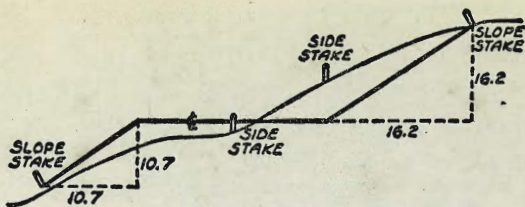


G-399



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side of roadway
cut for any width roadway, slope 1% to 10%
If ground is nearly horizontal cut or fill at side
of roadway by the amount of the slope stake

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of
any angle degree, divide by degree of curve and
add correction found in column of correction.
Degree of curve with a given length may be found
by dividing tangent (or external) opposite by
tangent (or external).
The distance from a point on the tangent to
the curve may be found by dividing the tangent
length divided by twice the radius.

- 0
- 1
- 2
- 3
- 4
- 5
- 6
- 7
- 8
- 9
- 10
- 11
- 12
- 13
- 14
- 15
- 16
- 17
- 18
- 19
- 20
- 21
- 22
- 23
- 24
- 25
- 26
- 27
- 28
- 29
- 30
- 31
- 32
- 33
- 34
- 35
- 36
- 37
- 38
- 39
- 40
- 41
- 42
- 43
- 44
- 45
- 46
- 47
- 48
- 49
- 50

1
2
3
4
5
6
7
8
9
10

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.055
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.887	.977	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

CHOLLAS VIEW IMP'S:

INDEX

SEWER: S'ly CRAIGIE between

45th + 47th (CHOLLAS #2)

1

SEWER: S'ly Hilltop

E'ly 44th

2

CB Grades: - 45th -
MARKET to Hilltop

3

"G" ST: 45th E'ly to END

8

BOYLSTON ST: 45th E'ly to END

9

"F" ST: 45th E'ly to 47th

11

CRAIGIE ST: 45th E'ly to 47th

14

HILLTOP DR: 43rd to 47th

17

47th ST: SUB-linearly to Hilltop

24

4' TYPE "K" INLET & CURBOUT "G" ST

26

4' " " " " CRAIGIE

26

(4' " " " " 44th)

27

STA 5+41.5 (w'ly side)

(4' TYPE "K" INLET 44th ST.)

27

STA 8+92 w'ly side

(4' TYPE "K" INLET
TREMONT - E'ly OF 44th
- ALSO PROP. GRADES (R-GRADES) OUT-DE-SAC)

28

INDEX (CONT)

Pg.

CRAIGIE ST: 45th-Wly	23	WATER MAIN: COLUSA	MILDRED to LINDA VISTA RD:	50
"F" ST: 45th-Wly to 44th	29	SEW LINE: ESMT LOT 18		48
49th ST: MKT to "F" ST (= 90° LT 44th)	31	(ENCANTO) RO MISSION S. DIEGO CITY-COUNTY BDRY to 60th		
"G" ST: 45th wly to Cul-De-Sac	34	SEW Line: 49th Nly Imp.		51
TREMONT: 44th-NEly to CUL-DE-SAC	37	Permit Job w.o. 20034 No plans (no const. drawings) No data (Designed in field)		
TREMONT: 44th SWly to CUL-DE-SAC	38			
44th ("F" ST. to HILLTOP DRIVE)	40			
Sew-Lats: LOTS 135+136	47			

CLARK
GARBER
MOORE
ABRENILLA
5-21-58
W.O. 21700

Sewer: S'ly CRAIGIE
bet. 45' +h + 47' +h

Ref: DWG: 5550-D
Notes: J-22 - ALLEN-

1

CHK: 176.41 = 176.37 = 2x2 HUB 5+09:33

2+80

176.44
167.38
C 9.06

(Fd ^{2x2} HUB AS per ALLEN)

2+45

175.82
167.09
C 8.73

5+09:33 = M.H. #3
stubs 6+12' RT M.H.

177.03
169.27
C 7.76

2+10

175.58
166.80
C 8.78

4+90

175.67
169.11
C 6.56

1+75

174.85
166.51
C 8.34

4+55

177.21
168.82
C 8.39

1+40

174.48
166.22
C 8.26

4+20

177.50
168.54
C 8.96

1+05

173.14
165.94
C 7.80

3+85

177.57
168.25
C 9.32

0+70

173.51
165.65
C 7.86

3+50

177.37
167.96
C 9.41

(Stubs set 6' RT)

0+35

172.53
165.36
C 7.17

3+15

176.78
167.67
C 9.11

stubs M.H. 6+12' RT

0+00 = M.H. #1

= 2x2 HUB AS per
city notes (Allen)

171.68
165.07
6.61

stubs 6+12' RT M.H.

3+01 = M.H. #2

(Fd 2x2 HUB as per Allen)

176.70
167.55
C 9.15

B.M. dir. Elev. Pads

Kol. 19 = E.P.K.
45' +h + "F"

C/ARK
GAEBER
MOORE
ABRENNIA
5-22-58
W.O. 21700

SEWER: SLY HILLTOP DR.
Ely 44' to ST.

Ref: DWG: 5554-D

Notes J-22 (Allen)

Prelim. Survey 10' OFF FAT 2
Prop. M.H. #4 + 5' off
At m.H. #6 (to W'ly)
New Survey Necessary in
Field, required 3 hrs. time

CHK: 159.66 = 159.64 = 2x2 HUB
(4 + 61.17 - Allen's Survey)

STA.	FL. Elev's	STA:	FL. Elev's
		Stubs 6' + 12' RT	168.93
		2 + 74.5 = M.H. #4	163.81
		(W'ly of M.H. #5)	C 5.12
(Ely of M.H. #5 = 0+00)		2 + 45	168.25
Stubs set 6' + 12' RT			162.43
			C 5.82
1 + 87.67 = M.H. #6	158.33	2 + 10	166.40
	151.87		160.78
	C 6.46		C 5.62
1 + 75	158.78	1 + 75	164.02
	151.81		159.14
	C 6.97		C 4.88
1 + 40	158.27	1 + 40	161.57
	151.63		157.49
	C 6.64		C 4.08
1 + 05	157.04	1 + 05	159.65
	151.45		155.85
	C 5.59		3.80
0 + 70	154.99	0 + 70	158.12
	151.27		154.20
	C 3.72		C 3.92
0 + 35	154.02	0 + 35	157.50
LINE (to Ely)	151.09	LINE (to W'ly)	152.56
	C 2.93		C 4.94
0 + 00 = M.H. #5	150.91	0 + 00 = M.H. #5	156.14
		(Stubs 6' + 12' RT to W'ly Line)	150.91
= RE. EXIST 8" N'ly 15'ly SOWER			C 5.23
+ 8' E + W - 8' EASEMENT			
B.M. (Dir. Elev. Rod):	170.80 = E Bolt 44' H + Hilltop		

Stubs 6' RT E
-0.511 gradient

Stubs 6' RT E

478 gradient

CLARK
GARBER
MOORE
AGRENILLA
5-27-58
W.O. 21700

C.B. GRADES:

45th ST

REF: DWG: 5545-D
5557-D

Notes: J-22

3

MKT to "G"

STA	LT CB	E	RT CB	STA	LT CB	E	RT CB
				#2	162.18 162.00 Co.18		62.67 162.65 Co.02
1+75	161.14 161.41 Fo.27		61.42 161.51 Fo.09 <small>(changed to gain coverage over EXIST Pav.)</small>	61.42 161.61 Fo.19	#3 <small>(out)</small>	161.81 161.60 Co.21	161.64 161.60 Co.04 62.73 162.67 Co.06
1+50	160.93 161.13 Fo.20		61.20 161.27 Fo.07	61.20 161.34 Fo.14	CBEC "G" NWly <small>(out)</small>	161.64 161.31 Co.33	161.47 161.31 Co.16 162.98 162.70 Co.28
1+25	160.72 160.85 Fo.13		60.82 161.03 Fo.21	60.82 161.06 Fo.24	2+30 = 2"G"		162.02 162.02 = FL 8' X- RT.
1+00	160.33 160.58 Fo.25		60.33 160.78 Fo.45		CBEC "G" SWly	161.10 161.31 Fo.21	162.88
0+75	160.20 160.30 Fo.10		60.40 160.54 Fo.14		#3	161.37 161.55 Fo.18	162.38 162.40 Fo.02
0+50	159.93 160.02 Fo.09		59.97 160.29 Fo.32		#2	161.55 161.74 Fo.19	62.02 162.20 Fo.18
0+30	159.78 159.80 Fo.02		59.73 160.10 Fo.37		#1	161.52 161.72 Fo.20	61.36 161.97 Fo.61 61.36 162.00 Fo.64
0+12 = Beg New CB	meet EXIST 159.48		meet EXIST 159.76		1+90 = CB BC'S	161.40 161.58 Fo.18	61.46 161.66 Fo.20 61.46 61.78 Fo.32

B.M. (Dir. Elev. Rod)

158.85 = NW RP
MKT + 45th

454h
"G" to Boylston

4

STA	CB	E	CB	RT	STA		
					(See P. 5 opp. B.C. RT)		
4+20	165.65 165.79 Fo. 14		65.98 165.78 Co. 20			165.99 166.50 Fa. 51	
3+95	165.13 165.30 Fo. 17		65.08 165.30 Fo. 22		5+06.95 LT. only		
3+87 Lot-Liner RT					4+86.95 = SF LT. only	166.50 166.80 Fo. 30	
3+70	164.16 164.81 Fo. 65	164.54 (out) 164.81 Fo. 27	64.84 164.83 Co. 01				
3+65 Lot-Liner LT					4+66.95 LT. only	166.37 166.65 Fo. 28	
3+45	164.15 164.32 Fo. 17		164.00 164.35 Fo. 35				
3+35 Lot-Liner							167.50 167.39 Co. 11
3+20	163.27 163.84 Fo. 57	163.74 (out) 163.84 Fo. 10	163.76 163.87 Fo. 11				SELY E.C. Boylston
2+95	163.31 163.35 Fo. 04		163.13 163.39 Fo. 26			67.14 167.18 Fo. 04	#3
						66.90 166.87 Co. 03	#2
2+70 CB = B.C.	162.77 162.86 Fo. 09		162.47 162.91 Fo. 44			66.74 166.64 Co. 10	#1
#1	162.52 162.47 Co. 05		62.58 162.75 Fo. 17		4+46.95 = CB BC RT. only (SELY Boylston)	166.06 166.31 Fo. 25	66.23 166.30 Fo. 07

