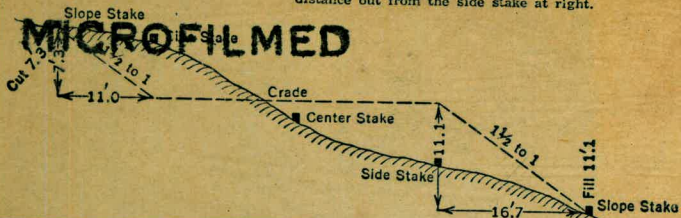


NOTE
LEVEL BOOK
W. B. A.

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 Roadway of any Width. Side Slopes 1½ to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	Distance out from Side or Shoulder Stake										Cut or Fill
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

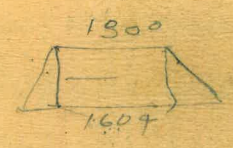
KEUFFEL & ESSER CO., N. Y.

477° 32' 56" W
 D.I.P.F. 145.662110+00

30 28 30
 30 28 30
 60° 57' 00"

91.50 - 16° 17' 00" } 95989
 90.85 - 14° 41' 00" } 96734

BOOK No. 14



The paper in this book No. 373A
 is made of 50% high grade rag stock
 with a WATER RESISTING surface sizing.

R

8

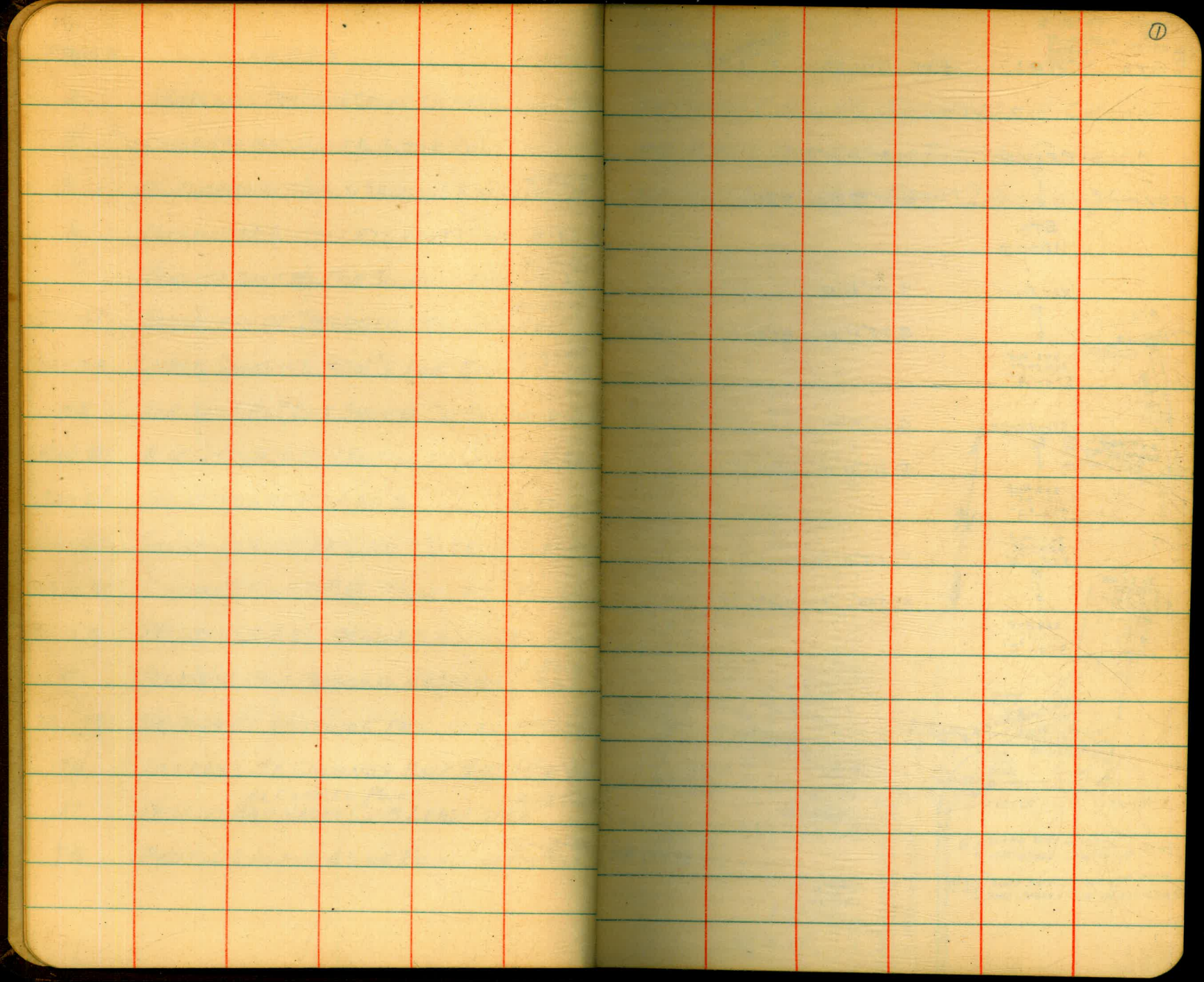
35-70
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12-24

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33
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35
36
37
38
39
40

PAGES	INDEX	DATE
2	SHORELINE TRAVERSE CROWN PT. AREA	4-18-47
3	CAUSEWAY BASELINE E. SIDE & N.W. LY	4-21-47
4	B/L FOR PROJECT NO. 8, X-SECTION E. OF CAUSEWAY	4-25-47
6	LOCATION OF SEXTANT PTS VENT & DUNE	4-30-47
7	VENTURA DUNE B/L FOR SOUNDING PROJ. NO. 7	5-7-47
9-41	SOUNDINGS OF DREDGED AREA PROJ. NO. 7	5-19-47
42-44	CHECK SOUNDING PROJ.'S FOR RUNOUT	6-9-47
45	SURVEY OF P.L. # 205 SHOWING CITY AC. LAND	6-12-47
46-49	Δ OF CITY ENGR MAN FAMOSA & A CHURCH	6-20-47
50-61	SOUNDINGS OF PROJ. NO. 8	6-27-47
62-63	SOUNDINGS OF PROJ. NO. 7 D. BASIN	7-2-47
64-66	FINISHED FILL X-SEC. PROJ. NO. 7	7-19-47
66-70	PROGRESS X-SEC. PROJ. NO. 8	7-14-47
71	TRAVERSE FROM FAMOSA TO N.E. COR. BIK NO. 28	7-30-47
72-75	DE-ANZA PT. BASELINE PROJ. NO. 3-1	8-20-47
76	SEXTANT PT. CHIMNEY BACK BAY	11-9-47
77	EL CARMEL POINT MISSION BAY YACHT CLUB LEASE AREA	4-22-48
78	PROFILE ALONG E. SIDE PAL HI-WAY PROJ. #3,1	6-18-48



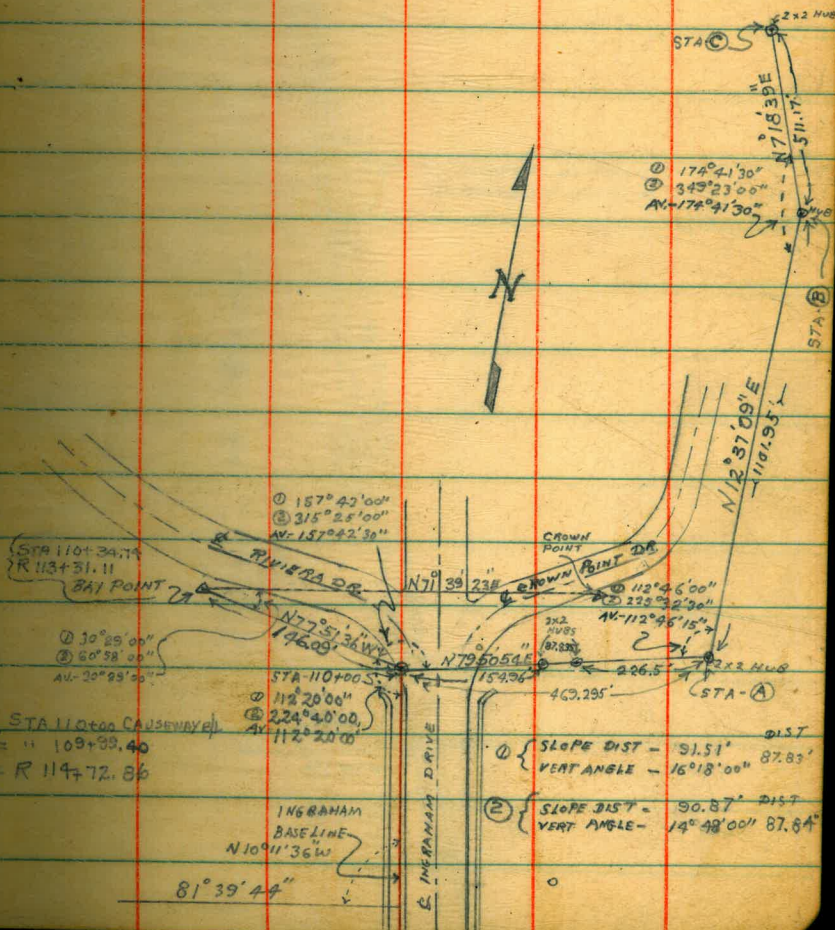
4-22-47 CLEAR
BARRAGAN
SHERRY
STANLEY
MEAN
SLIGHT WIND

Indexed

4-18-47 CLEAR
BARRAGAN
SHERRY
STANLEY (2)

STA	OBJ.	SIX ANGLES	MEAN
	CROWN R ↓	① 30°29'00"	
BAYPT		② 60°58'00"	30°29'00"
	STA 110+00		
	BAY POINT R ↓	① 157°42'00"	
STA 110+00		② 315°25'00"	157°42'30"
	2x2 HUB 469.295' STA-"A"		
	STA-110+00 R ↓	① 112°46'00"	
2x2 HUB 469.295' STA-"A"		② 225°32'30"	112°46'15"
	2x2 HUB 1101.95' STA-"B"		
	2x2 HUB 469.295' STA-"A"	① 174°41'30"	
2x2 HUB 1101.95' STA-"B"		② 349°23'00"	174°41'30"
	2x2 HUB 511.17' STA-"C"		

TRAVERSE ALONG SHORELINE CROWN
PT. AREA FOR CROSS SECTION CONTROLS
OF PROJECT NO. 8 E. OF CAUSEWAY



CORRECTED
= " 109+89.40
= R 114+72.86

① SLOPE DIST - 91.51' DIST
VERT ANGLE - 16°18'00" 87.83°

② SLOPE DIST - 90.87' DIST
VERT ANGLE - 14°48'00" 87.84°

4-21-47

cloudy

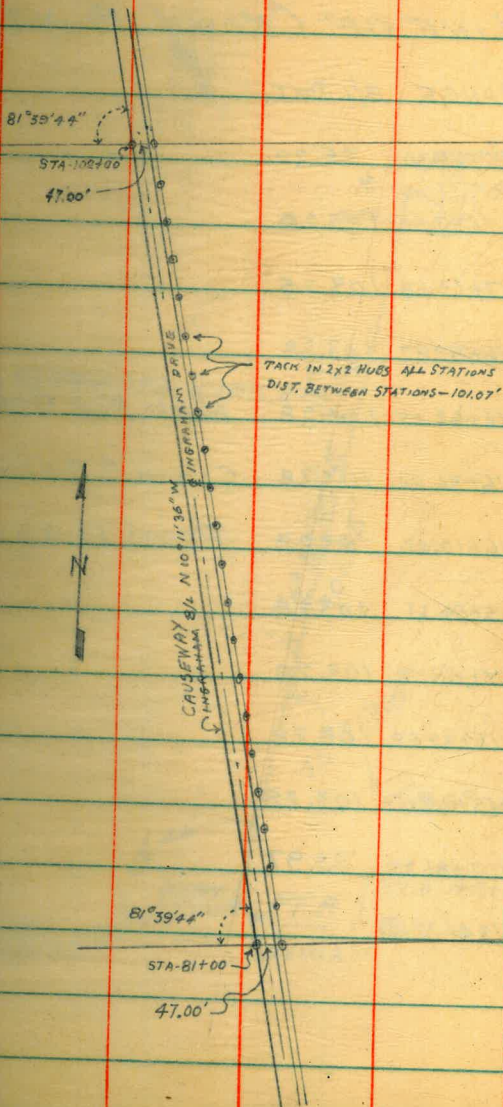
windy

(3)

CAUSEWAY
~~INFORMATION~~

EAST
B/L OFFSET - STATIONS 81+00 TO 102+00

Subsequent



BASELINE LAYOUT FOR
PROJECT NO. 8. X-SECTIONS
ALONG THE SOUTHERLY SHORE
LINE OF CROWN POINT

Indexed

4-25-47

(7)

THOMAS A STAMPER

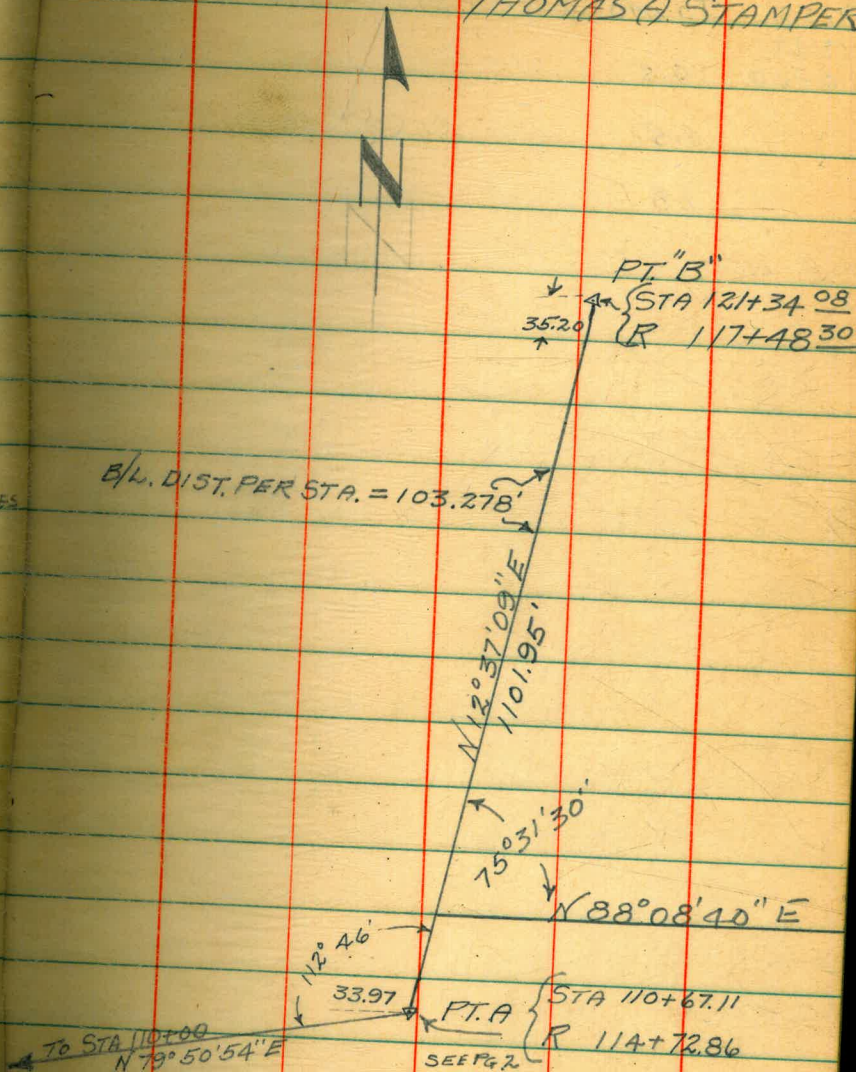
STA.	RANGE	B/L DIST.
PT. B" 121+34 ⁰⁸	117+48.30	35.20
121+00	117+39.50	103.28
120+00	117+13.68	103.28
119+00	116+87.87	103.28
118+00	116+62.05	103.28
117+00	116+36.24	103.28
116+00	116+10.42	103.28
115+00	115+84.61	103.28
114+00	115+58.79	103.28
113+00	115+32.98	103.28
112+00	115+07.16	103.28
111+00	114+81.35	33.97
PT. A" 110+67.11	114+72.86	

NOTE: FOR STAS. & RANGES

CONT'D. S. SEE F.B. NO. 3.

PAGES 61-62-64

B/L DIST. PER STA. = 103.278



SEE PG. 2

DIST SOUND

10:34

0+00 0.5

1.5

1.8

DIST SOUND

(5)

TRIANGULATION OF SEXTANT
POINTS FOR ARC SHEET OF
PROJECT NO 8.

STA	OBJ.	SIX ANGLES	VERNIER	MEAN
U.S.C.&G.S.	VENTURA DUNE	1.	20° 16' 00"	
U.S.C.&G.S.	BAYPT R	2.	40° 32' 00"	0° 00' 00" 20° 16' 00"
U.S.C.&G.S.	COASTER	6.	121° 36' 00"	
U.S.C.&G.S.	COASTER	1.	51° 26' 30" v	
U.S.C.&G.S.	BAYPT R	2.	102° 53' 00"	0° 00' 00" 51° 26' 30"
	SOUTH		308° 39' 00"	
	VENT	6.	309° 00' 30"	
	SOUTH			
	VENT	1.	52° 55' 15"	
U.S.C.&G.S.	COASTER R	2.	105° 50' 45"	0° 00' 00" 52° 55' 30"
U.S.C.&G.S.	BAYPT	6.	317° 33' 00"	
U.S.C.&G.S.	BAYPT	1.	57° 04' 00"	
U.S.C.&G.S.	COASTER R	2.	114° 08' 30"	0° 00' 00" 57° 04' 20"
	VENTURA			
	DUNE	6.	342° 26' 00"	

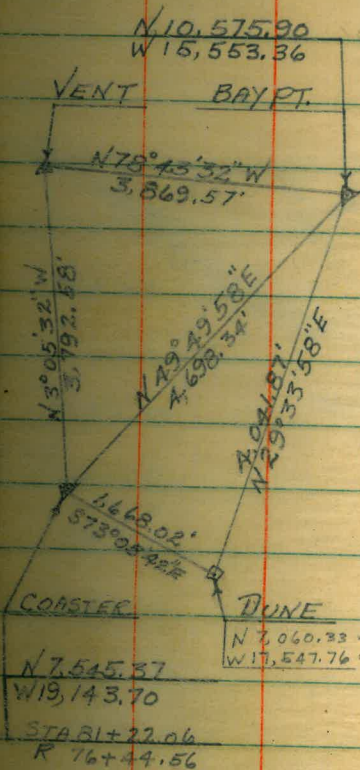
4-30-47

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WARM

VISIBILITY-GOOD



STATION DUNE

IS A 2X2 HUB ON THE
EASTERLY RIDGE OF
STOCKPILE FOR N.
VENTURA BRIDGE
APPROACH

STATION VENT

IS THE S.E. CORNER
OF THE S. VENT ON
BOATHOUSE ON
SANTA CLARA PT.

