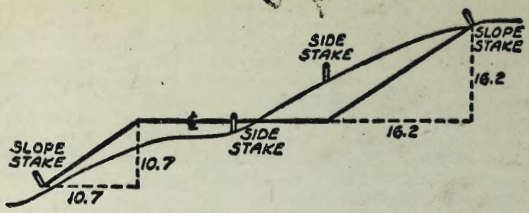


G-402



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

0	
1	
2	
3	
4	
5	
6	
7	
8	
9	
10	1
11	1
12	1
13	1
14	1
15	1
16	1
17	1
18	1
19	1
20	1
21	1
22	1
23	1
24	1
25	1
26	1
27	1
28	1
29	1
30	1
31	1
32	1
33	1
34	1
35	1
36	1
37	1
38	1
39	1
40	4
41	4
42	4
43	4
44	4
45	4
46	4
47	4
48	4
49	4
50	4

Dist
ground
column
side st.
side st.
cut or
If it do

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1% to 1.
If ground is nearly level, the cut or fill stake

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find tangent and distance for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Degree of curve which gives 1 may be found
by dividing tangent (of extent), opposite 1 by
given tangent (of extent).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the tangent.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.29	1.42	1.54
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

JOB:

Pg.

ENCANTO SEWERS:

CANYON-LINE	1
MALLARD (SPRINGFIELD-E'LY)	31
" (CANYON-W'LY)	8
" (CANYON-E'LY)	9
" (SPRINGFIELD E'LY)	11 (COR. RT.)
EASEMENT: LOTS 182-183-184 DEL NORTE ADD.	12
EASEMENT: LOTS 18+19 DEL NORTE ADD.	13
BLUEBIRD: { MALLARD to MULBERRY }	14
EASEMENT: { M.H. 18 (Blue Bird) to mulberry LOTS 145-146 M.H. 26 DEL NORTE }	16
EASEMENT: { M.H. 21 MULBERRY to SPRINGFIELD M.H. 90 }	17
MULBERRY: { M.H. 25 (CANYON-LINE) E'LY }	19
" M.H. 25 to W'LY	20

INDEX: Sewer

		Pg.
MULBERRY:	M.H.#20 (12+73.63 ESMT ELY to M.H.#23	21
"	M.H.#20 - W'ly to D.END	21
69th ST:	KLAUBER to MAILLARD	23

CULVERTS:

15+39.29	MAILLARD ^{10' w'ly} CANYON-LINE	25
7+91.41	BLUEBIRD	26
7+95	MULBERRY	27
14+59	MULBERRY	28

(CONT.)

SEWER: SPRINGFIELD	M.H.#40 W'ly	29
	M.H.#40 to ELY	30

SPRINGFIELD	M.H.#45 to ELY	32
	M.H.#45 to W'ly	34

		Pg
PARADISE:	{ M.H.#47 SPRINGFIELD - N'ly to M.H.#48 }	35 (RT)
"	MAILLARD to TOOLEY	36
SWAN:	MAILLARD to TOOLEY	38
ORIOLE:	MAILLARD to TOOLEY	41

C/ARK
GARBER
MOORE
ABRENIHA
6-12-59
W.O. 32767

ENCANTO-SEWER:
CANYON-LINE

FED: S'ly to mallard,
SIVE BRD. + ESSENTS to
D. END S'ly mallard

Ref: / City notes: L-20-21-22
K-20-21-22
DWG: 5394-D - 5413-D (incl.)

STA:	Elev:	STA.	Elev.
			302.20
		4+90	295.67
			C 6.53
			300.69
		4+55	294.34
			C 6.35
			299.35
		4+20 = P.O.T. = M.H. #52	293.00 = F.L.
		(stubs 6' + 12' RT)	C 6.35
			294.27
			288.13
			C 6.14
			293.93
		3+80	292.52
			C 5.47
			292.88
		3+45	292.09
			C 8.72
			291.93
		3+10	291.67
			C 11.05
			301.45
		2+75	291.25
			C 10.20
			290.8
		2+40	299.73
			290.83
			C 8.70
		2+05	297.70
			290.41
			C 7.29
			294.98 = Ch. to W'ly
			end S'ly hd wall FED. + McARTHUR DR.

= L LT 20° 44.9

EA 1+70.74 Ad
1+74.29 BK
(stubs 6.10' + 12.2' RT split)

= M.H. #51

(3 L 9 stubs
6' RT E)

0+63.99 (- Beg. CONT. WORK
- END City Forces work)

7.99%

0+100 = Pt. INT. EXIST FED. - MAIN
230.7' E'ly OF EXIST M.H.
#53
(stubs 8' + 16' LT
ON Line MAIN)

T.B.M

(DIA. Elev. RODS)

3.8236
↓

1.2049
↓

CANYON-LINE (CONT.)

STA.	Elev.	STA.	Elev.
7+70	311.42 305.59 C 5.83	10+65	320.59 314.90 C 5.69
7+35	310.33 304.53 C 5.80	10+30.57 = M.A. #54 (stubs 6.33' + 12.66' RT ON SPLIT)	319.60 313.50 = F.L. C 6.10
7+00	309.41 303.47 C 5.94	10+15	319.13 313.03 C 6.10
6+68.51 = #M.A. #53 (stubs 6' + 12' RT ON SPLIT)	308.96 302.50 = F. line C 6.46	9+80	317.53 311.97 C 5.56
6+30	307.37 301.03 C 6.34	9+45	316.86 310.90 C 5.96
5+95	306.03 299.68 C 6.35	9+10	316.39 309.84 C 6.55
5+60	304.51 298.34 C 6.17	8+75	315.36 308.78 C 6.58
5+25	303.38 297.01 C 6.37	8+40	313.94 307.72 C 6.22
		8+05	313.03 306.65 C 6.38

309.86
↓

= L.L.T. 3° 13.5'

3.8236
↓

3.808
↓

L.R.T. = 37° 11.35'

3.0386
↓

CANYON-LINE (CONT.)

