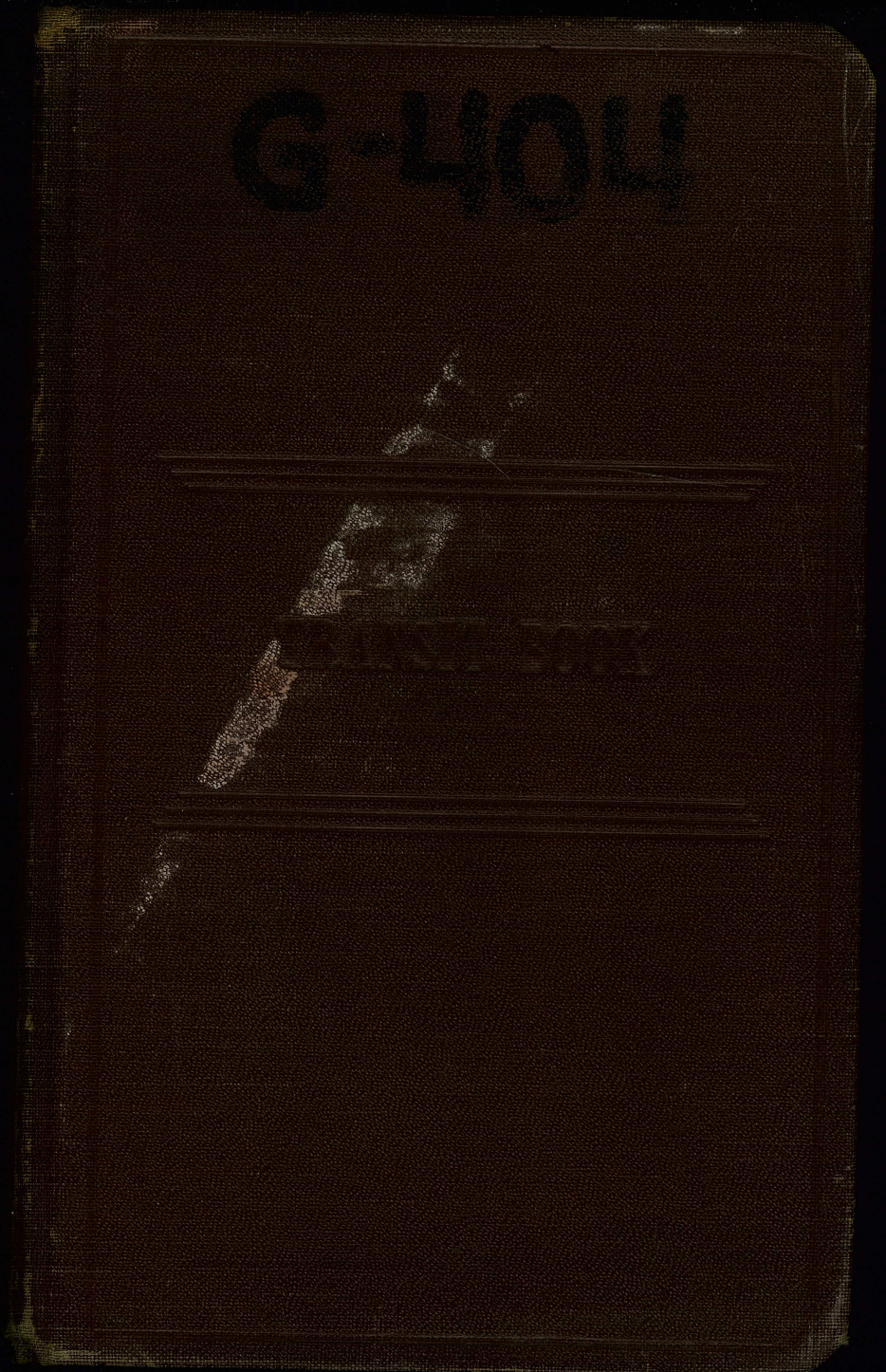
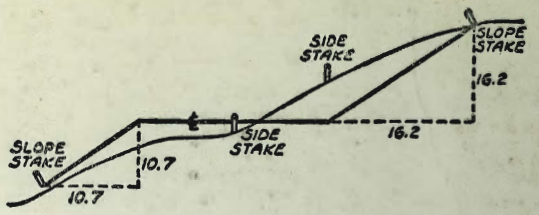


G-404



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

[1] Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

IMPROVED TABLES
AND
INFORMATION

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	.34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	.24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

FOR EXTERNALS ADD

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

ENCANTO

INDEX: ST. GRADES: & STORM-DRAINS (see next Pg)

INDEX:
STORM-DRAINS

Note: REF: For ties & alignment
ENCANTO: City Notes. L-21-22
lc-21-22
et al

CLARK
GARBER
ABRENILLA
ANDERSON
7-21-60
W.O. 33043

ST. GRADES: DIPPER

REF: DWG: 6330-D
46347-D

=FINAL grade chk: 2-20-61

	LT.	℄	RT (S/L)	
		10.1		310.2
0+52 = B.V.C. RT.		20.0	←	320.0
		F9.9		F9.8
		1½:to1		
		@ 14.8'		toe-stub 9.8' BK P.L
	315.44			
0+43.7 = E.V.C. LT.	321.1			
Stub 1.5' BK Toe	F5.66			
	1½:1			
	@10'			
	09.82	20.72		
0+42 = B.V.C. ℄	320.20	320.20		
	F10.38	C0.52		
	316.02			
0+31.70 = prop. LT.	321.40			
	F 5.38			
Stubs 5' BK. P.L				
(Note: 36' CBS BNK-pt 5' IN ST.)				
0+16.76 ℄ entry		21.07		
		320.40		
		C0.67		313.76
0+01.8 = Prop. RT.				320.35
				F6.59
				Stub at toe 5' BK P.L
(0+00 = ℄ Dipper & 60'th)			(Note: 36' CB's BNK-pt 5' IN ST NEAT)	
Note: All stubs 5' BK Prop-Line				
T.B.M		325.40 = 2x2 REF. PT.		
40'W'ly & 66'th - ON EDIPPAR (Projected)				

Cut-sheet formed in 7-25-60

DIPPER (CONT.)

STA	LT.	℄	RT (S'LY)
1+75	320.25 319.50 C0.75	20.23 319.50 C0.73	319.47 319.50 F0.03
1+50	318.11 318.50 F0.39	19.40 318.50 C0.90	317.23 318.50 F1.27
1+25	316.30 318.40 F2.1	19.2 318.4 C0.8	315.04 318.40 F3.36 stub 4.9 BK toe.
1+00 = P.R.V.C stub 5' BK P.L - 4.8' BK toe	315.48 319.00 F3.52 1½:1 @ 10'	19.26 319.00 C0.26	313.31 319.00 F5.69 stub 1½ BK toe
0+76 RT ONLY		19.96 319.80 C0.16	312.13 319.88 F7.75 1½ to 1 @ 11.7
0+71 LT + ℄ ONLY stub 5' BK = 2.2 BK toe	314.88 320.09 F5.21 1½:1 @ 10'	311.77 320.07 F8.30	stub KT

	LT.	℄	RT (S'LY)
3+40.92 ℄ RT.		38.5 340.1 F1.6	37.6 340.1 F2.5
3+31. LT. ONLY	332.33 337.70 F5.37		
3+25 = E.V.C. stub 5' BK P.L = 9.6" BK toe	332.58 336.20 F3.62	35.10 336.20 F1.1	337.2 336.20 C1.0
2+95	330.80 330.20 C0.6	30.27 330.20 C0.07	335.0 330.20 C4.8
2+65 = P.V.C.	327.1 326.6 C0.5	26.95 326.60 C0.35	329.6 326.6 C3.0
2+32.5	325.11 323.90 C1.21	23.92 323.90 C0.02	325.20 323.90 C1.3
2+00 = E.V.C.	324.53 321.20 C3.33	21.30 321.20 C0.10	321.66 321.20 C0.46

DIPPER (CONT.)

(Note: Stubs 5' BK P. Line 36' CB's Brk-pt 5' into STREET)

ST. GRADES: UPLAND

REF: DWG: 6329-D 6343-D

STA:	LT.	℄	RT. (s'ly)	(N'ly) LT.	℄	RT	
Chk:	340.41 =	340.51 =	Chx Con				
	Note:		Walk = 100' tie to Con mon = B.C Weaver: tie to N'ly From mon = Pink Stucco House	314.18 317.10 F3.08 @ 10'			
				0+27 = E.V.C. LT.			
				0+24 RT only		306.7 16.4 F7.7 1½:1 @14.5 ←	306.92 316.40 F9.48
				0+18 ℄ only	16.13 318.20 F2.07	14.60 318.20 F3.6	
3+63.16 = W.L. WEAVER	334.42 342.40 F7.98		342.45 344.7 F2.25	(344.95) 0+15 = Prop Conn. LT.	315.74 319.20 F3.46		
3+56.9 ℄		41.45 342.90 F1.45	40.9 342.90 F2.0	0+04 = B.V.C. RT. only		309.2 16.9 F7.7 1½:1 @10.6 ←	309.92 316.90 F6.98
3+51.08 LT. only toe stub 65' BK P.L	333.65 341.30 F7.65 1½:1 @11.5			0-14.95 = Prop Conn. RT. 0+03 ℄ only 0+00 = E.L. 60'+/- ℄ UPLAND (℄ 60'+/- = 0-16.76)	15.52 318.60 F3.08		310.67 316.00 F5.33 @10'
3+51.16 RT. only			339.8 342.50 F2.7				
				T.B.M.		319.10 = NAIL Pole # 3460 83-14 STA: 16+84 ± 60'+/- 15' RT℄	

Cut-sheet 7-25-60

UPLAND (CONT.)

STA:	LT.	℄	RT
1+49	290.73	95.63 ow RIM min	287.28
	295.60	295.60	295.60
2.7' BK toe	F4.87	C0.03	F8.32
			1½:1 @12.4'
1+24	295.15	96.16	88.4 288.55
	297.30	297.30	97.3 297.30
	F2.15	F1.14	F8.9 F8.75
			1½:1 @13.4'
0+99	298.14	299.0	91.2 291.42
	300.50	300.5	300.5 300.50
	F2.36	F1.5	F9.3 F9.08
			1½:1 @14'
0+74 = B.V.C	304.3	304.00	95.20 295.61
	305.80	305.80	305.8 305.80
	F1.5	F1.8	F10.6 F10.19
	@10'		1½:1 @15.9'
0+44 E.V.C Rt. only			302.30 302.27
			13.0 313.00
			F10.7 F10.73
			1½:1 @16' @10'
0+33 E.V.C Lt only	13.14	312.70	
	315.70	315.70	
	F2.56	F3.0	

STA:	LT.	℄	RT
3+80	312.65	14.00	314.12
	313.60	313.60	313.60
	F0.95	C0.40	C0.52
3+40 = E.V.C	307.02	07.72	306.76
	307.10	307.10	307.10
	F0.08	C0.62	F0.34
3+00	303.06	302.05	300.86
	301.80	301.80	301.80
	C1.26	C0.25	F0.94
2+60 = B.V.C	300.61	98.07	297.00
	299.10	299.10	299.10
	C1.51	F1.03	F2.1
2+30	298.27	96.25	294.74
	297.95	297.95	297.95
	C0.32	F1.70	F3.21 5' BK Toe
2+00	294.25	94.95	292.10
	296.80	296.80	296.80
	F2.55	F1.85	F4.70 3' BK toe
1+74 = E.V.C	290.95	945	288.96
	295.80	295.80	295.80
2.7 BK toe	F4.85	F1.3	F6.84
	@10'		@10' = toe

UPLAND (CONT.)

STA:	(W&W) LT	E	RT
5+78.15 = B.V.C. E & LT. only	345.55 352.60 F7.05 1½:1 @10.5'	50.40 352.60 F2.20	
5+49	338.63 345.60 F6.97 @1½:1, @10.5'	43.7 345.60 F1.9	341.49 345.60 F4.13 4' BK to C
5+20 = E.V.C	338.17 338.60 F0.43	37.44 338.60 F1.16	33597 338.60 F2.63 6' BK to C
4+90	331.38 332.00 F0.62	32.21 332.00 C0.21	330.88 332.00 F1.12
4+60 = B.V.C	327.08 326.50 C0.58	27.52 326.50 C1.02	327.25 326.50 C0.75
4+20	320.99 320.06 C0.93	21.06 320.06 C1.00	321.18 320.06 C1.12

	LT.	E	RT
Chk: T.B.M	338.95 =	338.92 = Ch ⊓ (S ely corn of conc. - LDG) + house at N w'ly corner WEAVER + UPLAND	
5+93.15 = prop. Conn. LT.	349.14 355.00 F5.86		
5+91.65 = prop. Conn. RT only = E Brk		52.8 354.90 F2.1	348.57 355.10 F6.53
5+79.7 = B.V.C. RT. only			346.50 352.90 F6.40 6.4 BK to C

CUT short 7-25-60

BURIAN (60th to WEAVER)

Ref: DWG: 6329-D
6349-D

(Note: Stubs 5' BK. P.L
36' CB's
BTK-PT 5' into ST. (P.L. LINE)

STA:	(N'ly) LT.	℄ = FINAL ℄ CLR.	RT.	STA:	(N'ly) LT.	℄	RT
			327.08		315.90	21.14	330.86
0+36.50 = RT only			313.90	1+30	321.70	321.70	321.70
			C13.18		F5.80	Fo.56	C9.16
		313.87	27.03	Stub 5' BK P.L = 2.2' BK to	314.89	19.85	329.79
0+35 = EVC ℄ only		312.70 → Stub RT	312.70	1+10 = B.V.C ℄ & RT & P.C.V.C LT.	320.10	320.10	320.10
		C1.17	C14.33		F5.21	F0.25	C9.69
	312.20				313.80	18.42	
0+31.70 = Prop. Conn. LT. only	308.80			0+90	317.70	318.10	
	C3.40				F3.90	Co.32	
		313.02	26.57		312.87		
0+23 = ℄ only		312.10 → stub RT	312.10	0+70 = B.V.C LT only	314.60		
		C0.92	C14.47		F1.73		
0+14 = B.V.C RT only		326.10					
0+11 ℄ BVC		314.60					
		12.65	C11.50				
		312.3					
		Co.35	324.91			15.75	328.01
0+01.82 = prop Conn - RT. only			315.50	0+59 = ℄ + RT only		315.10	315.10
			C9.41			Co.65	C12.91
			@10				
					312.00		
[0+00 = ℄ 60th + ℄ BURIAN]				0+44 = E.V.C LT. only	310.10		
					C1.9		

T.B.M 312.07 = 312.10 = 2x2 = 45° REF. PT
45' N'ly ℄ 60th ON ℄ BURIAN (Proj.)

BURIAN (CONT.)

STA:	(Lty) LT	℄	RT	
4+10 = B.V.C	323.14	29.20		335.89
stub 5' BK P.L	328.40	328.40		328.40
= 2' BK Toe	F 5.26	C0.80		C 7.49
3+70	322.69	28.60		334.88
stub 5' BK. P.L	328.00	328.00		328.00
= 1.1' BK Toe	F 5.31	C0.60		C 6.88
stub 5' BK P.L				
= 3' BK toe	323.03	28.30		337.08
3+30	327.60	327.60		327.60
stub 5' BK P.L	F 4.57	C0.70		C 9.48
4.6' BK toe	323.67	27.07		338.07
3+02.80 = B.C.	327.30	327.33		327.30
Street	F 3.63	F0.26		C10.77
stub 5' BK P.L				
= 3' BK toe	322.64	27.56		337.69
2+90 = E.V.C	327.20	327.20		327.20
	F 4.56	C0.36		C10.49
	321.39	26.92		335.40
2+70	326.90	326.90		326.90
	F 5.71	C0.02		C 8.50
stub 5' BK P.L				
= 2' BK Toe	320.99	26.28		335.16
2+50 = B.V.C.	326.30	326.30		326.30
	F 5.31	F0.02		C 8.86
stub 5' BK P.L				
= 2.8' BK toe	319.74	24.70		334.20
2+00	324.50	324.50		324.50
	F 4.76	C0.20		C 9.7
stub 5' BK P.L				
= 0.7' BK Toe	316.48	22.40		333.01
1+50 = E.V.C.	322.70	322.70		322.70
	F 6.22	F0.30		C10.31
	@10'			@10'

STA:	LT.	℄	RT. (Sty)	
		341.81		41.73
5+48.5 = B.V.C		344.40		344.40
℄ only		F 2.59	→ stub	RT. F.267
				341.13
5+41.50 = B.V.C.				342.90
RT. only				F1.77
	337.23	39.03		340 42
5+30 = E.V.C.	340.40	340.40		340.40
	F 3.17	F1.37		C0.02
	333.42	34 98		339.07
5+00	335.00	335.00		335.00
	F 1.58	F0.22		C4.07
	328.50	31.70		336.68
4+70 = B.V.C.	331.70	331.70		331.70
	F 3.20	grade		C4.98
toe stub 5' BK P.L	323.55	30.80		337.05
4+50 = E.V.C	330.10	330.10		330.10
	F 6.55	C0.70		C 6.95
stub 5' BK P.L = 1.7' BK toe	323.70	30.02		331.39
4+34.34 = E.C ST.	329.20	329.20		329.20
	F 5.50	C0.8		℄ 8.19
	323.67	29.80		321.12
4+30	328.90	328.90		328.90
stub 5' BK P.L	F 5.23	C0.90		8.22
= 2' BK toe				

BURIAN

STA: (N'ly)	LT.	℄	RT.
Ch.F: T.B.M.			349.22 = ch x .26 Conc Con walk = 63' w'ly Ref. Pt. to prop B.C. W. Lille Weaver Approx 108' S'ly of S.L. BURIAN
5+78.50 = EVC ℄ only		4590 347.60 F1.70	
5+71.50 = W.L. WEAVER	345.39 348.70 F3.31		343.99 346.10 F2.11
5+63.50 = ℄ only		43.92 346.80 F2.88	
5+59.44 = B.V.C LT. only	342.95 346.70 F3.75		
5+56.5 = RT only			342.5 345.30 F2.8 @16

ST. GRADES: TOOLEY (60'L, E'ly) Ref: 6330-D, 6347-D

Note: (40' CB's)

(Stubs 5' BK Prop. Line: BK-PT 3' IN Street.)

	LT.	℄	RT.
0+30 LT. only	381.00 374.00 C7.00		
0+28.8 = E.V.C ℄ only	381.00 371.00 C10.00	69.73 371.00 F1.27	
0+20 RT. only			363.70 367.30 F3.60 @8 Stub 2.6' BK toC
0+15.76 = prop. Cor. LT. & ℄ grade BK	380.97 373.80 C7.17 @8'		
0+07.88 ℄		69.18 370.20 F1.02	
0+00 = Prop. Corn RT			364.79 366.10 F1.31 @8'

(Stubs 5" BK Prop. L.)

[℄ 60'L + Tooley = 0-07.63]

T.B.M 383.89 = 2x2 = 50' N'ly

(Ref. Pt. to ℄ 60'L + ℄ Tooley)

Cot-Sheet D-2-55-60

Tooley (cont.)