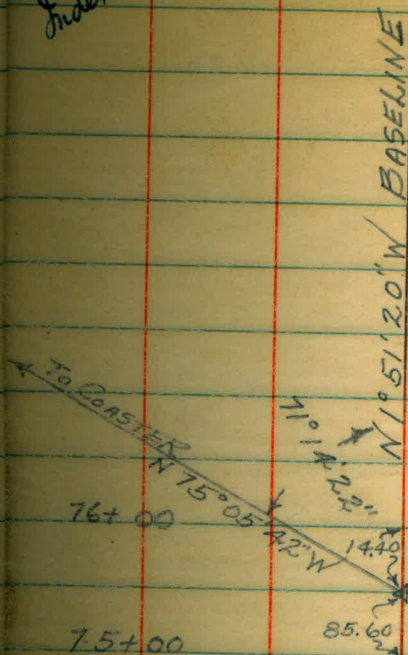
BASELINE FOR SOUNDINGS
OF DREDGED AREA IN PROJ. No. 7

Indexed

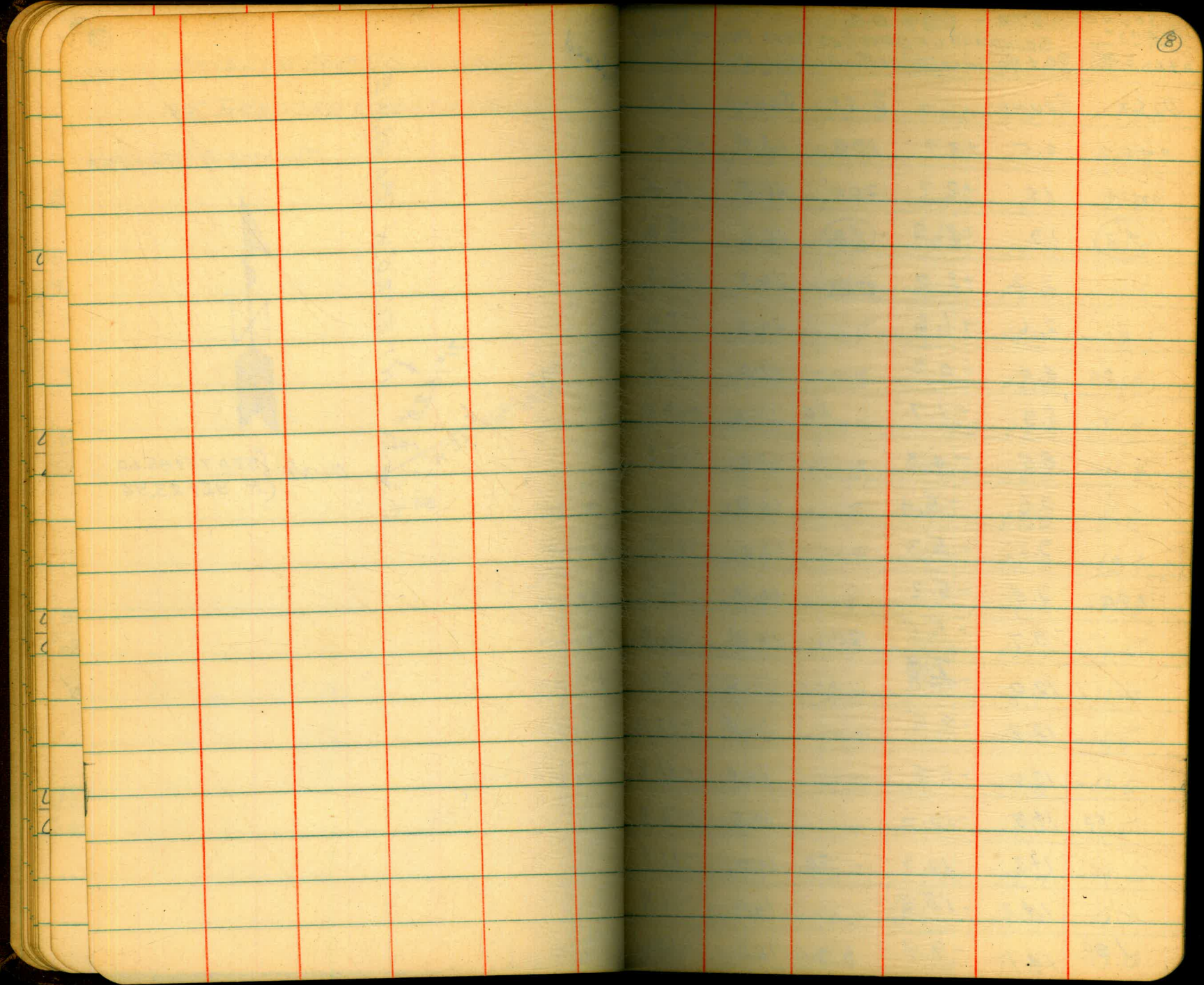
⑦

5-7-47

THOMAS A. STAMPER



DUNE { STA 75+85.60
(R 92+23.96



SOUND EAST
 0+00 = R/4
 STA - 69+00
 SOUNDINGS OF DREDGED AREA FROM NO. 7
 90+00 LINES ARE RUN AT 90° 00' 00" To R/4
 5-19-17

DIST	SOUND	DIST	SOUND
0+00	0.5 +3.7	190	15.4 -11.2
<u>09:34</u>	1.5 +2.7	200	16.7 -12.5
(4.2)	1.9 +2.3	(4.2)	16.6 -12.4
	2.2 +2.0	<u>09:38</u>	16.5 -12.3
	2.6 +1.6		16.6 -12.4
50	4.4 -0.2		17.0 -12.8
	5.9 -1.7	50	17.2 -13.0
	8.5 -4.3		17.0 -12.7
	9.6 -5.4		16.9 -12.7
	9.5 -5.3		17.0 -12.8
100	9.4 -5.2		16.7 -12.5
	9.7 -5.5	300	16.4 -12.2
	12.0 -7.8 -7.8		16.6 -12.4
	12.7 -8.5		16.4 -12.2
	13.0 -8.8		16.0 -11.8
50	14.8 -10.6		16.5 -12.2
	14.7 -10.5	50	16.0 -11.8
	14.7 -10.5		16.0 -11.8
180	14.1 -9.9	370	16.3 -12.2

Indexed
 STA - 69+00
 5-19-17
 DIST SOUND DIST SOUND

DIST	SOUND	DIST	SOUND
380	16.4 -12.2	580	16.2 -12.0
	16.0 -11.8		16.0 -11.8
400	15.5 -11.3	600	16.0 -11.8
(4.2)	15.2 -11.0	(4.2)	16.0 -11.8
<u>09:40</u>	15.4 -11.2	<u>09:42</u>	16.0 -11.8
	15.7 -11.5		16.3 -12.1
	16.0 -11.8		16.0 -11.8
50	16.0 -11.8	50	16.0 -11.8
	16.0 -11.8		16.0 -11.8
	16.0 -11.8		16.0 -11.8
	16.1 -11.9		16.8 -12.6
	16.0 -11.8		16.0 -11.8
500	16.1 -11.9	700	15.7 -11.5
	16.2 -12.0		16.1 -11.9
	16.4 -12.2		15.7 -11.5
	16.4 -12.2		15.8 -11.6
	16.4 -12.2		15.7 -11.5
50	16.4 -12.2	50	15.4 -11.2
	16.4 -12.2	(4.2)	15.3 -11.1
570	16.4 -12.2	770	15.2 -11.0

STA- 69 + 00			5-19-47		
DIST	SOUND		DIST	SOUND	
780	15.0	-10.8	980	14.0	-9.8
(4.2)	14.8	-10.6	<u>09:48</u>	13.8	-9.6
800	14.5	-10.3	1000	14.0	-9.8
	14.2	-10.0		14.1	-9.9
	14.0	-9.8	(4.2)	14.0	-9.8
	13.8	-9.6		14.0	-9.8
	13.7	-9.5		13.8	-9.6
50	13.8	-9.6	50	13.6	-9.4
	13.5	-9.3		13.5	-9.3
	13.1	-8.9		13.6	-9.4
	13.0	-8.8		13.5	-9.3
	13.4	-9.2		13.4	-9.2
900	13.8	-9.6	1100	13.2	-9.0
	14.4	-10.2	(4.2)	13.0	-8.6
	14.4	-10.2	<u>09:50</u>	13.0	-8.6
	14.4	-10.2	(4.1)	13.0	-8.6
	14.6	-10.4		13.0	-8.6
50	14.7	-10.5	50	13.2	-9.1
	14.4	-10.2		13.4	-9.3
970	14.2	-10.0	1170	13.7	-9.1

STA- 69 + 00			5-19-47		
DIST	SOUND		DIST	SOUND	
1180	14.0	-9.9	1380	16.0	-11.9
	14.0	-9.9		15.1	-11.0
	14.0	-9.9	1400	15.0	-10.9
(4.1)	14.4	-10.3	(4.1)	15.0	-10.9
	14.6	-10.5		15.0	-10.9
	13.4	-9.3		15.0	-10.9
<u>09:55</u>	12.8	-8.7		15.7	-11.6
50	12.6	-8.5	50	15.5	-11.4
	12.5	-8.4		15.3	-11.2
	12.5	-8.4		15.3	-11.2
	12.5	-8.4		15.0	-11.9
	12.8	-8.7		14.8	-10.7
1300	13.2	-9.1	1500	14.0	-9.9
	13.5	-9.4		14.0	-9.9
<u>09:58</u>	13.8	-9.7		14.0	-9.9
	13.2	-9.1		14.0	-9.9
	14.2	-10.1		14.0	-9.9
50	15.7	-11.6	50	13.5	-9.4
	16.0	-11.9	(4.1)	13.4	-9.3
1370	16.0	-11.9	1570	13.8	-9.7

STA - 69+00 5-19-47

DIST	SOUND		DIST	SOUND	
1580	13.3	-9.2	1780	14.0	-10.0
<u>10:00</u>	13.3	-9.2		13.4	-9.4
1600	13.3	-9.2	1800	13.0	-9.0
(4.1)	14.2	-10.1	<u>10:05</u>	13.2	-9.2
	14.1	-10.0	(4.0)	14.0	-10.0
	15.1	-11.0		14.0	-10.0
	16.2	-12.1		13.7	-9.7
50	16.0	-11.9	50	13.4	-9.4
	14.7	-10.6		13.8	-9.8
	13.3	-9.2		14.5	-10.5
	13.1	-9.0		15.1	-11.1
	13.1	-9.0		15.1	-11.1
1700	13.0	-8.9	1900	15.2	-11.2
	13.3	-9.2		15.0	-11.0
<u>10:03</u>	13.8	-9.7		15.0	-11.0
	13.8	-9.7		15.0	-11.0
(4.1)	14.0	-9.9		15.5	-11.0
50	14.1	-10.1	50	16.5	-12.5
(4.0)	14.0	-10.0		17.3	-13.3
1770	14.0	-10.0	1970	17.4	-13.4

STA - 69+00 5-19-47 (11)

DIST	SOUND		DIST	SOUND	
1980	18.0	-14.0			
	18.5	-14.5			
2000	18.7	-14.7			
<u>10:08</u>					

SOUND EAST
 STA-70+00 PX 5-19-47
 0+00 = R/L 96+74 : LINES ARE RUN AT 90°00'00" To R/L

DIST	SOUND	DIST	SOUND
0+00	+ 7	250	14.4 -10.6
10:28 75	0.0 +3.8	(3.8) 10:30 15.2	-11.4
(3.8) 80	0.5 +3.3	(3.7) 15.2	-11.5
	1.0 2.5 +2.8	15.2	-11.6
100	3.7 +0.1	15.8	-12.1
	3.5 +0.3	300 16.7	-13.0
	5.1 -1.3	16.7	-13.0
	5.8 -2.0	16.4	-12.7
	5.3 -1.5	16.8	-13.1
50	5.8 -2.0	16.8	-13.1
	6.7 -2.9	50 16.9	-13.2
	7.0 -3.2	17.3	-13.6
	7.0 -3.2	17.7	-14.0
	9.4 -5.6	17.9	-14.2
200	10.4 -6.6	18.0	-14.3
	11.1 -7.3	400 18.0	-14.5
	11.0 -7.2	17.4	-13.7
	12.5 -8.7	16.5	-12.8
240	13.4 -9.6	430 16.2	-12.5

STA-70+00 5-19-47 PX (2)

DIST	SOUND	DIST	SOUND
440	15.9 -12.2	14.0	-10.3
50	15.9 -12.2	50 13.7	-10.0
	15.5 -11.8	14.0	-10.3
(3.7)	15.2 -11.5	10:35 14.4	-10.7
	14.7 -11.0	(3.7) 14.6	-10.9
	14.5 -10.8	15.6	-11.9
500	14.3 -10.6	700 15.0	-11.3
	14.5 -10.8	14.1	-10.4
	14.2 -10.6	14.0	-10.3
	14.8 -11.1	14.1	-10.4
	14.4 -10.7	15.5	-11.8
50	14.1 -10.4	50 15.0	-11.3
	14.0 -10.3	14.4	-10.7
	15.2 14.2 -11.5	14.3	-10.6
	15.1 -11.4	14.4	-10.7
	15.1 -11.4	15.2	-11.5
600	14.0 -10.3	800 15.0	-11.3
	14.0 -10.3	15.0	-11.3
	13.8 13.8 -10.1	(3.7) 14.5	-10.8
80	14.0 -10.3	830 14.0	-10.3

STA - 70 + 00				PX		5-19-47	
DIST	SOUND		DIST	SOUND			
840	14.5	-10.8	1040	12.7	-9.0		
50	14.4	-10.7	50	13.1	-9.4		
(3.7)	14.0	-10.3		13.1	-9.4		
	14.0	-10.3	(3.7)	12.8	-9.1		
	14.7	-11.0		13.5	-9.8		
	14.5	-10.8		14.1	-10.4		
900	14.3	-10.6	1100	14.2	-10.5		
<u>10:38</u>	14.5	-10.8		14.1	-10.4		
	15.4	-10.7	<u>10:40</u>	14.4	-10.7		
	14.0	-10.3		14.4	-10.7		
	14.0	-10.3		14.0	-10.3		
50	14.0	-10.3	50	14.5	-10.8		
	14.0	-10.3		13.8	-10.1		
	13.8	-10.1		13.6	-9.9		
	13.5	-9.8		13.0	-9.3		
	14.0	-10.3		13.2	-9.3		
1000	13.5	-10.8	1200	13.5	-9.8		
	13.0	-9.3		14.0	-10.3		
	12.8	-9.1		14.2	-10.3		
1030	12.7	-9.0	1230	14.0	-10.3		

STA - 70 + 00				PX		5-19-47	
DIST	SOUND		DIST	SOUND			
1240	13.8	-10.1	1440	13.4	-9.8		
50	13.7	-10.0	50	13.0	-9.4		
(3.7)	13.8	-10.1	(3.6)	12.8	-9.2		
	13.7	-10.0		12.8	-9.2		
	13.3	-9.6		13.0	-9.4		
	13.1	9.4		12.8	-9.2		
1300	13.0	-9.3	1500	13.0	-9.4		
	13.0	-9.3		13.1	-9.5		
	13.0	-9.3		13.2	-9.6		
	13.0	-9.3		13.2	-9.6		
50	13.0	-9.3	50	13.7	-10.1		
	13.0	-9.3		14.5	-10.9		
	13.0	-9.3		14.3	-10.7		
	13.1	-9.4		13.7	-10.1		
<u>10:43</u>	13.1	-9.4		13.2	-9.6		
1400	13.2	-9.6	1600	13.4	-9.8		
(3.6)	13.0	-9.4	<u>10:45</u>	14.0	-10.4		
	13.1	-9.5	(3.6)	13.5	-9.9		
1430	13.1	-9.5	1630	13.1	-9.5		

STA - 70+00			PX, 5-19-47			SOUND EAST			STA - 71+00			PX 5-19-47 (2)		
DIST	SOUND		DIST	SOUND		DIST	SOUND		DIST	SOUND		DIST	SOUND	
1640	12.5	-8.9	1840	13.9	-10.3	0+00	+P		200	12.0	-8.6			
50	13.3	-9.7	50	13.9	-10.3	0+25	0.0	+3.4	(3.4)	12.7	-9.4			
(3.6)	14.0	-10.4	(3.6)	14.1	-10.5	11:10				12.7	-9.4			
	13.0	-9.4		14.1	-10.5	30	—			12.7	-9.4			
	12.7	-9.1		13.9	-10.3	(3.4) 40	1.0	+2.4		13.0	-9.6			
	12.8	-9.2	10:48	13.7	-10.1	50	2.8	+0.6		13.0	-9.6			
1700	13.2	-9.6	1900	13.5	-9.9		4.2	-0.8	50	19.5	-11.1			
	13.0	-9.4		13.4	-9.8		4.4	-1.0		15.0	-11.6			
	12.4	-8.8		13.0	-9.4		5.0	-1.6	11:13	15.0	-11.6			
	13.4	-9.8		13.2	-9.6		5.2	-1.8		15.1	-11.7			
	13.4	-9.8		13.1	-9.5	100	6.0	-2.6		15.5	-12.1			
50	13.5	-9.9	50	13.4	-9.8		6.5	-3.1	300	15.4	-12.0			
	13.6	-10.0		14.0	-10.4		7.0	-3.6		15.4	-12.0			
	13.8	-10.2		14.0	-10.4		7.1	-3.7		15.7	-12.3			
	13.5	-9.9		14.0	-10.4		7.4	-4.0		15.9	-12.5			
	13.7	-10.1		14.0	-10.4	50	7.8	-4.4		15.8	-12.4			
1800	13.8	-10.2	2000	14.0	-10.4		8.4	-5.0	50	15.7	-12.3			
	13.8	-10.2					9.3	-5.9		15.7	-12.3			
	14.0	-10.4					10.4	-7.0	(3.4)	15.7	-12.3			
1830	14.0	-10.4				190	11.5	-8.1	380	15.6	-12.2			

STA - 71+ 00			PX 5-19-47		
DIST	SOUND		DIST	SOUND	
390	15.3	-11.9	590	13.6	-10.2
400	15.8	-12.4	600	14.4	-11.0
(3.4)	15.2	-11.8	(3.4)	14.4	-11.0
	15.0	-11.6		13.8	-10.4
<u>11:15</u>	14.7	-11.3		13.4	-10.0
	15.0	-11.6		13.3	-9.9
50	15.1	-11.7	50	13.3	-9.9
	15.0	-11.6		12.8	-9.9
	14.5	-11.1		12.7	-9.3
	14.0	-10.6		12.7	-9.3
	13.4	-10.0		12.6	-9.2
500	14.0	-10.6	700	12.6	-9.2
	12.7	-9.3		12.7	-9.3
	13.2	-9.8		12.6	-9.2
	13.0	-9.6	(3.4)	12.6	-9.2
	14.0	-10.6	<u>11:18</u>	12.7	-9.3
50	13.7	-10.3	50	12.8	-9.5
	13.1	-9.7	(3.3)	13.0	-9.7
	13.2	-9.8		13.0	-9.7
580	13.6	-10.2	780	12.7	-9.4

STA - 71+ 00			PX 5-19-47 (15)		
DIST	SOUND		DIST	SOUND	
790	12.9	-9.6	990	12.9	-9.6
800	12.9	-9.6	1000	12.8	-9.5
	12.8	-9.5		12.7	-9.4
	12.6	-9.3	(3.3)	12.1	-8.8
	13.0	-9.7		12.0	-8.7
	12.8	-9.5		12.2	-8.9
50	12.5	-9.2	50	12.0	-8.7
	12.5	-9.2		11.9	-8.6
	12.7	-9.4		11.7	-8.4
	12.7	-9.4		11.9	-8.6
	13.4	-10.1		12.1	-8.8
900	13.4	-10.1	1100	12.4	-9.1
	13.0	-9.7		12.5	-9.2
	12.5	-9.2		13.0	-9.7
	12.3	-9.0		12.8	-9.5
	12.4	-9.1	<u>11:23</u>	13.0	-9.7
50	13.5	-10.2	50	13.2	-9.9
	13.1	-9.8		13.5	-10.2
	12.8	-9.5	(3.3)	14.1	-10.8
980	12.5	-9.2	1180	14.4	-11.1

STA 717 00		5-19-47		PX	
DIST	SOUND	DIST	SOUND	DIST	SOUND
1190	14.0 -10.7	1390	14.0 -10.7		
1200	13.7 -10.4	1400	15.0 -11.7		
(3.3)	13.5 -10.2	(3.3)	14.1 -10.8		
	13.2 -9.9		13.7 -10.4		
	13.4 -10.1		13.4 -10.1		
	13.6 -10.3		13.8 -10.5		
50	13.8 -10.5	50	13.0 -9.7		
	13.6 -10.3		12.5 -9.2		
	13.5 -10.2		12.6 -9.3		
	13.6 -10.3		12.4 -9.1		
	13.7 -10.4		12.5 -9.2		
1300	13.4 -10.1	1500	12.5 -9.2		
	13.3 -10.0		12.5 -9.2		
	13.7 -10.4		12.5 -9.2		
	14.0 -10.7		12.5 -9.2		
<u>11:25</u>	13.8 -10.5		12.4 -9.1		
50	13.5 -10.2	50	12.4 -9.1		
	13.6 -10.3		12.4 -9.1		
	13.6 -10.3	<u>11:28</u>	12.4 -9.1		
1380	13.8 -10.5	1580	12.4 -9.1		

STA 717 00		5-19-47		PX (10)	
DIST	SOUND	DIST	SOUND	DIST	SOUND
1590	12.0 -8.7	1790	13.1 -9.8		
1600	12.0 -8.7	1800	13.0 -9.7		
(3.3)	12.2 -8.9	(3.3)	13.0 -9.7		
	12.7 -9.4		12.9 -9.6		
	12.2 -8.9		12.5 -9.2		
	12.0 -8.7		11.6 -8.3		
50	12.1 -8.8	50	12.0 -8.7		
	12.5 -9.2	1860	12.8 -9.5		
	12.0 -8.7	<u>11:32</u>			
	13.0 -9.7				
	13.4 -10.1				
	14.1 15.0 -10.8				
	14.0 -10.7				
	14.0 -10.7				
	13.4 -10.1				
	13.5 -10.2				
50	13.5 -10.2				
	13.3 -10.0				
	13.1 -9.8				
	13.5 -10.2				
		<u>11:30</u>			
1780	13.5 -10.2				

SOUND
EAST

STA - 72+00 PX

5-19-47

0+00 = R-92+ 23.96 (DUNE 3/4): LINES ARE RUN AT 90° 00' 00" T. 2.7

DIST	SOUND		DIST	SOUND	
0+00	+?		290	10.2	-7.5
1+13	0.0	+2.7	300	11.4	-8.7
<u>12:28</u> 20	0.6	+2.1	(2.7)	12.0	-9.3
(2.7)	1.9	+0.8		12.2	-9.5
	5.0	-2.3		12.2	-9.5
50	4.9	-2.2		12.2	-9.5
	5.5	-2.8	50	12.1	-9.4
	5.5	-2.8		13.3	-10.6
	5.4	-2.7		15.6	-12.9
	6.4	-3.7		15.0	-12.3
200	7.1	-4.4		13.5	-10.6
	7.8	-5.1	400	15.3	-10.6
	8.6	-5.9		14.5	-11.8
	9.2	-6.5		14.1	-11.4
<u>12:30</u>	9.3	-6.6		13.5	-10.8
50	9.9	-7.2		13.4	-10.7
	10.3	-7.6	50	13.4	-10.7
	7.7	-5.0	<u>12:33</u>	13.0	-10.3
280	7.0	-4.3	470	13.0	-10.3

STA - 72+00

PX

5-19-47 (17)