STA.	ELEV.	STA.	Elev.
13+30	329.57 321.87 C 7.70	15+80	334.49 328.23 C 6.26
12+95	328.75 321.26 C 7.49	15+45	333.18 326.62 C 6.56
12+60	327.45 320.65 C 6.80	P.O.T 15+10 = <u>M.H. #55</u> (Stubs 6' x 12' RT)	332.69 325.00 C 7.69
12+25 (12+20 end. Con. BK-Fill)	326.91 320.04 C 6.87		
11+90 = 11+81.59 Ahead } EQ: 11+81.90 BK	326.34 319.43 C 6.91	15+05 (not set)	
∠ RT = 11° 39.4'			
11+65.29 = M.H. #34 (= 15+49.35) } EMALLARD } (stubs 6.034' } (12.04' RT } -split	324.8 348.8 = TPANH F 24.0 324.77 319.00 = F.L. C 5.77	14+70	331.97 324.31 C 7.66
11+35	323.40 317.76 C 5.64	14+35	331.25 323.70 C 7.55
11+00 = 1309 Con BACK-Fill	322.10 316.33 C 5.77	14+00	330.69 323.09 C 7.60
		13+65	330.36 322.48 C 7.88

1.742

4.6266

1.742

4.080

CHK: 345.70 = 345.71 = 2x2 E Bluebird
C Canyon-Line

Set T.B.M. (Tie) (ST. STA.)
ON 2x2 = 7460.71 Bluebird (MH #17) 4
40' RT (W'ly) & Bluebird: Elev = 351.65

CANYON-LINE (CONT.)

STA.	Elev's:	STA.	Elev's:
18+50	346.29 340.01 C 6.28	21+57.05 = M.H. #56 (= 0+100 ESMT, N'ly) (Stubs 6.01' & 12.02' RT on split canyon-line)	355.60 349.80 = F.L. C 6.80 ESMT LINE to N'ly
	346.89 340.00 = F.L. C 6.89 Bluebird N'ly	21+30	355.42 347.57 C 7.85
∠: LT: 63° 17.5'	346.9 350.8 = T.p.m.H F 3.9	20+95	353.72 346.62 C 7.10
18+12.66 = M.H. #17 (= 7460.71 Bluebird) (ST. STA.) (Stubs 7' & 14' RT M.H.# AT 90° to Bluebird)	346.89 339.00 = F.L. C 7.89 CANYON LINE to Bluebird S'ly	20+60	354.06 345.68 C 8.38
17+90	347.37 337.94 C 9.43	20+25	350.61 344.73 C 5.88
17+55 = end con. BK-Fill	345.57 336.32 C 9.25	19+90	348.82 343.79 C 5.03
17+20	345.00 334.70 C 10.30	19+55	347.68 342.84 C 4.84
(17+11 809 Con. BK-Fill)	344.09 333.08 C 11.01	19+20	346.27 341.90 C 4.37
16+85	341.24 331.46 C 9.78	18+85	346.24 340.95 C 5.29
16+50	337.67 329.85 C 7.82		

2.700
↓

4.6260
↓

2.70
↓

CANYON-LINE (CONT.)

STA.		Elev.	STA.	Elev.
STA. [stubs 6.04 + 12.08 RT-SPLIT]				
$\angle LT = 18^\circ 22' 01''$			27+15	377.98 371.43 C 6.55
= 23+84.64 AHA) = M.H. #25		364.71 356.80=FL.		
23+84.44 BK) EQ:		364.71 356.30=FL.	26+80 = M.H. #57	376.12 369.50=FL.
(= 8+27.37 MULBERRY)		C 7.91 IN C 8.41 OUT	P.O.T	C 6.62
			(stubs 6' + 12' RT)	
23+60		363.95 355.44 C 8.51	26+65	375.45 368.85 C 6.60
23+25		361.90 354.20 C 7.70	26+30	373.86 367.35 C 6.51
22+90 TR		360.32 352.97 C 7.35	25+95	372.15 365.84 C 6.31
22+55		358.63 351.74 C 6.89	25+60	370.30 364.34 C 5.96
22+20	3.52 S	357.44 350.51 C 6.93	25+25	368.97 362.83 C 6.14
21+85		356.51 349.28 C 7.23	24+90	367.78 361.33 C 6.45
21+50			24+55	366.33 359.82 C 6.51
			24+20	365.36 358.32 C 7.04

CANYON-LINE (CONT.)

STA.		Elev.	STA.	Elev.
30+00	46.52	393.05 386.80 C 6.25	32+70	413.39 405.20 C 8.19
			32+40	411.75 402.66 C 9.09
EQ: 29+66.45 BK (stubs 6.14' + 15' RT.)		390.90 385.30 C 5.60	32+10	409.92 400.11 C 9.81
29+60		390.54 384.94 C 5.60	31+80	408.12 397.56 C 10.56
29+25		389.15 383.01 C 6.14	31+50	406.24 395.02 C 11.22
28+90		387.35 381.08 C 6.27	31+16.40 = M.H. #59 (0+00 ESMT 5' L to SPRINGFIELD = 7+32.80) - See Pg 13 -	403.44 FL 392.67 ESMT C 10.77 5' L
28+55	5.5168	385.15 379.15 C 6.00	31+05	403.44 392.17 = FL C 11.27 CANYON
28+20		383.72 377.22 C 6.50		403.02 391.64 C 11.38
27+85		381.70 375.29 C 6.41	30+70	399.96 390.03 C 9.93
27+50		379.71 373.36 C 6.35	30+35	396.64 388.41 C 8.23

CANYON-LINE (cont.)

STA.	Elev.
33+93.20	429.62 420.46 C 9.16
33+70 = E.V.C.	422.85 415.92 C 6.93
33+60	420.57 414.18 C 6.39
33+50	418.90 412.66 C 6.24
33+40	417.44 411.37 C 6.07
33+30 = B.V.C.	416.66 410.30 C 6.36
33+00	414.77 407.75 C 7.02

19.582

8.492

STA. Elev.
CHK: 460.08 = 460.08 = CON MAN
(ST. STA = 10+06.55 MAILLARD)
C.H.S

Set T.B.M. = ch. □ Near (6' N 2 1/2)
SE'ly Corn. Con slab
@ #6665 MAILLARD. = Elev. 451.95
At approx STA (ST.) 10+30 on South.