= Final grade chk 2-16-61

STA:	LT.	℄	RT
	381.00	70.83	
0+90 = EVC LT only	371.70	371.70	
	C 9.3	F 0.87	
			354.37
0+80 = EVC RT only			371.50
			F 17.13
	381.32		
0+70 LT.	371.9		
	C 9.42		
℄		70.35	354.30
0+60 RT		371.35	370.80
		F 1.00	F 16.50
	381.52		
0+50 = P.R.V.C. LT. only	373.00		
	C 8.52		
	@ 8'		
		58.4	359.72
0+40 = P.R.V.C. RT. only		C 7.2 ←	369.20
		F 10.8	F 9.48
		1½:1	@ 8'
		@ 6.2'	

STA: (N½)	LT.	℄	RT		
					376.45
3+28.9 = Prop Corn R.T. only (WEAVER)					376.50
					F 0.05
	389.79	75.19			374.41
3+00	375.00	375.00			375.00
	C 14.79	C 0.79			F 0.59
	387.46	74.58			372.43
2+70	373.80	373.80			373.80
	C 13.66	C 0.78			F 1.37
	385.32	73.65			371.41
2+45.76 = B.V.C.	373.40	373.45			373.40
	C 11.92	C 0.20			F 1.99
	382.75	72.41			368.49
2+00	372.95	372.95			372.85
	C 9.80	F 0.54			F 4.36
					1.4 BK toe
	381.34	71.62	65.9		366.07
1+60	372.49	372.49	72.4	←	372.40
	C 8.85	F 0.87	F 6.5		F 6.33
			1½:1		
			@ 9.7		
	379.97	71.30			355.50
1+20	372.04	372.04			371.95
	C 7.93	F 0.74			F 16.45
	@ 8'				@ 8'

Tooley (cont)

STA:	LT.	℄	RT.	
				385.81
4+14.18 = prop.				384.50
Conn. RT. only				C1.31
(WEAVER)				
		84.20		
4+10	384.00	384.00		
		C0.20		
	389.33			
4+03.66 = Prop.	383.30			
Cor. LT. only	C6.03			
(WEAVER)				
	388.95	81.47		
3+85.76	381.40	381.40.		
	C7.55	C0.07		
	388.18	79.21		
3+60	378.90	378.90		
	C9.28	C0.31		
	390.38	77.31		
3+30	376.60	376.60		
	C13.78 @8	C0.71		

STA:	(N'Ly) LT.	℄	RT	
	422.42			426.90
6+33.78 = end	422.90	422.90		422.90
1911-A&T	F0.48			C4.00 @8'
GRADES:	@8'			
	413.30	16.66		418.22
6+00	416.36	416.36		416.36
stub 5' BK P.L	F3.06	C0.30		C1.86
= 3.4' BK toe				
	401.60	06.45		407.72
5+50	406.70	406.70		406.70
stub 5' BK P.L	F5.1	F0.25		C1.02
= 0.5' BK toe	1½:1			
	@8'			
	398.06	402.04		403.85
5+25.76 = E.V.C.	402.00	402.00		402.00
toe stub	F4.00	C0.04		C1.85
stub = 2.4' BK P.L.				
	394.31	97.4		399.57
5+00	397.30	397.3		397.30
	F2.99	C0.1		C2.27
	391.90	92.57		395.52
4+70	392.20	392.2		392.20
	F0.30	C0.37		C3.32
4+60.51 = prop.	391.52			
conn. LT.	390.90			
	C0.62			
		87.80		391.40
4+40	387.90	387.90		387.90
	Not set LT.	F0.10		C 3.5

Tooley (Cont.)

STA:	Lt.	℄	Rt.
Chk:	391.95	= 391.98 = Elev 40' Ref Pt. Hub, NELy of Con Mon! (STA MON) = 4+60.51 Tooley	
7+33.78 meet grid (end city-Forces work)	441.4 ± 441.8 ± F0.4 @27'		441.6 ± 441.8 ± @24'
7+03.78	438.77 437.7 C1.07 @21.30		440.57 437.7 C2.87 @19.2
6+83.78	433.32 434.40 F1.08 @17.5		438.21 434.40 C3.81 @16'
6+63.78	428.4 430.1 F1.7 @13.7'		435.8 430.1 C5.7 @12.8'

Cut sheet 6-25-60

Set T.B.m: 7+40 ± Pole # 546079-H
NAIL = 344.43

11

Ref. DWG's: 5916-D, 6322-D, 6329-D, 6330-D, 6345-D, 6346-D, 5920-D

60'h. ST. GRADES

STA 7+96.16 N'Ly to Tooley

STA:	Lt.	℄	Rt. (℄ly)
8+80	337.71 339.20 F1.49 10' BK. P.L.		349.57 339.20 C10.37 @10' 5' BK
8+60	337.31 339.30 F1.99 10' BK.		348.70 339.30 C9.40 @10 5' BK P
8+40	336.84 338.90 F2.06 10' BK		347.33 338.90 C8.43 @10 5' BK Prop
8+20 = B.V.C	335.74 337.80 F2.06 10' BK		346.50 337.80 C8.70 @10' 5' BK
7+96.16	334.12 336.30 F2.18 10' BK. P.L.		345.87 336.30 C9.57 @10 5' BK P.L.
T.B.m.			312:10 = 2x2 = 45 N'Ly R.P. to ℄ 60'h & BURIAN

Note:
- Vert. - Cut W.P.L & Brk Pt. 5' IN ST. FROM E. LINE.
- All stubs 5' BK P.L. UNLESS noted
- EXIST width 60'h. ST = 30'

60'ch

STA:	LT.	℄	RT. (E'ly)
10+58.31 = SE Corn BURIAN (See Pg. 6)	10' BK P.L 316.08 317.30 F1.22	317.05 317.30 F0.25	317.3
10+20	321.95 323.63 F1.68 10' BK		332.24 323.63 C8.61 @10' 5' BK
9+80 = E.V.C	327.06 330.10 F3.04 10' BK P.L = 9' BK toe		341.06 330.10 C10.96 @10' 5' BK
9+60	330.30 333.00 F2.7 10' BK		345.83 333.00 C12.83 @10' 5' BK P.
9+40	334.03 335.30 F1.27 10' BK		348.53 335.30 C13.23 @10' 5' BK P.
9+20	336.41 337.20 F0.79 10' BK		349.68 337.20 C12.48 @10' 5' BK P.
9+00	337.21 338.50 F1.29 10' BK P.L		350.04 338.50 C11.54 @10' 5' BK P.

STA:	LT.	℄ (Final grade chk 2-21-61)	RT
		280.76 280.10 C0.66	
12+50	265.60 280.10 F14.5 20' BK P.L	65.8 80.1 F14.3 1½:1 @21.4 toe-stub	283.09 280.10 C2.99 @10' 5' BK
12+20	278.20 284.40 F6.2 10' BK P.L	84.78 284.40 C0.38 =1' BK toe	290.26 284.40 C5.86 @10' 5' BK P.L
11+90 = B.V.C	287.70 290.60 F2.9 10' BK P.L = 10' BK toe	91.40 290.60 C0.80	298.53 290.60 C7.93 @10' 5' BK
11+40 = E.V.C	302.76 302.60 C0.16 10' BK. P.L	02.30 302.60 F0.30	310.60 302.60 C8.00 @10' 5' BK P.L
11+25.35 = NE (See BURIAN Pg 6)			
11+20	306.35 307.00 F0.65 10' BK P.L	06.51 307.00 F0.49	307.00 Not set (IN ST.)
11+00 = BVC (10+84.36 = ℄ BURIAN)	309.86 310.60 F0.74 10' BK P.L	310.13 310.60 F0.47	310.60 Not Set

Set T.B.M NAIL
P.S.I.# 546082-H
= 290.62
(Sta 14+10±)

60' Rt (CONT.)

STA:	LT.	℄	RT. (E'LY)
14+43.33	294.50 294.40 Co.10 5' BK	92.80 294.40 F1.6	290.02 294.40 F4.38 @10' 5' BK P.L = 3.4' BK toe
(36.66')			
14+06.66	288.95 288.70 Co.25 5' BK	87.4 288.70 F1.3	282.22 288.70 F6.48 @10' 5' BK = toe
(36.66')			
13+70=E.V.C	282.85 283.00 F0.15 5' BK	82.15 283.00 F0.85	277.08 283.00 F5.92 @10' 5' BK P.L. = 1' BK toe
13+40	279.22 279.20 Co.02 5' BK	79.25 279.20 Co.05	274.26 279.20 F4.94 @10' 5' BK P.L = 2.9' BK toe
		78.27 277.60 Co.67	
13+10 ℄	277.05 277.60 F0.55 5' BK P.L	72.5 77.6 F 5.1 1½:1 @7.6 to est ub	273.99 277.60 F3.61 @15' 10' BK. P.L
12+80	270.96 277.90 F6.94 15' BK P.L	78.80 277.90 Co.90	278.20 277.90 @10' Co.30 5' BK P.L
12'			

STA:	LT.	℄	RT.
16+60	320.73 319.60 C1.13		319.60 (not set)
16+40=BVC	319.20 317.90 C1.3		317.90 (not set)
16+11.74=S.E. UPLAND	(see Pg 3)		315.00
16+00	315.50 313.70 C1.8		308.69 313.70 F5.01 @10' 5' BK P.L = 2.5' BK toe
Note: Final cut from here to Sta: 21+80 OFFSETS W=24' 5 stubs			
15+60	310.87 309.50 C1.37		304.16 309.50 F5.34 @10' 5' BK P.L = 2' BK toe
15+20=E.V.C	309.00 305.30 C3.7 5' BK	303.3 305.30 F2.0	301.70 305.30 F3.6 @10' 5' BK P.L = toe
15+00	306.66 303.00 C3.66 5' BK	300.7 303.00 F2.3	299.12 303.00 F3.88 @10' 5' BK P.L = 5' BK toe
14+80=B.V.C	303.93 300.10 C3.83 5' BK	298.05 300.10 F2.05	295.95 300.10 F4.15 @10' 5' BK P.L = 5' BK toe
(36.66')			

60'ft (CONT.)

STA.	LT.	℄	RT
18+50=E.V.C	325.58 323.70 C1.88 5'BK		317.62 323.70 F6.08 @10' 5'BK P.L=1'BK toe
18+30	325.87 323.80 C2.07 5'BK		317.67 323.80 F6.13 @10' 5'BK P.L=1'BK toe
18+10=B.V.C	326.17 323.50 C2.67 5'BK		317.29 323.50 F6.21 @10' 5'BK P.L=0.7'BK toe
17+66.66	325.45 322.50 C2.95 5'BK		317.11 322.50 F5.39 @10' 5'BK P.L=2.5BK toe
17+23.33	323.60 321.50 C2.1 5'BK		316.50 321.50 F5.0 @10' 5'BK P.L =2.5'BK toe
(43.33)			
16+80=E.V.C	322.02 320.50 C1.52 5'BK P.L		315.3 320.50 =5'BK P.L F5.2 =2.2'BK toe 320.40
16+78.78=N.E. UPLAND			

STA.	LT.	℄	RT
20+60	323.02 321.05 C1.97 5'BK	12.90 21.1 ← F8.2 1½:1 @12.3 toe stub	313.21 321.05 F7.84 @10' 5'BK
20+20=E.V.C	324.02 321.30 C2.72 5'BK	13.6 21.3 ← F7.7 1½:1 @11.2 toe stub	313.82 321.30 F7.48 @10' 5'BK
20+00	324.27 321.50 C2.77 5'BK		314.91 321.50 F6.59 @10' 5'BK P.L=Toe
19+80=B.V.C	325.07 321.70 C3.37 5'BK		315.47 321.70 F6.23 @10' 5'BK P.L=1'BK toe
19+36.66	325.68 322.37 C3.31 5'BK	16.9 22.4 ← F5.5 1½:1 @8.2 toe stub	316.60 322.37 F5.77 @10' 5'BK
18+93.33	325.94 323.04 C2.90 5'BK P.L.	18.0 23.0 ← F5.0 1½:1 @7.5 toe stub	316.97 323.04 F6.07 @10' 5'BK P.L.
(43.33)			

Goth (cont.)

- FINAL grade chk 2-21-61

STA:	LT.	℄	RT.	
22+60	324.44 323.90 C0.54 5'BK	23.35 323.90 F0.55	317.28 323.90 F6.62 5'BK P.L	@10' =toe
22+32.84=N.E Dipper (See Pg 1)			15.7 322.20 F6.5 1½:1 @10 toe stub	
22+20=E.V.C.	323.36 321.40 C1.96 5'BK	21.69 321.40 C0.29	321.40	
22+00 (21+91.85=℄ Dipper)	322.81 320.50 C2.31 5'BK	20.71 320.50 C0.21	320.50	
21+80=B.V.C 21+65.8=S.E Dipper (See Pg 1)	322.30 320.30 C2.0 5'BK	20.09 320.30 F0.21	320.30	(not set) 13.0 320.40 F7.4 1½:1 @11.1 toe stub
21+40	321.94 320.55 C1.39 5'BK	12.9 20.6 F7.7 1½:1 @11.5 toe stub	313.18 320.55 F7.37 5'BK	@10'
21+00	322.55 320.80 C1.75 5'BK P.L	12.3 20.8 F8.5 1½:1 @12.7 toe stub	312.86 320.80 F7.94 5'BK P.L	@10'

Chk: 325.41 = 325.40 = T.B.M=2x2

40' R.P. to ℄ Goth & Dipper

STA:	LT.	℄	RT.	
		38.45 338.70 F0.25		
24+50=B.V.C.	339.45 338.70 C0.75 5'BK	33.5 38.7 F5.2 1½:1 @7.8 =toe stub	334.48 338.70 F4.22 5'BK	33 @10'
24+20=E.V.C.	336.33 335.10 C1.23 5'BK	34.96 335.10 F0.14	328.35 335.10 F6.75 5'BK P.L=toe	@10'
24+00	334.65 332.90 C1.75 5'BK	33.01 332.90 C0.11	328.50 332.90 F4.4 5'BK P.L=5'BK toe	@10'
23+80=BVC	333.43 331.40 C2.03 5'BK	31.37 331.40 F0.03	326.53 331.40 F4.87 5'BK P.L=3'BK toe	@10'
23+40	330.56 328.90 C1.66 5'BK	28.40 328.90 F0.5	324.03 328.90 F4.87 5'BK P.L=3'BK toe	@10'
23+00	327.64 326.40 C1.24 5'BK P.L.	25.7 326.40 F0.7	320.33 326.40 F6.07 5'BK P.L.=3'BK Toe	@10'

60'th (CONT.)

STA:	LT.	C	RT.	
26+25	371.52 364.80 C6.72 5'BK	65.52 364.80 C0.72	364.80 5'BK	(not set) @10'
26+22.03=S.E Tooley				
26+05=B.V.C.	364.75 361.60 C3.15 5'BK	61.96 361.60 C0.36	361.82 361.60 C0.22 5'BK	@10'
25+66.66	354.95 355.80 F0.85 5'BK	55.40 355.80 F0.4	352.60 355.80 F3.2 5'BK P.L	@10' =5'BK toe
25+28.33 (38.33)	350.25 350.0 C0.25 5'BK	48.80 350.00 F1.2	345.55 350.00 F4.45 5'BK P.L	@10' =3.3 BK toe
24+90=E.V.C.	343.07 344.20 F1.13 5'BK	43.2 344.20 F1.0	340.60 344.20 F3.6 5'BK P.L	@10' =5'BK toe
24+70	341.48 341.30 C0.18 5'BK P.L	40.75 341.30 F0.55	337.16 341.30 F4.14 5'BK P.L	@10' =4'BK Toe

T.B.M=254.73 60'th - FEDERAL, S'Ly

= 15' N'Ly Chx R.P

to CITY Disc

W'Ly Line 60'th & Fed: (E'Ly)

All Stubs 5' BK. RL

STA:	LT.	C	RT. (W'Ly)	
			255.87 255.00 C0.87	
0+16.13=SW Prop. Corner				
0-05.2=SE Prop. Corner	263.28 255.50 C7.78			
0+00=PT ℄ 60'th & Pt. 5.20' S'Ly of S'Ly Line FEDERAL at S.E. Prop. Corner	meet Pav edge	55.06 255.00	254.4	

Note: For GRADING X-Sect. this portion 60'th used detail ON DWG: #5916-D: OFFICE refused to produce DWG: #5915-D which is given as grading ref. Sheet, this Area 8-1-60: J.C.

Beg 60'th at FED:

Ref: 5920-D

Chk: 383.83 - 383.89 = 50' N'Ly R.P.

Hub - (to ℄ 60'th (& Tooley

(Cut-Sheet 7-27-60)

END GRADING this AREA:

26+84.09=90° to N.L. Tooley on RT.= Prop. Conn.	382.37 375.40 C6.97 5'BK	81.01 375.40 C5.61	375.40	@10'
26+45=E.V.C.	372.77 368.30 C4.47 5'BK P.L.	68.31 368.30 C0.01	368.30 5'BK P.L	(not set) @10'

60 4L (CONT.)

FEDERAL – S'LY

FINAL grade checks 2-13-61

STA:	(E'LY) LT	℄	RT:
	265.58	65.40	260.90
1+60	264.50	264.50	264.50
	C1.08	C 1.1	F3.6
	269.23	63.56	260 61
1+20	263.40	263.40	263.40
	C5.83	C0.16	F2.79
	266 30	61.60	259.89
0+80=E.V.C.	262.30	262.30	262.30
	C4.0	F0.70	F241
	266 27	60.34	258.92
0+60	261.20	261.10	261.00
	C 5.07	F0.76	F2.08
	266 12	58.7	257.77
0+40=P.R.V.C.	258.60	258.4	258.20
	C7.52	C0.3	F0.43
	265.38	257.08	256 16
0+20	256 30	255.90	255.00
	C9.08	C1.18	C1.16

Chk: 272.54 =272.48= Ck ☐ 17

CON DRIVE @ #6009

S'LY FULMAR

STA:	(E'LY) LT.	℄	RT (W'LY).
	278.38	79.45	284.83
3+00=E.V.C.	278.40	278.40	278.40
	F0.02	C1.05	C6.43
	271.38	73.15	276 99
2+70	272.40	272.40	272.40
	F 1.02	C0.75	C4.59
	267.68	70 50	272 53
2+50	269.50	269.50	269.50
	F1.82	C1.00	C3.03
66.4	264.49	68.37	268.93
2+30 67.2 ←	267.20	267.20	267.20
F0.8 @ 5' Stub at P.L.	F2.71	C1.17	C1.73
	264.05		
2+05.18= S.E.	265.80		
FULMAR	F1.75		
	265.09 60 (offset) LT.	66.74	265.13
2+00=B.V.C.		265.60	265.60
		C1.14	F0.47
	266.05		
1+65.18=N.E.	165.18		
FULMAR	C0.87		

60'46: Federal-54
(CONT.)

