD to OLNEY)						#1		71.36 71.60 Fo.24		69.83 70.90 F1.07	70.90
SET. T.B.M			70.59	= SE. B.P EMERALD to OLNEY							
BM	Dir. Elev.	Rod	83.11 SW A.P	DIAMOND to PENDLETON		(0+00) R.G. only	71.60				70.90

## EMERALD ST (CONT.)

3

LT (N4)						RT					
STA	P.L	CB	E	CB	P.L	STA	P.L	CB	E	CB	P.L
2+70	69.37 68.29 C1.08	67.77 68.38 Fo.61		67.66 67.66 Grade	66.22 67.58 F1.36						
2+45	68.33	67.69 68.42 Fo.73		67.52 67.74 Fo.22	67.66	4+00	68.08	67.89 68.17 Fo.28		67.20 67.28 Fo.08	67.19
2+35=W.S. LT	69.30 68.35=TPCB C0.95					3+90=W.S. LT	70.68 68.10=TPCB C2.58				
2+20	69.31 68.37 C0.94	67.68 68.46 Fo.78		67.58 67.81 Fo.23	65.66 67.73 F2.07	3+75	70.34 68.12 C2.22	67.95 68.21 Fo.26		67.56 67.36 Co.20	66.91 67.27 Fo.36
1+95	68.41	68.07 68.50 Fo.43		67.72 67.88 Fo.16	67.81	3+50	68.16	67.98 68.25 Fo.27		67.45 67.43 Co.02	67.34
1+90=W.S. LT	70.06 68.42=TPCB C1.64					3+40=W.S. LT	70.15 68.18=TPCB C1.97				
1+70	69.90 68.45 C1.45	68.63 68.54 Co.09		67.74 67.96 Fo.22	65.48 67.88 F2.40	3+25	69.91 68.20 C1.71	67.88 68.29 Fo.41		67.64 67.51 Co.13	67.38 67.42 Fo.04
1+45	68.49	68.43 68.58 Fo.15		67.57 68.03 Fo.46	67.96	3+00	68.24	67.89 68.33 Fo.44		67.85 67.58 Co.27	67.49
1+40=W.S. LT	69.61 68.50=TPCB C1.11					2+90=W.S. LT	69.98 68.26=TPCB C1.72				
1+20=E.V.C	68.60 68.53 C1.07	68.29 68.62 Fo.33		67.94 68.10 Fo.16	66.74 68.03 F1.29	2+85	68.27	67.80 68.35 Fo.55		67.75 67.62 Co.13	67.54



## EMERALD ST (CONT)

4

4499.17	ACTUAL GOTT = 67.39		66.37	ACTUAL = GUTT
4499.17	PLAN (67.89) EXIST. = 68.00 = W. LINE Pendleton = CR ACS		67.01	= EXIST PLAN (66.90 EXIST.)
4490 = W.S LT.	70.33 67.91 = TP CB C 242			
4479.17 = BRK	70.18 67.95 C 223 Fo. 33	67.72 68.05 Fo. 33	66.81 67.05 Fo. 24	67.64 66.95 Ca. 69
4475	67.96	67.72 68.06 Fo. 34	66.69 67.06 Fo. 37	66.97
4450	68.00	67.95 68.10 Fo. 15	66.86 67.13 Fo. 27	67.04
4440 = W.S LT.	70.88 68.02 = TP CB C 286			
4430 = W.S RT			66.81 67.10 = TP CB Fo. 23	
4425	70.59 68.04 C 255 Fo. 33	67.81 68.14 Fo. 33	66.99 67.21 Fo. 22	67.11 67.12 Fo. 01

CLARK  
GARBER  
O'NEIL  
AGRENILLA

7-2-57  
W.O. = 2 21186  
STA.

MADERA ST. STORM-  
DRAIN % 69th sly to AKINS

REF: DWG'S: 4209-D; 4210-D; 4211-D  
4212-D  
CITY ENG. Notes: L-22 (ROBERTS)

5

1400

296.43  
294.99  
C 1.44

STA  
4+20

292.32  
285.00  
C 7.32

0+74.17 = L:RT 10°

↑  
1/8" AT 90°  
↓

299.00  
295.80  
C 3.20

3+40

293.08  
287.50  
C 5.58

0+62.17 = L:10°  
= Gvd BvK

↑  
1/8" AT 90°  
↓

300.99  
296.17  
C 4.82

3+00

294.15  
288.75  
C 5.40

0+31.08

(See 0+00)  
(To meet EXIST) 300.89  
Plan = 296.58 296.77  
C 4.12

2+60

294.87  
290.00  
C 4.87

2+20

295.32  
291.25  
C 4.07

0+00 = (SURVEY STA.)  
0+70.17  
= END EXIST 42"  
Pipe

EXIST = 297.37  
Plan = 297.00 (meet EXIST)

1+80

297.04  
292.50  
C 4.54

(Stub s to LTR)

1+40

295.27  
293.74  
C 1.53

B.M (Dir. Elev. Rod.)

306.41 = L+T

Q MADERA City BDRY  
(E. Line 69th)

MADERA DRAIN (CONT)

STA.

STA.

7+00

289.87  
280.99  
C 8.88

9+60

281.91  
275.92  
C 5.99

6+60

293.61  
281.52  
C 12.09

9+20

283.96  
276.81  
C 7.15

6+20

292.49  
282.04  
C 10.45

8+80

285.88  
277.70  
C 8.18

5+80

292.49  
282.56  
C 9.93

8+40

287.58  
278.59  
C 8.99

5+40

292.14  
283.09  
C 9.05

8+00

289.35  
279.48  
C 9.87

5+00

291.87  
283.62  
C 8.25

7+76.00 =  
GND Bnk

↑ 2.228

289.63  
280.00  
C 9.63

4+60

↑  
1.318

291.92  
284.14  
C 7.78

7+68.17 & TYPE F  
CLEANOUT = #4

290.25  
286.64 = TP.  
C 3.61

290.25  
280.10 = FL  
C 10.15

4+39.17 = GND Bnk →

↑  
3.125

292.35  
284.40  
C 7.95

7+40

↑  
1.872

288.30  
280.47  
C 7.83

MADERA DRAIN (Cont)

STA.	
11+80	277.08 271.70 C 5.38
11+40	278.10 272.33 C 5.77
11+00	278.62 273.96 C 4.66
10+78.17 Grid Brk	279.07 273.30 C 5.77
10+70.17 = CRT 10°	279.10 273.48 C 5.62
↑ 10° AT 90° ↓	
10+58.17 = CRT 10°	279.21 273.75 C 5.46
10+40	279.32 274.15 C 5.17
10+00	280.41 275.03 C 5.38

15.85 ↑

2.228 ↑

STA.	
14+20	269.28 267.94 C 1.34
13+80	269.81 268.57 C 1.24
13+40	271.04 269.20 C 1.84
13+00	274.31 269.82 C 4.49
12+60	275.84 270.45 C 5.39
12+20	276.39 271.09 C 5.30



MADERA DRAIN (CONT.)

STA.			STA.	
17+20		271.65 262.55 C 9.10	18+39.61	263.73 258.55 C 5.18
16+80		271.92 263.21 C 8.71	18+12.61 = Grid Bnk	267.62 260.21 C 7.41
16+40		272.08 263.84 C 8.24	18+04.61 = Grid Bnk	268.36 260.63 C 7.73
16+00	↑ 8.91	272.61 264.53 C 8.08	17+96.61 = Grid Bnk	269.16 260.89 C 8.27
15+60		273.32 265.20 C 8.12	17+64.61	268.15 261.62 C 6.53
15+20 (Stub 6' LT)	↑ 3.63	271.32 265.85 C 5.41	17+32.61 = Grid Bnk	271.53 262.36 C 9.17

Contractor  
note: (adjust)  
Clear top con. -  
ENC. Sewer with  
Buff. Storm-Drain

MADERA - DRAIN (CONT.)

STA.		
19+28.61 = B.M.K	260.68 253.17 C 7.51	
19+20.61 = B.M.K	260.76 253.59 C 7.17	
18+93.61	262.58 255.24 C 7.34	
18+68.11 = EASEMENT E.H.	260.20 258.00 F.L. 24" C 2.20 AT BOX	261.95 259.00 = F.L. C 2.95 END PIPE
	(OFF stub 10' Lt. Box) AT 60° OFF BEARING (10.90' to F.L. hd wall) FROM E DRAIN	
	260.20 259.50 = F.L. AT BOX 18" PIPE TO NLY C. 70	
	(OFF stub 10' Lt. Box)	
18+66.61 = E CLEANOUT TYPE 'B' BOX	#2 260.20 267.30 = Tp. Box F 7.10	260.20 256.90 = F.L. Box C 3.30

STA.	
22+40	254.56 243.60 C 10.96
22+00	255.28 244.82 C 10.46
21+60	255.96 246.04 C 9.92
21+20	257.22 247.26 C 9.96
20+80	257.84 248.48 C 9.36
20+40	257.17 249.70 C 7.47
20+00	258.66 250.92 C 7.74
19+60	259.95 252.14 C 7.81
19+36.61 = B.M.K	260.29 252.86 C 7.43

(OFF stub 10' B.L.F. hd wall)

END PIPE

MADERA - DRAIN (CONT.)

STA.			STA.	
24+40		254.31 238.24 C 160.7	26+80	246.16 233.05 C 13.11
24+00	↑ 2.93	257.00 239.10 C 17.90	26+40	249.23 233.92 C 15.31
23+58.17 = Grid Brk		257.68 240.00 C 17.68	26+00	253.86 234.78 C 19.08
23+14.17	↑ 2.50	250.58 241.34 C 17.24	25+60	254.05 235.64 C 18.41
22+70.17 = 4' L. Feet 18" Con. Pipe to Ely AT 90° OFF BIC. TANG.	(Fc Hdwall on Prop.)	252.30 249.00 = FL 18" pipe At Prop. C 3.30	25+20	252.06 236.51 C 15.55
(CONT.)				
22+70.17 = 8' Con. LUG	↓	252.30 242.68 = FL 48" Pipe C 7.30	24+80	249.19 237.37 C 11.82

↑ 2.93

↑ 2.50

(off stub to 27' LUG)

252.30  
245.00 = FL 18" Pipe Ely At LUG  
C 7.30

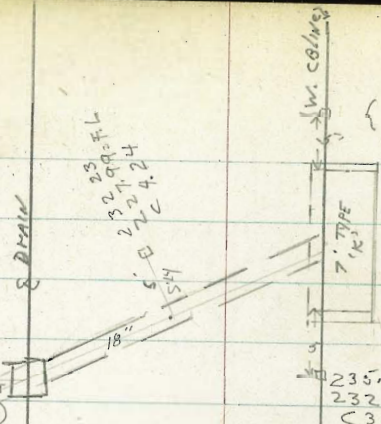
252.30  
242.68 = FL 48" Pipe  
C 9.62



MADERA-DRAIN (CONT)

STA.	
29+20	240.71 227.87 C 12.84
28+80	239.03 228.73 C 10.30
28+40	240.60 229.60 C 11.00
28+00	238.51 230.46 C 8.05
27+60	240.82 231.32 C 9.50
27+20	242.28 232.19 C 10.09

STA.			
		234.73 232.70 CB C 2.03	234.73 231.90 GUT C 2.83
	10' Box CLEANOUT (20+52.34)	235.70 232.70 CB C 3.00	235.70 228.10 FLYNET C 7.60
		235.70 231.90 = GUT C 3.80	
30+52.34 = 4" TYPE 'B' CLEANOUT #3		233.64 234.00 TP Fo. 36 Box	233.64 227.88 FL 18" C 5.76 Pipe At Box
			233.64 225.00 = C 8.64 F.L. Box
30+40			233.77 225.27 C 8.50
30+00			235.52 226.14 C 9.38
29+60			238.08 227.00 C 11.08



23  
22.99 = L  
22.71  
22.42  
22.24  
22.06  
21.88  
21.70  
21.52  
21.34  
21.16  
20.98  
20.80  
20.62  
20.44  
20.26  
20.08  
19.90  
19.72  
19.54  
19.36  
19.18  
19.00  
18.82  
18.64  
18.46  
18.28  
18.10  
17.92  
17.74  
17.56  
17.38  
17.20  
17.02  
16.84  
16.66  
16.48  
16.30  
16.12  
15.94  
15.76  
15.58  
15.40  
15.22  
15.04  
14.86  
14.68  
14.50  
14.32  
14.14  
13.96  
13.78  
13.60  
13.42  
13.24  
13.06  
12.88  
12.70  
12.52  
12.34  
12.16  
11.98  
11.80  
11.62  
11.44  
11.26  
11.08  
10.90  
10.72  
10.54  
10.36  
10.18  
10.00  
9.82  
9.64  
9.46  
9.28  
9.10  
8.92  
8.74  
8.56  
8.38  
8.20  
8.02  
7.84  
7.66  
7.48  
7.30  
7.12  
6.94  
6.76  
6.58  
6.40  
6.22  
6.04  
5.86  
5.68  
5.50  
5.32  
5.14  
4.96  
4.78  
4.60  
4.42  
4.24  
4.06  
3.88  
3.70  
3.52  
3.34  
3.16  
2.98  
2.80  
2.62  
2.44  
2.26  
2.08  
1.90  
1.72  
1.54  
1.36  
1.18  
1.00  
0.82  
0.64  
0.46  
0.28  
0.10  
0.00

MADERA DRAIN (cont)

STA		
32+00		235.28 223.42 C 11.86
31+60		234.07 223.85 C 10.22
31+20	1.072	233.21 224.28 C 8.93
30+93.11 = E.C. = 6+1 BTK		233.23 224.57 C 8.66
30+78.72 = mid. pt		233.28 224.72 C 8.56
30+64.34 = B.C. LT		233.34 224.88 C 8.46
$\left( \begin{array}{l} A = 39^\circ 14' 54'' \text{ LT.} \\ R = 42 \\ T = 14.98' \\ L = 28.77' \end{array} \right)$		

STA		
34+37.11 = 6+1 BTK		242.70 <del>220.89</del> C 21.81
34+00		245.66 221.28 C 24.38
33+60		249.25 221.71 C 27.54
33+20	✓	249.34 222.14 C 27.20
32+80		244.48 222.57 C 21.91
32+40		239.40 223.00 C 16.40

MADERA DRAIN (CONT.)