DIST	SOUND		DIST	SOUND	
480	13.0	-10.3	680	15.2	-12.5
	13.5	-10.8		15.4	-12.7
500	13.2	-10.5	700	14.5	-11.8
(2.7)	12.8	-10.1	(2.7)	13.5	-10.8
	12.1	-9.4		12.6	-9.9
	12.5	-9.8		12.3	-9.6
	12.3	-9.6		12.3	-9.6
50	13.8	-11.1	50	12.4	-9.7
	13.8	-11.1		13.0	-10.3
	13.0	-10.3		12.7	-10.0
	13.0	-10.3		12.5	-9.8
	12.6	-9.9		12.4	-9.7
600	12.4	-9.7	800	12.1	-9.4
<u>12:35</u>	13.1	-10.4		12.0	-9.3
	13.1	-10.4		13.2	-10.5
	13.5	-10.8		13.4	-10.7
	14.1	-11.4		13.2	-10.5
50	14.5	-11.8	50	13.1	-10.4
	15.0	-12.3	(2.7)	12.9	-10.2
670	15.0	-12.3	870	12.8	-10.1

STA - 72 + 00			PX	5-19-47
DIST	SOUND		DIST	SOUND
880	12.7	-10.0	1080	13.0 -10.4
	12.5	-9.8		13.2 -10.6
900	12.5	-9.8	1100	13.1 -10.5
(2.7)	12.5	-9.8		13.0 -10.4
<u>12:38</u>	12.4	-9.7	<u>12:40</u>	13.0 -10.4
(2.6)	12.0	-9.4	(2.6)	12.7 -10.1
	11.8	-9.2		12.2 -9.6
50	11.0	-8.4	50	12.5 -9.9
	11.0	-8.4		11.8 -9.2
	11.3	-8.7		11.5 -8.9
	12.6	-10.0		12.0 -9.4
	13.6	-11.0		11.4 -8.8
1000	13.9	-11.3	1200	12.5 -9.9
	13.9	-11.3		12.6 -10.0
	14.7	-12.1		12.8 -10.2
	14.7	-12.1		13.1 -10.5
	14.3	-11.7		12.8 -10.2
50	14.0	-11.4	50	13.0 -10.4
	13.9	-11.3		12.7 -10.1
1070	13.4	-10.8	1270	12.7 -10.1

STA - 72 + 00			PX	5-19-47 (18)
DIST	SOUND		DIST	SOUND
1280	12.6	-10.0	1480	13.0 -10.4
	12.5	-9.9	<u>12:45</u>	13.1 -10.5
1300	12.5	-9.9	1500	13.1 -10.5
(2.6)	12.4	-9.8	(2.6)	13.0 -10.4
<u>12:43</u>	12.4	-9.8		12.9 -10.3
	12.3	-9.7		12.6 -10.0
	12.3	-9.7		12.1 -9.5
50	12.3	-9.7	50	12.0 -9.4
	12.4	-9.8		12.0 -9.4
	12.4	-9.8		12.1 -9.5
	12.4	-9.8		12.0 -9.4
	12.8	-10.2		11.7 -9.1
1400	12.8	-10.2	1600	11.9 -9.3
	13.0	-10.4		12.0 -9.4
	13.8	-11.2		11.7 -9.1
	14.0	-11.4		11.7 -9.1
	13.7	-11.1		12.0 -9.4
50	13.6	-11.0	50	12.0 -9.4
	13.4	-10.8	(2.6)	12.0 -9.4
1470	13.1	-10.5	1670	11.8 -9.2

DIST	SOUND	DIST	SOUND
1680	11.7 -9.1		
<u>12:48</u>	11.6 -9.0		
1700	11.6 -9.0		
(2.6)	12.1 -9.5		
	12.3 -9.7		
	12.7 -10.1		
	12.7 -10.1		
50	12.7 -10.1		
	12.8 -10.2		
	12.8 -10.2		
	12.5 -9.9		
	12.6 -10.0		
1800	12.7 -10.1		
	12.5 -9.9		
	12.4 -9.8		
	12.3 -9.7		
	12.1 -9.5		
50	12.3 -9.7		
<u>12:51</u>	12.0 -9.4		
1870	12.0 -9.4		

5-19-47 SOUND EAST STA-73+00 PY 5-19-47 (19)

2200=Range 32+23.96 (DUNE Pt.) LINES ARE RUN AT 90°00'00" To B/L

DIST	SOUND	DIST	SOUND
0700	+P	350	10.2 -7.8
1466	0.0 +2.4	<u>13:10</u>	10.0 -7.6
1780	1.2 +1.2	(2.4)	10.0 -7.6
<u>13:08</u>	3.0 -0.6		9.5 -7.1
200	3.5 -1.1		9.0 -6.6
(2.4)	4.8 -2.4	4.00	9.8 -7.4
	6.0 -3.6		10.2 -7.8
	6.8 -4.4		10.4 -8.0
	6.7 -4.3		10.4 -8.0
50	7.4 -5.0		14.0 -11.6
	8.4 -6.0	50	14.0 -11.6
	9.0 -6.6		13.2 -10.8
	9.5 -7.1		12.5 -10.1
	9.7 -7.3		12.7 -10.3
300	9.8 -7.4		12.3 -9.9
	9.7 -7.3	500	12.0 -9.6
	9.5 -7.1		12.0 -9.6
	9.2 -6.8	(2.4)	12.4 -10.0
340	9.0 -6.6	530	12.0 -9.6

STA- 73+00 PX				5-19-47			
DIST	SOUND		DIST	SOUND			
540	11.5	-9.1	740	11.8	-9.4		
50	11.0	-8.6	50	12.1	-9.7		
(2.4)	11.0	-8.6	(2.4)	12.5	-10.1		
	11.3	-8.9		13.0	-10.6		
	12.4	-10.0		13.3	-10.9		
<u>13:13</u>	12.0	-9.6		13.0	-10.6		
	130						
600	12.0	-10.6	800	13.0	-10.6		
	13.0	-10.6		13.0	-10.6		
	13.1	-10.7	<u>13:15</u>	12.9	-10.5		
	13.0	-10.6		12.7	-10.3		
	12.8	-10.4		12.4	-10.0		
50	12.7	-10.3	50	12.3	-9.9		
	12.5	-10.1		12.0	-9.6		
	12.4	-10.0		11.5	-9.1		
	12.3	-9.9		13.2	-10.8		
	12.0	-9.6		13.7	-11.3		
700	12.0	-9.6	900	12.0	-9.6		
	12.0	-9.6		11.6	-9.2		
	12.0	-9.6		11.5	-9.1		
730	11.5	-9.1	930	11.5	-9.1		

STA- 73+00 PX				5-19-47			
DIST	SOUND		DIST	SOUND			(20)
940	11.8	-9.4	1140	12.4	-10.1		
50	12.0	-9.6	50	12.3	-10.0		
(2.4)	12.2	-9.8	(2.4)	12.1	-9.8		
	12.2	-9.8	(2.3)	12.4	-10.1		
	12.0	-9.6		12.6	-10.3		
	12.0	-9.6		12.7	-10.4		
1000	12.0	-9.6	1200	13.2	-10.9		
	12.1	-9.7		13.6	-11.3		
	12.1	-9.7		13.6	-11.3		
(2.4)	12.1	-9.7		13.5	-11.2		
<u>13:18</u>	12.3	-9.9		13.5	-11.2		
50	12.6	-10.3	50	13.4	-11.1		
(2.3)	12.6	-10.3		13.0	-10.7		
	12.6	-10.3	<u>13:20</u>	12.7	-10.4		
	12.4	-10.1		12.5	-10.2		
	12.4	-10.1		12.3	-10.0		
1100	12.4	-10.1	1300	12.2	-9.9		
	12.4	-10.1		12.3	-10.0		
	12.4	-10.1	(2.3)	12.7	-10.4		
1130	12.4	-10.1	1330	12.7	-10.4		

STA - 73+00 PX 5-19-47

DIST	SOUND	DIST	SOUND
1340	12.8 -10.5	1540	12.0 -9.7
50	12.9 -10.6	^{13:23} 50	12.2 -9.9
(2.3)	12.7 -10.4	(2.3)	12.5 -10.2
	12.3 -10.0		12.3 -10.0
	12.0 -9.7		12.0 -9.7
	11.8 -9.5		11.8 -9.5
1400	11.9 -9.6	1600	12.0 -9.7
	12.0 -9.7		12.0 -9.7
	11.8 -9.5		12.0 -9.7
	11.7 -9.4		12.0 -9.7
	11.5 -9.2		12.3 -10.0
50	11.5 -9.2	50	12.5 -10.2
	11.9 -9.6		12.4 -10.1
	11.9 -9.6		12.4 -10.1
	11.9 -9.6		12.0 -9.7
	12.0 -9.7	^{13:25}	12.0 -9.7
1500	12.0 -9.7	1700	11.9 -9.6
	12.0 -9.7		11.8 -9.5
	12.0 -9.7		11.7 -9.4
1530	12.0 -9.7	1730	11.7 -9.4

STA - 73+00 5-19-47 PX (31)

DIST	SOUND	DIST	SOUND
1740	11.6 -9.3		
50	11.7 -9.4		
	11.5 -9.2		
	11.2 -8.9		
	12.0 -9.7		
	11.5 -9.2		
1800	11.5 -9.2		
	11.8 -9.5		
	12.0 -9.7		
	12.5 -10.2		
	12.0 -9.7		
50	11.8 -9.5		
1860	12.0 -9.7		
		(2.3)	

SOUND EAST
 STA-74+00 PX. 5-19-47
 6+00 = RANGE - 22+23.26 (DUNE #4: LINES ARE RUN AT 90° 00' 00" To E)

DIST	SOUND	DIST	SOUND
0+00	+?	390	9.7 -7.6
2+10	0.0 +2.1	400	9.0 -6.9
<u>14:08</u>	0.6 +1.5	(2.1)	9.0 -6.9
(2.1)	2.5 -0.4		8.4 -6.3
	4.3 -2.2	<u>14:10</u>	8.0 -5.9
50	5.7 -3.6		7.2 -5.1
	6.4 -4.3	50	7.9 -5.8
	7.4 -5.3		8.5 -6.4
	7.4 -5.3		8.8 -6.7
	8.3 -6.2		9.3 -7.2
300	8.7 -6.6		10.0 -7.9
	9.0 -6.9	500	10.1 -8.0
	9.1 -7.0		10.4 -8.3
	9.1 -7.0		13.0 -10.9
	9.1 -7.0		13.7 -11.6
50	9.7 -7.6		13.0 -10.9
	10.2 -8.1	50	12.6 -10.5
	10.2 -8.1		12.6 -10.5
380	9.5 -7.4	570	14.2 -12.1

STA-74+00 PX. 5-19-47 (2)

DIST	SOUND	DIST	SOUND
580	14.2 -12.1	780	11.8 -9.7
	14.0 -11.9		12.2 -10.1
600	13.7 -11.6	800	12.7 -10.6
(2.1)	13.1 -11.0	(2.1)	11.8 -9.7
	12.7 -10.6		11.5 -9.4
	12.4 -10.3		11.6 -9.5
	12.0 -9.9		11.6 -9.5
50	12.0 -9.9	50	11.0 -8.9
	12.0 -9.9		10.8 -8.7
	11.6 -9.5	<u>14:15</u>	10.5 -8.4
	11.6 -9.5		10.5 -8.4
	11.5 -9.4		10.6 -8.5
700	11.9 -9.8	900	10.8 -8.7
	12.7 -10.6		11.0 -8.9
<u>14:22</u>	12.4 -10.3		11.0 -8.9
	11.7 -9.6		11.1 -9.0
	11.5 -9.4		11.0 -8.9
50	11.4 -9.3	50	10.8 -8.7
	11.5 -9.4	(2.1)	10.9 -8.8
770	11.4 -9.3	970	11.0 -8.9

STA- 74+00			5-19-17		
DIST	SOUND	PX	DIST	SOUND	
980	11.0	-8.9	1180	11.5	-9.4
(2.1)	11.5	-9.4	(2.1)	11.8	-9.7
1000	11.5	-9.4	1200	12.1	-10.0
	11.6	-9.5		13.0	-10.9
	11.8	-9.7		13.2	-11.1
	11.9	-9.8		13.0	-10.9
	11.7	-9.6		12.5	-10.4
50	11.8	-9.7	50	12.0	-9.9
	12.2	-10.1		12.8	-10.0
	11.8	-9.7		13.1	-11.0
	12.0	-9.9		13.0	-10.9
	11.8	-9.7		12.7	-10.6
1100	12.7	-10.6	1300	12.5	-10.4
	12.4	-10.3	14:20	12.4	-10.3
	12.1	-10.0		12.4	-10.3
14:18	11.0	-8.9		12.0	-9.9
	11.8	-9.7		11.9	-9.8
50	11.7	-9.6	50	11.9	-9.8
	11.4	-9.3		11.8	-9.7
1120	11.5	-9.4	1370	11.5	-9.4

STA - 74+00			5-19-17		
DIST	SOUND	PX	DIST	SOUND	
1380	11.3	-9.2	1580	10.5	-8.4
	11.0	-8.9		10.8	-8.7
1400	11.8	-9.7	1600	10.8	-8.7
(2.1)	12.0	-9.9	(2.1)	11.0	-8.9
	12.0	-9.9		11.1	-9.0
	12.0	-9.9		11.2	-9.1
	11.7	-9.6		11.1	-9.0
50	11.6	-9.5	50	11.1	-9.0
	11.5	-9.4		11.2	-9.1
	11.5	-9.4		11.2	-9.1
	11.0	-8.9		11.0	-8.9
	10.5	-8.4		11.2	-9.1
1500	10.3	-8.2	1700	11.2	-9.1
	10.5	-8.4		11.5	-9.4
	10.5	-8.4		11.8	-9.7
	10.7	-8.6		12.2	-10.1
	10.5	-8.4		12.5	-10.4
50	10.7	-8.6	50	12.4	-10.3
	10.7	-8.6	14:22	12.4	-10.3
1570	10.6	-8.5	1770	12.4	-10.3

STA- 74+ 00 PX 5-19-47
 SOUND EAST
 DIST SOUND DIST SOUND

1780 12.4 -10.3

12.3 -10.2

1800 12.2 -10.1

12.0 -9.9

11.8 -9.7

11.5 -9.4

11.0 -8.9

18450 11.0 -8.9

(2.1)

SOUND EAST STA- 75+ 00 PY
 DIST SOUND DIST SOUND
 0200 = P-9212396 (DUNE 3/4) LINES ARE DOWN AT 203.0000 TO 3/4 (24)

DIST SOUND DIST SOUND
 0400 + ? 420 8.5 -6.4

2727 0.0 +2.1 9.0 -6.9

14:38 40 1.0 +1.0 (2.1) 9.5 -7.4

50 5.0 -2.9 90 10.0 -7.9

(2.1) 6.7 -4.6 10.3 -8.2

7.0 -4.9 11.3 -9.2

7.3 -5.2 11.7 -9.6

8.0 -5.9 11.0 -8.9

200 8.8 -6.7 500 10.7 -8.7

9.2 -7.1 11.2 -9.1

9.4 -7.3 12.2 -10.1

9.4 -7.3 12.2 -10.1

50 9.5 -7.4 14:43 12.2 -10.1

9.4 -7.3 50 12.5 -10.4

9.0 -6.9 12.2 -10.1

9.2 -7.1 12.0 -9.9

9.2 -7.1 12.0 -9.9

400 8.8 -6.7 (2.1) 11.7 -9.6

410 8.7 -6.6 600 11.7 -9.6

STA - 75 + 00 PX 5-19-47

DIST	SOUND	DIST	SOUND
610	11.6 -9.5	810	11.6 -9.5
(2.1)	11.0 -8.9	14:45	12.4 -10.3
	10.5 -8.4	(2.1)	12.0 -9.9
	11.0 -8.9		12.0 -9.9
50	11.0 -8.9	50	12.5 -10.3
	10.5 -8.4		12.5 -10.4
	10.3 -8.2		12.4 -10.3
	^{10.0} 8.0 -7.9		12.3 -10.3
	^{10.0} 8.8 -7.9		12.3 -10.3
	^{10.3} 9.2 -8.2	900	12.3 -10.3
	^{12.4} 9.4 -10.3		12.2 -10.3
	^{12.8} 9.4 -10.7		11.8 -9.9
	^{12.4} 9.4 -10.3		11.5 -9.4
	^{11.5} 9.5 -9.4		11.5 -9.4
	^{11.2} 9.4 -9.1	50	11.5 -9.4
	9.5 -7.4		11.9 -9.8
	10.5 -8.4		11.9 -9.8
	10.4 -8.3		12.4 -10.3
	10.4 -8.3		12.0 -9.9
800	10.6 -8.5	1000	12.0 -9.9

STA - 75 + 00 PX 5-19-47 (25)

DIST	SOUND	DIST	SOUND
1010	13.1 -11.0	1210	13.0 -10.9
	13.0 -10.9		13.2 -11.1
(2.1)	12.2 -10.1		13.2 -11.1
	12.0 -9.9		13.3 -11.2
50	12.0 -9.9	50	13.1 -11.0
	12.0 -9.9		12.7 -10.6
	12.4 -10.3		12.1 -10.0
	13.6 -11.5		12.4 -10.2
	13.6 -11.5	(2.1)	12.5 -10.4
1100	13.0 -10.9	1300	12.9 -10.8
	12.8 -10.7		13.1 -11.0
	12.5 -10.4	^{14:50}	13.0 -10.9
	12.3 -10.2	(2.1)	12.7 -10.6
	12.0 -9.9		12.8 -10.7
50	13.1 -11.0	50	12.5 -10.4
	13.4 -11.3		12.2 -10.1
	13.2 -11.1		12.0 -9.9
	13.0 -10.9		12.0 -9.9
	12.8 -10.7		12.0 -9.9
1200	12.8 -10.7	1400	12.0 -9.9

STA-75+00		P.X	
DIST	SOUND	DIST	SOUND
1410	12.4	1610	11.6
0400	12.7		11.6
	-10.3		-9.5
2127	0.0		11.8
	13.0		-9.7
(2.1)	1.0	(2.1)	11.8
	12.5		-9.7
	-5.0		11.8
	11.8		-9.7
50	6.7	50	11.8
	11.0		-9.7
	7.0	10.53	12.0
	11.0		-9.7
	7.7		12.1
	1		-10.0
	11.3		12.1
	-9.2		-10.0
	11.3		12.2
	-9.2		-10.0
1500	11.3	1700	12.7
	-9.2		-10.0
	11.4		12.7
	-9.3		-10.0
	11.5		12.4
	-9.4		-10.0
	11.5		11.8
	-9.4		-9.7
	11.5		11.8
	-9.4		-9.7
50	11.4	50	11.8
	-9.3		-9.7
	11.4		11.7
	-9.3		-9.6
	11.4		11.4
	-9.3		-9.3
	11.4		11.3
	-9.3		-9.2
	11.4		11.3
	-9.3		-9.2
1600	11.5	1800	11.2
	-9.4		-9.1

STA-75+00		5-19-47	
DIST	SOUND	DIST	SOUND
1810	11.2		-9.1
	11.3		-9.2
(2.1)	11.3		-9.2
	11.2		-9.1

(26)

SOUND EAST STA -76+00 PX. 5-19
 0+00 = R-32+2396 (DUNE 3/4) : LINE A RE RUN AT 90° 30' 00" TO 3/4

DIST	SOUND	DIST	SOUND
0400	+ P	400	9.0 -6.8
2+17	9.0 +2.2		9.0 -6.8
<u>15:06</u>			
30	2.5 -0.3		9.3 -7.1
(2.2)	4.1 -1.9	(2.2)	10.3 -8.1
50	6.4 -4.2		10.4 -8.2
	7.8 -5.6	50	10.0 -7.8
	8.7 -6.5		10.1 -7.9
	9.4 -7.2		10.2 -8.1
	9.8 -7.6		10.3 -8.1
300	10.0 -7.8	<u>15:08</u>	10.0 -7.8
	10.1 -7.9	500	11.2 -9.0
	10.1 -7.9		11.3 -9.1
	10.0 -7.8		12.5 -10.3
	10.0 -7.8		12.6 -10.4
50	10.0 -7.8		12.4 -10.2
	10.0 -7.8	50	12.4 -10.2
	10.1 -7.9		12.2 -10.0
	9.8 -7.6		12.4 -10.2
390	9.7 -7.5	580	12.4 -10.2

STA -76+00 5-19-47 (27) PX

DIST	SOUND	DIST	SOUND
590	12.3 -10.1	790	12.0 -9.8
600	12.0 -9.8	800	14.0 -11.8
	11.4 -9.2		14.0 -11.8
	12.0 -9.8		13.6 -11.4
(2.2)	12.8 -10.6	(2.2)	13.0 -10.8
	12.5 -10.4		13.2 -11.0
50	12.6 -10.4	50	13.3 -11.1
	12.4 -10.2		13.3 -11.1
	12.3 -10.1		13.0 -10.8
	12.4 -10.2		12.7 -10.5
<u>15:10</u>	12.5 -10.3		13.1 -10.9
700	12.5 -10.3	900	13.4 -11.2
	12.7 -10.5		11.5 -9.3
	12.8 -10.6	920	5.0 -2.8
	12.7 -10.5	<u>15:14</u>	
	12.4 -10.2		
50	12.1 -9.9	50	
	12.3 -10.1		
	12.3 -10.1	(2.2)	
780	12.3 -10.1		