STA:	(E'ly) LT.	℄	RT
5+80	343.48 342.61 C0.87	42.78 342.61 C0.17	345.25 342.61 C2.64
5+40	333.39 333.44 F0.05	33.00 333.44 F0.44	334.55 333.44 C1.11
5+00	322.55 324.27 F1.72	23.26 324.27 F1.01	323.57 324.27 F0.70
4+60 06:1 15:1 1½:1 F9.0 @13.5' toe-stub	303.85 315.10 F11.25	313.93 315.10 F1.17	314.31 315.10 F0.79
4+20 290.1 305.9 1½:1 F15.8 @23.7' toe stub	293.78 305.92 F12.14	305.00 305.92 F0.92	304.18 305.92 F1.74
3+80 toe stub= 5' BK P.L	290.13 296.75 F6.62	296.60 296.75 F0.15	300.38 296.75 C3.63
3+40	286.34 287.57 F1.23	288.20 287.57 C0.63	293.50 287.57 C5.93

STA:	(E'ly) LT.	℄	RT (w'ly)
CHK:		= 358.46 = 50' 2x2	
		w'ly R.P. to ℄ 2x2 60'46 + EGRET	
6+72.11 = S.E EGRET LT. (Pg. 20)	363.80	363.80	364.93 363.80 C1.13
6+52.11 = ℄ EGRET		359.3 359.2	
6+32.11 = N.E EGRET (Pg. 20)	354.60	355.30 354.60 C0.70	355.63 354.60 C1.03
6+20	354.28 351.78 C2.50	352.64 351.78 C0.86	353.10 351.78 C1.32

Cot. sheet 8-7-60

EGRET

WEAVER & TOOLEY to 60 Ph

REF: DWG'S:
5917-D
5923-D

STA:	LT.	℄ = Final grade elev:	RT (el'y)
	386.54	78.6	375.61
0+38 = E.V.C	380.50	380.50	380.50
	C 6.04	F 1.9	F 4.89
	10' BK		10' BK P.L = 4.2' BK toe
		79.9	
0+30 ℄ only		382.3	
	388.04	F 2.4	
0+23 = LT only	383.20		
	C 4.84		
	10' BK		
		81.4	379.3
0+21 = BVC RT		384.10	384.3
		F 2.7	F 5.0
		82.4	5' BK
0+15 ℄ only		385.00	
		F 2.6	382.38
0+12.69 = S.E. CORN			385.70
WEAVER			F.332
			At Prop.
	388.62	83.5	
0+08 = B.V.C LT	384.70	385.6	
	C 3.92	F 2.1	
0+00 = ℄ EGRET & WEAVER	10' BK	84.5	
		386.3	
		F 1.8	
0-12.69 = S.W. CORN	385.70		
WEAVER			
	10' BK P.L		

T.B.M

391.98 = 2x2 = 40' NELy
Ref. At 40' NEly Con mon
Tooley & WEAVER

Note: Stubs set 10' BK P.L
HINGE-PT = 2' into ST.

DWG 5916-D 19
As reference (IN ABSENCE OF DWG 5915-D Showing grading DIAGRAM-EGRET)

STA:	LT.	℄	RT (E'ly & N'ly)
	373 28	61.83	352.05
2+13.34	361.40	361.40	361.40 → 50.6 61.4
	C 11.88	C 0.43	F 9.35 F1 0.8 1½:1 @16.2 Toe-Stub
(33.66')			10' BK
	373.15	62.43	355.06
1+79.68 = EVC	361.60	361.60	361.60
	C 11.55	C 0.83	F 6.54
	10' BK		10' BK = 2.3' BK toe
	373.48	63.71	357.49
1+49.68	362.60	362.60	362.60
	C 10.88	C 1.11	F 5.11
	10' BK		10' BK = 4.4' BK toe
	374.09	65.77	360.78
1+19.68	365.20	365.20	365.20
	C 8.89	C 0.57	F 4.42
	10' BK		10' BK = 5.4' BK toe
	375 64	69.92	365.23
0+89.68	369.50	369.50	369.50
	C 6.14	C 0.42	F 4.27
	10' BK		10' BK = 5.6' BK toe
	378 38	74.9	371.39
0+59.68 = BVC	375.60	375.60	375.60
	C 2.78	F 0.7	F 4 21
	10 BK P.L		10 BK P.L = 5.7' BK toe

EGRET (CONT.)

= FINAL grade chk'd 2-13-61

STA:	LT.	℄	RT.	
4+47.48	369.69 359.98 C 9.71	60.65 359.98 C0.67	356.82 359.98 F3.16 10'BK P.L = 7.2 BK toe	
(36.10)				
4+11.38 = E.C.	369.02 360.20 C 8.82	60.33 360.20 C0.13	356.13 360.20 F 4.07 10'BK P.L = 5.8 BK toe	
3+70.28	367.28 360.45 C 6.83	60.42 360.45 F0.03	353.22 360.45 F 7.23	53.7 60.5 F 6.8 1½:1 @ 10.2' stub toe ℄
3+29.19	366.33 360.70 C 5.63	60.66 360.70 F0.04	348.00 360.70 → F 12.70	44.0 60.7 F 16.7 1½:1 @ 25' toe stub
2+88.10	366.08 360.95 C 5.13	60.85 360.95 F0.10	347.03 360.95 → F 13.92	42.6 61.0 F 18.4 1½:1 @ 27.6 toe-stub
(CURVE 4 PTS. dcF = 7° 50' 56" ℄ ch = 40.97' Δ = 62 47 30 ℄ R = 150 d =				
2+47.01 = B.C.	368.6 361.20 C 7.4 10'BK	61.30 361.20 C0.10	349.73 361.20 → F 11.47 10'BK	47.0 61.2 F 14.2 1½:1 @ 21.3 toe stub
(33.66)				

STA:	LT.	℄	RT	
			58.42'	
CHK:		358.40	= 358.46 = 2x2' =	
			50' w/y R.P. to ℄ HUB 60'Ht EGRET	
5+99.68 = W.L. 60'Ht		60. 359.2 C0.8		
5+84.68 = ℄ 60'Ht.		59.3 = Ring mkr 359.2 C0.1		
5+69.68 = E.L. 60'Ht (end grading EGRET)	368.77 363.00 C 5.77	59.9 359.2 C0.7	354.57 355.4 Fa.83	
5+57.68 = BVC	369.215 362.10 C7.15	60.16 359.3 C0.86	355.11 356.50 F 1.39	
5+43.68 = E.V.C.	369.97 360.7 C9.27	60.1 359.4 C0.7	355.7 358.1 → F2.4	58.1
5+31.68	370.22 359.80 C10.42		354.99 359.10 F4.11	
5+19.68 = BVC	369.93 359.50 C 0.43	59.90 359.50 C0.30	355.50 359.50 → F4.0	56.5 59.5 F3.0 stub 2.5 BK toe
(36.10)				
4+83.58	371.27 359.75 C 11.52	60.22 359.75 C0.47	356.80 359.75 F 2.95 10'BK P.L	= 7.5' BK toe
(36.10)				

8-1-60 Cut-Sheet

WEAVER:

Fulmar to Tooley

(Note: Fulmar = 0+00)

Ref. Dwg's: 3916-D, 17-D, 22-D

Final Grade chk 2-14-61

STA:	LT.	℄	RT (N'Ly)	
0+71	406.29 385.70 C 20.59 10' BK.	87.23 385.70 C 1.53	386.36 385.70 C 0.66 2' BK P.L	
(31')				
0+40 = E.V.C.	407.94 386.70 C 21.24 10' BK.	88.51 386.70 C 1.81	386.69 386.70 F 0.01 2' BK P.L.	
0+39.65 = Prop. P.R.C. R.T. Fulmar.				
0+20	408.33 387.70 C 20.63 10' BK	89.43 387.70 C 1.73	387.70	(not set)
0+00	408.10 389.30 C 18.8 10' BK	390.73 389.30 C 1.43	389.30	(not set)

(On Curve:
℄ R = 245
℄ d = 7.01589
Δ = 70° 36' { 0+00 to E.C. Sta 3+01.89)

Note:
0+00 = P.T. ℄ Weaver
39.65' E'ly of P.T. ℄ Weaver Radial to NW'ly Prop Rad. Fulmar ℄ Weaver
= 7+32.31 Fulmar

T.B.M.: 387.07 = 2x2' R.P (20') to 1" P.R.C. Pipe LT Fulmar

(Orig. Stubs set 10' BK P.L)

T.B.M. 387.07 = 2x2 20' E'ly tie to Prop BC Sta 7+20 ± LT. Fulmar

STA:	LT.	℄	RT (W'Ly & N'Ly)	
2+71	397.51 373.08 C 14.43 10' BK	71.48 373.08 F 1.60	362.53 373.08 F 10.55 10' BK	60.0 73.1 F 13.1 @ 19.1 on Toe
(43')				
2+28	388.89 376.22 C 12.67 10' BK	74.85 376.22 F 1.37	367.56 376.22 F 8.66 10' BK	67.0 76.2 F 9.2 1½:1 @ 13.8, toe stub 11.8 BK P.L
(43')				
1+85	394.27 379.36 C 14.91 10' BK	79.30 379.36 F 0.06	372.76 379.36 F 6.60 10' BK P.L	71.6 79.4 F 7.8 1½:1 stub 6.3 BK toe
(43') 1+44.23 end 8' opng RT.				
1+42 = E.V.C.	400.02 382.50 C 17.52 10' BK	83.96 382.50 C 1.46	382.54 382.50 C 0.04 2' BK. P.L.	
1+22	403.95 383.80 C 20.15 10' BK	85.37 383.80 C 1.57	383.82 383.80 C 0.02 2' BK P.L	
B.V.C. = 1+02	405.87 384.70 C 21.17 10' BK P.L	386.22 384.70 C 1.52	384.85 384.70 C 0.15 2' BK P.L	
(31')				

WEAVER (cont.)

Fulmar to Tooley

STA:	LT.	℄	RT (N'ly)	
4+37	372 16 364.60 C 7.56 10' BK	64.5 364.6 F0.1	353.53 364.60 F11.07 10' BK	F11.7 @17.5 stub toe
4+00	380.08 364.70 C15.38 10' BK	65.29 364.70 C0.59	355.18 364.70 F8.92 10' BK	
(8.11') A=33° Curve: ℄R=200' ℄d=8.5944'				
3+91.89=B.C	381.55 365.00 C1.655 10' BK	65.74 365.00 C0.74	356.48 365.00 F8.52 10' BK	F10.0 @15' stub toe
(34.89')				
3+57=B.V.C	382 40 366.80 C15.60 10' BK	67.03 366.80 C0.23	358.29 366.80 F8.51 10' BK	57.7 64.8 V F9.1 @13.6
(43')				
3+14	383.79 369.94 C13.85 10' BK	68.89 369.94 F1.05	361.06 369.94 F8.88 10' BK P.C	
(12.11')				
3+01.89=E.C	384.90 370.82 C14.08 10' BK P.C	369.52 370.82 F1.30	361.53 370.82 F9.29 10' BK P.C	59.2 70.8 F11.6 @17.4
(30.89')				

STA:	LT.	℄	RT (N'ly)	
6+38=B.V.C R.T.	389.92 382.80 C7.12 10' BK	82.70 382.80 F0.10	372.74 382.80 F10.06 10' BK	71.8 82.8 F11.0 1½:1 @16.5 stub at toe =14.5 BK P.C
(40.33')				
5+97.66	386.28 378.42 C7.86 10' BK	78.22 378.42 F0.20	367.86 378.42 F10.56 10' BK	66.2 78.4 F12.2 1½:1 @18.3 stub-toe
(40.33')				
5+57.33	383.97 374.06 C9.91 10' BK	73.65 374.06 F0.41	364.50 374.06 F9.56 10' BK	63.7 74.1 F10.4 1½:1 @15.6 stub-toe
(40.33')				
5+17=E.V.C	381.73 369.70 C12.03 10' BK	69.31 369.70 F0.39	362.00 369.70 F7.70 10' BK	60.6 69.7 F9.1 1½:1 stub 2.4' BK toe
(9.92')				
5+07.08=E.C	381.40 368.60 C13.20 10' BK	68.38 368.60 F0.22	361.51 368.60 F7.09 10' BK	F8.3 1½:1 3.6' BK toe
(27.08')				
4+80	383.57 366.30 C17.27 10' BK P.C	366.31 366.30 C0.01	358.44 366.30 F7.86 10' BK P.C	
(43')				

WEAVER (CONT. (Fulmar to Tooley)

STA:	LT.	℄	RT.	
Chk:		391.94 =	391.98 = 2×2 =	
			40 NE'ly R.P. to NE Con Mon Tooley-WEAVER	
		86.4		
7+45.98		386.4 grade		
		87.18		
7+30.5 ℄ only		387.20		
		F0.02		
7+25.78 = N.L.	390.10			
= 4+60.51 Tooley (See Pg 16)	At P.L			
7+16.50 LT (not set) only	390.10			
	BK			
		87.48		
7+10 ℄ only		387.4		
	391.61	C0.08		
6+93 = BVC LT. only	388.80			
	C2.81			
	10' BK			
		87.36		
6+90.5 ℄ only		387.00		
		C0.36		
6+84.38 = NE EGRET RT. only			358.90	
(See pg 19)			At P.L.	
= 0+12.69 EGRET				
	390.63	86.02	377. Ro	F 8.4
6+70.50	386.20	385.90	381.30 →	@ 126
	C4.43	C0.12	F 8.14	106' BK
	10' BK P.L.		10 - BK P.L.	P.L.
		84.02		
6+50.5		384.00		
		C0.02		

(Cut-sheet 8-1-60)

(HINGE-PT 2' INTO ST. from P.L.)

Ref: 5916-17-D
5922-D

FULMAR: 7+32.31 to END (WEAVER 0+00 (SLY) to end grading)

Note: ↓ for FINAL grade check

STA:	LT.	℄	RT (ELY)	℄
	403 50	398.9	420.90	11.74
8+81.85 = BC	411.83 →	411.8	411.83	411.83
	F 8.33	F12.9, 1½:1, toe stub @ 19.3	C 9.07	F0.09
(40')				
	399.81	99.5	416.72	06.02
8+41.85 = E.C	405.47 →	405.5 toe stub	405.47	405.47
	F 5.66	F6.0 1½:1 @ 9'	C11.25	C 0.55 ℄
(34.77)				
	395.49	96.4	411.15	400.85
8+07.08	399.93 →	99.9	399.93	399.93 ℄
	F 4.44	F3.5 toe stub 1½:1 @ 5.2	C11.22	C0.92
(34.77) 7+76.22 = P.RC. LT.				
	392.00		409.35	395.32
7+72.31 = E.V.C	394.40		394.40	394.40 ℄
	F 2.4		C14.95	C 0.92
	390.10		407.91	9250
7+52.31	391.50		391.50	391.50 ℄
	F 1.4		C16.41	C1.00
	389.30		408.10	
7+32.31 (= 0+00 WEAVER)			389.30	
↓ (See pg. 21)			C18.80	See Pg.

T.B.M.

387.07 = 20' R.P. to Prop PAC on LT. 7+20.97 LT.

8+41.85 = ℄ C

FULMAR (CONT.) (E'LY)
(WEAVER - S'LY)

STA:	LT.	℄	RT
10+10.48 = E.C.	421.78 426.55 F 4.77	26.76 426.55 C0.21	429.51 426.55 C 2.02
stub toe =	5' B.L. P.L.		
10+06 = E.V.C.	421.37 426.20	26.54 426.20	428.52 426.20
def = 35° 33.9'	F 4.83	C0.34	C 2.32
℄ ch = 29.89'	= toe = 5' B.L. P.L.		
(30')			
9+76	419.85 423.80	23.73 423.80	426.63 423.80
20.9 23.8 F 2.9 @ 4:1			
def 26° 58.3'	F 3.95	F0.07	C 2.83
(30') ℄ ch = 29.89'	toe stub		
9+46	414.73 420.70	20.37 420.70	421.01 420.70
def 18° 22.6'	F 5.97	F0.33	C 6.31
℄ ch = 29.89'	1½:1 @ 9'		
(30')	toe stub		
9+16	411.90 416.80	16.56 416.80	426.27 416.80
def 9° 47'	F 4.90	F0.24	C 9.47
℄ ch = 29.89'	1½:1 @ 7.4'		
(30')	toe stub		
8+86 = B.V.C.	403.79 412.50	12.40 412.50	420.99 412.50
def 1° 11.3'	F 8.71	F0.10	C 8.49
℄ ch = 4.15			

STA:	LT.	℄	RT
T.B.M chk:		430.42 = ch □ CON. LDG. TO STAIRWAY @ ℄ 61+50 FULMAR	
11+15.83 end CITY Forces work	431.28 433.94 F 2.66		439.09 433.94 C 5.15
10+65.83 = end 1911-ACT	426.03 430.40 F 4.37 stub 5' B.L. P.L. = 0.4' Rt. toe	Meet EXIST R/W 2-15-61	436.93 430.40 C 6.53
10+38.15	423.48 428.49 F 5.01 1½:1 @ 7.5' toe stub	29.16 428.49 C0.67	435.14 428.49 C 6.65

CUT-SHEET 8-8-60

WEAVER (60'h to Tooley)

Ref: DWG's: 6322-D, 29-D, 30-D, 6348-D, 49-D

HINGE-pt = 5' into ST. From P.L

Final grade chk 2-20-61

STA: (W'ly / W'ly)	LT.	℄	RT (E'ly / E'ly)		STA:	LT.	℄	RT.	
0+25.77 = NE Corn. 60'h	300.7 298.6 C 2.1								
					1+00	303.04 302.17 C 0.87	301.18 302.17 F 0.99	296.04 302.17 F 6.13	stub 1' BK toe
0+21 RT. only			294.59 297.80 F 3.21	stub 5.2' BK 1½:1 toe	0+69 = E.V.C LT.	301.17 300.40 C 0.77	300.40	295.19 300.40 F 5.21	stub 2.2' BK toe
0+15 ℄		98.10 298.30 F 0.20			0+55 EVC ℄		99.2 299.6 F 0.4		
0+01 RT. only = P.R.V.C			294.02 297.00 F 2.98		0+49 LT. only	300.33 299.40 C 0.93			
0+00 ℄		97.48 297.80 F 0.32			0+35 ℄		98.63 298.7 F 0.07		
0-14 RT. only			293.13 296.20 F 3.07		0+41 RT only = E.V.C.			294.99 298.80 F 3.81	stub 3.3' BK toe
0-25.77 = SE Corn 60'h & WEAVER			293.24 295.00 F 1.76						
					0+29 LT. only = P.R.V.C	300.17 298.90 C 1.27			

All stubs 5' BK P.L unless noted

Note: 0+00 = ℄ WEAVER = ℄ E.L. 60'h

T.B.M. 294.68 = 56' (E'ly / Ch X) on Con Wall = R.P to E2x2 WEAVER on 4L

WEAVER (CONT)
(Go'th To Tooley)

STA:	LT.	℄	RT	
3+70	323.68 317.40 C 6.28	16.95 317.40 F0.45	311.67 317.40 F5.73	stub @ P.L
3+35 = B.V.C	320.10 315.60 C4.5	15.34 315.60 F0.26	308.20 315.60 F7.4	stub @ P.L
3+00	317.97 313.59 C4.38	13.90 313.59 C0.31	308.29 313.59 F5.30	stub @ P.L
2+50	314.86 310.73 C4.13	10.97 310.73 C0.24	306.44 310.73 F4.29	stub @ P.L
2+00	310.38 307.88 C2.50	307.78 307.88 F0.10	302.70 307.88 F5.18	stub 2.2' BK toe
1+50	306.57 305.02 C1.55	304.36 305.02 F0.66	300.46 305.02 F4.56	stub 3.1' BK toe

STA:	LT.	℄	RT	
5+69.92	329.64 322.35 C7.29	22.50 322.35 C0.15	314.30 322.35 F8.05	STUB @ T 120 OUT. hinge pt.
5+31.61	329.47 321.60 C7.87	21.95 321.60 C0.35	314.62 321.60 F6.98	STUB AT 10.5 OUT BK hinge PT.
4+93.30 (38.305)	320.20 320.85 C 7.35	21.57 320.85 C0.72	314.86 320.85 F5.99	STUB 1' BK TOE
4+55 = E.V.C	327.01 320.10 C6.91	20.35 320.10 C0.25	315.67 320.10 F5.07	STUB 2.4 BK TOE
4+20	325.92 319.30 C6.62	19.31 319.30 C0.01	313.17 319.30 F6.13	stub 1' BK toe
3+95	324.69 318.40 C6.29	18.00 318.40 F0.40	312.94 318.40 F5.46	

