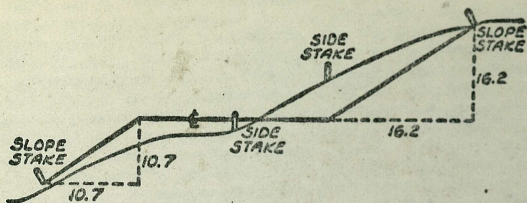


G-406



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

DIRECTIONS FOR USE OF TABLES

TABLE No. XIV

Distance of slope stake from side or shoulder
stake for any width roadway, slope 1 1/2 to 1.
If ground is nearly level the cut or fill of side
stake is located by the double entry method.

IMPROVED TABLES
AND
INFORMATION

TABLE No. VIII

To find Tangent and External for curve of
any other degree, divide by degree of curve and
add correction found in column of corrections.
Length of curve with a given I may be found
by dividing tangent (or external) opposite I by
given tangent (or external).
The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

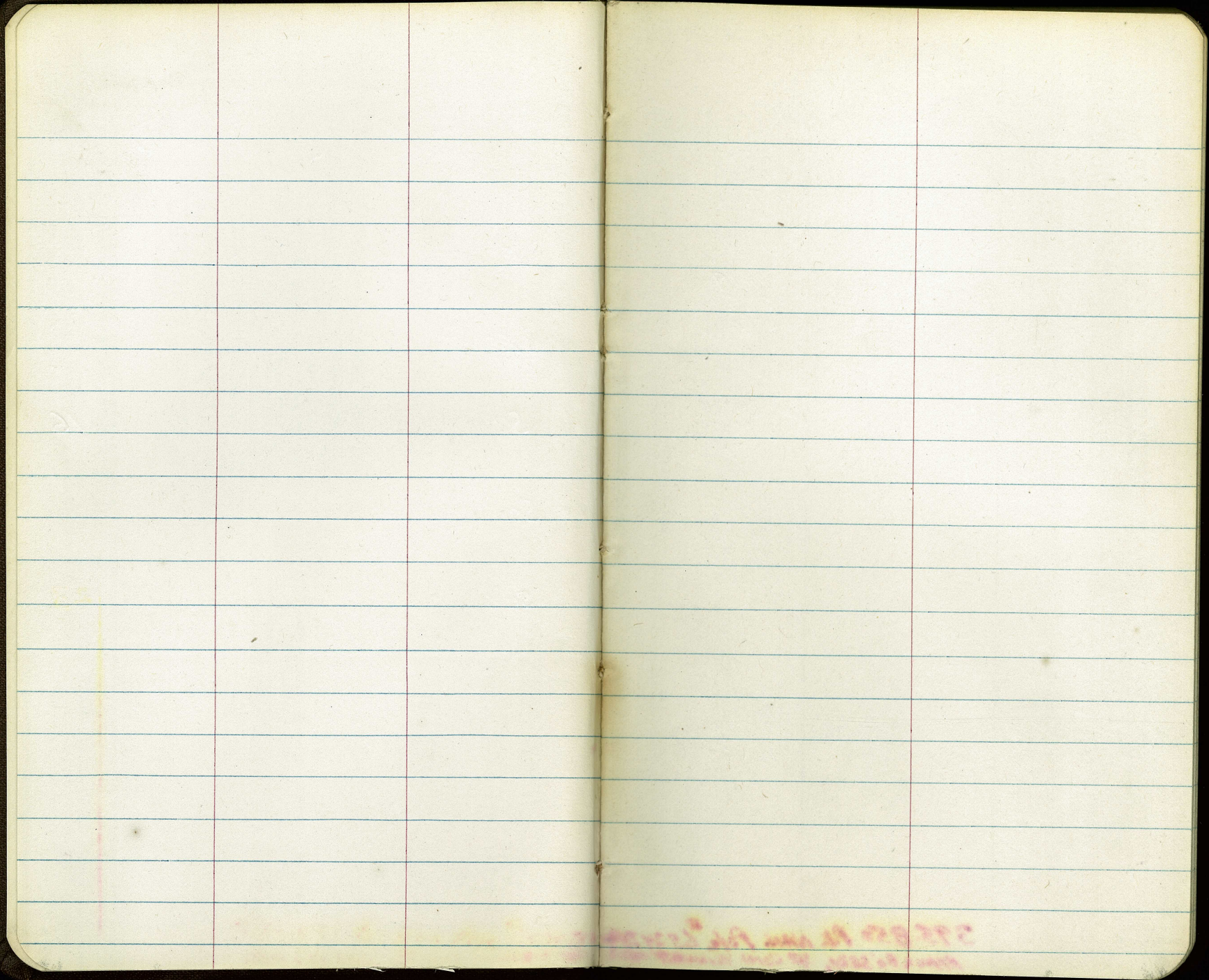
Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.58	.65	.72	.79
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.89	.99	1.09	1.20	1.31	1.42	1.54
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.037	.043	.049	.054	.060	.066
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX

TITLE	Pg.
ENCANTO: SEWERS (Conts. See Book 405)	1
EIDER: (WINNETT to KLAUBER)	1
ESMIT: (WUNDERLIN, N'ly)	6
ESMIT (M.H #165, Ely to SPARROW)	13
SCIMITAR (WINNETT, M.H #115 Ely to KLAUBER)	16
SCIMITAR (WINNETT, M.H #115, W'ly to Plug-end)	20
SCIMITAR: (Bridway N'Ely)	23



272 670 10 1000 1000 1000
1000 1000 1000 1000 1000

2-6-61

ENCANTO SEWERS: (Cont. See Book #405)
W.O. 33043

ELDER ST.
(E WINNETT TO KLAUBER)

STA:

GRADE:

0+73.60

85.32
378.06
C7.26

0+63.60

84.69
377.29
C7.40

0+53.60

84.24
376.72
C7.52

0+43.60=BVC

84.03
376.35
C7.68

0+00=M.H. #143

(See Book 405)
(Pg 20)
=5+43.76 Winnett

385.64
375.09 (out)
85.64 C10.55
386.00=TP
Fo.36 M.H.
385.64
375.59 (in)
C10.05

REF: DWG: 6337-D
6356-B-D + C-D

T.B.M. 40471 = P.K. Pole
#692854-H
Sew STA: 2450 LT.