Set T.B.M. on chx ON CON Ldg (W'ly side)
House @ #6703 MAILLARD - chx tie to
CITY HUB & MULBERRY + S. Line
MAILLARD: 71' ELYE
Elev = 440.65

= end Canyon-Line
34+16.40 = M.H #60
[Stubs 6' + 12" LT]
432.68
+ 2.5.00 = FL
C 7.68 M.H

MAILLARD (CANYON-LINE 11+65.29)
(to W'ly end)

STA		Elev's	
1+19.35	344.03 342.88 C 1.15	344.16 342.88 C 1.28	Advised by W.A. Dept.
1+09.35	342.36 341.82 C 0.54	343.19 341.82 C 1.37	
0+99.35	341.65 340.46 C 1.19	341.88 340.46 C 1.42	
0+89.35		340.48 338.80 C 1.68	
0+79.35 = B.V.C		338.79 336.85 C 1.94	
(0+63.35 = end CONC. BK-FILL)			
0+52.90		332.71 330.90 C 1.81	
0+26.45	326.38 324.95 C 1.43	326.63 324.95 C 1.68	Fixed by Gent.
0+00 MAILLARD = 11+65.29 CANYON = M.H # 34 (See Pg. 3)		319.00	

22.568

Set T.B.M. = 356.50 = Ch. II NW Corn Con. 8
LDG. House (SE Corn
Bluebird + MAILLARD)
#6509 Bluebird

STA.		Elev's	
3+25.66 = end (-plug)		359.10 354.00 = F.L. C 5.10	
2+96.76		356.82 351.26 C 5.56	9.468
2+67.88		355.05 348.53 C 6.52	
2+39 = M.H # 15 stubs 6" RT+LT		353.23 345.80 = F.L. C 7.43	
2+05.78		351.54 345.23 C 6.31	1.708
1+72.56		349.32 344.67 C 4.65	
1+39.35 = E.V.C		346.42 344.11 C 2.31	
1+29.35		345.20 343.64 C 1.56	

MAILLARD

(CANYON 11+65.29
to ELY)

Set T.B.M

= 2x2 tie 35' Lt. (ELY) & Akedo 9
& ST. STA = 1+60.83
Elev = 412.28

STA.	Elev.
2+20	362.00 354.05 C 7.95
1+85	360.63 352.09 C 8.54
1+50	359.20 350.13 C 9.07
1+15	356.59 348.17 C 8.42
P.O.T	
0+90.65 = M.H # 33	351.89 346.80 C 5.09
0+60.44	343.08 337.52 C 5.56
(0+55.65 = end CONC. BK-FILL)	
0+30.22	333.53 328.26 C 5.27
0+00 = (11+65.29 CANYON) = M.H # 34 (see Pg 3)	319.00

30.678
↓

STA.	Elev.
5+35	398.55 387.79 C 10.76
4+99.25 = M.H # 31 (Stubs 6' + 12' RT)	392.43 385.20 C 7.23
4+65	386.77 380.72 C 6.05
4+30	380.88 376.16 C 4.72
3+95	375.27 371.60 C 3.67
3+60	371.13 367.03 C 4.10
3+25	368.22 362.47 C 5.75
= P.O.T	
2+90.65 = M.H # 32 (5' stubs 6' + 12' RT)	365.72 358.00 C 7.72
2+55	363.52 356.01 C 7.51

72578
↓

13048
↓

MALLARD - CANYON ELY (CONT.)

STA.	Elev.	STA.	Elev.
- P.O.T.			
8+49.25 = M.H. #30 (stubs 6' x 12' RT)	420.42 410.60 C 9.82	10+45	444.63 437.61 C 7.02
8+15 (8+07.64 = chimney LT.)	418.28 408.10 C 10.18	10+09.25 = E.V.C.	441.02 434.91 C 6.11
7+80 (7+57.65 = Chmy LT.)	415.93 405.56 C 10.37	9+99.25	440.00 433.98 C 6.02
7+45	414.12 403.02 C 11.10	9+89.25	439.10 432.88 C 6.22
7+10	412.79 400.48 C 12.31	9+79.25	437.91 431.60 C 6.31
6+75	411.65 397.94 C 13.71	9+69.25 = B.V.C.	436.50 430.14 C 6.36
6+40	409.67 395.40 C 14.27	9+55	434.64 427.83 C 6.81
6+05	406.67 392.86 C 13.81	9+20	429.68 422.12 C 7.56
5+70	403.31 390.32 C 12.99	8+85 (8+59.25 = chimney LT.)	424.46 416.41 C 8.05

7.257%

16.286%

MALLARD (CANYON - ELY - CONT.)

MALLARD (E SPRINGFIELD TO D. END ELY) 11

STA.	elev.	STA.	Elev.
CHK: <u>T.B.M</u>	451.94 = 451.95 =		
	CHA SELY CON. CON Slab 10+30 ± mallard (#6665) on Sly side		
		2+11.12 = M.H #66	450.30
		1+75	450.10
		1+40	449.91
		1+05	449.74
= END ELY SEWER (P.O.T.)			
11+32.64 = M.H #29 (Stub 6' RT Spike 12' RT)	454.31 444.20 C 10.11	0+70	449.56
11+15	452.21 442.87 C 9.34	0+35	449.38
10+80	448.32 440.24 C 8.08	0+00 = M.H #65 E SPRINGFIELD	449.20

EASEMENT ~~7~~ LOTS 182-183-184DEL NORTE ADD:
(M.H #56) 21+57.05 CANYON LINE, ton 24

STA.

Elevs:

2+25 = M.H #56-A	368.97 365.09 = F.L C 3.88
2+10	368.44 364.00 C 4.44
1+75	367.09 361.46 C 5.63
1+40	365.10 358.93 C 6.17
1+05	362.67 356.40 C 6.27
0+70	359.98 353.86 C 6.12
0+35	356.75 351.33 C 5.42
M.H #56 = 0+00 (= 21+57.05 CANYON) LINE	348.80 = F.L ESMT LINE

7.248
(Studs 6.818)

(See Pg 4)

Common-Line

EASEMENT - Lots 18-19

DEL NORTE ADD:

(M.H #59) = 31+16.40 CANYON Line s'ly to
7+32.80 SPRINGFIELD - m.h #40

Set T.B.M = ch. NE 1/4 Cor. Bott Step (conc)

#6715 - s'ly side SPRINGFIELD
Elev = 440.44

STA.	Elevs:
1+70	415.63 409.19 C 64.4
1+35	410.30 404.41 C 589
1+00	405.31 399.64 C 5.67
0+72.80 = EVK	401.14 395.93 C 5.21
0+62.80	399.57 394.82 C 4.75
0+52.80	398.45 393.96 C 4.49
0+42.80	398.38 393.35 C 5.03
0+32.80 = BVC	398.86 393.00 C 5.86
M.H #59 = 0+00 (= 31+16.40 CANYON LINE) (see Pg 6)	392.67 = F.L. ESMT s'ly

STA.