WEAVER (CONT.)
(60+46 to Tool+4)

STA:	LT.	℄	RT.	
7+59.45	335.67 328.05 C7.62	28.98 328.05 C0.93	324.47 328.05 F3.58	
7+25.63	339.10 326.72 C12.38	27.38 326.72 C0.66	323.36 326.72 F3.36	
3 pts (33.82')				
6+94.80=E.V.C.	336.84 325.40 C11.44	25.75 325.40 C0.35	321.13 325.40 F4.27	3.6' BK toe
				toe stub 6.1' BK P.L
6+51.80	329.80 324.10 C5.70	24.07 324.10 F0.03	316.74 324.10 F7.36	316.77 324.10 F7.33 1½:1 @11.1
6+11.80=B.V.C.	329.58 323.10 C6.48	22.86 323.10 F0.24	315.34 323.10 F7.76	
				toe stub 7.1' BK Prop.
6+08.22=B.C.	329.55 323.03 C6.52	22.93 323.03 F0.10	315.24 323.03 F7.79	314.95 323.03 F 8.08 1½:1 @12.1

STA:	LT.	℄	RT.	
				toe stub 4' BK P.L
9+80.03=B.C.	344.04 336.67 C7.37	36.97 336.67 C0.30	330.45 336.67 F6.22	330.67 336.67 F6.00 1½:1 @9 + S =4 BK P.L
9+33.33	344.15 334.85 C9.30	34.97 334.85 C0.12	328.72 334.85 F6.13	28.85 334.85 F6.0 1½:1 @9'
				toe stub 4' BK P.L
8+86.65	344.65 333.02 C11.63	33.25 333.02 C0.23	328.11 333.02 F4.91	329.00 333.02 F4.0 1½:1 @6
				toe stub 1' BK P.L
8+39.96	342.55 331.20 C11.35	31.96 331.20 C0.76	327.14 331.20 F4.06	stub 5' BK toe
(46.68')				
7+93.28=E.C.	338.46 329.37 C9.09	30.42 329.37 C1.05	324.88 329.37 F4.49	stub 5' BK toe

WEAVER (CONT)
(604h to Tooley)

STA:	LT.	℄	RT.	
11+31.94 = SW CORN - BURIAN (Pg 8)				
11+11.85 = E.V.C	343.42 343.80 F0.38	44.48 343.80 C0.68	347.01 343.80 C3.21	
10+81.85	342.95 341.10 C1.85	42.63 341.10 C1.53	343.00 341.10 C1.9	
10+51.85	342.44 340.00 C2.44	40.47 340.0 C0.47	336 47 340.00 F3.53	
10+24.19 = E.C.	343.50 338.60 C4.90	38.9 338.6 C0.3	333 85 338.60 F4.75	
9+91.85 = B.V.C	344 33 337.20 C7.13	37.51 337.20 C0.31	332 49 337.20 F4.71	stub @ P.I.

Chk:

349.22 = 63' R.P. chx
W'ly of Prop (W'ly) ℄
HUB. Sta: 10+24.19
Weaver

STA:		LT.	℄	RT.
12+40	46.7 55.7	347.28 355.70	54.84 355.70	361.02 355.70
toe stub 8.5' Bx RL	F 9.0 1½:1 @13.5	F 8.42	F0.86	C5.32
12+00 = P.R.V.C		34444 351.60	51 18 351.60	354 02 351.60
toe-stub 5.8' B/C P.L		F7.16	F0.42	C2.42
11+91.94 = NW CORN BURIAN (Pg 8)				
11+70		348.30	48.28 348.30 F0.02	353.59 348.30 C5.29
11+61.94 = ℄ BURIAN BURIAN (Pg 8)				
11+40 = B.V.C.		342.31 345.80 F3.49	46.14 345.80 C0.34	350.62 345.80 C4.82

WEAVER (CONT.)
(60'± to Tooley)

STA:	LT.	℄	RT.	
13+80.28 = E.C = NE Republic defF: ℄ch 40.26 5'BK = 36.69'	361.80	62.26 361.80 Co,46	370.94 361.80 C 9.14 @	1'BK sh 10:1 to toe 1:1
13+80. (wet set) See above STA:	353.25 361.80 F 8.55	51.8 61.8 F10.0 1½:1 @15	361.80	
13+40 defF: ℄ch = 39.98' 5'BK LT = 36.45'	353.77 360.80 F 7.03	61.44 360.80 Co.64 59.28 359.10 Co.18	371.4 360.80 C10.6 @	1'BK sh. 11½' to toe 1:1
13+00 = B.V.C defF = 1° 14.64 ℄ch = 17.20' 5'BK Prop ch. LT = 15.68'	351.09 359.10 F 8.01	50.5 59.1 F 8.6 1½:1 @12.9	371.5 359.10 C12.4 @	1'BK sh 13.4' to toe 1:1
(d = 04.3396') 12+82.80 = BC (Note: Beg cut slope 1:1 on RT.)	350.06 358.43 F 8.37	58.04 358.43 Fo.39 49.4 58.4 F 9.0 1½:1 @13.5	366.50 358.43 C8.07 @	Stub 1'BK shoulder 9.1' to toe 1:1
12+80 = EVC	349.95 358.30 F 8.35	57.81 358.30 Fo.49	66.75 358.30 C 8.45	

STA:	LT.	℄	RT	
16+03.73 = EC defF = 4° 14' 30" ℄ Ch = 24.27' 5'BK LT = 21.68'	350.57 359.73 F 9.16	49.41 59.7 F10.3 1½:1 @15.4 58.99 359.73 Fo.74	368.65 359.73 C 8.92 @	1'BK sh. 9.9' to toe 1:1
15+79.45 defF = 2° 07' 15" ℄ ch 24.27' Ch. 5'BK P.L. LT = 21.68	351.77 360.08 F 8.31	50.7 60.1 F 9.4 1½:1 @14.1 59.49 360.08 Fo.59	368.80 360.08 C 8.72 @	1'BK sh. 9.7 to toe 1:1
15+55.18 = BC	350.17 360.42 F10.25	48.4 60.4 F12.0 1½:1 @18 59.95 360.42 Fo.47	369.20 360.42 C 8.78 @	1'BK sh 9.8' to toe 1:1
15+07.59	350.80 361.12 F10.32	60.80 361.12 Fo.32	369.50 361.12 C 8.38 @	1'BK sh. 9.4' to toe 1:1
(47.59') 14+60 = E.V.C	351.72 361.80 F10.08	61.63 361.80 Fo.17 49.8 61.8 F12.0 1½:1 @18	370.00 361.80 C 8.2 @	1'BK sh. 9.2' to toe 1:1
14+20	353.43 362.10 F 8.67	62.33 362.10 Co.23	370.00 362.10 C 7.9 @	stub 1'BK shoulder 8.9 to toe 1:1

WEAVER (CONT.)

60'th to Tooley

STA	LT.	℄	RT.	
18+84.56=EC	355.63 in upland	55.16 / 355.63 C0.13	364.00 / 355.63 C8.37 @1:1	Stub 1' Bk Sh. 9.4' to toe
18+59.71=SW upland (Pg 5)				
18+38.34	346.85 / 356.33 F9.48	46.3 / 56.3 / 56.33 / 356.33 F1.00 1½:1 @15'	364.03 / 356.33 C7.70 @1:1	1' Bk Sh. 8.7' to toe
17+92.11	346.33 / 357.00 F10.67	43.8 / 57. / 56.3 / 357.0 F13.2 1½:1 @19.8' F0.7	364.1 / 357.00 C7.1 @1:1	1' Bk sh. 8.1' to toe
3 pts (46.223)				
17+45.89=BC	345.35 / 357.67 F12.32	40.9 / 57.7 / 56.30 / 357.67 F16.8 1½:1 @25.2 F1.37	364.10 / 357.67 C6.43 @1:1	1' Bk sh. 7.4' to toe
16+98.50	345.09 / 358.36 F13.27	40.80 / 68.36 / 51.04 / 358.36 F17.56 1½:1 @26.3 F1.32	366.00 / 358.36 C7.64 @1:1	1' Bk sh. 8.6' to toe
(47.386)				
16+51.11	348.24 / 359.05 F10.81	45.2 / 59.1 / 58.43 / 359.05 F13.9 1½:1 @20.8' F0.62	367.93 / 359.05 C8.88 @1:1	Stub 1' Bk Shoulder 9.9' to toe
(41.336)				

CHK:

338.92=ch ⊡ (S'ELY CORNER CONC. LDG.) — HOUSE NW'LY WEAVER & UPLAND

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STA:	LT.	℄	RT.	
		54.05 / 353.53 C0.52		
21+20	345.31 / 353.53 F8.22	44.7 / 53.5 F8.8 1½:1 @13.2'	361.60 / 353.53 C8.07 @1:1	Stub 1' Bk Sh. 9.1' to toe
20+70	342.92 / 353.82 F10.90	53.56 / 353.82 F0.26	361.97 / 353.82 C8.15 @1:1	Stub 1' Bk Sh. 9.2 to toes
		54.23 / 354.31 F0.08		
20+20 ℄	342.84 / 354.31 F11.47	42.0 / 54.3 F12.3 1½:1 @18.4'	361.10 / 354.31 C6.79	stub 1' Bk shoulder 7.8' to toe @1:1
		55.09 / 354.86 C0.29		
19+70 ℄	345.15 / 354.80 F9.65	44.5 / 54.8 F10.3 1½:1 @15.4	361.90 / 354.80 C7.1 @1:1	1' Bk sh. 8.1' to toe
19+20 ℄	348.04 / 355.30 F7.26	47.8 / 55.3 F7.5 1½:1 @11.2	364.40 / 355.30 C9.1 @1:1	1' Bk sh 10.1' to toe
19+07.71=NW upland (Pg 5)		55.38 / 355.30 C0.08		
18+89.71=grid Brk =℄ upland	355.60	355.60	363.80 / 355.60 C8.2 @1:1	1' Bk sh. 9.2 to toes

WEAVER (CONT)

60th to Tooley

STA:	LT.	℄	RT
23+60=E.N.C.	340.60 346.00 F5.4	45 30 346.00 F0.70	353.26 346.00 C7.26
23+38.30=S.W DIPPER (Pg 3)		48.40 348.80 F0.40	
23+20	341.71 348.80 F7.09	46.0 48.8 Stub F2.8 diff 0.8 Bk toe	360.26 348.80 C11.46
22+90	348.11 350.40 F2.29	50.57 350.40 C0.17	360.61 350.40 C10.21
22+60	349.48 351.50 F2.02	52.24 351.50 C0.74	362 79 351.50 C11.29
22+20=B.V.C Stub 2.4' Bk toe	347.25 352.30 F5.05	53.20 352.30 C0.90	363 41 352.30 C11.11
21+70 stub toe	346 01 352.82 F6.81	53.89 352.82 C1.07	361.81 352.82 C8.99
21+50 end 1:1 Slope RATIO - RT stub toe	346.38 353.03 F6.65		361.60 353.03 C8.57 @1:1

Stub 1' Bk shoulder 9.6 to toe From stub

STA.	LT.	℄	RT.
25+00	340.08 342.40 F2.32	42.70 342.40 C0.30	343.71 342.40 C1.31
24+75 3' Bk toe	336.55 341.20 F4.65	41.06 341.20 F0.14	341.14 341.20 F0.06
24+65.57=B.C stub 1.5' Bk toe	335.34 341.00 F5.66	40.72 341.00 F0.28	339.76 341.00 F1.24
24+50	334.31 340.80 F6.49	40.60 340.80 F0.20	338.85 340.80 F1.95
24+20 toe stub 6.2' Bk P.L	334.08 341.60 F7.52 1½:1 @11.2'	41.50 341.60 F0.10	341.61 341.60 C0.01
24+15.67=N.W Cor. Dipper (Pg 3)			
23+95=B.V.C (not set)	343.20	42.90 343.20 F0.30	347.05 343.20 C3.85

WEAVER (CONT.)
60th to Tooley

STA:	LT	℄	RT
	371.74	70.11	370.57
27+00	369.86	369.86	369.86
	C1.88	C0.25	C0.71
35.30'			
	366.02	64.00	364.24
26+64.65 = E.C	364.07	364.07	364.07
	C1.95	F0.07	C0.17
24.65'			
	360.29	60.04	360.95
26+40 = grade Brk	360.03	360.03	360.03
	C0.26	C0.01	C0.92
42.5'			
	352.94	53.90	354.40
25+97.50	354.01	354.01	354.01
	F1.07	F0.11	C0.39
42.50'			
	344.42	48.37	348.93
25+55 = E.V.C	348.00	348.00	348.00
	F-3.58	C0.37	C0.93
	343.03	45.56	346.31
25+30	344.90	344.90	344.90
	F1.87	C0.66	C1.41

STA:	LT	℄	RT	
Chk:		391.79 =	391.98 = 40' NELy R.P HUB (40 NELy Common) (Tooley & WEAVER)	
27+95.75 = SE Tooley RT.			383.50	(See pg 10) Not-Set
27+91 = E.V.C RT. only			385.70 383.10 C2.6	
27+71 RT only			382.36 381.10 C1.26	
27+57 ℄		78.77 378.7 C0.07		
27+51 = B.V.C RT. only			378.70 378.20 C0.5	
27+37 ℄		76.1 375.9		
27+35.15 = SW Tooley LT. (See Pg 10)	376.38 375.61 C0.77	C0.2	374.39 375.61 F1.22	

Cut-Shoot 8-5-60

FULMAR:

(STAKED 8-4-60 by Pope)

60'th to WEAVER

STA:	LT.	℄ = Final grade chk's 2-15-61	RT
1463.25	286.70	87.72 286.70 C 1.02	286.70
1443.25=B.V.C	284.14 283.8 C0.34	84.48 283.8 C0.68	283.72 283.8 F0.08
1+00	277.18 278.14 F0.96	78.04 278.14 F0.10	277.78 278.14 F0.36
Prop. 0+48=E.V.C START	270.08 271.40 F1.32	71.59 271.40 C0.19	271.40 271.40 grade
0+30 ℄ E.V.C only		69.87 269.1 C0.77	
0+12	266.23 266.40 F0.17	67.96 266.7 C 1.26	266.20 267.10 F0.90
0+00=℄ FULMAR @ E.L. 60'th	265.42 265.1 C0.32	266.65 265.60 C 1.05	263.50 266.00 F2.5

T.B.M 272.48= CHIS CONCRETE MON 9AH #6009 Fulmar -RT

STA:	LT.	℄	RT
2+83.25	318.23 312.40 C-5.83	11.44 312.40 F0.96	310.25 312.40 F 2.15 sta 5' BK P.I = 3.7' BK to ℄
2+63.25	308.10	307.50 308.10 F0.6	308.10
2+43.25= B.V.C	308.27 303.40 C4.87	303.37 303.40 F0.03	303.06 303.40 F0.34
2+23.25= E.V.C	303.36 298.60 C4.76	99.31 298.6 C0.71	299.64 298.60 C 1.04
2+03.25	294.10	95.4 294.10 C1.3	294.10
1+83.25	292.00 290.10 C1.90	291.39 290.10 C1.29	291.00 290.10 C0.90

FULMAR (CONT)

60th to weaver

STA:	LT.	℄	RT
4+45.60	349.55 342.30 C-7.25	42.71 342.30 C 0.41	340.96 342.30 F-1.34
4+18.25 = B.C	344.90 337.36 C-7.54	37.56 337.36 C 0.30	334.96 337.36 F-2.40 5' BK P.L = 4.4' BK toe
4+00.25 = Beg. 8' opening RT	341.32 334.09 C-7.23	334.09	330.03 334.09 F 4.06 = 1.8 BK toe sta 6 5' BK P.L at opening
3+73.25	336.13 329.22 C-6.91	28.90 329.22 F 0.32	326.18 329.22 F 3.04 5' BK P.L = 1.5 BK toe
3+23.25 = E.V.C	328.2 320.2 C 8.0	19.4 320.2 F 0.8	317.00 320.2 F 3.2 5' BK P.L = 2.2 BK toe
3+03.25	316.50	315.5 316.5 F 1.0	316.50

STA:	LT.	℄	RT
6+04.10	367.98 369.30 F-1.32	369.30	372.33 369.30 C-3.03
5+52.96 = E.V.C	363.05 361.00 C-2.05	361.00	362.25 361.00 C-1.25
5+32.96	361.13 357.70 C-3.43	357.70	361.67 357.70 C-3.97
5+12.96 = E.C	358.77 354.30 C 4.47	54.61 354.30 C 0.31	358.42 354.30 C 4.12
4+92.96	356.62 350.80 C 5.82	51.20 350.80 C 0.40	352.22 350.80 C-1.42
4+72.96 = B.V.C	354.00 347.20 C 6.80	47.75 347.20 C 0.55	346.83 347.20 F 0.37

FULMAR (CONT.)
60th to WEAVER

STA.	LT.	℄	RT.
7+17.65 RT. ONLY			386.42 387.10 F0.68
7+10 E.V.C. LT. ONLY	385.65 386.80 F1.15		
7+02.65 B.V.C. RT. ONLY			385.39 385.30 C0.09
7+00.99=P.C.C. RT ONLY =Weaver			385.07 385.03 C0.04
6+90=B.V.C LT.	382.13 383.20 F1.07	383.20	383.20
6+55.25=B.C. (1.15')	375.16 377.60 F-2.44 ← 5' BK P.L.	377.60	381.16 377.60 C-3.56
=2.8 BK toe			

STA:	LT.	℄	RT.
Chk:		387.07	= 20' Ely 2x2 R.P to Prop P.R.C Ely Line FULMAR STA: 7+20.97
7+20.97=P.R.C LT.	388.99		
7+20=B.V.C LT. ONLY	388.11 388.80 F0.69		

Cutsheet 8-8-60

REPUBLIC

(STA: 13+00 to WEAVER)

Final grade chk'd 2-28-61

STA:	Lt.	℄	Rt.
15+18.03	433.00 436.66 F 3.66 5' BK P.L =4.5' BK toe	37.40 436.66 Co.74	442.42 436.66 C 5.76
14+72.49	433.03 437.75 F 4.72 5' BK P.L = toe	3843 437.75 Co.68	443.76 437.75 C 6.01
14+26.95 5.8' BK P.L	433.67 438.84 F 5.17 1½:1 @ 7.8	39.00 438.84 Co.16	443.00 438.84 C 4.16
13+81.44 = P.C.C. 5' BK P.L = 0.2' BK toe (d = 12.1046 CURVE IN 4 pts)	435.45 439.92 F 4.47	440.19 439.92 Co.27	442.61 439.92 C 2.69
Beg 1911-ACT 13+52.60 end C. Forces work stub at P.L.	437.94 440.60 F 2.66	409 40.6 F0.6	444.35 440.60 C 3.75
13+00 Beg City - Forces GRADING	(meet EXIST GR.)		
T.B.M.		445.85 = NAIL Pole ± Republic - STA: 12+68 ±	P-37118 RT.

REF: DWG'S: 6329-D, 6331-D, 6350-D

(Hinge-pt = 2' into ST. From P.L.)