CHK:

14  
222.22 = 222.29 = P.K.  
S.E. Wood  
C.S. Bridge

STA.		STA.	
		37+66.74 = S'ly end 10' con. apron	215.65 212.70 = F.L. C 2.95
36+00	222.16 215.81 C 6.35	37+56.74 = Fc. Kidwall #4	219.37 213.50 = F.L. line C 5.87
35+60	223.91 217.10 C 6.81		
		37+20	221.30 213.87 C 7.43
35+20	230.64 218.40 C 12.24		
		36+80	221.60 214.27 C 7.33
34+80	238.59 219.68 C 18.91		
		36+40.89 = E.C	222.03 214.66 C 7.37
34+53.11 = Grd Brk	241.24 220.55 C 20.69		
		36+33.30 = B.C	222.09 214.74 C 7.35
34+45.11 = Grd Brk	242.07 220.76 C 21.31	$\Delta = 10^\circ$ $R = 43.5'$ $T = 3.81$ (1-8' length Pipe) 5° Banded ends	

(arrow)  
3.188  
↑  
= 3.225

CLARK  
GARBER  
MOORE  
ABRENILLA  
2-24-59  
W.O. 31686

ALLEY BIK 23 - FAIRMOUNT ADD:

REF: DWG: 5153-D  
CITY DATA [J-19 - W.O. 31686 - C.H.S.]

Note: <sup>STAKES</sup> Rough Grades For Ck. Fill to STA: 2+40  
See pg 18 For Pav. Grades 0+00 to 2+40 E.Y.C.

STA:	LT.	RT.	STA.	LT.	E	RT.
			2+20.85 = W.S. LT	307.35 TP 310.36 = Pav F 3.0 TP Pav		
1+00	309.60	309.49	2+20	310.31		310.42
0+88.85 = W.S. LT.	315.48 309.2 = TP Pav C 6.28		2+00	7' BK Prop 302.5 309.50 F 7.0		313.1 5' BK Prop 309.57 C 3.53
0+80	315.71 310.45 C 5.26	313.71 310.20 C 3.51	1+80	308.98		309.02
0+60	315.55 311.57 C 3.98	311.37	1+60	7' BK Prop 301.6 308.72 F 7.1	308.32	308.74 8.3' BK Prop 308.72 grade
0+40	315.07 312.97 C 2.10	313.91 312.72 C 0.19		Set NAIL Pole 1452 1/5 LG to E at E grade ALLEY		
0+26.85 = W.S. LT.	315.8 314.0 = TP Pav C 1.8 TP Pav		1+48.85 = 2' D catch BASIN		308.20 = E Pav	
0+20	315.67 314.50 C 1.17	314.15 314.20 F 0.05	1+40	308.74	308.32	308.71
= B.V.C. 0+00 = N.L. UNIVERSITY	315.71	4.35 C.K. 314.34	1+20	7' BK Prop 300.3 309.08 F 8.78		309.0 7' BK Prop 308.97 grade
B.M. Dir. Elev. Rod:		312.36 = N.E.B.P 494th UNIVERSITY				

STA	LT	RT (E24)	STA	LT	E	RT
3+88.85 = Sew LAT #(2) LT.	320.23 316.5 = P.L. C 3.73		5+28.85	324.75 325.18 Fo.43		325.58 325.48 C 0.10
3+65 (k'out) →	317.80 319.88 F 2.08	321.85 320.14 C 1.71	5+26.85 = W.S LT.	324.72 325.14 = TP PAR Fo.42 TP PAR		
3+40 (k'out) →	316.30 318.19 F 1.89	319.63 318.41 C 1.22	5+13.85 = Sew LAT #(3) LT.	324.29 319.88 P.L. C 4.41	315.8 = E	
3+20.85 = W.S LT.	315.5 316.9 = TP PAR F 1.4 TP PAR		5+08.85	324.23 324.78 Fo.55		325.50 325.08 C 0.42
3+15	315.58 316.49 Fo.91	318.60 316.69 C 1.91	4+83.85	324.52 324.41 C 0.11		325.45 324.71 C 0.74
3+08.85 = Sew LAT #(4) RT.		318.83 310.75 P.L. C 8.08	4+58.85	323.93 324.04 Fo.11		325.02 324.34 C 0.68
2+90	314.25 314.79 Fo.54	317.16 314.97 C 2.19	4+33.85 = E.V.C.	322.29 323.67 F 1.38		324.42 323.97 C 0.45
2+65	312.34 313.09 Fo.75	315.54 313.24 C 2.30	4+11.85 = W.S LT.	321.35 323.0 = TP PAR F 1.65 TP PAR	(k'out) ↓	
2+40 = E.V.C.	311.14 311.39 Fo.25	313.96 311.52 C 2.44	4+08.85 = E.V.C.	321.59 322.86 F 1.27	(k'out) ↓	323.65 323.16 C 0.49
2+38.85 = Sew LAT #(1) RT.		315.94 306.52 P.L. C 9.42	3+90	320.62 321.57 Fo.95		323.00 321.86 C 1.14

STA.

LT.

RT.

CHK:

327.80 = 327.11 = P.K. & ALLEY  
+ 54.7' POLK

ALLEY



(MAP)  
= 5778.85 } = S.L.  
5799.04 } = POLK

5778.85

327.82  
327.68  
327.30  
Co. 38

328.31  
329.09  
327.60  
C 1.49

5763.85

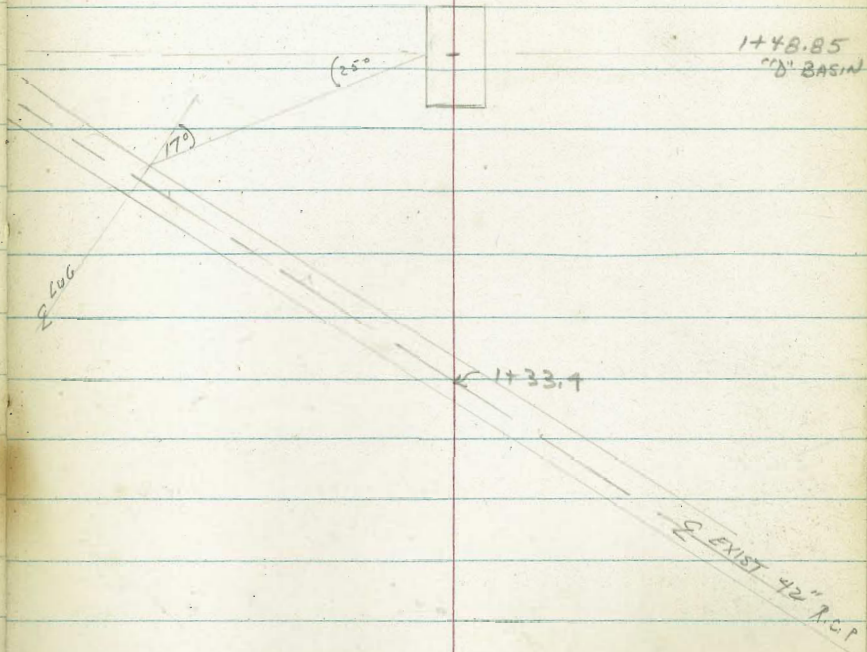
326.94  
326.61  
Co. 33

327.98  
326.91  
C 1.07

5748.85

325.79  
325.92  
Fo. 13

327.09  
326.22  
Co. 87



CLARK  
GARBER  
MOORE  
- ABRENNILLA  
4-22-59  
W.O. 31686

ALLEY BK 23: FAIRMOUNT ADD:

PAV. GRADES 0+00 to 2+40 EVK  
+ replacement missing stubs  
to Park St.  
(See Pg 15) LT. RT (E4)

1+40

308.42 308.58 → 308.58  
308.74 308.32 308.71  
Fo. 32 Co. 26g Fo. 13

1+20

308.76 308.68  
309.08 308.97  
Fo. 32 Fo. 29

1+00

308.88 308.65  
309.60 309.49  
Fo. 72 Fo. 84

0+85.85 = W.S. LT

308.98  
309.2 TP PAV  
Fo. 22

0+80

309.78 309.04  
310.45 310.20  
Fo. 67 F. 1.16

0+60

310.90 310.26  
311.57 311.37  
Fo. 67 F. 1.11

0+40

315.06 313.91  
312.97 312.72  
C 2.09 C. 1.19

0+26.85 = W.S. LT

315.77  
314.0 TP PAV  
C. 1.77

0+20

315.65 314.44  
314.50 314.20  
C. 1.15 Co. 24

0+00

(met) 315.71

314.35 chk  
314.34 (met)

B.M. (Dir. Elev. Rod)

312.36 = N.E. B.P  
49' L + UNIV.

E F.L. 308.32 - 308.35 (RT)  
308.71 (edge Pav)  
Fo. 36

[Cont on Pg 19-LT]

2+40 = E.V.C

2+38.85 = Sew #1  
RT

2+20.85 = W.S. LT

2+20

2+00

1+80

1+60

1+48.85 = Catch Basin  
Stubs 2' BK PAV Edge  
LT + RT.

LT

E

RT (E4)

311.14  
311.39  
Fo. 25

310.20  
310.4 TP  
Fo. 20 PAV

309.38  
310.31  
Fo. 93

308.39  
309.50  
F. 1.11

308.80  
308.98  
Fo. 18

308.66  
308.72  
Fo. 06

308.03  
308.20g  
Fo. 17

308.03  
299.00 = F.L. connect. 18"  
C 9.3 436"

313.96  
311.52  
C 2.44

315.94  
306.52 P.L.  
C 9.42

313.69  
310.42  
C 3.27

310.78  
309.57  
C. 1.21

309.06  
309.02  
Co. 04

308.32 ← 308.32  
308.32 grade E 308.72  
Fo. 40

308.45  
308.20 E  
Co. 25

308.45  
299.61 = FL  
C 8.84 BASIN





COLUSA, ET-AL DRAIN

CLARK  
GARBER  
MOORE  
ABRENILLA  
3-3-59  
W.O. 32837

AZUSA  $\div$  200' SLY GAINES, N'ly to  
CONNECT.

REF: City Notes: W.O. 32837 by ROBERTS 20  
DWG: 5599-D } inclusive  
5591-D }

Note: See Prec. Pg (19) For EXTENSION 33"  
Pipe to face EXIST. PAV

1+68	31.16 13.84 C 17.32
1+36	30.41 13.52 C 16.89
1+04 = E.V.C	29.89 13.20 C 16.69
0+84	28.64 12.77 C 15.87
0+64	27.94 11.92 C 16.02
0+44	27.24 10.63 C 16.61
0+24 = B.V.C stubs 10' RT E	27.01 8.90 C 18.11
0+00 = PT. 200' SLY OF S.L. GAINES	26.91 6.50 F.L. C 20.41

4+16.28 = B.C. $\Delta = 20^\circ$ LT $E R = 22'$	(NAILS 6' RT at 90° to 4' tang.) Line only No grade
4+12.28 = E.C	
4+04.60 = B.C. $\Delta = 20'$ RT $E R = 22'$	29.18 16.21 C 12.97
3+85	29.18 16.01 C 13.17
3+45	29.21 15.61 C 13.60
3+05	29.67 15.21 C 14.46
2+65	30.07 14.81 C 15.26
2+25 = $L 4^\circ 34' 25''$ LT (2+25.08) = N.L. GAINES	30.86 14.41 C 16.45
2+00 = $L 4^\circ 34' 25''$ RT = S. Line GAINES	31.80 14.16 C 17.64

Chks. to Con Wall  
10.2' BTE

T.B.M: Dir. Elev. Rod: 31.56 = Ch + CONC FDTN  
Pile #5700 at  
N.E CORN GAINES

+ AZUSA (City notes - Roberts)

AZUSA DRAIN (CONT.)