Elevs:

432.24 421.00 = F.L. SPRINGFIELD Ely + Wly C 11.24
432.24 420.50 = ESMT FL C 11.74
432.52 421.00 = F.L. SPRINGFIELD Ely + Wly C 11.52 (K. o'd by S.D. G. + E. Co.)
[Stubs 8.48' + 16.9' in S'ly QUAD] 2+52.80 = M.H #40 (= 7+32.8 SPRINGFIELD)
432.52 420.50 = F.L. ESMT C 12.02
2+40 429.06 418.75 C 10.31
2+05 421.54 413.97 C 7.57

BLUEBIRD - M.H.#15 (MALLARD) S64
to D.END

BLUEBIRD: M.H.#17 (18+12.66) } 14
CANYON-LINE }
NLY to D.END

STA.

ELVS:

1+75.03 = Plug-end

1+40

1+05

0+70

0+35

0+00 = M.H.#15
(E. MALLARD)
= 2+39
(see pg 8)

356.50 T.B.M. Chg. A. Job 6509 Bluebird

2+80

2+45

2+10

1+75

1+40

1+05

0+70

0+35

M.H.#17 - 0+00
(E. ST. STA 7+60.71)
= 18+12.66 CANYON-LINE
see pg 4

353.62
346.32
C7.30

352.82
345.53
C7.29

352.15
344.74
C7.41

351.38
343.95
C7.43

350.95
343.16
C7.79

350.57
342.37
C8.20

349.73
341.58
C8.15

348.16
340.79
C7.37

340.00

E. 5739

E. 2538

BLUEBIRD: M.H. #17 - NLY (CONT.)

BLUEBIRD: M.H. #17

$\int_{18+12.66}$
= (CANYON-LINE) 15

Sly to M.H. #18

STA.	Elevs:
CHK:	356.47 (Conn. Ldg) WALK = 356.50 = ch x 43 LT & BLUEBIRD ST. STA 1+10 (Sly Cann. MALLARD + BLUEBIRD)
5+05.71 = Plug-end	359.86 355.24 = F.L C 4.62
4+85	358.62 354.37 C 4.25
4+50	357.30 352.89 C 4.41
4+15	356.39 351.41 C 4.98
3+80	355.70 349.93 C 5.77
3+45	355.24 348.45 C 6.79
3+10.71 = M.H. #16	354.07 347.00 = F.L C 7.07

352.9. RIM

STA.	Elevs:
	- See Pg 16 - stubs 8.48' + 15' N.W. QUAD = END BLUEBIRD = BQ. ES. MNT SEWER # 18 $\Delta = 90^{\circ} 05' 58''$ RT
	354.84 343.00 F.L C 11.84
	352.32 342.33 C 9.99
	349.51 341.50 C 8.01
	347.21 340.66 C 6.55
	346.69 339.83 C 6.86
	339.00 = F.L
	0+00 = M.H. #17 ST. STA = 7+60.71 = 18+12.66 CANYON-LINE (see Pg 4)

2.788

EASEMENT: M.H #18 BLUEBIRD - SW 1/4 + 5 Ely

LOTS 145-146

STA.

Elev's:

2+35.29 = B.V.C

360.27
354.93
C 5.34

2+00

2.0

360.37
354.21
C 6.16

(stubs 8.48' x 15' on split NW 1/4 quad)

3+68.92 = M.H #20
= 8 MULBERRY - 0+00 Ely
+ W 1/4 MULBERRY
See pg.

374.08 FL
366.53 W 1/4
C 7.55 MULBERRY

374.08
366.03 = FL
C 8.05 E 1/4
mulberry
ESMT
W 1/4

1+70

360.72
353.62
C 7.10

3+34.46

2.5

370.57
362.78
C 7.79

Δ = 90° LT

1+38.90 = M.H #19
(stubs on split 8.48' x 15' RT)
NW Quad

361.96
353.00
C 8.96

3+00

366.97
359.54
C 7.43

1+05

356.80
350.56
C 6.24

2+75.29 = E.V.C

363.36
357.21
C 6.15

0+70

7.20

353.40
348.04
C 5.36

2+65.29

362.38
356.43
C 5.95

0+35

353.75
345.52
C 8.23

2+55.29

361.45
355.78
C 5.67

M.H #18 = 0+00 ESMT
= 1+44 BLUEBIRD
See pg 15

343.00

2+45.29

360.65
355.28
C 5.37

EASEMENT: M.H. 21 (MULBERRY)
 - 5' ELY - LOTS 200-201-5-6
 DEL NORTE ADD: HIGHLAND AVE.
 to M.H. #45 & SPRINGFIELD

STA.	Elev's:
1+55	386.44 380.64 C 5.80
1+25	383.44 376.32 C 7.12
0+95.60 = E.V.C	380.51 372.08 C 8.43
0+85.60	379.36 370.87 C 8.49
0+75.60	378.24 369.89 C 8.35
0+65.60	377.19 369.14 C 8.05
0+55.60 = B.V.C	375.56 368.63 C 6.93
0+27.80	372.38 373.40 367.84 367.84 364.54 365.56
M.H. #21 = 0+00, ESM T NLY (See pp. 21)	367.55 = F.L. WLY MULBERRY 367.05 = F.L. ESM T+ ELY MULBERRY

4.42 1/2

1.30 6 8

STA.	Elev's:
4+15	416.58 395.28 C 21.30
(3+95.6 = Chmny RTW 4)	412.77 394.82 C 17.95
3+80	408.16 394.37 C 13.79
3+45	(3+30.6 Beq Con. BK-Fill)
3+10 (5' RT)	405.67 393.91 C 11.76
2+75	402.06 393.43 C 8.61
2+40.60 = M.H. #49 (Stubs 6' 1/2 RT)	397.86 393.00 = F.L. C 4.86
2+15	394.31 389.30 C 5.01
1+85	390.30 384.96 C 5.34

EASEMENT - M.H #21 - MULBERRY - SLY
to M.H #45 Springfield (CONT)

STA.

elevs.