45th (Boylston to "F")

G+10	163.53 163.66 Fo.13	63.62 163.65 Fo.03	# 2	60.96 161.94 Fo.44 Fo.18	62.68 162.21 Co.47
5+89 LOT LINE RT.					
5+85 ✓	164.09 164.32 Fo.23	164.11 164.30 Fo.19	# 1	61.45 161.70 Fo.25	62.34 161.93 Co.41
			(SW 1/4 RT.)		
5+60 ✓	164.74 164.97 Fo.23	65.04 164.95 Co.09	=CB BC RT 7+37.95 (SE 1/4 "F")		(SE 1/4 RT.) 61.92 161.89 Co.03
5+46.95 ✓	165.24 165.32 Fo.08	65.37 165.29 Co.08	=CB BC LT. 7+36.45 (SW 1/4 "F")	161.61 161.87 Fo.26	61.72 161.87 Fo.15 (RT)
CB BC 5+26.95 (NE 1/4 45th + Boylston)	165.55 166.00 Fo.45	65.85 165.96 Fo.11	7+25	161.62 161.93 Fo.31	61.78 162.03 Fo.05
		65.98 #1 166.34 Fo.36	7+00	161.72 162.06 Fo.34	62.08 162.29 Fo.21
		66.67 #2 166.77 Fo.10	6+75	161.76 162.20 Fo.44	61.81 162.32 Fo.51
		67.09 #3 167.22 Fo.13	6+73 LOT LINE RT. 6+62 = " " LT. 6+50 = 9th BPK	162.41 162.63 Fo.22	62.79 162.62 Co.15
		67.02 167.34 Fo.32	NE 1/4 E.C. Boylston	6+35 162.42 163.02 Fo.60	63.10 163.01 Co.09

				# 3	164.80 164.91 Fo.11	66.57 166.59 Fo.02
CB BC LT 8+21.45 NWLY	61.82 162.26 Fo.44			# 2	164.78 165.21 Fo.43	66.17 166.05 Co.12
CB BC RT 8+19.95 NELY		62.50 162.32 Co.18	(NELY)	# 1	164.90 165.33 Fo.43	65.80 165.55 Co.25
# 1	61.42 161.94 Fo.52	62.46 162.21 Co.25		(SWLY RET) 75 1/2 CRAIGIE 9468.91 = CB BC'S:	164.96 165.14 Fo.18	65.11 165.10 Co.01
# 2	60.95 161.33 Fo.38	62.64 162.35 Co.29		9460	164.79 164.95 Fo.16	64.83 164.93 Fo.10
# 3	60.64 160.60 Co.04	62.97 162.77 Co.20		9435	164.26 164.46 Fo.20	64.28 164.46 Fo.18
CB EC "F" NWLY	60.27 160.21 Co.06	63.43 163.20 Co.23	CB EC "F" (NELY)	9+10	163.66 163.97 Fo.31	64.04 163.99 Co.05
(7+96.70 = E+W X-GUT)				8+98.95 Lot Line RT+LT	163.10 163.49 Fo.39	63.30 163.53 Fo.23
(7+59.70 = E+W X-GUT)				8+85	162.56 163.00 Fo.44	63.19 163.06 Co.13
E.C. ON "F" (SWLY)	60.20 160.15 Co.05	63.09 163.15 Fo.06	EC "F" (SELY)	8+60		
# 3	60.53 160.89 Fo.36	62.74 162.68 Co.06		8+35	162.13 162.52 Fo.39	62.58 162.60 Fo.02

45th ST (CRAIGIE to Hilltop)

	LT.	RT	
11+28.91= Lotline LT.			
11+25	166.58 166.16 Co.42	166.45 166.18 Co.27	166.12 166.18 F.O.06
11+21.86 Lotline RT.			
11+00= Grade SW	166.78 166.53 Co.25	167.01 166.51 Co.50	
10+75	166.79 166.60 Co.19	167.14 166.60 Co.54	
10+48.91= CB 136'S (NW 1/4)	166.46 166.39 Co.07	166.61 166.41 Co.20	(NW 1/4 Ret.)
#1	166.28 166.11 Co.17	166.82 166.32 Co.50	166.41 166.32 Co.09
#2	165.92 165.53 Co.39	166.96 166.42 Co.48	166.51 166.42 Co.09
#3	165.59 165.01 Co.58	166.96 166.70 Co.26	166.56 166.70 F.O.14
CB EC'S: CRAIGIE (NW 1/4)	165.35 164.66 Co.69	167.15 166.72 Co.23	(NW 1/4)
10+08.91= GRAIGIE			165.35 F.M. & CUT: 165.55 GRADE
EC CRAIGIE (SW 1/4)	164.49 164.50 F.O.01	166.97 166.94 Co.03	(SE 1/4)

	163.70 162.28 C1.92	163.69 162.28 C1.41	
CB EC Hilltop			167.64 165.49 C2.15
#3	163.82 162.85 Co.97	163.87 162.85 C1.62	166.71 164.69 C2.02
#2	164.19 163.31 Co.88	164.31 163.31 C1.00	166.31 164.38 C1.93
#1	164.45 163.83 Co.62	164.78 163.83 Co.95	165.75 164.29 C1.46
12+38.91= CB 80'S		164.72 164.43 Co.29	165.76 164.56 C1.20
12+25		165.17 164.63 Co.54	165.57 164.67 Co.90
12+00		165.04 165.02 Co.02	165.54 165.01 Co.53
11+75	165.02 163.41 F.O.39	165.35 165.41 F.O.06	166.30 165.48 Co.82
11+50		166.26 165.83 Co.43	166.61 165.95 Co.76

165.39
165.49
F.O.10

165.22
165.11
Co.11

164.70
164.69
164.40
164.38
F.O.07

164.32
164.24
Co.03

164.56
164.56
F.O.17

166.15
165.81
Co.30

marked out

marked out

(EC Hilltop)

#4 (RT only)

(SE 1/4 Ret.)

66.67
164.56
C2.11

457L E4

LT.	E		RT.		LT.	E		RT.	
	CB	E	CB	E		CB	E	CB	E
2+00	171.44 171.11 Co.33		170.99 171.18 Fo.19						
1+75	69.50 169.20 Co.30		169.04 169.20 Fo.16		4+00	82.10 182.21 Fo.11		181.97 182.27 Fo.30	
1+50 = E.V.C.	67.61 167.30 Co.31		67.19 167.23 Fo.04		3+75	81.35 181.43 Fo.08		81.71 181.43 Co.28	
1+25	66.00 165.75 Co.25		65.31 165.75 Fo.44		3+50	80.59 180.41 Co.18		80.50 180.45 Co.05	
1+00	64.82 164.32 Co.50		64.04 164.38 Fo.34		3+25	79.41 179.32 Co.09		79.36 179.36 grade	
0+75	63.44 163.50 Fo.86		63.24 163.50 Fo.26		3+00	78.12 177.99 Co.13		77.76 178.06 Fo.30	
0+50 = B.V.C.	63.22 163.07 Co.25		62.74 163.01 Fo.27		2+80.77 = ST. BC	76.73 176.95 Fo.22		176.57 177.02 Fo.45	
0+25	63.02 162.80 Co.22		62.39 162.76 Fo.37		2+65.38	75.72 175.00 Fo.28		75.58 175.10 Fo.52	
0+16 = CB. E.C.S. 454L (See pg 3)	62.98 162.70 Co.28		62.21 162.68 Fo.47		2+50 = B.V.C.	75.21 174.87 Co.40		74.60 174.95 Fo.35	
					2+25	73.51 173.10 Co.41		173.05 173.19 Fo.14	

"G" ST (CONT) ELY #57h

BOYLSTON

9

45.76 ELY TO END

LT. CB RT CB

2+25 76.50 76.32
176.48 176.44
Co.02 Fo.12

2+00 75.26 75.10
175.22 175.19
Co.04 Fo.09

1+75 73.99 73.88
173.96 173.93
Co.03 Fo.05

1+50 72.78 72.61
172.70 172.68
Co.08 Fo.07

1+25 71.45 71.46
171.46 171.43
Fo.01 Co.03

1+00 70.16 70.23
170.18 170.18
Fo.02 Co.05

4+63⁵ END 82.91 83.37
"G" ST. 183.37 183.36
Fo.46 Co.01

0+75 68.78 68.66
169.05 169.10
Fo.27 Fo.44

4+675 83.02 83.24
183.20 183.20
Fo.18 Co.04

0+50 67.96 68.38
168.10 168.25
Fo.14 Co.13

4+30= 82.80 83.14
ST. EC 183.00 183.02
Fo.20 Co.12

0+25 67.34 67.64
167.44 167.49
Fo.10 Co.15

4+15 82.52 82.75
182.85 182.89
Fo.33 Fo.14

0+16 = CB ELS 67.02 67.50
(See Pg 4) 167.34 167.39
(75) Fo.32 Co.11

4+30=Ec. ST.	183.82 183.50 Co.32	83.40 183.50 Fo.10
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4+15	183.75 183.40 Co.35	83.38 183.40 Fo.02
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4+00	183.40 183.33 Co.07	183.19 183.31 Fo.12
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3+75	183.78 182.97 Co.51	182.87 182.92 Fo.05
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3+50	182.86 182.26 Co.60	182.26 182.30 Fo.04
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3+25	181.83 181.48 Co.35	181.27 181.33 Fo.06
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3+00=8.V.C.	180.40 180.28 Co.13	180.07 180.20 Fo.13
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2+80.77= ST.8C	78.99 179.31 Fo.32	178.94 179.23 Fo.29
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2+75	178.70 179.01 Fo.31	78.46 178.94 Fo.48
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2+50	77.80 177.74 Co.06	77.70 177.69 Co.01
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4+66.5=END
Boylston

4+46.75

183.36

183.82
183.43
Co.39

183.37

83.34
183.43
Fo.09

(See Pg 9)

"F" ST.
(45th Ely to 47th)

LT. RT.