1=29°02'35" RT.

2+50=M.H. #98
Stubs 5.15' + 10' RT
on split.

404.17
404.30=TP M.H.
FO.13

404.17
398.30=FL
C5.87

2+00

99.23
392.51
C6.72

1+50

93.33
386.71
C6.62

1+00

87.59
380.92
C6.67

0+83.60=E.V.C

86.18
379.02
C7.16

T.B.M.

395.85 = P.K. NAIL Pole #652478
Approx. 80' SE 24', SE Corn. Winnett

STUBS 5' RT (Upgrade)

1.75'

11.59'

EIDER (CONT.)

STA:

GRADE:

STA:

GRADE

4+50

417.73
411.06
C6.67

6+50

1.798

26.92
419.85
C-7.07

6+00

25.80
418.96
C6.84

4+00

6.388

414.82
407.87
C6.95

$\Delta = 37^\circ 54' 27''$ RT

423.99
418.30 = F.L.
C5.69

5+63.41 = m.H #99
stubs 5.29' + 10' RT
on split

23.99
424.30 = F.L.
F0.31 m.H

3+50

411.58
404.68
C6.90

5+50

423.61
417.44
C6.17

6.388

3+00

408.50
401.49
C7.01

5+00

421.05
414.25
C6.80

FIDER (CONT.)

STA:

GRADE:

8+50

0.40

29.69
422.58
C 7.11

8+00

29.97
422.38
C 7.59

$\Delta = 50^{\circ} 28' 36''$ LT.

29.64
422.33 FL
C 7.31

7+88.69 = M.H. #100
Stubs 5.53' + 10' RT
ON SPLIT

29.64
428.80 = TP
C 0.84 M.H.

STA:

GRADE:

$\Delta = 4^{\circ} 10' 24''$ RT.

31.67
423.22 = FL
C 8.45

10+11.53 = M.H. #101

31.67
431.71 = TP
F 0.04 M.H.

Stubs 5.00' + 10' RT.
ON SPLIT

10+00

31.49
423.18
C 8.31

7+50

1.79%

430.07
421.64
C 8.43

9+50

30.80
422.98
C 7.82

7+00

29.43
420.75
C 8.68

9+00

0.40

430.11
422.78
C 7.33

EIDER (CONT.)

STA:
 Δ = 7° 34' 10" RT
 12 + 30.69 = M.H. 102
 stubs 5.01' + 10' RT
 ON SPLIT

33.49
 433.17 = TP
 M.H.
 Co. 32

GRADE:
 33.49
 424.10 = F.L.
 C 9.39

STA:
 14 + 27.84

GRADE:
 31.30
 424.89
 C 6.41

12 + 00

33.70
 423.97
 C 9.73

14 + 00

31.49
 424.78
 C 6.71

11 + 50

33.75
 423.77
 C 9.98

13 + 50

32.24
 424.58
 C 7.56

11 + 00

0.40
 ↓

32.91
 423.57
 C 9.34

13 + 00

32.75
 424.38
 C 8.37

10 + 50

32.31
 423.37
 C 8.94

12 + 50

33.39
 424.18
 C 9.21

EIDER (CONT.)

STA:

GRADE:

T.B.M.

424.78 =

424.82 = W/Ly ch"x" on

Rim m.H @ C
EIDER + KLAUBER

= end EIDER SEW:

14 + 55.69 = M.H # 103

stops 5' + 10' RT

31.19
431.05 = TP
CO. 14 M.H

31.19
425.00 = FL
C 6.19

50.10E

2-8-61

ESMT SEW:
(Wunderlin, N'ly)

REF: DWG: 6333-D+34-D+35-D
6356-G-D + H-D

6

STA:

DATE:

STA:

GRADE:

0+59.49 = E.C

56.28
245.87
C 104.1

EQ: { -2+47.80 Ahd
2+50.34^{BF} = M.H #163
Stubs 6' + 12' LT

71.86
262.00
C 9.86

0+33.01 (mid-pt)
def. 6° 35' 43"
Ech = 26.42'

53.35
243.64
C 9.71

2+00

66.44
257.74
C 8.70

0+06.54 = B.C
 $\Delta = 26^\circ 22' 53''$
EP = 115'
T = 26.95'

8.45
Stubs 6' LT (upgrade)

249.81
241.40
C 8.41

1+50

62.15
253.51
C 8.64

0+00 = EXIST
M.H
Wunderlin

240.85 (IN)

240.35 (out)

1+00

258.97
249.39
C 9.58

T. B. M.

301.02 = P.K. NAIL Pole # 685871-H
S'ly side B'dway +
ELY 40'± ESMT

8.45

ESMT SEW: NLY (CONT.)

