

G-385

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

MICROFILMED

APR 19 1965

386.00

PAGES	INDEX	DATE
1-8	WATER GRADES ALSO GRADES AERO COURT; RESEARCH PARK	4-26-57
9-12	SEWER GRADES RESEARCH PARK M.H. 10-8	4-26-57
13-16	" " " " M.H. 3-12	
17-34	" " " " M.H. 2-9	
35-39	GRADES ALLEY BLK. 318 REED & DALEY'S ADDN	6-18-57
40	STORM DRAIN BLK H, SILVER TERRACE	6-25-57
41-51	JUNIPER ST. SEWER; SUMAC TO FAIRMOUNT	7-16-57
52-55	MODESTO ST. SEWER, JUNIPER TO SUMAC.	7-17-57
56-63	SUMAC DRIVE SEWER; JUNIPER TO MODESTO	
64	SEWER LATERALS; COLUMBINE & LAUREL ST.	

Ref DWG 4189-D

4-26-57

①

G-13 10-27-56

1-15-57

±

H₂O
LINE

E.P.
Stamped
Bluff
Keiley
Wentworth

PAVING GRADES AERO COURT RESEARCH
PARK W.O. 24785 E.P.

NOTE: Stakes 3" bk. E.P.
or. Curb.

P.O.C.
Δ = 120° ④

F1 ⁶⁹
940
401.09

F2 ⁵⁵
9854
401.09

P.O.C.
Δ = 90° ③

F1 ³⁶
978
401.14

F2 ³⁹
9875
401.14

P.O.C.
Δ = 70° 08' 33" ②

F1 ⁰²
0005
401.07

F2 ⁰¹
99.06
401.07

P.R.C.
Δ = 50° 17' 06" ①

C14 ⁴⁰

40040
86.00
Sewer MH
5' R.P.R.T.

F1 ¹⁴
9987
401.01

F1 ⁵¹
9950
401.01

0° 00' = North Along Δ Azim Clockwise

L = 172.06'

∠ @ Ctr. EPR = 38' Δ = 259° 25' 48"

0+00 = ± Cul-De-Sac.

(Inst 3" H₂O B.O.)

400.54 400.54

^{.90}
400.40
397.30
H₂O

401.14 401.14

C3 ¹⁰

B.M.

399.74

0+00 Hub (G-13 Sta. 17)

GRADES AERO COURT

EP Lt

€

EP ②

P.O.C.
 $\Delta = 289^{\circ} 51' 27''$ ⑩

C1 ⁰⁷	CO ³⁸
155	0086
400.48	400.48

P.O.C.
 $\Delta = 270^{\circ}$ ⑨

CO ⁴⁹	CO ²³
1.03	0077
400.54	400.54

P.O.C.
 $\Delta = 240^{\circ}$ ⑧

CO ⁵⁹	FO ⁴⁰
1.29	00.30
400.70	400.70

P.O.C.
 $\Delta = 210^{\circ}$ ⑦

F1 ²⁵	F1 ⁰¹
960	9984
400.85	400.85

P.O.C.
 $\Delta = 180^{\circ}$ ⑥

FO ⁷⁰	F1 ⁸³
0030	99.17
401.00	401.00

P.O.C.
 $\Delta = 150^{\circ}$ ⑤

FO ⁷⁵	F2 ³⁷
0030	98.68
401.05	401.05

GRADES AERO COURT

	EP	Lt	E	Rt	EP	
4+50 v	C 1 ⁸⁴ 0.94 399.10	F 0 ¹² 8.98 399.10	399.46	H ₂ O LITE C 3 ⁰⁰ 98.90 395.90	F 0 ⁰⁹ 9.67 399.70	C 0 ⁹⁷ 0.67 399.70
4+00 ✓	C 1 ²⁰ 0.46 399.26	F 0 ⁰⁴ 9.22 399.26	399.62	C 3 ⁰⁰ 99.00 396.00	C 0 ²¹ 0.07 399.86	C 1 ²⁹ 1.15 399.86
3+50 v	C 1 ³⁶ 0.078 399.42	C 0 ²⁰ 9.62 399.42	399.78	C 2 ⁹² 99.12 396.20	C 0 ⁵⁸ 0.60 400.02	C 1 ⁴⁷ 1.49 400.02
3+01.80 = W. Lat Rt. (20')	C 1 ⁷⁸ 1.36 399.58	C 0 ³⁴ 9.92 399.58	C 1 ⁸⁷ 399.94	C 3 ²⁰ 99.50 396.30	C 5 ⁹² 402.42	C 1 ⁹⁷ 2.15 400.18
3+00 (Inst. 8"X8"X6" Tee)			2.17 400.30	H ₂ O RP 5' BK. C 0 ⁴²		
2+61.80 = N.W. Cor Lot H - - -	C 2 ⁰⁴ 1.78 399.74	C 0 ⁵² 0.26 399.74	400.10	C 3 ¹⁴ 99.64 396.50	C 0 ⁴² 0.60 400.18	C 2 ⁰¹ 2.35 400.34
2+50						
2+00	C 2 ⁴⁶ 2.36 399.90	C 0 ⁷⁵ 0.65 399.90	400.26	C 2 ⁸⁴ 99.54 396.70 H ₂ O	C 0 ²⁶ 0.76 400.50	C 1 ¹² 1.62 400.50

GRADES AERO COURT

EP
Rough

L

£

Rt ⑤

EP
Rough

	CO ⁰³	FO ²⁶		H ₂ O Line	FO ¹¹	CO ⁶³	
6+60	825 398.22	796 398.22		398.60	8.75 398.86	949 398.86	
6+40V	CO ⁵⁶	FO ⁰³		C2 ⁷⁴	CO ¹⁸	CI ²²	
	896 398.40	837 398.40		398.77	794 395.20 H ₂ O	920 399.02	024 399.02
6+20	CI ⁶⁰	CO ¹⁴		398.91	CO ⁴⁵	CI ⁸⁸	
	015 398.55	869 398.55			9.60 399.15	103 399.15	
6+00VV	C2 ⁰⁰	CO ⁵⁶		399.00	C2 ⁹²	CO ³⁶	C2 ⁰⁵
	063 398.63	919 398.63			832 395.40	459 399.23	128 399.23
5+50	CI ²⁸	CO ⁵⁹		399.15	C3 ⁰⁸	CO ³⁶	CI ⁸⁹
	077 398.79	938 398.79			8.68 395.60	975 399.39	128 399.39
5+00	CI ³⁵	CO ³⁰		399.31	C3 ⁰⁶	CO ⁰⁷	CI ²⁵
	030 398.95	925 398.95			8.76 395.70 H ₂ O	962 399.55	080 399.55

GRADES AERO COURT

LT Curb EP Gut E Gut EP Curb Curb RT ⑦
 Rough Rough

E.C. End Curb
 $\Delta = 38^{\circ} 07' 35''$ (Sta. 7+75.83)

CO²⁴ FO¹² C1⁴⁴
 7.80 7.80 9.36
 397.08 397.56 397.92 397.92 397.92
 Gut

10.65'

C1⁰¹ C1⁰¹
 8.91 8.91
 397.90 397.90

P.O.C.
 $\Delta = 19^{\circ} 03' 47''$

10.64

CO⁹⁷ CO⁶⁷ CO⁶⁵
 8.83 8.83 8.81
 397.86 398.16 398.16

P.
 E.C. $\Delta = 90^{\circ}$

2-d=
 $L = 21.29'$ $R = 20'$
 $\Delta = 38^{\circ} 07' 35''$ Cb. R = 32'

$\Delta = 90^{\circ}$
 $R = 5'$
 $L = 7.85'$
 $7+56.80 =$ P.C.C. Ch. Ref Rt.
 51.93

CO⁰⁷ FO⁴³ Grade
 7.57 7.57 8.00
 397.50 398.00 398.00

Curb E.P.

C1²⁴

C1⁹⁵

C1⁵³

P.O.C. P.L.
 $\Delta = 41^{\circ} 34' 24''$

8.13 8.84 8.13
 396.89 396.89 396.89 396.89 396.60

5.93'

C1⁹⁴

C1⁹³

$\Delta = 30^{\circ} 57' 30''$

8.90 8.89
 396.96 396.96

8.65

T.B.M.

399.22

Top 32' Rad Hub 7+56.80 Rt (E) 4)

GRADES AERO COURT LT RT ②
 EP. GUT GUT EP.
 Rough H₂O Rough

(Make Connection to Existing 10" Line)
 8+15.83 = End Line H₂O

7+75.83 = E Sta @ R. Aero Drive ✓

8+15.50 Meet Existing Pav't. ✓
 395.95
 EXIST

C3²⁰
 6.80
 393.60
 H₂O

GUT E.P.