	LT	CB	E	CB	RT		LT	CB	E	CB	RT
1+75		68.48 168.43 C0.05		68.57 168.46 C0.11							
1+50. EVC.	167.64 168.08 Fo.44	68.83 168.88 Fo.05	(K ^{od})	68.02 168.11 Fo.09	67.69 168.11 Fo.42	4+00		71.72 171.63 C0.09	(K ^{od})	71.78 171.61 C0.17	71.44 171.61 Fo.17
1+25		167.61 167.60 C-0.01		67.49 167.60 Fo.11		3+75		71.52 171.27 C0.25	(K ^{od})	71.52 171.26 C0.26	171.18 171.26 Fo.08
1+00		166.88 166.98 F-0.10		66.82 167.01 Fo.19		3+50		71.14 170.92 C0.22	(K ^{od})	71.06 170.91 C0.15	170.62 170.91 Fo.29
17.1		166.34 166.25 C-0.14		66.30 166.25 C0.05		3+25	170.41 170.56 Fo.15	70.74 170.56 C0.18	(K ^{od})	70.83 170.56 C0.27	
0+82.88		165.79 165.63 C-0.16		65.55 165.60 Fo.05	165.27 165.60 Fo.33	3+00		70.36 170.21 C0.15	(K ^{od})	70.47 170.21 C0.26	
0+65.77 = ST. B.C	165.46 165.63 Fo.17	165.79 165.63 C-0.16	(K ^{od})	65.55 165.60 Fo.05	165.27 165.60 Fo.33	2+75		69.96 169.85 C0.11	(K ^{od})	69.89 169.86 C0.03	169.76 169.86 Fo.10
0+50		165.02 164.82 C-0.20		64.78 164.82 Fo.04		2+50	169.58 169.50 C0.08	69.40 169.50 Fo.10	(K ^{od})	69.60 169.51 C0.09	
0+25		163.71 163.64 C0.07		63.54 163.59 Fo.05		2+25	168.84 169.14 Fo.30	69.13 169.14 Fo.01	(K ^{od})	69.28 169.16 C0.12	69.14 169.16 Fo.02
CB E.C'S = 0+16 (See pg 6)		163.43 163.20 C0.23		163.09 163.15 Fo.06		2+00		168.73 168.79 Fo.06	(K ^{od})	68.93 168.81 C0.12	168.81

T.B.M. (Dir. Elev. Rod:

161.19 = E.P.K
45th "F"

"F" ST. (CONT.)

LT		E		RT		LT		RT	
CB		E		CB		CB		E	
6+25	172.12 172.14 Fo.02			171.66 172.16 Fo.50		8+75	170.09 169.92 Co.17		169.80 169.92 Fo.12
6+00	172.51 172.30 Co.21			172.14 172.34 Fo.20		8+50	170.14 169.74 Co.40		169.49 169.69 Fo.20
5+75	172.75 172.50 Co.25			172.33 172.43 Fo.10		8+23=9 TYPE "A" X-GUTT (8) RADIAL ALIGN. 3	170.09 169.67 Co.42	169.09 168.95 Co.13	169.66 169.58 Co.08
5+50	172.87 172.69 Co.18			172.06 172.52 Fo.46		8+00	170.25 169.75 Co.50		169.25 169.83 Fo.58
5+25	172.89 172.72 Co.17			172.50 172.69 Fo.19		7+75	170.68 170.05 Co.63		170.18 170.00 Co.18
5+00	172.83 172.68 Co.15			172.02 172.69 Fo.57		7+50	171.10 170.52 Co.58		170.42 170.40 Co.02
4+78.22 = P.R.C	172.61 172.60 Co.07	72.72 (K-od)		72.66 172.56 Co.10		7+25	71.17 71.13 Co.04		170.42 171.04 Fo.62
4+64.1	72.53 172.50 Co.03			72.43 172.46 Fo.03		7+00	172.08 171.58 Co.50		171.36 171.51 Fo.15
4+50 = BVL	72.56 172.34 Co.22			72.32 172.30 Co.02		6+75	72.07 171.86 Co.21		171.59 171.83 Fo.24
4+25	71.66 171.98 Fo.32	72.06 (K-od)		72.11 (K-od) 171.95 Co.16	71.73 171.95 Fo.22	6+50	172.41 171.98 Co.43		171.90 171.98 Fo.08

(=E 4" TYPE "K" INLET
OF RT)

Resos
169.51
169.58
Fo.07 - IF CB
169.51
168.75 - GUT
to Co.76

"F" ST. (CONT)

	LT	RT		LT (Reset 7/25)	RT (Reset 7/25)
10+75	175.03 174.90 Co. 13	174.37 174.93 Fo. 56	E.C. 474h (wily)	175.17 174.75 Co. 42	173.68 172.48 C 1.15 (sw'ly)
10+50	174.68 174.14 Co. 54	174.08 174.21 Fo. 13	# 3	174.76 174.73 Co. 03	174.59 174.73 F-0.14 C 1.04
10+25	173.88 173.48 Co. 40	173.28 173.52 Fo. 24	# 2	175.60 174.84 Co. 76	175.84 174.84 C-1.00 C 2.11
10+00	172.82 172.53 Co. 29	172.25 172.55 Fo. 30	# 1	175.46 175.00 Co. 46	175.76 175.00 C-0.76 Co. 45
9+75	172.16 171.84 Co. 32	171.72 171.86 Fo. 14	12+26.52= C B B C	175.42 175.30 Co. 12	174.93 175.25 Fo. 32
9+50	171.42 170.97 Co. 45	170.84 170.99 Fo. 15	12+00	176.25 175.67 Co. 58	175.53 175.69 Fo. 16
9+25	171.00 170.63 Co. 37	170.38 170.65 Fo. 27	11+75	176.66 175.97 Co. 69	175.98 176.06 Fo. 18
9+00	170.49 170.12 Co. 37	169.63 170.12 Fo. 49	11+50	176.20 176.11 Co. 09	175.77 176.14 Fo. 37
8+89.61= P.R.C	170.41 170.01 Co. 40	169.69 169.99 Fo. 30	169.41 169.99 Fo. 58	176.52 175.86 Co. 66	175.80 175.96 Fo. 16
			11+00	176.04 175.41 Co. 63	175.34 175.43 Fo. 09

CRAIGIE ST:
(454h ELY to 474h)

	LT CB	E	RT CB		LT CB	E	RT CB
2+00	72.43 172.05 Co.38		72.00 172.05 Fo.05				
1+75	71.82 171.39 Co.43		71.32 171.39 Fo.07	4+25	77.42 177.28 Co.14		77.28 177.27 Co.01
1+50	70.84 170.73 Co.11		70.24 170.73 Fo.49	4+00 EKC	77.03 176.85 Co.18		76.70 176.85 Fo.15
1+25	70.30 170.06 Co.24		69.87 170.06 Fo.19	3+75	76.64 176.40 Co.24		76.30 176.40 Fo.10
1+00	69.75 169.40 Co.35		69.28 169.40 Fo.12	3+50	76.35 175.95 Co.40		75.50 175.84 Fo.34
0+82.88 df 23.26	69.13 168.89 Co.24		68.72 168.90 Fo.18	3+25	75.40 175.41 Fo.01		75.12 175.40 Fo.28
0+65.97 ST. B.C df 11.63	68.53 168.38 Co.15		68.00 168.40 Fo.40	3+00 BVC	75.00 174.70 Co.30		74.65 174.72 Fo.07
0+41	67.93 167.65 Co.28		67.70 167.71 Fo.01	2+75	74.30 174.04 Co.24		74.01 174.06 Fo.05
0+16= CB EGS (See Pg 7)	67.15 166.92 Co.23		66.97 166.94 Co.03	2+50	73.66 173.38 Co.28		72.77 173.39 Fo.62
				2+25	72.86 172.71 Co.15		72.57 172.71 Fo.14

T.B.M (Dir. Elev. Rod) 165.62 - E P.K. NAIL
454h CRAIGIE

CRAIGIE (CONT.)

67

15

	LT.	RT.		LT.	RT.
	CB	CB		CB	CB
6+50 BVC	81.51 181.18 Co.33	81.02 181.10 Fo.08	8+89.61 =P.R.C.	82.42 182.36 Co.06	82.01 182.28 Fo.27
6+25	80.89 180.73 Co.16	80.38 180.68 Fo.30	8+75	82.38 182.30 Co.08	81.92 182.22 Fo.30
6+00	80.30 180.30 Grade	80.15 180.25 Fo.10	8+50	82.40 182.20 Co.20	82.01 182.12 Fo.11
5+75	80.24 179.86 Co.38	79.80 179.83 Fo.03	8+25	82.36 182.10 Co.26	81.99 182.02 Fo.05
5+50	79.64 179.41 Co.23	79.08 179.41 Fo.33	8+00	82.17 182.00 Co.19	81.79 181.92 Fo.13
5+25	79.40 178.98 Co.72	78.88 178.98 Fo.10	7+75	82.34 181.90 Co.44	81.84 181.82 Co.02
5+00 21.9'	78.76 178.55 Co.21	78.38 178.55 Fo.17	7+50	82.26 181.80 Co.46	81.57 181.72 Fo.15
4+78.22 =P.R.C.	78.42 178.18 Co.24	78.06 178.18 Fo.12	7+25	81.77 181.70 Co.07	81.62 181.62 Grade
4+64.1	78.11 177.94 Co.17	77.65 177.94 Fo.29	7+00 E.V.C.	81.98 181.60 Co.38	81.48 181.52 Fo.04
4+50	77.81 177.71 Co.10	77.56 177.70 Fo.14	6+75	81.75 181.45 Co.30	81.25 181.40 Fo.15

CRAIGIE (CONT.)