SOUND
EAST

STA - 67 + 00

5-21-47

0 + 00 = RANGE LINE 110 + 00: LINES AGE RUN AT 90° 00' 00" To R/A

DIST	SOUND		DIST	SOUND	
0 + 00	+ ?		240	12.1	-9.2
<u>09:14</u>					
0 + 65	0.0	+2.8	50	12.0	-9.1
70	1.0	+1.8	(2.9)	11.8	-8.9
(2.8)	3.1	-0.3	<u>09:18</u>	11.4	-8.5
	3.1	-0.3		12.4	-9.5
100	3.8	-1.0		12.4	-9.5
	3.9	-1.1	300	12.4	-9.5
	5.2	-2.4		12.4	-9.5
	6.8	-4.0		12.5	-9.6
	7.6	-4.8		12.5	-9.6
50	7.8	-5.0		12.6	-9.7
	8.7	-5.9	50	12.7	-9.8
	11.2	-8.4		12.8	-9.9
	11.7	-8.9		12.5	-9.6
	11.8	-9.0		12.0	-9.1
200	11.9	-9.1		12.0	-9.1
(2.8)	12.1	-9.3	400	12.0	-9.1
	12.2	-9.4	<u>09:20</u>	12.0	-9.1
230	12.3	-9.5	420	11.7	-8.8

STA - 67 + 00

5-21-47

(38)

DIST SOUND DIST SOUND

430	11.2	-8.3			
(2.9)	11.2	-8.3			
50	11.4	-8.5			
	15.0	-12.1			
	15.0	-12.1			
	14.1	-11.2			
	13.0	-10.1			
500	10.5	-7.6			
	6.8	-3.9			
	6.5	-3.6			
	3.0	-0.1			
574	0.0	+2.9			

SOUND WEST STA-68+00 5-21-41
 0+00 = PT. -540' W. OF CAUSEWAY 3/4" LINES ARE RUN AT B¹ 23°46' 16"

DIST	SOUND		DIST	SOUND	
	EDGE CUT		190	11.8	-8.4
0+02			200	11.7	-8.3
10	4.3	-0.9			
(3.4)	9.4	-6.0	(3.4)	12.3	-8.9
	12.0	-8.6		12.9	-9.5
	12.0	-8.6		12.4	-9.0
50	12.0	-8.6		12.4	-9.0
	12.0	-8.6	50	12.8	-9.4
	12.3	-8.9		12.5	-9.1
	12.3	-8.9		12.2	-8.8
	12.5	-9.1		12.2	-8.8
100	12.6	-9.2		12.2	-8.8
	12.5	-9.1	300	12.3	-8.9
	12.5	-9.1	10:23	12.3	-8.9
	11.7	-8.3		12.3	-8.9
	11.0	-7.6		12.4	-9.0
50	11.0	-7.6		12.5	-9.1
	11.0	-7.6	50	12.8	-9.4
	11.3	-7.9		12.7	-9.3
180	11.7	-8.3	370	12.5	-9.1

(29)

DIST	SOUND		DIST	SOUND		
380	12.5	-9.1	580	13.0	-9.3	
10:25	12.5	-9.1		13.2	-9.7	
400	12.5	-9.1	600	13.2	-9.7	
(2.4)	12.6	-9.2	(3.5)	14.1	-10.6	
	12.1	-8.7		13.7	-10.2	
	12.0	-8.6		13.7	-10.2	
	11.8	-8.4	X	13.6	-10.1	
50	12.4	-9.0	50	14.0	-10.5	
	12.8	-9.4		14.1	-10.6	
	12.8	-9.4		14.8	-11.3	
	13.3	-9.9		17.5	-14.0	
	13.0	-9.6	X	16.8	-13.3	
500	13.0	-9.6	700	15.0	-11.5	
	12.8	-9.4		15.0	-11.5	
	13.0	-9.6		15.0	-11.5	
(3.4)	13.0	-9.6		15.6	-12.1	
10:25	12.8	-9.4	X	16.0	-12.5	
10:25	50	13.5	-10.0	50	16.0	-12.5
(3.5)	13.5	-10.0		16.4	-12.9	
570	13.0	-9.5	770	16.7	-13.2	

STA - 68+ 00			5-21-47			
DIST	SOUND		DIST	SOUND		
780	16.2	-12.7	980	13.1	-9.6	
X (3.5)	16.2	-12.7		13.1	-9.6	
800	16.0	-12.5	1000	13.1	-9.6	
	16.0	-12.5	(3.5)	12.9	-9.4	
	15.7	-12.2		12.9	-9.3	
	15.5	-12.0	(3.6)	12.9	-9.3	
X	15.0	-11.5	X	12.9	-9.3	
	50	15.0	-11.5	50	12.8	-9.2
		15.3	-11.8		12.7	-9.1
		16.5	-13.0		12.7	-9.1
<u>10:40</u>	16.0	-12.5	<u>10:43</u>	13.0	-9.4	
X	15.2	-11.7	X	12.8	-9.2	
900	14.0	-10.5	1100	12.7	-9.1	
	13.0	-9.5		12.7	-9.1	
	12.8	-9.3		13.7	-10.1	
	12.7	-9.2		14.1	-10.5	
X	12.7	-9.2	X	13.2	-9.6	
	50	12.5	-9.0	50	13.3	-9.7
		13.0	-9.5		13.4	-9.8
970	13.1	-9.6	1170	14.5	-9.9	

STA - 68+ 00			5-21-47			
DIST	SOUND		DIST	SOUND		
1180	14.0	-10.4	1380	13.4	-9.8	
	13.1	-9.5		13.3	-9.7	
1200	13.2	-9.6	1400	12.8	-9.2	
	13.0	-9.4		12.8	-9.2	
<u>10:45</u>	13.0	-9.4	<u>10:48</u>	13.7	-10.1	
(3.6)	13.0	-9.4	(3.6)	13.4	-9.8	
	13.0	-9.4	X	12.5	-8.9	
	50	13.4	-9.8	50	12.4	-8.8
		13.7	-10.1		12.1	-8.5
		13.9	-10.3		12.4	-8.8
	14.0	-10.4		12.9	-9.3	
	14.3	-10.7		13.1	-9.5	
1300	14.5	-10.9	1500	13.0	-9.4	
	14.7	-11.1		13.0	-9.4	
	15.0	-11.4		12.7	-9.1	
	14.7	-11.1		12.5	-8.9	
	14.5	-10.9	X	12.6	-9.0	
	50	14.5	-10.9	50	13.0	-9.4
		14.0	-10.4		13.2	-9.6
1370	13.6	-10.0	1570	13.2	-9.6	

STA - 68+00			5-21-47		
DIST	SOUND		DIST	SOUND	
1580	13.5 12.5	-9.9	1780	14.3	-10.7
<u>10:50</u>	13.5	-9.9		14.3	-10.7
1600	13.5	-9.9	1800	14.7	-11.1
(3.6)	13.5	-9.9	<u>10:53</u>	15.0	-11.4
	13.1	-9.5	(3.6)	15.3	-11.7
	13.1	-9.5		15.3	-11.7
x	13.1	-9.5	x	15.0	-11.4
50	13.2	-9.6	50	14.9	-11.3
	13.1	-9.5		14.4	-10.8
	13.0	-9.4		14.0	-10.4
	12.9	-9.3		13.6	-10.0
	13.1	-9.5		13.4	-9.8
1700	13.5	-9.9	1900	13.4	-9.8
	13.9	-10.3	<u>10:55</u>	13.7	-10.1
	14.0	-10.4		14.0	-10.4
	14.0	-10.4		14.2	-10.6
x	14.0	-10.4	x	14.4	-10.8
50	14.1	-10.5	50	14.4 ⁷	-11.1
	14.1	-10.5		15.0	-11.4
1770	14.1	-10.5	1970	15.0	-11.4

STA - 68+00			5-21-47		
DIST	SOUND		DIST	SOUND	
1980	15.0	-11.4	2180	17.3	-13.6
(3.6)	14.8	-11.2		16.8	-13.1
2000	14.8	-11.2	2200	17.0	-13.3
	15.1	-11.5	(3.7)	17.4	-13.7
	15.5	-11.9		17.2	-13.5
	16.0	-12.4		17.0	-13.3
(3.6)	16.0	-12.4	x	16.7	-13.0
50	16.0	-12.4	50	16.4	-12.7
<u>10:58</u>	16.1	-12.5		16.5	-12.8
(3.7)	16.0	-12.4		16.4	-12.7
	16.0	-12.4	<u>11:03</u>	16.5	-12.8
	16.5	-12.9		16.8	-13.1
2100	16.3	-12.7	2300	16.5	-12.8
	16.7	-12.6		16.3	-12.6
	16.7	-13.0		16.3	-12.6
11:00	16.8	-13.1		16.5	-12.8
	16.7	-13.0		16.8	-13.1
50	16.5	-12.8	50	16.0	-12.3
	16.5	-12.8		15.4	-11.7
2170	16.6	-12.9	2370	15.4	-11.7

STA - 68+00 5-21-47

DIST	SOUND	DIST	SOUND
2380	15.1 -11.4		
(3.7)	15.1 -11.4		
2400	15.2 -11.5		
	15.0 -11.3		
	15.3 -11.6		
	15.3 -11.6		
X	15.0 -11.3		
50	14.8 -11.1		
	14.5 -10.8		
	14.5 -10.8		
	14.8 -11.1		
	15.2 -11.5		
2500	14.0 14.0 -10.3		
	13.0 -9.3		
	13.4 -9.7		
	11.5 -7.8		
X 2540	11.1 -7.4		
<u>11.08</u>			

SOUND WEST STA - 69+00 5-21-47 (33)

2400 FT - 580' W of Causeway $\frac{3}{4}$ INCHES ARE RUN AT $81^{\circ}35'44''$ TO B/L

DIST	SOUND	DIST	SOUND
180	13.8 -10.1		
0+00	+7' EDGE CUT		
1121			
0+85			
0+10	1.0 +3.7	200	13.6 -9.9
(3.7)	3.0 +0.7	(3.7)	13.8 -10.1
	8.4 -4.7		13.9 -10.2
	11.1 -7.4		14.4 -10.7
50	11.1 -7.4		14.4 -10.7
	11.0 -7.3	50	13.4 -9.7
	10.9 -7.2	1425	12.3 -8.6
	11.0 -7.3		14.0 -10.3
	11.2 -7.5		15.4 -11.7
190	11.3 -7.6		15.0 -11.3
	11.6 -7.9	300	14.5 -10.8
	11.8 -8.1		15.0 -11.3
	11.7 -8.0		15.2 -11.5
	12.5 -8.8		14.7 -11.0
50	12.5 -8.8		14.4 -10.7
	12.0 -8.3	50	16.1 -12.4
170	13.7 -10.0	360	16.8 -13.1

STA- 69+00			5-21-47		
DIST	SOUND		DIST	SOUND	
370	17.0	-13.3	570	17.0	-13.3
	19.2	-15.5		16.5	-12.8
(3.7)	18.5	-14.8	(3.7)	16.0	-12.3
400	18.2	-14.5	600	15.6	-11.9
	19.4	-15.7		15.0	-11.3
	20.0	-16.3		14.6	-10.9
	20.0	-16.3		14.5	-10.8
	19.5	-15.8		14.3	-10.6
50	20.0	-16.3	50	14.7	-11.0
	19.8	-16.1	660	14.7	-11.0
<u>11:28</u>	19.8	-16.1	<u>11:27</u>		
<u>11:35</u>	17.8	-14.1			
	17.0	-13.3			
500	21.0	-17.3			
	21.2	-17.5			
	21.0	-17.3			
	20.0	-16.3			
	18.1	-14.4			
50	18.0	-14.3			
560	17.6	-13.9			

SOUND WEST			STA-70+00			5-21-47 (33)		
2000 FT. - 430' W OF CAUSEWAY 3/4. LINES ARE RUN AT 90° 00' 00" TO 7/4								
DIST	SOUND		DIST	SOUND		DIST	SOUND	
0700	+?					200	14.5	-10.8
<u>11:45</u>							14.1	-10.4
0720	0.0	+3.7					14.3	-10.6
0730	1.5	+2.2					14.0	-10.3
(3.7)	2.0	+1.7				<u>11:48</u>	14.0	-10.3
50	2.6	+1.1				(3.7)	14.0	-10.3
	3.0	+0.7				50	14.5	-10.8
	4.1	-0.4					14.9	-11.2
	6.0	-2.3					14.6	-10.9
	8.2	-4.5					14.8	-11.1
100	10.0	-6.3					16.0	-12.3
	10.9	-7.2				300	17.0	-13.3
	11.9	-7.3					17.0	-13.3
	11.1	-7.4					17.7	-14.0
	11.5	-7.8					17.5	-13.8
50	13.0	-9.3					17.0	-13.3
	14.4	-10.7				50	18.8	-15.1
	14.0	-10.3					17.2	-13.5
	13.7	-10.0					15.0	-11.3
190	13.8	-10.1				380	14.4	-10.7

STA 70+00

5-21-47

DIST	SOUND	DIST	SOUND
390	16.4 -12.7		
400	16.5 -12.8		
(3.7)	16.5 -12.8		
	16.0 -13.3		
	15.8 -13.1		
	15.5 ¹¹ -12.8		
50	15.0 -11.3		
	15.0 -11.3		
	14.7 -11.0		
	14.7 -11.0		
	16.3 -12.6		
500	16.3 -12.6		
	15.0 -11.3		
	14.2 -10.5		
	14.0 -10.3		
	14.0 -10.3		
50	13.0 -9.3		
	13.0 -9.3		
570	13.0 -9.3		

11:50

PROFILE ALONG W. SIDE -

5-21-47

(34)

- SOUTH CAUSEWAY BRIDGE
SOUND SOUTH ALONG W. CAUSEWAY 3/4

0+00 = 80+05

DIST	SOUND	DIST	SOUND
	10.5		
0+00	11.5 -7.1	170	15.0 -11.6
13:27	14.0		
10	13.2 -10.6		16.0 -12.6
(3.4)	18.5	(3.4)	15.2 -11.8
	14.5		
	18.0 -11.1	200	14.3 -10.9
	12.0 -8.6		15.4 -12.0
50	9.4 -6.0		16.0 -12.6
	9.4 -6.0		15.0 -11.6
	9.5 -6.1		13.7 -10.3
	10.2 -6.8	50	14.8 -11.4
	12.5 -9.1		14.0 -10.6
100	15.0 -11.6	12:55	12.9 -9.5
12:52	14.7 -11.3		14.3 -10.9
	14.0 -10.6		14.8 -11.4
	14.1 -10.7	300	12.7 -9.3
	15.0 -11.6		12.5 -9.1
50	15.4 -12.0		15.0 -11.6
160	14.5 -11.1	330	13.7 -10.3

W/SIDE			S/CAUSEWAY			BRIDGE			5-21-47			PROFILE ALONG			5-21-47		
DIST			SOUND			DIST			SOUND			EAST SIDE-SOUTH CAUSEWAY BRIDGE			(35)		
340	12.0	-8.6	540	13.0	-9.7												
x 50	14.1	-10.7	50	14.7	-11.4				0+00 = 80+12								
(3.4)	14.3	-10.9	^{13:00}	13.0	-9.7				DIST	SOUND		DIST	SOUND				
	13.0	-9.6	(3.3)	13.0	-9.7				0+00	16.4	-8.1	170	18.0	-14.7			
	11.1	-7.7		14.1	-10.8				^{13:11}	15.5	-12.2		18.0	-14.7			
	10.3	-6.9		13.2	-9.9				(3.2)	17.0	-13.7	(3.3)	16.3	-13.0			
x 400	13.2	-9.8	600	13.0	-9.7					19.1	-15.8	200	16.8	-13.5			
	14.5	-11.1		14.5	-11.2					19.8	-16.5		16.5	-13.2			
(3.4)	13.2	-9.8		16.0	-12.7				50	18.0	-14.7		15.8	-12.5			
^{12:58}	11.4	-8.0		15.2	-11.9					15.7	-12.4	^{13:15}	14.0	-10.7			
(3.3)	13.4	-10.0		15.0	-11.7					17.5	-14.2		14.3	-11.0			
50	13.0	-9.6	50	15.0	-11.7					16.8	-13.5	50	15.0	-11.7			
	14.0	-7.6		14.0	-10.7					15.0	-11.7		13.8	-10.5			
	11.0	-7.6		12.6	-9.3				100	17.2	-13.1		14.1	-7.8			
	12.3	-8.9		12.3	-9.0					17.5	-13.2		13.5	-10.2			
	14.2	-7.8		11.5	-8.2					16.0	-12.7		13.0	-9.7			
500	19.0	-6.6	700	10.4	-7.1					16.0	-12.7	300	11.0	-7.7			
	12.1	-8.7		10.1	-6.8					17.2	-13.9		11.0	-7.7			
	11.8	-8.4	^{13:03}	8.0	-4.7				50	17.2	-14.1		13.0	-9.7			
530	12.0	-8.6	730	4.0	-0.7				160	16.0	-12.7	330	12.0	-8.7			
			740	0.5	+2.8												

EAST SIDE S/CAUSEWAY BRIDGE					
DIST	SOUND		DIST	SOUND	
340	9.5	-6.2	540	12.8	-9.6
Y 50	15.0	-11.7	50	14.0	-10.8
	13.5	-10.2		12.1	-8.9
	11.0	-7.7	(3.2)	12.7	-9.5
	9.7	-6.4		15.3	-12.1
	8.7	-5.3		15.5	-12.3
X 400	13.0	-9.7	600	15.0	-11.8
	13.4	-10.1		18.2	-15.0
	10.2	-6.9		18.0	-14.8
	12.0	-8.7		16.7	-13.5
	12.4	-9.1	13:22	16.0	-12.8
50	11.0	-7.7	50	16.6	-13.4
(3.3)	8.8	-5.5		15.7	-12.5
<u>13:10</u>	11.5	-7.2		15.0	-11.8
(3.2)	12.0	-8.7		13.6	-10.4
	10.0	-6.7		14.0	-11.8
500	8.4	-5.2	700	10.2	-7.0
	12.3	-9.1		10.5	-7.5
	10.8	-7.6		11.3	-8.1
530	9.2	-6.0	730	9.5	-6.3

E/SIDE S/CAUSEWAY BRIDGE					
DIST	SOUND		DIST	SOUND	
740	9.0	-5.8			
50	8.0	-4.8			
757	7.2	-4.0			
(3.2)					

(36)

X

PROFILE ALONG WEST SIDE

5-21-47

NORTH CAUSEWAY BRIDGE : SOUND SOUTH

ALONG WEST CAUSEWAY B/L :

80'
0+00 = ?