5+70 28.57  
17.84  
C10.73

5+30 NML 10' RT 28.11  
17.45  
C10.66

4+90 ch's 10' RT-TP wall 29.19  
17.05  
C12.14

4+51.66 = E.C. 29.24  
16.67  
C12.57

4+43.98 = B.C. 6' RT at 90°  
Δ = 20° RT to 4' + 4' + 6'  
ER = 22' Line only

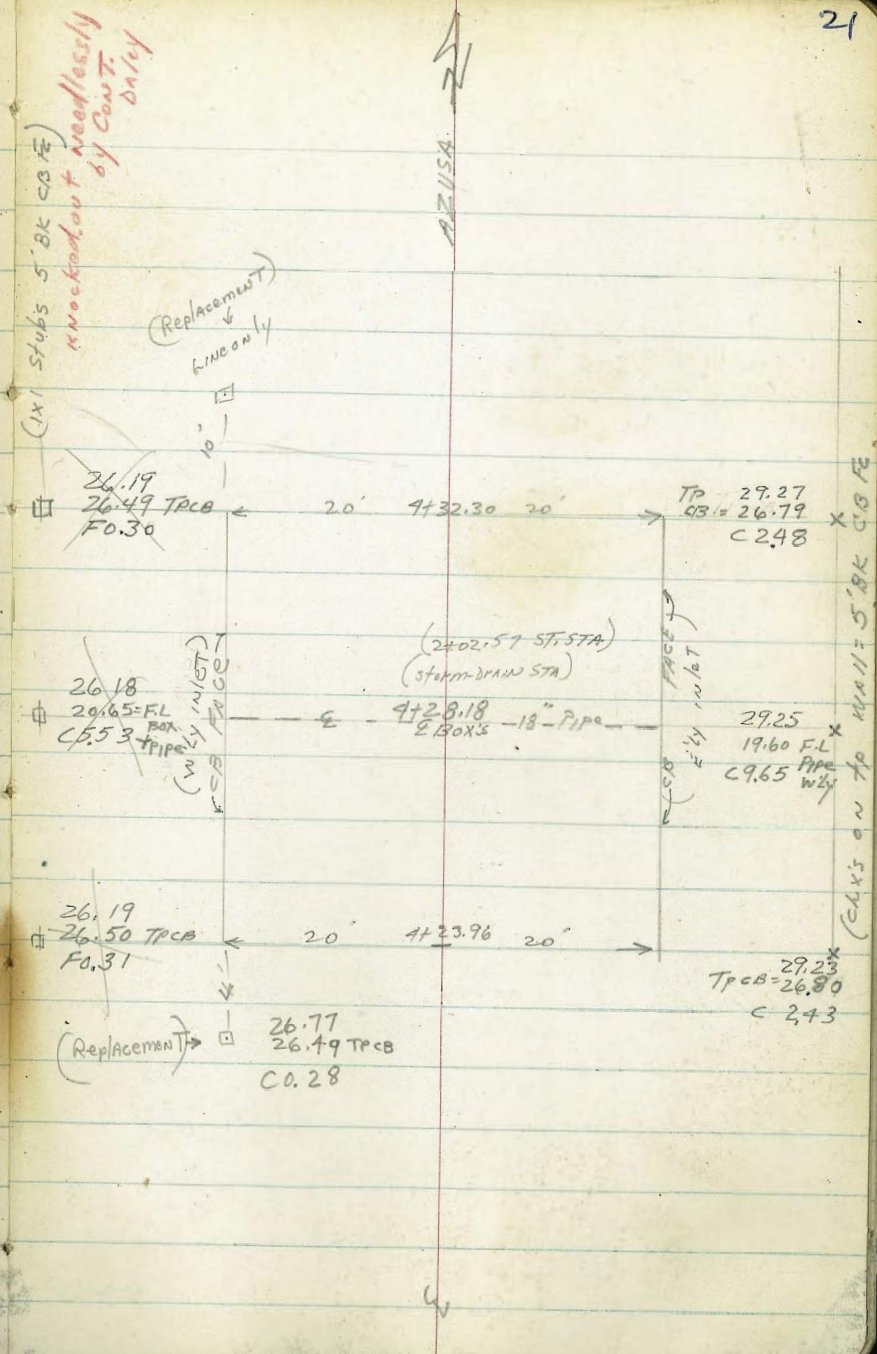
4+39.98 = E.C.

(2 inlets: 202.6 N'ly OF N.L. GAINES AS PER DWG. 5598-D) Δ = 20° LT = B.C. ER = 22'

4+32.30 (outside) N'ly edge INLET 26.19  
20.65 = F.L. w/ly Box C 5.54  
29.27  
16.44 F.L. Ely Box  
C12.83

4+28.13 = 7' TYPE K-1 = 8" 18" CROSS-DRAIN INLETS

4+23.96 (outside) S. Edge TYPE K-1-7' INLET (8.34 outside) 26.19  
20.65 = F.L. w/ly Box C 5.54  
29.23  
16.44 F.L. Ely Box  
C12.79



AZUSA DRAIN (CONT.)

32.56 = NEB.P  
LAURETTA YAZUSA

For 2 - small curves Nly Box  
(Ch's swails 6' RT AT 90°  
to 4' TANG

31.43  
2x80  
C 10.63  
(Cared-  
-IN)  
31.48  
30.97 CB  
20.41  
30.97 CB  
20.41

(0135 CG grade)

+77.64  
7+79.64 = Nly edge Box File 20.80  
(outside) C 10.45

31.25  
31.25  
31.00 = TP CB  
C 0.25

10+50 stub 9' RT E

44.51  
34.34  
C 10.17

(7+75.47) = E K - INLET

30.70  
F.Lim 20.80  
Box C 9.90

30.70  
30.86 CB  
F 0.16

stubs 5' RT CB E

30.75  
20.60  
C 9.95

(Cared-  
-IN)  
30.75  
30.87 CB  
F 0.12

10+10

44.99  
33.13  
C 11.86

+769.30  
7+71.30 = Sly edge Box F.L 20.88  
(outside) C 10.22

31.02  
31.02  
30.90 = TP CB  
C 0.12

Note: Box had to be moved sly 2' to avoid conflict  
with Fire-Hydr.

39.24  
(NAIL 10' LT E)

(Note: STAs not Fig. For  
4 - small curves (2 on Each Side  
Box RT. AT 90°  
to 4' TANG  
Cont. STA: STRAIGHT-through  
I.E. 18.80' S'ly + N'ly From edge Box  
= Bc + E.C.)

STUBS 6'  
RT. AT 90°  
to 4' TANG

9+70.76 = E "G" CLEANOUT  
(= E ALLEY LINE Ely)

41.04 41.04 41.04 F.L.  
31.50 = F.L. 32.00 Nly 32.50 Ely  
C 9.54 Box C 9.04 C 8.54

7+52.50 = B.C

30.34  
20.40  
C 9.94

9+30

37.58  
28.60  
C 8.98

7+29.54

29.92  
19.94  
C 9.98

8+90

35.40  
25.65  
C 9.75

(NAIL 10' LT E)

1x1-10  
Nly

stub 10' RT

6+87.71 = E CON-LUG  
4E 12" PIPE - Ely = grid Bk C 10.61  
29.61 29.61 29.66  
F.L 30" = 19.00 20.00 = F.L 25.00 = F.L  
C 9.61 Pipe to Alley C 4.66 end PIPE

8+51.51 = 9th Bk

33.81  
22.80  
C 11.01

6+50

31.15  
18.64  
C 12.51

8+35.51 9th Bk ch 10 RT

31.96  
22.00  
C 9.96

6+10

30.95  
18.24  
C 12.71

8+07.57 ch 10 RT

31.51  
21.44  
C 10.07

AZUSA DRAIN (CONT)

clerk

52.01 = 52.02 = STATE MDL  
 APPROX  
 S.W 2y CORNER  
 MILDRED & AZUSA

(Stubs 8' x 16' RT)

note 54.20 = F.L. 18" PIPE

12+35.46 = E "H" CLEANOUT: F.L. 59.74  
 BOX C 8.74 59.74  
 57.30 = F.L. EXIST  
 18" SQ. OPENING  
 E 2y F.L.

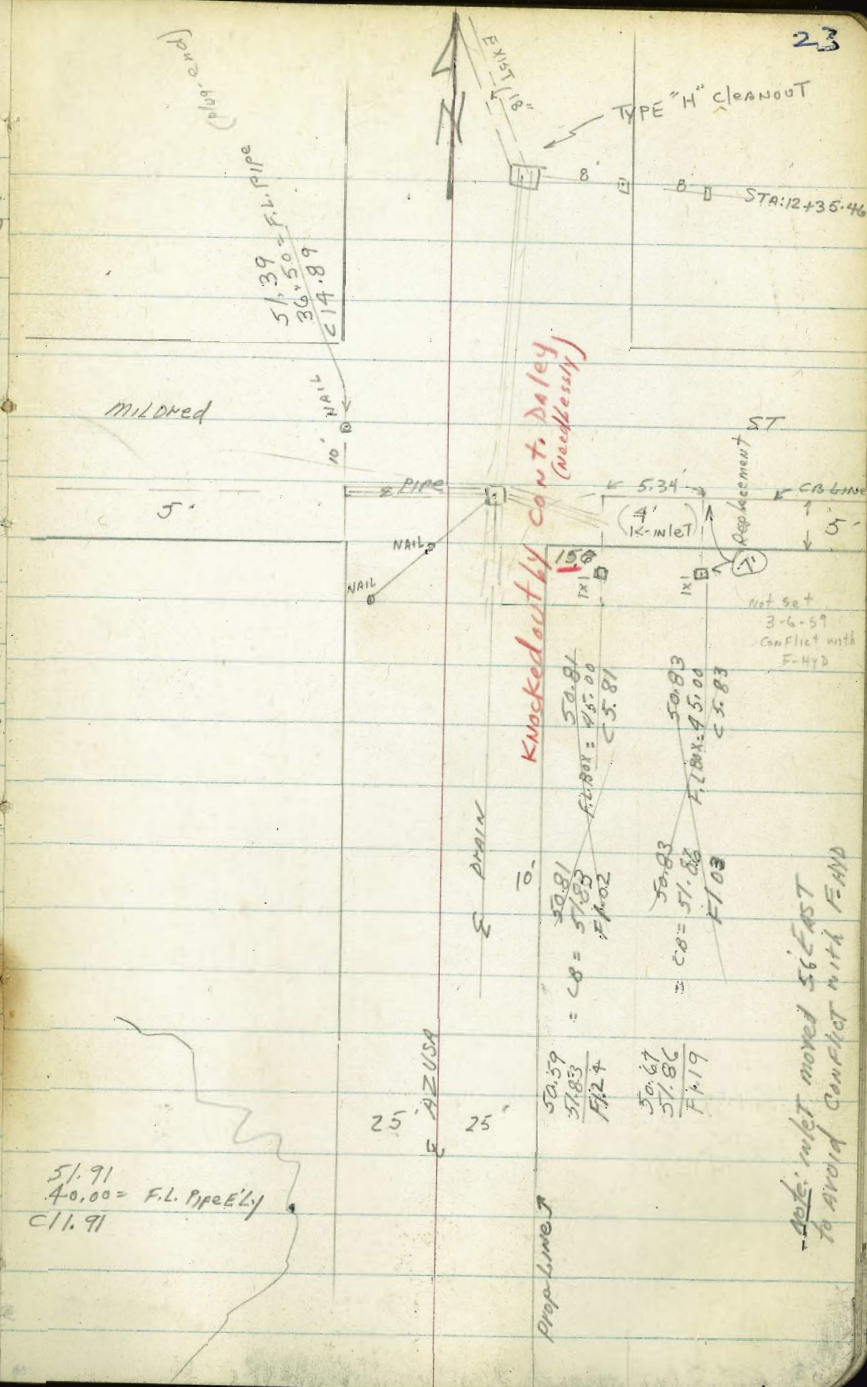
11+95 (10' RT) 59.57  
 46.84  
 C 12.73

11+55 (10' RT) 53.87  
 42.72  
 C 11.15

note (NAIL PROBE) (LINE ONLY)  
 NAILS 10' 7" (9" IT) (CONCRETE)  
 (4' 10" W OF F.L. LINE AZUSA)  
 (5' N OF S.L. MILDRED)

11+14.88 = E "G" CLEANOUT  
 = 9" d. BOX F.L. BOX 51.91  
 C 13.61 36.30  
 38.80 = F.L. PIPE  
 N 4y

10+90 NAIL 10' LT 50.13  
 35.55  
 C 14.58



DRAIN - ALLEY BIK H &  
EASEMENT BIK - II -

STA.	Grade	STA.	GRADE
2+49.56 = E.V.C.	42.00 39.15 C 2.25		
2+39.56	42.15 39.16 C 2.99		
2+29.56 = B.V.C.	41.54 38.76 C 2.78		
2+00	41.42 37.95 C 3.47		
1+60 (All stubs 6' BT &)	40.03 36.85 C 3.18		
1+20	39.12 35.75 C 3.37	5' by end 3+39.09 = EXIST 24" pipe	46.13 = FLATIST 24" PIPE
0+80	39.32 34.65 C 4.67	3+18.79 = E.C.	46.34 44.67 C 1.67
0+40	41.64 33.55 C 8.09		
0+00 = & CLEANOUT = 9+70.76 AZUSA See pg 22	41.04 32.50 = F.L Pipe Ely C 8.54	2+78.42 = B.C.	45.56 43.22 C 2.34
B.M (See pg 20)		2+78.42	44.02 41.80 C 2.22

CONT. pg. 25

CO/USA - et. al

DRAIN - BK 4 - Silver HTS  
(BENILIA & MILDRED)

0+77 ± = grad. BK = N. edge Type K" inlet  
59.32  
58.00 = F.L  
C1.32

0+72 ± = grad. BK = BK  
TYPE K" inlet  
59.02  
58.00 F.L  
C1.02

CHK: 65-26 = F.L EXIST

0+39.63 = E.C

62.08  
55.82  
C6.26

2+25 = EXIST 24" Pipe

65.27

F.L  
meet

LINDA VISTA Rd

Δ = 28° 59' 14"  
R = 22'

1+85

66.01  
63.29  
C 2.72

0+28.5 = B.C

57.83  
55.07  
2.76

stubs 6' RT &

(stubs set 6' RT.)

1+45

62.51  
61.33  
C 1.18

0+00 = Nly end EXIST  
24" PIPE IN BONICIA

PLAN = 53.50

53.17

1+05

60.29  
59.37  
C 0.92

T.B.M

52.02: Study STATE  
man mildred + AZUSA

MILDRED

AZUSA-ELY

STA.	P.L.	LT. (N4) CB	E	CB	RT. (S4) P.L.	STA.	P.L.	CB	E	CB	P.L.
0+67.5 = W.S. LT	61.3 52.7 TP CB C8.6					2+22.5 = W.S. LT.	58.7 54.75 TP CB C3.95				
0+58 = MS RT.					51.3 52.1 TP CB F0.8	2+10	54.43	55.41 54.43 C0.98		53.45 53.93 F0.48	53.93
0+50	52.55	52.90 52.55 C0.35		51.74 52.05 F0.31	52.05	1+90	56.41 53.88 C2.53	53.69 53.88 F0.19		53.00 53.38 F0.38	51.69 53.38 F1.70
0+25	52.39	52.15 52.39 F0.24		51.10 51.89 F0.79	51.10 51.89 F0.79	1+73 = W.S. RT.		53.18 53.47 F0.29		52.75 52.97 F0.22	51.3 53.0 TP CB F1.7 52.97
0+20.94 = Ely end inlet (moved)						1+58 = SEW LAT (9) RT.			51.1 47.9 C.3.2		51.1 48.4 PL C2.7
0+15.60 = W. End Inlet (see p 23)						1+50 = B.V.C.	55.65 53.18 C2.47	53.04 53.18 F0.14		52.46 52.68 F0.22	51.50 52.68 F1.18
0+13.54 LT. only	59.67 52.32 C7.35	52.35 52.32 C0.03				1+25	53.02	52.86 53.02 F0.16		52.35 52.52 F0.17	52.52
0+10 = CB E.C. RT.					51.80	1+00	52.86	52.64 52.86 F0.22		52.34 52.37 F0.03	52.37
0+00	55.75 52.30 C3.45	53.59 52.30 C1.29		47.88 51.70 F3.82		0+82.5 = SEW LAT (6) LT.	60.93 48.8 PL C12.13		60.93 46.7 17.23		
0-10	52.15	51.73 52.15 F0.42				0+75	52.71	52.30 52.71 F0.41		51.85 52.21 F0.36	52.21
0-30	55.80 51.90 C3.90	51.50 51.90 F0.40									
0-50	55.05 51.40 C3.65	54.90 51.40 C3.50		51.92 51.20 F. PL							
T.B.M			51.92 51.20 F. PL	52.02 =	S.W. STATE AZUSA +						MILDRED (Approx. Loc.)