36

STA:	Lt.	℄	Rt.
		m.H.R.m. Meet	
17+00 toe stub F 6.9 ← =8.3' BK P.L 1½:1 @ 10.3	423.58 429.55 F 5.97	29.6 429.55	438.54 429.55 C 8.99
16+70 = E.V.C. toe stub 7.4' BK P.L	424.96 431.30 F 6.34 1½:1 @ 9.4	31.48 431.30 Co.18	439.81 431.30 C 8.51
16+20 F 7.8 ← toe stub 9.7 BK P.L 1½:1 @ 14.7	427.54 434.24 F 6.70	33.87 434.24 F0.37	440.54 434.24 C 6.30
15+70 = B.V.C.	432.33 435.40 F 3.07	35.85 435.40 Co.45	443.37 435.40 C 7.97
15+63.57 = E.C.	433.16 435.58 F 2.42 5' BK P.L = 5 BK Toe	436.13 435.58 Co.55	442.07 435.58 C 6.49

Note: (All stubs 5' BK P.L. UNless Noted)

REPUBLIC (CONT.)

STA:	LT.	℄	RT.
19+30=B.V.C	407.30	15.94	416.08
stub 11.2 BK P.L	416.10	416.10	416.10
at toe	F8.8	F0.16	F0.02
(27.87)	1½:1 @13.2'		
19+02.13	414.55	17.66	418.21
	417.74	417.74	417.74
	F3.19	F0.08	C0.47
(27.86')	5' BK P.L = 2.2' BK toe		
18+74.27=	414.59	19.16	419.14
Δ=33°22' B.C	419.37	419.37	419.37
ER=200'	F4.78	F0.21	F0.23
d=8.5944'	5' BK P.L = toe		
18+50	410.00	20.71	422.01
stub 14' BK P.L	420.79	420.79	420.79
16' BK hpt.	F10.78 @1½:1	F0.08	C1.22
18+00 F9.5	416.85	23.30	434.73
1½:1 @14	423.71	423.71	423.71
stub toe = 12' BK P.L	F6.86	F0.41	C11.02
17+50	421.11	426.65	438.03
toe stub F6.6	426.63	426.63	426.63
= 8' BK P.L 1½:1 @10	F5.52	C0.02	C11.40

CLK 418.40 = 418.42 = W'ly 25'

CLX = tie to W'ly Prop. BC Sta 18+74.27

STA:	LT.	℄	RT.
21+40	385.6	01.30	413.37
stub at toe	400.60	400.60	400.60
20.5' BK P.L	F15.0 1½:1 @22.5	C0.70	C12.77
21+00	387.0	03.12	415.18
stub at toe	402.70	402.70	402.70
21.5' BK P.L Line	F15.7 1½:1 @23.5	C0.42	C12.48
20+60	389.4 405.5	396.70	05.87	416.99
stub at toe	F16.1	405.50	405.50	405.50
22.1' BK P.L	1½:1 @24'	F 8.8 @7'	C0.37	C11.49
20+20=B.V.C		400.38	09.41	421.11
		409.00	409.00	409.00
		F8.62	C0.41	C12.11
20+10=E.V.C		397.9	10.23	421.29
stub at toe		409.90	409.90	409.90
16' BK P.L.		F12.0 1½:1 @18'	C0.33	C11.39
19+90.74=E.C.		400.4	11.80	420.78
stub toe		412.00	412.00	412.00
15.4' BK P.L		F11.6 1½:1 @17.4'	F0.20	C8.78
20.74				
19+70	405.3	407.5	413.29	415.70
stub at toe	413.40	413.40	413.40	413.40
(40') 16' BK P.L	F 8.1 1½:1	F5.9	F0.11	C2.3

REPUBLIC (CONT

STA:	LT.	℄	RT.
24+10 = E.V.C.	383.1	93.37	404.47
	393.10	393.10	393.10
Stub Toe 13' BK P.L	F10.0 1½:1 @15	C0.27	C11.37
(50')			
23+60	83.60	9516	405.73
	394.80	394.80	394.80
Stub Toe 14.8' BK P.L	F11.2 1½:1 @16.8	C0.36	C10.93
(50.00)			
23+10 = B.V.C.	379.60	96.65	409.35
	396.20	396.20	396.20
Stub @ Toe 22.9' BK P.L	F16.6 1½:1 @24.9	C0.45	C13.15
(29.56')			
22+80.44 = B.C.	386.30	97.38	409.81
	396.91	396.91	396.91
Stub at Toe 13.9' BK P.L	F10.61 1½:1 @15.9	C0.47	C12.90
(50.22)			
22+30.22	382.1	98.64	402.50
	398.10	398.10	398.10
Stub @ Toe 22' BK P.L	F16.0 1½:1 @24'	C0.54	C4.4
(50.22)			
21+80 = E.V.C.	384.3	400.03	411.47
	399.30	399.30	399.30
Stub at Toe 20.5' BK P.L	F15.0 1½:1 @22.5	C0.73	C12.17

CHK: 400.73 = 400.75 = SPIKE Pole #541182-H
Sta 22+80.44 BC - LT

STA:	LT.	℄	RT.
26+50	78.60	84.09	393.13
	384.03	384.03	384.03
Stub Toe 6.1 BK P.L	F5.43 1½:1 @8.1	C0.06	C9.10
(40')			
26+10	378.00	85.71	395.12
	385.54	385.54	385.54
Stub Toe 9.2' BK P.L	F7.54 1½:1 @11.2	C0.17	C9.58
(40')			
25+70	375.80	87.01	396.53
	387.06	387.06	387.06
Stub Toe 14.9' BK P.L	F11.26 1½:1 @16.9	F0.05	C9.47
(40')			
25+30	379.10	88.70	400.74
	388.57	388.57	388.57
Stub Toe 12.2' BK P.L	F9.47 1½:1 @14.2	C0.13	C12.17
(40')			
24+90	378.08	8996	400.34
	390.08	390.08	390.08
Stub Toe 16' BK P.L	F12.00 1½:1 @18	F0.12	C10.26
(40')			
24+50	382.00	91.36	402.64
	391.59	391.59	391.59
Stub Toe 12.4' BK P.L	F9.59 1½:1 @14.4	F0.23	C11.05
(40')			

REPUBLIC (CONT.)

STA:	LT.	℄	RT.
29+22.60=B.V.C	358.20	67.55	374.78
toe stub	368.50	368.50	368.50
13.9' BK P.L	F10.3	F0.95	C6.28
	1½:1		
	@15.7'		
(44.20)			
28+78.40	363.80	70.33	377.95
stub toe	371.43	371.43	371.43
9.4' BK P.L	F7.63	F1.10	C6.52
	1½:1		
	@11.4		
(44.20)			
28+34.20	368.37	74.05	381.80
stub toe	374.37	374.37	374.37
7' BK P.L	F6.00	F0.32	C7.43
	1½:1		
	@9		
(44.20)			
27+90 =E.V.C	372.3	77.18	385.14
stub toe	377.30	377.30	377.30
5.5' BK P.L	F5.0	F0.12	C7.84
	1½:1		
	@7.5		
(50')			
27+40	375.1	80.11	388.30
stub toe	380.30	380.30	380.30
5.8' BK P.L	F5.2	F0.19	C8.0
	1½:1		
	@7.8		
(50')			
26+90 =B.V.C	378.1	382.52	392.00
stub at toe	382.50	382.50	382.50
4.6' BK P.L	F4.4	C0.02	C9.50
	1½:1		
	@6.6'		
(40')			

TBM 357.26 = 357.24 = 2x2 = 18.54

s/y R.P. to prop E.C STA 29+72.60

STA:	LT.	℄	RT.	
				361.33
30+81.86= NE Corn				355.61
WEAVER - RT.				C5.72
			363.20	
30+71=E.V.C RT			355.30	
only			C7.9	
	355.99			
30+67.76= SE Corn.	353.00			
WEAVER - LT.	C2.99			
stub at P.L				
	353.32			
30+58=B.V.C	353.90			
LT. only	F0.58	56.1		
30+57℄		354.8		
		C1.3	366.38	
30+51 RT only			355.60	
		57.8	C10.78	
30+37℄		356.7		
		C1.1		
		58.37	370.59	
30+31 B.V.C RT		357.50	357.50	
℄ + RT. only		C0.87	C13.09	
	358.83	59.21	370.85	
30+22.60	358.60	358.60	358.60	
	C0.23	C0.61	C12.25	
(50')				
	362.8	364.05	370.31	
29+72.60=E.C	364.30	364.30	364.30	
	F1.5	F0.25	C6.01	
(50')				

CUT - Sheet 8-1-60

STAKED 8-8-60 by Pope.

BURIAN
(RADIO DR. to WEAVER)

STA:	LT.	℄	RT.
			291.87 282.30 C9.57
0+58 = EVC RT only			
0+45.53 = NW CORN. RADIO DR.	279.54 279.35 C0.19	81.49 281.20 C0.29	
0+43	278.54 279.00 C0.54		
0+38 RT only			288.70 280.90 C7.8
0+26 ℄ only			
0+18 = BVC RT			286.10 280.30 C5.8
0+05.30 = NE CORN RADIO DR - RT.			not set by Pope
(0+00 = ℄ BURIAN & ℄ RADIO DR.			

T.B.M. 280.42 = PK NAIL = [illegible] to M. [illegible] = PK NAIL Pole [illegible] ST

Ref: DWG's: 6322-D, 6351-D

(HINGE-PT = 5' into ST. From P.L.)

STA:	LT.	℄	RT.
2+09.90 toe stub. 6.2 BK P.L	288.82 296.28 F7.48 1½:1 @11.2	96.06 296.28 Fo.22	304.89 296.28 C8.61
1+81.90 toe stub 3.7' BK P.L	287.7 293.50 F5.8 1½:1 @8.7	93.79 293.50 C0.24	305.95 293.50 C12.45
1+53.90 = EVC toe stub 2' BK P.L	286.1 290.80 4.7 1½:1 @7.0	91.23 290.80 Co.93	301.62 290.80 C10.82
1+33.90 = B.C Stub = 2x2 @ P.L	286.2 288.80 F2.6	89.42 288.90 Co.52	297.95 288.80 C9.15
1+13.90 = BVC	285.13 287.10 F1.97	87.60 287.10 C0.50	296.95 287.10 C9.85
0+85.95	282.87 283.33 Fo.46	85.05 284.70 Co.35	295.18 284.70 C10.48
0+63 = EVC LT only	281.25 280.70 Co.55		

BURIAN
(RADIO-RD. to WEAVER)

STA:	LT.	℄	RT.	
3+97 K-od by Const	318.32 315.50 C2.82	15.39 315.50 Fo.11	322.60 315.50 C 7.10	K'od by Cont.
3+47.00 = B.V.C	309.43 309.70 F.27	09.40 309.70 Fo.30	318.10 309.70 C 8.40	
3+20.44	307.10	06.80 307.10 Fo. 30	307.10	
2+93.89 = E.C. Toe Stub 5.6' BK P.L	297.45 304.50 F 7.05 1½:1 @10.6	04.27 304.50 Fo.23	311.43 304.50 C.6.93	
2+65.90 toe stub 6.4' BK P.L	294.17 301.76 F 7.59 1½:1 @11.4	01.59 301.76 Fo.17	309.92 301.76 C 8.16	
2+37.90 ~~toe stub~~ 6.8' BK P.L	291.10 299.02 F 7.92 1½:1 @11.8	98.84 299.0 Fo.16	307.64 299.02 C 8.62	

Ch.K:

34.22 = W'ly 63' 41
R.P Ch.K
(to Prop(W'ly HUB)
E.C STA 10+24.19
WEAVER)

STA:	LT.	℄	RT.	
5+95			345.36 342.20 C 3.16	
5+85		3	341.70	
5+75 = B.V.C (ending ℄ grading)		341.00	343.45 341.00 C 2.45	341.36
5+56 = E.V.C		338.3 339.6 Fo.77		339.70 C 1.66
5+36		3677 337.80 F1.03	338.47 337.80 Co.67	
5+23.89 = N.W. Cor. WEAVER = B.C.P.L. - R.T.	336.00	336.25	336.25	
5+16 = B.V.C.	332.33 334.90 F2.57	34.04 334.9 Fo.86	335.77 334.90 Co.87	
4+81.50	327.07 329.00 F1.93	27.99 329.0 F 1.01	331.37 329.00 C 2.37	
4+47 = E.V.C.	322.42 323.10 Fo.68	22.24 323.10 Fo.86	326.77 323.10 C 3.67	

cut-sheet 8-11-60

WINNETT

(SCIMITAR to RADIO RD) 3-3-61

HINGE-Pt { 10' into ST. LT. / 3' " " RT.

= Final grade chk

STA:	LT.	℄	RT (E'Ly)	(℄ chk: —)
0+83	394.06 387.80 C6.26 @10'	86.52 387.80 F1.28	394.3 387.80 C6.5	866 387.80 F1.2
0+53	95.93 390.10 C5.83 @10'	88.32 390.10 F1.78	98.64 390.10 C8.54	88.1 390.10 F2.0
0+23 = B.V.C	394.53 390.45 C4.08 @10'	390.00 390.45 F0.45	97.30 390.45 C6.85	89.70 390.45 F0.75
0-02 Lt. only	meet EXIST grd.			
0-10 Rt only			meet EXIST OIL-SURFACE	

[0+00 = Pt. ℄ 30' LT of 1" Pipe = N.L. Scimitar ℄ E.L.
WINNETT RT = NE Corner]

T.B.M: 395.85 = P.K. Pole # 65-178-H
E'Ly Line Scimitar

Ref: DWG's: { 6337-D, 6316-D / 6355-D, 6318-D }

Note: Stubs w'Ly side (LT.) on P.L. } 10' grading exception, LT. unless Noted
Stubs E'Ly side (RT.) 5' BK

STA:	LT.	℄	RT (E'Ly)	
2+23	360.17 358.66 C1.51 @10'	59.50 358.66 C0.84	361.41 358.66 C2.75	
(40')				
1+83	370.40 368.08 C2.32 @10'	69.08 368.08 C1.00	373.72 368.08 C5.64	
(40')				
1+43 = E.V.C	381.72 377.50 C4.22 @10'	77.4 377.5 F0.1	385.23 377.50 C7.73	77.45 377.50 ℄ F0.05 Chk
(1+34.77 = N'Ly Line EIDER-RT)				
1+32.53 RT. only			387.07 379.80 C7.27	
1+13	388.24 383.60 C4.64 @10'	383.10 383.60 F0.50	83.25 383.60 F0.35	not set or ck.
0+92.24 RT. only			386.70	not set
(0+90 = S'Ly Line EIDER-RT)				

WINNETT (CONT.)

STA:	LT.	℄	RT. (℄)
4+70	301.06 304.80 F3.74 @10'	0539 304.80 C0.59	308.75 304.90 C3.85
4+30	304.61 311.00 F6.39	1.42 311.00 C1.42	318.67 311.00 C7.67
(40')			
3+90 = B.V.C	314.3 319.30 F5.0	19.78 319.30 C0.48	326.38 319.30 C7.08
(47')			
3+43 stub P.L = toe 1½:1	323.89 330.39 F6.50	30.39 330.39 grade	334.92 330.39 C4.53
(40')			
3+03	338.13 339.82 F1.69	39.94 339.82 C0.12	342.15 339.82 C2.33
(40')			
2+63	350.52 349.24 C1.28 @10'	349.89 349.24 C0.65	352.34 349.24 C3.10
(40')			

Chk: 297.28 = 297.26 = Ch ☐ CORN WALK @ 6353 RADIO RD.

STA:	LT.	℄	RT.	
6+29.5 RT only end grading			299.05	(meet grd) not set
6+24 LT only end grading	298.00 (not set)	(meet grd)		
6+10 LT only	297.75 297.80 F0.05		297.20 299.05 F1.85	
5+96 LT only	297.48 298.00 F0.52			Cut-Sheet 8-22-60
5+87 ℄ + RT only		98.00 298.55 F0.55	295.52 299.05 F3.53	5' BK P.L = 3' BK toe
5+68.50	294.91 298.55 F3.64	98.1 298.6 F0.5	294.7 299.10 F4.4	5' BK P.L = 1.4' BK toe
5+50 = E.V.C.	293.54 298.90 F5.36	98.73 298.90 F0.17	293.9 299.30 F5.4	5' BK P.L = toe
5+10	295.11 300.90 F5.79	300.72 300.90 F0.18	294.1 301.00 F6.9 1½:1 @10.3	stub 7.3' BK P.L

EIDER

WINNETT to KLAUBER

Ref: 6337-D
6356-B-D
6356-C-D

Note: Stubs 5' BK P.L unless noted
(HINGE PT = 2' into ST From P.L)

STA: (N&E)	LT.	℄ (final profile chk 2-28-61)	RT.	STA.	LT.	℄	RT.	Chk: RT. side
0+36.50 = LT EVC only	385.33 382.70 C2.63							
0+29.5 ℄		843 383.9 C0.4	90.1 385.3 C4.8	1+86.10 = B.C Δ = 31° 29' 30" ℄ R = 200.40'	397.1 401.50 F4.9	01.1 401.50 F0.4	412.05 401.50 C10.55	
0+20 RT only				toe stub = 4.6' BK P.L	1½:1 @ 6.6'			
0+16.50 LT. only	385.23 381.10 C4.13							
				1+60 toe stub = 2.6' BK P.L.	95.7 398.80 F3.1 1½:1 @ 4.6'	98.4 398.8 F0.4	407.5 398.80 C8.7	
0+10.08 = NE Corn Winnett	384.94 381.00 C3.94							
0+10 ℄		383.53 383.6 F0.07		1+30 5' BK P.L = 2.2' BK toe	391.36 395.30 F3.94	94.9 395.3 F0.9	403.5 395.30 C8.2	
0+03 = BVC RT. only			395.10 385.80 C9.3	88.5 385.80 C2.7				
				0+86.10 = BVC	386.84 389.60 F2.76	89.5 389.60 F0.10	398.7 389.60 C9.1	
0-10.08 = SE Corn Winnett			393.85 386.50 C7.35	85.56 386.50 F0.94				
				0+83 = EVC RT only			398.31 389.10 C9.21	
				0+70 ℄		87.66 387.4 C0.26		
[0+00 = ℄ EIDER & E.L. WINNETT]				0+50 ℄		385.8 385.1		
(℄ WINNETT = 0-33.60)				0+43 RT. only		C0.7	397.17 385.60 C11.57	92.14 385.60 C7.54

T.B.M

395.85 = P.K. Pole # 652478-H
E'ly Line Scimitar

EIDER (CONT.