398.06
 Existing
 on P.K.

	C0 ³⁰		C1 ²¹		C0 ⁵¹		C0 ⁵⁷	C0 ⁵¹
8+05.15 (Gut. Line)	6.15 395.85	396.31	7.06 95.85 E.P.		7.11 396.60	396.89	7.86 397.29	7.80 397.29

RR TIE
 on GUT

	C1 ⁸⁰		C1 ⁴¹				C0 ⁸⁸	C1 ⁴⁴
7+85.33	8.17 396.37	7.78 396.45	7.78 96.37 E.P.		396.84	397.22	8.48 397.60	9.09 397.60

Ref DWG 4415-D €

Stk. 3

NOTE: Stakes

Set 10' et. C 8 69

02 06

393.37

C 9 57

03.47

393.90

C 9 45

03.87

394.42

C 9 62

04.57

394.95

C 9 38

04.86

395.48

C 8 95

04.95

396.00

R.P. 20' et

2x2 Hub 0+73.62 SE Cor. Lot B, Research Park.

8+00 (G-13; 11-7-56)

SEWER GRADES RESEARCH PARK

1+25

1+00

0+75

0+73.62 = Hub & Cul-de-Sac.

0+50

~~2.10%~~

0+25

0+00 = End of Line Plug

T.B.M.

403.99

T.P.

403.94

B.M.

394.55

SEWER GRADES RESEARCH PARK

2+50

2+25

2+00

1+90 = E.M.H. No 10

1+75

TP.

1+50

5.68 98

2.10 98

399.44

C 7 18

95 83
388.65

C 6 32

6 37
390.05

C 5 97

7 42
391.45

C 5 77

7 78
392.01 RP/10 + 20'

C 6 42

8 7 4
392.32

C 7 52

0. 37
392.85

SEWER GRADES RESEARCH PARK

4+00

€
C 15 36
95.61
380.25

3+75

C 13 83
95.48
381.65

3+50

C 11 45
94.50
383.05

3+25

5.6096

C 10 00
94.45
384.45

3+00

C 7 62
93.47
385.85

2+75

C 8 22
95.47
387.25

SEWER GRADES RESEARCH PARK

TBM. RP. M.H. N° 8 Stub. ⁵⁸³N.W. 383.06

5+47 = ~~E~~ M.H. N° 8 = (22+80.29 Main Line)

C 8 04

80.45

372.41 RP. 10'+20' FH.

TBM. 24+45.03 P.O. Hub ^{orig} Notes 390.69

G-13, 1-16-57
Sht 13

390.69

C 6 17

9.42

373.25

5+25

5+00

C 4 58

79.23

374.65

TP.

383.59

C 10 87

86.92

376.05

4+75

5.60 ⁰⁷⁶

TP.

391.94

C 15 52

92.97

377.45

4+50

C 16 28

95.13

378.85

4+25

NOTE: Ref 10' Lt ϵ

SEWER GRADES RESEARCH PARK

0+70 = ϵ C.O. Wall

C 4 92
48 68
343.76

0+60

C 5 83
46 05
340.22

0+50

C 7 42
44 40
336.48

0+40

C 8 13
42 16
334.03

TP
0+35 = ϵ C.O. Wall

348.15

C 8 33
37 05
328.72

0+20

TP

339.20

0+00 = ϵ M. H. No 3

C 7 67
31 08
323.41

TBM RP 44.13 E14

331.98

TBM 30.68' RP W14

330.81

B.M.

330.60

(Orig Hub P1. 9+39.47 G-13, Sht 17)

SEWER GRADES RESEARCH PARK

C 9 05

1+60

84.81
375.76 RR 20'TP
(302.34) POT HUB

383.47

C 6 85

1+40 = E.M.H.N. 011

81.85
375.00 RR 20'
RR 10'

TP

374.74

C 7 52

1+20

73.09
365.57TP
1+15 = E.C.O. Wall

366.00

C 8 03

1+00

64.17
356.14

TP

356.875

C 7 49

0+90 = E.C.O. Wall

9.21
351.72C 6 38

0+80

53.97
347.59

SEWER GRADES RESEARCH PARK

3+00

C 15 42
96 48
381.06

2+75

C 14 95
95 07
380.12

TP

392.27

C 14 03
93 20
379.17

2+50

2+25

3.79 80

C 12 61
90 83
378.22

2+00

C 11 28
88 55
377.27

1+80

C 10 47
86 49
376.52

B.M.

SEWERGRADES RESEARCH PARK

81.55
4+80 = END PING

399.74 (P.1)

56.55
4+55

C 13 93
40099
387.06
R.P. 10' 514.
Lat.

4+71.55 = Sewer Lat N° 1 Lt.

31.55
4+30 = E.M.H. N° 12 E Cul-De-Sac
Aero Ct.

4+00

3+75

3.79 96

3+50

3+25

C 13 87 C ~~14 63~~
00.07 00.83
386.20 386.20

C 13 97 C ~~14 22~~
00.07 00.32
386.10 386.10

C 14 15 C ~~14 09~~
00.15 400.00
386.00 386.00

C 15 49 C ~~14 87~~
400.34 99.72
384.85 384.85

C 15 08
98.99
383.91

C 15 34
98.30
382.96

C 15 77
97.78
382.01

NOTE: Stakes 10' et ← 5-07-57

GRADES 8" SEWER RESEARCH PARK

1+25

C 7 09
03 00
295.91

1+00

C 6 94
02.07
295.13

0+75

C 5 59
30.94
294.35

0+50

C 5 34
98.90
293.56

3.13 970

0+25

C 4 95
97.73
292.78

A = 51° 25' 37" RT
0+00 = ← EXISTING M.H. N° 2

292.00

B.M.

300.75

Chis/⊙ Top Sly Rim M.H. N° 2

SEWER GRADES RESEARCH PARK

2+75

C 8 11
08 72
300.61

2+50

C 8 54
08 36
299.82

2+25

C 8 57
07 61
299.04

2+00

C 8 66
TR. 06.92
298.26

1+75

3.13%

C 7 47
04.95
297.48

1+50

C 7 19
03.89
296.70

SEWER GRADES RESEARCH PARK

5

4+25

2

C 6 63
12.07
305.44

4+00

2

3.34%

C 6 76
11.37
304.61

3+75

C 8 15
11.92
303.77

3+50 = E.M.H. No 1

C 9 85
12.79
302.94 R.P. 20' RT

3+25

C 8 58
10.75
302.17

3+00

3.13%

C 8 19
09.58
301.39

SEWER GRADES RESEARCH PARK

5+75

C 6 02
16 47
310.45

5+50

C 6 99
16 61
309.62

5+25

C 7 03
TP. 15 81
308.78

5+00

3.34 %

C 6 27
14 22
307.95

4+75

C 5 38
12 49
307.11

4+50

C 6 21
12 49
306.28

SEWER GRADES RESEARCH PARK

7+25

3.37%

6+75

6+50

3.34%

6+25

6+00

7+00 = M.H. No 2 $\Delta = 2^{\circ}12'43''$ RT

Δ

(2)

C 6 95
22.42
315.47

C 8 02
22.63
314.63

RP. 20' RT

C 7 00
20.79
313.79

C 7 97
20.23
312.96

C 6 29
18.41
312.12

C 5 35
16.64
311.29

SEWER GRADES RESEARCH PARK

8+75

C 6 87
27 40
320.53

8+50

C 7 35
27 03
319.68

8+25

C 7 14
25 98
318.84

8+00

5.37%

C 6 90
TP. 24.90
318.00

7+75

C 7 19
24 35
317.16

7+50

C 7 02
23 33
316.31

SEWER GRADES RESEARCH PARK

10+00

3.34%

9+80

9+60.28 = E.M.H. N° 3 Δ = 25° 44' 40" RT.

9+50

3.37%

9+25

9+00

€

(23)