LT.	CB	E	CB	RT.	RT.
11424.44 =E.C	86.09 185.88 Co.21		85.70 185.91 Fo.21		
11400	86.16 185.80 Co.36		85.81 185.79 Co.02		(Knocked-out) (Reses 7/25) (Reset 7/25)
10775	85.83 185.50 Co.33		85.44 185.50 Fo.06	CB, 3 EC, 3 on 474h (NW 1/4)	182.02 181.11 Co.91
10750	85.33 185.03 Co.30		185.04 185.06 Fo.02	# 3	181.81 181.08 Co.73
10725	84.70 184.40 Co.30		84.42 184.40 Co.02	# 2	181.08 181.08 0.00
10700	84.06 183.76 Co.30		183.58 183.61 Fo.03	# 1	80.98 179.57 C 1.41
9775	83.35 183.10 Co.25		82.88 183.15 Fo.27		181.40 181.34 C 0.46
9750	82.97 182.58 Co.39		182.71 182.64 Co.07		81.54 180.53 C 1.01
9725	82.70 182.58 Co.22		182.61 182.50 Co.11		181.82 181.75 C 0.07
9700	82.47 182.40 Co.07		82.30 182.32 Fo.02		81.94 181.43 C 0.51
				12+26.28 =CB, BC'S	182.30 182.23 Co.07
				12+00	83.57 183.16 Co.41
				11+75	84.72 184.18 Co.54
				11+50	85.56 185.20 Co.36
					82.27 182.18 Co.09
					83.50 183.16 Co.34
					84.45 184.23 Co.22
					85.23 185.30 Fo.07

HillTOP DR:
(43'rd to 47'4h)

DAY. 1013-4-0.40

STA.	LT	RT
		Berm P.L
1+50		164.86 164.88 164.55 164.55 Co.31 Co.33
1+25		164.89 164.60 Co.29
1+00		164.82 164.95 164.66 164.63 Co.16 Co.32
0+75		164.97 164.80 Co.17
0+50		165.06 165.00 164.88 164.88 Co.18 Co.12
0+22.2 Beg 6" Berm 20' RT		165.28 165.22 164.92 164.92 Co.36 Co.3.0
0+00=EL/line 43rd (J.22)		
T.B.M	(44'4L + TREMONT)	153.47 = E.P.K

STA.	LT	RT
3+00		168.40 168.40 168.03 168.03 Co.37 Co.37
2+75		167.40 167.20 Co.20
2+50		166.54 166.53 166.42 166.42 Co.12 Co.11
2+25		165.80 165.64 Co.16
2+16.6 Beg CB RT END Berm		Knocked-out 165.46 165.25 165.44 165.44 Co.02 Fo.19
2+00		164.94 165.05 165.02 165.02 Fo.08 Co.03
175		164.88 164.65 Co.23
catch-basin (abandon EXIST)		164.65 164.50 Co.15
1+68 = E TYPE D catch-BASIN		184.65 163.90-grate Co.75
Set stub E (1+68) 20" BASIN 3' BK inside - Fe. BK-wall (5'5") OF BOX		161.16 F.L

HILLTOP DR (CONT.)

LT.	RT.	STA	E	CB	STA	LT.	RT.	(S'ly)	
		5+00		172.84 172.49 Co. 35	172.92 172.49 Co. 43			162.19 161.79 Co. 40	162.18 161.79 Co. 39
		4+75		173.12 172.83 Co. 29				162.78 162.34 Co. 44	
		4+50		172.98 172.60 Co. 38	173.03 172.60 Co. 43			163.70 163.21 Co. 49	163.86 163.21 Co. 65
		4+25		172.46 172.25 Co. 21				164.28 164.14 Co. 14	
		SE'ly 4+19.06 = CB. EC HILLTOP 44' 4h (See Pg 42)		172.17 172.12 Co. 05	172.08 172.12 Fo. 04			165.68 165.49 Co. 19	165.71 165.49 Co. 22
								167.13 166.92 Co. 21	
								168.21 168.31 Fo. 10	168.30 168.31 Fo. 01
								169.98 169.80 Co. 18	
		3+37.06 = SW'ly - CB. EC HILLTOP 44' 4h (see Pg 42)		169.75 169.44 Co. 31	169.62 169.72 Co. 20			171.31 171.01 Co. 30	171.41 171.00 Co. 41
		3+25		169.34 168.96 Co. 38				172.32 172.00 Co. 32	

LT.	RT.	CB			
10+00		161.28 160.26 C1.02	61.83 160.26 C1.37	11+75	160.56 160.00 Co.56
9+75		161.63 160.49 C1.14		11+50	160.04 159.73 Co.31
9+50		161.21 160.72 Co.49	61.75 160.72 C1.03	11+25	159.29 159.50 Fo.21
9+25		161.67 160.83 Co.84		(Lower EXIST. BASIN) IN-ST, 12" etc.	E. end 58.81 159.35 Fo.54
9+00		161.68 160.94 Co.74	61.92 160.94 Co.98	11+04 = E T-TYPE "K" IN/ET RT (stubs 5' BK CB FO ON outside edge Box)	(200) 159.35 158.52 = 60TT. W. end 58.60 159.35 Fo.73
8+75		161.68 161.05 Co.63		11+00 (not set)	159.35 159.35
8+50		161.11 161.16 Fo.05	161.40 161.16 Co.24		159.36 159.57 Fo.21
8+25		161.70 161.27 Co.43		10+75	160.00 159.80 Co.20
8+00		161.61 161.39 Co.22	161.63 161.39 Co.24	10+50	59.75 159.80 Fo.05
7+75		161.76 161.53 Co.23		10+25	160.50 160.03 Co.47

LT.	RT. (SLY)		♀	RT. (SLY)	
	CB	P.L		CB	P.L
13+75	166.61 166.80 F-0.19	166.80	16+00	177.05 177.23 F-0.18	178.40 177.23 C1.17
13+53.30 =SELYCBEC Hilltop 45th (See Pg 7)	165.39 165.49 F-0.10	165.49	15+75	176.77 176.90 F-0.13	
			15+50=EXC	176.16 176.32 F-0.16	177.42 176.32 C1.10
			15+25	174.97 175.64 F-0.67	
			15+00	174.18 174.56 F-0.38	175.74 174.56 C1.18
12+67.30 =SWLYCBEC Hilltop 45th (See Pg. 7)	162.28	64.30 162.28 C2.02	14+75	173.23 173.34 F-0.11	
12+50	163.10 161.85 C1.25	63.50 161.85 C1.65	14+50=BYC	172.03 171.87 C-0.16	173.40 171.87 C1.53
12+25	162.17 161.09 C1.08		14+25	175.35 170.30 C-0.05	170.30
12+00	161.29 160.52 C0.77	61.70 160.52 C1.18	14+00	168.39 168.50 F-0.11	72.13 168.50 C3.63

HILLTOP DR. (CONT.)

21

KT.	RT	CB	CB
18+50		181.22 82.32 181.25 181.25 F-0.03 C1.07	
			20+75
18+25		180.65 180.70 F-0:05	
			20+50
18+00		180.16 81.51 180.16 180.16 0.00 C1.35	
			20+25
17+75		169.68 179.70 F-0.02	
			20+00
17+50		179.45 180.53 179.25 179.25 C-0.20 C1.28	
			19+75
17+25		178.82 178.88 F-0.06	
			19+50
17+00		178.49 79.81 178.51 178.51 F-0.02 C 1.30	
			19+25
16+75		178.09 178.23 F-0.14	
			19+00
16+50		178.00 179.15 177.94 177.94 C-0.06 C1.21	
			18+75
16+25		177.36 177.59 F-0.23	
			186.87 187.12 F-0.25
			186.24 87.60 186.47 186.47 F-0.23 C 1.13
			185.91 185.82 C-0.09
			185.31 86.42 185.18 185.18 C-0.13 C1.24
			184.34 184.53 F-0.19
			183.91 84.75 183.88 183.88 C-0.03 C 1.07
			183.39 183.23 C-0.16
			182.61 83.72 182.58 182.58 C-0.03 C 1.14
			181.96 181.90 C-0.06

HILLTOP DR. (CONT.)

26

LT.	RT.	CB	LT.	RT.	CB
			25+50		
23+00	192.61 192.89 F-0.28	93.06 192.89 C 0.17			189.79 189.70 C-0.09
			25+25		
22+75	192.07 192.40 F-0.33				190.72 90.60 190.48 190.48 F-0.06 C 0.12
			25+00		
22+50	191.64 191.67 F-0.03	92.19 191.67 C 0.52			190.57 191.05 F-0.48
			24+75		
22+25	190.89 191.02 F-0.13				192.08 192.13 191.73 191.73 C-0.35 C 0.40
			24+50		
22+00	190.26 190.37 F-0.11	91.26 190.37 C 0.89			192.53 192.40 C-0.13
			24+25		
21+75	189.61 189.71 F-0.10				192.51 92.90 192.93 192.93 F-0.32 F 0.03
			24+00		
21+50	188.84 189.07 F-0.23	90.08 189.07 C 1.01			193.43 193.25 C-0.18
			23+75		
21+25	188.34 188.42 F-0.08				193.18 93.44 193.35 193.35 F-0.17 C 0.09
			23+50		
21+00	187.80 187.77 C-0.03	188.68 187.77 C 0.91			192.90 193.20 F-0.30
			23+25		

(#3) = PT. 5' BK CB FC
(see p 26)
155.25
156.27

STA:	Prop	CB	CB	Prop
(NAILS SET 3' INSIDE CB FC ON PAV)			F1.02	
(# 2)		156.43 156.96 Fo.53	156.25 156.73 Fo.48	(# 2)
(# 1)		157.48 158.10 Fo.62	157.50 158.11 Fo.61	(# 1)
		158.64 159.40 Fo.76	158.64 159.60 Fo.96	
		159.96 160.67 Fo.71	160.20 160.97 Fo.77	
		161.13 161.19 Fo.06	161.37 161.19 Co.18	
		188.38 187.73 Co.65	162.28 162.28 Grade	
		188.52 188.50 C-0.02	162.88 163.36 Fo.48	
		188.73 189.04 F-0.31	64.25 164.24 Co.01	
		89.14 189.04 Co.10	(Stubs set 5' BK CB FC.) 164.49 164.50 Fo.01	
			165.35 164.66 Co.69	
				165.62 = 4' P.K. 45 1/2 W'ly CRAIGIE

SW 1/4
CB EC
on 4744

186.46
186.25
C-0.21

P.R.C. LT.