STA.	LT.	℄	RT.
3+65.73	407.7	15.07	423.10
	414.53	414.53	414.53
toe stub 7.2' BK P.L	F6.83	C0.54	C8.57
	1½:1		
	@10.2		
3+25.73	408.6	12.53	421.08
	412.05	412.05	412.05
toe stub 3.2' BK P.L.	F3.45	C0.48	C9.03
	1½:1		
	@5.2		
2+96.23=E.C	406.5	10.63	318.78
	410.23	410.23	410.23
toe stub 3' BK P.L	F3.7	C0.40	C8.55
	1½:1		
	@5' rather than 5.5 here		
note: stubs have changed to 12=13 cut			
L= 10.13'			
2+86.10=EV.C	406.00	09.97	417.93
	409.60	409.60	409.60
Toe stub 3' BK P.L	F3.6	C0.37	C8.33
	1½:1		
	@ 5' here rather than 5.4		
L= 46.10'			
2+40	404.1	06.58	414.4
	406.30	406.30	406.30
toe stub 1.3' BK P.L	F2.2	C0.28	C8.1
	1½:1		
	@3.3		
L= 30'			
2+10	400.6	403.55	412.55
	403.80	403.80	403.80
toe stub 2.8' BK P.L	F3.2	F0.25	C8.75
	1½:1		
L= 23.90'	@4.8		

STA.	LT.	℄	RT.
	423.8	26.89	433.03
5+90	426.50	426.50	426.50
stub 2' BK P.L	F2.7	C0.39	C6.53
	1½:1		
	@4'		
	22.8	25.93	431.34
5+57.29	425.50	425.50	425.50
5' BK P.L = 5' BK toe	F2.1	C0.43	C5.84
	423.5	24.70	429.24
5+30	424.30	424.30	424.30
	F0.8	C0.40	C4.94
	417.6	22.26	29.58
4+85.73=B.C	421.90	421.90	421.90
4 B.V.C	F4.3	C0.36	C7.68
toe stub 4.4' BK P.L	1½:1		
	@6.4'		
	413.4	19.66	428.68
4+45.73	419.46	419.46	419.46
toe stub 7' BK P.L	F6.06	C0.20	C9.22
	1½:1		
	@9'		
	409.8	417.30	425.0
4+05.73	417.00	417.00	417.00
toe stub 8.8' BK P.L	F7.2	C0.30	C8.
	1½:1		
	@10.8		

4.3292 on P.I. Pipe

EIDER (CONT.)

STA:	LT.	℄	RT.	
8+01.85 = E.C toe stub 17.8' BK P.L	16.4 429.56 F 13.16 1½:1 @ 19.8'	29.61 429.56 C 0.05	34.72 429.56 C 5.16	stub 1' BK P.L
7+68.88 toe stub 14.2' BK P.L	18.3 429.13 F 10.83 1½:1 @ 16.2'	29.60 429.13 C 0.47	35.72 429.13 C 6.59	stub 1' BK P.L
7+35.92 toe-stub 9.4' BK P.L (℄ L = 32.966' (curve in 3 pts)	421.1 428.71 F 7.61 1½:1 @ 11.4'	29.30 428.71 C 0.59	37.42 428.71 C 8.71	
7+02.95 = BC Δ = 56° 40" ℄ R = 100' toe stub 11.6' BK P.L	19.2 428.28 F 9.08 1½:1 @ 13.6	29.02 428.28 C 0.74	37.09 428.28 C 8.81	
6+65.90 toe stub 11.5' BK P.L	18.8 427.79 F 8.99 1½:1 @ 13.5	28.58 427.79 C 0.79	35.91 427.79 C 8.12	
6+28.85 = E.C & E.Y.C toe stub 1.3' BK P.L	42.51 427.30 F 2.2 1½:1 @ 3.3	27.73 427.30 C 0.43	43441 427.30 C 7.17	

STA:	LT.	℄	RT	
10+85.55 = B.C Δ = 12° 26' ℄ R = 200' toe-stub 0.1' BK P.L	31.6 433.00 F 1.4 1½:1 @ 2.1'	33.66 433.00 C 0.66	40.36 433.00 C 7.36	
10+48.60 = B.V.C. toe-stub = P.L	31.4 432.70 F 1.3 1½:1 @ 2'	33 49 432.70 C 0.79	40.19 432.70 C 7.49	
10+00 toe stub 9.5' BK P.L	24.4 432.10 F 7.7 1½:1 @ 11.5'	32 36 432.10 C 0.26	39.14 432.10 C 7.04	
9+50 toe-stub 9.2' BK P.L	24.00 431.46 F 7.46 1½:1 @ 11.2'	31.46 431.46 grade	3775 431.46 C 6.29	
9+00 toe stub 14.3' BK P.L	19.90 430.82 F 10 92 1½:1 @ 16.3	3061 430.82 F 0.21	36.78 430.82 C 5.96	
8+50 toe-stub 13' BK P.L	420.18 430.18 F 10.00 1½:1 @ 15'	930.06 430.18 F 0.12	34.18 430.18 C 4.00	Stub 1' BK P.L.

EIDER (CONT.)

STA:	LT.	℄	RT.
13+00	26.4 432.30	32 23 432.30	34.77 432.30
toe-stub 6.8' BK P.L	F5.9 1½:1 @8.8'	F0.07	C2.47
12+50	30.8 432.74	32.91 432.74	37 34 432.74
toe-stub = 0.8' BK P.L	F1.94 1½:1 @2.8	C0,17	C4.60
12+08.60 = E.V.C	31.5 433.10	33.19 433.10	3866 433.10
toe-stub 0.4' BK P.L	F1.6 1½:1 @ 2.4	C0.09	C5.56
11+60	31.9 433.30	34.04 433.30	4083 433.30
toe-stub 0.1' BK P.L	F1.4 1½:1 @ 2.1	C0.74	C7.53
11+28.60=E.C def.= 6° 10' ℄ ch = 21.52 Ch. 5' BK P.L LT. 18.83	31.6 433.3 F1.7 1½:1 @2.5 toe stub 0.5' BK P.L	33.90 433.30 C0.60	40 96 433.30 C7.66
11+07.07 def.= 3° 05' ℄ ch = 21.52' (L = 21.52')	431.6 433.20 F1.6 1½:1 @2.4 toe stub 0.4' BK P.L	433.88 433.20 C0.68	440 06 433.20 C6.86

Chk: 424.80 = 424.82 = 47

W'Ly Ch "X" ON Rim ℄ M.H AT EIDER + KLAUBER

STA:	LT.	℄	RT.
15+17.20 = end dirty Forces grading	28.8 428.3 C0.5 stub 5' BK P.L	28.63 428.3 C0.33	4482 428.3 C1.9
14+93 = E.V.C	29.48 429.18 stub 5' BK P.L C0.30	29.60 429.18 C0.42	440.18 429.18 C1.00
(14+69.36 = N.E CHICADEE)			
14+67.20 = end 1911 - CONT. stub at P.L	30.6 430.00 C0.6	30.34 430.00 C0.34	439.6 430.00 C9.6
14+43	28.2 430.60	30.86 430.60	37.75 430.60
toe stub 1.6' BK P.L	F2.4 1½:1 @3.6	C0. 26	C7.15
(14+17.36 = N.W CHICADEE)			
13+93 = B.V.C	30.3 431.40	31.17 431.40	32.4 431.40
stub at P.L = 0.4' BK toe	F1.1	F0.23	C1.0
13+50	425.20 431.86	431.80 431.86	435.75 431.86
toe-stub 8' BK P.L	F6.66 1½:1 @ 10.0'	F0.06	C3.89

cut-sheet 8-22-60

T.B.M 30493 = W'ly 2x2 R.P. to ℄ WREN + SEW ESMT.

WREN
(KLAUBER to SCIMITAR)

STA	LT	℄	RT (E'ly)	
0+63 = E.V.C. LT. only toe stub 6.6' BK P.L	323.0 328.10 → F. 5.1 1½:1 @ 7.6'	24.7 = FINISH GRK 328.10 F3.4		
0+44 = EVC, RT only		32.44 332.6 ← F0.16	32.4 332.60 F0.2	
0+41.50 LT. only stub 5' BK P.L = 3.5' BK toe	330.2 331.90 → F1.7	30.32 331.90 F1.58		
0+32 RT only		33.8 334.80 ← F1.0	33.8 334.80 F1.0	stub
(0+30 = N'ly + W'ly Line KLAUBER)				
0+20 = B.V.C	32.9 333.20 F1.2		335.6 335.50 C0.1	
0+10 meet edge EXIST CON. R&V				
(0+00 = ℄ WREN + ℄ KLAUBER)				

T.B.M 335.35 = 16' E'ly R.A. CL x ℄ KLAUBER + ℄ WREN

REF: DWG'S: 6334-D
6333-D
6356-D-D
& Pg 35 (12-8-38) City notes by C.H.S

Note: All stubs 5' BK P.L. unless noted.
(HINGE-PT = 1' INTO ST from P.L STA: 0+00 to 6+76.39 ℄ hence 2' INTO ST.

48

STA:	LT.	℄	RT	
2+20 toe stub = 10.2' BK P.L	300.4 307.90 F7.5 1½:1 @ 11.2'	08.4 307.90 C0.5	03.9 307.90 F4.0 1½:1 @ 6'	toe stub = 5' BK P.L
1+90 toe stub 10.1' BK P.L	300.1 307.50 F7.4 1½:1 @ 11.1	7.78 307.50 C0.28	05.6 307.50 F1.9	stub 5' BK P.L = 3.1 BK toe
1+60 1+43.5 = NW Corn house	07.5 309.10 F1.6	09.3 309.10 C0.2	09.4 309.10 C0.3	
1+30 stub 5' BK P.L = toe	09.1 313.10 F4.0 1½:1 @ 6'	13.50 313.10 C0.40	13.84 313.10 C0.74	
1+00 = B.V.C toe stub 4.2' BK P.L	15.7 319.20 F3.5 1½:1 @ 5.2	19.26 319.20 C0.06	18.31 319.20 F0.89	
0+84 = SW Corn. house (New addit.)				
0+75 toe stub 7.7' BK P.L	319.4 325.20 F5.8 1½:1 @ 8.7	25.27 325.20 C0.07	22.2 325.20 F3.0 1½:1 @ 4.5	toe stub = 3.5' BK P.L

WREN (CONT.)

STA	LT.	℄	RT
4+30	44.20 344.80 F0.6	44.60 344.80 F0.2	48.99 344.80 C4.19
3+90=B.V.C	336.6 337.70 F1.1	37.62 337.70 F0.08	42.68 337.70 C4.98
3+60	330.46 331.76 F1.30	31.70 331.76 F0.06	337.60 331.76 C5.84
3+20	21.83 323.73 F1.90	23.41 323.73 F0.32	26.86 323.73 C3.13
2+80=E.V.C stub 5' BK P.L =0.2' BK toe	11.8 315.70 F3.9	15.40 315.70 F0.30	16.21 315.70 C0.50
2+50 toe-stub=6.9' BK P.L	305.4 310.70 F5.3 1½:1 @ 7.9	10.68 310.70 F0.02	09.3 310.70 F1.4

STA:	LT.	℄	RT	
6+70=B.V.C toe stub 3.8' BK P.L 6+63.30=Prop BC RT. only	53.4 356.60 F3.2 1½:1 @ 4.8	56.94 356.60 C0.34	356.60	(not set) 358.33 356.50 C1.83
6+30 stub 5' BK P.L	54.80 356.03 F1.23	56.43 356.03 C0.40	360.01 356.03 C3.98	
5+90	55.30 355.46 F0.16	55.40 355.46 F0.06	359.27 355.46 C3.81	
5+50=E.V.C	53.20 354.90 F1.7	54.28 354.90 Fa62	58.01 354.90 C3.11	
5+10	51.55 353.40 F1.85	53.17 353.40 F0.23	55.88 353.40 C2.48	
4+70	48.5 350.10 F1.6	49.8 350.10 F0.3	53.17 350.10 C3.07	

WREN (CONT.)

STA:	LT.	℄	RT
8+30 toe stub 4.7' BK P.L (40')	362.80 367.24 F4.44 1½:1 @6.7	67.44 367.24 C0.20	72.30 367.24 C5.06
7+90=E.V.C toe stub 3.7' BK P.L	59.5 363.30 F3.8 1½:1 @5.7	63.62 363.30 C0.32	68.05 363.30 C4.75
7+60 toe-stub 2.2' BK P.L	57.9 360.70 F2.8 1½:1 @4.2	61.15 360.70 C0.45	64.56 360.70 C3.86
7+30 toe-stub 1.9' BK P.L (30')	56.1 358.70 F2.6 1½:1 @3.9'	59.20 358.70 C0.5	62.7 358.70 C4.0
→ ℄ →		57.73 57.30 C0.43	
7+00	357.30 →	54.5 357.3 F2.8 1½:1 @4.2	59.35 357.30 C2.05
6+77.94=℄ Prop LT. =BC Prop Line (STA: Radial to ℄) (toe stub 3.4' BK P.L)	353.2 356.80 F3.6 1½:1 @5.4	toe stub =2.2' BK P.L	
6+76.35=B.C.℄ NOT SET →	356.70		

Chk:

352.64 = 40.74 W/4 50 R.P Chk

to ℄ B.C STA: 6+76.35' WREN

STA:	LT.	℄	RT
10+50 toe stub 2.3' BK P.L (30')	87.1 390.00 F2.9 1½:1 @4.3'	90.41 390.00 C0.41	90.92 390.00 C0.92
10+20 toe stub 0.7' BK P.L (30')	84.4 386.20 F1.8 1½:1 @2.7'	86.8 386.20 C0.60	90.18 386.20 C3.98
9+90=B.V.C toe stub 2.2' BK P.L	80.2 383.00 F2.8 1½:1 @4.2	83.6 383.00 C0.6	86.70 383.00 C3.70
9+50 toe stub 3.7 BK P.L	75.30 379.06 F3.76 1½:1 @5.7	79.43 379.06 C0.37	84.00 379.06 C5.06
9+10 toe stub 3.8' BK P.L	71.2 375.12 F3.92 1½:1 @5.8	75.11 375.12 F0.01	380.80 375.12 C4.32
8+70 toe stub 4.9' BK P.L	66.6 371.18 F4.58 1½:1 @6.9	70.97 371.18 F0.21	76.76 371.18 C5.58

WREN (CONT)

STA:	LT.	℄	RT	
			410.61	toe
11+78.98 = Prop			412.60	stub 1'
Cor. RT.			F1.99	BK P.L
only			1½:1	
(Scimitar)				
	400.00	10.73	410.48	
11+70.57 =	409.90	410.6	411.30	
B.V.C RT.	F9.9	C0.13	F0.82	stub 1' BK
grd BrK LT.	1½:1			P.L
toe stub 12.8' BK P.L	@14.8'			
	397.90	05.6	6.96	
11+40	404.60	404.60	404.60	stub 1' BK
toe-stub 8' BK P.L	F6.7	C1.0	C2.36	P.L
	1½:1			
	@10'			
	95.0	99.7	403.15	
11+10 = E.V.C	399.40	399.40	399.40	
toe-stub 46'	F4.4	C0.3	C3.75	
BK P.L	1½:1			
(30')	@6.6'			
	91.5	95.0	97.23	
10+80	394.40	394.40	394.40	
toe-stub 23' BK P.L	F2.9	C0.6	C2.83	
	1½:1			
	@4.3'			
City notes: CHS.	90.6	93.9	396 4	
10+73.53 = P.R.C	393.40	393.40	393.40	
(10+72.14 = Rec.)	F2.8	C0.5	C3.0	
toe-stub 2.2' BK P.L	1½:1			
	@4.2			

STA:	LT.	℄	RT.
Chk:			419.63 = chk tp w'ly end BlK-Wall - Near 346 se'ly chx tie to m.H #118
12+76 meet EXIST Edge OIL-PAV Scimitar	stub 10' BK oil		
	4045		
(SCIMITAR =Sta 29+05.72)	409.0		at pt. 18' into ST. From P.L
Eq:	F4.5		
12+58.79 = P.C.C	1½:1		
toe stub 11' IN ST.	@6.7'		
	02.2	11.77	= Final chk
12+15.60 = Prop	412.40	412.40	this Column.
Cor. LT. only	F10:2	F0.63	
(Scimitar) toe. stub	1½:1		
13.3' BK P.L	@15.3		
	402.0	11.8	
12+07 = E.V.C	413.00	413.00	
LT. only	F11.0	F1.2	
toe-stub 14.5'	1½:1		
BK P.L	@16.5		
	401.1	12.23	
11+94 LT.	413.20	413.20	
only	F12.1	F0.97	
toe-stub 16.1' BK P.L	1½:1		
	@18.1		
	400.5	11.70	
11+81 = B.V.C LT.	411.70	411.70	
only	F11.2	Grade	
toe stub 14.8' BK P.L	1½:1		
	@16.8'		

Cut-Sheet 8-22-60

SPRINGFIELD

WINNETT to PARADISE

STA: (N'ly)	P.L LT.	℄ = Final Chk grade	P.L RT.
0+30	336.1 328.70 C 7.4		
℄ + 0+20 = E.V.C RT. only		27.7 326.6 C 1.1	28.80 325.80 C 3.0
0+10 BVC LT. only	332.11 326.70 C 5.41		
0+05 RT only			26.48 323.20 C 3.28
0+00 = E.L. SPRINGFIELD	330.57 326.00 C 4.57	24.8 324.6 C 0.2	324.8 323.00 C 1.8
(0-30 = ℄ WINNETT & ℄ SPRINGFIELD)			
T.B.M.		325.56 = 80' SW'ly R.P. Chx on Conc. Ldg – (Hinge ℄ WINNETT & SPRINGFIELD)	

Ref: DWG: 6338-D
6353-D
6354-D

Note: All stubs 5' Bk. P.L unless noted 52

(HINGE-PT = 5' INTO ST. From P.L)

STA:	P.L LT.	℄	P.L RT.
1+90	65.77 354.00 C 11.77	53.7 354.0 F 0.3	55.55 354.00 C 1.55
1+60	60.96 351.30 C 9.66	50.9 351.3 F 0.4	52.25 351.30 C 0.95
1+30	61.73 347.50 C 14.23	47.3 347.5 F 0.2	49.03 347.50 C 1.53
1+00	50.80 342.70 C 8.1	42.6 342.7 F 0.1	341.16 342.70 F 1.54
0+70 = B.V.C	44.5 336.70 C 7.8	37.0 336.7 C 0.3	340.2 336.70 C 3.5
0+50 = E.V.C LT. only	339.98 332.30 C 7.68		
0+40 = EVC ℄		31.3 330.1 C 1.2	

SPRINGFIELD (CONT.)