C 5 84
30.59
324.75

C 5 96
30.04V
324.08

C 6 09
29.50
323.41

C 5 97
29.02
323.05

C 5 84
28.05
322.21

C 6 25
27.63
321.37

SEWER GRADES RESEARCH PARK

11+50

C 8 71
38.47
329.76

11+25

C 9 12
38.04 ✓
328.92

11+00

C 7 61
35.70 ✓
328.09

10+75

5.34 90

C 6 17
33.42
327.25

10+50

C 5 76
32.18 ✓
326.42

10+25

C 6 14 ✓
31.72
325.58

SEWER GRADES RESEARCH PARK

13+00

5.34 1/2

12+75

19.72

12+55.28 = \pm M.H. No 4

27.64

12+2769

27.64

12+00

5.34 1/2

11+75

C 11 05
45 80
334.75

C 10 35
44 27 ✓
333.92

C 9 21
42 47 ✓
333.26

C 8 13
40 48 ✓
332.35

C 7 58
39 01 ✓
331.43

C 7 71
38 30 ✓
330.59

SEWER GRADES RESEARCH PARK

14+50

$$\begin{array}{r} C 7 \underline{03} \\ 4679 \checkmark \\ 33976 \end{array}$$

14+25

$$\begin{array}{r} C 7 \underline{87} \\ 4680 \checkmark \\ 33893 \end{array}$$

14+00

$$\begin{array}{r} C 8 \underline{65} \\ 4675 \checkmark \\ 33810 \end{array}$$

13+75

5.34 7/10

$$\begin{array}{r} C 10 \underline{00} \\ 4726 \\ 33726 \end{array}$$

13+50

$$\begin{array}{r} C 10 \underline{76} \\ 4718 \checkmark \\ 33642 \end{array}$$

13+25

$$\begin{array}{r} C 11 \underline{56} \\ 4715 \checkmark \\ 33559 \end{array}$$

SEWER GRADES RESEARCH PARK

15+80

4.20%

15+60

17.72

15+42.28 = ϵ M.H. N^o5 $\epsilon = 47^{\circ}$ Lt

17.28

15+25

15+00

5.34%

14+75

$$\begin{array}{r} \epsilon 9 \underline{19} \\ 53.62 \\ 344.43 \end{array}$$

$$\begin{array}{r} \epsilon 9 \underline{21} \\ 53.30 \\ 343.59 \checkmark \end{array}$$

$$\begin{array}{r} \epsilon 10 \underline{19} \\ 53.04 \\ 342.85 \checkmark \end{array}$$

$$\begin{array}{r} \epsilon 9 \underline{35} \\ 51.62 \\ 342.27 \checkmark \end{array}$$

$$\begin{array}{r} \epsilon 7 \underline{37} \\ 4880 \checkmark \\ 341.43 \end{array}$$

$$\begin{array}{r} \epsilon 6 \underline{51} \\ 47.11 \checkmark \\ 340.60 \end{array}$$

SEWER GRADES RESEARCH PARK

17+25

C 9 68
6020 ✓
350.52

17+00

C 9 36
58 83 ✓
349.47

16+75

C 8 48
56.90 ✓
348.42

16+50

4.20 90

C 8 71
56 08 ✓
347.37

16+25

C 8 84
55 16 ✓
346.32

16+00

C 8 93
54 20 ✓
345.27 ✓

5 SEWER GRADES RESEARCH PARK

18+50

18+25

18+00

17+85

14.74

17+70.26 = \leftarrow M.H. No 6 \rightarrow

20.26

17+50

4.20 0/0

4.20 0/0

4

(29)

C 7 90
63.68
355.78 ✓

C 7 79
62.52 ✓
354.73 ✓

C 8 35
62.23 ✓
353.68 ✓

C 9 38
62.43 ✓
353.05 ✓

C 9 59
62.02 ✓
352.43 ✓

C 9 93
61.50 ✓
351.57 ✓

SEWER GRADES RESEARCH PARK

T.B.M. NWRPM.H. 7 376.95

19+98.90 = E.M.H. No 7 $\angle = 20^{\circ}09'14''$ Lt

T.B.M. SW.RP.M.H. 7 376.27

23.90

19+75

TP

379.37

19+50

19+25

4.20 40

19+00

18+75

~~C 8 67 C 10 97 C 9 86~~

~~70.70 73.00 ✓ 71.39~~

~~362.03 362.03 362.03~~

~~RP 15' Lt 10' Rt 10' Lt 10' Rt~~
 line @ 90° bk Tan.

~~C 7 82 C 8 10~~

~~68.85 69.13~~

~~361.03 361.03~~

~~C 7 30 C 7 49~~

~~67.29 67.27 ✓~~

~~359.98 359.98~~

~~C 7 60 C 7 57~~

~~66.53 66.50 ✓~~

~~358.93 358.93~~

~~C 8 20 C 9 19~~

~~66.08 66.07 ✓~~

~~357.88 357.88~~

~~C 8 33~~

~~65.16 ✓~~

~~356.83~~

SEWER GRADES RESEARCH PARK

5-03-57
 Re-set - 8-12-57

(31)

Stakes 10' RT

21+50

C 11 76	C 12 05
79.36 ✓	79.65
367.60	367.60
7' Lt.	

21+25

C 12 02	C 11 85
78.70 ✓	78.53 ✓
366.68	366.68
7' Lt.	

T.P.

378.70

21+00

C 11 84	C 11 24
77.60 ✓	77.70 ✓
365.76 ✓	365.76
7' Lt.	

20+75

3.69%

C 11 71	C 11 39 T.P.
76.55 ✓	76.23
364.84 ✓	364.84
7' Lt.	

20+50

C 11 03	C 11 21
74.94 ✓	75.12
363.91 ✓	363.91
7' Lt.	

20+25

C 12 73	C 9 93
75.73 ✓	72.93
363.00	363.00
10' Lt.	

26.10

SEWER GRADES RESEARCH PARK

NOTE: Stakes 10' Lt
- or Wly.
10' Rt 8-12-57

5-01-57 (32)
5-03-57
8-12-57 Re-Set

T.B.M. (See Pg. 12) 383.06
22+80.29 = M.H. No 8 & = 1°13'29" Lt

C 8 04
80.43
372.41 372.41

T.B.M. 382.67
15.29

set chisel Wly side
Top M.H. No 8

77
C 8 83

22+65

371.85 8068 ✓
371.85

22+50

C 10 12
81.42
371.30 371.30 ✓

22+25

3.69%

C 8 96
79.33
370.37 8055 ✓
370.37

22+00

C 11 14
80.59
369.45 C 10 91
80.36 ✓
369.45

21+75

C 12 01
80.54
368.53 C 11 67
80.20 ✓
368.53

SEWER GRADES RESEARCH PARK.

C 10 81

90 99

380.18

24+25

C 11 07

89 91

378.84

24+00

TP

390.32

C 11 38

88.88

377.50

23+75

C 9 61

85 76

376.15

23+50

5.37%

C 6 62

381.43

374.81

23+25

23+00

373.47

19.71

SEWER GRADES RESEARCH PARK

€

34

24+97.74 = End = € M.H. N° 9
(Make Connection Exist 8" Sewer)

25'

24+72.74 Begin Conc. Etc.

22.74

5.378

24+50

C 3 27

7 35

384.08

RP. 20' RT

C 6 46

9.20

382.74

C 10 18.

91.70

381.52

Stamper
Blunt
Kelley
Wentworth

GRADES ALLEY BLK 318 REED & DALEYS ADD'N.

0+60

W032155

0+35

0+10

0+00

0-08

0-08-12' Lt = Ch. 2' Ch. Ret Rad (Street)

0+00 = E.L. 28-44 St.

B.M.

80.14

RT 11-14 St 1 &

Ref L. Leaf H-23
11 April 1956

C055 DW93935-D

1.63
81.08

C053

1.33
80.80

C022

80.75
80.53
15 bk.

C009

80.39
80.30
G

C050

80.40
79.90
G
Alley

0+00 Hub: 44-27 Blt + Rd. on Rt.

RT (35)

6-18-57

C059

1.97
81.38

C093

2.14
81.21

C105

2.10
81.05

80.95

ALLEY BLK. 318

2+40

LT

FO³⁸
3.76
84.14

RT

FO¹⁰
3.80
83.90
1st bk.

2+20

CO⁰⁵

3.62
83.57
1st bk.

2+00

FO²⁹

2.34
82.63

1+50

CO⁰⁷

1.72
81.68

1+00

CO²²

1.57
81.35

0+80

6-18-57

(36)

C 2³⁸

6.78
84.44
0.05' inside
Alley Nail
in Wall

C 2⁴²

6.62
84.20
0.17' inside Alley
Nail in Bldg

C 2⁴⁰

6.27
83.87
1st inside Alley
Nail in P.P.

C 1³⁰

4.23
82.93

CO⁹⁷

2.95
81.98

CO⁶⁷

2.32
81.65

ALLEY BLK. 318

3+75

3+50

TP

84.00

3+20

3+00

2+80

2+60

CO¹⁸

4 00
83.82

0.24' inside
Nail in bldg

FO⁵⁹

3 42
84.01

0.7642%

F1²²

3 02
84.24

FO⁹²

3 43
84.35

FO⁹⁷

3 40
84.37

CO²⁶

4 56
84.3030

Chisel +

6-18-57

C1³⁹

5 51
84.12

0.24' inside Alley
Nail in frame bldg

CO⁸⁸

5 19
84.31

C2⁰⁰

6 54
84.54

0.22' bk. Nail
in Wall

C1⁹²

6 57
84.65

0.05' bk. Nail in
Wall

C2⁰³

6 70
84.67

0.006' bk. Nail in Wall

CO⁸²

5 52
84.70

0.25' inside
Chisel +

ALLEY BLK. 318

5+25

5+00

4+75

4+50

4+25

4+00

Lt

+

Rt

(38)

6-18-57

CO 66

333
82.67
chist ⊕

CO 75

3.61
82.86

FO 36

2.69 ✓
83.05

CO 46

371
83.25
1.25' bk

FO 15

329
83.44
P.K.

CO 05

368
83.63
1.25' bk, P.K.