35' spans

DIST	SOUND		DIST	SOUND	
13:43 0+00	2 RD CLMN. N. END + ?		160	2.0	+1.0
+13	0.0	+3.0		1.8	+1.2
20	0.2	+2.8	(3.0)	1.8	+1.2
(3.0)	0.8	+2.2		1.8	+1.2
	0.9	+2.1	200	1.7	+1.3
50	1.3	+1.7		1.8	+1.2
	1.5	+1.5		2.5	+0.5
	1.8	+1.2		3.1	-0.1
	2.0	+1.0		4.0	-1.0
	2.0	+1.0	50	4.4	-1.4
100	3.5	-0.5		4.5	-1.5
	4.4	-1.4		5.0	-2.0
	5.0	-2.0		5.2	-2.2
XSP	5.4	-2.4		5.3	-2.3
13:45	4.5	-1.5	300	5.0	-2.0
150	2.8	+0.2	310	5.7	-2.7

W/SIDE N/CAUSEWAY BRIDGE

5-21-47 (37)

DIST	SOUND		DIST	SOUND	
320	6.5	-3.5	520	1.9	+1.1
4:00	6.5	-3.5		1.9	+1.1
	6.0	-3.0	(3.0)	1.3	+1.7
50	6.8	-3.8	50	1.8	+1.2
(3.0)	6.8	-3.8		2.3	+0.7
	6.0	-3.0		3.0	0.0
	3.5	-0.5		4.0	-1.0
	3.3	-0.3		2.8	+0.2
400	3.1	-0.1	600	2.7	+0.3
	2.5	+0.5		2.9	+0.1
	2.5	+0.5		4.0	-1.0
	2.8	+0.2		1.5	-1.5
	2.7	+0.3		0.6	-2.6
50	2.6	+0.4	650	0.5	-2.5
2:50	2.3	+0.7			
	2.4	+0.6			
	2.1	+0.9			
	2.0	+1.0			
500	2.0	+1.0			
510	2.0	+1.0			

PROFILE ALONG EAST SIDE				5-21-47	E/SIDE N/CAUSEWAY BRIDGE				5-21-47
NORTH CAUSEWAY BRIDGE: SOUND SOUTH				DIST	SOUND	N/CAUSEWAY BRIDGE		DIST	SOUND
ALONG EAST CAUSEWAY $\frac{B}{L}$				340	6.7	-3.8	540	4.0	
$\frac{105'}{0+00} = ?$				50	3.4	-0.5	50	4.3	
DIST	SOUND		DIST	SOUND					
14:00	3RD. CLIMB. N-END				5.2	-2.3	(2.9)	2.0	
0+00	0.0		170	3.7	-0.8	14:08		3.0	
	0.0	+2.9		5.2	-2.3	(2.9)		2.7	
(2.9)	0.7	+2.2	(2.9)	5.5	-2.6			3.2	
	1.0	+1.9	200	4.0	-1.1	400	4.6	600	0.7
	2.3	+0.6		4.1	-1.2		3.0	610	0.2
50	2.0	+0.9		6.4	-3.5		1.5	613	0.1
	2.4	+0.5		6.8	-3.9		4.0		
	4.5	-1.6		5.3	-2.4		4.4		
	5.0	-2.1	50	6.5	-3.6	50	1.8		
	4.8	-1.9		8.0	-5.1		1.4		
100	6.0	-3.1		7.5	-4.6		4.5		
14:03	5.4	-2.5		6.7	-3.8		3.5		
	2.5	+0.4		7.2	-4.2	14:10	1.4		
	2.4	+0.5	300	8.0	-5.1	500	4.0		
	2.8	+0.1		7.0	-4.1		4.7		
50	6.4	-3.5		6.4	-3.5		3.0		
160	5.3	-2.4	330	7.8	-4.9	530	1.8		

SOUNDINGS AFTER SHOAL REMOVAL 6-3-47 SOUND EAST STA -75+00 6-3-47 (39)
 PROJECT #7: STA -76+00 SOUND EAST ADUNE B/L.
 0+00 = R-92+23.96: LINES ARE RUN AT 90°00'00" To R/L (DUNE) 0+00 = R-92+23.96: LINES ARE RUN AT 90°00'00" To R/L

DIST	SOUND		DIST	SOUND		DIST	SOUND		DIST	SOUND	
2+09	0.0	+3.4	4+00	11.5	-8.1	2+15	0.0	+3.5	4+00	12.0	-8.5
<u>09:27</u> 2+20	1.4	+2.0		11.5	-8.1	2+20	0.5	+3.0		11.7	-8.2
(3.4)	2.4	+1.0	(3.4)	11.8	-8.4	<u>09:42</u> 1.5	+2.0			11.4	-7.9
	4.3	-0.9		12.0	-8.6	(3.5)	2.4	+1.1	(3.5)	11.4	-7.9
50	7.0	-3.6		12.1	-8.7	50	4.9	-1.4		11.5	-8.0
	8.4	-5.0	50	12.1	-8.7		6.8	-3.3	50	12.0	-8.5
	9.6	-6.2		11.1	-7.7		8.2	-4.7		12.7	-9.2
	10.3	-6.9		11.5	-8.1		8.6	-5.1		13.0	-9.5
	11.0	-7.6		11.5	-8.1		9.4	-5.9		13.0	-9.5
3+00	11.2	-7.8		11.3	-7.9	3+00	10.3	-6.8	<u>09:48</u>	12.0	-8.5
	11.3	-7.9	5+00	11.5	-8.1	<u>09:45</u>	10.5	-7.0	5+00	12.4	-8.9
	11.3	-7.9	<u>09:32</u>				10.9	-7.4		13.0	-9.5
	11.2	-7.8					11.0	-7.5		13.5	-10.0
	11.1	-7.7					11.7	-8.2		13.4	-9.9
50	11.1	-7.7				50	11.8	-8.3		13.4	-9.9
<u>09:30</u>	11.3	-7.9					12.0	-8.5	50	13.0	-9.5
	11.0	-7.6					12.0	-8.5			
	11.6	-8.2					12.0	-8.5			
3+90	11.5	-8.1				3+90	12.0	-8.5			

SOUND EAST
STA-74+00 6-3-47

0+00 = R-32+23.96; LINES ARE RUN AT 90°00'00" To R/L

DIST	SOUND	DIST	SOUND
1+91	0.0 +3.6	3+80	11.3 -7.7
2+00	1.0 +2.6		12.4 -8.8
<u>10:09</u>	1.1 +2.5	4+00	12.4 -8.8
(3.6)	2.0 +1.6	(3.6)	11.8 -8.2
	3.0 +0.6		11.8 -8.2
	4.5 -0.9		11.7 -8.1
50	6.6 -3.0		11.5 -7.9
	7.5 -3.9	50	11.5 -7.9
	8.1 -4.5		11.6 -8.0
	9.0 -5.4		11.6 -8.0
	9.5 -5.9		11.6 -8.0
3+00	10.0 -6.4		11.5 -7.9
	10.4 -6.8	5+00	12.0 -8.4
	10.5 -6.9		12.3 -8.7
<u>10:07</u>	10.6 -7.0		12.5 -8.9
	10.7 -7.1		14.6 -11.0
50	10.5 -6.9	<u>10:10</u>	14.4 -10.6
	11.7 -8.1	50	14.5 -10.9
3+70	11.7 -8.1		

SOUND EAST
STA-73+00 6-3-47 (40)

0+00 = R-32+23.96; LINES ARE RUN AT 90°00'00" To R/L

DIST	SOUND	DIST	SOUND
1+55	0.0 +3.7	3+40	12.0 -8.3
1+60	0.4 +3.3	50	12.0 -8.3
<u>10:25</u>	1.9 +1.8		12.0 -8.3
(3.7)	2.5 +1.2	(3.7)	12.1 -8.4
	3.0 +0.7		12.0 -8.3
2+00	4.5 -0.8		12.0 -8.3
	5.6 -1.9	4+00	12.3 -8.6
	7.0 -3.3		12.4 -8.7
	7.4 -3.7		12.4 -8.7
	7.3 -3.6		12.2 -8.5
50	8.0 -4.3		12.8 -9.1
	8.8 -5.1	50	14.1 -10.4
	9.7 -6.0		14.2 -10.5
	10.4 -6.7		13.7 -10.0
	10.5 -6.8		13.0 -9.3
3+00	10.7 -7.0		13.4 -9.7
<u>10:27</u>	11.0 -7.3	500	14.0 -10.3
	12.3 -8.6	<u>10:30</u>	
3+30	12.0 -8.3		

SOUND
EAST

STA-72+00

6-3-47

0+00 = R-92+23.96 : LINES ARE RUN AT 90°00'00" To R/L

(7)

DIST	SOUND		DIST	SOUND	
1+03	0.0	+3.7	2+90	12.3	-8.6
1+10	0.7	+3.0	3+00	12.2	-8.5
10:49	1.6	+2.1	10:53	11.5	-7.8
(3.7)	2.2	+1.5	(3.7)	11.4	-7.7
	2.8	+0.9		11.8	-8.1
50	5.0	-1.3		12.7	-9.0
	6.1	-2.4	50	14.0	-10.3
	6.0	-2.3		14.8	-11.1
	6.1	-2.4		16.0	-12.3
	7.3	-3.6		16.0	-12.3
2+00	8.0	-4.3		15.0	-11.3
	8.8	-5.1	4+00	14.5	-10.8
	8.5	-4.8			
	9.5	-5.8			
	9.8	-6.1			
50	10.9	-7.2			
	12.1	-8.4			
	12.8	-9.1			
2+80	12.4	-8.7			

CHECK ON LEVEE RUNDUX PROJ # 8, ⁶⁻⁴⁻¹¹

0+00 = Pt. 460' W. OF STA-81+00 CAUSEWAY $\frac{3}{4}$ AND AT -

81°39'44" To B/L: SOUND WEST FROM THIS PT. ALONG SAME LINE.

DIST	SOUND		DIST	SOUND	
0+10	0.0	+2.8	1+90	12.5	-9.7
<u>14:45</u>	0.2	+2.6	2+00	12.4	-9.6
(2.8)	0.2	+2.6	(2.8)	12.0	-9.2
	1.0	+1.8		12.2	-9.4
50	5.1	-2.3		12.5	-9.7
	9.0	-6.2		12.2	-9.4
	12.0	-9.2	50	12.0	-9.2
	12.0	-9.2		12.0	-9.2
	11.5	-8.7		11.5	-8.7
1+00	12.0	-9.2		11.2	-8.4
	11.8	-9.0		11.4	-8.6
	12.0	-9.2	3+00	11.4	-8.6
	12.1	-9.3		11.0	-8.2
	12.0	-9.2		10.7	-7.9
50	12.0	-9.2		11.4	-8.6
	12.1	-9.3		11.0	-8.2
	12.3	-9.5	50	11.5	-8.7
1+80	12.3	-9.5	3+60	12.0	-9.2

P.X. Indexed (42)

0+00 = Pt. 460' W. OF STA-81+00 CAUSEWAY $\frac{3}{4}$ AND AT -

81°39'44" To B/L: SOUND WEST FROM THIS PT. ALONG SAME LINE.

DIST	SOUND		DIST	SOUND	
3+70	11.6	-8.8			
(2.8)	11.8	-9.0			
	11.4	-8.6			
4+00	11.1	-8.3			
	11.5	-8.7			
	11.3	-8.5			
	10.0	-7.2			
	9.3	-6.5			
50	5.0	-2.2			
4+60	0.0	+2.8			

CHECK ON LEVEE RUNOUT 6-4-47
 PROJ. NO. 8.

TX,

6-4-47 (43)

0+00 = PT 540' W. OF STA-82+00 CAUSEWAY 3/4 AND AT 0+00 = PT. 840' W. OF STA-82+00 CAUSEWAY 3/4 AND AT-

81° 29' 44" TO B/L: SOUND SOUTH AT 90° FROM THIS PT. 81° 29' 44" TO B/L: SOUND SOUTH AT 90° FROM THIS PT.

DIST	SOUND		DIST	SOUND		DIST	SOUND		DIST	SOUND	
0+00	1.1	+1.7	1+80	10.6	-7.8	0+23	0.0	+2.8	2+00	12.2	-9.4
<u>1+30</u>	2.8	0.0	(2.8)	11.3	-8.5	0+30	2.0	+0.8		11.5	-8.7
(2.8)	5.4	-2.6	2+00	10.8	-8.0	<u>15:12</u>	4.1	-1.3	(2.8)	12.0	-9.2
	7.8	-5.0	<u>14:58</u>	11.1	-8.3	50	6.5	-3.7		11.9	-9.1
	8.3	-5.5		12.2	-9.4	(2.8)	7.5	-4.7	<u>15:15</u>	12.6	-9.8
50	9.0	-6.2		13.0	-10.2		9.6	-6.8	50	12.7	-9.9
	10.2	-7.4		13.4	-10.6		10.4	-7.6		12.9	-10.1
	10.7	-7.9	50	12.8	-10.0		10.8	-8.0		15.0	-12.2
	11.0	-8.2		11.7	-8.9	1+00	11.0	-8.2		12.8	-10.0
	11.0	-8.2		11.2	-8.4		11.4	-8.6		12.8	-10.0
1+00	11.3	-8.5		10.8	-8.0		11.5	-8.7	3+00	12.5	-9.7
	12.1	-9.3		11.4	-8.6		11.3	-8.5		12.2	-9.4
	12.8	-10.0	3+00	11.2	-8.4		11.3	-8.5		11.7	-8.9
	12.7	-9.9		11.0	-8.2	50	12.0	-9.2		12.0	-9.2
	13.0	-10.2		10.7	-7.9		12.0	-9.2		13.5	-10.7
50	13.5	-10.7		11.1	-8.3		10.8	-8.0	50	13.1	-10.3
	12.3	-9.5	<u>15:00</u>	11.3	-8.5		12.5	-9.7		12.9	-10.1
1+70	10.7	-7.9	50	11.5	-8.7	1+90	12.8	-10.0	3+70	13.3	-10.5

P.A. 6-4-47
DIST SOUND DIST SOUND

3+80 12.5 -9.7

(2.8) 11.5 -8.7

4+00 12.0 -9.2

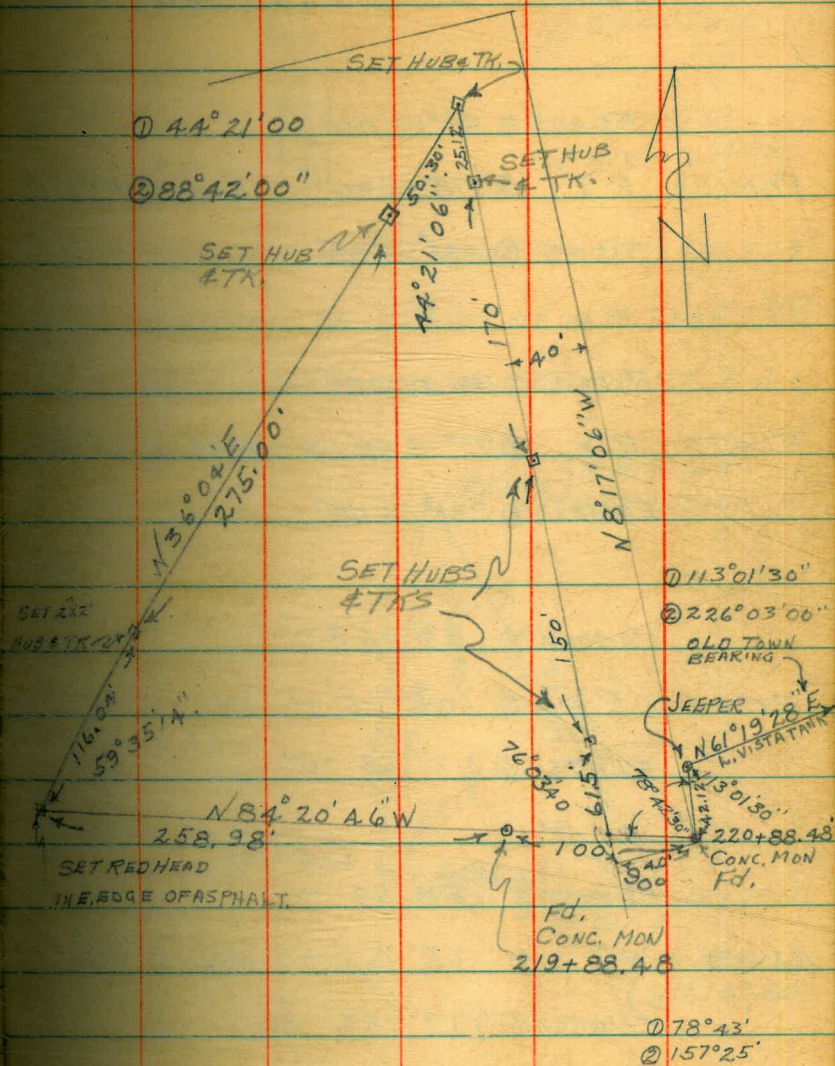
12.3 -9.5

15.18

(49)

SURVEY OF PORTION OF
 PUEBLO LOT 205 SHOWING
 LAND ACQUIRED BY CITY
 OF SAN DIEGO BY CONDEMNATION

6-12-47



TRIANGULATION OF CITY MON

"FAMOSA" & CHURCH

STA OBJECT SIX ANGLES VERNIER MEAN

FLATS @ 89° 17' 00"

FAMOSA R ↗ @ 178° 34' 30" 0° 00' 00" 89° 17' 15"

RIDGE @ 535° 43' 30"

535 42

RIDGE @ 38° 39' 00"

FLATS R ↗ @ 77° 18' 00" 0° 00' 00" 38° 39' 00"

FAMOSA @ 231° 54' 00"

FAMOSA @ 52° 04' 30"

RIDGE R ↗ @ 109° 08' 00" 0° 00' 00" 52° 04' 30"

FLATS @ 312' 23' 30"

FAMOSA @ 37° 59' 00"

FLATS R ↗ @ 75° 58' 00" 0° 00' 00" 37° 59' 10"

CHURCH @ 227° 55' 00"

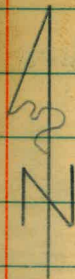
Indexed

6-12-47

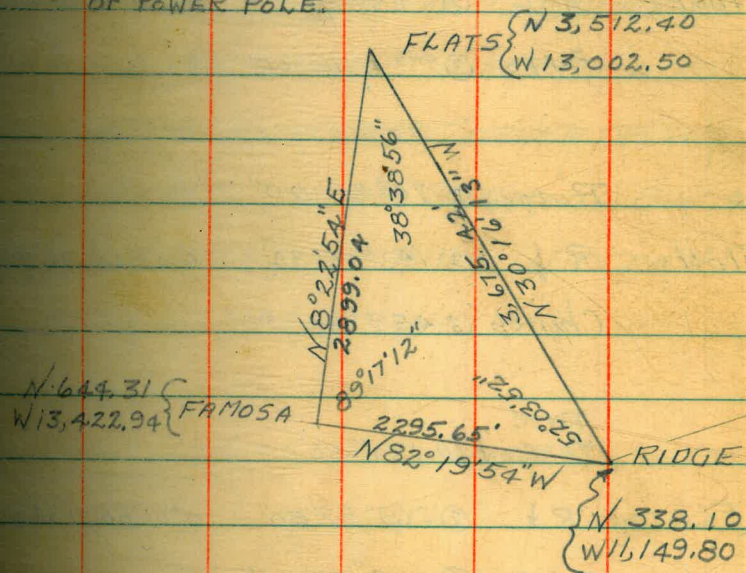
46

T. STAMPER
C. BARRAGAN
A. SHERRY
N. STANLEY

WEATHER
FAIR - WARM

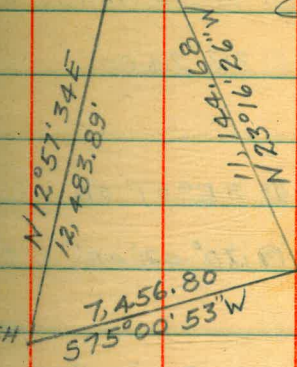
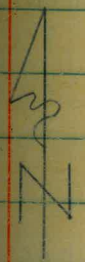


NOTE: "FAMOSA" IS 6" CONC MON. MKD CITY ENGR. &
IS LOCATED ON N. SIDE OF W. PT. LOMA BLVD
& APPROX 150' W. OF + OF FAMOSA ST. & 4' N.
OF POWER POLE.



6-13-47
 BARRAGAN (47)
 SHERRY
 STANLEY
 CALM & CLEAR

N 10,575.90 } BAY PT.
 W 15,553.36 }



COMPUTED
 6-17-47
 T.A. STAMPER
 RIDGE { N 338.10
 W 1,149.80 }

S 1,590.01 }
 W 18,353.01 }

CHURCH

STATION "CHURCH" IS THE DOME ON
 THE NEW CATHOLIC CHURCH LOCATED
 ON THE SOUTH EAST CORNER OF THE
 INTERSECTION OF SARATOGA AVE &
 SUNSET CLIFFS BLVD IN OCEAN
 BEACH CALIF

STA	OBJECT	SIX	ANGLES	VERNIER	MEAN
	CHURCH	①	176° 56' 00"		
RIDGE	R ↓ MARSTON'S	②	353° 52' 00"	0° 00' 00"	176° 56' 00"
	TOWER	③	1061° 35' 00"		
	CHURCH	①	74° 43' 00"		
RIDGE	R ↓	②	149° 25' 30"	0° 00' 00"	74° 43' 00"
	FLATS	③	448° 16' 00"		
	Ridge	①	76° 38' 00"		
Flatts	R ↓	②	153° 15' 30"	0° 00' 00"	76° 37' 45"
	Church	③	459° 46' 30"		
	TWR MARSTON'S	①	134° 56' 00"		
FLATS	R ↓	②	269° 52' 30"	0° 00' 00"	134° 56' 00"
	CHURCH	③	809° 37' 00"		

6-13-47

48

STA OBJECT SIX ANGLES VERNIER MEAN

RIDGE @ $36^{\circ}14'00''$

BAY PT. R \checkmark @ $72^{\circ}28'00''$ $0^{\circ}00'00''$ $36^{\circ}14'00''$

CHURCH @ $217^{\circ}24'00''$

RIDGE @ $35^{\circ}21'00''$

BAY PT. R \checkmark @ $70^{\circ}42'00''$ $0^{\circ}00'00''$ $35^{\circ}21'$

"C"

RADIUS

TWR

MARKSTONS @ $163^{\circ}36'00''$

CAUSEWAYEN R @ $327^{\circ}12'00''$ $0^{\circ}00'00''$ $163^{\circ}36'00''$

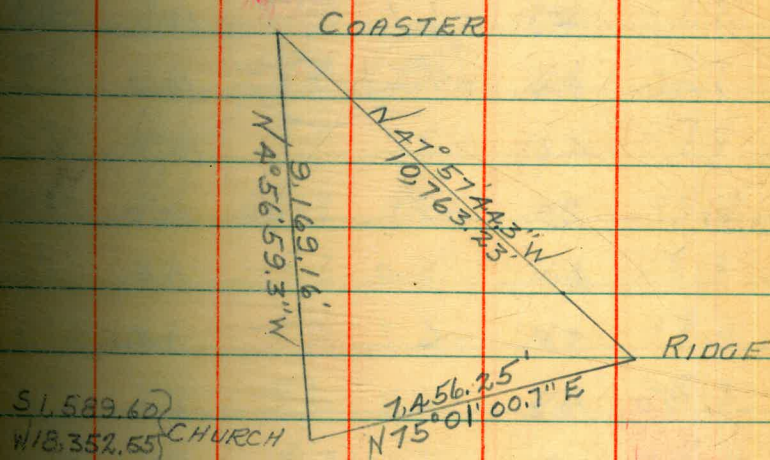
"C"

RADIUS

TRIANGULATION OF "CHURCH"

STA	OBJECT	SIX	ANGLES	VERNIER	MEAN	HORIZON	ADJ. ANGLE	
	RIDGE	①	43°	01'	00"			
U.S.C. & G.S.	↓							
COASTER		R.	②	86°	02'	00"	00° 00' 00"	43° 01' 43"
						360° 00' 30"	43° 00' 45"	
	CHURCH	③	258°	04'	45"			
	CHURCH	①	57°	01'	00"			
	↓							
RIDGE		R.	②	104°	03'	00"	00° 00' 00"	57° 01' 16"
						251° 59' 45"	57° 01' 16"	
	COASTER	③	342°	07'	30"			