STA.	P.L.	CB	E	CB.	P.L.
3+45.5 = W.S. LT.	70.1 60.6 = TP C 9.5 CB				
3+37.07 = mid-pt	60.30	60.20 60.30 Fo. 10		59.58 59.80 Fo. 22	59.80
ER = 100 Δ = 13° 56' RT (Dwg 3+25.34) (Δ = 13° 25' 55")					
3+25 = CB B.C.	68.60 59.70 C 8.90	59.40 59.70 Fo. 30		59.12 59.20 Fo. 08	59.79 59.20 C 0.59
3+00	63.60 58.43 C 5.17	58.12 58.43 Fo. 31		57.77 57.93 Fo. 16	58.43 57.93 C 0.50
2+85	57.66	57.43 57.66 Fo. 23		57.02 57.16 Fo. 14	57.16
2+83.25 = SEW LAT RT (5)			57.9 50.6 C 7.9	57.9 50.5 = P.L. C 7.4	
2+70 = E.V.C	62.75 56.90 C 5.85	56.75 56.90 Fo. 15		56.33 56.40 Fo. 07	56.35 56.40 Fo. 05
2+50	55.93	55.74 55.93 Fo. 19		55.06 55.43 Fo. 37	55.43
2+32.5 = SEW LAT LT. (7)	59.5 49.8 P.L. C 9.7		59.5 49.2 C 10.3		
2+30	58.62 55.12 C 3.50	54.87 55.12 Fo. 25		54.28 54.62 Fo. 34	53.00 54.62 F 1.62

STA.	P.L.	CB	E	CB	P.L.
(ch STA) to meet easement (4+80.97) = (map dist. wrong)					
(4+82.61) = W end inlet RT ONLY					
4+74.80 = B.V.C	63.69 66.20 F 2.51	65.54 66.20 Fo. 66		65.43 65.70 Fo. 27	58.67 65.99 Fo. 36
4+49.1	65.35	64.74 65.35 Fo. 61		64.35 64.85 Fo. 50	64.85
4+23.5 = B.V.C	67.63 64.50 C 3.13	64.13 64.50 Fo. 37		63.39 64.00 Fo. 61	58.50 64.00 F 5.50
4+17 = W.S. RT Stub 5' B.C.				61.4 63.7 TP CB F 2.3	58.5 63.7 = TP CB F 5.2 (K.O.D. by Cont.)
4+00	68.40 63.36 C 5.04	63.05 63.36 Fo. 31		62.53 62.86 Fo. 33	59.19 62.86 F 3.67
3+75	62.15	62.07 62.15 Fo. 08		61.39 61.65 Fo. 26	61.65
3+64 = Sew CAT (8) LT.	70.26 57.7 P.L. C 12.56			70.26 51.6 C 18.66	
3+49.14 = CB E.C.	69.5 60.90 C 8.6	60.80 60.90 Fo. 10		60.13 60.40 Fo. 27	60.19 60.40 Fo. 21



## MILDRED (CONT.)

28

STA.	LT.			RT.			STA.	LT.			RT.		
	P.L.	CB	E	CB	P.L.			P.L.	CB	E	CB	P.L.	
↳ Prop. opening													
5+15.99-BRK	71.66 72.05 F0.39	71.94 72.05 F0.11		71.60 71.55 C0.05	73.34 <sup>572</sup> 71.55 C1.79		7+00 RT. only				80.03 80.30 F0.27	80.00 80.30 F0.30	
5+6.34-EC <sup>CB</sup>	68.57 71.25 F2.68	70.78 71.25 F0.47		70.23 70.75 F0.52	69.32 70.75 F1.43		6+75 RT. only				78.18 78.55 F0.37	78.55	
5+52.95=mid-PT.	70.35	69.91 70.35 F0.38		69.72 69.85 F0.13	69.85								
ER=100' A=13° 03' 45" (DME 13° 25' 35")							#1 Line only NWly Re.T. = 2 end CB →	80.00		82.10 80.00 C2.10			
5+41.56=CB BC	64.28 69.45 F5.17	69.20 69.45 F0.25		68.94 68.95 F0.01	68.36 68.95 F0.59		(CB R=15' A=48° 11.4') Mildred + Josephine = CB-B.C	81.59 78.76 C2.83		78.66 78.76 F0.10			
5+34.81	69.03	68.64 69.03 F0.39		68.46 68.53 F0.07	68.53		6+71.24						
5+14.81	62.12 67.90 F5.78	67.41 67.90 F0.49		67.10 67.40 F0.30	61.86 67.40 F5.54		6+50	80.64 77.26 C3.38	77.08 77.26 F0.18		76.51 76.80 F0.29	77.39 76.80 C0.59	
4+94.81	66.94	66.33 66.94 F0.61		66.44 66.44 grade	66.44		6+25	75.50	75.49 75.50 F0.01		74.74 75.06 F0.32	75.06	
4+86.3 ch. STA (4+87.95=) E. END INLET RT only				chk: 66.20 66.18	66.33 66.18 C0.15		6+00	75.84 73.74 C2.10	73.89 73.74 C0.15		73.00 73.20 F0.20	74.32 73.30 C1.02	

(see Pg 25) → F. Line Box 758.00

MILDRED (Josephine, Ely) - CONT. -

MILDRED (Co/USA, Ely) (-CONT.) 29

Set T.B.M. = 100.72 = LANDING to CON steps #5662 on LT (UPSTAIRS)

STA.	P.L.	CB	E	CB	P.L.
8434.2 <sup>SEM LAT</sup> (2) LT.	90.4 87.8 PL C2.6	90.21 91.48 F1.27	(13' w/4y 90.4 to MAIN 81.2) 9.2	90.58 90.99 F0.41	90.99
8425	91.48	90.21 91.48 F1.27		90.58 90.99 F0.41	90.99
8409.2 = W.S. LT.	89.9-TPCB	(IN)			
8400	90.64 89.18 SEM LAT C1.76	88.55 89.18 F0.63		88.30 88.69 F0.39	85.13 88.69 F3.56
7499.2 = (1) LT.	84.4 P.L.	(IN)	80.32		
7475	86.88	86.44 86.88 F0.44		85.89 86.39 F0.50	86.39
7459.2 = W.S. LT.	85.4-TPCB	(IN)			
7457.24 = E.V.C	86.50 85.25 C1.25	85.19 85.25 F0.06		84.58 84.75 F0.17	83.60 84.75 F1.15
NE'ly Ret = CB, BC Mildred + Jose.	86.63 83.51 C3.12	83.76 83.51 C0.25		82.95 83.01 F0.06	82.31 83.01 F0.70
CB R=15' Δ=48° 11.4' (at CLINE ONLY) #2 end CB-on Joseph - Prop	83.25	85.34 83.25 C2.09			
7417.24 RT ONLY B.V.C.				81.11 81.49 F0.38	80.45 81.49 F1.04
Set T.B.M	77.995			= N.W. CON STAIR 5629 MILDRED-RT.	

STA	P.L.	CB	E	CB	P.L.
7490.7 = W.S. LT.	112.5 108.7-TPCB C3.8				
7475	109.63 106.39 C3.24	105.98 106.39 F0.41		105.32 105.39 F0.07	106.44 105.39 C1.05
7450	105.64 102.64 C3.00	102.35 102.64 F0.29		100.82 101.65 F0.83	103.90 101.65 C2.25
MILDRED-COLUSA Ely = CB BCs	103.10 100.50 C2.60	100.37 100.50 F0.13		99.30 99.50 F0.20	102.27 99.50 C2.77
EQ: 7445.74 =					
For Ret: See Colusa - P434					
MILDRED + COLUSA = CB BCs	84.34 96.15 F11.81	95.74 96.15 F0.41		93.84 95.65 F1.81	92.40 95.65 F3.25
8475.74					
8465.74 (-Prop BC RT) SEM LAT	95.23	94.91 95.23 F0.32		93.77 94.74 F0.97	94.74
8455.7 = (2) RT.				87.6 81.5 (90' w/4 to MAIN) C6.1	87.6 82.3 = P.L. C5.3
8450	85.66 93.78 F8.12	92.17 93.78 F1.61		92.77 93.29 F0.52	86.84 93.29 F6.45
8442 = W.S. LT. →	93.3-TPCB F3.7				

## MILDRED (Colusa to Brunner) cont

CHK

Brunner + 11110.30  
119.87 = 119.00 = MAIL NELY 904-File  
(ROBERTS - notes)

STA.	(Nly) LT.		RT		
	P.L.	CB	E	CB	P.L.
11+22.80	122.03	121.67 122.03 Fo.36		120.53 121.03 Fo.50	121.03
11+02.80	124.90 121.42 C3.48	121.58 121.42 Co.16		120.15 120.42 Fo.27	119.36 120.42 F1.06
10+82.80	120.27	120.84 120.27 Co.57		119.08 119.27 Fo.19	119.27
10+62.80	120.73 118.58 C2.15	118.86 118.58 Co.28		117.20 117.58 Fo.38	117.06 117.58 Fo.52
10+50.7= SEW LAT (10) LT	120.5 112.1 P.L. C8.4		120.5 110.3 C10.2		
10+42.80	116.35	116.08 116.35 Fo.27		115.00 115.35 Fo.35	115.35
10+35.7= W.S. LT	119.2 115.3 P.L. C3.7				
10+22.80= B.V.C.	117.27 113.58 C3.69	113.17 113.58 Fo.41		112.22 112.58 Fo.36	112.67 112.58 Co.09
10+00	113.39 110.15 C3.24	109.96 110.15 Fo.19		109.01 109.15 Fo.14	110.56 109.15 C1.41

STA.	P.L.		E		
	CB	P.L.	CB	E	P.L.
Set T.B.M.	=122.05=	TP 5th Con. Step	RT	AT	#5737
#3	121.94			121.67 121.94 Fo.27	
#2	121.58			121.30 121.58 Fo.28	119.81 120.15 Fo.34
#1	121.50			121.21 121.50 Fo.29	120.33 #2 120.15 =CB Co.18 END
11+94.20= CB BC RT (N.W. 24)	128.02 121.59 C6.43	121.08 121.59 Fo.51			119.89 120.00 Fo.71
11+75.40= CB BC RT (SW 24 BRUNNER)	128.17 121.77 C6.40	121.26 121.77 Fo.51			120.60 #1
11+73= SEW. LAT (4) LT	128.3 116.8 P.L. C11.5				119.81 120.77 Fo.96
11+59.10	121.93			121.80 121.93 Fo.13	120.25 120.77 Fo.52
11+42.80= E.V.C.	127.88 122.10 C5.78	122.00 122.10 Fo.10			128.3 115.0 E C13.3
					120.32 120.93 Fo.61
					120.93
					120.78 121.10 Fo.32
					119.16 121.10 F1.94

CO/USA (RILEY to LAURETTA)

STA	P.L	CB	E	CB	P.L
0+95.95 Alley CB BC'S:	62.37	61.91 62.37 Fo.46		62.95 62.81 Co.14	62.81
0+75	61.03	60.47 61.03 Fo.56		61.16 61.43 Fo.27	61.43
0+50	60.39 59.47 Co.92	59.34 59.47 Fo.13		59.57 59.88 Fo.37	63.08 59.88 C3.20
0+25	57.92	58.29 57.92 Co.37		57.89 58.34 Fo.45	58.34
0+10=CB BC'S (6+08.5 RT)	59.2 57.00 C2.2	57.96 57.00 Co.76		56.92 57.40 Fo.48	61.85 57.40 C4.45
# 1	55.85 56.55 Fo.70	58.79 56.55 (K'od) C2.24		57.34 56.75 Co.59	56.75
# 2	55.63 56.45 Fo.82	58.75 56.45 (K'od) C2.28			56.54 EW&T
# 3 = EC. RILEY	56.00	55.90 56.00 Fo.10			
0+00 = N.L. Riley T.B.M. Dir. Elev. Rod:	59.2 56.5 C2.7				

STA	P.L	CB	E	CB	P.L
2+00	67.52	67.22 67.52 Fo.30			67.35 68.02 68.02 Fo.67
1+75	64.50 66.32 F1.82	66.08 66.32 Fo.24			66.34 66.82 66.82 Fo.48 Co.46
1+50	65.12	64.89 65.12 Fo.23			65.37 65.62 65.62 Fo.25
1+23.95 Alley CB BC'S: (A.R. STUB)	63.16 63.87 Fo.71	63.64 63.87 Fo.23			64.15 64.37 64.37 Fo.22 C1.43 (A.R. STUB)
Alley 1+20 EC'S	63.76	63.64 63.76 Fo.12			64.15 64.26 64.26 Fo.11
Alley at Prop LINE-ST.	63.16 63.78 Fo.62	63.40 63.78 Fo.38			64.69 64.28 64.28 Fo.41 C1.52
Alley at Prop LINE-ST.	62.72	62.13 62.72 Fo.59			63.65 63.22 63.22 Co.43
1+00 = ALLEY E.C'S	62.10 62.70 Fo.6	61.91 62.70 Fo.79			62.95 63.18 63.18 Fo.23 C1.58

71.74 = NERP CO/USA + LAURETTA



Colusa (LAURETTA to MILDRED)  
(CONT.)