CO 33

3.30
82.97

CO 78

394
83.16
chist +

CO 40

3.75
83.35
chist +

CO 31

386
83.55
chist ⊕

CO 31

4.05
83.74
2.25' bk, chist +

CO 29

422
83.93

0.7642026

ALLEY BLK. 318

TBM.

82.32, - 82.32 Rino Sewer M.H. Ely Rino.

6+07⁷⁸

E.C. Street

CO ⁷²	CO ⁰⁹
2.74	2.74
82.02	82.70
Gut	cb
Street	Street

6+07⁷⁸ - 12' RT = ctr 2' cb. Ret. P.K. P.P.

Alley

CO ⁷¹	CO ¹⁴
2.74	2.74
82.03	82.60
Gut	cb
Alley	Alley

5+99⁷⁸ = W.L. 29-74. St.

82.10

CO ²⁹	FO.11
2.69	2.69
82.40	82.80
Gut	cb

5+75

CO⁰⁶
2.35
82.29
0.75' bk.

CO⁶⁹
3.28
82.59
1.0' bk.

5+75

82 2492.0

CO¹⁷
2.65
82.48
0.75' bk.

C | 32
4.10
82.78

5+50

LT

6-18-57

RT

(39)

Ref DWG 6535-B
(Loose Leaf E-17 3-21-57)

6-25-57

(40)

GRADES STORM DRAIN THROUGH LOTS 8, 9, & 10

BLK. H. SILVER TERRACE W.O. 21610

1+08 = END.

1+00

+75

+50

+25

0+00 = ϕ CURTAIN WALL

B.M.

54.65

ϕ Hub Lauretta & Benicia

C 1 09

54.54

53.50

C 1 12

54.06

52.94

C 0 50

51.70

51.20

C 0 51

49.98

49.47

C 1 00

48.73

47.73

C 1 27

47.27

46.00

6.94 $\frac{57}{8}$

Ref DWG 3472-D 5/15/10 (11)
(Loose Leaf J-20, 21 8-8-55)
7-16-57
Lt

Stampel (11)
0155011
Kelle
Elmore
RT

SEWER GRADES JUNIPER ST FROM
SUMAC DRIVE TO FAIRMOUNT AVE

~~6 26~~
9.66
253.40

Moved to 0+75 Sumac St. (P95)
0+63 = S. Lat N° 22 Lt 30'

0+50

C 24 70
59 24 ✓
234.54

0+25

C 24 26
58 90 ✓
234.64

4 E14 to 314.100° 50'
0+18 = S. Lat N° 20-30' Rt

C 8 17
59 87
251.70

(See POT, Tie P94A)

4 N14 to E14 = 74° N 45'

conc. Mon. 25.98' Wly of E Sumac.

0+00 = E Juniper & Sumac = E M.H. N° 6.

234.74

NOTE! Stakes Set 6' Rt.

B.M.

252.84

Mon.
E Juniper & Wly Line Sumac Drive

JUNIPER ST. SEWER

1+50

1+35 (Moved)
~~1+31~~ = S. Lat No 23-30' Lt

1+25

by Parsons
 Moved
 0+80
 1+07 = S. Lat No 24-30' Rt

¹⁵
 18' from Rt
 $\frac{27}{86}$

1+00

0+75

Lt

Rt

Rt

92

C 26 64
 60 78 ✓
 234.14

C 5 46
 62.16
 256.70

C 25 94
 60 18 ✓
 234.24

C 6 52 ~~C 6 52~~
 58 52 ✓ ~~58 52~~
 252.00 ~~252.00~~

C 25 41 ✓
 59 75
 234.34

C 24 98
 59.49 ✓
 234.44

JUNIPER ST. SEWER

2+53.50 = E.M.H. N°5

2+46 = S. Lat N°26 - 30' Lt

2+25

2+00

1+75

1+61 = S. Lat N°25 - 30' Lt

0.4
0.10

Lt

E

Rt

(B)

C 28 13

61 86 TD
233.73 ✓
6184

C 6 80

6460 ✓
257.80

C 27 62

61 46
233.84 ✓

C 27 36

61 30 ✓
233.94

C 27 13

61 17
234.04

C 6 15

6345
257.30 ✓

JUNIPER ST. SEWER

3+50 ± Chisl + Conc. & Brick Wall 30, 20' Lt. 45 = Stub (long)

TBM. Top Chisl + 266.24

C 29 43
62 77 ✓
233.34 ✓

3+25

C 29 83
63 27 ✓
233.44 ✓

3+00

C 29 38
62 92 ✓
233.54 ✓

2+86 = S. Lat N^o 28 - 30' Lt.

C 660
64.70 ✓
258.10 ✓

2+75 TP.

261.86

C 28 72
62 36 ✓
233.64 ✓

2+72 = S. Lat N^o 27 - 30' Rt

C 12 ²⁶
61.06 ✓
248.80 ✓

JUNIPER ST. SEWER

4+25 TP

4+00

3+91 = S. Lat N^o 31 - 30' Lt

3+75

3+69 = S. Lat N^o 30 - 30' Lt.

3+59 = S. Lat N^o 29 - 30' Rt

Lt.

E

Rt

(25)

C 24 20
57 24 TP ✓
233.04

C 25 93
59 07 ✓
233.14

C 744
6274 ✓
255.30

C 27 70
60 94 ✓
233.24

C 956
6596 ✓
256.40

C 594
6184 ✓
255.90

JUNIPER ST. SEWER

5+63.50 Begin CONC. ETC.

~~135~~

5+50

0.4 0/10

5+25

def $1^{\circ}08'$ Lt. Ahead (see Nor. Ties P 9, 48)
 5+13.28 @ 90° bk. Tan. = 23' Rt.; 37.47' Rt. = Hubs.

215 R.P. 20' S 1/4 $\&$ Modesto Line RR 45# on $\&$ Prod.
 $\&$ W 1/4 To N 1/4. $77^{\circ}32'15''$ - from $\&$ Juniper

5+03.49 = $\&$ M. H. N^o 4 $\&$ Modesto St.
 Sewer $\&$ def Lt. = $1^{\circ}07'00''$

27.5

4+76

26

4+50

0.4 0/10

Lt.

$\&$

Rt

(46)

C 21 12

53 66
 232.54 ✓

C 20 86

53 50
 232.64 ✓

C 20 59

53 32 ✓
 232.73 ✓

C 21 45

54 29 ✓
 232.84 ✓

C 22 79

53 73 ✓
 232.94 ✓

JUNIPER ST. SEWER

Lt.

E

Rt

(47)

7+00

C 24 31
56 25 ✓
231. 94 ✓

6+75

C 25 17
57 21 ✓
232. 04 ✓

6+50

C 25 75
57 89 ✓
232. 14 ✓

6+25

C 24 53
56 77 ✓
232. 24 ✓

6+00

C 23 18
55 52 ✓
232. 34 ✓

5+75

C 22 16
54 60 ✓
232. 44 ✓

JUNIPER ST. SEWER

8+25

22.30

def'd Rt = 6°06'47"
8+02.70 = E.M.H. N°3

22.70

7+80

16.50 (Set Hubs) Elev. 60' RP 248.99
7+63.35 R.P. 30' + 60' RT E Elev. 30' RP = 248.56
7+63.50 End CONC. ETC.

13.50

7+50

TP. 251.80

7+25

7+03.1 ± P.O.T. RP 30' & 50' ± RT.

35.73%

30.4%

Lt.

±

Rt

(48)

C 5 39

28 97
223.58

C 3 57

35 10
231.53

15' R.P.
LINE

6' 47"

233.18

15' R.P.

LINE

C 10 00

41 62
231.62

C 14 66

46 35 ✓
231.69

C 17 63

49 37 ✓
231.74

C 21 91

53 75 ✓
231.84

JUNIPER ST. SEWER

9+33

17.80

9+15.20 = € C.O. Wall

15.20

9+00

22.30

8+77.70 = € C.O. Wall

17.70'

8+60

19.80

8+40.20 = € C.O. Wall (Set Strs 6' Lt)

15.20

55.75

Lt.

€

Rt.

(42)

C 7 81
92 81
185.00

C 9 08
200 43
191.35

C 8 88
205 66
196.78

C 9 28
14 03
204.75

C 8 35
19 42
211.07

C 6 62
24 77
218.15

JUNIPER ST. SEWER

14.4'
10+42.47 = ϵ Conc. Pier

17.7'
10+24.77 = ϵ Conc. Pier

17.9'
10+06.87 = ϵ Conc. Pier

18.4'
9+88.47 = ϵ Conc. Pier

16.2'
9+72.70 = ϵ Conc. Pier

19.57
def $\epsilon = 4^{\circ} 35' \frac{1}{2}$ Lt.
9+52.70 = ϵ M.H.N^o 2 (stakes 6' Lt)
(Beq. Cast. Iron Pipe)

19.70

0.71890

35.7390

C 6 41
83.71
177.30

C 6 29
83.72
177.43

6 17
83.73
177.56

C 6 00
83.69
177.69

C 4 00
181.81
177.81

C 7 40 ✓
85.35
184.97
15' Lt. 177.95
6' Lt.