STA:	GRADE:
4+55.64 <i>4+35.64 = M.H. #164</i>	95.88 271.48 C 27.40
(4+43 = Beg. CONC. BK-FILL)	
4+35.64	94.41 270.56 C 23.85
3+90	82.65 268.48 C 19.17
3+40	78.28 266.20 C 120.8
2+90	274.41 263.92 C 10.49

Beg. studs 10' LT

4.52%

STA:	GRADE:
5+35.64 <i>stub 10' RT</i>	293.52 274.20 C 19.32
5+15.64 <i>NAIL 10' RT</i>	300.77 274.00 26.77
<p>Note: AT CONTRACTORS REQUEST NAILS SET 8' + 16' RT bat 90° to E ESMT.</p>	
(NAIL 8' 0" + 16' RT ON SPIIT. (NE'LY QUAD))	300.96 288.00 (w/ly IN-Bridwy) C 12.96
4+95.64 = M.H. #164 (= 4+50 Bmdway See BOOK 405, Pg I)	300.96 273.80 (IN, N'LY) C 27.16
	300.96 273.30 (out, S'LY) C 27.66
4+75.64 <i>NAIL 10' LT</i>	301.26 272.39 C 28.87

1.8%

T.B.M

293.60 = 50' 2x2 = Wly to m.H. #165
93.50

ESMT. SEW, Nly (CONT.)

8

STA:

GRADE

STA:

GRADE:

7+00

87.66
282.35
C 5.31

9+40

301.03
295.36
C 5.67

5.16 90°
STUBS 6' RT

6+50

84.54
279.77
C 4.77

8+90

98.19
292.56
C 5.63

5.594 90°

8+40

95.96
289.76
C 6.20

6+00

83.25
277.19
C 6.06

$\Delta = 15^\circ 44' 12''$ LT

7+94.10 = M.H. #166
Stubs Set 6.06' + 12' RT
ON SPLIT

93.87
287.20
C 6.67

5+55.64 = M.H. #165
= 0+00 Ely ESMT
Stubs 8' + 12' RT
@ 90°

282.75 282.75
274.90 (in) 274.40 (out)
C 7.85 C 8.35

7+50

290.30
284.93
C 5.37

5.16 90°

(5+46 = end CONC-ENC.)

T.B.M

312.36 = NAIL to 4"x4" Fence-Post
70' LT Sta 11+00

ESMT, N'y (CONT.)

STA:

GRADE:

STA:

GRADE:

13.62
308.92
C 4.70

12+00

13.49
308.06
C 5.43

11+90

13.95
307.45
C 6.50

11+80

15.12
307.10
C 8.02

11+70 = B.V.C.

11+40

16.44
305.86
C 10.58

11+00

14.03
303.79
C 10.24

10+60

11.50
301.73
C 9.77

10+20

308.46
299.66
C 8.80

P.O.T

9+80 = M.H #166-A

304.58
297.60
C 6.98

$\Delta = 97^{\circ} 59' 05''$ LT.

11+62.35 = M.H #167
Stubs 9.14' + 18' RT
on split

3 17.89
307.02
C 10.81

5.166 80
|
|
|

ESMT, N'ly (CONT)

STA: GRADE:
 $\Delta = 108^\circ 59' 24''$ RT
 EQ } $\left. \begin{array}{l} = 11 + 94.74 \text{ Ahd} \\ 12 + 85.35 \text{ Bk} \end{array} \right\} = \text{M.H. } 167.7 \text{ A}$
 stubs set to 33' RT & 10.33' LT
 (ON split) grade stub on RT.
 Line-only, stub LT.

P.O.T #
 $14 + 03.77 = \text{M.H. } 168$
 stub 6' LT.
 32.22
 324.27
 C 7.95

13 + 75
 31.83
 324.15
 C 7.68

12 + 50
 23.73
 316.79
 C 6.94

13 + 25
 34.29
 323.95
 C 10.34

12 + 30 = E.V.C.
 18.04
 313.03
 C 5.01

12 + 75
 34.75
 323.75
 C 11.00

12 + 20
 16.11
 311.41
 C 4.70

12 + 10
 314.64
 310.04
 C 4.60

12 + 25
 332.60
 323.55
 C 9.05

0.4

Big stubs 6' LT

ESMT SEW, N'ly (CONT.)

STAI	GRADE
15+00	32.43 327.02 C 5.41
14+90	31.42 326.03 C 5.39
14+80	30.55 325.28 C 5.27
14+70	29.90 324.77 C 5.13
14+60 = B.V.C	29.60 324.49 C 5.11
14+30	332.07 324.37 C 7.70

6' RT
← 8.9' stubs

0.4' RT
← End stubs 6.4'

STAI	GRADE
M.I.H + 18.65' N'ly = plug-end	45.92 334.75 = F.L. C 11.17
Note: CONT. ON LINE OF BK. Tang. 18.65' to D. end	
A = 89° 57' 40" RT 15+44.74 = M.I.H #769 Stubs 8.48' + 15' RT ON SPLIT	40.47 333.88 (OUT) C 6.59
	40.47 334.38 (IN) C 6.09
15+20 = E.V.C	35.33 329.69 C 5.64
15+10	333.63 328.24 C 5.39

ESMT, Sew, n'y (cont.)