STA	P.L.	LT. CB	E	RT. CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
1+75	90.93 91.44 Fo.51	90.96 91.44 Fo.48		91.81 91.94 Fo.13	98.32 91.94 C6.38						
1+50	88.50	88.20 88.50 Fo.30		89.07 89.00 Co.07	89.00						
1+23.71=ALLEY CB BC'S:	85.14 85.40 Fo.26	84.82 85.40 Fo.58		85.56 85.90 Fo.34	91.39 85.90 C5.49						
1+19.71=EC'S	85.14 85.01 CB 113	84.71 85.01 Fo.30		85.54 85.51 Co.03	91.39 85.51 C5.88	CR EC on MILDRED	93.84 95.65 F1.81		(see Pg 29)		99.30 99.50 Fo.20
ALLEY AT Prop Line - 57 (N4)	85.03	84.73 85.03 Fo.30		91.24 85.53 C5.71	85.53	#2	96.10 94.35 96.10 F1.75		97.49 97.70 Fo.21		97.70
ALLEY AT Prop Line ST. (S4)	82.58	81.90 82.58 Fo.68		84.30 83.08 C1.22	83.08	#1	96.10 94.43 96.10 F1.67		97.08 97.40 Fo.32		97.40
1+99.71=EC'S	81.51 82.56 F1.05	81.81 82.56 Fo.75		83.88 83.06 Co.82	84.54 83.06 C1.48	2+09.43= CB BC'S	93.40 95.50 F2.1	95.15 95.50 Fo.35	95.69 96.00 Fo.31		101.39 96.00 C5.39
0+95.71=ALLEY CB BC'S:	81.51 81.95 Fo.44	81.19 81.95 Fo.76		83.13 82.45 Co.68	84.54 82.45 C2.09	2+00	94.40 93.90 94.40 Fo.50		94.46 94.88 Fo.42		94.88



Colusa at LINDA VISTA RD.

LT			RT (ELY)								
STA	P.L	CB	E	CB	P.L	STA	P.L	CB	E	CB	P.L
S'W 1/4 CB Ret				S ELY CR. Ret							
#9 = CB EC	109.18 110.10 FO.9.2	109.30 110.10 FO.80									
#8	110.45	109.75 110.45 FO.70									
#7	109.76 110.80 F1.04	109.80 110.80 F1.00									
#6	111.00	110.52 111.00 FO.48									
#5	108.30 111.05 F2.75	110.41 111.05 FO.64									
#4	110.95	110.09 110.95 FO.86									
#3	105.59 110.65 F5.06	109.78 110.63 FO.87									
#2	110.15	109.40 110.15 FO.75									
#1	103.09 109.50 F6.71	108.92 109.50 FO.58									

#3 = CB EC.

115.20  
115.40  
FO.20

114.30  
115.40  
F1.10

#2 114.90

114.55  
114.90  
FO.35

#1 114.40

113.62  
114.40  
FO.78

See pg 34 For  
CB BC LT  
1110.28

See pg 34 For CB BC



BRUNNER (MILDRED to LINDA VISTA)

LT				RT (Ely)			LT				RT (Ely)		
STA	P.L	CB	E	CB	P.L	STA	P.L	CB	E	CB	P.L		
0+01.70 = CB B.C LT only	128.00 121.94 C 6.06	121.67 121.94 F 0.27				0+95.2 = MS RT					126.7 128.2 TP CB F 1.5		
						(0+96.55) Alley at Prop. LT	132.59 129.65 C 2.94	132.59 129.65 C 2.94					
						Alley E.C. LT (S'ly side alley)	129.60	132.58 129.60 C 2.98					
						0+93.85 = Alley CB BC LT	129.30	132.64 129.30 C 3.34					
0-10.19 RT only				120.76 121.20 F 0.44	121.20								
						0+80	128.33	129.02 128.33 C 0.69		127.53 127.33 C 0.20	127.33		
0-26.93 = CB E.C RT				120.26 120.70 CB F 0.44	116.77 120.20 F 3.43	0+60	129.94 126.92 C 3.02	127.19 126.92 C 0.27		125.99 125.92 C 0.07	125.37 125.92 F 0.55		
(C STA) 0-36.26 mid-pt. RT				120.14 120.20 F 0.06		0+40	125.28	125.18 125.28 F 0.10		124.24 124.28 F 0.04	124.28		
(E STA) 0-45.6 = CB BC RT only				119.51 119.70 F 0.13	113.15 119.70 F 6.55	0+19 = B.V.C.	128.69 123.45 C 5.24	123.99 123.45 C 0.54		122.48 122.45 C 0.03	121.86 122.45 F 0.59		
						0+06.54 = Prop RT only				121.74 121.70 C 0.04	119.59 121.70 F 2.11		

For CB RT  
N.W. Ely  
see p. 30

(E STA)  
B.M. : dir. Elev. Rod:

52.02 = SW 4y STATE  
MON

AZUSA + Mildred

Set. chd  
T.B.M. TP Con. Step (5th) = 122.05  
(#5737) 11+40-RT

## BRUNNER (CONT.)

STA.	P.L.	CB	E	CB	P.L.
1475	132.31	131.94 132.31 Fo.37		130.42 131.31 Fo.89	131.31
1460	132.33 131.83 Co.50	132.01 131.83 Co.18		129.42 130.83 F1.41	128.43 130.83 F2.40
1452=MS RT				127.5 130.6=TRCB F3.1	
1440	131.27	131.67 131.27 Co.40		128.95 130.27 F1.32	130.27
H20 RT only				129.76 129.51 Co.25	128.64 129.51 Fo.87
(1428.79 Alley B.C. LT	130.59	131.74 130.59 C1.15			
Alley E.C.	130.56	132.14 130.56 C1.58			
(H1721) Alley at Prop LT (w/ly side alley)	132.10 130.64 C1.46	131.97 130.64 C1.33			
H400 RT only				128.74 128.53 Co.21	127.45 128.53 F1.08

#2 = CB END

#1 = CB  
end RT.2+71.59=  
CB B.C. RT

2+53.3

2+43.3

2+33.3 = Prop  
RT

#2 = CB END LT.

#1 =

(SW 1/4 RT)

2+32.21 = CB  
B.C. LT2+20.29 = Prop  
LT2+16.65 = RT  
only2+09 = MS  
RT

2+00

135.34	133.11
137.65	137.65 37
F 2.31	F 4.5
136.21	
136.92	
F 0.71	
136.13	132.25
136.20	136.20
F 0.07	F 4.0

133.83	
134.40	134.40
F 0.57	

133.08	
133.60	133.60
F 0.52	

133.05	129.74
133.15	133.15
F 0.10	F 3.5

134.15	134.16
134.15	134.15
grade	Co.01
134.35	133.85
	134.35
	F 0.50

133.58	133.86
134.10	134.10
F 0.52	F 0.29

133.74	133.68
	133.74
	F 0.06

132.41	
132.62	132.62
F 0.21	

HAVE INSUR CHG	125.88
(IN)	132.4 = TRCB
	F 6.5

132.58	132.94
133.10	133.10
F 0.52	F 0.16

131.92	128.70
132.09	132.09
F 0.17	F 3.39

BENICIA

(RILEY, N.Y. - LAURETTA)

CT.

RT. (64)

STA.	P.L.	CB.	E	CB.	P.L.
0+95.89 = CB BC Alley	48.65 47.45 C1.20	48.73 47.45 C1.28		47.56 47.94 F0.38	49.80 47.94 C1.86
0+75	46.23	45.88 46.23 F0.35		46.44 46.73 F0.29	46.73
0+50	46.25 44.78 C1.47	44.44 44.78 F0.34		45.29 45.29 Grade	48.03 45.29 C2.74
0+25	43.36	43.12 43.36 F0.24		43.55 43.86 F0.31	43.86
0+10 = CB BCs	45.02 42.50 C2.52	42.47 42.50 F0.03		42.57 43.00 F0.43	46.55 43.00 C3.55
#1	43.98 41.93 C2.05	42.89 41.93 C0.96		44.35 42.80 C1.55	46.3 42.80 C3.5
#2	41.70	43.63 41.70 C1.93		42.93 42.80 C0.13	42.80
#3 = E.C. on Riley	41.40	42.91 41.40 C1.51		42.72 43.00 F0.28	43.00 = EC on RILEY

STA.	P.L.	CB.	E	CB.	P.L.
2+00	53.43	52.98 53.43 F0.45			53.26 53.73 F0.67
1+75	51.95 51.99 F0.04	51.75 51.99 F0.24			52.29 52.49 F0.20
1+50	50.56	50.49 50.56 F0.07			50.94 51.06 F0.12
ALLEY CB 1+23.89 BC	49.51 49.05 C0.46	48.66 49.05 F0.39			50.45 49.55 C0.90
ALLEY E.C.	48.90	48.66 48.90 F0.24			50.45 47.40 C1.05
(1+19.79) ALLEY AT Prop (N.Y.)	49.51 48.97 C0.54	49.55 48.97 C0.58			50.80 49.47 C1.33
ALLEY AT (0+99.89) Prop. (54)	48.65 47.82 C0.83	48.75 47.82 C0.93			49.64 48.32 C1.32
ALLEY E.C.	47.75	48.73 47.75 C0.98			47.56 48.25 F0.69

BENICIA (Riley - N<sup>W</sup> 4)  
Cont.

STA.	P.L.	CB	E	CB	P.L.
CHK			56.62 = 56.60 = NE BP		
				BENICIA LAURETTA	

0+05 = CB  
BC RT  
(NE 4) #1 RT  
0-15 E only

0-07.5 LT  
only

32.90	34.88	
35.26	35.26	3.5.40 PAY
F2.36	F0.38	

0-27.28 = CB  
BC LT  
(NW 4)  
RET.  
#1 (Line only)

32.60	35.15	
35.10	35.10	
F2.50	00.05	

#2 = CB end

34.95	33.55	
	34.95	
	F1.40	

35.64 CHK. EXIST.  
35.60 35.60 #2

(Line only) #1

IND. EXIST CO

#1 54.23

meat EXIST

54.98

(stubs' RT LT)

0-55 = CB BC  
RT  
(SE 4) RET

30.86	TR. COVN	
34.30 = PAY.		
F3.44		

35.00 PAY

35.09	35.30
35.40	35.40
F0.31	F0.10

2+09.79 = CB	53.00	53.58	54.82	55.06
BGS	54.00	54.00	54.50	54.50
	F1.0	F0.42	00.32	00.56

0-70 R. Grade  
only

31.96	
34.30	
F2.34	

35.09
34.80
00.29

BENICIA -  
LAURETTA

(0+0) = N.L. GAINES to Ely

B.M. DIF. Elev Rod:

33.87 = E MON  
BENICIA &  
GAINES

BENICIA :

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GAINES - to RILEY

STA.	LT. P.L.	CB	E	CB	RT-Ely P.L.
					35.14
					35.75
					F0.61
					35.32
					36.05
					F0.73
					36.14
					36.15
					chk. 36.15 EXIST #2

35.10 PAY

3.5.40 PAY

35.14	35.67
35.75	35.75
F0.61	F0.08

#1

#2

BENICIA (GAINES to RILEY) - (Cont)

LT.

RT/ELY

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
1+27.50	33.09	33.51 33.09 Co.42		34.10 33.59 Co.51	33.59						
1+07.50	32.59 32.39 Co.20	32.47 32.39 Co.08		32.88 32.89 Fo.01	29.47 32.89 F3.42	#3 = E.C. RILEY	40.90	41.18 40.90 Co.28		42.68 42.50 Co.18	42.50 E.C. RILEY
0+91.34-Nly end inlet	32.19 32.17				32.70 chk 32.67 -	#2	41.02	41.27 41.02 Co.25		42.65 42.12 Co.53	42.12 #2
0+83.54 end EXIST inlet	32.16			32.67	32.67	#1	41.00	41.38 41.00 Co.38		42.61 41.95 Co.66	41.95 #1 (SEly)
0+67.5	32.44	32.37 32.44 Fo.07		32.87 32.94 Fo.07	32.94	(SWly) 2+37.90=CB BC'S BENICIA - RILEY	41.22 40.71 Co.51	41.35 40.71 Co.64		42.21 41.21 Cl.00	42.56 41.21 Cl.35
0+47.50 = B.V.C	32.38 33.18 Fo.80	32.98 33.18 Fo.20		33.43 33.68 Fo.25	30.37 33.68 F3.31	2+12.90	38.91	38.69 38.91 Fo.22		40.86 39.42 Cl.44	39.42
0+30 LT. only	33.94	33.66 33.94 Fo.28				1+87.90 20.4	37.63 37.13 Co.50	37.14 37.13 Co.01		39.39 37.64 Cl.75	39.68 37.64 Cl.04
0+26.25 RT. only				34.32 34.71 Fo.39	34.71	1+67.5 20	35.70	35.66 35.70 Fo.04		36.37 36.21 Co.16	36.21
0+12.5 LT. only	32.86 34.70 F1.84	34.25 34.70 Fo.95				1+47.50 = EVL	34.91 34.28 Co.63	34.14 34.28 Fo.14		34.83 34.78 Co.05	34.79 34.78 Co.01

CO/USA -

GAINES to RILEY

STA	RT (ELY)			RT (ELY)		
	P.L	CB	E	P.L	CB	E
0+75	46.94	46.41 46.94 Fo.53		47.33 47.45 Fo.12	47.45	
0+50	46.05 45.78 Co.27	45.44 45.78 Fo.34		46.76 46.29 Co.47	46.96 46.29 Co.67	
0+25	44.62	44.78 44.62 Co.16		44.74 45.12 Fo.38	45.12	
0+03.83 = CB BC LT (N'W'ly)	44.41 43.64 Co.77	43.49 43.64 Fo.15		43.89 44.14 Fo.25	46.36 44.14 C2.22	
#1 LT	43.35					
0-14.26 RT only				43.39 43.21 Co.18		
0-32.53-CB B.C RT (N'W'ly)				42.61 42.29 Co.32	43.94 42.29 C1.65	
#1 RT				41.41 41.79 Fo.38	41.79	
#2 = CB end RT				41.30 41.30 C2.21	41.30	
0-48.53 = N.L GAINES E'ly					40.00	
0+00 = N.L GAINES W'ly						