JUNIPER ST. SEWER

T.B.M.

186.81

PPN^o 2298 W. Side Fairmount

LT

+

RT

(5)

11+11.47 = End = \pm M.H. N^o 1 (Make Connection)

176.81

11.47

11+00

176.89

10+75

177.07

18.13

10+56.87 = \pm Conc. Pier

0.718 / 0%

C 6 56
83 76
177.20

Ref DWG 3472-3 D &

See Sht. 3, laterals

RT

7-16-57

(52)

SEWER GRADES MODESTO ST. FROM

JUNIPER TO SUMAC. W.O. 32138

1+25

C 16 33
59 63
243.30

22³

C 15 57
38 78
243.21 ✓

C 7 98
59 38
251.40 ✓

1+02⁷ = S. Lat N° 47 - 25' RT

TR. 0+94 - Lt. Nail Mail Box Post

259-68-72 - T.A.S.

26⁷

C 14 44
57 54 ✓
243.10

0+76

26'

C 13 25
56 25 ✓
243.00

0+50

0.4 0.0

C 12 16
55.06
242.90 ✓

0+25

C 10 52
353.32
242.80 = Drop Inlet

∠ = 77° 33' W. To N.

0+00 = E. M.H. N° 4 (See Pg. 46)

Stakes 6' RT

B.M.

Laterals 5' bk. RT.

MODESTO ST. SEWER

LT

¢

RT

53

2+35 = 5. Lat N^o 43 - 25' LT

C 8 52
6232 ✓
253.80

C 16 08
59.82 TP,
243.74 ✓

16⁵

2+18⁵ = 5. Lat N^o 44 - 25' RT

C 16 47
60.14 ✓
243.67

C 11 95
58.65
246.70

23⁵

1+95 = 5. Lat N^o 45 - 25' LT

C 8 96
6246 ✓
253.50

C 16 77
60.35 ✓
243.58

20
1+81 = 5. Lat N^o 46 - 25' RT

C 4 88
59.68 ✓
254.80 ✓

1+75

C 16 98
60.48 ✓
243.50

1+50

C 16 79
60.19 ✓
243.40

MODESTO ST. SEWER

LT

¢

RT

54

3+38⁵ = 5. Lot N^o 38 - 25' RT

C 14 ⁷⁹
58 94
244.15 ✓

C 7 ⁹⁰
55 10
247.20

C 8 ⁸⁰

63 00
254.20

3+37⁵ = 5. Lot N^o 39 - 25' LT

C 14 ⁹³
59 00
244.07

3+18⁵

20'

C 14 ⁹⁸
58.98 ✓
244.00

C 8 ⁵³
53 53
247.00

2+98⁵ = 5. Lot N^o 40 - 25' RT

22⁵

C 8 ⁰⁴ C 15 ³²
61 92 ✓ 59 22
253.90 243.90

253.90

2+76 = 5. Lot N^o 41 - 25' LT.

17⁵

C 15 ⁵⁷
59 40
243.83

C 9 ⁸⁸
56 78 ✓
246.90

2+58⁵ = 5. Lot N^o 42 - 25' RT.

23⁵

MODESTO ST. SEWER

Lt. £ Rt. (55)

4+58⁵ = S. Lat No 35 - 25' Rt

C 14 21
58 84 ✓
244.63 ✓

C 6 96
54 56
247.60

20'

4+38⁵ -

C 14 36
58 91 ✓
244.55 ✓

opp. House No 2420 Modesto St.
TBM. 4+40 ± Set chis. / # NW cor Walk 263.14
20'

4+18⁵ = S. Lat No 36 - 25' Rt

C 14 58
59.05
244.47

C 7 6.5
55 15 ✓
247.50

20'

3+98⁵

C 14 59
58 98 ✓
244.39 ✓

20'

3+78⁵ = S. Lat. No 37 - 25' Rt

C 14 62
58.93
244.31 ✓

C 8 00
55 30
247.30

28⁵

3+50 = £ M.H. No 9

C 14 72
58 92
244.20

11⁵

6+02.89 @ Modesto

MODESTO ST. SEWER

5+91.82 = (5+83)⁵³ Sta = S. Lat N° 32 - 25' RT)

5+70

21.12

Def 4 = 36° 42' 30" RT = 6" Lateral to R
5+50 = End 8" Line Plug.

5+38⁵ = S. Lat N° 33 - 25' RT.

TBM. 5+19 - 18' RA PK. Pole N° 577302 258.61 - (258.55)

20

5+18⁵

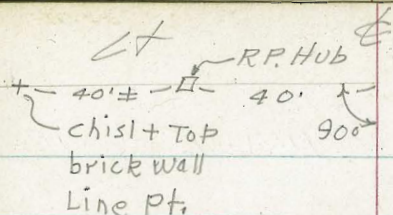
20'

4+98⁵ = S. Lat N° 34 - 25' RT

20'

4+78⁵

20



RT

(56)

C	10	65
	56	85
	246.2	

C	11	66
	57	39
	245.73 ✓	

C	14	24
	59	24
	245.00	

C	14	16
	59	11
	244.95 ✓	

C	9	05
	56	05
	247.00 ✓	

C	14	17
	59	04
	244.87 ✓	

C	14	23
	59	22
	244.79	

C	7	00
	54	80
	247.80 ✓	

C	14	17
	58	88
	244.71	

SUMAG DRIVE SEWER

2+09 = S. Lat. No 14-25' Lt

25'

1+84 = S. Lat. No 15-25' Lt

28

1+56

27

1+29 = S. Lat No 16-25' Lt

20'

1+09

20

0+89 = S. Lat No 17-25' Lt

14

Lt.

+

Rt

(58)

C 16 ⁵⁵
50.05
238.50 ✓

C 17 ¹²
52.70
235.58 ✓

C 10 ⁹⁰
49.10
238.20 ✓

C 17 ¹²
52.60
235.48 ✓

C 17 ⁴⁶
52.82 ✓
235.36 ✓

C 12 ⁴⁰
50.50 ✓
238.10 ✓

C 17 ⁹⁸
53.24 ✓
235.26 ✓

C 18 ⁴⁷
53.65 ✓
235.18 ✓

C 12 ⁰⁵
50.25 ✓
238.20 ✓

C 19 ⁰³
54.13 ✓
235.10 ✓

SUMAC DRIVE SEWER

2+86^s = S. Lat No 11 - 25' Lt

18^s

2+68

18

2+50

11.80

2+48 = S. Lat No 12 - 25' Lt.

0.4 90

2+38 = 4 = 60° 35' Rt Sewer M.H. No 7

17^s

2+21 = S. Lat. No 13 - 25' Rt

12'

LX € RT 53

C 10 ⁹⁰
49 80
238.90

C 18 ¹²
54 00 ✓
235.88

238.90

C 17 ⁶⁹
53 50 ✓
235.81

C 17 ³⁷
53 11 ✓
235.74

C 11 ⁸⁵
50.55 ✓
238.70

C 17 ²⁵
52 44 ✓
235.69

6' Rt @ 90° bk Tail 15' Rt RP.

C 17 ¹²
52 74 ✓
235.62

C 9 ³⁰
55 50 ✓
246.20

SUMAC. DRIVE SEWER

~~4+92~~
4+06⁵ = S. Lat N^o 6-25' Lt.

4+00 = S. Lat N^o 7-25' Rt

3+75

22

3+53 = S. Lat N^o 8-25' Rt.

26⁵

3+26⁵ = S. Lat N^o 9-25' Lt.

19⁵

3+07 = S. Lat N^o 10-25' Rt

20⁵

0.4
0.6

Lt. Rt 60

C 13 ⁶⁰
52.80
239.20

C 20 ⁹⁰
57.24 ✓
236.34 ✓

C 10 ⁸⁵
62.55 ✓
251.70 ✓

C 20 ²⁸
56.52 ✓
236.24 ✓

~~C 10 ^{51.90}
250.20~~

C 19 ⁷⁵
55.90
236.15

C 10 ⁷⁰
60.90 ✓
250.20 ✓

C 12 ⁶⁰
51.30
238.70

C 19 ⁰⁸
55.12
236.04 ✓

C 18 ⁶⁶
54.62 ✓
235.96 ✓

C 11 ⁵⁰
59.20 ✓
247.70 ✓

SUMAC DRIVE SEWER

5+26⁵ = S. Lat N^o 4-25' Lt

5+00

4+75

4+65 = S. Lat N^o 5-25' Rt

4+50

4+25

0.490

Lt E Rt 61

C 15 ⁷⁸
55.28
239.50

C 23 ⁹⁹
60.78
236.84 ✓

C 23 ⁴⁴
60.18
236.74 ✓

C 22 ⁷⁶
59.40 TP
236.64 ✓

C 10 ⁶⁰
64.40
253.80 ✓

C 22 ²⁹
58.83
236.54 ✓

C 21 ⁵⁶
58.00
236.44 ✓

SUMAC DRIVE SEWER

6+36⁵ = 5. Lat. N^o 2-25' Lt.