STA:	LT.	℄	RT.	
3+70 = E.V.C.	57.86 346.40 C5.46	46.70 346.40 C0.3	38.5 346.40 F7.9 1½:1 @11.8	toe-stub = 6.8' BK P.L
3+40	57.97 350.50 C7.47	50.98 350.5 C0.48	44.5 350.50 F6.0 1½:1 @9'	toe-stub 4' BK P.L
3+10	68.07 353.40 C14.67	53.97 353.4 C0.57	49.85 353.40 F3.55	(No enchroachment)
2+80	66.81 355.20 C11.61	55.1 355.2 F0.1	53.42 355.20 F1.78	
2+50	69.92 355.90 C14.02	55.5 355.9 F0.4	55.97 355.90 C0.07	
2+20	67.65 355.50 C12.15	55.2 355.5 F0.3	56.65 355.50 C1.15	

Chk: 336.57 = 336.59 = Chk sely 7-53

Corn. Conc. Porch @ #6404 Springfield = NEly " & Oriole

STA:	LT.	℄	RT.	
5+00	33.06 334.10 F1.04	4.2 334.1 C0.1	25.8 334.10 F8.3 1½:1 @12.4'	T.S = 7.4 BK P.L (No ench.)
4+95.60 = E'ly Line - Oriole	33.08 334.00 F0.92			
4+70 ℄ RT. only		35.6 335.00 C0.6	25.5 335.00 F9.5 1½:1 @14.2	T.S = 9.2 BK P.L
4+40 RT. only		37.7 337.1 C0.6	28.6 337.10 F8.5 1½:1 @12.7	T.S = 7.7 BK P.L
4+35.60 = W'ly Line Oriole	39.3 337.5 C1.8			
3+95 = B.V.C.	347.48 342.60 C4.88	43.1 342.6 C0.5	34.2 342.60 F8.4 1½:1 @12.6	toe-stub = 7.6 BK P.L

SPRINGFIELD (CONT)

STA:	LT.	℄ (ON Rim Mill)	RT.	
			Correct	
	52 45	354.1	5755	(error)
6+80 (error)	354.40	354.1	354.40	
stub 7.5' BK toe	F1.95		C3.15	
(No enc.)				
	47.5	49.2	35077	
6+55 = P.C.V.C	349.30	349.3	349.30	
stub 7.3' BK to	F1.8	F0.1	C1.47	
(No enc.)				
	37.50	41.2	340.9	
6+10	341.50	341.5	341.50	
T.S = 1' BK P.L	F4.09	F0.3	F0.6	
	1½:1			
	@6			
	30.90	37.5	35.1	Stub 8.7 BK toe
5+80 T.S = 5.3' BK P.L	337.80	337.8	337.80	(No anch)
	F6.9	F0.3	F2.7	
	1½:1			
	@10.3			
	25.7	35.1	31.2	(No anch.)
5+50	335.50	335.5	335.50	
T.S = 9.7 BK P.L	F9.8	F0.4	F4.3	
	1½:1			
	@14.7			
	29.90	41	26.2	T.S = 5.1' BK P.L
5+25 toe-stub	334.30	334.3	334.30	
= 1.6' BK P.L	F4.40	F0.2	F8.1	
	1½:1		1½:1	
	@6.6		@12.1	

STA:	LT.	℄	RT.	
stub 3' BK toe = 4.3 BK P.L				
(anch)	80 2	82.7	80 13	P.L stub = 8.7' BK hinge-pt.
8+50 = E.V.C.	382.30	382.3	382.30	= 6.6' BK toe
	F2.1	C0.4	F2.17	
	72.9	75.7	73 81	P.L. stub = 6.6' BK hinge-pt.
8+10	375.10	375.1	375.10	= 4.6' BK toe
stub 3' BK toe	F2.2	C0.6	F1.3	
stub 2.15' BK AL Radial	@6' 1½:1		1½:1 @6.6	
(No Enc.)				
(error)	68.9	71.0	69.1 (error)	stub 6.1 BK toe
→ 7+82.59 = B.C	372.4	370.5	372.4	
(For Fut. CB's)	F3.5	C0.5	F3.3	69.1
stub 5' BK toe	68.9			370.5
(No enc.)	370.5			F 1.4 correct.
	F1.6			
correct.				
	662	69.0	67.3	(No enc.)
7+70 = B.V.C.	368.50	368.5	368.50	
stub 7.3' BK toe	F2.3	C0.5	F1.2	
(No enc)				
	60.8	63.4	58.45	
7+37.5	363.40	363.4	363.40	(No enc.)
stub 7.3' BK toe	F2.6	grade	F4.95	
(No enc)				
	56 24	58.1	58 13	
7+05 = E.V.C.	358.30	358.3	358.30	
stub 7.6' BK toe	F2.06	F0.2	F0.17	
(No enc)				

SPRINGFIELD (CONT.)

STA:	LT	℄	RT	
10+15 = B.V.C	406.93 404.40 C2.53	404.4 404.4 grade	399.9 404.40 F4.5 1½:1 @6.7	toe stub =1.7' BK P.L
(10+13.38 = E. SWAN) See SWAN				
10+10 = E.V.C ℄ & RT ONLY		404.2 404.2 grade	400.8 404.20 F3.4	P.L stub =toe
℄ & 9+60 RT ONLY		400.6 401.0 F0.4	99.1 401.00 F0.9	P.L. stub =3.4' BK toe
(9+48.77 = W. SWAN) See SWAN				
9+10 = B.V.C P.L. stub = 2.9' BK toe	92.55 393.70 F1.15	93.4 393.7 F0.3	91.9 393.70 F1.8	P.L stub =3.4' BK toe
→8+96.34 = E.C (FUT. CB'S) P.L stub = 0.4' BK toe	87.65 390.80 F3.15	90.9 390.8 C0.1	88.3 390.80 F2.5	P.L. stub = 1.2' BK toe
8+80 toe-stub = 7.9' BK P.L	379.5 388.00 F8.5 1½:1 @12.7	88.3 388.0 C0.3	85.33 388.00 F2.67	P.L stub = 5.6' BK APT. = 2.0' BK toe

STA:	LT	℄	RT	
12+70	401.78 394.20 C7.58	94.9 394.2 C0.7	85.70 394.20 F8.50 @12.5'	stub @ Toe = 7.7' BK P.L
12+40 = B.V.C	403.49 395.20 C8.29	95.4 395.2 C0.2	87.10 395.20 F. 8.10 @12'	stub @ toe = 7' BK P.L
12+05	406.08 397.44 C8.64	97.2 397.4 F0.2	92.70 397.44 F4.74 @7'	stub @ toe = 2' BK P.L
11+70	409.28 399.67 C9.61	99.5 399.7 F0.2	95.90 399.67 F3.77 @10'	Stub 5' BK P.L. = 6.3' BK toe
11+35 = E.V.C	410.55 401.90 C8.65	401.9 401.9 grade	399.0 401.90 F2.9 @10	Stub 5' BK P.L WR = 6.3 BK toe
10+75	409.64 404.40 C5.24	404.3 404.4 F0.1	401.9 404.40 F2.5 @5'	P.L. stub = 1.3 BK toe

SPRINGFIELD (CONT.)

STA:	LT.	℄	RT	
15+00 BVC	435.7 426.60 C7.1	27.0 426.6 C0.4	414.0 426.60 F12.6 1½:1 @12.3	Stub 3' BK P.L toe =7.3' BK P.L (toe=4.3 BK P.L)
14+53.32	425.40 418.40 C7.00	18.8 418.4 C0.4	13.8 418.40 F4.6 1½:1 @6.9	toe-Stub =1.9' BK P.L
14+06.66	418.8 410.20 C8.6	10.0 410.2 F0.2	403.20 410.20 F7.00 @10.5'	Stub @ toe = 5.5' BK P.L
13+60=E.V.C	412.4 402.00 C10.4	02.5 402.00 C0.5	90.90 402.00 F11.10 @16.6	Stub @ toe = =11.6' BK P.L
13+30	402.57 397.50 C5.07	98.6 397.5 C1.1	87.60 397.50 F9.90 @14.8'	Stub @ toe= 9.8' BK P.L
13+00	405.65 395.00 C10.65	96.08 395.00 C1.1	85.4 395.00 F9.6 @14.4'	Stub @ toe = 9.4' BK P.L

STA:	LT.	℄	RT	
16+80=E.V.C	41.04 432.90 C8.14	33.9 432.90 C1.0	30.1 432.90 F2.8 @4.6'	Stub 1' IN street =toe
16+40	45.54 435.90 C9.64	35.8 435.90 F0.1	32.3 435.90 F3.6 @5.4	toe stub 0.4' BK P.L
16+10	52.9 436.50 C16.4	36.5 436.5 grade	33.0 436.50 F3.5 1½:1 @5.2	T.S= 0.2' BK P.L
15+90	45.41 436.10 C18.0	36.2 436.1 C0.1	31.9 436.10 F4.2 1½:1 @6.3	T.S=1.3' BK P.L
15+70	53.5 435.10 C18.4	35.2 435.1 C0.1	30.9 435.10 F4.2 1½:1 @6.3	T.S=1.3' BK P.L
15+40	450.0 432.00 C18.0	32.7 432.4 C0.3	428.3 432.00 F3.7 1½:1 @5.5	toe-Stub =0.5 BK P.L

SPRINGFIELD (CONT.)

STA:	LT.	℄ = FINAL CHK. grade	RT	
			23.1 424.2 F1.1	P.L 2x2 = grade stub (No encroach)
17+70.34=SW PARADISE				
17+67.31 ℄		27.0 426.4 C0.6		
17+64.28=N.W PARADISE	34.89 428.00 C6.89			
17+51.12=B.V.C RT. ONLY		27.9 426.4 C1.5	25.85 425.40 C0.45	P.L stub
17+37 LT. ONLY	39.89 428.30 C11.59			
17+23 ℄		30.3 428.4 C1.9		
17+15.56 RT. ONLY			28.55 429.15 F0.60	ch+ @ P.L
16+97=B.V.C LT. ONLY	40.63 431.10 C9.53			

CHK:

STA:	LT.

430.46 = ch. NW Ly Cor. Conc Lpg @ par # 6569 Springfield

℄	RT.

ORIOLE
(SPRINGFIELD, N'LY)

Ref: DWG'S: 6338-D
6356-E-D

Note: All stubs 5' BK P.L unless noted
(HINGE-pt. 8' into ST.)

STA:	LT.	℄ = FINAL cl&k grade	RT. (E'ly)		STA:	LT.	℄	RT.	
						78.5	72.62	62.4	
					3+00 = E.V.C	372.60	372.60	372.60	Toe stub =
						C5.9	grade	F.10.2	7.3' BK P.L
								@15.3'	
T.B.M P.K NAIL Pole #666777-H 2+70 LT = 370.90									
	44.9		34.3			72.6	64.0	58.2	
0+60 = E.V.C. LT. = 9d BK RT.	338.40		338.40	Toe-stub 2' IN ST.	2+60	363.30	363.30	363.30	P.L. stub =
	C6.5		F4.1 @6'			C9.3	C0.1	F5.1 @8'	0.4' BK toe
		37.4							
0+46 = E.V.C		336.7							
		C0.7							
	41.6					67.8	57.7	49.9	
0+42 LT only	336.80				2+20 = B.V.C	357.00	357.00	357.00	Toe stub =
	C4.8					C10.8	C0.7	F7.1 @10.6	2.6' BK P.L
			33.1			61.40	52.80	46.85	
0+34 = E.V.C RT. ONLY			335.30	P.L. stub = 5' BK. Toe	1+80	352.35	352.35	352.35	P.L. = toe
			F2.2 @8'			C9.05	C0.45	F5.50 @8'	
0+32 ℄ ONLY		6.5							
		335.50							
	39.3	C1.0	32.9			56.24	48.1	44.20	
0+30 = N.L. SPRINGFIELD	336.50		334.90	P.L. stub 5' BK. Toe	1+40	347.70	347.70	347.70	P.L. stub
	C2.8		F2.0 @8'			C8.54	C0.4	F3.50 @	3' BK Toe
		35.9				50.8	43.00	36.7	
[0+00 ORIOLE = ℄ SPRINGFIELD]		335.1	= Tp. M.H		1+00	343.00	343.00	343.00	Toe stub
		C0.8				C7.8	grade	F6.3 @9.6'	1.6' BK P.L
(Stubs 5' BK P.L. unless noted)									
T.B.M			336.59 = Chiseled corner conc. Porch @ #6404 Springfield = NE'ly Springfield & Oriole						

ORIOLE (CONT.)

℄ = FINAL CHK grades

STA:	LT.	℄	RT.	
T.B.M		447.31 =	P.K NAIL Pole, LT. J-P-27074 STA 5+48' ± LT (C.H.S.)	
5+16.20 = end grading	39.8 431.40 C8.4	32.86 431.40 C1.46	29.2 431.40 F2.2 @8'	P.L. stub = 5.5 BK. Toe
5+00 = ℄ M.H	32.3 427.00 C5.3	28.18 427.00 C1.2	25.00 427.00 F2.00 @8'	P.L. stub = 4.6' BK. toe
4+50	16.7 413.40 C3.3	13.65 413.4 C0.25	10.7 413.40 F2.7 @8'	P.L. stub = 4.7' BK toe
4+00	402.0 399.80 C 2.2	99.98 399.80 C0.18	88.4 399.80 F11.4 @17.1'	T.S. = 9.1' BK. P.L.
3+50	85.5 386.20 Fa.T	86.03 386.20 F0.17	79.9 386.20 F6.3 @9.4'	T. stub = 1.4' BK P.L.

STA:	LT.	℄	RT.

SWAN
(SPRINGFIELD, N'LY)

Final grade chgs

STA:	LT.	℄	RT. (E'LY)
		2.18	
0+34 = ℄ EVC		402.20	
	394.4	F0.02	
0+25 LT. ONLY	402.40		
P.L. stub (No encroach)	F8.0 @8		
			407.35
0+23 = EVC			402.90
RT. ONLY			C4.45
		2.5	
0+17 ℄		402.90	
	394.3	F0.4	
0+10 = BVC	402.20		
LT. ONLY	F7.9 @8		
P.L. stub (No encroach)			
			406.47
0+11.99 = NE'LY			403.30
Cor. Springfield			C3.17
		253	
0+00 ℄ = BVC		402.80	
	395.1	F0.27	
0-11.99 = NW'LY	401.40		
Cor. Springfield	F6.3 @8		
P.L. stub (No encrock)			

[Note: ℄ HUB, SPRINGFIELD & ℄ SWAN = 0-32.31]

T.B.M. 405.60 = NAIL - DISC
Pole # 578863 (SE'LY SPRINGFIELD & SWAN

Ref: DWG's: 6338-D
6356-F-D

Note: Stubs 5' BK P.L unless noted (hinge-pt = 8' into ST.)

60

STA:	LT.	℄	RT
	84.2	89.07	402.97
2+50 = BVC	389.10	389.10	389.10
P.L. stub (No enchroch)	F4.9 @8'	F0.03	C13.87
	83.50	92.10	406.23
2+00	392.17	392.17	392.17
T.S = 5' BK P.L	F8.67 1½:1 @13'	F0.07	C14.06
1+88 ± = ℄ MH		92.86 392.90 = grade	
	88.2	95.13	407.38
1+50	395.20	395.20	395.20
toe-stub = 2.5' BK P.L	F7.0 1½:1 @10.5	F0.07	C12.18
	396.3	848	408.61
1+00	398.23	398.23	398.23
P.L stub (No enc)	F1.93	C0.25	C10.38
	394.92	400.25	409.01
0+70	400.05	400.05	400.05
P.L stub (No	F5.13 @8'	C0.20	C8.96
	394.9		
0+40 = E.V.C LT. ONLY	401.90		
P.L. stub (No Encroach)	F7.0 @8'		

SWAN (CONT.)

STA:	LT.	℄	RT.
5+00 E.Y.C	63.4 374.10	74.27 374.10	79.2 374.10
T.S = 8' BK P.L	F 10.7 1½:1 @16'	C 0.17	C 5.1
4+60	71.7 375.10	75.29 375.10	82.4 375.10
P.L. stub (NO ENCROACH)	F 3.4 @8'	C 0.19	C 7.3
4+40 = ℄ M.H →		75.83 376.00 = TP F 0.17	
4+20 = B.V.C.	73.0 377.30	77.77 377.30	84.2 377.30
P.L stub (No enc)	F 4.3 @8	C 0.47	C 6.9
3+85	72.6 379.90	80.13 379.90	87.7 379.90
T.S = 2.9' BK P.L	F 7.3 1½:1 @10.9'	C 0.23	C 7.8
3+50 = E.V.C	77.0 382.50	2.66 382.5	94.36 382.50
T.S = 0.2' BK P.L	F 5.5 1½:1 @8.2	C 0.16	C 11.86
3+00	78.9 386.00	85.96 386.00	400.79 386.00
Toe-stub = 2.6' BK P.L	F 7.1 1½:1 @10.6	F 0.04	C 14.79

T.B.M 378.06 = 80' NW'LY 2x2 tie to ℄ ESMT & ℄ SWAN

78.08 CAL

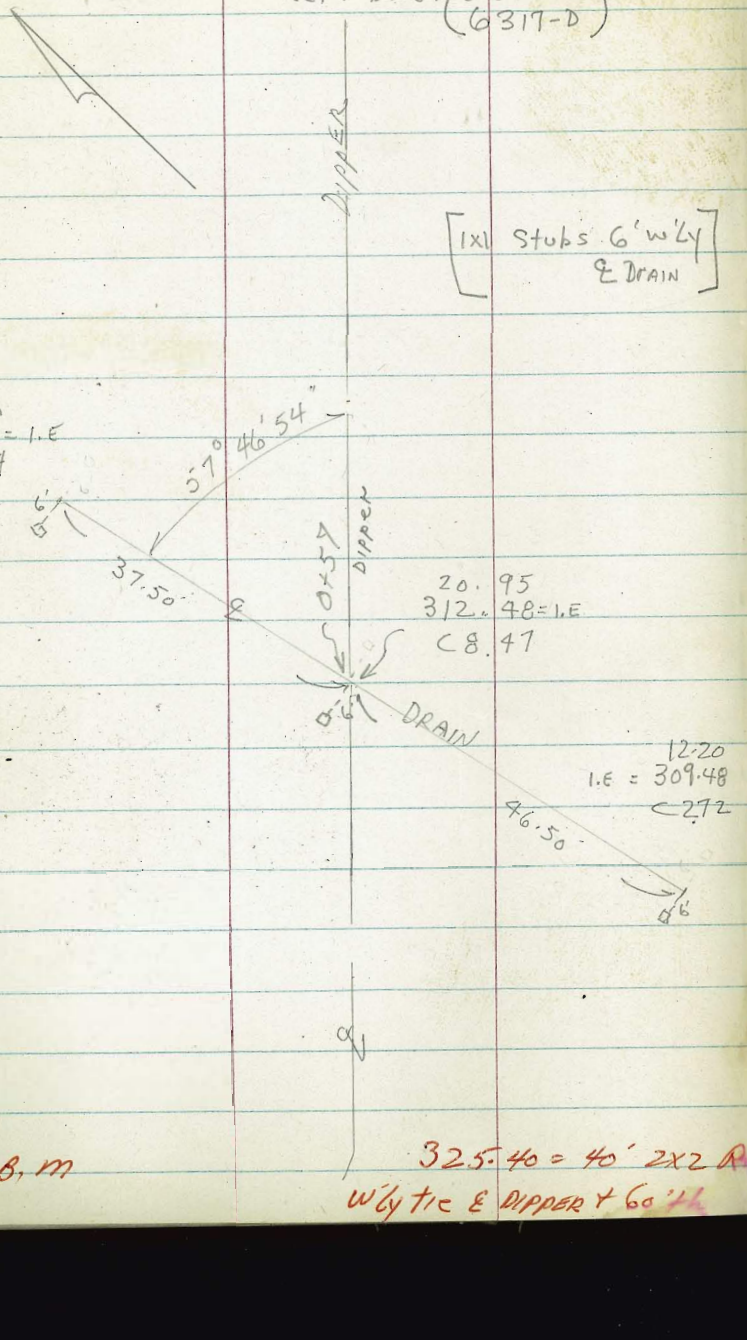
STA:	LT.	℄	RT.
P.L stub (No ench.)			
7+21.60 = end grading	94.60 394.98 F 0.38 @8'	94.98 394.98 Grade	407.1 394.98 C 12.2
7+10 = E.V.C	90.7 392.20	91.04 392.20	404.6 392.20
P.L. stub (No ench.)	F 1.5 @0'	F 1.16	C 2.4
6+70	79.9 383.80	83.5 383.80	88.15 383.80
P.L stub (NO ENCROACH)	F 3.9 @8	F 0.3	C 4.35
6+30	76.8 378.0	78.6 378.0	79 378.0
P.L stub (NO ENCROACH)	F 1.2 @8	C 0.6	C 1.0
5+81.4 = M.H →		4.76' 374.20 = TP C 0.56	
5+90	69.8 374.60	75.22 374.60	86.4 374.60
P.L. stub (NO ENCROACH)	F 4.8 @8'	C 0.62	C 11.8
(O.K. STA.)			
5+50 = B.V.C	67.1 373.70	74.33 373.7	84.1 373.70
Toe-stub = 1.9' BK P.L	F 6.6 1½:1 @9.9	C 0.63	C 10.4