CHK:

416.71

= 416.77 - Chk

Sly and Tr 3rd
con. step #6620
Springfield - N 1/4
side ST + W 1/4 ESMT

Stubs 8.48 + 15.00 on split
- NW 1/4 Quad -

420.94
422.2 + P -
Rim -
F 1.26

420.94
416.20 = F.L. E 1/4
C 4.74 Springfield

(End Conc. BR-FIN - ESMT)

Drop -
4+95.60 M.H #45

Springfield
= 20+32.80 ST. STA:
See pg

420.94 F.L.
396.83 W 1/4
C 27.11 Spring-
Field

420.94
396.33 F.L.
C 24.61 ESMT

4+85

420.99
396.19
C 24.80

4+50

← 13068

418.27
395.74
C 22.53

MULBERRY = MH #25 (23+84.64)
 (CANYON-LINE)
 to 6Lj - to MH #20

STA.	Elevs:
2+65	390.25 384.19 C 6.06
2+30	386.55 379.53 C 7.02
1+95	382.59 374.87 C 7.72
1+60	378.90 370.21 C 8.69
1+37.37 = MH #26 Stubs 6' 412' RT.	376.92 367.20 = F.L. C 9.72
1+05	372.67 364.75 C 7.92
0+70	369.63 362.10 C 7.53
0+35	365.19 359.45 C 5.74
0+00: MH #25 =(23+84.64 CANYON-LINE) (See p 5)	

Set. T.B.M = 2x2 tie 60' sly & 19
 MULBERRY ON Proj. sly of E
 ALGEDO
 Elev = 372.20

STA.	Elevs:
5+60	428.61 421.16 C 7.45
5+25	425.80 416.97 C 8.83
4+90	421.65 412.78 C 8.87
4+55	417.00 408.59 C 8.41
4+20	412.40 404.40 C 8.00
3+87.37 = MH #27 Stubs 6' 412' RT.	407.67 400.50 = F.L. C 7.17
3+70	405.25 398.17 C 7.08
3+35	399.67 393.51 C 6.16
3+00	394.76 388.85 C 5.91

MULBERRY - M.H. 25 - ELY. (CONT.)

MULBERRY 20
M.H. 25 - to WLY - to M.H. 24

CHK

440.66 = 440.65 = T.B.M.
= Chx Tot. LT of
2x2 HUB & MULBERRY
& S.L. MAILLARD
(See pg 7)

2+72.63 = M.H. #24
Stubs 6' 4 1/2' RT

2+45

2+10

1+75

1+40

1+05

0+70

0+35

0+00 = M.H. #25
= (23+84.64 CAÑON-
LINE)

(See pg 5)

396.62
386.03 = F.L.
C 10.59

394.18
383.06
C 11.12

390.00
379.31
C 10.69

384.79
375.55
C 9.24

379.14
371.80
C 7.34

373.93
368.05
C 5.88

370.53
364.30
C 6.23

368.57
360.55
C 8.02

= and MULBERRY ELY

6+32.09 = M.H. #28
(Stubs 6' 4 1/2' RT)

5+95

435.05
429.80 = F.L.
C 5.25

432.50
425.35
C 7.15

MULBERRY + M.H. #20 = (12+73.63 ESMT)

Ely to M.H. #23

STA.

elevs.

MULBERRY + M.H. #20

Wly to 2-END

21

STA.

elevs.

= end Ely

1+97.89 = M.H. #23

1+75

1+40

1+05

0+70

0+35

0+00 = M.H. #20
= (12+73.63 ESMT)

(See pg 16)

10.268

366.53 = F.L.
Wly
MULBERRY

366.03 F.L.
Ely
MULBERRY
& ESMT

M.H. #20

(See pg. 16)

1+02.11

0+92.11

0+82.11

0+72.11

0+62.11 = B.V.C.

0+51.70 = M.H. #21 = (0+00)
(ESMT Sly to M.H. #40)

0+25.85

375.83
371.12
C 4.71

374.21
369.79
C 4.42

372.64
368.77
C 3.87

371.69
368.05
C 3.64

371.16
367.65
C 3.51

371.00
367.55 = F.L.
C 3.45 Wly
MULBERRY

371.00
367.05 = F.L.
3.95 ESMT
&
Ely MULBERRY

372.17
366.79
C 5.38

366.53 = F.L.
Wly
MULBERRY

MULBERRY = M.H #20 - w'ly (CONT.)

STA:	elev's:
3+35	431.46 421.75 C 9.71
3+01.7 = M.H #22	425.99 415.14 = F.L. C 10.85
2+95	424.51 413.62 C 10.89
2+60	416.74 405.73 C 11.01
2+25	408.23 397.85 C 10.38
1+90	398.88 389.98 C 8.90
1+55	388.88 382.10 C 6.78
1+22.11 = E.V.C	380.26 374.70 C 5.56
1+12.11	377.97 372.76 C 5.21

19.66

23.57

STA:

elev's:
457.77 = 457.77 = ch D
#1949 PARADISE = (SEL)
ON CON. WALK PARADISE & MULBERRY

4+01:70 = D-END - Plug

3+70

elev's:

441.64
435.00 = FL
C 6.64
436.95
428.70
C 8.25

STA:	Elevs:	STA:	Elevs:
2+35	461.23 450.56 C10.67	5+50	462.24 451.82 C10.42
2+00	461.12 450.42 C10.70	5+15	462.13 451.68 C10.45
1+65	460.95 450.28 C10.67	4+80	462.01 451.54 C10.47
1+30	460.49 450.14 C10.35	4+45	461.92 451.40 C10.52
0+95	459.58 450.00 C9.58	4+10	461.83 451.26 C10.57
0+60	458.34 449.86 C8.48	3+77.25 = M.H. #63 NAILS 6' x 12' RT	461.75 451.13 = F.L. C10.62
A = 50° 53' LT			
0+28.10 = M.H. #64 Stubs 6.64' RT (95908) + 8' LT ON SPLIT	455.96 449.73 = F.L. C6.23	3+40	461.66 450.98 C10.68
		3+05	461.54 450.84 C10.70
0+00 = EXIST. END KLAUBER	455.54 449.00 ± (meet) 6.54	2+70	461.39 450.70 C10.69
T.B.M	463.39 = CON. MAN NELY CON. MALLARD + 69 th		

(NAILS 6' RT IN PIV)

0.48

69th = (CONT.)

STA:

8+65

8+30

7+95

7+60

7+27.25 = M.H. #62
(NAILS 6' x 12' RT.)

6+90

6+55

6+20

5+85

Elev's:

463.10
454.71
C 8.39462.96
454.16
C 8.80462.84
453.60
C 9.24462.78
453.05
C 9.73462.69
452.53 = F.L.
C 10.16462.61
452.38
C 10.23462.47
452.24
C 10.23462.35
452.10
C 10.25462.31
451.96
C 10.35

STA:

CHK:

462.24

(= PT. 65' S'ly OF ♀ MAILLARD)

(= end 69th sewer)

10+72.25 = M.H. #61
(NAILS 6' x 12' RT.)

10+40

10+05

9+70

9+35

9+00

(City Notes
Radio-Dri.)