3

187.92
186.85
C-1.07

1+18.10
= CB BC'S
1+10 = Lot-Line

1+00

2

0+75

0+55 = Lot-Line

0+50

1

0+25

(Stubs set 5' BK
CB FC.)

0+16 = CB
EC'S
(see P.T.)

T.B.M.

25+52.30
SW. CB BC
Hilltop 4744

47 1/4 ST:

SUB-LINE - N'y to HULLTOP DR.

24

STA	LT. C/B	RT.	STA	
			SW CBEC.	
			3+47.83	179.73
			47 1/4 + CRAIGIE (See Pg 16)	178.89
1+57.83 = 8 "F" (see Pg 13)				C-0.84
			3+25	178.61
				178.24
				C-0.37
swly 47 1/4 "F"	172.46		3+00	177.57
1+16.83 = CBEC	172.48			177.54
	F-0.02			C-0.03
			2+75	176.83
1+00	171.70			176.85
	172.00			F-0.02
	F-0.30		2+50	176.08
				176.16
				F-0.08
0+75	171.60		2+25	175.37
	171.36			175.47
	C-0.24			F-0.10
0+50	171.17		2+00 (Not set)	
	170.67			
	C-0.50			
0+25	170.22			
	169.80			
	C-0.42			
0+00 = PT. int. W. line 47 1/4 + SUB-LINE Hollas #2 - wzy	170.97		NWly CBEC	174.65
	168.66			174.75
	C-2.31		1+98.83	F-0.10
			47 1/4 "F"	

474w ST. (CONT.)

25

L.T.

R.T.

STA.	
6+00	185.95 185.88 C-0.07
5+75	185.46 185.19 C-0.27
5+50	184.40 184.50 F-0.10
5+25	183.52 183.80 F-0.28
5+00	182.98 183.11 F-0.13
4+75	182.20 182.42 F-0.22
4+50	181.70 181.73 F-0.03
NW CBEC	
4+27.83	181.08 181.11
474w CRAIGIE (See Pg 16)	F-0.03
3+87.83 = E CRAIGIE	

STA.

	186.46
= SW CBEC	186.25
6+12.83	C-0.21
474w HUNTAP	
(See Pg 23)	

4' TYPE "K" INLET & Culvert
WLY D. END - "G" ST.

4' TYPE "K" INLET & Culvert
WLY D. END - CRAIGIE ST.

26

STA.

CB

STA.

CB

GUT

mid pt culvert

37.54
135.24 = FL
C 2.30

mid pt culvert

154.92
152.45
C 2.47

NAILS / 5' BK. CB.F.C.
4 5' BK & Culvert.

E Box at
9+35.25 = CB.F.C.
(ONE "G" Proj.)
Ahead

FL = 37.85
135.85
C 2.00

37.85
138.68 CB.F.C. 137.85 = G.
F 0.83

CB.F.C. at "H"
2+00 = E 4' TYPE "K"
CB INLET
(ON C CRAIGIE)
(Proj. ahead)

55.25 55.25 155.25
156.27 155.44 153.44 = FL
F 1.02 F 0.19 C 1.81 Box

9+00.25 = 35' RADIUS
CUL-DE-SAC
(E STA. "G")

(1+65 = 35' CB RAD.)
{ CUL-DE-SAC }
E STA CRAIGIE
T.B.M.

165.62 = 6' PK
45' H + CRAIGIE

4' TYPE "K" INLET

44th ST (STA: 5+41.5 ON LT-W'LY)

STA.

LT (W'LY)

CB GUT

5+41.5

145.97	145.97
145.67	144.87
Co 30 CB	C 1.13 GUT

T.B.M

145.35 = E EC 44th ST.
(5+74.65)

4' TYPE "K" INLET

27

44th ST (STA: 8+42 ON LT-W'LY)

STA.

LT (W'LY)

CB GUT

8+42

Blend
Inlet

144.11	144.11
145.89	145.06
F 1.78	Fo. 95 - 6.11
	T.C.S

Blend
Inlet

144.40	144.40
145.89	145.06
F 1.47	Fo. 66 - 6.11
	T.C.S

Stubs Set 5' 10" BK CB FC ON LINE S'ly & N'ly edge Box

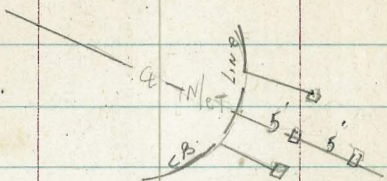
A' TYPE "K" INLET

TREMONT - E'ly 44th (0-225.5)

STA.

LT. (S'ly)

CB GUT



1/4 5' x 10' BK CB FC ON E (RADIAL) BOX
 Stubs set 5' BK CB along line outer edges Box
 (grade stub 5' BK CB FC ON E Box (RADIAL))

0-225.5

on LT (S'ly) TP CB

154.44

155.00

FG 56

154.44

154.17

CO. 27 GUT.

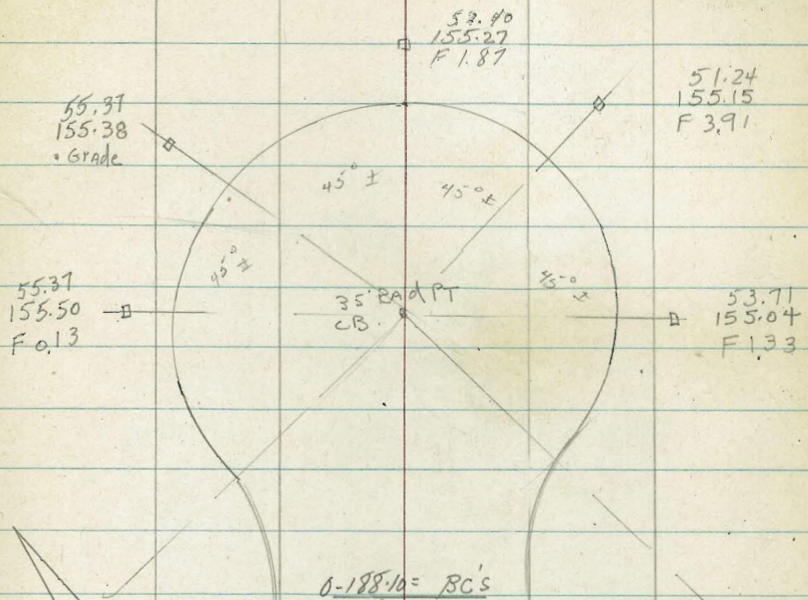
T.B.M.

153.49 = E Tremont + 44th (R'ly)

Prop.
 Rough-grades

TREMONT - E'ly of 44th 28
 Cul-DE-SAC.

STA.



(Stubs set 10' BK CB FC)

"F" ST: (7576- W'ly to 44th)

STA	LT	RT (N'ly)	STA	LT	RT
			4+25	149.92 149.55 Co.37	149.55 149.55 Grade
2+00	154.75 154.78 Fo.03	154.94 154.83 Co.11	4+00	150.04 149.95 Co.09	150.04 149.99 Co.05
1+75	155.32 155.50 Fo.18	155.23 155.55 Fo.32	3+75	150.51 150.30 Co.21	150.21 150.30 Fo.11
1+50	156.13 156.24 Fo.11	156.32 156.29 Co.03	3+50	151.00 150.79 Co.21	151.02 150.82 Co.20
1+25	156.88 156.97 Fo.09	157.02 157.02 Grade	3+25	151.56 151.24 Co.32	151.40 151.24 Co.16
1+00	157.58 157.70 Fo.12	157.75 157.75 Grade	3+00	151.92 151.92 Grade	152.03 151.89 Co.14
0+75	158.30 158.43 Fo.13	158.22 158.48 Fo.26	2+79.95 ST.B.C	152.20 152.42 Fo.22	152.22 152.48 Fo.26
0+50	158.67 159.16 Fo.49	158.92 159.22 Fo.30	2+75	152.58	152.63
0+25	159.88 159.93 Fo.05	159.99 159.99 Co.02	2+50	153.27 153.31 Fo.04	153.67 153.36 Co.31
0+16=SB EC (See pp. 6)	160.20 160.15 Co.05	160.27 160.21 Co.06	2+25	154.02 154.05 Fo.03	154.10 154.09 Co.01

STA.	P.L.	LT.	CB	RT.	P.L.	STA.
5+26.14 = end "F" (=7+14.73+44th)			(See p. 33) 149.04 149.95 Co.09			
CB.E.C. 44th (w/ly)				147.67 147.05 Co.62	147.05	
# 3				147.62 147.25 Co.37	147.25	
# 2				147.80 147.50 Co.30	147.50	
# 1				147.93 147.80 Co.13	147.80	
5+09.14 = CB BC RT (44th) ST.				148.23 148.25 Fo.02	148.25	
5+00			148.40 148.39 Co.01	148.27 148.37 Fo.10		
4+75			148.56 148.72 Fo.16	148.65 148.72 Fo.07		
4+50			148.97 149.16 Fo.19	148.94 149.16 Fo.22		
4+36.14 =E.C			149.93 149.90 Co.03	149.22 149.42 Fo.20		

44' 4" ST

MKT to F ST
(= 90° L to 44' 4")