STORM-DRAIN: DIPPER & STA. 0+57

10-20-60

(84"-18" Pipe + 2-Curtain Walls)

Ref: Dwg: (6330-D)
(6317-D)



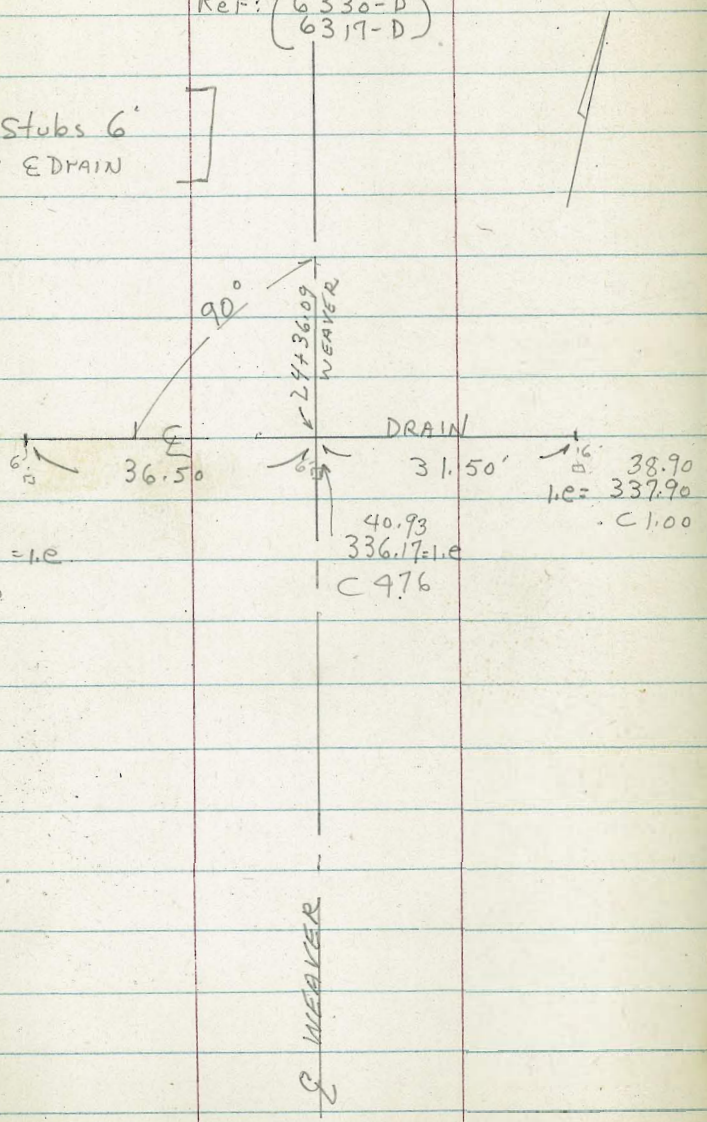
STORM DRAIN : WEAVER : STA: 24+36.09

10-20-60

(68' - 18" Pipe & 2 - Curtain Walls)

Ref: (6330-D)
(6319-D)

[1x1 Stubs 6' s/y ℄ Drain]



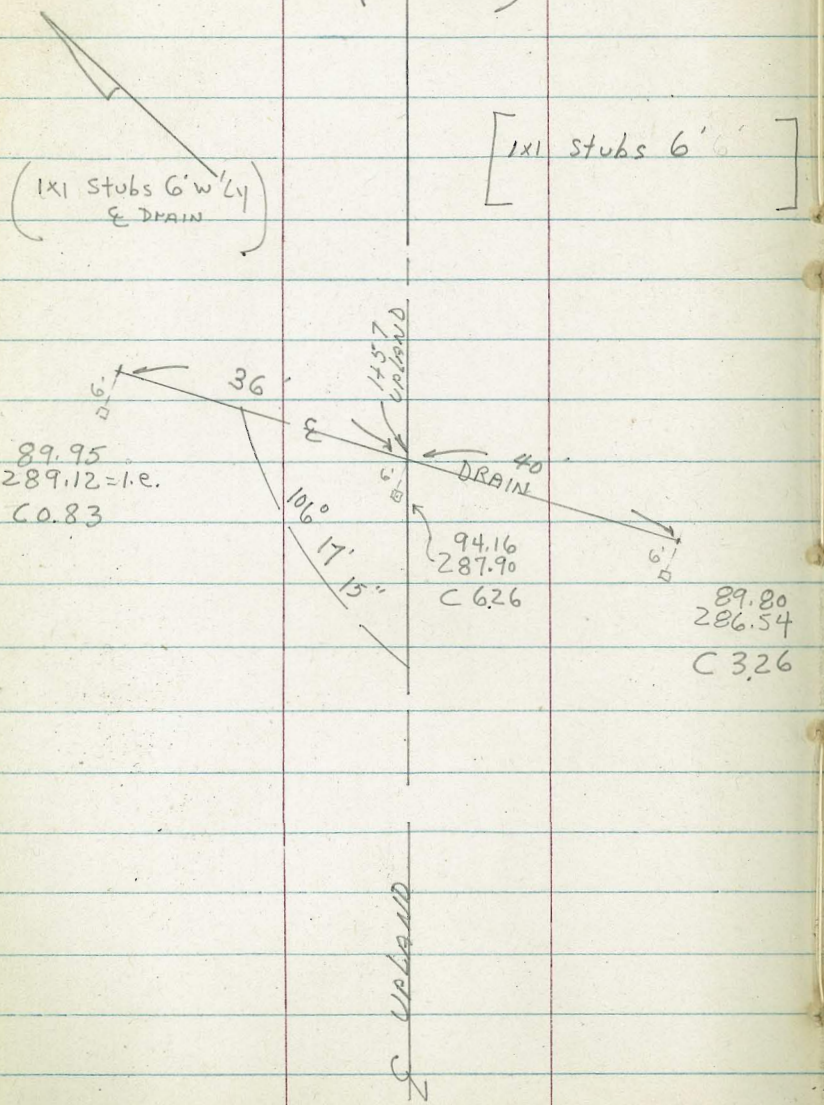
T.B.M. [redacted] 340.51 = 100' w/y R.P. Chx (Conc. Porch)
tie to w/y [redacted] mon at B.C Sta 24+65.57

DRAIN: UPLAND : STA: 1457

10-20-60

76'-27" Pipe & 2-Curtain Walls

Ref: (6329-D, 6317-D)



T.B.M.

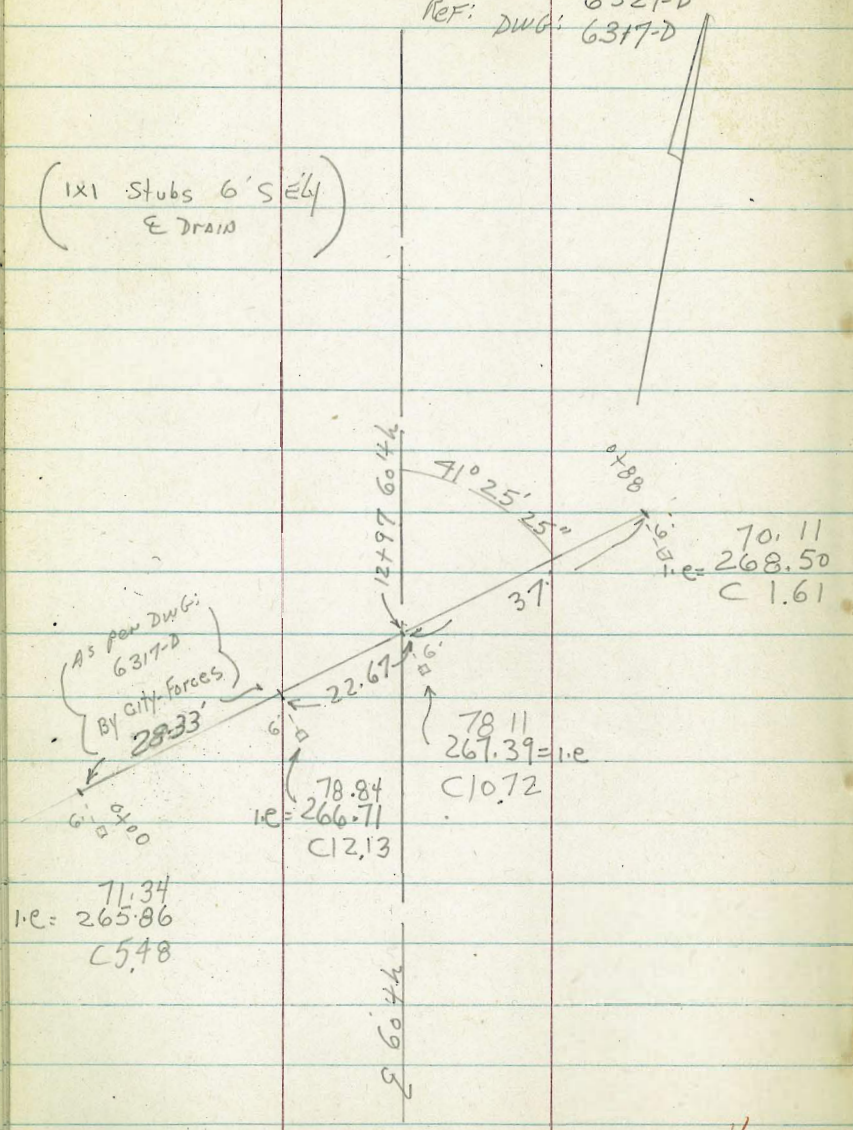
319.10 = Nail Pole # 546 [illegible] 60th St.

DRAIN: 60'h STA: 12+97

10-20-60

59.67' - 30" Pipe + 2-Curtain Walls

Ref: DWG: 6329-D
6317-D



T.B.M.

283.10 = 60' w/4 2x2 R.P.
tie ℄ 60'th. + ESMT Mon

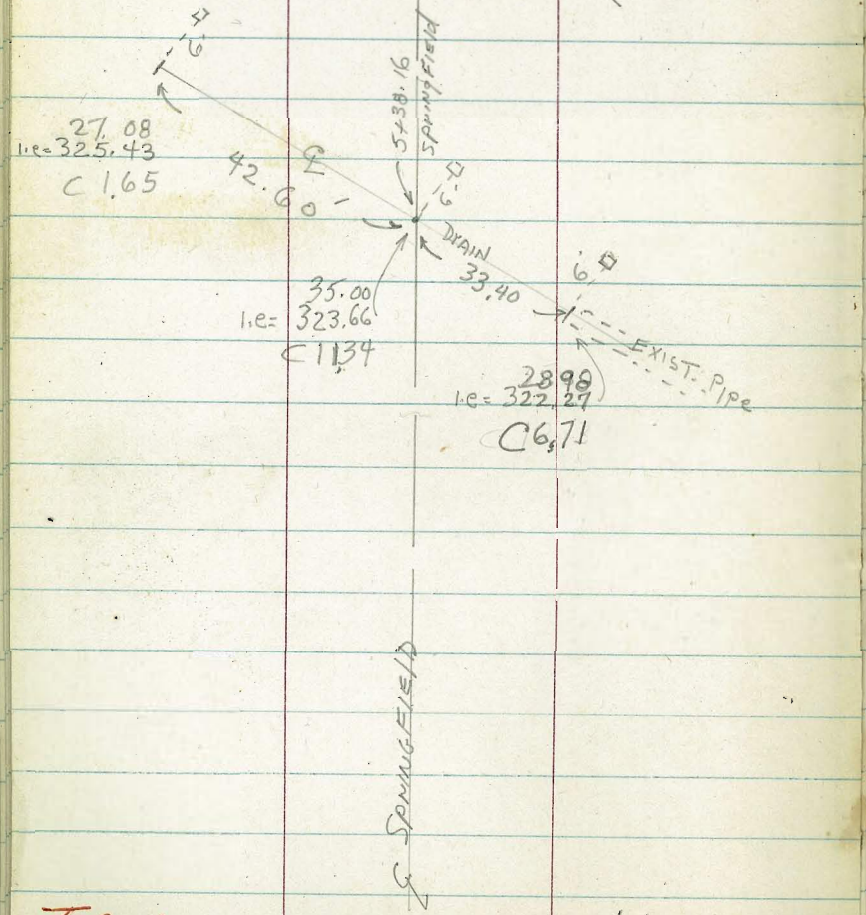
DRAIN: Springfield Sta: 5+38.16

10-20-60

76'-21" pipe - 1 coil and 1 cont.-wall

Ref: Dwgs: 6338-D
6318-D

(1x1 stubs 6' Ely ℄ Drain)



T.B.M. 336.59 = chd SEly

Corn. Conc-Porch
#640 Springfield

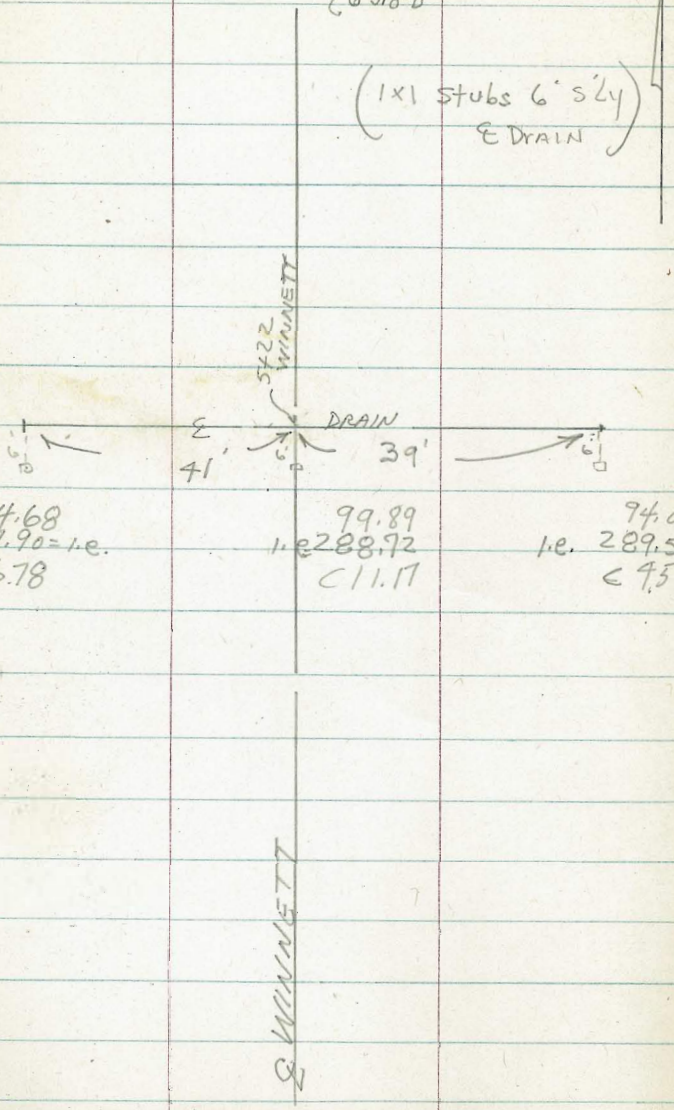
DRAIN: WINNETT : STA: 5+22

10-21-60

80' - 48" PIPE + 2-CURTAIN WALLS

REF: DWG: {6337-D / 6318-D

(1x1 Stubs 6' s'Ly @ DRAIN)



T.B.M 297.26 = Chi WAK # 6353 RADIO-PK.

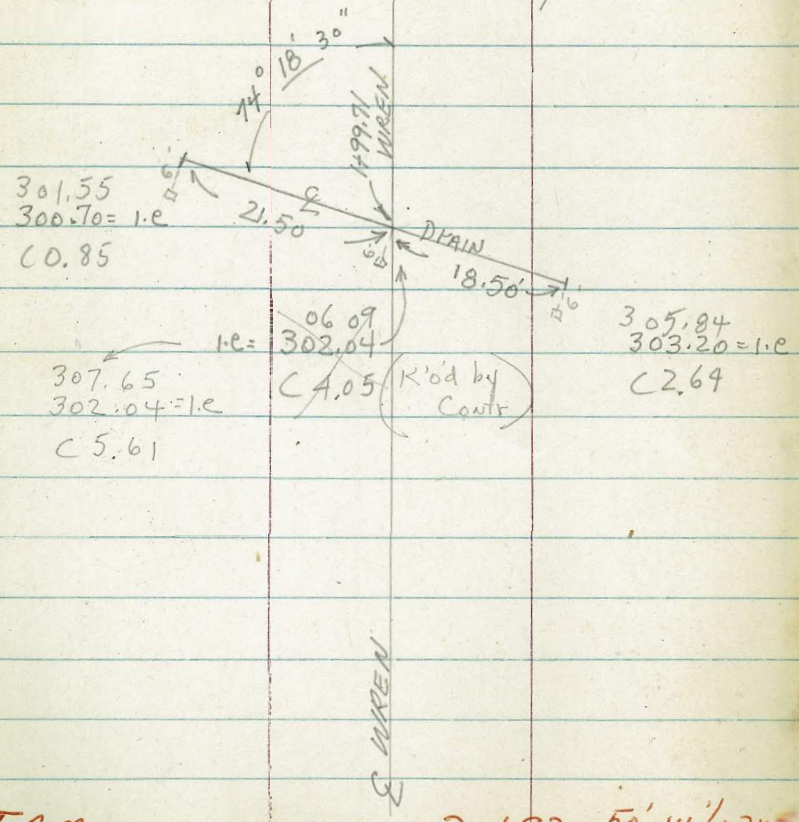
DRAIN: WREN: STA 1+99.71

10-21-60

40'-21" - Pipe & 2-CURTAIN WALLS

REF: DWG: {6334-D
{6318-D

(1x1 stubs 6' S'Ly & DRAIN)



T.B.M. 304.93 = 50' W'Ly 2x3 R.P.
tie to ℄ WREN (DWG #158)

DRAIN: 60.46 STA: 1497.09

10-21-60

48' - 21" PIPE
& 2 - CONTAIN WALLS

S'LY of FULMAR

REF: 5916-D
5918-D

1x1 stubs 6'
S'LY & DRAIN

Note: 5.32' FT. PIPE, w'ly end city Forces

℄ FULMAR ST

1497.09 60.46

12.09'

6' 5.32 20'

64.10
260.80 = I.E.
℄ 3.30

63.73
260.92
℄ 2.81

6' 20'

66.23
261.44 = I.E
℄ 4.79

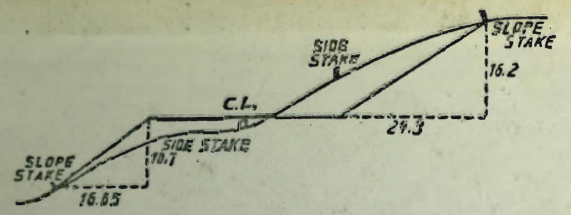
41° 24' 41° 6'

66.90
261.90 = I.E
℄ 5.00

60.46

T.B.M

272.48 = ℄ N'LY edge CON. DR. #6008 FULMAR



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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