16⁵

6+20

23⁵

5+96⁵ = 5. Lat N^o 3-25' Lt.

21⁵

5+75

8⁵

5+66⁵ = ~~4~~ M. H. N^o 8 - Set 8" Lat 25' Lt. + Plug. & Tuberosa Lame ✓

16⁵

5+50

23⁵

Lt.

¢

Rt

(22)

C16⁴²
5832
241.90

C24²²
63.38
239.16 ✓

C24³⁶
63.01
238.65 ✓

C16⁴⁶
57.56 ✓
241.10

C24⁶⁷
62.60 ✓
237.93 ✓

C24⁸²
62.08
237.26

C19⁷⁷ C24⁹⁰
5687 61.90
237.10 ✓ 237.00 ✓
25'

C24⁴⁹
61.43
236.94 ✓

5.09 90

0.4 90

SUMAC DRIVE SEWER

Lt. & Rt. (63)

TBM.

260.17 PK. P.P. N^o P 2957 NE Cor Modesto & Sumac.

T.B.M.

262.34 —

Set Chis/□ in Conc Drive S/W side 2' Ely of Garage fce. on S/W side @ House N^o 2448 Sumac Dr.

TP

def 4 = 25° 04' 30" Lt. 9.84 = S. Lat N^o = 1

C 18 ³⁵
6025 ✓
241.90

9.84'

C 22 ²¹
6221
240.00

6 + 63 ⁵⁰ = End 8" Line Plug

13.5

C 24 ⁰⁰
6358 ✓
239.58

6 + 50

13.5

3.09%

Sht #3, Laterals

Lt.

¢

Rt

(64)

SEWER LATERALS VARIOUS STREETS

C 2 37

82.77

280.40

2+41.33 = End Lateral N^o 48 R & ¢ Columbine

C 4 04

84.54

280.50

2+00⁵ - 23' Lt. = S. Lat N^o 49 (Sht. B)

1+85 52 = ¢ B.C. Rt.

RR - 40' Lt. + 68' Lt

C 3 21

83.81

280.60

1+37 - 25' Lt. = S. Lat. N^o 50 (see Sht N^o 8)

0+00 = ¢ Columbine & W.L. Fairmount

B.M.

288.17

Fairmount & Columbine

N.W. 7' x 9⁵ Lt.

C 5 70

64.00

258.30

def $\alpha = 20^{\circ} 20' 24''$

2+13^v P.O.C. = S. Lat. N^o 51 - 25' Lt. (Sht #7)

C = 208.55'

¢ R = 300 d = 5.729578/ft.

0+00 = W.L. Fairmount & Laurel = B.C. Rt.

T.B.M.

268.14

Set Chis/4 on Conc Walk. opp House #4320

N.W. Cor

Laurel St.

B.M.

280.17

NW BP Sumac & Fairmount
Maple ✓

18" STORM DRAIN SUMAC. DRIVE

0+98.57 = END PIPE + 1.88 = fce Wing Type Hdwall

8.84'

0+89.73 P.O.C. Mid. Pt.

8.83'

0+80.90 = B.C. Lt. $T=9.24'$
 $\Delta=45^\circ R=22.5' L=17.67'$

NOTE: Stakes 20' Rt

20.90

0+60

22.92

20

0+40

19.10

0+20.90 = Inside fce Type K Inlet N^o 5

0+00/18" Drain = fce Sumac. Dr. Sta. 1+62.45 (See G-389)
 @ 90° To & Thence Wly.

B.M.

252.84

Mon & Juniper & Wly Line Sumac

LT

20
 25.20

RT

(65)

1+00.45 fce Wall.

30.20

225.00

25.80

31.00

225.20

27.94

35.76

227.22

29.24

38.49

229.25

29.46

43.50

234.04

29.69

48.31

238.62

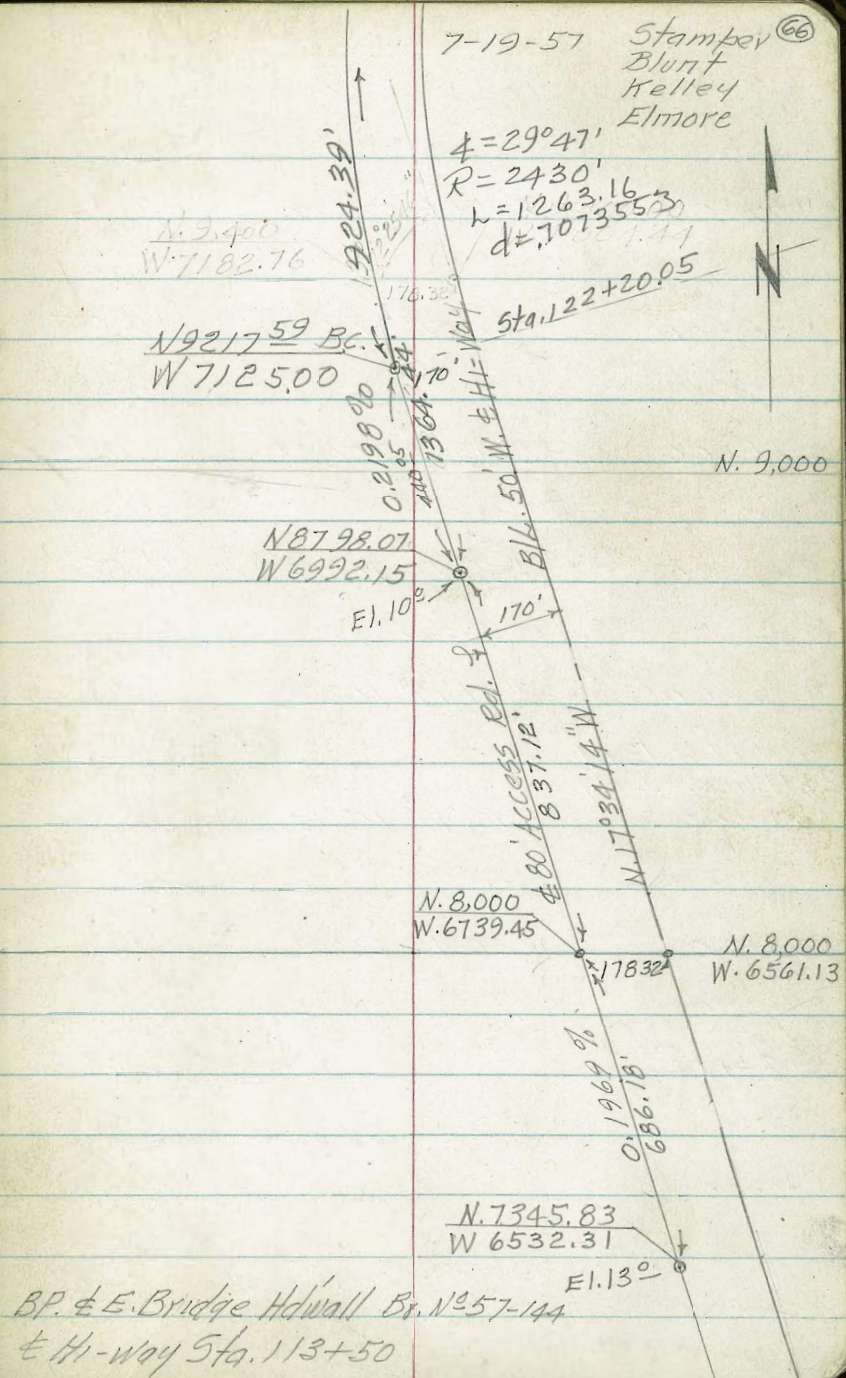
28.17

51.17

243.00

GRADES ACCESS ROAD MISSION BAY

211.81'	W064501	10.00
N87+98.02		
207.762		
N86+00		10.41
N84+00		10.82
N82+00		11.23
N80+00		11.65
N78+00		12.06
N76+00		12.47
209.786		
N74+00		12.88
56.822		
N7345.83		13.00
J.B.M.		13.79



Sta	Def 4	Chord	Grade
N99+00	8°11'06"	100.08	Grade 12.49 12.49
N98+00	7°00'07"	100.34	C 20 12.27 12.27
N97+00	5°49'08"	100.77	C 30 5.05 12.05
N96+00	4°37'50"	101.38	C 20 4.83 11.83
N95+00	3°26'07"	102.20	C 30 13.61 11.61
N94+00	2°13'49"	103.19	C 40 14.38 11.38
N93+00	1°00'49"	85.97	C 40 15.16 11.16
N92+00			C 40 14.97 10.97
N90+00			C 50 15.46 10.46

N95+25 ±
TBM, P.K. Gd. Rail Elev. 13.90

TBM, Elev. 13.01
24.44 Gd. R.P. Ely

ER = 2430'
BC, R.F. Δ = 29°47'
N92+17.59

18.45'

209.786'
TBM, P.K. Nail, 11.81
20 R.P. @ 90° to PL.