STA:	GRADE		
16+00	48.68 337.82 C 8.86	T.B.M	375.08 = 375.00 = NAIL Pole #270920
			STA: 8+75 75' LT WREN
15+90	47.69 337.27 C 8.42		
15+80	46.43 338.49 C 7.94	17+54.74 = M.H #170 Stubs 6'4 1/2' RT	54.53 341.60 C 12.93
15+70	44.50 337.48 C 7.02		50 1.0
		17+10	46.31 341.15 C 5.16
15+60	342.72 336.24 C 6.48		
		16+60	49.34 340.65 C 8.69
15+50 = B.V.C (could not set)	334.77		
		16+10 = E.V.C	349.29 340.15 C 9.14

ESMT [M.H #165 (N'y B'dwy) E'y
to SPARROW]

REF: 6334⁺5-D
6306-H-D

STA: GRADE:
2+00 88.11
277.04
C11.07

STA: GRADE:
4+00 93.91
286.86
C7.05

1+50 82.70
276.50
C6.20

3+50 91.14
284.25
C6.89

1+00 80.76
275.97
C4.79

107.8
↓
Stubs 6' RT

3+00 88.67
281.64
C7.03

5-222.88
↓

0+50 80.55
275.43
C5.12

2+50 86.78
279.03
C7.75

0+00 = M.H #165 274.90(out) 274.90 (IN)
(= 5+55.64 ESMT N'y)
(See Pg 8)

P.O.T.
2+15 = M.H #172 288.03
Stubs 6' + 12' RT 277.20
C10.83

T.B.M. 293.60 = 50' wly 2x2 tie to
M.H #165

T.B.M.

304.93 = wly 2x2 (line-tie) to
E WREN + E ESM.T.

14

STA:

GRADE:

STA:

GRADE:

6+50

5-5438

05.93
300.74
C5.19

9+00.14=M.H #173

25.73
314.60
C11.13

6+00

304.61
297.97
C6.64

8+50

18.87
311.82
C7.05

A=15° 41' 30" LT.

5+50.14 = M.H 158
(= 0+00 WREN
see Book 405 - pg 22
stubs 6.06' & 12' RT
ON SPLIT

307.23
295.20 (in) C12.03
307.23
294.70 (out) C12.53

8+00

5-5438
Stubs 6' RT top grade

13.76
309.05
C4.71

5+00

5-2228

298.73
292.08
C6.65

7+50

311.35
306.28
C5.07

4+50

296.51
289.47
C7.04

7+00

309.09
303.51
C5.58

ESMT. M.H. #165, Ely (CONT)

STA:	GRADE:
10+90	34.04 328.30 C 5.74
10+80 = B.V.C.	33.54 327.38 C 6.16
10+50	32.10 325.25 C 6.85
10+00	30.08 321.70 C 8.38
9+50	327.84 318.15 C 9.69

7.105

T.B.M

35226 = 33' Wly chx tie 15
TP. Wly INLET-SPARROW

STA:
(For SPARROW See Book 405-Pg. 45)
Δ = 90° LT-SPARROW

GRADE:

11+80.60 = M.H. #174	52.51	52.51
Stubs Set 8.48' + 15' RT ON SPIT (S.E. QUAD)	343.40 (IN)	342.90 (OUT)
(= 0+00 SPARROW Sew.) See Book 405-Pg 45	C 9.11	C 9.61

11+50	41.94 337.55 C 4.39
11+20.00 = E.V.C.	36.72 332.30 C 4.42
11+10	35.56 330.76 C 4.80
11+00	334.42 329.43 C 4.99

17.498

2-14-61

SCIMITAR: (WINNETT
M.H. #115, ELY to KLAUBER)Ref: 6333-34-D
6356-AD

16

STAI	GRADE:	STAI	GRADE
2+00	94.70 383.72 C10.98	4+00	403.25 394.59 C 8.66
1+50	92.30 382.04 C10.26	3+50	401.36 391.09 C10.27
1+00	90.24 380.36 C 9.88	3+00	98.80 387.59 C11.21
0+50	89.85 378.68 C11.17	2+85.99 = M.H. #116 Stubs 6.03' + 10' RT. ON SPLIT	97.71 386.61 C11.10
0+00 = M.H. #115 E WINNETT (See Book 405-Pg 20)	390.31 376.50 (out) C13.81	2+50	96.75 385.40 C11.35

3.36 88
Stubs 6' RT88
70

T.B.M. →

P.K.
395.85 = NAIL Pole # 65247 B-H
60' SEBY OF NE cornd. Winnett + Scimitar

SCIMITAR, (WINNETT, ELY, -CONT.)

T.B.M

419.63 = ch^o TP. w^o 17
end BIK-Wall approx 35'
s'ly of m.H #118

STA: GRADE
6+00 414.97
407.87
C 7.10

STA: GRADE
8+00 25.35
414.92
C 10.42

$\Delta = 28^{\circ} 05' 43''$ LT
5+86.18 = M.H #117
Stubs 6.18' + 10' RT.
ON SPLIT

413.85
407.62
C 6.23

7+50

423.75
412.03
C 11.72

5+50

411.13
405.09
C 6.04

$\Delta = 18^{\circ} 40' 23''$ LT.
7+14.79 = M.H #118
Stubs 6.08' + 10' RT
ON SPLIT

422.42
410.00
C 12.42

5+00

07.60
401.59
C 6.01

7+00

421.78
409.72
C 12.06

4+50

405.19
398.09
C 7.10

6+50

419.12
408.80
C 10.32

SCIMITAR (WINNETT, ELY - CONT.)

STA:

10+00

Stub 6' LT. here

GRADE

32.75
420.43
C12.32

9+50

0.40

31.14
420.23
C10.91

9+00

29.35
420.03
9.32

$\Delta = 40^{\circ} 04' 04''$ RT.

8+87.69 = M.H. #119
Stubs 6.39' + 10' RT
ON SPLIT.

28.65
419.98
C 8.67

8+50

427.13
417.80
C 9.33

T.B.M. ELEV = 427.42

STA:

(11+95.63 = chimney LT.)

$\Delta = 24^{\circ} 10' 04''$ LT.
11+68.63 = M.H. #120
Stubs 6.14' + 15' RT
ON SPLIT.