Elev's:

462.25

= 462.16 = L+T &
KLAUBER & 48'±
W'ly & PERINO463.94
458.00 = F.L.
C 5.94463.73
457.49
C 6.24463.62
456.93
C 6.69463.61
456.38
C 7.23463.52
455.82
C 7.70463.28
455.27
C 8.01

CULVERTS ÷

REF
(Dwg. 5397-D)

1513929 MAILARD + CANYON-LINE-SEWER
30" R.P.

CHK: 351.63 = 351.65 = T.B.M P97

STA. ELEV:

1+48 = end culvert stubs 8' RT + 15' LTR	(5 stubs 8' RT & 15' LTR)	327.38	
		325.40 = F.L	
		C 2.98	
1+18.4		326.40	
		324.51	
		C 1.89	
0+88.8		326.30	
		323.62	
		C 2.68	
0+79.65 = E MAILARD (= P.O.C. culvert)		326.49	
	323.35		
	C 3.14		
0+59.2	325.72		
	322.74		
	C 2.98		
0+29.6	323.37		
↑ (on curve)	321.83		
	C 1.52		
↓ 0+00 = NLY edge CANYON-WALL	321.93		
(stubs 8' RT)	320.96 = F.L		
	C 0.97		
[B.C. = 0-00.36] T.B.M	356.50 = T.B.M P98		

CURTAIN 7+91.41 BLUEBIRD

21" R.C.P

REF (DWG 5400-D)

Elevs:

STA.

CHK:

351.65 = 351.65 (see below)

1+16 = Sly edge CURTAIN-WALL
(Stubs 8'+16' RT)

350.76
347.04 = F.L
C 3.72

0+87
(0+64 = E BLUEBIRD)

(Stubs 8' RT (Wig))

349.14
345.88
C 4.26

0+58

346.82
344.72
C 2.10

0+29

346.40
343.56
C 2.84

(Stubs 8'+16' RT)
0+00 = Nly edge
CURTAIN WALL

344.20
342.40 = F.L
C 1.80

T.B.M.

351.65 = T.B.M Pg 4

21" CURTERT - 7+95 MULBERRY
(W'ly of ALCEDO) ref. (Dwg 5400-2)

STA.

Elevs:

CHK:

0+96 = Ely. edge CURTAIN-WALL
(stubs 8' 1/16" RT)

366.58
363.80 = F.L.
C 2.78

0+72

366.20
363.27
C 2.93

(0+49 = E MULBERRY)

0+48

365.43
362.74
C 2.69

0+24

364.85
362.21
C 2.64

0+00 = W'ly edge CURTAIN-WALL
(stubs 8' 1/16" RT)

363.40
361.69 = F.L.
C 1.71

T.B.M

372.20 (Pg 19)

CULVERT ÷ 14+59 MULBERRY

REF: (DWG: 5400-D)

28

STA:

Elev's

CHK: 351.66 = 351.65 = T.B.M pg. 4

0+64 = fc, hd wall

372.50
372.80
F 0.30

0+32

371.41
370.10
C 1.31

0+00 = fc hd wall

367.80
367.40 = F.L.
C 0.40

(stubs 8' RT E)

T.B.M

401.46 = 2x2 60' S'ly E MULBERRY
ON E Proj. OF BLUEBIRD

SPRINGFIELD

M.H #40 - w'ly to M.H #41

STA	Elev's:
2+45	442.43 432.68 C 9.75
2+10	441.32 431.01 C 10.31
1+75	440.40 429.34 C 11.06
1+40	438.74 427.67 C 11.07
1+05	435.89 426.00 C 9.89
0+70	433.13 424.34 C 8.79
0+35	432.70 422.67 C 10.03
0+00 = M.H #40 (See Pg 13)	421.00 = F.L

476.6

STA	Elev's:
<u>CHK</u>	440.44 = 440.44 = T.B.M CHK NE'ly Corn Batt CON. STEP # 6775 - sly side SPRINGFIELD

3+50 = M.H #41 (Stubs 6' + 12' RT)	443.4 = TP	444.76 437.68 = F.L C 7.08
3+15		444.70 436.01 C 8.69
2+80		443.82 434.34 C 9.48

T.B.M (see Pg 13)

440.44 = CHK NE'ly Corn Batt
CON STEP #6775 SPRINGFIELD

SPRINGFIELD ÷ M.H. #40 Ely to Mallard
M.H. #65

STA:	Elev's:	STA:	Elev's:
2+60	446.33 437.42 C 8.91	5+45	455.93 448.14 C 7.79
2+32.80 = M.H. #39 stubs 6'4 1/2' RT	444.43 436.00 = F.L. C 8.43	5+10	456.49 447.94 C 8.55
2+10	442.89 434.52 C 8.37	4+75	457.90 447.74 C 10.16
1+75	440.64 432.26 C 8.38	4+52.80 = M.H. #38 (stubs 6'4 1/2' RT)	458.91 447.61 = F.L. C 11.30
1+40	438.44 430.01 C 8.43	4+35	459.39 446.66 C 12.73
1+05	436.55 427.76 C 8.79	4+00	458.22 444.82 C 13.40
0+70	434.55 425.51 C 9.04	3+65	454.92 442.97 C 11.95
0+35	433.02 423.25 C 9.77	3+30	451.51 441.12 C 10.39
M.H. #40 = 0+0.0 (see p. 13)	421.00 = F.L.	2+95	440.81 439.27 C 9.54

SPRINGFIELD (CONT.)

MALLARD: SPRINGFIELD (M.H.#65) ³¹
 Ely to m.H #66

STA: Ely's:
 CAR: 463.38 = 463.39 = NE Conn-
 Con. Min @
 MALLARD 46944

STA: Ely's:

Set stub to Ely

(=E EXIST 30' ST. MALLARD)
 7+32.80 = m.H #65
 A = 41° 31' RT. (See opp. Pg)
 (Stubs 6' 42" + 12.84 RT on split.)