STA	LT			RT (ELY)		
	P.	CB	E	P.L	CB	P.L
#3 = E.C's ON RILEY	55.00	54.03 55.00 Fo.97				
#2	55.00	53.98 55.00 F1.02				
#1	54.95	53.97 54.95 Fo.98				
2+37.58 = CB BC's	55.88 54.50 C1.38	53.19 54.50 Fo.71				
2+25	53.92	53.62 53.92 Fo.30				
2+00	54.23 52.75 C1.48	52.58 52.75 Fo.17				
1+75	57.59	51.62 51.59 Co.03				
1+50	51.70 50.42 C1.28	50.70 50.42 Fo.22				
1+25	49.26	48.98 49.26 Fo.28				
1+00	48.15 48.10 Co.05	47.80 48.10 Fo.30				

= EXIST  
cb end

54.42  
54.42  
grade

53.07  
53.25  
Fo.18

52.08  
52.10  
Fo.02

51.08  
50.93  
Co.15

49.45  
49.77  
Fo.32

47.94  
48.60  
Fo.66

# COLUSA

(YUMA to GAINES)

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
(A.G. only) 0+00 LT only = N.L. Yuma	14.52 14.00 10.52										
0-05 RT only				13.76 14.10 Fo.34	14.13 14.10 Co.03	1+15 = BYG 1+00	37.06 32.09 C4.97	32.51 32.09 Co.42		31.08 31.59 Fo.51	31.20 31.59 Fo.39
0-25 = E Yuma	11.75 = T.F. fare			11.89 12.40 Fo.51	12.54 12.40 Co.14	0+75	32.25 25.82 C6.43	25.59 25.82 Fo.23		28.94 29.33 Fo.39	29.33
0-45 RT only				10.68 11.27 Fo.59	11.27	0+50	21.90	21.34 21.90 Fo.56		25.32 25.57 Fo.25	25.20 25.57 Fo.37
#2 = end ca RT 35° 25' 50"	10.90	10.20 10.90 Fo.70				0+35 = E.V.C	24.01 19.55 C4.46	19.00 19.55 Fo.55		21.47 21.81 Fo.34	21.81
#1 Line only						0+15	16.44	16.03 16.44 Fo.41		19.17 19.55 Fo.38	19.00 19.55 Fo.55
0-70 = CB BC LT. = Beg CB RT.	10.92 10.35 Co.57	10.83 10.35 Co.48		9.86 10.35 Fo.49	11.26 10.35 Co.91	0+08 = CB BC LT.	15.58 15.35 Co.23	14.92 15.35 Fo.43		16.26 16.55 Fo.29	16.55
Set T.B.M. B.M.	= 11.96	= Sw 1/4 Corn				#1 = end ca	13.40	14.63 13.40 C1.23			
				7.61 = Con Mon							
				E. Line Colusa &							

LT.

RT (E4)



Sly 15' Line Yuma - w'ly

Colusa - (Yuma to Gaines) - Cont.

STA	P.L	CB	E	RT(EV)	P.L
2+19.96 = GAINES	41.29	41.23 41.29 Fo.06			41.14 TP 40.50 = RT Co.64
H95 LT ONLY CB.	40.79 40.35 Co.44	40.26 40.35 Fo.09			39.42 R.G. only 40.30 Prop. inc Fo.88
#1 RT = CB END →				40.13 40.30 Fo.17	#1 40.30
H84.96 = CB BC RT. ONLY				39.05 39.40 Fo.35	39.22 39.40 Fo.18
H75	39.05	38.90 39.05 Fo.15		38.20 38.55 Fo.35	38.55
H55	38.60 37.23 C1.37	36.88 37.23 Fo.35		36.27 36.73 Fo.46	36.65 36.73 Fo.08
H35	34.92	34.55 34.92 Fo.37		33.84 34.42 Fo.58	34.42

(R. grade)

2+45 RT only

40.75  
41.00  
Fo.25

EXIST  
CB  
#2 = CH 42.32 42.32

CHK 42.33

#1 42.04 41.94  
42.04  
Fo.10

2+30 = 41.88 41.87  
CB BC 41.57 41.57  
LT Co.31 Co.30

2+27.49 = 41.50 41.50  
P.L. BC



RILEY

- AZUSA to BENICIA -

RT (524)

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LT.						RT.					
STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
1450	34.87 33.19 C1.68	33.16 33.19 F0.03		32.56 32.69 F0.13	32.57 32.69 F0.12	3+75	40.33	40.68 40.33 C0.35		39.89 39.83 C0.06	39.83
1+25	32.40	32.17 32.40 F0.23		31.92 31.90 C0.02	31.90	3+50	41.57 39.54 C2.03	40.07 39.54 C0.53		39.19 39.04 C0.15	39.47 39.04 C0.43
1+00	32.76 31.61 C1.15	31.49 31.61 F0.12		31.09 31.11 F0.02	31.09 31.11 F0.02	3+25	38.75	39.09 38.75 C0.34		38.41 38.25 C0.16	38.25
0+85.5 = 8.70	Commercial Drive RT										
0+75	30.81	30.79 30.81 F0.02		30.23 30.31 F0.08	30.31	3+00	41.18 37.95 C3.23	38.04 37.95 C0.09		37.58 37.45 C0.13	37.87 37.45 C0.42
0+68 = M.S. LT.	32.1 30.6 = TP C1.5					2+75	37.16	37.29 37.16 C0.13		36.92 36.66 C0.26	36.66
0+50	32.62 30.02 C2.60	30.95 30.02 C0.93		30.14 29.52 C0.62	30.05 29.52 C0.53	2+50	40.09 36.37 C3.72	36.69 36.37 C0.32		36.06 35.87 C0.19	36.27 35.87 C0.40
0+25	29.23	30.14 29.23 C0.91		29.71 28.73 C0.98	28.73	2+25	35.57	35.92 35.57 C0.35		35.20 35.07 C0.13	35.07
0+10 = CB ECS	31.08 28.75 C2.33	29.52 28.75 C0.77		29.39 28.25 C1.14	29.26 28.25 C1.01	2+00	36.38 34.78 C1.60	34.86 34.78 C0.08		34.45 34.28 C0.17	34.66 34.28 C0.38
0+00 = E.L. AZUSA						1+75	33.99	33.75 33.99 F0.24		33.31 33.49 F0.18	33.49

B.M. (See Pg 20)

STA. P.L. CB E CB P.L.

STA. P.L. CB E CB P.L.

For Ret's  
See BENICIA  
P7

446.5±  
W.L. BENICIA

	44.09	42.91			
4+08.50=	41.40	41.40		41.18	41.29
CB BC's	2.69	1.51		40.90	40.90
				40.28	40.39

4+00	44.15	41.25		40.73	41.03
	41.13	41.13		40.63	40.63
	3.02	0.12		40.10	40.40

RILEY ÷

- BENICIA to COLUSA -

STA.	P.L	CB	E	CB	P.L
1+28=B.V.C	47.82 46.03 C1.79	45.78 46.03 Fo.25		45.54 45.53 Co.01	45.64 45.53 Co.11
1+14	45.67	45.33 45.67 Fo.34		45.45 45.17 Co.28	45.17
1+00	47.38 45.33 C2.05	45.02 45.33 Fo.31		44.72 44.83 Fo.11	44.75 44.83 Fo.08
0+81.5=Sew (11) LT	47.34 40.00 PL C7.34		47.3 38.3 C9.0		
0+75	44.70	44.28 44.70 Fo.42		44.33 44.20 Co.13	44.20
0+66.5=WS LT	47.25 44.5 TP C2.75 CB				
0+50	46.37 44.06 C2.31	43.63 44.06 Fo.43		43.74 43.56 Co.18	43.89 43.56 Co.33
0+25	43.43	43.17 43.43 Fo.26		42.53 42.93 Fo.40	42.93
0+08= CB EC'S	46.04 43.00 C3.04	42.72 43.00 Fo.28		42.68 42.50 Co.18	43.03 42.50 Co.53

(See Pg 39 For Ret's).

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STA.	P.L	CB	E	CB	P.L
3+25	52.95	52.77 52.95 Fo.18			52.08 52.25 52.25
3+03.2 LT only	52.10	51.74 52.10 Fo.36			Fo.17
3+00	53.66 51.98 C1.68	51.77 51.98 Fo.21			51.64 51.37 Co.27
2+75	51.08	50.74 51.08 Fo.34			50.41 50.48 50.48
2+50	50.64 50.17 Co.47	50.04 50.17 Fo.13			49.60 49.60 grade Co.45
2+25	49.28	49.01 49.28 Fo.27			48.15 48.72 48.72
2+00	49.51 48.37 C1.14	48.12 48.37 Fo.25			47.49 47.84 47.84 Fo.35 Co.05
1+75	47.48	47.45 47.48 Fo.03			46.63 46.96 46.96 Fo.33
1+68=E.V.C	48.85 47.22 C1.63	47.08 47.22 Fo.14			46.42 46.71 46.71 Fo.29 Fo.25
1+48	46.57	46.73 46.57 Co.16			45.73 46.06 46.06 Fo.33

RILEY  
(- BENICIA to COLUSA -) CONT.

(NELY) LT.

RT.

STA. P.L. CB. E CR. P.L.

CHK: 56.42 = 56.40 = CH. NELY CB  
BC. ON RILEY  
AT COLUSA

For Ret's See  
Colusa Pg 31 + 41

4+13.20 =  
W.L. Colusa

(5.88)	58.71	55.90	54.03	55.64
4+03.20 =	56.00	56.00	55.00	55.00
CBEC'S:	02.71	F0.10	F0.97	00.64

4+00	55.87	55.66 55.87 F0.21	53.90 54.89 F0.99	54.89
------	-------	-------------------------	-------------------------	-------

3+75	54.90	54.65 54.90 F0.25	53.42 54.01 F0.59	54.01
------	-------	-------------------------	-------------------------	-------

3+50	56.41 53.92 C2.49	53.86 53.92 F0.06	52.89 53.13 F0.24	54.06 53.13 00.93
------	-------------------------	-------------------------	-------------------------	-------------------------

## AZUSA:

48

GAINES to RILEY

LT

LT

RT (Ely)

STA.	P.L.	CB	E	CB	RT (Ely) P.L.
1+336 = BYC	27.27 27.20 Co.07	26.90 27.20 Fo.30		27.27 27.50 Fo.23	28.04 27.50 Co.54
1+25	27.39	27.10 27.39 Fo.29		27.57 27.69 Fo.12	27.69
1+00	28.52 27.93 Co.59	28.25 27.93 Co.32		28.00 28.23 Fo.23	28.75 28.23 Co.52
0+75	28.46	28.39 28.46 Fo.07		28.39 28.76 Fo.37	28.76
0+50	29.80 29.00 Co.80	28.73 29.00 Fo.27		29.09 29.30 Fo.21	30.04 29.30 Co.74
0+25	29.54	29.24 29.54 Fo.30		29.66 29.84 Fo.18	29.84
0+08 = CB BC	30.66 29.90 Co.76	29.53 29.90 Fo.37		30.02 30.20 Fo.18	30.37 30.20 Co.17
#1 = CB END	29.95	30.11 29.95 Co.16		30.92 30.30 Co.62	30.30 CB END
[0+00 = N.L.] GAINES	30.87 29.95 Co.92			30.98 30.30 Co.68	

STA.	P.L.	CB	E	CB	RT (Ely) P.L.
2+83.57 = CB B.C. RT SELY	27.17	28.00 27.17 Co.83			27.19 28.17 27.47 27.47 Fo.28 Co.70
2+68.6	26.93	27.89 26.93 Co.96			27.04 27.23 27.23 Fo.19
2+53.6 = E.V.C	27.67 26.70 Co.97	27.39 26.70 Co.69			26.75 27.72 27.00 27.00 Fo.25 Co.72
2+33.6	26.51 26.55 Fo.04	26.45 26.55 Fo.10			26.52 27.60 26.85 26.85 Fo.33 Co.75
2+13.6	change to meet inlet → 26.49	26.07 26.46 Fo.39			26.11 change to meet inlet 26.74 26.79 Fo.63
(2+02.57 = E) inlet DWG:	26.42 26.42 26.49				26.68 26.73 26.79 26.79
1+93.6	change to meet inlet → 26.52	26.46 26.49 Fo.03			26.43 change to meet inlet 26.79 26.82 Fo.36
1+73.6	26.46 26.65 Fo.19	26.13 26.65 Fo.52			26.54 27.81 26.95 26.95 Fo.41 Co.86
1+53.6	26.80	26.38 26.80 Fo.42			26.79 27.18 27.18 Fo.39

AZUSA

- GAINES to RILEY - (CONT.)