STA:	P.L.	CB	E	CB	P.L.	STA:	P.L.	CB	E	CB	P.L.
						#2		145.51 145.04 Co. 97		146.37 145.64 Co. 73	
1+75		143.16 143.10 Co. 06		143.51 143.10 Co. 41		#3		145.20 144.30 Co. 90		146.30 145.72 Co. 58	
1+50		142.68 142.66 Co. 02		143.17 142.66 Co. 51		CB ELS (NW'ly) "G" ST.		144.75 143.98 Co. 77		146.51 146.00 Co. 51	NE'ly "G" ST
1+25		142.17 142.39 Fo. 22		142.71 142.39 Co. 32		2+29.77 = mid-pt N'ly & S'ly X-GUTT (-ELY only)					144.77 E 144.49 - GUTT. Co. 28 FL
1+00		142.09 142.12 Fo. 03		142.16 142.12 Co. 04		CB, ELS "G" ST.		143.80 143.94 Fo. 14		145.78 146.00 Fo. 22	
0+75		141.38 141.85 Fo. 47		141.65 141.85 Fo. 25		#3		143.85 143.94 Fo. 09		145.10 145.33 Fo. 23	
0+50		141.40 141.58 Fo. 18		141.78 141.58 Co. 20		#2		143.60 143.95 Fo. 35		144.42 144.51 Fo. 09	
0+25		141.14 141.30 Fo. 16		141.64 141.38 Co. 26		#1		143.67 143.81 Fo. 14		144.14 143.90 Co. 24	
(MKT EXIST) 0+16 = Beg CB'S (TYPE "G")						1+89.77 = CB 8'S (SW'ly)		143.43 143.46 Fo. 03		143.78 143.46 Co. 27	(SE'dy)
[0+00 = Pt. 40' N'ly MKT ST]											
B.M.				141.05 = NERP 44' 4" MKT							

44th

32

LT				RT				LT				RT			
STA.	P.L	CB	E	CB	P.L	STA	P.L	CB	E	CB	P.L	STA	P.L	CB	E
						6+00		145.89 146.10 Fo. 21		145.85 146.10 Fo. 25					
4+00		148.56 148.75 Fo. 19		148.93 148.75 Co. 18		5+74.65 ST.E.C		145.82 145.82 grade		145.86 145.82 Co. 04					
3+75		148.39 148.85 Fo. 46		148.85 148.85 Grade		5+50		145.92 145.73 Co. 19		145.90 145.75 Co. 15					
3+50		148.26 148.67 Fo. 41		148.71 148.67 Co. 04		5+41.52 (Scoop 21) X-GUTT INLET-4		145.67		145.94 145.73 Co. 21					
3+25		147.93 148.25 Fo. 32		148.45 148.30 Co. 15		5+25		146.17 146.00 Co. 17		146.28 146.00 Co. 28					
3+00		147.50 147.60 Fo. 10		147.96 147.60 Co. 36		5+00		146.17 146.65 Fo. 48		146.53 146.65 Fo. 12					
2+75		146.64 146.70 Fo. 06		147.09 146.65 Co. 44		4+75		147.08 147.20 Fo. 12		147.20 147.20 Grade					
						4+50		147.74 147.87 Fo. 13		147.44 147.87 Fo. 43					
CB BC'S 2+69.77 (NW 4)		146.40 146.52 Fo. 12		146.81 146.52 Co. 29	NE 1/4	4+33.88		148.13 148.20 Fo. 07		148.26 148.24 Co. 02					
#1		145.88 145.83 Co. 05		146.40 145.88 Co. 52		4+16.77 ST.B.C		148.35 148.55 Fo. 20		148.62 148.55 Co. 07					

444L (Cont
(to "F")

33

STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
(= 5+26.14 "F" ST)				148.04							
7+14.73				147.95							
				CO.09							
7+00 RT				147.70							
only				147.70							
				grade							
6+75 RT				147.42							
only				147.27							
				CO.15							
CB											
EC 7+32.29		147.15									
SW 6/4		147.05									
(44' 14" w 6/4)		CO.10									
#3		147.07									
		147.15									
		FO.08									
#2		147.05									
		147.10									
		FO.05									
#1		146.93									
		147.05									
		FO.12									
6+49.73		146.75		146.79							
= SW 6/4 CB		146.80		146.84							
(6.90' LT 44' 14")		FO.05		FO.05							
6+25		146.54		146.45							
		146.40		146.40							
		CO.14		CO.05							

"G" ST ÷ 45th W'ly
to CUL-DE-SAC

(Const. +0.50)

3+

LT.				RT		RT (N'ly)					
STA	P.L.	CB	E	CB	P.L.	STA	P.L.	CB	E	CB	P.L.
2+00	157.44	157.44 157.44 grade		157.67 157.44 Co. 23	157.44	4+25	152.72	152.90 152.72 Co. 18		153.00 152.72 Co. 28	152.72
1+75	157.97	157.83 157.97 Fo. 14		157.99 157.97 Co. 02	157.97	4+00	153.24	153.37 153.24 Co. 13		153.31 153.24 Co. 07	153.24
1+50	158.49	158.53 158.49 Co. 04		158.47 158.49 Fo. 02	158.49	3+75	153.77	153.86 153.77 Co. 09		154.20 153.97 Co. 43	153.77
1+25	159.02	159.07 159.02 Co. 05		159.39 159.02 Co. 37	159.02	3+50	154.29	154.38 154.29 Co. 09		154.92 154.29 Co. 63	154.29
1+00	159.54	159.64 159.54 Co. 10		160.36 159.54 Co. 82	159.54	3+25	154.82	154.47 154.82 Fo. 35		155.53 154.82 Co. 71	154.82
0+75	160.07	160.02 160.07 Fo. 05		160.72 160.07 Co. 65	160.07	3+00	155.34	155.50 155.34 Co. 16		155.91 155.34 Co. 57	155.34
0+50	160.59	160.38 160.59 Fo. 21		160.79 160.59 Co. 20	160.79 160.59 Co. 20	2+75	155.87	156.01 155.87 Co. 17		156.43 155.87 Co. 56	155.87
0+25	161.12	160.98 161.12 Fo. 14		161.27 161.12 Co. 15	161.12	2+50	156.39	156.53 156.39 Co. 14		157.12 156.39 Co. 73	156.39
(see Pg 3) 0+16 = CB E.C. "G" (at 45 th)		161.10 161.31 Fo. 21		161.47 161.31 Co. 16		2+25	156.92	157.03 156.92 Co. 11		157.46 156.92 Co. 54	156.92

BM (Dir. Elev. Rod.)

158.85 = NWB.P 45th
4 MKT

"G" CUI-DE-SAC
ST. W/L of 457h

36

LT
CB

2

RT (N.L.)
CB

#3-mid-
PT.

138.68

2 138.93

137.98
138.93
Fo. 95

139.00

138.24
139.00
Fa. 76

1

139.58
139.42
Fo. 84

139.53

138.54
139.53
Fo. 99

P.R.C

139.10
140.09
Fo. 99

138.62
140.14
F 1.52

139.85
140.14
F 1.29

Knock
out

(note: STA'S Backed-in)

TREMONT:

44th to N'ELY

STA	P.L	LT. CB	E	RT. (N'ELY) P.L
(Pots see p. 71)				
0-67=CB ELS	155.00			155.68 155.00 Co.68
0-75	155.34 155.22 Co.12			155.60 155.22 Co.38
0-100	155.93 155.96 Fo.03			156.41 155.94 Co.97
0-125	156.33 156.48 Fo.15			156.66 156.50 Co.16
0-150	156.54 156.53 Co.01			156.87 156.53 Co.34
0-175	156.10 156.30 Fo.20			156.67 156.30 Co.37
0-188.10=CB BC'S	155.97 156.20 Fo.23			156.41 156.20 Co.21
0-75				
P.R.C Ann. (3 inside CB Fe.) ELS	154.84 155.30 Fo.16	154.84 155.40 Fo.56		154.88 155.83 Fo.95

B.M

141.05 = NEBP 44th T.M.K.T

CUL-De SAC (N'ELY Tremont)

STA	P.L	CB	E	CB	P.L
(Head)					
# 1	153.77 155.04 F1.29				154.92 155.50 Fo.58
5' BK					
(K-04)					
# 2	154.13 155.15 F1.02	154.08 155.15 F1.07			155.12 155.38 Fo.26
5' BK					
#3 = mid-pt.				154.18 155.27 F1.09	
5' BK					

(see p. 28 for in/pt)

+ 0.50

TREMONT - 44 1/2
SW'y to D-END

LT.

RT.

STA	LT		CB	E	CB	RT (NE 1/4)		STA	P.L	CB	E	CB	P.L
	P.L					P.L							
2+00	147.67					148.36		4+50	141.73				141.75
	147.65					147.71			142.29				142.34
	C0.02					C0.65			F0.56				F0.59
1+75	147.80					148.30		4+25	142.45				142.42
	148.21					148.21			142.90				142.90
	F0.41					C0.09			F0.45				F0.48
1+50	148.83					149.48		4+00	143.09				143.02
	148.73					148.77			143.61				143.56
	C0.10					C0.71			F0.52				F0.54
1+25	149.40					150.06		3+75	K.O'd 144.10	143.89		144.57	K.O'd 145.00
	149.38					149.38			144.12	144.12		144.10	144.10
	C0.02					C0.68			F0.02	F0.23		C0.47	C0.90
1+00	150.15					150.64		3+50	144.74				145.34
	150.09					150.06			144.50				144.55
	C0.06					C0.58			C0.24				C0.79
0+75	150.25					150.94		3+25	144.63				145.13
	150.80					150.85			145.10				145.15
	F0.55					C0.09			F0.47				grade
0+50	151.30					151.94		3+00	145.78				146.22
	151.50					151.72			145.55				145.60
	F0.20					C0.22			C0.23				C0.62
0+25	152.21					152.80		2+75	146.18				146.70
	152.23					152.33			146.09				146.09
	F0.02					C0.47			C0.09				C0.61
0+15 = CB	152.48					153.02		2+50	146.17				146.75
EC'S	152.51					152.51			146.60				146.65
(See pg 41)	F0.03					C0.51			F0.43				C0.10
T.B.M @ P.K 44 1/2 TREMONT = 153.465								2+25	147.64				148.13
									147.15				147.15
									C0.49				C0.98