CLEAR & COOL
VISIBILITY GOOD



SOUNDINGS PROJECT # 8

6-27-47
BARBARA ANN
SHERRY
STANLEY0+00 = { STA-101+00
P-27+30 } : SOUND WEST AT 90°

PX.	STA-101+00					
DIST	SOUND	DIST	SOUND			
0+16	0.0	+3.4	2+00	12.3	-8.9	
0+30	2.0	+1.4		12.0	-8.6	
<u>15:00</u> 40	3.0	+0.4		12.0	-8.6	
	50	3.5		12.0	-8.6	
		4.1		12.0	-8.6	
		4.2	50	12.0	-8.6	
(3.4)	4.3	-0.9		12.1	-8.7	
	4.5	-1.1	<u>15:05</u>	12.3	-8.9	
1+00	5.0	-1.6	(3.5)	12.3	-8.9	
	6.6	-3.2		12.1	-8.6	
<u>15:03</u>	7.3	-3.9	3+00	12.0	-8.5	
	8.4	-5.0		11.7	-8.2	
	9.5	-6.1		11.4	-7.9	
50	10.2	-6.8		11.1	-7.6	
	11.0	-7.6		11.1	-7.6	
	11.8	-8.4	50	11.1	-7.6	
	12.0	-8.6		11.3	-7.8	
1+90	12.3	-8.9	3+70	11.8	-8.3	

PX	STA-101+00					
DIST	SOUND	DIST	SOUND			
3+80	12.0	-8.5		11.1	-7.6	
	12.2	-8.7		11.1	-7.6	
4+00	12.0	-8.5	6+00	11.5	-8.0	
	12.2	-8.7		11.3	-7.8	
<u>15:08</u>	12.2	-8.7		11.1	-7.6	
	12.3	-8.8		11.0	-7.5	
	12.5	-9.0		11.4	-7.9	
50	13.0	-9.3	50	11.1	-7.6	
	13.3	-9.8	<u>15:10</u>	11.2	-7.7	
(3.5)	13.0	-9.3		11.2	-7.7	
	12.7	-9.2	(3.5)	11.2	-7.7	
	11.6	-8.1		11.3	-7.8	
5+00	11.6	-8.1	700	11.5	-8.0	
	11.7	-8.2		11.8	-8.3	
	11.7	-8.2		11.9	-8.4	
	11.7	-8.2		11.8	-8.3	
	11.7	-8.2		12.0	-8.5	
50	11.7	-8.2	50	12.0	-8.5	
	11.5	-8.0		11.9	-8.4	
5+70	11.1	-7.6	7+70	11.7	-8.2	

6-27-47
Indexed (50)

PX STA-101+00				TX STA-97+00			
DIST	SOUND		DIST	SOUND		SOUNDINGS PROJECT #8	
7+80	12.5	-9.0	9+80	10.5	-7.0	STOO=PT. 500' W. OF STA-97+00 CAUSEWAY $\frac{3}{4}$ LINES	
	12.7	-9.2		10.8	-7.2	LAD RUN AT $81^{\circ}29'44''$ TO $\frac{3}{4}$	
8+00	12.5	-9.0	10+00	11.0	-7.4	DIST	SOUND
	12.0	-8.5		11.0	-7.4	0+7	0.0 +2.6 1+70 10.0 -7.4
	12.0	-8.5		10.5	-7.0	0+10	0.5 +2.1 10.0 -7.4
	11.3	-7.8	(3.6)	10.7	-7.1	^{13:15} 20	4.3 -1.7 ^{13:17} 10.2 -7.6
	11.4	-7.9		11.4	-7.8		5.3 -2.7 2+00 10.2 -7.6
50	11.3	-7.8	50	11.2	-7.6		6.4 -3.8 9.8 -7.2
(3.5)	11.4	-7.7		11.0	-7.4	50	7.0 -4.4 9.7 -7.1
	11.4	-7.9	^{15:15}	10.5	-6.9	(2.6)	8.0 -5.4 (2.6) 9.7 -7.1
	11.4	-7.9		10.5	-6.9		9.1 -6.5 9.4 -6.8
	11.3	-7.8		10.5	-6.9		10.0 -7.4 50 9.1 -6.5
9+00	11.3	-7.8	11+00	10.4	-6.8		10.7 -8.1 10.0 -7.4
	11.2	-7.7		10.4	-6.8	1+00	10.7 -8.1 9.0 -6.4
	11.8	-8.3		10.4	-6.8		10.6 -8.0 9.0 -6.4
	10.5	-7.0		10.7	-7.1		10.0 -7.4 9.0 -6.4
	10.5	-7.0		11.3	-7.7		10.0 -7.4 3+00 8.8 -6.2
50	10.6	-7.1	50	11.7	-8.1		10.5 -7.9 8.0 -5.4
	10.8	-7.3		12.0	-8.4	50	10.5 -7.9 7.8 -5.2
9+70	10.6	-7.1	11+70	12.3	-8.7	1+00	10.4 -7.8 3+30 7.1 -4.5

8-30-97 (51)

6-30-47
 TX STA - 97+00
 DIST SOUND DIST SOUND
 3+40 2.7 -0.1
 50 3.0
 8.0 -0.4
 (26) 60 1.5 +1.1
 3+67 0.0 +2.6
 13:20

6-30-47
 TX STA - 98+00
 0+00 = Pt 433' W. OF STA - 98+00 CAUSEWAY B/L:
 LINES ARE RUN AT 81° 33' 44" To B/L.
 DIST SOUND DIST SOUND
 0+10 0.0 +2.5 1+90 11.3 -8.8
 12:25 20 4.1 -1.6 2+00 12.0 -9.5
 30 5.3 -2.8 13:28 11.5 -9.0
 6.4 -3.9 11.7 -9.2
 50 7.8 -5.3 12.8 -10.3
 8.0 -5.5 12.3 -9.8
 (2.5) 8.5 -6.0 50 11.5 -9.0
 9.1 -6.6 10.0 -7.5
 9.5 -7.0 (2.5) 11.0 -8.5
 1+00 10.5 -8.0 10.5 -8.0
 11.0 -8.3 10.8 -8.3
 11.0 -8.5 3+00 10.8 -8.3
 11.0 -8.5 11.5 -9.0
 10.9 -8.4 11.5 -9.0
 50 11.0 -8.5 11.5 -9.0
 11.0 -8.5 13:31 11.5 -9.0
 11.0 -8.5 50 11.4 -8.9
 1+80 11.1 -8.6 3+60 11.3 -8.8

PX STA - 98+00

DIST	SOUND	DIST	SOUND
3+70	11.1	-8.6	
	11.1	-8.6	
	10.8	-8.3	
4+00	10.5	-8.0	
	10.2	-7.7	
	10.0	-7.5	
(2.5)	9.6	-7.1	
	8.5	-6.0	
50	7.7	-5.2	
	6.2	-3.7	
	4.0	-1.5	
80	2.0	+0.5	
4+87	0.0	+2.5	

13:34

PX STA - 99+00

6-30-47 (53)

2+00 = Pt. 410' W. OF STA 99+00 CAUSEWAY B/L

LINES APP. RUN AT 81° 33' 14" TO B/L

DIST	SOUND	DIST	SOUND
0+10	0.0	+2.5	1790 11.1 -8.6
0+20	2.8	-0.3	2+00 11.2 -8.7
2+30	6.7	-4.2	11.4 -8.9
	9.0	-6.5	11.4 -8.9
50	9.8	-7.3	11.3 -8.8
	10.1	-7.6	11.5 -9.0
(2.5)	10.5	-8.0	50 11.4 -8.9
	10.5	-8.0	<u>13:45</u> 11.3 -8.8
	10.7	-8.2	11.0 -8.5
1+00	10.5	-8.0	(2.5) 11.3 -8.8
	10.4	-7.9	11.4 -8.9
	10.4	-7.9	3+00 11.5 -9.0
	10.8	-8.3	11.6 -9.1
	11.0	-8.5	12.0 -9.5
50	11.5	-9.0	12.0 -9.5
<u>13:49</u>	11.3	-8.8	12.3 -9.8
	11.4	-8.9	50 12.3 -9.8
1+80	11.5	-9.0	3+60 12.3 -9.8

6-30-97

PX STA - 99+00

DIST	SOUND	DIST	SOUND
3+70	12.5 -9.9		
	12.2 -9.7		
	12.1 -9.6		
4+00	12.0 -9.5		
	11.8 -9.3		
<u>13:47</u>	11.5 -9.0		
	11.1 -8.3		
(2.6)	10.4 -8.8		
50	10.0 -7.4		
	9.5 -6.9		
	8.4 -5.8		
	5.0 -2.4		
	2.8 -0.2		
4+95			
5+00	0.0 +2.6		

6-30-97

P STA - 100+00

1+00 = Pt. 409' W OF STA - 100+00 CAUSEWAY 3/4

LINES ARE RUN AT 81°39'44" TO 3/4

DIST	SOUND	DIST	SOUND
0+09	0.0 +2.6	1+90	10.8 -8.2
0+20	4.0 -1.4	2+00	10.8 -8.2
<u>13:55</u>	5.5 -2.9	<u>13:58</u>	11.4 -8.8
	7.3 -4.7		11.4 -8.8
50	8.0 -5.4		11.0 -8.4
	8.7 -6.1	(2.6)	10.8 -8.2
(2.6)	9.7 -7.1	50	10.5 -7.9
	10.0 -7.4		10.6 -8.0
	10.2 -7.6		11.0 -8.4
1+00	10.3 -7.7		11.0 -8.4
	10.8 -8.2		11.3 -8.7
	11.0 -8.4	3+00	11.5 -8.9
	10.8 -8.2		11.5 -8.9
	11.0 -8.4		11.6 -9.0
50	10.9 -8.3	<u>14:00</u>	11.0 -8.4
	10.8 -8.2		11.2 -8.6
	10.8 -8.2	50	10.7 -8.1
1+80	11.0 +0 -8.4	3+60	11.0 -8.4

6-30-47

PX STA-100+00

DIST	SOUND	DIST	SOUND
3+70	10.6 -8.0		
	11.0 -8.4		
	11.0 -8.4		
4+00	10.9 -8.3		
	10.4 -7.8		
	10.3 -7.7		
(2.6)	10.0 -7.4		
	9.3 -6.7		
50	7.4 -4.8		
<u>14:03</u>	4.1 -1.5		
	1.5 +1.1		
4+73	0.0 +2.6		

6-30-47

PX STA-101+00

(55)

PT. 405' W. OF STA-101+00 CAUSEWAY B/LH:

LINES ARE RUN AT $81^{\circ}39'44''$ TO B/LH

DIST	SOUND	DIST	SOUND
0+00	0.0 +2.7	1+90	10.7 -8.0
0+20	3.5 -0.8	2+00	11.0 -8.3
430	6.1 -3.4		11.1 -8.4
<u>14:10</u>	6.7 -4.0	<u>14:13</u>	11.3 -8.6
50	9.2 -6.5		11.2 -8.5
	8.0 -5.3		10.8 -8.1
(2.7)	9.3 -6.6	50	10.4 -7.7
	9.3 -6.6	(2.7)	10.0 -7.3
	10.5 -7.8		10.4 -7.7
1+00	10.7 -8.0		10.0 -7.3
	10.7 -8.0		10.3 -7.6
	10.5 -7.8	3+00	10.3 -7.6
	10.5 -7.8		10.8 -8.1
	10.5 -7.8		11.6 -8.9
50	10.6 -7.9		11.6 -8.9
	10.5 -7.8		11.8 -9.1
	10.5 -7.8	50	12.0 -9.3
1+80	10.7 -8.0	3+60	11.7 -9.0

101+00 6-30-47		DIST SOUND	
3+70	11.5	-8.8	
	11.3	-8.6	
	11.3	-8.6	
4+00	11.3	-8.6	
	11.3	-8.6	
	10.8	-8.1	
<u>14:15</u>	10.2	-7.5	
<u>(2.7)</u>	10.0	-7.3	
50	6.0	-3.3	
	3.1	-0.4	
	1.5	+1.2	
4+74	0.0	+2.7	

STA-102+00 6-30-47		DIST SOUND	
PT. 362' W. OF STA-102+00 CAUSEWAY B/H			
LINES ARE RUN AT 91° 39' 44" TO B/H			
DIST SOUND		DIST SOUND	
0+15	0.0	+2.8	1+90 11.6 -8.6
0+20	0.8	+2.0	2+00 11.8 -9.0
+30	1.5	+1.3	<u>14:30</u> 11.8 -9.0
14:35 40	3.8	-1.0	11.7 -8.9
50	4.5	-1.7	11.7 -8.9
	5.4	-2.6	<u>(2.8)</u> 11.6 -8.8
<u>(2.8)</u>	7.0	-4.2	50 11.5 -8.7
	9.0	-6.2	11.3 -8.5
	9.3	-6.5	11.3 -8.5
1+00	10.2	-7.4	11.2 -8.4
	10.1	-7.3	11.2 -8.4
	10.1	-7.3	3+00 11.1 -8.3
	11.0	-8.2	11.0 -8.2
	11.5	-8.7	11.0 -8.2
50	11.5	-8.7	11.0 -8.2
	11.6	-8.8	11.0 -8.2
	11.5	-8.7	50 10.8 -8.0
1+80	11.5	-8.7	3+60 11.7 -8.9

STA - 102 + 00

DIST	SOUND	DIST	SOUND
3+70	12.2	-9.4	
<u>14:33</u>	12.2	-9.4	
	11.8	-9.0	
4+00	11.4	-8.6	
	11.4	-8.6	
	11.6	-8.8	
<u>(2.8)</u>	11.4	-8.6	
	11.6	-8.8	
50	11.5	-8.7	
	11.0	-8.2	
	10.7	-7.9	
	9.0	-6.2	
	7.5	-4.7	
5+00	6.7	-3.9	
	5.0	-2.2	
	3.5	-0.7	
	3.2	-0.4	
<u>17:35</u>	3.2	-0.4	
50	1.6	+1.2	
5+55	0.0	+2.8	

SOUNDINGS PROJECT # 8
STAKE #

7-2-47 (57)
BARRAGAN
SHERRY
STANLEY
PT

0+00 = STAKE # 43
LINE WAS RUN AT
15° TO TAN BETWEEN # 41 & # 42 : SOUND N/E

DIST	SOUND	DIST	SOUND
0+65	0.0	+3.3	2+30 12.8 -9.5
0+70	1.3	+2.0	12.6 -9.3
<u>09:27</u> +80	4.0	-0.7	2+50 12.0 -8.7
	3.9	-0.6	<u>09:30</u>
1+00	5.5	-2.2	
	8.3	-4.9	
	8.5	-5.2	
<u>(3.3)</u>	9.0	-5.7	
	10.6	-7.3	
50	11.8	-8.5	
	12.0	-8.7	
	12.4	-9.1	
	12.5	-9.2	
	12.5	-9.2	
2+00	13.0	-9.7	
	13.0	-9.7	
2+20	13.0	-9.7	

STAKE # 42					# "100 W. 42"						
PT					PT						
0+00 = STAKE # 42; LINES ARE RUN AT 90° TO TAN BETWEEN STAKES # 42 & 41; SOUND NORTH					0+00 = PT. 100' W. OF STAKE # 42 AND ON TAN BETWEEN STAKES # 42 & 41; SOUND NORTH.						
DIST	SOUND		DIST	SOUND	DIST	SOUND		DIST	SOUND		
0+88	0.0	+3.4	2+70	11.5	-8.1	0+92	0.0	+3.4	2+90	12.5	-9.1
1+00	4.0	-0.6		11.8	-8.4	1+00	2.0	+1.4		11.6	-8.2
<u>09:33</u>	5.6	-2.2		12.2	-8.8	<u>09:45</u> +10	3.8	-0.4		11.5	-8.1
	7.0	-3.6	3+00	12.2	-8.8		4.0	-0.6	3+00	12.0	-8.6
	8.0	-4.6		12.5	-9.1		4.6	-1.2		12.4	-9.0
	8.5	-5.1	<u>09:38</u>	12.5	-9.1		7.0	-3.6	(3.4)	12.3	-8.9
50	8.4	-5.0		12.5	-9.1	50	7.5	-4.1	<u>09:50</u>	12.0	-8.6
(3.4)	9.6	-6.2	(3.4)	12.5	-9.1		8.1	-4.7		12.0	-8.6
	10.3	-6.9	50	12.5	-9.1	(3.4)	10.0	-6.6	50	11.8	-8.4
<u>09:35</u>	11.0	-7.6		12.7	-9.3		10.5	-7.1		11.8	-8.4
	11.4	-8.0		12.7	-9.3		11.6	-8.2		11.8	-8.4
2+00	12.0	-8.6		12.4	-9.0	2+00	12.1	-8.7		12.1	-8.7
	12.0	-8.6		12.0	-8.6		12.7	-9.3		12.0	-8.6
	12.0	-8.6	4+00	11.8	-8.4		13.0	-9.6	4+00	11.8	-8.4
	12.0	-8.6		11.6	-8.2	<u>09:43</u>	13.0	-9.6		11.5	-8.1
	11.8	-8.4		11.0	-7.6		13.0	-9.6		9.5	-6.1
50	11.5	-8.1	<u>09:40</u>	8.7	-5.2	50	12.9	-9.5		3.0	+0.4
				1.5	+1.9				+40	2.0	+1.4
2+60	11.5	-8.1	4+40 4+50	1.5	+1.9	2+60	12.5	-9.1	4+50	1.8	+1.6

SOUND NORTH # " 200' W" PX 7-2-47
 0+00 = Pt. 200' W. OF STAKE # 42 AND ON TAN BETWEEN #41 & #42

STAKES # 41 & 42: LINES ARE RUN AT 90° TO TAN

DIST	SOUND		DIST	SOUND	
0+95	0.0	+3.4	2+70	12.5	-9.1
1+00	0.9	+2.5		12.1	-8.7
09:58 +10	4.0	-0.6		11.8	-8.4
	4.5	-1.1	3+00	12.0	-8.6
	6.0	-2.6		12.1	-8.7
(3.4)	7.4	-4.0	(3.4)	12.0	-8.6
50	8.5	-5.1		12.0	-8.6
	8.5	-5.1		12.4	-9.0
	9.5	-6.1	50	12.5	-9.1
	10.3	-6.9	10:03	12.5	-9.1
	11.5	-8.1		12.0	-8.6
2+00	12.0	-8.6		12.0	-8.6
	12.4	-9.0		12.4	-9.0
	12.4	-9.0	4+00	12.4	-9.0
10:00	12.4	-9.0		12.4	-9.0
	12.4	-9.0		12.0	-8.6
50	12.4	-9.0	10:05	9.5	-6.1
				4.7	-1.3
2+60	12.5	-9.1	4+50	2.0	+1.0

" 300' W" PX 7-2-47 (59)
 0+00 = Pt. 300' W. OF STAKE # 42 AND ON TAN BETWEEN #41 & #42

* LINES ARE RUN AT 90° TO TAN: SOUND NORTH

DIST	SOUND		DIST	SOUND	
0+94	0.0	+3.4	2+70	13.5	-10.1
1+00	1.0	+2.4		12.8	-9.4
1+10	4.7	-1.3		12.6	-9.2
	5.0	-1.6	3+00	12.6	-9.2
	7.5	-4.1		12.7	-9.2
(3.4)	7.7	-4.3	10:15	12.7	-9.2
50	8.3	-4.9	(3.5)	12.7	-9.2
	9.4	-6.0		12.5	-9.0
	11.0	-7.6	50	12.2	-8.7
	11.8	-8.4		12.2	-8.7
	12.3	-8.9		12.4	-8.9
2+00	12.3	-8.9		12.5	-9.0
	12.2	-8.8		12.5	-9.0
	12.5	-9.1	4+00	12.5	-9.0
	13.0	-9.6		12.6	-9.1
	13.1	-9.7		12.3	-8.8
50	13.4	-10.0	10:18	8.8	-5.3
			1+40	2.7	+0.8
2+60	13.5	-10.1	4+50	2.5	+1.0

STAKE # 41

7-2-47

0+00 = STAKE # 41 : LINES ARE RUN AT 90° TO TAN
 BETWEEN STAKES # 42 & # 41 : SOUND NORTH

DIST	SOUND	DIST	SOUND
------	-------	------	-------

0+37	0.0	+3.5	
------	-----	------	--

1+10	1.3	+2.2	
------	-----	------	--

<u>10:27</u>	3.2	+0.3	
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	5.4	-1.9	
--	-----	------	--

<u>3.5</u>	6.0	-2.5	
------------	-----	------	--

5.0	7.1	-3.6	
-----	-----	------	--

	9.0	-5.5	
--	-----	------	--

	10.3	-6.8	
--	------	------	--

	11.1	-7.6	
--	------	------	--

	11.6	-8.1	
--	------	------	--

2+00	12.10	-8.5	
------	-------	------	--

	12.5	-9.0	
--	------	------	--

	12.8	-9.3	
--	------	------	--

	13.0	-9.5	
--	------	------	--

2+40	13.0	-9.5	
------	------	------	--

STAKE # 40

7-2-47 (60)

0+00 = STAKE # 40 : LINES ARE RUN RADIAL
 THROUGH STAKE # 40 : SOUND N/W

DIST	SOUND	DIST	SOUND
------	-------	------	-------

0+87	0.0	+3.5	
------	-----	------	--

1+00	2.8	+0.7	
------	-----	------	--

4+0	3.5	0.0	
-----	-----	-----	--

	4.0	-0.5	
--	-----	------	--

<u>3.5</u>	5.0	-1.5	
------------	-----	------	--

	5.6	-2.1	
--	-----	------	--

5.0	7.0	-3.5	
-----	-----	------	--

	8.0	-4.5	
--	-----	------	--

	9.5	-6.0	
--	-----	------	--

	10.5	-7.0	
--	------	------	--

	11.0	-7.5	
--	------	------	--

2+00	12.0	-8.5	
------	------	------	--

	12.0	-8.5	
--	------	------	--

	12.1	-8.6	
--	------	------	--

	12.5	-9.0	
--	------	------	--

1+44	12.0	-8.5	
------	------	------	--

5.0	12.0	-8.5	
-----	------	------	--

2+60	12.0	-8.5	
------	------	------	--

STAKE # 39

7-2-47

0+00 = STAKE # 39 : LINES ARE RUN RADIALY THROUGH

STAKE # 39: SOUND NORTH WEST

DIST SOUND DIST SOUND

0+82 0.0 +3.5

0+90 1.0 +2.5

¹⁺⁰⁰
10:54 2.5 +1.0

+10 4.0 -0.5

5.5 -2.0

3.5 6.4 -2.9

7.0 -3.5

50 8.0 -4.5

9.8 -6.3

11.0 -7.5

11.5 -8.0

12.0 -8.5

2+00

STAKE # 38

7-2-47

0+00 = STAKE # 38 : LINES ARE RUN RADIALY THROUGH

STAKE # 38: SOUND N/W

DIST SOUND DIST SOUND

0+87 0.0 +3.4

1+00 2.0 +1.4

¹⁺⁰²
+10 3.0 +0.4

3.5 -0.1

5.0 -1.6

3.4 7.3 -3.9

50 7.3 -3.9

9.0 -5.6

9.5 -6.1

10.5 -7.1

10.8 -7.4

2+00 10.8 -7.4

11.0 -7.6

2+20 11.0 -7.6

(61)

SOUNDINGS - DANA BASIN PROJ. #7 7-2-47

STA - 62+00

PX

DIST

STA - 62+00

7-2-47

PX

(62)

SOUND

DIST

SOUND

Indexed

0+00 = Pt. 410' W. OF STA - 62+00 CAUSEWAY B/A.