2+11.12 = m.H #66
 (Stubs 6' 42" RT)

455.50
 450.30 = F.L.
 C 5.20

7+20

459.62
 449.20 = F.L.
 C 10.42

1+75

454.30
 450.11
 C 4.19

6+85

459.43
 449.13
 C 10.30

1+40

454.32
 449.92
 C 4.40

6+50

0.572

458.38
 448.94
 C 9.44

1+05

455.65
 449.74
 C 5.91

6+15

457.59
 448.74
 C 8.85

0+70

458.14
 449.56
 C 8.58

5+80

456.92
 448.54
 C 8.38

0+35

459.76
 449.38
 C 10.38

M.H #65 = 0+00

449.20

(See opp. Pg)

SPRINGFIELD :

- m.H. #45 to ELY -

STA	Elev's	STA	Elev's:
2+45	438.80 430.40 C 8.40	5+45	442.50 435.20 C 7.30
2+10	437.67 428.38 C 9.29	5+10	441.68 434.99 C 6.69
1+75	436.06 426.35 C 9.71	4+75	441.65 434.78 C 6.87
1+40	434.69 424.32 C 10.37	4+40	441.53 434.57 C 6.96
1+05	432.88 422.29 C 10.59	4+05	441.23 434.35 C 6.88
0+70	430.13 420.26 C 9.87	3+70	441.12 434.12 C 7.00
0+35	426.66 418.23 C 8.43	3+35	440.80 433.93 C 6.87
(Drop - m.H.) 0+00 = M.H. #45 (= 4495.60 E.S.M.T.) (see pg 18)	420.94 416.20 = F.L. ELY C 4.74	3+02.80 = m.H. #43	440.30 433.73 = F.L. C 6.57
		2+80	439.88 432.42 C 7.46

5.795

0.612

STA	Elevs:
8+50 = D.END	443.87 437.07 = F.L. C 6.80
8+25	443.69 436.92 C 6.77
7+90	443.39 436.71 C 6.68
7+55	443.30 436.50 C 6.80
7+20	443.25 436.28 C 6.97
6+85	443.34 436.07 C 7.27
6+52.80 = m.H # 42 Stubs 6' 1/2 RT E.	443.29 435.87 = F.L. C 7.42
6+15	443.09 435.63 C 7.46
5+80	442.69 435.42 C 7.27

CHK: TBM = 447.68 = 447.69 - do NELY
COR. CON STEP (1st step)
@ 6733 SPRINGFIELD

3
19.0

2
19.0

SPRINGFIELD:
M.H.#45, W'ly

STA:	Elev's:	STA:	Elev's:
(1+25 = Chim'y LT)	414.38	3+75	428.95
1+17	398.48		417.34
(1+12 END CONC. BK-FILL)	C15.90		C11.61
1+07	414.70	3+40	425.32
	398.06		415.20
	C16.64		C10.12
0+97 = BVC	415.16	3+05	421.28
(0+75 = Chim'y LT)	397.80		413.06
	C17.36		C8.22
0+70	416.05	2+70	417.91
	397.53		410.92
	C18.52		C6.99
0+35	418.10	2+37.20 = M.H.#46	415.41
	397.18	Stubs 6'4.12' RT	408.90 = F.L.
	C20.92		C6.51
(0+25 = Chim'y LT)		2+05	414.00
			406.00
			C8.00
(Beg Conc. BK-FILL)		1+70	413.50
(Drop-mid)			402.82
0+00 = M.H.#45	420.94		C10.68
(4+95.60 ESMIT)	396.83 = F.L. W'ly	1+37 = E.V.G	413.91
(see Pg 18)	C24.11		399.82
		1+27	C14.07
			414.21
			399.07
			C15.14
T.B.M	416.77 = chn S'ly end Tp		
	3rd Conc. Step @ #6620 SPRINGFIELD		

SPRINGFIELD: M.H. #45. Wly (CONT.)

STA:

CHK: (see opp. pg) →

Elev's:

6.1130

5+30.03 = M.H. #47
E PARADISE
(Stubs 8.48' + 15' split
NELY QUAD.)

5+15

4+80

4+45

4+10

435.30
426.80 = F.L.
C 8.50

435.14
425.89
C 9.25

433.37
423.75
C 9.62

432.45
421.62
C 10.83

430.92
419.48
C 11.44

PARADISE ÷ M.H. #47 E SPRINGFIELD
- Nly to M.H. #48

35

CHK: 430.45 = 430.46 = NW Corn. Conc. Ldg.
C #6569 SPRINGFIELD
SEly Corn. Springfield +
PARADISE

2+21.43 = M.H. #48

2+10

1+75

1+40

1+05

0+70

0+35

0+00 = M.H. #47
E SPRINGFIELD
(See opp. pg.)

6.1119

(3' x 6' stubs)

446.93
440.40 = F.L.
C 6.53

446.45
439.70
C 6.75

444.81
437.55
C 7.26

442.91
435.40
C 7.51

440.58
433.25
C 7.33

438.24
431.10
C 7.14

436.53
428.95
C 7.58

435.30
426.80
C 8.50

PARADISE :-
MALLARD to Tooley

36

STA:	Elev's
2+45	344.18 335.75 C 8.43
2+10	342.51 334.39 C 8.12
1+75	342.06 333.02 C 9.04
1+40	341.13 331.66 C 9.47
1+05	341.13 330.29 C 10.84
0+70	340.93 328.93 C 12.00
0+35	340.00 327.56 C 12.44
0+00 = EXIST M.H. & MALLARD # (DWG 13498-L)	326.12 CLK: 326.20 F.L. PARADISE
=(6+48.08 MALLARD)	
T.B.M.	340.89 = CLK NE 1/4 RT. MALLARD & PARADISE

3.90

(stubs 6' RT. & E)

STA:	Elev's:
5+52.82 = M.H. #13 stubs 6' + 12' RT	376.13 364.00 = F.L. C 12.13
5+15	370.73 360.07 C 10.66
4+80	366.70 356.43 C 10.27
4+45	362.34 352.79 C 9.55
4+10	358.79 349.15 C 9.64
3+75	355.44 345.51 C 9.93
3+40	351.82 341.87 C 9.95
3+02.82 = M.H. #12 stubs 6' + 12' RT. & E	348.03 338.00 = F.L. C 10.03
2+80	346.30 337.11 C 9.19

10.40

PARADISE: mallard to Tooley (CONT.)