44th ST $\frac{1}{2}$ \angle (At "F")

(CONST = +0.50)

40

to HILLTOP

STA	LT		E	RT (NEly)		STA	LT		E	RT (NEly)	
	P.L	CB		CB	P.L		P.L	CB		CB	P.L
8+75	145.92 146.24 Fo.32			146.42 146.24 Co.18		#2	152.59 152.92 Fo.33			154.23 153.62 Co.61	
8+60	145.59 146.04 Fo.45			146.10 146.04 Co.06		#1	152.59 152.94 Fo.15			153.88 153.07 Co.81	
8+50	145.62 145.96 Fo.34			145.96						153.02 152.38 Co.64 (Sely BC)	
8+42 = E INLET + X-GUT (see Pg 27)	145.89		145.36 145.32 FL Co.04 X-GUT	146.10 145.89 Co.21		7+77.80 CB BC RT	152.30 152.31 Fo.01				
8+25	145.20 146.07 Fo.87			146.13 146.07 Co.06		7+76.8 CB BC LT (swly BC)					
8+00	146.23 146.34 Fo.11			146.40 146.34 Co.06		7+75	151.71 151.23 Co.48			152.58 151.23 Co.35	
7+75	146.65 146.60 Co.05			147.15 146.60 Co.5.5		7+50	150.29 149.95 Co.34			150.73 149.93 Co.80	
7+50	147.15 146.86 Co.29			147.53 146.86 Co.67		7+25	148.76 148.48 Co.28			149.26 148.48 Co.78	
7+32.23 (see Pg 33 & Pg 30)	147.15 147.05 Co.10			147.67 147.05 Co.62		7+00	147.03 147.05 Fo.02			147.55 147.12 Co.43	

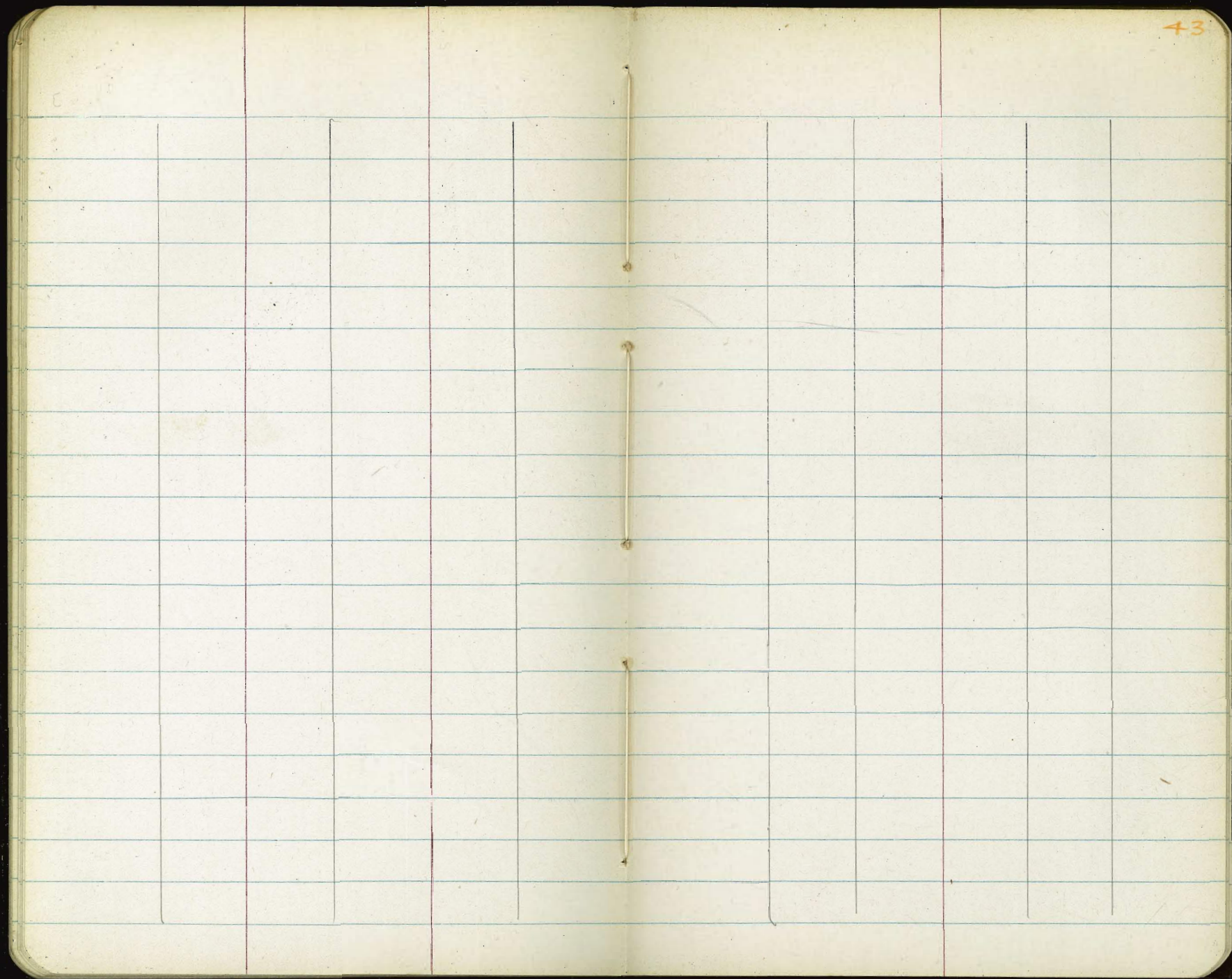
44th (L NE 1/4) to Hill Top

41

44th (L NE 1/4) to Hill Top						RT. (NE 1/4)					
STA.	P.L.	CB	E	CB	P.L.	STA.	P.L.	CB	E	CB	P.L.
# 1	154.27 154.31 Fo.04				155.43 154.62 Co.81	12+25	159.23 159.54 Fo.31				160.58 159.46 C1.12
# 2	153.76 153.70 Co.06				155.33 154.54 Co.79	12+00	158.78 158.62 Co.16				159.84 158.66 C1.18
# 3	153.48 153.21 Co.27				155.30 154.62 Co.68	11+76.40	157.93 157.89 Co.04				159.30 157.96 C1.34
CBFC'S (TREMONT)	153.02 152.51 Co.51				155.68 155.00 Co.68	ST. B.C 11+50	157.01 157.10 Fo.09				158.36 157.16 C1.20
						11+25	156.07 156.36 Fo.29				156.55 156.40 Co.15
10+37.80 = TREMONT X-GUTH - RT.					153.55 153.57 FL Fo.02 ^{GUTH}	11+00	155.30 155.62 Fo.32				156.31 155.64 Co.67
CB E.C'S (on TREMONT)	152.48 152.51 Fo.03				155.17 155.00 Co.17	10+78.8	154.61 155.00 Fo.39				
# 3 (chk on mt) 5' BK	152.55 152.91 Fo.36				154.53 154.29 Co.24	10+77.8	CB BC RT (NE 1/4 B.C)				155.69 154.97 Co.72

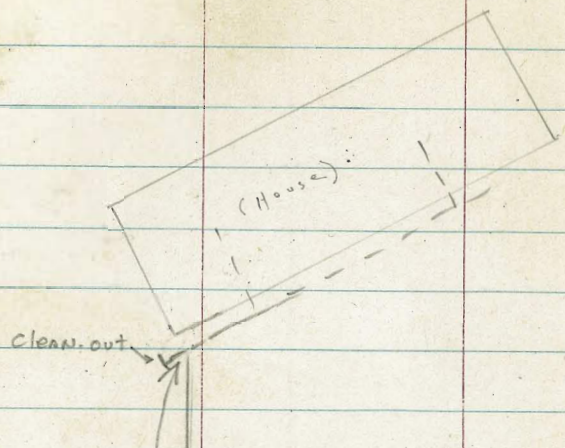
4476 ÷ L (AT "Fst") to Hilltop

14+25	168.45 168.33 Co.12	169.12 168.37 Co.75			
1400	167.17 167.23 Fo.06	167.69 167.24 Co.45			
13+75	165.95 166.13 Fo.18	166.70 166.10 Co.60	CB EIC (Hilltop)	169.75 169.44 Co.31	172.17 172.12 Co.05
13+50	164.93 165.02 Fo.09	165.77 164.97 Co.80	#4	169.87 170.01 Fo.14	171.67 171.70 Fo.03
13+40.43 = E.C	164.60 164.60 grade	165.50 164.54 Co.96	#3	169.81 170.06 Fo.25	171.31 171.25 Co.06
13+25	163.72 163.85 Fo.13	164.76 163.85 Co.91	#2	169.72 170.00 Fo.28	170.82 170.50 Co.32
13+00	162.34 162.70 Fo.36	163.46 162.70 Co.76	#1	169.58 169.69 Fo.11	170.32 169.80 Co.52
12+75	161.81 161.60 Co.21	162.64 161.60 Co.104		169.32 169.22 Co.10	170.11 169.28 Co.83
12+50	160.55 160.59 Fo.04	160.67 160.59 Co.08	14+45.43 = CB B's		



Sew LATS: Chollas #2

LOT 136



Clean-out

(House)

28 grade

50'

25'

25'

138.97
131.46 = F.L.
C 7.01

(Stabs 5 NEly)

EXIST.