11+50

35.33
421.10
C14.23

35.25
421.03
C14.22

11+00

0.40

34.92
420.83
C14.09

(10+77.63 = chimney LT.)

10+50

Stub 6' LT here

33.72
420.63
C13.09

SLY/18
= 59.95' CHX-TIE
to M.H. #119 ON CONC.
D.R. @ 6491 SCIMITAR

SCIMITAR (WINNETT, Ely- CONT.)

T. B. M

428.95 = NAIL Pole
 #JP 171024
 APPROX 80' Ely OF
 S.E. CORN. KLAUBER
 & SCIMITAR

STA:
 = Ely end sewer.

GRADE
 34.03
 422.00
 C12.03

13+94.61 = M.H. #121
 Stubs 6 + 10' RT.

13+50

34.58
 421.83
 C12.75

13+00

34.90
 421.63
 C13.27

(12+95.61 = chimney ^{LT.} _{ST.})

12+50

0.7
 |
 1

35.21
 421.43
 C13.78

12+00

35.24
 421.23
 C14.01

SCIMITAR: (WINNETT, M.H. #115)
(WY to Plug-end)

Ref: 6332-33-D
6356-D

20

STA:

grade:

STA:

GRADE

1+20

90.53
384.10
C 6.43

$\Delta = 34^{\circ} 32' \text{LT}$
2+87.01 = M.H. #113
STUBS 6.28' + 12' RT
ON SPLIT

400.31
388.00
C 12.31

0+80

5.928
STUBS 6' RT

90.01
381.74
C 8.27

2+50

1.488

96.99
387.45
C 9.54

0+40

390.11
379.37
C 10.74

2+00

93.60
386.71
C 6.89

0+00 = M.H. #115
(WINNETT & SCIMITAR)
(See pg. 16)

(OOT) 390.31 390.31
376.50 377.00 (INS)
C 13.81 C 13.31

$\Delta = 27^{\circ} 41' 08'' \text{LT}$
1+52.01 = M.H. #114
STUBS 6.18' + 12' RT
ON SPLIT

91.54
386.00
C 5.54

390.31
390.10 = TP
C 0.21

T.B.M

395.85 = P.K. NAIL IN
Pole # 652478-H = 60' ± SEELY
OF NE CORN. SCIMITAR & WINNETT

SCIMITAR (WINNET, W'ly - CONT.)

412.44 ^{NOIL} Pole

21

STA:	GRADES:
5+00	407.26 400.74 C 6.52
4+50	405.25 399.75 C 7.50
4+00	403.34 394.76 C 8.58
3+50	402.15 391.77 C 10.38
3+00	400.76 388.78 C 11.98

5+98.00

STA:	GRADE
6+50	415.22 406.92 C 8.30
6+00	412.40 406.18 C 6.22
P.O.T.	411.81 406.00 C 5.81
5+87.99 = M.H. #112 Stubs 6+12' RT	
5+50	409.88 403.73 C 6.15

1.483

5+98.00

SCIMITAR - (WINNETT, W. Va. - CONT.)

STA:

Δ = 35° 47' 54" RT.
 8+91.40 = M.H. III
 Stubs 6.30 + 16' RT
 on split

GRADES:

26.82
 410.50
 C 16.32

STA:

GRADES:

(8+59 = Beg Conc BK-Fill)

8+50

24.30
 409.89
 C 14.41

8+00

21.77
 409.15
 C 12.62

7+50

20.48
 408.41
 C 12.07

9+59.40 = Plug-end

29.49
 418.00
 C 11.49

7+00

17.90
 407.66
 C 10.24

9+25.40

28.18
 414.25
 C 13.93

(9+13 = end Conc. BK-Fill)

3-1-61

SCIMITAR: (Bridway NEly)Ref: 6332-33-D
6356-D

23

STA:

1+50

GRADES:

77.12
366.32
C 10.80

STA:

3+00

GRADES:

89.12
380.03
C 9.09

1+00

70.93
361.64
C 9.29

2+50

84.23
375.57
C 8.66

9.3570

0+50

63.56
356.97
C 6.59 $\Delta = 76^{\circ} 29.5' RT$ 2+32.42 = M.H. #106
stubs 7.64' + 12' RT
ON SPLIT82.45
374.00
C 8.45Set T.B.M.363.18 = 2" Pipe 27.90' RT
M.H. #105 = 0+000+00 = M.H. #105
stubs 6' + 12' RT359.10
352.30 = PLAN
C 6.8 ±

2+00

81.81
371.00
C 10.81Set T.B.M.333.38 = 37' chx tie to
& LTT Bridway + 63' rd ON SE'ly CB RT.

T.B.M.

332.85 = E LTT Bridway +
63' rd

SCIMITAR (Brdwy NELY)
CONT.

24

STA.

5+00

GRADE
404.62
395.17
C 9.45

STA:

6+50

GRADE:
12.05
403.49
C 8.56

4+50

401.39
391.69
C 9.70

70

3.445

6+00

08.82
401.77
C 7.05

4+00

97.10
388.21
C 8.89

$\Delta = 75^\circ 28.3' RT$

3+62.54 = M.H. 107
Stubs 7.59' + 12' RT

93.63
385.60
C 8.03

P.O.T.

5+89.42 = M.H. 108 #
Stubs 6' + 12' RT.

08.41
401.90
C 7.01

3+50

393.18
384.49
C 8.69

5+50

407.08
398.65
C 8.43

SCIMITAR (Roadway NELY)
CONT.