3+50

12.4

-9.6

LINES ARE RUN AT 81° 09' 44" TO B/A: SOUND WEST.

12.4

-9.6

DIST SOUND

DIST SOUND

12.4

-9.6

0+09 0.0 +2.8

1+80 12.4 -9.6

12.0

-9.2

0+20 1.0 +1.8

12.5 -9.7

9.0

-6.2

12:45

2.5 +0.3

2+00 12.9 -10.1

4+00

8.0

-5.2

5.0 -2.2

12.7 -9.9

7.4

-4.6

50 5.5 -2.7

12:50

13.0 -10.2

7.3

-4.5

6.0 -3.2

12.7 -9.9

(2.8)

6.0

-3.2

6.4 -3.6

(2.8)

13.0 -10.2

5.1

-2.3

(2.8) 7.2 -4.4

50 12.8 -10.0

50

4.3

-1.5

7.8 -5.0

12.9 -10.1

12:55

2.1

+0.7

1+00 8.7 -5.9

12.7 -9.9

0.8

+2.0

10.2 -7.4

11.5 -8.7

4+00

0.0

+2.8

10.0 -7.2

11.0 -8.2

12.0 -9.2

3+00 11.0 -8.2

12:46

12.7 -9.9

11.5 -8.7

50 12.8 -10.0

11.7 -8.9

12.4 -9.6

12.0 -9.2

1+70 11.6 -8.8

3+40 12.4 -9.6

STAKE # 13 PX 7-2-47
 0+00 = STAKE # 13 DANA BASIN: LINES ARE RUN IN

THE DIRECTION OF RADIUS: SOUND NORTH WEST RUN IN THE DIRECTION OF RADIUS OF CIRCLE.

DIST.	SOUND	DIST	SOUND
0+42	0.0	+2.6	
0+50	1.5	+1.1	
<u>13:18</u>	4.5	-1.9	
1+00	5.6	-3.0	
	6.5	-3.9	
<u>2.6</u>	8.0	-5.4	
1+00	9.6	-7.0	
	10.0	-7.4	
	11.4	-8.8	
	11.5	-8.9	
<u>13:20</u>	12.4	-9.8	
50	11.2	-8.6	
	12.3	-8.7	
	12.5	-8.9	
	12.5	-8.9	
	12.5	-8.9	
2+00	12.5	-8.9	
2+10			

STAKE # 15 PX 7-2-47 (63)
 0+00 = STAKE # 15 DANA BASIN: LINES ARE

THE DIRECTION OF RADIUS OF CIRCLE.

DIST	SOUND	DIST	SOUND
0+42	0.0	+2.6	2+20 11.3 -8.7
+50	1.0	+1.6	<u>13:38</u>
+60	3.2	-0.6	
<u>3.2</u>	5.2	-2.6	
<u>2.6</u>	7.5	-4.9	
	8.0	-5.4	
1+00	9.4	-7.0	
	12.0	-9.4	
	12.4	-9.8	
	12.6	-10.0	
	12.8	-10.2	
50	12.8	-10.2	
	12.8	-10.2	
	12.6	-10.0	
	12.6	-10.0	
	12.5	-9.9	
2+00	11.3	-8.7	
2+10	11.3	-8.7	

FINAL X-SECTIONS PROJECT #7
STA-49+ 10

PX

7-14-47
BARRAGAN
SHERMAN
STANLEY

7-14-47

(62)

(STA-48+00)
R-114+00) STA-49+ 00

PX

DIST	+	H.I.	-	ELEV
T.B.M.	2.41	18.58		16.12
0+00 =	{ STA-49+10 -R-114+00 }		4.2	14.4
E 0+42			11.4	7.2
E 0+85			12.2	6.4
E 130			12.8	5.8
E 190			13.2	5.4
W 32			4.0	14.6
W 45			9.0	9.6
W 55			12.1	6.5
W 85			12.6	6.0
W 125			12.9	5.7
W 148			13.1	5.5
T.P.			12.12	6.46

TOP HUB
R-114+00
STA-49+00

STATE
10' EAST
STA-49+00

DIST	+	H.I.	-	ELEV
TR	5.05	11.51		6.46
0+00			5.0	6.5
E 0+60			5.3	6.2
E 113			5.7	5.8
E 170			6.3	5.2
W 0+21			3.0	8.5
W 0+35			5.0	6.5
W 0+90			6.0	5.5
W 125			6.1	5.4
				6.9
				4.6

Indexed

T.P.

Sta 48+00 TR, 114+00

DIST + H.I. - ELEV

Sta. 48+00

SINGLE SHOT ON STA-48+00 - R-114+00 (GROUND)

GROUND APPARENT TO BE UNCHANGED ALONG SECTION

7-14-47

 $0+00 = \left\{ \begin{array}{l} \text{STA-50+00} \\ \text{R-114+00} \end{array} \right\}$

Sta 50+00

PX

DIST	+	H.I.	-	ELEV
T.B.M.	5.09	19.92		14.83 Sta 51+00
0+00			5.0	14.9
W 0+40			5.0	14.9
W 0+85			5.0	14.9
W 132			5.6	14.6
W 140			9.3	10.6
W 15x1			13.2	6.7
W 195			13.9	6.0
W 240			14.0	5.9

STA- 51+00

 $0+00 = \left\{ \begin{array}{l} \text{STA-51+00} \\ \text{R-114+00} \end{array} \right\}$

SECTIONS ARE AT 90° To R/L

PX

DIST	+	H.I.	-	ELEV
T.B.M.	2.41	18.58		16.17
W 360			12.8	5.8
W 310			12.3	6.3
W 265			11.5	7.1
W 255			8.2	10.4
W 242			3.8	14.8
W 185			3.7	14.9

TOP HUB
R-114+00
STA-50+00

STA-51+00

7-14-47

(65)

DIST	+	H.I.	-	ELEV
W 142		18.58	3.4	15.2
W 95			4.2	14.4
W 35			4.2	14.4
0+00			3.0	13.6

STA-52+00

PX

 $0+00 = \left\{ \begin{array}{l} \text{R-111+00} \\ \text{STA-52+00} \end{array} \right\}$

SECTIONS ARE AT 90° To R/L

DIST	+	H.I.	-	ELEV
T.B.M.	4.54	19.73		15.19
0+00			4.9	14.8
W 30			5.2	14.5
W 60			5.5	14.2
W 70			9.9	9.8
W 76			12.6	7.1
W 110			13.0	6.7
W 160			13.3	6.4

TOP HUB
STA-53+00
R-111+00

PROJECT # 7

7-14-47

STA- 53+ 00

PX

0+00 = {^{STA-53+00}
_{A-111+00}}; SECTIONS ARE AT 90° TO R/L.

DIST	+	H.I.	-	ELEV
T.B.M.	4.40	19.50		15.10
W 290			12.9	6.6
W 250			12.9	6.6
W 225			12.9	6.6
W 185			12.8	6.7
W 180			9.6	9.9
W 170			6.0	13.5
W 125			5.8	13.7
W 70			5.3	14.2
0+00			5.0	14.5

TOP HUB
STA-54+00
A-111+00

X-SECTIONS PROJECT # 8

7-14-47
BARBARA
SHAW
STAMP

(66)

PX

STA- 102+ 00

Indexed

0+00 = {^{STA-102+00}
CAUSEWAY B/L}; SECTIONS AT 81° 40' TO B/L.

DIST	+	H.I.	-	ELEV
B.M.	4.43	16.67		12.24
0+00			4.5	12.2
0+11 W			4.5	12.2
W 52			4.8	11.9
W 110			4.5	12.2
W 168			4.7	12.0
W 230			4.1	12.6
W 285			4.4	12.3
W 332			6.9	9.8
W 360			11.0	5.7
W 370			13.3	3.4

TOP HUB
STA-101+00
CAUSEWAY B/L

PX STA-101+00 7-14-47					PX STA-100+00 7-14-47 (67)						
0+00 = STA-101+00 CAUSEWAY B/L. Sect At 81°39'44" To B/L					0+00 = STA-100+00 CAUSEWAY B/L. Sect At 81°39'44" To B/L						
T.B.M.	+	H.I.	-	ELEV	TOP HUB	DIST	+	H.I.	-	ELEV	TOP HUB
T.B.M.	4.30	16.25		11.95	STA-100+00 CAUSEWAY						
W 110			13.5	2.7		T.B.M.	4.95	16.68		11.73	TOP HUB STA-99+00 CAUSEWAY
W 390			8.1	8.1		0+00			4.7	12.0	
W 370			4.5	11.7		W 0+11			4.8	11.9	
W 325			4.7	11.5		W 70			4.9	11.8	
W 260			4.9	11.3		W 120			4.6	12.1	
W 265			4.5	11.7		W 170			4.7	12.0	
W 150			4.5	11.7		W 295			4.7	12.0	
W 95			4.4	11.8		W 310			4.5	12.2	
W 45			4.4	11.8		W 372			3.9	12.8	
0+00			4.7	11.5		W 395			8.2	8.5	
						W 420			13.0	3.7	

PX STA- 99 + 00 9-14-47
 0+00 = STA- 99+00 CAUSEWAY B/L: SECTIONS ARE AT 0° 55' 44" To B/L

DIST	+	H.I.	-	ELEV.	
B.M.	4.59	16.54		11.95	T.O.P HUB STA-100+00 CAUSEWAY
W 415			13.0	3.5	
W 390			8.2	8.3	
W 370			4.4	12.1	
W 345			4.0	12.5	
W 295			4.4	12.1	
W 230			4.3	12.2	
W 165			4.3	12.2	
W 110			4.6	11.9	
W 75			4.7	11.8	
W 30			4.6	11.9	
0+00			4.8	11.7	

PX STA- 98 + 00 9-14-47 (68)
 0+00 = STA- 98+00 CAUSEWAY B/L: SECTIONS ARE AT 0° 55' 44" To B/L

DIST	+	H.I.	-	ELEV.	
B.M.	4.66	16.39		11.73	T.O.P HUB STA-99+00 CAUSEWAY
0+00				4.7	11.7
W 30				4.3	12.1
W 105				4.1	12.3
W 190				4.2	12.2
W 265				4.2	12.2
W 335				3.9	12.5
W 385				3.3	13.1
W 410				2.5	8.9
W 435				12.4	4.0

Px STA- 97+00 7-14-47

0+00 = STA- 97+00 CAUSEWAY 3/4 SECTION'S AREA AT 81°46' TO 3/4

DIST	+	H.I.	-	ELEV
B.M.	4.45	16.15		11.70
W 495			12.2	3.9
W 470			7.7	8.4
W 440			3.3	12.8
W 390			3.7	12.4
W 330			3.9	12.2
W 265			4.1	12.0
W 205			3.5	12.6
W 130			3.9	12.2
W 65			3.7	12.4
W 11			4.0	12.1
0+00			4.7	11.4

TOP NUB
STA-98+00
CAUSEWAY

Px STA- 96+00 7-14-47 (29)

0+00 = STA- 96+00 CAUSEWAY 3/4 SECTION'S AREA AT 81°46' TO 3/4

DIST	+	H.I.	-	ELEV.
B.M.	4.61	16.08		11.47
0+00			4.8	11.3
W 13			4.5	11.6
W 52			4.3	11.8
W 115			4.2	11.9
W 195			4.1	12.0
W 265			4.1	12.0
W 330			4.0	12.1
W 385			4.5	11.6
W 465			4.4	11.7
W 535			4.1	12.0
W 565			5.5	10.6
W 605			7.3	8.8
W 645			9.2	6.9
W 710			8.7	7.4
W 745			7.7	8.4
W 800			5.0	11.1
W 840			4.1	12.0
W 905			4.0	12.1

TOP NUB
STA-97+00
CAUSEWAY

DX
0+00 - STA - 95+00 CAUSEWAY B/L: SECTIONS ARE AT 81°40' TO B/L.

DIST	T	H.I.	-	ELEV	TOP HUB STA - 96+00 CAUSEWAY
B.M.	4.64	15.99		11.35	
W 885			3.5	11.5	
W 780			4.5	11.5	
W 690			3.8	12.2	
W 560			3.8	12.2	
W 455			3.8	12.2	
W 325			3.8	12.2	
W 240			4.0	12.0	
W 150			3.8	12.2	
W 80			3.6	12.4	
W 30			4.3	11.7	
0+00			4.8	11.2	

116. 4-26-51

STA	T	H.I.	-	ELEV	CITY BM NEAR STATE
B.M.	5.20	17.20		12.00	
79 W.			5.0	12.2	
80 W			5.8	11.4	
81 W			5.6	11.6	
82			5.4	11.8	
83			5.0	12.2	
84			4.8	12.4	
85			5.1	12.1	
86			5.7	11.5	
87			5.1	12.1	
88			4.0	13.2	
89			4.6	12.6	
90			5.4	11.8	
91			5.4	11.8	
92			5.5	11.7	
93			5.8	11.4	
94			6.0	11.2	

TRAVERSE TIE OF "FAMOSA" MON.

E NE COR. BLOCK No 28

Indexed

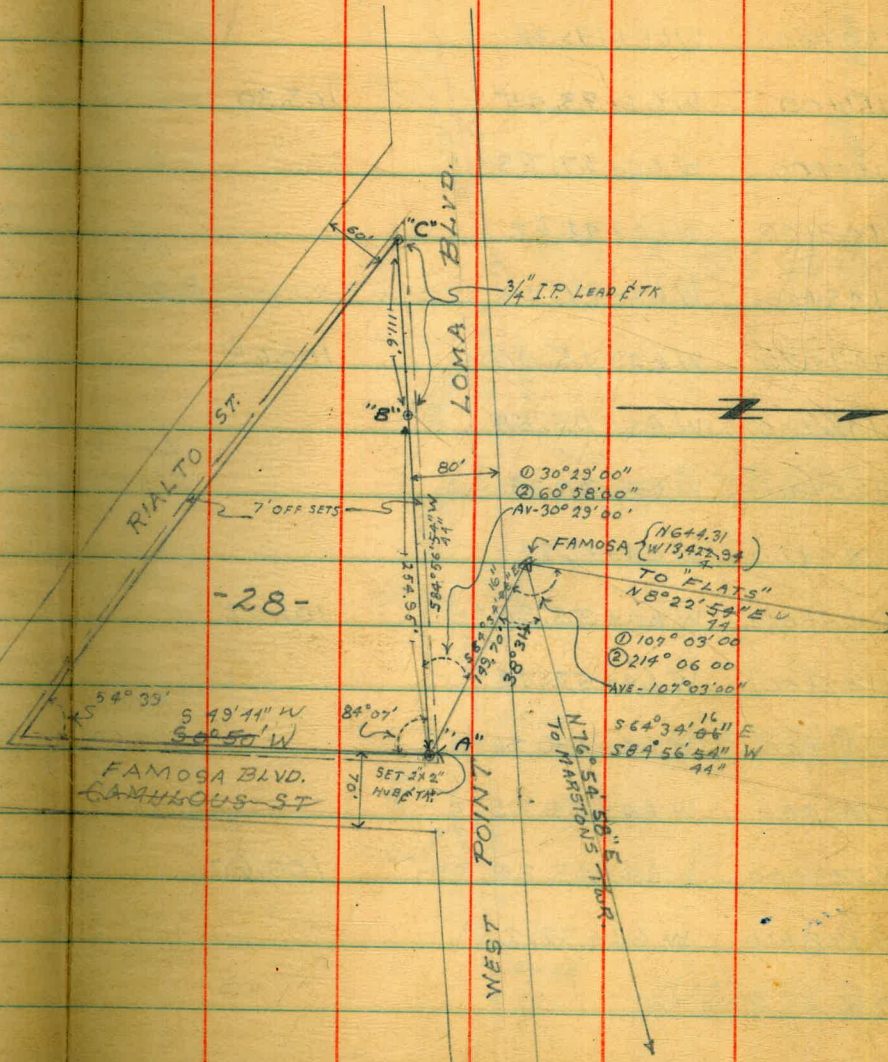
259.95
111.60
366.55

	N.	W.
FAMOSA	644.31	13,422.94
Pt. A	580.02	13,287.75
Pt. B	557.57	13,541.70
Pt. C	547.75	13,652.87

STA OBJECT ANGLE DIST. BEARING

CITY
"FAMOSA"
U.S.E.D
"FLATS"
① 107° 03' 00"
INT. RT.
(NE COR. BLK. 28)
② 214° 06' 00" 199.70' S 69° 31' 06" E
AVE. 107° 03' 00"

"FAMOSA"
① 30° 29' 00"
(NE COR. BLK. 28) INT. LEFT
② 60° 58' 00" 366.55' S 89° 56' 59" W
(NW COR. BLK. 28) AV. 30° 29' 00"



-28-

DE-ANZA POINT FILL AREA

PROJECT NO 3-1 BASELINE

8-20-47

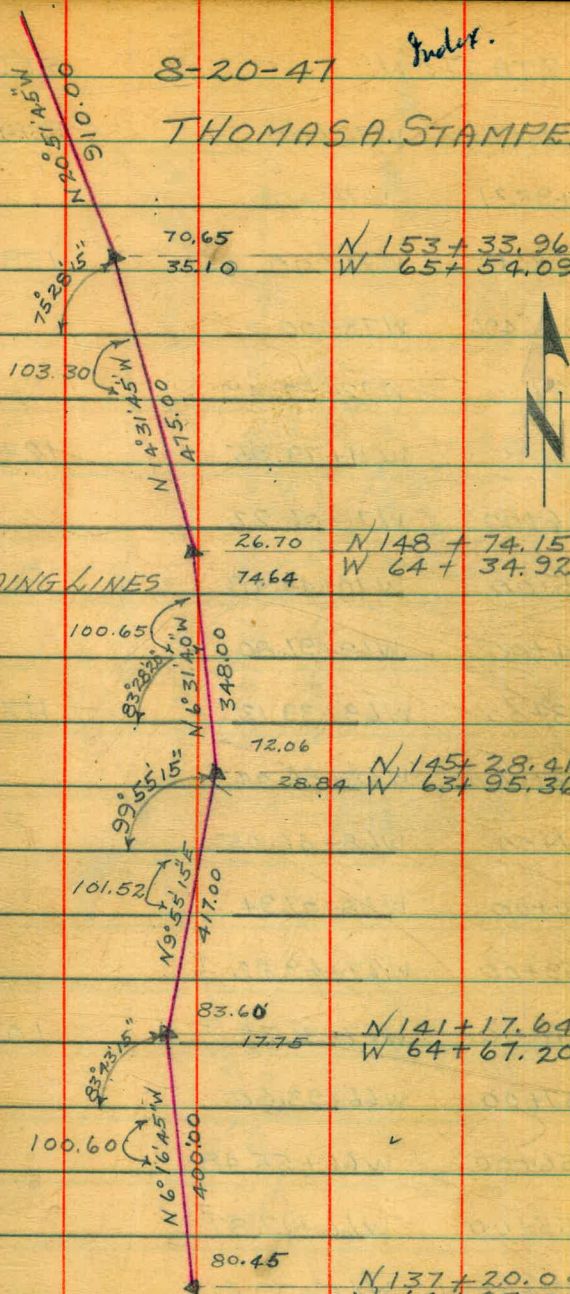
Index.