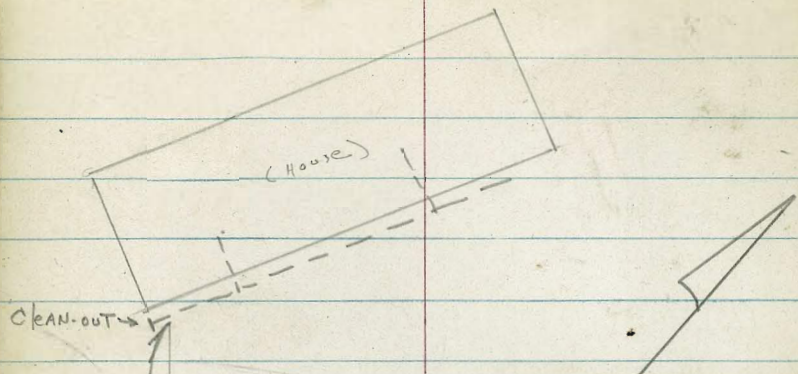
138.18
I.E. = 130.66
C 7.52

MAIN 130' to M.H.

Note! 0.30' rise allowed at invert elev at MAIN for LAT connection

LOT 135

47



Clean-out

(House)

Future
CB elev =
139.08 ±

139.60
134.88 = F.L.
C 4.72

139.51
134.57 = F.L.
C 4.94

28 grade

90'

30'

30'

140.15
I.E. = 133.07
C 7.08

72' to m.H.

CLARK
GARBER
ANDERSON
4-22-60
W.O. 21859

E.S.M.T SEWER
Lot 18 R^o MISSION SAN DIEGO
ENCANTO (W^{ly} OF 60th)

Ref: DWG'S: 7472-D + 6328-D, 6329-D
7303-D + 6317-D
[CITY notes K, L, 21-22; W.O. 32767]
CLARK
T.B.M. 202.37 = 2X2 (25' S^{ly} R.P.)
E 60th Lth & E.S.M.T

48

2+55		263.23 248.51 C 14.72
2+15		262.09 247.36 C 14.73
1+75		259.50 246.20 C 13.30
(40')		
1+35		258.40 245.05 C 13.35
(info. 51)		
0+98.49 = M.H. Stubs 8' 10" + 16' RT on split.	#5	252.34 244.00 = F.L. C 8.34
0+65.66	4579	251.61 242.50 C 9.11
0+32.83		250.92 241.00 C 9.92
Bag Sewer: 0+00 = Plug-end = Pt. 381.23' W ^{ly} OF W.L. 60th ON City-County line = (11+06.86 E.S.M.T-LINE) (N ^{ly} From RADIO DR.)		249.69 239.50 = F.L. C 10.19
B.M. = S.E. BR Broadway & 60th = 202.13		

5+60		265.00 258.05 C 6.95
5+20		266.75 256.65 C 10.10
(40')		
4+80		268.47 255.25 C 13.22
(356)		
4+44.40 = M.H. stubs 8' + 16' RT on split	#6	267.64 254.00 C 13.64
(29.4')		
4+15.00		266.23 253.15 C 13.08
3+75.00		265.10 251.99 C 13.11
3+35.00		265.05 250.82 C 14.23
2+95		264.25 249.67 C 14.58
T.B.M. 315.95 = 2X2 E 60th & E BURIAN (10+84.36 60th)		

$$7+62.21 \left\{ \begin{array}{l} = (19+36.35 \text{ DWG: } 7303-D) \\ = \text{w.l. 604h} \\ = \text{END EASEMENT Sew} \\ \text{plug-end.} \end{array} \right.$$

279.26
 265.15 = F.L.
 C 14.11

(42.24)

7+20

277.09
 263.67
 C 13.42

6+80

17.8

274.50
 262.26
 C 12.24

6+40

5 stubs

272.66
 260.86
 C 11.80

6+00

271.30
 259.46
 C 11.84

CLARK
GARBER
MOORE
ABRENNIA
4-14-59
W.O. 42505

Colusa WATER-MAIN
MILDRED to LINDA VISTA RD.

STA.	Elev's	STA.	Elev's
1+47.5	110.75 107.7 C 3.05		
1+00	106.67 103.3 C 3.37		
0+50	102.52 98.7 C 3.82		
0+20	100.01 95.50 C 4.51		
0+00 = N.L. MILDRED	98.71 94.30 C 4.41		
0-25 = S. MILDRED	97.33 93.30 C 4.03	1+92.85 = Edge Pav L.V. Road	113.44 108.7 C 4.74
0-50 = S.L. MILDRED	96.12 91.80 C 4.32	1+72.5	112.25 108.8 C 3.45
[0+00 = N.L. MILDRED]		1+62.5	111.63 108.6 C 3.03
T.B.M	100.72 = CHD Con. Ldg to Con Stairs # 5662 MIL DRED (upstairs)		

(stubs 5' (w/2) S)

Meet EXIST L.V. Road main (10')

5-13-60

W.O. 20034 SEW:

C/ARK
GARBER
ANDERSON

47th ST, N/ly IMPERIAL

REF DWG'S: NO DWG'S -
- Designed in Field -
Approved by COBURN

51

grade set on
Prop-pipe
2'±

3+34 = W. LINE 47th
= END SEW.

104.17
98.55
C 5.62

2+94 = 90' RT.
NAILS 5.80' & 10.0' RT
NOT ON SPLIT.

103.66
97.75
C 5.91

2+80

103.11
97.27
C 5.84

0+80

93.41
86.91
C 6.50

0.00
0.00
0.00

2+40

101.20
95.95
C 5.25

0+40

90.17
83.71
C 6.46

Note: 8" CON. PAF
005-100020
AC. CON. PAF
47th ST

0.00
0.00
0.00

2+00 = F.V.C

99.41
94.63
C 4.78

0+00 = 90' LT.

86.51
80.51
C 6.00

NAILS 7.10' & 18.44' RT
ON SPLIT OF X.

1+80

98.70
93.86
C 4.84

(not exposed)

0-26.7 ±

Meet
74.85 = F.L. elev

1+60
= mid-pt vic

98.01
92.84
C 5.17

1+40

97.46
91.59
C 5.87

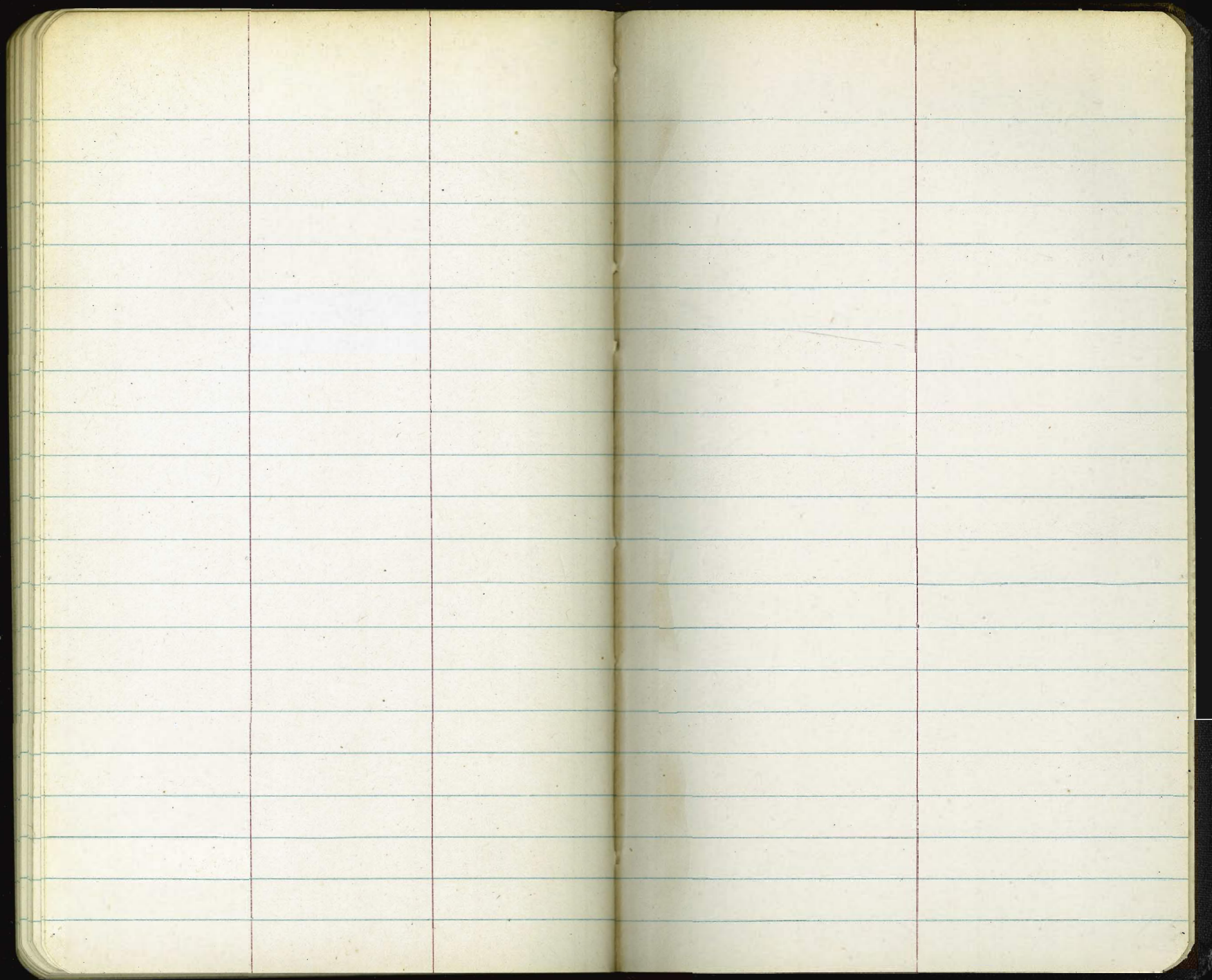
0- = EXIST. D.E (DWG:
2154-D)

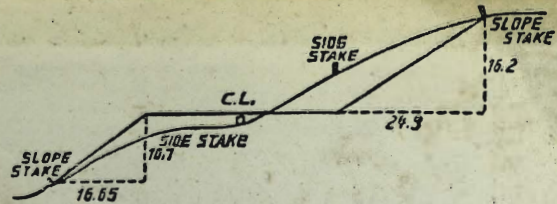
B.M. DIR. Elev. Rod:

112.17 = S.E. B. P
47th & IMPERIAL.

52

74





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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