AZUSA

- RILEY to LAURETTA -

49

STA. P.L. CB E CB P.L. RT. (E'ly)

STA. P.L. CB E CB P.L. RT. (E'ly)

\* [0+00 Ahead] 28.95  
 28.13  
 29.82  
 29.95  
 3+43.57 LT. 28.13 28.68  
 only C1.82 Co.55  
 28.13  
 28.13  
 3+23.57 LT. 27.81 28.33  
 only 27.81 Co.52  
 (3+18.57 = Gu. TT grade RT)  
 28.80 28.58  
 3+03.57 LT. 27.49 27.49  
 only C1.31 C1.09  
 #3 = E.C. 29.39 28.25  
 ON RILEY 28.25 C1.14  
 #2 = 29.24 27.80 27.80  
 27.80 C1.44  
 #1 29.23 27.75 27.75  
 C1.48

0+72 = W.S. 29.50  
 29.28 = TP 48  
 LT. Co.22  
 0+50 29.61 29.05 28.65 31.10  
 28.93 28.93 28.84 28.84  
 Co.68 Co.12 Fo.19 C2.26  
 0+40 = W.S. 31.80  
 RT. 28.70 = TP 48  
 C3.10  
 0+27 = SEW  
 LAT (13) LT. 29.28 21.60 PL. 21.3 E  
 C7.68  
 0+25 28.53 28.79 28.21  
 28.53 28.50 28.50  
 Co.26 Fo.29  
 0+22 = W.S. 29.28 28.48 TP 48  
 LT. Co.80  
 0+10 = CB BC 28.23 30.20  
 RT. (NE'ly) 28.30 28.30  
 Fo.07 C1.90  
 #1 28.72 28.35  
 28.35 28.35  
 Co.37  
 #2 28.62 28.42 28.42  
 28.42 28.42  
 Co.20  
 29.52 28.75 28.75  
 28.75 28.75  
 Co.77  
 #3 = E.C. RILEY  
 [0+00 = N.L.]  
 RILEY

T.B.M. = 31.56 = ch+ CONFD TN Pole #5400 NE Cor. GAINES + AZUSA

## AZUSA: (CONT.)

- RILEY to LAURETTA -

50

LT.		RT (ELY)		LT.		RT (ELY)					
STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
				29.61		#2					
1423.93=				29.83	29.83	EXIST. CB					
ALLEY B.C.				F0.22		#1	31.83 chk				
RT.							31.85	31.85		31.20	31.20
ALLEY E.C.				29.61							
				29.86	29.86						
				F0.25							
ALLEY AT				29.62	29.60	2+09.86=CB	30.91	31.20		30.76	31.13
Prop.				29.88	29.88	B.C.	31.50	31.50		31.00	31.00
				F0.26	F0.28	= NLY end	F0.59	F0.30		F0.24	CO.13
						INLET-RT, only					
1+00 LT.	29.53	29.47									
only	29.73	29.73									
	F0.20	F0.26									
ALLEY AT				29.46	29.39	2+01.52=SLY				30.89	30.89
Prop.				29.61	29.61	end inlet					
				F0.15	F0.22	RT, only					
ALLEY E.C.				29.18		2+00 LT	30.68	31.11			
				29.59	29.59	only	31.33	31.33			
				F0.41			F0.65	F0.22			
0+95.93=				29.18		1+75	30.93	30.57		30.08	
ALLEY B.C.				29.46	29.46			30.93		30.52	30.52
RT				F0.28				F0.36		F0.44	
0+77 SEW.						1+50	30.00	30.32		29.75	29.68
LAT (12) LT.	29.48		21.9E				30.53	30.53		30.18	30.18
	22.20 P.L.						F0.53	F0.21		F0.43	F0.50
	C7.28	29.74		28.82							
0+75	29.33	29.33		29.18	29.18	1+25 LT	30.13	29.84			
		CO.41		F0.36		only		30.13			
								F0.29			

(moved sly  
Sec 18, 22)

AZUSA

- LAURETTA to MILDRED -

CHK: 49.29 = 100' WLY R.P. R.R. SPIRO = T.B.M

LAURETTA to MILDRED						MILDRED to LAURETTA						
STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.	
ALLEY E.C	41.78	42.52 41.78 Co.74		40.60 41.28 Fo.68	41.28							
1+21.12= ALLEY BC	42.60 41.41 C1.19	42.52 41.41 C1.11		40.60 40.91 Fo.31	41.78 40.91 Co.87		2+60.24= CB BC'S	51.19 51.00 Co.19		50.26 51.00 Fo.74	50.23 50.50 Fo.27	51.03 50.50 Co.53
1+00	41.94 39.88 C2.06	39.68 39.88 Fo.20		38.83 39.37 Fo.54	38.30 39.37 F1.07		2+35	49.28		48.72 49.28 Fo.56	48.60 48.78 Fo.18	48.78
0+75	38.06	37.81 38.06 Fo.25		37.19 37.55 Fo.36	37.55		2+10	47.77 47.58 Co.19		47.13 47.58 Fo.45	46.58 47.08 Fo.50	45.13 47.08 F1.95
0+50	38.13 36.22 C1.91	35.96 36.22 Fo.26		35.26 35.72 Fo.46	35.19 35.72 Fo.53		1+85	45.88		45.46 45.88 Fo.42	44.09 45.38 Fo.49	45.38
0+25	34.40	34.33 34.40 Fo.07		34.10 33.90 Co.20	33.90		1+60	44.75 44.18 Co.57		43.90 44.18 Fo.28	43.21 43.68 Fo.47	45.19 43.68 C1.51
0+10=C.B.C'S	34.05 33.30 Co.75	34.04 33.30 Co.74		33.48 32.80 Co.68	33.47 32.80 Co.67		1+49.12= ALLEY BC	43.93 43.43 Co.50		43.25 43.43 Fo.18	42.64 42.93 Fo.29	44.94 42.93 C2.01
#1	32.70	32.70		32.40	32.40		ALLEY E.C	43.24		43.25 43.24 Co.01	42.64 42.74 Fo.10	42.74
#2 Meet EXIST							ALLEY AT Prop	43.26		43.82 43.26 Co.56	44.91 42.76 C2.05	42.76
0+00=N.L LAURETTA							ALLEY AT Prop	41.80		42.61 41.80 Co.81	41.60 41.30 Co.30	41.30



AZUSA

(CONT.)

52

- LAURETTA to MILDRED -

STA. P.L.

#3 = E.C  
MILDRED

50.93 change to meet  
51.78 in/kt  
51.80  
FO.85

#2 RT only

50.59  
51.40 51.40  
FO.81

#1 CBEND ON LT  
51.16 51.38  
51.20 51.20  
FO.04 CO.18

50.48  
51.30 51.30  
FO.82

CLARK  
WENTWORTH  
ABRENNILLA  
BIRMING  
8-21-61  
MO 14503

STAKE SEW REPLACEMENT  
ALLEY Bet. Pynchon & 47th

53

STA:	GRADE
1+00	15.79 105.57 C 10.22
0+75	13.91 105.14 C 8.77
0+50	11.92 104.72 C 7.20
0+25	110.53 104.29 C 6.24
0+00 = EXIST. M.H.	103.87 = F.L.

STA:	GRADE:
2+50	18.67 108.12 C 10.55
2+25	20.48 107.69 C 12.79
2+00	21.02 107.27 C 13.75
1+75	20.84 106.84 C 14.00
1+50	19.92 106.42 C 13.50
1+25	117.77 105.99 C 11.78

1.78

Stubs 5' x 7' (w/4) E

used F.L. EXIST. M.H. AS 103.87 (PLAN)

(OUT)

118.77 = N.W. B.P. LOGAN  
& 47th

B.M.

Clark  
Wentworth  
A. BRENINIA  
Berning  
8-22-61  
W.O. 14503

SEW. REPLACEMENT: 54  
ALLEY bet. DEL MONTE +  
SANTACRUZ: SUNSET CLIFFS  
TO EBERS

STA:

GRADE

STA:

GRADE:

1+00

45.78  
40.48  
C 5.30

0+75

45.20  
38.58  
C 6.62

0+50

44.85  
36.69  
C 8.16

0+25

43.98  
34.79 = F.L.  
C 9.19

52y  
3+04 = D.END

17.09  
109.04 = F.L.  
C 8.05

3+00 (not set)

1.7%

2+75

117.10  
108.54  
C 8.56

Note:  
EXIST. ALLEY PAV. CONC.

B.M.

(meet) 32.89 = F.L. EXIST.

37.05 = S.E. L+T.

DEL MONTE + Sunset CLIFFS

7.59  
8.0  
(Set ch's 5' L+T)

STA:	GRADE:	STA:	GRADE
2+50	56.47 51.87 C 4.60	3+75	69.57 60.39 C 9.18
2+25	54.24 49.97 C 4.27	3+50	66.59 59.03 C 7.56
2+00	52.05 48.07 C 3.98	3+29.6 = <u>E</u> EXIST. M.H. (meet)	57.91 = <u>E</u> EXIST. FIL
1+75	49.95 46.17 C 3.78	3+25 (Not-Set)	
1+50	48.13 44.28 C 3.85	3+00	61.02 55.66 C 5.36
1+25	46.75 42.38 C 4.37	2+75	58.69 53.76 C 4.93

5.469

—

7.592

—

STA:

GRADE:

Note:

(6+59.7)

= EXIST M.H. & Alley 75.96 = F.L. <sup>EXIST.</sup>  
& EBERS+  
= end planned replacement  
5+00 = end grades set78.06  
67.23  
C10.83

4+75

77.31  
65.86  
C11.45

4+50

(Set 5' 7" E)

5-469%

76.36  
64.49  
C11.87

4+25

(Set 5' 7" E)

74.73  
63.13  
C11.60

4+00

72.36  
61.76  
C10.60

CLARK  
WENTWORTH  
ANDERSON  
VARONFOLIS  
8-8-62  
W.O. 33248

STORM DRAIN:  
53rd & Trojan  
(53rd Ely along N.Y. Line)  
LOTS 56-7 + PORTION 8  
ANDREW JACKSON TRACT

Ref: City notes: DWG: 10245-D 57

CHK:

STA:

2+23.46 = Ely Fe. sidewalk  
Note: As per Office request 8" pipe  
= added to Drains

GRADE:

342.85  
340.00 Fl. pipe  
C 2.85

STA:

Grade

2+15.46

342.65  
339.99  
C 2.66

0+34.96 =  
C 5" RT 15"  
PIPE

Stubs 5' LT  
&

341.21  
338.41  
C 2.80

1+93.46

341.98  
339.47  
C 2.51

0+29.21 = &  
INLET-FRAME

0.5' RT

339.60  
338.38  
C 1.22

1+71.46 = grade Brk

341.82  
339.08  
C 2.74

NAILS 5' & 10' LT & Structure  
(grade on 5' NAIL)

1+37.34

341.42  
338.92  
C 2.50

0+03.79 = &  
DRAIN-BOX  
Stubs 6' & 12' RT on split.  
(grade on 6' RT)

338.44  
337.93  
C 0.51 = FLL

1+03.21

340.93  
338.75  
C 2.18

0+00 = CB Fc  
Footlet

338.17  
TP CB. 338.45  
FO. 28

338.17  
337.87 = FL. GUTT.  
C 0.30

338.12 = elev  
overhead Box

0+69.09

341.04  
338.58  
C 2.46

B.M.

338.45 = TP CB & 0-5.77  
City notes:

CLARK  
WENTWORTH  
ANDERSON  
VARRONFAKIS  
8-16-62  
W.O. 33196

ALLEY BIK 287: PAC-BEACH  
GRESHAM to HAINES  
(Bet. Oliver & Reed)

Ref: City Notes (HATCH)  
Dwg: 10317-D

58

STA.	GRADE			STA.	LT.	E	RT.
	LT.	E	RT.				
0+85	28.70 28.77 Fo.07	Stub 0.45' BK	28.21 28.47 Fo.26	2+20		30.20 30.54 Fo.34	30.41 30.24 Co.17 chx 2' BK
0+60	28.73 28.69 Co.04	Stub 0.45 BK	28.30 28.39 Fo.09	1+95		29.81 29.90 Fo.09	29.45 29.60 Fo.15 Stub 5' BK
0+35	29.08 28.61 Co.47	chx 2' BK	28.58 28.31 Co.27	1+70		29.26 29.26 Grade	28.89 28.96 Fo.07
0+20	28.80 28.56 Co.24	28.01 Stub 1' BK	28.68 28.26 Co.42	1+50		29.17 28.97 Co.20	28.48 28.67 Fo.19
0+00 = E.L. GRESHAM	28.61 Meet EXIST GUT.		28.29 Meet EXIST GUT.	1+35		28.76 28.93 Fo.17	28.14 28.63 Fo.49
B.M.	28.08 = E.P.K. Alley			1+10		28.66 28.85 Fo.19	27.92 28.55 Fo.63

B.M.  
city notes  
(HATCH)

BIK 287 + E.P.K. 7' Line GRESHAM

STA.	LT.	RT.	STA.	LT.	RT.
3+55	39.59 39.41 Co.18	39.74 39.11 Co.63	4+78.92 = B.V.C. Stub 1.90' BK	45.26 44.85 Co.41	44.86 44.75 Co.11 ch x 2' BK
3+30	38.12 37.60 Co.52	37.36 37.30 Co.06	4+60 ch x 2' BK	44.65 44.45 Co.20	44.64 44.30 Co.34 ch x 2' BK
3+05 P.K 0.56' BK	36.68 35.19 Co.89	35.84 35.49 Co.35 Stub 0.9' BK	4+40	44.13 44.03 Co.10	43.85 43.82 Co.03
2+90 Stub 0.8' BK	35.82 34.70 Cl.12	35.31 34.40 Co.91 NAIL 1.05' BK	4+20	43.93 43.61 Co.32	43.33. 43.34 Fo.01
2+65	32.73 33.07 Fo.34	33.50 32.77 Co.73 NAIL 0.85' BK	4+00 ch x 2' BK	43.41 42.67 Co.74	42.22 42.37 Fo.15
2+40	32.21 31.45 Co.76	30.84 31.15 Fo.31 ch x 2' BK	3+80	41.00 41.22 Fo.22	41.04 40.92 Co.12





STA:	LT	RT	STA:	LT	RT
2+30 = Sew LAT #1 RT Stub 5 BK ALINE		20.21 = E. CONN.			
		27.27 22.60 = F.L. C4.67 Prop			
2+10	27.39 27.32 C0.07	26.95 27.10 F0.15	3+60	30.33 29.64 C0.69	30.00 29.35 C0.65
1+85	27.61 26.94 C0.67	26.85 26.73 C0.12	3+35 NAIL 0.58 BK	30.25 29.26 C0.99	29.43 28.98 C0.45
1+60	26.91 26.55 C0.36	26.61 26.35 C0.26	3+10 NAIL 1.02 BK	30.63 28.87 C1.76	28.85 28.60 C0.25
1+40	26.81 26.32 C0.49	26.60 26.14 C0.46	2+85 NAIL 0.40 BK	29.10 28.49 C0.61	28.44 28.23 C0.21
1+25	26.71 26.20 C0.51	26.45 26.04 C0.41	2+60 P.K 0.36 BK PAV.	28.87 28.10 C0.77	28.62 27.85 C0.77
1+00 NAIL 1.36 BK E. PAV.	27.08 26.00 C1.08	26.40 25.88 C0.52	2+35	28.30 27.71 C0.59	27.33 27.48 F0.15

ALLEY BIK 288 (CONT.)