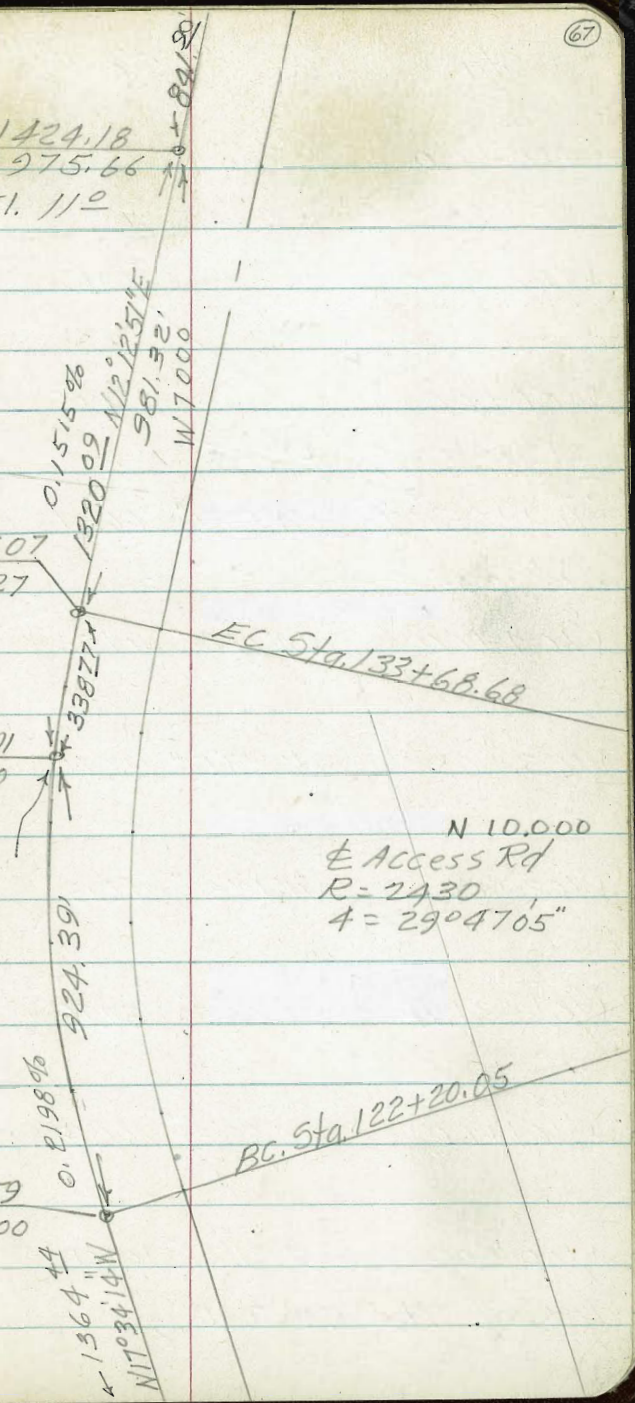
211.81

N. 11424.18
W. 6975.66
El. 11.0

N. 10465.07
W. 7183.27

N. 10134.91
W. 7231.30
El. 13.0

N. 9217.59
W. 7125.00



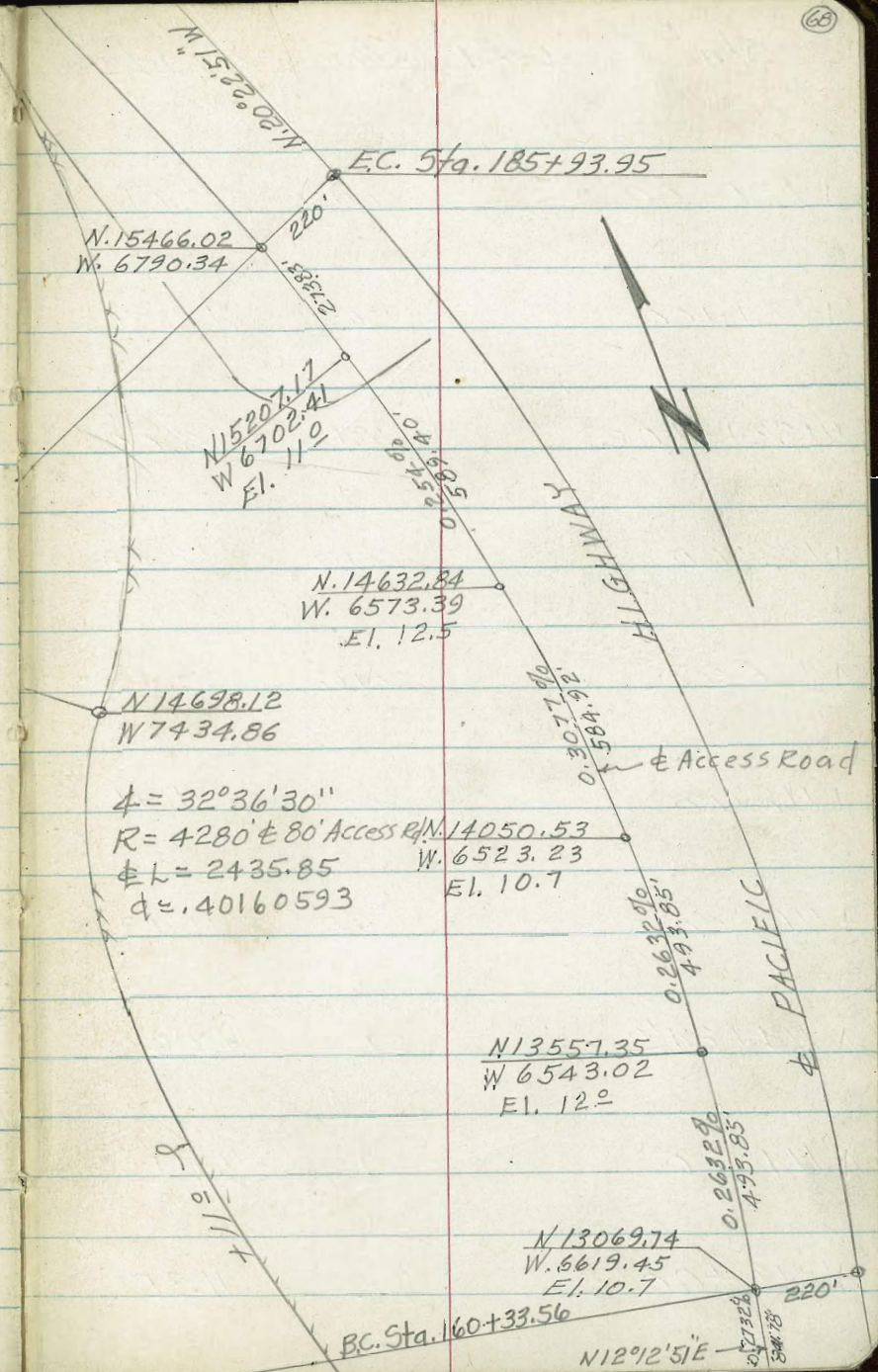
EC Sta. 133+68.68

N 10,000
Δ Access Rd
R = 2430
Δ = 29°47'05"

BC Sta. 122+20.05

0.1515%
1320.09
N 12°12'57"E
581.32'
W 7000
33827.41
924.391
0.8198%
1364.44
W 1034.14

Sta	Def. Δ	Chord	Grade
N/110+00		209.63	11.66
N/108+00		204.63	11.97
N/106+00		138.05	12.28
N/12°12'51"E E.C.			
N/104+65.07	14°53'30"	66.37	12.49
N/104+00	14°06'37"	101.38	12.59
N/103+00	12°54'54"	100.74	12.74
N/102+00	11°43'38"	163.19	12.89
N/101+34.91	10°58'56"	137.16	13.00
N/101+00	10°32'39"	100.08	12.93
N/100+00	9°21'51"	100.01	12.71
TBM, R.P. P.I. P.A. W. 7040			14.24



Sta	Defd	Chord	Grade
N126+00		204.63	12.01
N124+00	0.2732%	156.52	12.57
N122+47.02		48.11	13.00
N122+00		204.63	12.88
N120+00		204.63	12.40
N118+00		204.63	11.91
N116+00	0.2375%	179.89	11.43
N114+24'8		24.74	11.00
N114+00		204.63	11.04
N112+00.16	0.1515%	204.63	11.35

Sta.	Def. 4	Chord	Elev.
N136+00	3°35'31"	42.83	11.89
N135+57.35	3°18'20"	57.68	12.00
N135+00	2°55'09"	100.76	11.85
N134+00	2°14'41"	101.05	11.58
N133+00	1°34'06"	101.42	11.32
N132+00	0°53'22"	101.96	11.05
N131+00	0°12'25"	30.92	10.78
R=4280'			
Δ=32°36'30"			
BC Lt.			
N130+69.74		71.35	10.70
N130+00		204.63	10.89
N128+00		204.63	11.45