STA:	Elev's:
8+75	435.07 424.31 C10.76
8+40	428.70 417.37 C11.33
8+02.82 = M.H.#14 Stubs 6' 4 1/2' RT	422.00 410.00 = F.L. C12.00
7+65	415.88 403.04 C12.84
7+30	409.30 396.61 C12.69
6+95	402.20 390.17 C12.03
6+60	395.32 383.73 C11.59
6+25	387.90 377.29 C10.61
5+90	381.62 370.85 C10.77

19.822

18.462

Elev's:

STA:

chk

Elev's:

462.08 - 462.06 = 2" Pipe
@ L.N.L Tooley at
PARADISE

= END SEWER PARADISE

9+13.82 = M.H.#14-A

Stubs 6' 4 1/2' RT

441.43
432.00 = F.L.
C 9.43

SWAN:

- MALLARD to TOOLEY -

STA:	Elev's
2+45	340.57 327.18 C13.39
2+10	340.26 327.04 C13.22
1+75	340.36 326.90 C13.46
1+40	339.19 326.76 C12.43
(1+31.7 = chmy RT.)	
1+05	338.81 326.62 C12.19
0+70	339.05 326.48 C12.57
0+35	340.59 326.34 C14.25
0+00 = EXIST MAH #9 & MALLARD (6+48.08 MALLARD)	CHK. EXIST = 326.12 326.20 = F.L. SWAN
T.B.M	326.70 = F.L. HOLSTROM PLACE 340.89 = NEW CHOPARADISE AND MALLARD

STA:	Elev's:
4+65	341.58 328.05 C13.53
4+30	341.22 327.91 C13.31
3+95	341.20 327.77 C13.43
3+60	341.08 327.63 C13.45
3+25	340.93 327.49 C13.44
(3+11.7 = chmy LT.)	
2+93.99 = M.H #10	340.56 327.37 = F.L. C13.19
2+80	340.47 327.31 C13.16

0.402

↓

SWAN ÷ MAILLARD to Tooley (CONT.)

Set T.B.M. = ch x 72' C.E. 5+80 T = 349.92 39

STA:	Elev's:	STA:	Elev's:
6+95	357.86 349.96 C 7.90	9+85	417.25 408.87 C 8.38
6+60	352.81 342.95 C 9.86	9+50	409.72 401.69 C 8.03
6+25	348.62 335.95 C 12.67	9+15	402.32 394.51 C 7.81
(5+96 = end CONC. BK-F.II)		8+80	394.90 387.33 C 7.57
A = 2° 56' 15" RT		8+45	387.55 380.15 C 7.40
5+87.99 = M.H. #9 (Stubs 6' + 12' on split on RT)	345.09 328.55 = F.L. C 16.54	8+09.68 = M.H. #8	379.98 372.91 = F.L. C 7.07
5+70 (Bsp CONC. BK-F.III)	343.93 328.47 C 15.46	8+00	378.02 370.97 C 7.05
(5+68.7 = chmy RT)		7+65	370.92 363.94 C 6.98
5+35	342.62 328.33 C 14.29	7+30	363.90 356.96 C 6.94
c (5+20.7 = chmy LT)	341.94 328.19 C 13.75		
5+00			

20.01g

20.508g

20.4g

20.0g

SWAN: MALLARD to Tooley (CONT.)

40

= end Swan Sewer

10+53.63 = M.H. #7

432.07
422.94 = F.L.
C 9.13

10+20

424.80
416.05
C 8.75

ORIOLE: MAILLARD to Tooley

T.B.M. Sta: 4+00 (Street Sta) = 4+15.46 Sewer 41
 1x1.35 LT E = 340.07

STA:	Elev's:
1+25	302.06 294.47 C 7.59
0+90	295.59 287.88 C 7.71
0+55.46 = F.V.C.	289.96 281.37 C 8.59
0+45.46	288.31 279.83 C 8.48
0+35.46	286.76 278.63 C 8.13
0+25.46	285.54 277.77 C 7.77
0+15.46 = B.V.C.	284.81 277.20 C 7.61
0+00 = FIRST M.H. & MAILLARD & ORIOLE (= M.H. #2 - DWG: 13498-L)	277.00 = F.L.
T.B.M.	277.80 = City Disc # N.Y. & FEDERAL

STA:	Elev's:
4+00	337.18 326.16 C 11.02
3+65	333.86 323.60 C 10.26
3+30	329.90 321.04 C 8.86
2+95	326.13 318.48 C 7.65
2+60	322.55 315.92 C 6.63
2+25.46 = M.H. #2	319.03 313.40 = F.L. C 5.63
1+95	314.50 307.65 C 6.85
1+60	308.11 301.06 C 7.05

MAILLARD + 14' # N.Y. & FEDERAL

CRIOLE (CONT.)

STA:	Elev's:
6+45	348.93 329.59 C19.34
6+10	348.57 329.45 C19.12
(5+87.46 = Chm'y <u>LT</u>)	347.95 329.31 C18.64
5+75	
5+40	346.72 329.17 C17.55
5+05	345.14 329.03 C16.11
(4+87.46 = Chm'y <u>anLT</u>)	
(4+85.46 = Beg Conc. BK-Fill)	
4+70	343.14 328.89 C14.25
<u>4+35.46 = M.H. #3</u>	340.31 328.76 = F.L. C11.55

0.40%

STA:	Elev's:
(8+20.46 = END CONC. BK-Fill)	
8+15	350.39 335.09 C15.30
(7+87.46 = Chm'y <u>LT</u>)	
7+80	349.83 332.53 C17.30
<u>7+45.46 = M.H. #4</u>	349.65 330.00 = F.L. C19.65
7+15	349.59 329.87 C19.72
(6+87.46 = Chm'y <u>LT</u>)	
6+80	349.04 329.73 C19.31

0.40%

ORIOLE (CONT)

STA:

Elev's:

CHK: T.B.M. = 1X1 40' L.T.C. ST AT ST. STA 12+10

11+15

20.86

373.87
365.90
C 7.97

405.46 = 405.48

10+80

368.36
358.90
C 9.46

10+45.46 = M.H.#5

363.62
352.00 = F.L.
C 11.62

10+25

361.29
350.49
C 10.80

9+90

358.08
347.92
C 10.16

9+55

33.8

355.50
345.34
C 10.16

12+59.22 = M.H.#6

401.43
394.75 = F.L.
C 6.68

9+20

353.46
342.77
C 10.69

12+20

20.0

393.18
386.90
C 6.28

8+85

352.14
340.22
C 11.92

11+85

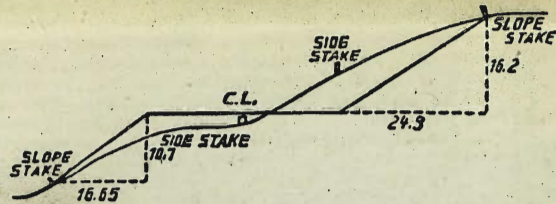
386.64
379.90
C 6.74

8+50

351.13
337.65
C 13.48

11+50

380.17
372.90
C 7.27



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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