CHK:

= 28.08 (See Pg. 58)

STA:	LT.	E	RT.
4+99.94 = W. L. GRESHAM	28.63 (meet)		28.58 meet
4+90 stub 0.65' BK	30.13 29.11 C 1.02	28.61 chk 3 BK	29.58 28.91 C 0.67
4+70 = BYC Stub 0.7' BK	30.38 29.83 C 0.55	Stub 0.45' BK	30.03 29.53 C 0.50
4+50 Stub 0.6' BK	30.52 29.90 C 0.62		30.35 29.60 C 0.75
4+25 chk 2' BK	30.77 29.99 C 0.78	Stub 0.5' BK	30.06 29.69 C 0.37
4+00	30.49 30.07 C 0.42		29.94 29.77 C 0.17
3+80	30.34 29.95 C 0.39		29.83 29.65 C 0.18

Clark

## CLIFFRIDGE

WATER-MAIN  
(10' SLY E ST.)8-22-62  
W.D. 62973

STA:

GRADES

1+00

362.72  
359.13  
C 3590+50.54 = C  
Fire-HYD. RTTp  
CB 362.02  
362.80  
grade-stub  
5' LT & MAIN F0.78St stub  
line-only  
TP Brow

0+50

362.11  
358.83  
C 328

0+20 = C Double W.S. LT.

(Stub 5' BK P. Line)  
LT.362.61  
362.64 = Tpcb  
F0.03

0+00 WATER-Line

= P.L.B.C. STA  
# 7+36.45 DWG  
10371-2-D361.64  
358.52  
C 3.12

T.B.M

371.99 = RP to ERI Co Toll Scenic PL.

grade (FL. Line) W. MAIN = 4.0 below C PAV.

REF: Revised Red-Line DATA by 63

AKINS - 8-21-62

DWG: 10371-1-D &amp; 10371-2-D

STA:

GRADES

4+00

363.75  
360.93  
C 282

3+50

363.35  
360.63  
C 272

3+00

363.32  
360.33  
C 299

2+50

363.48  
360.03  
C 345

2+00

363.05  
359.73  
C 332

1+50

363.03  
359.43  
C 3.60

Stubs 5' LT (ONLY E W. MAIN)

STA:

GRADES

5+71.77 = PT. INT. & MAIN  
LA JOLLA SCENIC PL. C 4.6

367.2  
362.6

5+42.95

365.8  
362.3  
C 3.5

5+30.17 = E. NYD 21.5 LT  
Prop. P. & L. LT SET Stub 5' N' 24' E NYD.  
ST. STA 2+0.35

364.54 TP  
365.75 CB  
F 1.27

5+14.13

365.32  
361.76  
C 3.56

4+85.31

365.5  
361.4  
C 4.1

4+56.49 =  
B. C

364.98  
361.27  
C 3.71

4+50 Not set

CLARK  
WENTWORTH  
ANDERSON  
KARONFAKIS  
8-28-62  
W.O. 32077

RET-WALL  
ALLEY BIK 231  
UNIV.-HT'S:

GRADES:

FTG-WALL

TP.PAV.	TP.WALL	1 <sup>ST</sup> STAGE	2 <sup>ND</sup> STAGE
---------	---------	-----------------------	-----------------------

0+39=end-wall	277.82 276.07	277.82 276.57	277.82 270.00
		C1.25	C7.82

0+25=grid BIK FTG-wall	269.00 273.53	269.00 274.03	269.00 269.00
		F 5.03	grade F1.00

0+15=grade BIK FTG-wall	268.72 271.72	268.72 272.22	268.72 268.00
		F 3.50	C 0.72 F 0.28

=Beg-wall	268.30	268.30	268.30
0+00=E.L. Richmond	269.00	269.50	268.00
		F 1.20	C 0.30

Ref: City Notes : G-19 65  
10-24-61  
Shorey  
DWG: #10433-D

NLY Prop-Line  
ALLEY

CLX TP  
EXIST  
WALL + 0.55'      10' 1x1  
□ Line only  
0+39  
end

NAIL 5'      10' 1x1  
□ Line only  
0+25

NAIL 5'      10' 1x1  
□ Line only  
0+15

1x1 5'      10' 1x1  
□ Line only  
0+00  
Beg

(grade REF PTS = 1x1, NAILS  
at chx NLY Prop-Line)

CLARK  
WENTWORTH  
ANDERSON  
VARUNFAKIS  
10-23-62  
W.O. 32077

ALLEY BIK 2.31: UNIV. HTS.

Richmond to ALBERT  
bet. Brookres & Cypress

REF: 10433-D: City Notes: [Shorey]

66

[Note: For Ret. wall see Pg 65]

T.B.M. 269.37 = P.K. nail (0-40) E Richmond (Shorey)

STA:	(NLY) LT		(SLY) RT	STA	LT		RT
	(See pg 65)						
0+00 = Prop. L (E.L. Richmond)	269.50 = CB		272.62 CB = 270.97 C1.65	0+90	83.62 283.55 C0.07	Stub 0.55 BK e. Pav.	84.14 283.77 C0.37
(PCB on minus stak's) 'grade' ↓							
0-07	68.78 268.90 CB FO.12	72.01 269.40 CB C2.61	72.01 270.83 C1.18	0+70 ch+ 2' BK	81.86 281.21 C0.65		83.16 281.49 C1.67
0-10 BIK LT. only	68.68 268.74 CB FO.06						
0-14 = BIK RT. only		71.40 269.12 CB C2.28	71.40 270.70 C0.70	0+50 ch+ 2' BK	77.85 278.06 FO.21		81.77 278.36 C3.41
Note: CB stakes 2' BK For uniformity				0+30 RT. only			276.02 274.80 C1.22
0-16 = CB, E.C.S. (9' LT & 10' RT)	68.52 268.62 CB FO.10		271.22 270.66 C0.56				
(Δ = 90°) (4' CB Radii)				0+20 RT. only			275.03 273.10 C1.93
0-20: CB B.C.S.	68.23 268.15 C0.08	268.88 CB	271.25 271.00 C0.25				
Note: Pav. grade = 0.50 below CB				0+10 LT. only			274.77 271.50 C3.27

B.M

289.13 = SEBP HERBERT  
& Brookres

Note: 0.25' acceptance LT. + RT. Pav. width

ALLEY BLK 231 (CONT)

67

STA:	(N'LY) LT.	(S'LY) RT.	STA:	LT.	RT.
2+09.58	288.66 288.37 Cht 0.32 BK e. Pav. Co. 29	89.09 288.37 Co. 72			
1+89.58	288.00 288.07 Cht 1' BK e. Pav. Fo. 07	88.18 288.07 Co. 11			
1+69.79	87.59 287.45 Co. 14	87.52 287.45 Co. 07			
1+50	86.53 286.82 Fo. 29	286.82 286.82 Grade	2+59.58 = w.L ALBERT	meet 286.07	meet 286.17
1+30	285.35 286.08 Fo. 73	86.16 286.10 Co. 06	2+49.58	87.73 287.00 Co. 73	289.18 287.00 C 2.18
1+10	284.24 285.08 Fo. 84	284.92 285.20 Fo. 28	2+29.58 cht 0.25' BK e. Pav.	288.75 288.01 Co. 74	289.21 288.01 C 1.20



CLARK  
ALLEN  
Pekarek  
ONEIL  
W.O. 33439  
Date 8-23-65

Alley Blk "C"  
Redlands GARDENS  
(MADISON to ADAMS)

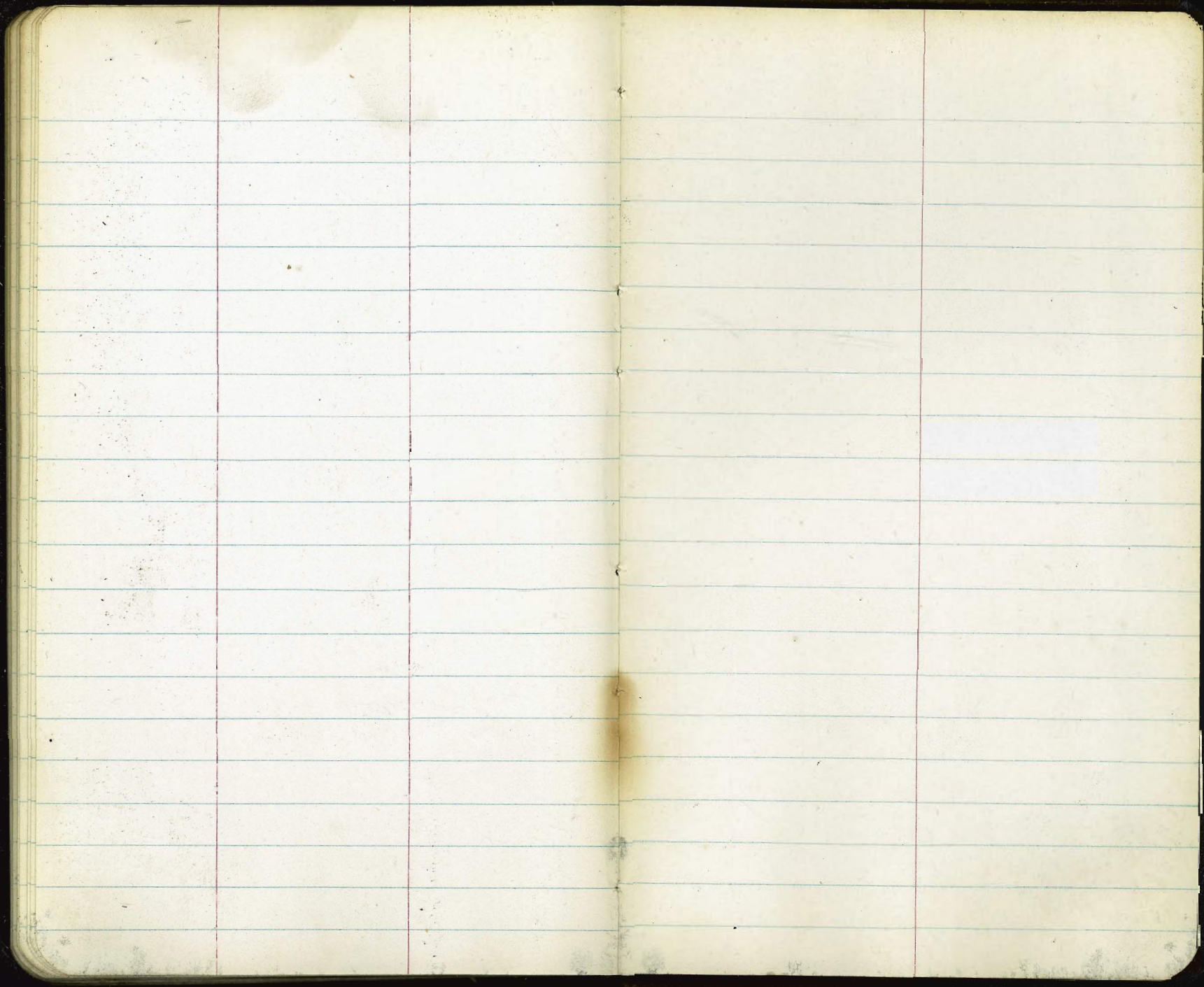
Ref: DWG: # 11838-D W.O. 3343968  
CITY Notes: 216-1745  
(Clark) 11-6-64

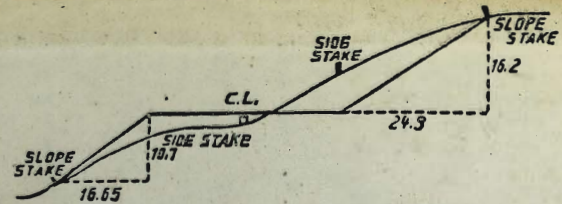
STA:	(W/L) LT.	(E/L) RT.
1+00	50.17 449.56 C 0.61	51.03 449.86 C 1.17
0+85	48.21 448.68 F 0.47	50.25 448.98 C 1.27
0+70 = B.V.C PK 0.85 BK	49.33 449.70 C 1.63	49.40 448.00 C 1.40
0+45 PK 0.70 BK	46.07 446.00 C 0.07	47.20 446.30 C 0.90
0+20 PK 0.78 BK e-pir	45.66 444.30 C 1.36	46.39 444.60 C 1.79
0+00 = Ni Line MADISON	(meet) 442.63	meet 443.22
T.B.M = = chx @ Alley @ 0-07	442.49	

STA.	(W/L) LT.	(E/L) RT.
1+90 = E.V.C	51.41 452.20 F 0.79	53.24 452.50 C 0.74
1+75	50.65 452.04 F 1.39	53.10 452.34 C 0.76
1+60	49.92 451.78 F 1.86	53.12 452.08 C 1.04
1+45	49.54 451.40 F 1.86	52.44 451.70 C 0.74
1+30	49.44 450.92 F 1.48	51.93 451.22 C 0.71
1+15	50.26 450.29 F 0.03	51.55 450.59 0.96

STA.	(W'4) LT.	(E'4) RT.	STA.	LT.	E	RT
3+40	53.01 452.95 C0.06	54.77 453.25 C1.52	4+70	53.79 453.40 C0.39		54.08 453.70 C0.38
3+15	52.21 452.83 F0.62	54.93 453.13 C1.80	4+50	53.79 453.49 C0.30		53.97 453.79 C0.18
2+90	52.15 452.70 F0.55	53.85 453.00 C0.85	4+30 = B.V.C	53.11 453.40 F0.29		54.09 453.70 C0.39
2+65	51.92 452.58 F0.66	53.21 452.88 C0.33	4+15	52.93 453.33 F0.40		54.12 453.63 C0.49
2+40	52.86 452.45 C0.41	54.06 452.75 C1.31	3+90	52.71 453.20 F0.49		56.07 453.50 C2.57
2+15	51.34 452.33 F0.99	52.91 452.63 C0.28	3+65	52.85 453.08 F0.23		53.58 453.38 C0.20







**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**  
**SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.**

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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