0.26 ± 2%

0.2732%

Sta.	Def. A	Chord	Grade
N145+00	9°37'42"	100.63	12.09
N144+00	8°57'17"	100.39	11.78
N143+00	8°16'58"	100.22	11.47
N142+00	7°36'43"	100.10	11.16
N141+00	6°56'31"	49.47	10.85
N140+50.53	6°36'40"	50.55	10.70
N.140+00	6°16'21"	100.01	10.83
N139+00	5°36'11"	100.01	11.10
N138+00	4°56'01"	100.14	11.36
N137+00	4°15'48"	100.30	11.62

0.3077%

0.2632%

Sta	Def \angle	Chord	Grade
EC. N154+66.02	16°18'15"	70.22	
N154+00	15°49'44"	105.57	
N153+00	15°07'20"	97.27	
N152+07.17	14°28'16"	111.47	11.00
N151+00	13°43'30"	103.33	11.28
N150+00	13°02'00"	102.71	11.54
N149+00	12°20'45"	102.17	11.81
N148+00	11°39'43"	101.67	12.06
N147+00	10°58'53"	68.06	12.32
N146+32.84	10°31'33"	33.24	12.50
N146+00	10°18'13"	100.88	12.40

0.25426

0.307796

Ref DWG 3478X-D SHH.9

Stamper (73)
Blunt
Stucky
Wentworth

8-7-57

NOTE: Stakes 6' rt.

18" STORM DRAIN NLY FROM NAPIER
ST. ALONG ELY SIDE OF MORENA BLVD
W.O. 22054

C 4 91
12.01
7.10

1+00

C 5 10
12.05
6.95

0+75

C 5 23
12.03
6.80

0+50

0.60270%

C 5 38
12.03
6.65

0+25

0+00 = NELY Inlet Type K. Morena & Napier St.

6.50
1. F
Meet

B.M.

12.06

Chis/D Ely End Inlet NE. Morena & Napier
Level Book Morena. (Osborne)

18" DRAIN MORENA BLVD

RP 10' N19' E Box
2+49.72 5.75 Rt = End 4-18" Stub. RP. 5' 410' BK
(End Pipe)

NOTE: Outside Fee Box Set @ P.

FO 95 C340
11.48 11.48
12.43 8.08
TOP End 4'
BOX Stub

2+48.85 = Sly Inside fee 21" X 35 Type D-C Basin

C348
11.48
8.00

2+25

C406
11.92
7.86

2+00

7.86
C398
11.68
7.70

1+75

7.70
C449
12.04
7.55

1+50

C460
12.00
7.40

1+25

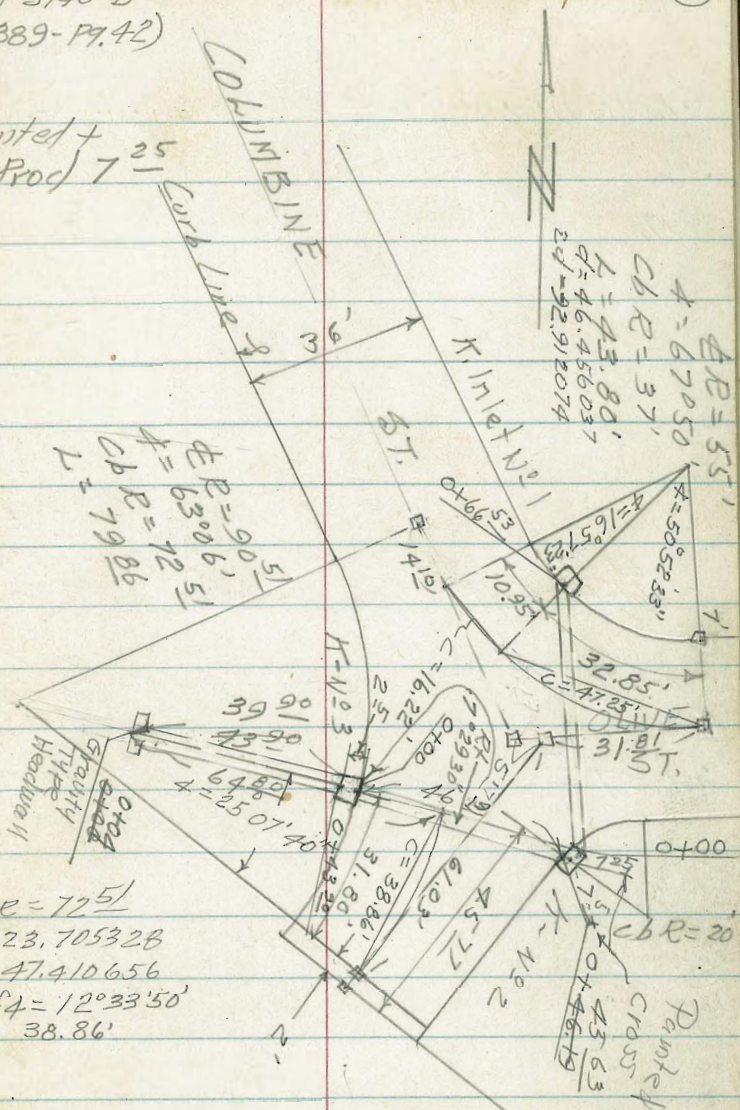
C465
11.90
7.25

Ref 3740-D
(G-389-Pg.42)

GRADES STORM DRAINS OLIVE & COLUMBINE STS.

0+45 ⁶³	87.90
0+46 ¹⁴ = End Pipe Inside Box Wly	276.00
<hr/>	
0+23 ¹⁰	1028
	85.53
	275.25
<hr/>	
0+00 = Inside Box Ely.	953
	89.03
	274.50
<hr/>	
2.5	933
	83.83
	274.50
<hr/>	
0+43 ²⁰ = End Pipe Inside Box Wly.	483
	79.6
	273.13
<hr/>	
219	608
	8.08
	272.00
<hr/>	
0+22	
18	
04	
0+00 = Wly fce Headwall	
<hr/>	
B.M.	288.17

Painted +
R.P. & Prod 7²⁵



cbR = 72.51
d = 23.705328
2d = 47.410656
def Δ = 12° 33' 50"
C = 38.86'

Type K Inlets 2⁵ x 4⁰ Inside
With 8" Walls

NW 7' x 9⁵ L.A.T. Columbine & Fairmount (Pg. 64)

STORM DRAIN OLIVE & COLUMBINE CONTD.

B.M.

5626
0+66.53 = End Pipe Inside fce. Box
5/4 K-N^o1

C751
8551
278.00

1876

C884
8617
277.33

0+375

1875

C937
8604
276.67

0+1875

18.75

C1164
8769
276.00 =

0+00 = Inside fce K-N^o2 N14.

RP. 75 5/4 & Proj.

GRADE STAKES ALONG ELY SIDE OF
MIDWAY DRIVE FOR LEVEE LINE

(9) NOTE: Stakes Set @ 100' Intervals	14.28
(8)	14.14
(7)	14.00
(6)	13.90
(5)	13.80
(4) (± Sunset Cliffs Blvd. Prod. Ely.)	13.72
(3)	13.64
(2)	13.56
(1) Thence S ¹ / ₄ Opp. Pipeline X-ing	13.48
A = N ¹ / ₄ . (see Pg. 78)	
B.M.	12.61

9-13-57 Stampet 77
Blunt
Elmore
Wentworth
@ Levee & Rd.
Embankment

(19)	16.0
(18)	15.8
(17)	15.6
(16)	15.4
(15)	15.2
(14)	15.00
(13)	14.85
(12)	14.70 (Pcd)
(11)	14.56
(10)	14.42

Ref. Divg. Sheet 3075
Corps of Eng'rs US Army
Jan. 1957
Mission Bay
Disposal Area "X"

GRADES ELY SIDE MIDWAY CONTD.

NOTE: Stakes Set @ 100' Intervals

J	12.69		
I	12.72		
H	12.80	R	12.00
G	12.90	Q	12.08
F	13.00	P	12.16
E	13.08	O	12.24
D	13.16	N	12.32
C	13.24	M	12.40
		Staked to L only	
B	13.32	L	12.48
A	13.40	K	12.56

GRAD

NOTE:

J

I

H

G

F

E

D

C

B

A

(D)

359-59-60

1-13-30

358-46-30

180

278-

965
 336
 21

 336
 672

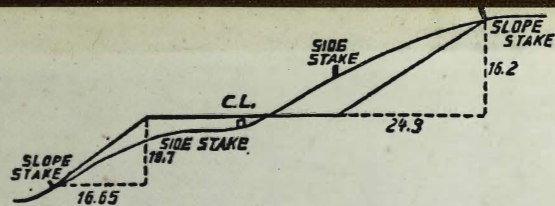
 7056

336
 2

 672
 3336

 108

12.11



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
 SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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