72

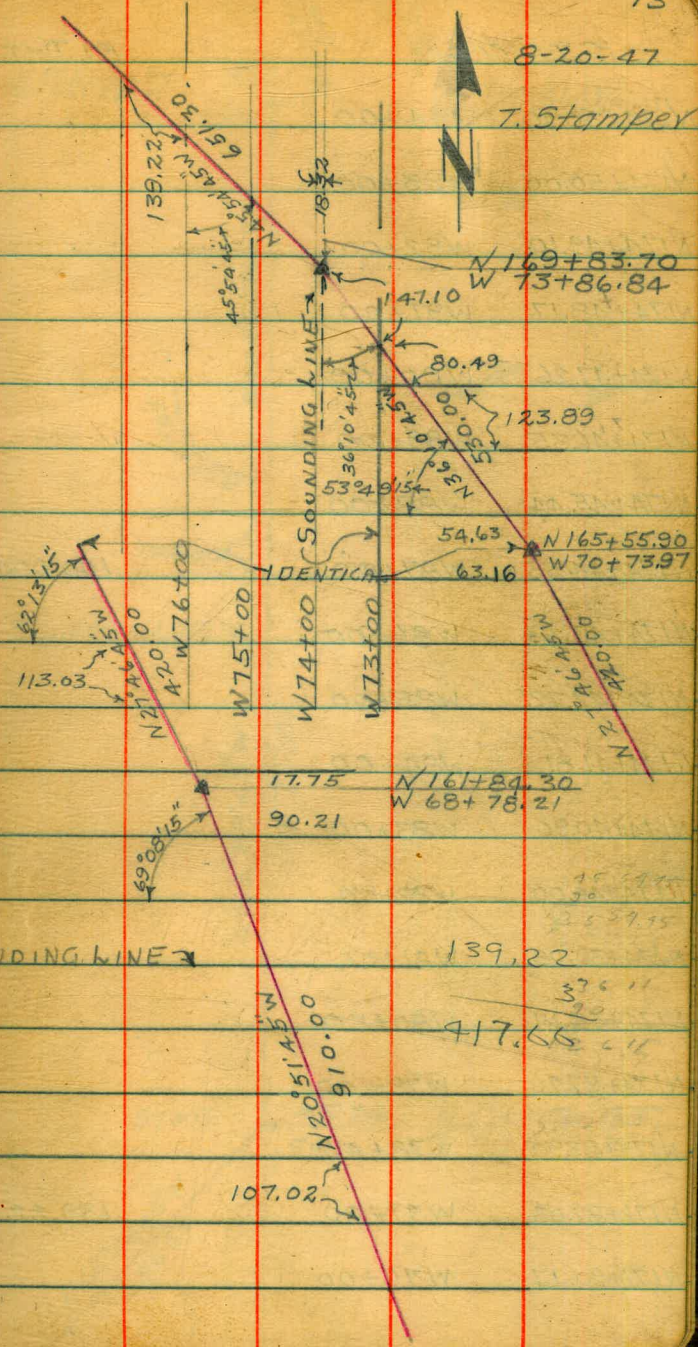
THOMAS A. STAMPER

STATION	B.L. DIST	DEF ANGLE LT.			
N153+00	W65+45.28	6°20'00"	1000'	70.65 35.10	N 153+33.96 W 65+54.09
N152+00	W65+19.36		1100'		
N151+00	W64+93.45	103.30	1200'		
N150+00	W64+67.53		1360'		
N149+00	W64+41.62				
N148+00	W64+26.43	LT. 8°00'05"		26.70 74.64	N 148+74.15 W 64+34.92
N147+00	W64+15.00	100.65			
N146+00	W64+03.55				
N145+00	W64+00.32	LT. 16°26'55"			
N144+00	W64+17.81				
N143+00	W64+35.30	101.52			
N142+00	W64+52.79				
N141+00	W64+65.26	RT. 16'12'00"		83.60 17.75	N 141+17.64 W 64+67.20
N140+00	W64+54.25				
N139+00	W64+43.25	100.60			
N138+00	W64+32.25			80.45	N 137+20.04 W 64+23.45

GRID SOUNDING LINES



STATION	B.L. DIST	DEF. ANGLE	
N171+90.17	W76+00	PER 100'	1000'
N170+93.31	W75+00		1100'
N169+96.44	W74+00	139.22	750'
N168+64.96	W73+00	LT. 9°44'00"	570'
N168+00	W72+52.49		50'
N167+00	W71+79.35	123.89	121'
N166+00	W71+06.22		194'
N165+00	W70+44.48	LT. 8°24'00"	2.56'
N164+00	W69+91.80		310'
N163+00	W69+39.12	113.03	560'
N162+00	W68+86.44		610'
N161+00	W68+46.05	LT. 6°55'00"	660'
N160+00	W68+07.94		670'
N159+00	W67+69.82		680'
N158+00	W67+31.71	107.02	710'
N157+00	W66+93.60		750'
N156+00	W66+55.48		800'
N155+00	W66+17.37		860'
N154+00	W65+79.26		930'



8-20-47

T. Stamper

IDENTICAL

680 SOUNDING LINE

139.22

417.65

8-20-47

STATION		B.L. DIST.	DEF. ANGLE
N174+50.90	W94+00		LT-89°51'30"
N174+50.00	W93+00		RT-74°57'30"
N174+49.10	W92+00		
N174+48.17	W91+00		
N174+47.26	W90+00		
N174+46.35	W89+00		
N174+45.44	W88+00		
N174+44.53	W87+00	100.004	
N174+43.63	W86+00		
N174+42.72	W85+00		
N174+41.81	W84+00		
N174+40.90	W83+00		
N174+40.00	W82+00		
N174+39.08	W81+00		
N174+38.17	W80+00		
N174+37.26	W79+00		
N173+83.90	W78+00		LT. 43°34'00"
N172+87.03	W77+00	139.22	
N171+90.17	W76+00		

2400'
2300'
2200'
2200'
2200'
2200'
2200'
2200'
2200'
2200'
2100'
2000'
2000'
1900'
1800'
1700'
1600'
950'
1000'
1000'

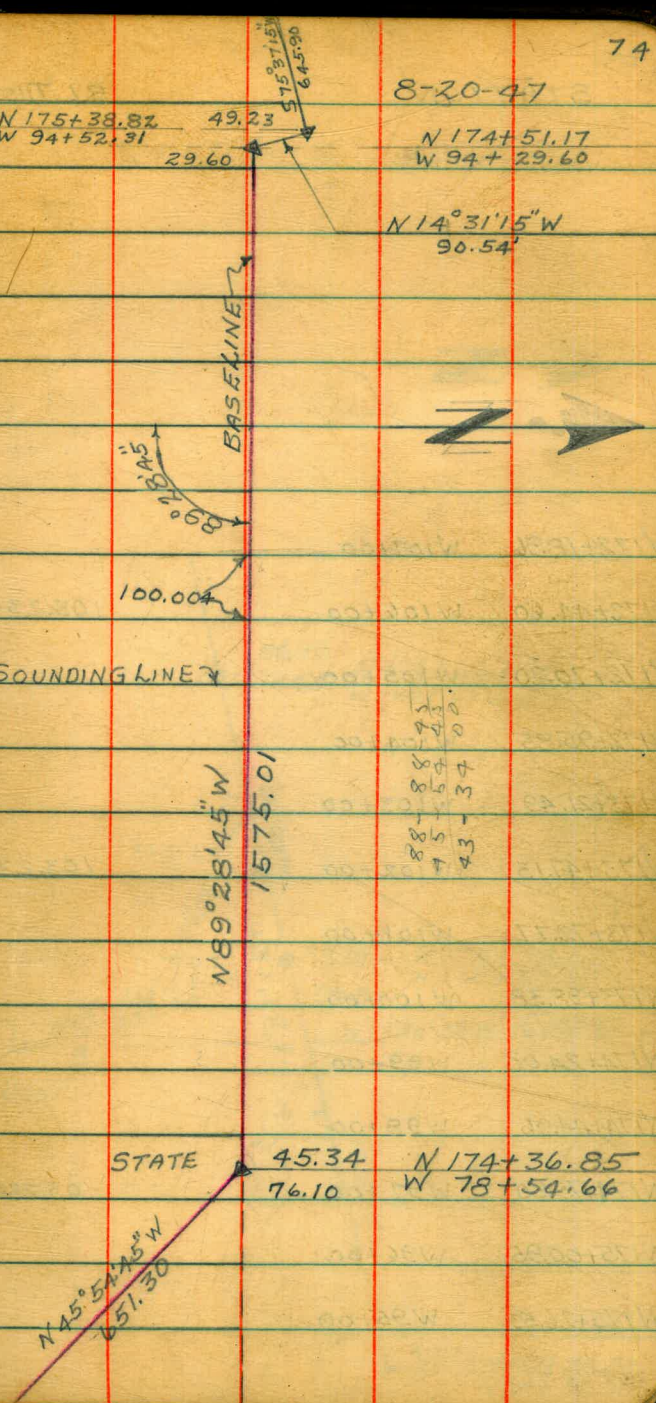
N 175+38.82
W 94+52.31

STATE 45.34
76.10

N 174+51.17
W 94+29.60

N 14°31'15" W
90.54'

88-88-93
75-59-73
43-34-00



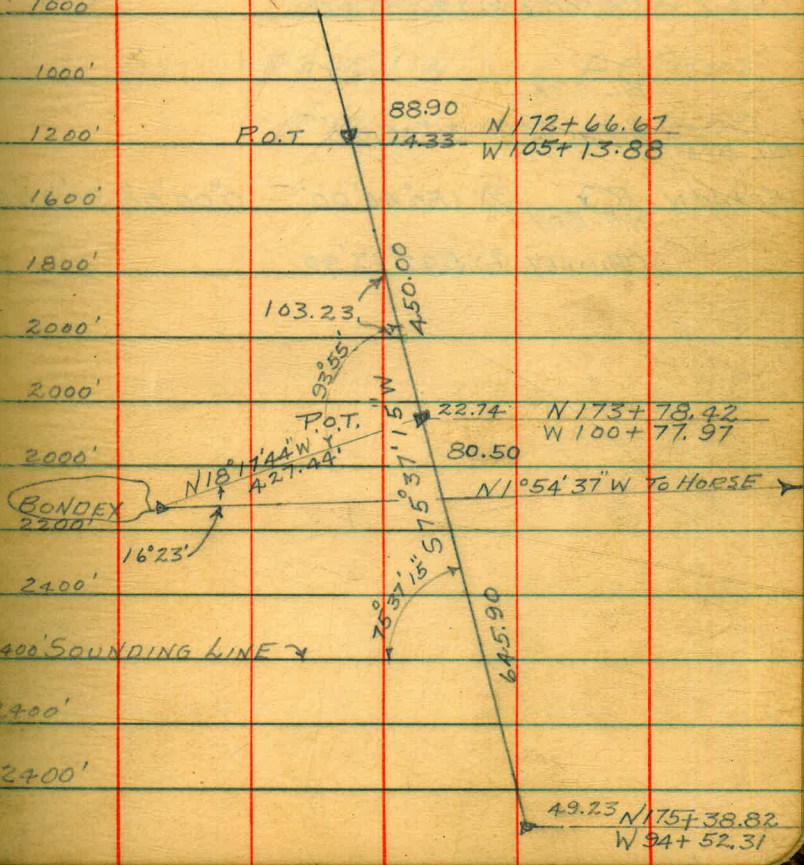
STATION

B.L. DIST DEF. ANGLE

8-21-47



N172+18.96	W107+00		1000'
N172+44.60	W106+00	103.234	1000'
N172+70.20	W105+00		1200'
N172+95.85	W104+00		1600'
N173+21.49	W103+00		1800'
N173+47.13	W102+00	103.234	2000'
N173+72.77	W101+00		2000'
N173+98.38	W100+00		2000'
N174+24.02	W99+00		2400'
N174+44.96	W98+00		2400'
N174+75.30	W97+00	103.234	2400' SOUNDING LINE
N175+00.95	W96+00		2400'
N175+26.59	W95+00		2400'



LOCATION OF SEXTANT
POINT CHIMNEY BACK BAY
AREA

STA	OBJECT	SIX ANGLES	VERNIER	MEAN
	N.E. BAY			
B/L STA	CHIMNEY	①	21°45'30"	
91+00 W	R ₂	②	43°31'00"	0°00'00" 21°45'30"
B/L STA.				
150+00 N		③	130°33'00"	
B/L STA.				
B/L STA.	91+00 W	④	90°22'30"	
150+00 N	R ₂	⑤	180°46'00"	0°00'00" 90°22'55"
	N.E. BAY			
	CHIMNEY	⑥	542'17'30"	

11-4-47

T. STAMPER
E. WATSON

76

Indexed

STATION CHIMNEY IS THE
E. OF A CHIMNEY APPROX.
1,000' EAST OF PACIFIC HI-WAY
ON THE WLY. RIDGE OF
BACK BAY AREA A LONE
RANCH HOUSE APPROX.
N 16,000' & W 6,000'

MISSION BAY
YACHT CLUB LEASE AREA
ELCARMEL POINT

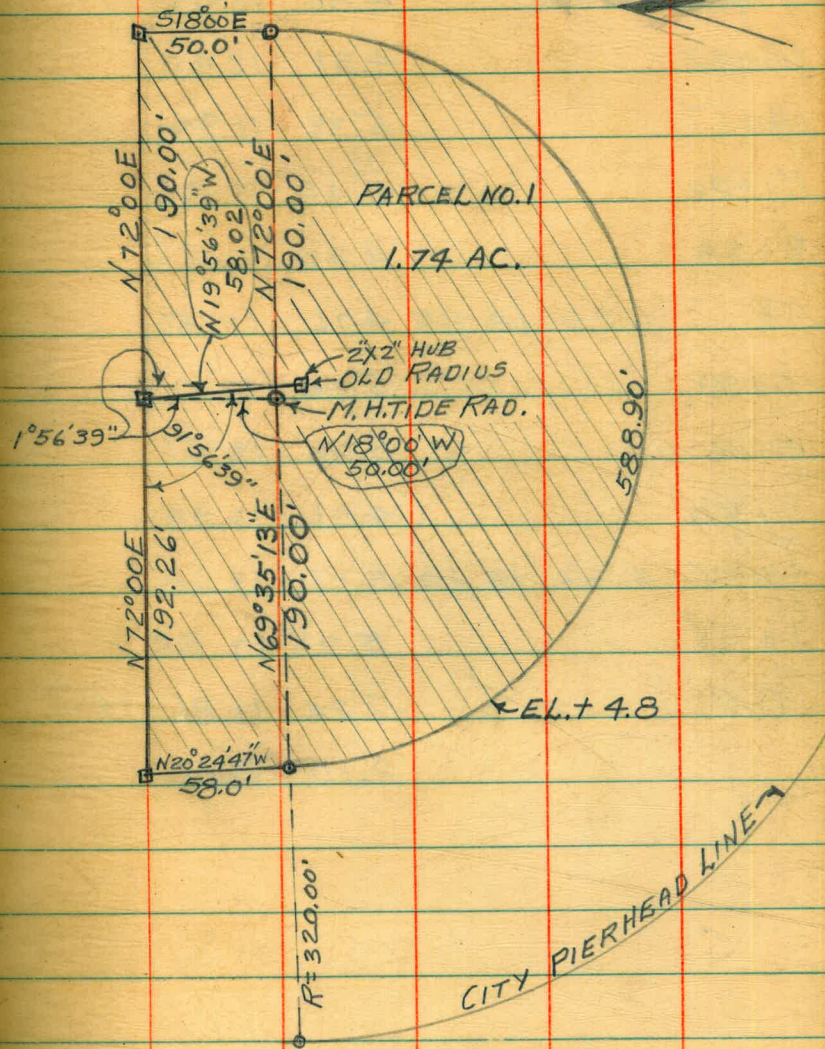
NORTH
OLD RADIUS \swarrow 2x2 HUB \rightarrow N18°00'W

4-22-48

T.A. STAMPER

77

Indexed



PROFILE ALONG E. SIDE OF
 PACIFIC HI-WAY ADJACENT TO PRDS #3.1
 STA H.I. - ELEV.

6-18-48

Index 78

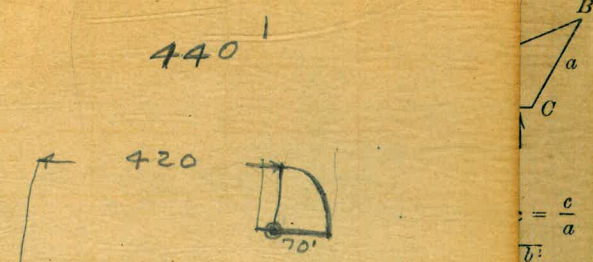
TBM	6.05	17.32		11.27
17+51			4.86	12.46
16+42			4.91	12.41
14+17			5.38	11.94
12+00			5.46	11.86
9+33			4.80	12.52
TP.	6.29	18.85	4.76	12.56
6+99			5.87	13.01
5+06			5.34	13.51
2+50			4.91	13.94
TP. 1+58	5.42	19.10	5.17	13.68
1+58			5.25	13.85
B.M.			7.24	11.86
			2.10	17.00

2X2 STA 16+42

T.A. STAMPER
 E.F. WATSON
 A.E. SHERBY

STATE

77			N 400
78		99	N 400
79	T. & 101	100	N 400
80		101	
81	S 1200	102	
82	S 1100	103	
83	S 1050	104	N 400
84	S 1050	105	
85	S 850	106	
86	S 750	107	S 50
87	S 650	108	N 400
88	N 100		S 100
88	S 500	109	N 400
89	N 200		S 150
89	S 300	110	N 400
90	N 200		S 150
90	S 250	111	N 400
91	N 300		S 200
91	S 550	112	N 400
92	N 300		S 200
92	S 600	113	N 400
93	N 300		S 200
93	N 400	114	N 400
94	N 400		S 300
94	N 400	115	N 400
95	N 400		S 550
96	N 400		
97	N 400		
98	N 400		

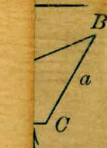


420
 103.23
 83.84
 19.39
 103.23 50'

5.8122
 103.23 / 600,000,000
 51615

110 + 83.84
 43850
 82584
 12660
 10323
 23970
 20696
 27270

103.23
 5.8122
 20696
 20696
 10323
 82584
 83893.906



$$\frac{c}{a} = \frac{c}{a}$$

$$\frac{b^2}{a^2} = \frac{a^2}{c^2}$$

C
 A
 +B)
 +B)

by the
 19.4 ft.
 10' =
 slope
 h the
 follow-
 = .0041.
 e dist-
 = 14 ft.,
 ft.

BOND 8.804
 MORENA-18.941

150
 3 60
 99-48=30
 4) 459 46-30
 76-37-45

275.00
 50.30
 110.04
 471.34
 325.30

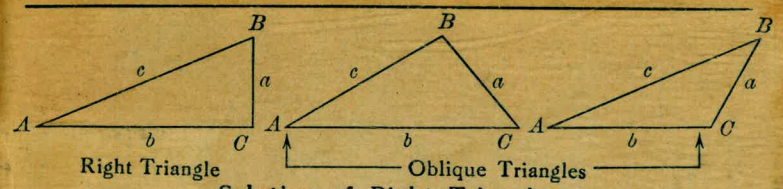
1004
 15
 20 6 258 05 300
 4300
 1000 6 258 04 95 325.30
 50.30
 275.00

342 07
 57 01
 359 60
 196-29
 163 36
 200.00
 103.23
 96.77
 179-60
 93.53
 86-05

102-362
 101-405
 100-409
 99-410
 98-453
 97-495

103.23
 619.38

TRIGONOMETRIC FORMULÆ



Solution of Right Triangles

For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{b}$, $\text{cosec} = \frac{c}{a}$

Given	Required	Formulas
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B$, $c = \sqrt{a^2 + b^2} = a \sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B$, $b = \sqrt{(c+a)(c-a)} = c \sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90^\circ - A$, $b = a \cot A$, $c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90^\circ - A$, $a = b \tan A$, $c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90^\circ - A$, $a = c \sin A$, $b = c \cos A$

Solution of Oblique Triangles

Given	Required	Formulas
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}$, $C = 180^\circ - (A + B)$, $c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180^\circ - C$, $\tan \frac{1}{2}(A - B) = \frac{(a - b) \tan \frac{1}{2}(A + B)}{a + b}$ $c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a + b + c}{2}$, $\sin \frac{1}{2}A = \sqrt{\frac{(s - b)(s - c)}{bc}}$ $\sin \frac{1}{2}B = \sqrt{\frac{(s - a)(s - c)}{ac}}$, $C = 180^\circ - (A + B)$
a, b, c	Area	$s = \frac{a + b + c}{2}$, $\text{area} = \sqrt{s(s - a)(s - b)(s - c)}$
A, b, c	Area	$\text{area} = \frac{bc \sin A}{2}$
A, B, C, a	Area	$\text{area} = \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL



Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10'. From Table, Page IX. $\cos 5^\circ 10' = .9959$. Horizontal distance = $319.4 \times .9959 = 318.09$ ft.
 Horizontal distance also = Slope distance minus slope distance times (1 - cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. $\text{Cosine } 5^\circ 10' = .9959$. $1 - .9959 = .0041$. $319.4 \times .0041 = 1.31$. $319.4 - 1.31 = 318.09$ ft.
 When the rise is known, the horizontal distance is approximately: - the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft. slope distance = 302.6 ft. Horizontal distance = $302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.