25

STA:	GRADE
$\Delta = 34^\circ 12.4' \text{ LT}$ = Beg. CONC. AR-Fill # $8+12.65 = \text{M.H. 109}$ Stubs 6.28' & 12' RT ON SPLIT.	24.51 409.09 C15.42
8+00	23.81 408.65 C15.16
7+50	19.64 406.93 C12.71
7+00	16.01 405.21 C10.80

3.475 000

STA:	GRADE:
10+00	25.29 409.84 C15.45
(9+55.78 = chimney LT.)	
9+50	25.64 409.64 C16.00
9+00	26.72 409.44 C17.28
8+50	25.44 409.24 C16.20
(8+31.65 = chimney LT.)	

0.708

SCIMITAR (Bridway N'Ely)
CONT.

STA:

GRADE:

T.B.M

= 427.27 = 35' chx on

CONC. DR. @ 6320 Scimitar =
NW'ly tie to M.H # 110

= end CON. BK. Fill

10 + 38.81 = Plug-end

25.05
410.00
C15.05

0.409
↓

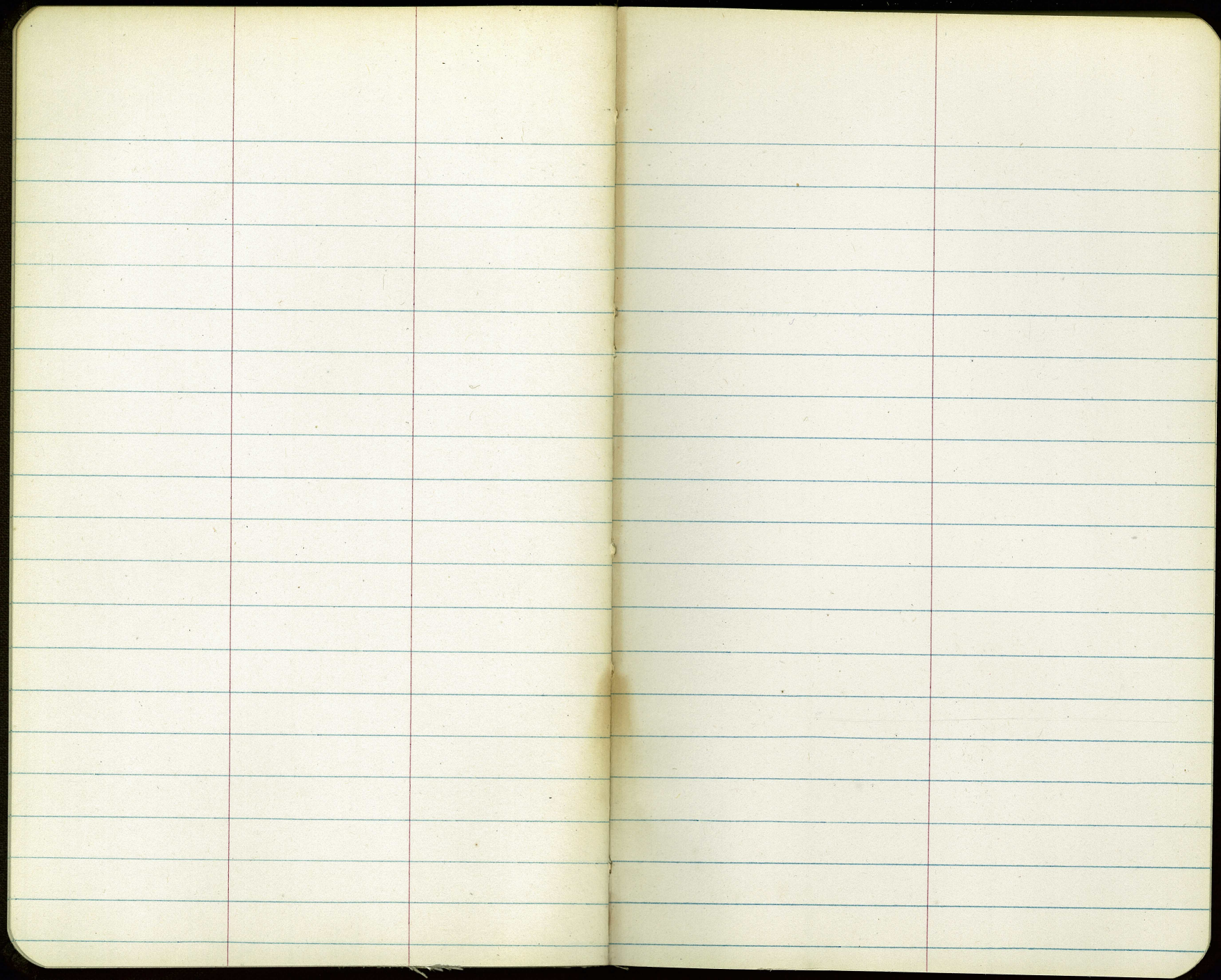
$\Delta = 29^\circ 39.4' RT$

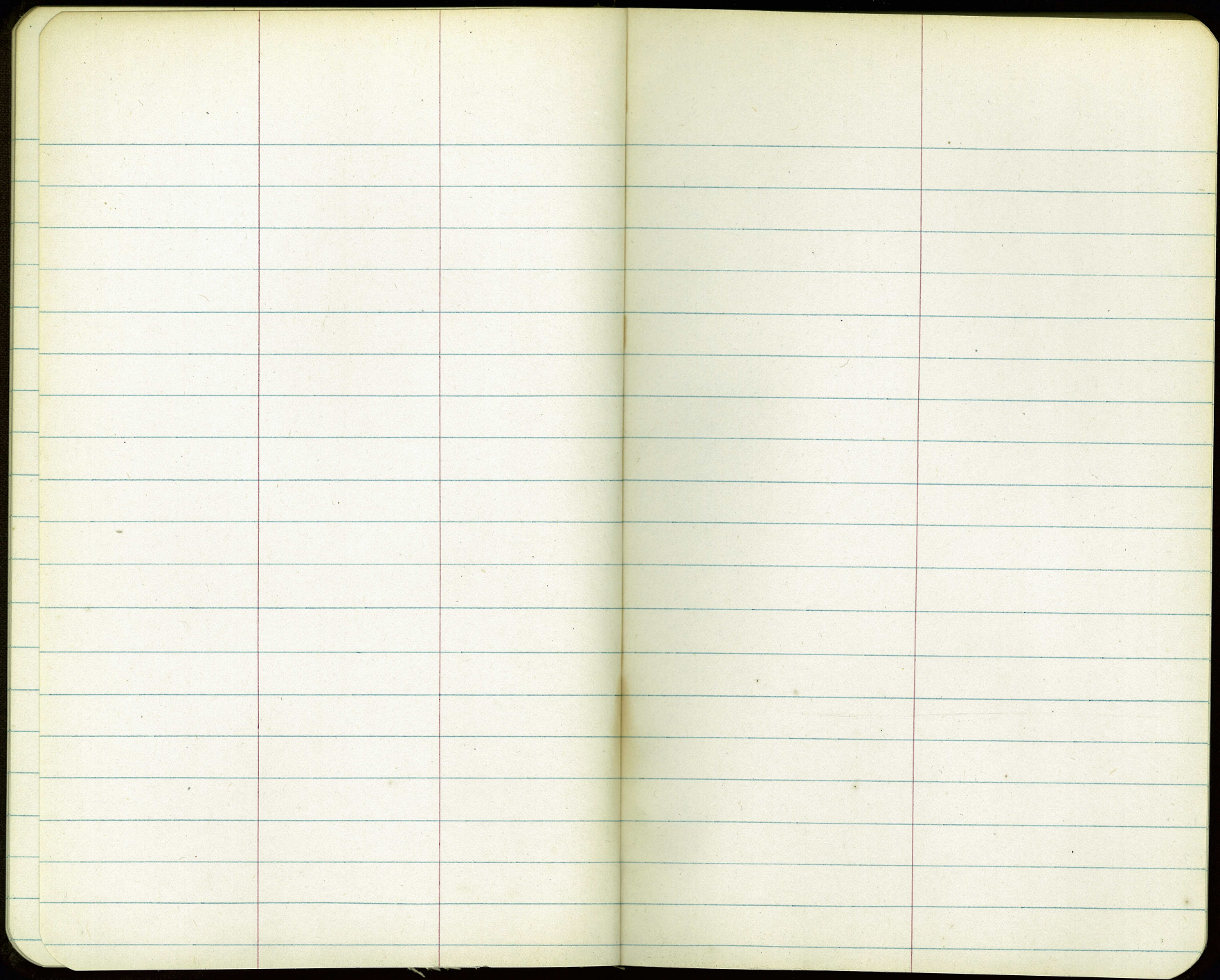
10 + 06.78 = M.H # 110

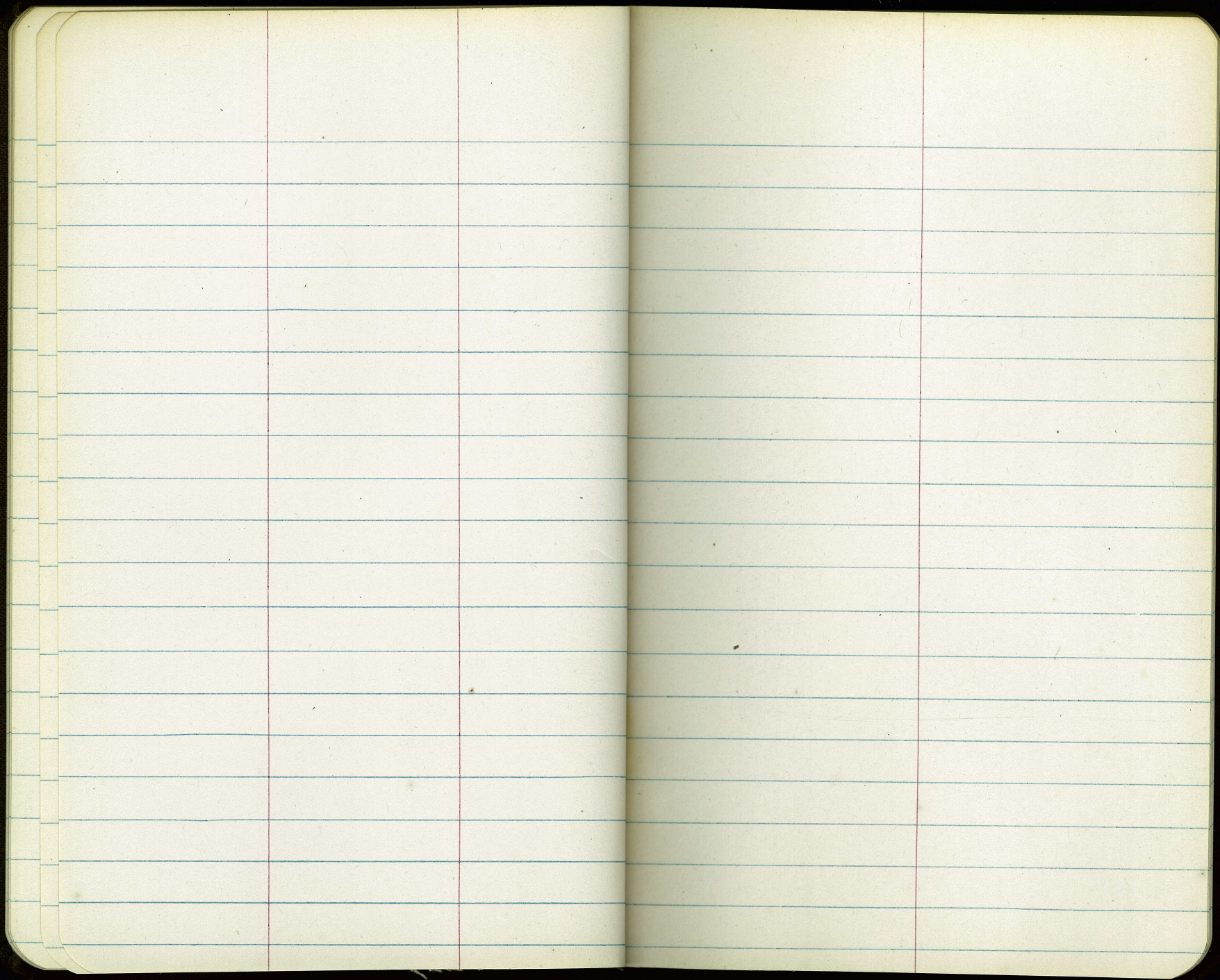
Stubs 6.20' + 12' RT
ON SPHT

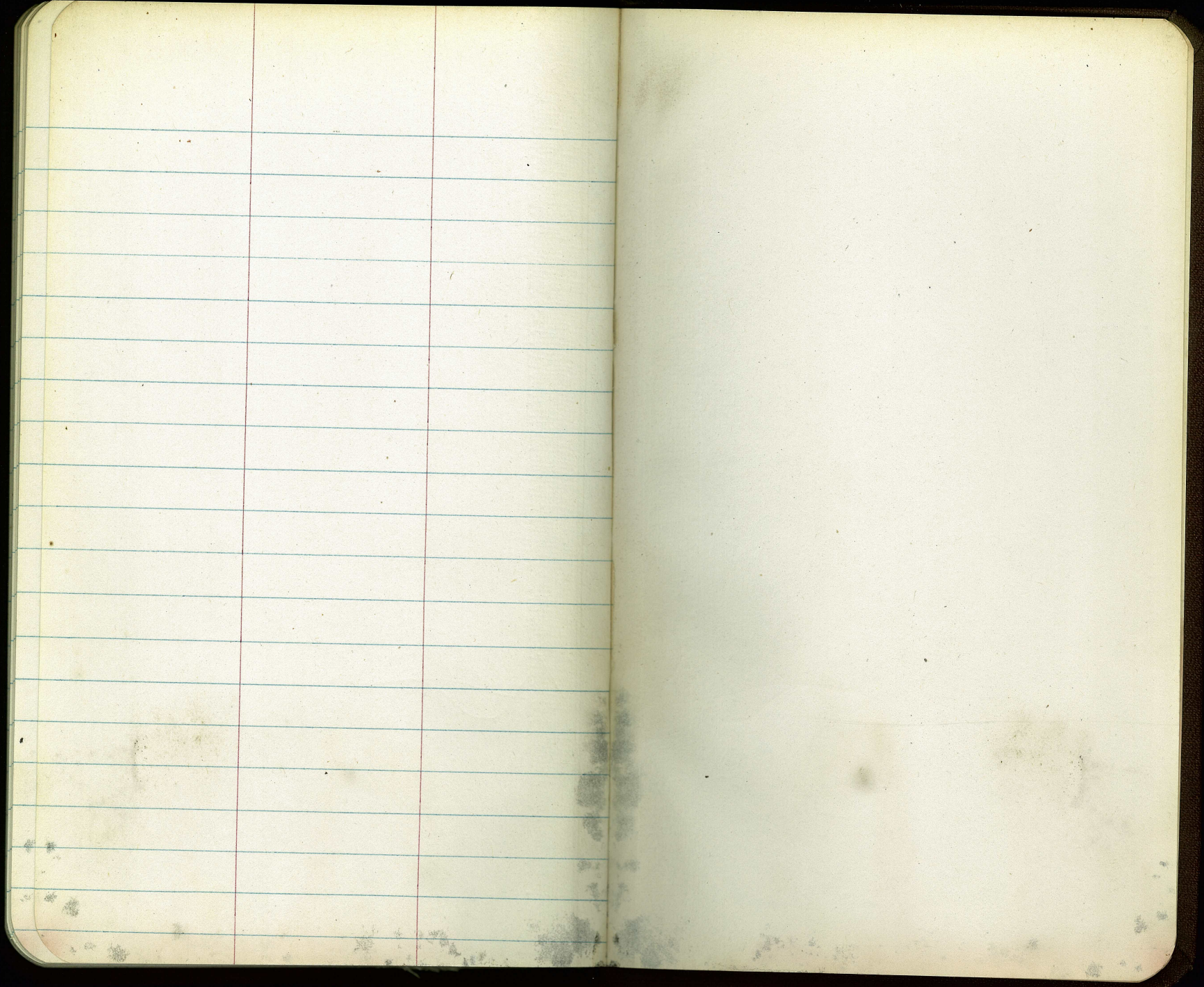
425.30
409.87
C15.43

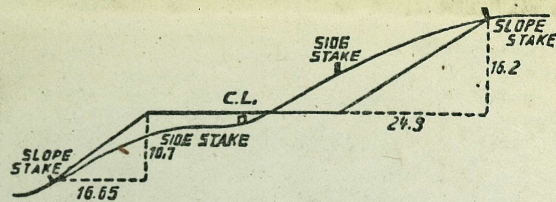
27.











DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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